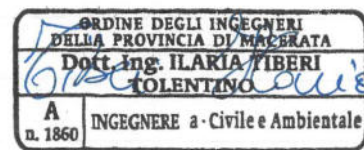




COMUNE
DI
PETRIOLO



PROGETTO DEFINITIVO

LOCALITA': PETRIOLO

OGGETTO: SCUOLA DELL'INFANZIA "PIETRO E SOFIA SAVINI"

AMPLIAMENTO

FASCICOLO DEI CALCOLI

SCALA nessuna

DATA NOVEMBRE 2020

AGG.TI

TAV. N°

S2

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Modellazione

La struttura è costituita da diversi elementi distinti, in base alla loro funzione, in:

- Fondazione in c.a. costituita da: graticcio di travi, platea
- Travi in c.a., acciaio, legno
- Pannelli XLAM
- Solaio per Copertura in legno_D

I livelli di sicurezza scelti dal Committente e dal Progettista in funzione del tipo e dell'uso della struttura, nonché in funzione delle conseguenze del danno, con riguardo a persone, beni, e possibile turbativa sociale, compreso il costo delle opere necessarie per la riduzione del rischio di danno o di collasso, hanno indirizzato al progetto di una struttura con i seguenti requisiti:

- sicurezza nei confronti degli Stati Limite Ultimi (SLU);
- sicurezza nei confronti degli Stati Limite di Esercizio (SLE).

La struttura è stata schematizzata attraverso un modello spaziale agli elementi finiti che tenga conto dell'effettivo stato deformativo e di sollecitazione, secondo l'effettiva realizzazione.

I vincoli esterni della struttura sono stati caratterizzati, a seconda della presenza degli elementi di fondazione, con: travi winkler, plinti diretti, plinti su pali, platee, ovvero con vincoli perfetti di incastro, appoggio, carrello, ecc.

I vincoli interni sono stati schematizzati secondo le sollecitazioni mutuamente scambiate tra gli elementi strutturali, inserendo, ove opportuno, il rilascio di alcune caratteristiche della sollecitazione per schematizzare il comportamento di vincoli interni non iperstatici (cerniere, carrelli, ecc.).

Il modello agli elementi finiti è stato calcolato tenendo conto dell'interazione tra strutture in fondazione e strutture in elevazione, consentendo un'accurata distribuzione delle azioni statiche e sismiche; il calcolo è stato eseguito considerando che la struttura abbia un comportamento elastico lineare.

I solai sono schematizzati come aree di carico, sulle quali vengono definiti i carichi permanenti (QP Solai), i carichi fissi (QFissi Solai) e i carichi variabili (QV solai); tali carichi sono assegnati alle aste in modo automatico in relazione all'influenza delle diverse aree di carico. Le masse corrispondenti ai carichi variabili sui solai nelle combinazioni sismiche sono state trattate in maniera automatica mediante un coefficiente moltiplicativo, definito in funzione della tipologia del solaio.

Il modello utilizzato è stato valutato alla luce dei diversi scenari di carico a cui la struttura è sottoposta durante la sua costruzione e la sua vita, al fine di garantire la sicurezza e la durabilità della stessa. Per la tipologia strutturale affrontata non è stato necessario definire scenari di contingenza; pertanto non si è tenuto conto delle fasi costruttive della struttura e, inoltre, si ritiene che non ci siano variazioni del modello di calcolo e degli schemi di vincolo, durante la vita dell'opera. Per il dettaglio degli scenari di calcolo si faccia riferimento alla "Relazione di Calcolo".

Il progetto e la verifica degli elementi strutturali è stato effettuato seguendo la teoria degli Stati limite. I parametri relativi alle verifiche effettuate sono riportati nella Relazione di Calcolo.

Il solutore agli elementi finiti impiegato nell'analisi è SpaceSolver, per il calcolo di strutture piane e spaziali schematizzabili da un insieme di elementi finiti tipo:

- BEAM
- PLATE-SHELL
- WINK
- BOUNDARY

Questi elementi interagiscono tra loro attraverso i nodi, con la possibilità di tenere in conto tutti i possibili disassamenti, mediante l'introduzione di concetti rigidi e traslazioni degli elementi bidimensionali. Il solutore lavora in campo elastico lineare, si basa sulle routines di Matlab ed è stato sviluppato in collaborazione con l'Università di Roma – Tor Vergata. Il solutore offre la possibilità di risolvere anche travi su suolo alla Winkler con molle spalmate sull'intera suola, anziché sul solo asse, plinti diretti e su pali, pali singoli, platee, piastre sottili e spesse, con controllo delle rotazioni attorno all'asse normale alla piastra (drilling). Inoltre, per gli elementi BEAM l'equilibrio è scritto rispetto alla linea dei centri di taglio anziché rispetto alla linea dei baricentri. L'affidabilità del solutore è stata testata su una serie di esempi campioni calcolati con altri procedimenti o con formule note, di cui si rende disponibile la documentazione.

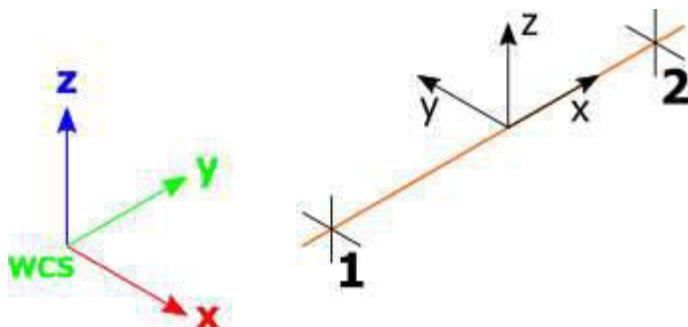
Affidabilità dei codici utilizzati

Il programma è dotato di una serie di filtri di auto diagnostica che segnalano i seguenti eventi:

- labilità della struttura;
- assenza di masse;
- nodi collegati ad aste nulle;
- mancanza di terreno sugli elementi in fondazione;
- controllo sull'assegnazione dei nodi all'impalcato;
- correttezza degli spettri di progetto;
- fattori di partecipazione modali;
- assegnazione dei criteri di verifica agli elementi;
- numerazione degli elementi strutturali;
- congruenza delle connessioni tra elementi shell;
- congruenza delle aree di carico;
- definizione delle caratteristiche d'inerzia delle sezioni;
- presenza del magrone sotto la travi tipo wink;
- elementi non verificati per semi progetto allo SLU, con inserimento automatico delle armature secondo i criteri di verifica;
- elementi non verificati allo SLU per armature già inserite nell'elemento strutturale;
- elementi non verificati allo SLE per armature già inserite nell'elemento strutturale.

Presentazione dei risultati

I disegni dello schema statico adottato sono riportati nel fascicolo allegato alla presente relazione. E' stato impiegato il Sistema Internazionale per le unità di misura, con riferimento al daN per le forze.



Il sistema di riferimento globale rispetto al quale è stata riferita l'intera struttura è una terna di assi cartesiani sinistrorsa OXYZ (X,Y, e Z sono disposti e orientati rispettivamente secondo il pollice, l'indice ed il medio della mano destra, una volta posizionati questi ultimi a 90° tra loro). La terna di riferimento locale per un'asta è anch'essa una terna sinistrorsa O'xyz che ha l'asse x orientato dal nodo iniziale I dell'asta verso il nodo finale J e gli assi y e z diretti secondo gli assi geometrici della sezione, con l'asse y orizzontale e orientato in modo da portarsi a coincidere con l'asse x a mezzo di una rotazione oraria di 90° e l'asse z di conseguenza.

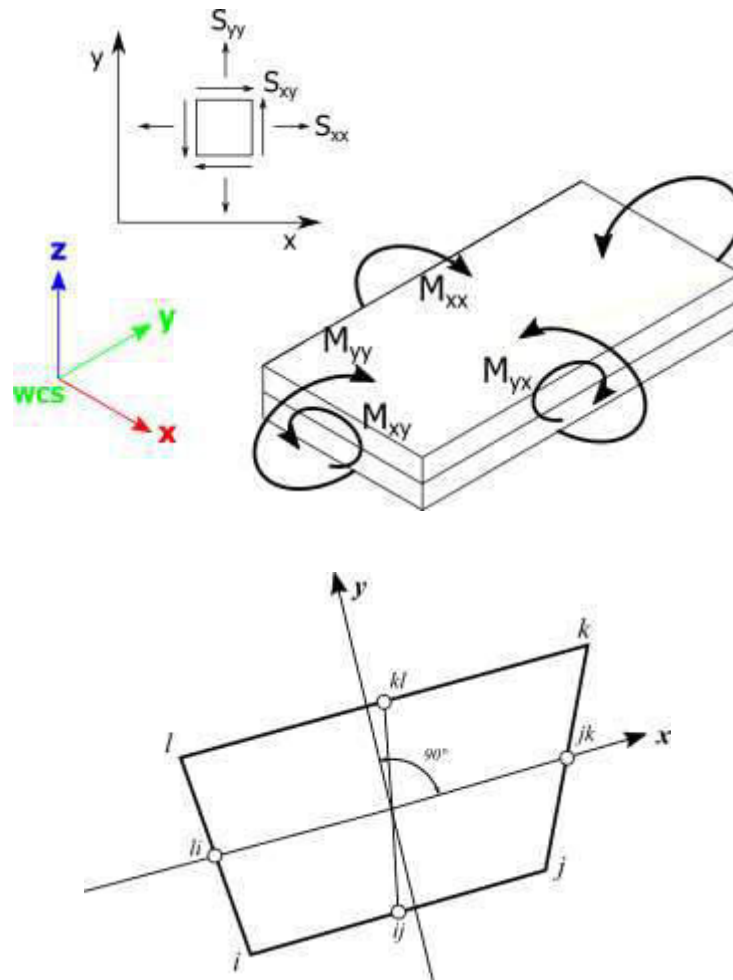
Per un'asta comunque disposta nello spazio la sua terna locale è orientata in modo tale da portarsi a coincidere con la terna globale a mezzo di rotazioni orarie degli assi locali inferiori a 180°.

- Le forze, sia sulle aste che sulle pareti o lastre, sono positive se opposte agli assi locali.
- Le forze nodali sono positive se opposte agli assi globali.
- Le coppie sono positive se sinistrorse.

Le caratteristiche di sollecitazione sono positive se sulla faccia di normale positiva sono rappresentate da vettori equiversi agli assi di riferimento locali; in particolare il vettore momento positivo rappresenta una coppia che ruota come le dita della mano destra che si chiudono quando il pollice è equiverso all'asse locale.

- Le traslazioni sono positive se concordi con gli assi globali.
- Le rotazioni sono positive se sinistrorse.

Il sistema di riferimento locale per gli elementi bidimensionali è quello riportato nelle figure seguenti.



La terna locale per l'elemento shell è costituita dall'asse x locale che va dal nodo li al nodo jk, l'asse y è diretto secondo il piano dell'elemento e orientato verso il nodo i e l'asse z, di conseguenza, è orientato in modo da formare la solita terna sinistrorsa. L'asse z locale rappresenta la normale positiva all'elemento.

Le sollecitazioni dell'elemento sono:

- Sforzi membranali
 - $S_{xx} = \sigma_x$
 - $S_{yy} = \sigma_y$
 - $S_{xy} = \tau_{xy}$
- Sforzi flessionali (momenti)
 - M_{xx} , momento che genera σ_x (intorno ad y)
 - M_{yy} , momento che genera σ_y (intorno a x)
 - M_{xy} , momento torcente che genera τ_{xy}

Le sollecitazioni principali dell'elemento sono:

$$M_{1,2} = \frac{M_{xx} + M_{yy}}{2} \pm \sqrt{\left(\frac{M_{xx} - M_{yy}}{2}\right)^2 + M_{xy}^2}$$

$$S_{1,2} = \frac{S_{xx} + S_{yy}}{2} \pm \sqrt{\left(\frac{S_{xx} - S_{yy}}{2}\right)^2 + S_{xy}^2}$$

$$\tan 2\theta = \frac{M_{xy}}{M_{xx} - M_{yy}} \quad \tan 2\psi = \frac{S_{xy}}{S_{xx} - S_{yy}}$$

dove θ è l'angolo formato dagli assi principali di M_1 e M_2 con quelli di riferimento e ψ è l'angolo formato dagli

assi principali di S_1 e S_2 con quelli di riferimento. L'elemento shell usato come piastra fornisce i momenti flettenti e non i tagli in direzione ortogonale all'elemento, che possono ottenersi come derivazione dei momenti flettenti;

$$\tau_{zx} = M_{xx,x} + M_{xy,y}$$

$$\tau_{zy} = M_{xy,y} + M_{yy,y}$$

Quando invece viene usato come lastra ci restituisce valori di σ e τ costanti, non adatti a rappresentare momenti flettenti, ma solo sforzi normali e tagli nel piano della lastra.

I tabulati di calcolo contengono due sezioni principali: la descrizione del modello di calcolo e la presentazione dei risultati.

La descrizione del modello di calcolo contiene:

- i dati generali (dimensioni);
- le coordinate nodali;
- i vincoli dei nodi e i vincoli interni delle aste, con le eventuali sconnessioni;
- le caratteristiche sezionali;
- le caratteristiche dei solai;
- le caratteristiche delle aste;
- i carichi sulle aste, sui nodi e sui muri (inclusa la distribuzione delle distorsioni impresse, e delle variazioni e dei gradienti di temperatura);
- configurazione di sistemi che introducono stati coattivi;
- le caratteristiche dei materiali;
- legami costitutivi e criteri di verifica;
- le condizioni di carico.

La stampa dei risultati contiene:

- le combinazioni dei carichi;
- le forze sismiche agenti sulla struttura;
- gli spostamenti d'impalcato, se l'impalcato è rigido;
- gli spostamenti nodali;
- le sollecitazioni sulle membrature per ogni combinazione di carico;
- la sollecitazione sul terreno sotto travi di fondazione o platee;
- deformate;
- diagrammi sollecitazioni.

Tabulati di input

Dati generali

Nome struttura	
Numero di frequenze	15
% Filtro masse libere	0.1
% Coefficiente di smorzamento viscoso	5
Spostamenti modali con segno	Si
Deformabilità a taglio delle aste	Si
Spostamento ammissibile impalcato	0.0050*h

Impalcato

N°	Quota mm	Rigido mm	Incr.Soll.Pil	Inc.Soll.Par.
0	0	No	1.000	1.000
1	3870	Si	1.000	1.000

Percentuali Spostamento masse impalcato

Posizione	% Spostamento direzione X	% Spostamento direzione Y
1	0	-5
2	5	0
3	0	5
4	-5	0

Combinazioni del Sisma in X e Y e Verticale

Comb.	Pos. SismaX	Pos. SismaY	Fx	Fy	Fz
1	1	2	1	0.3	0
2	1	2	0.3	1	0
3	1	4	1	0.3	0
4	1	4	0.3	1	0
5	3	2	1	0.3	0
6	3	2	0.3	1	0
7	3	4	1	0.3	0
8	3	4	0.3	1	0

Comb.	Numero di combinazione dei sismi
Pos. SismaX	Posizione in cui viene scelto il sisma in direzione X
Pos. SismaY	Posizione in cui viene scelto il sisma in direzione Y
Fx	Fattore con cui il sisma X partecipa
Fy	Fattore con cui il sisma Y partecipa
Fz	Fattore con cui il sisma Verticale partecipa (quando richiesto)

Ogni combinazione genera al massimo 8 sotto-combinazioni in base a tutte le combinazioni possibili dei segni di Fx ed Fy ed Fz.

Spettri di risposta

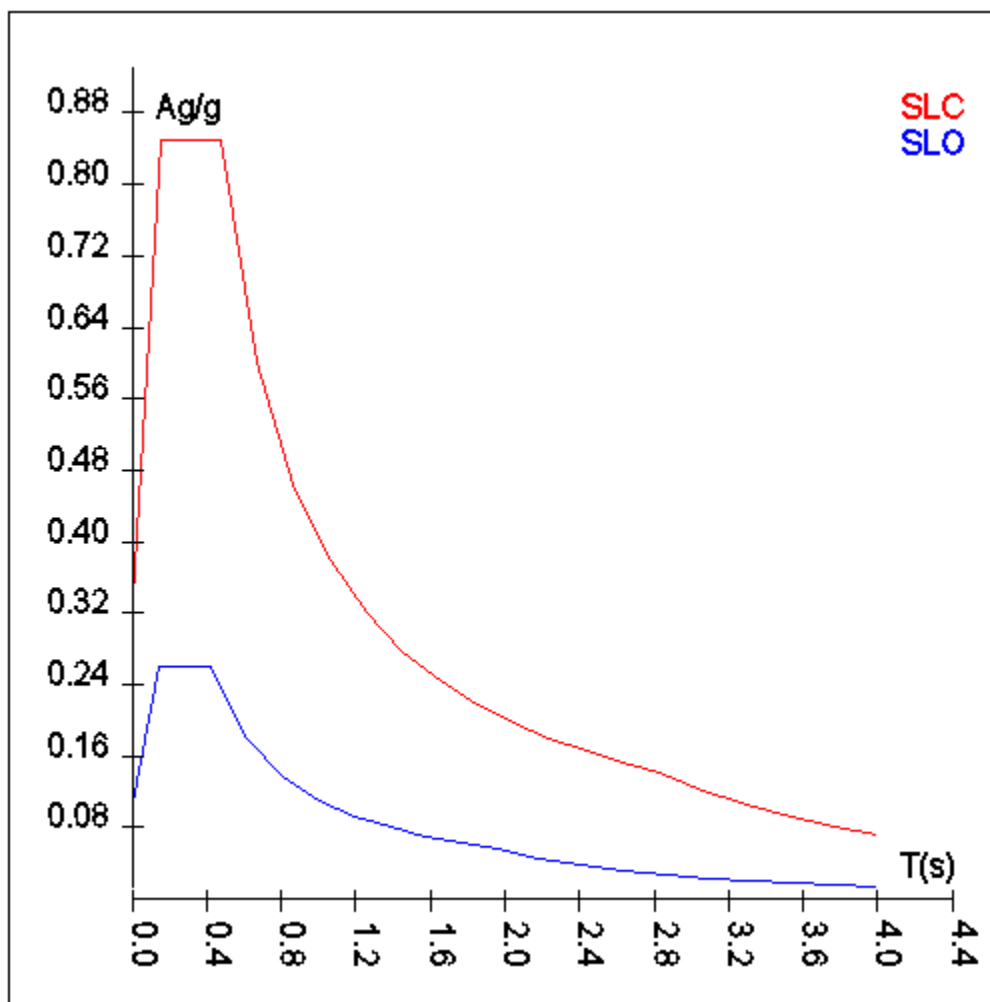
Spettro: **SpettroNT_2018**

Il calcolo degli spettri e del fattore di comportamento sono stati calcolati per la seguente tipologia di terreno e struttura.

Vita della struttura	
Tipo	Grandi opere imp. strategica (>100)
Vita nominale VN [anni]	100.0
Classe d'uso	III
Coefficiente d'uso CU	1.500
Periodo di riferimento VR [anni]	150.000
Probabilità di superamento PVR allo Stato limite di esercizio - SLO	81.0%
Probabilità di superamento PVR allo Stato limite ultimo - SLC	5.0%
Periodo di ritorno TR SLO [anni]	90.3
Periodo di ritorno TR SLC [anni]	2475.0
Parametri del sito	
Comune	Petriolo - (MC)
Longitudine	13.465
Latitudine	43.223
Id reticolo del sito	22533-22532-22754-22755
Valori di riferimento del sito	
Accelerazione orizzontale massima del sito Ag/g - SLO (TR=90.3)	0.0891
Fattore di amplificazione dello spettro Fo - SLO (TR=90.3)	2.4299
Periodo di riferimento di inizio del tratto a velocità costante T*C [s] - SLO (TR=90.3)	0.307
Accelerazione orizzontale massima del sito Ag/g - SLC (TR=2475.0)	0.3073
Fattore di amplificazione dello spettro Fo - SLC (TR=2475.0)	2.5383
Periodo di riferimento di inizio del tratto a velocità costante T*C [s] - SLC (TR=2475.0)	0.350
Coefficiente Amplificazione Topografica St	1.000
Categoria terreno	B
Stato limite SLC	
Coefficiente di amplificazione stratigrafica Ss	1.09

Periodo di inizio del tratto ad accelerazione costante dello spettro TB [s]	0.16
Periodo di inizio del tratto a velocità costante dello spettro TC [s]	0.47
Periodo di inizio del tratto a spostamento costante dello spettro TD [s]	2.83
Stato limite SLO	
Coefficiente di amplificazione stratigrafica Ss	1.20
Periodo di inizio del tratto ad accelerazione costante dello spettro TB [s]	0.14
Periodo di inizio del tratto a velocità costante dello spettro TC [s]	0.43
Periodo di inizio del tratto a spostamento costante dello spettro TD [s]	1.96
Fattore di comportamento (SLC)	
Classe duttilità	B
Fattore per spettro elastico	1.000
Fattore di comportamento SLO (spettro elastico)	
q	1.000

T SLC [s]	Sd SLC[a/g]	T SLO [s]	Sd SLO[a/g]
0.00000	0.33435	0.00000	0.10688
0.15832	0.84869	0.14243	0.25971
0.47495	0.84869	0.42729	0.25971
0.67114	0.60060	0.61841	0.17945
0.86734	0.46474	0.80953	0.13708
1.06353	0.37901	1.00066	0.11090
1.25972	0.31998	1.19178	0.09311
1.45592	0.27686	1.38290	0.08025
1.65211	0.24398	1.57402	0.07050
1.84830	0.21808	1.76515	0.06287
2.04450	0.19716	1.95627	0.05673
2.24069	0.17989	2.18335	0.04554
2.43689	0.16541	2.41043	0.03736
2.63308	0.15309	2.63751	0.03121
2.82927	0.14247	2.86459	0.02646
3.06342	0.12152	3.09167	0.02271
3.29756	0.10488	3.31876	0.01971
3.53171	0.09143	3.54584	0.01727
3.76585	0.08042	3.77292	0.01525
4.00000	0.07128	4.00000	0.01357



Caratteristiche del terreno

Strat o n°	Spessor e cm	γ kg/mc	γ_{Sat} kg/mc	ϕ °	Addensato	OCR	Coesione kg/cm ²	Cu kg/cm ²	E kg/cm ²	ν
Terreno1: Cost.Winkler=2.00 kg/cm ² - Falda assente										
1	100	1900	2000	15	No	--	0.06	0.00	2E02	0.30
2	1200	2000	2000	30	No	--	0.10	0.00	2E02	0.30

Materiali		
C25/30		
Peso specifico	kg/mc	2500
Modulo di Young E	kg/cm ²	3E05
Modulo di Poisson ν		0.13
Coefficiente di dilatazione termica λ	1/°C	1e-05
C30/37		
Peso specifico	kg/mc	2500
Modulo di Young E	kg/cm ²	3E05
Modulo di Poisson ν		0.13
Coefficiente di dilatazione termica λ	1/°C	1e-05
Acciaio		
Peso specifico	kg/mc	7850
Modulo di Young E	kg/cm ²	2E06
Modulo di Poisson ν		0.30
Coefficiente di dilatazione termica λ	1/°C	1.2e-05

Legno_isotropo		
Peso specifico	kg/mc	700
Modulo di Young E	kg/cm ²	1E05
Modulo di Poisson ν		0.30
Coefficiente di dilatazione termica λ	1/°C	5e-06
Pannello XLAM: Pannello XLAM 12		
Coefficiente di dilatazione termica λ	1/°C	5e-06
Peso specifico	kg/mc	350
Proprietà della piastra equivalente		
Spessore	cm	12
Modulo di Young Ex	kg/cm ²	9E04
Modulo di Young Ey	kg/cm ²	2E04
Modulo tangenziale Gxy	kg/cm ²	2E03
Modulo tangenziale Gxz	kg/cm ²	1E03
Modulo tangenziale Gyz	kg/cm ²	6E02
Proprietà della lastra equivalente		
Spessore	cm	12
Modulo di Young Ex	kg/cm ²	7E04
Modulo di Young Ey	kg/cm ²	5E04
Modulo tangenziale Gxy	kg/cm ²	3E03
Composizione strati		
N°	dir	Nome
1	0°	C24 L.C.
2	90°	C24 L.C.
3	0°	C24 L.C.
4	90°	C24 L.C.
5	0°	C24 L.C.

Nodi - Geometria e vincoli

Nodo	X	Y	Z	Tx	Ty	Tz	Rx	Ry	Rz	Impalcato
	Coordinate [mm]			Vincoli						
1	1050	20520	3870	0	0	0	0	0	0	1
1	11540	5170	2990	0	0	0	0	0	0	1
2	2670	21630	3870	0	0	0	0	0	0	1
2	13410	5910	2990	0	0	0	0	0	0	1
2	16974	8979	2200	0	0	0	0	0	0	1
2	17370	7048	2200	0	0	0	0	0	0	1
3	17609	5872	2200	0	0	0	0	0	0	1
3	15280	6650	2990	0	0	0	0	0	0	1
3	17215	7804	2200	0	0	0	0	0	0	1
3	4290	22730	3870	0	0	0	0	0	0	1
4	5910	23840	3870	0	0	0	0	0	0	1
4	13490	2330	2370	0	0	0	0	0	0	1
5	7530	24950	3870	0	0	0	0	0	0	1
5	15360	3070	2370	0	0	0	0	0	0	1
5	174	17670	0	1	1	0	0	0	1	0
6	11644	27253	2700	0	0	0	0	0	0	1
6	3660	13150	-0	1	1	0	0	0	1	0
6	17230	3810	2370	0	0	0	0	0	0	1
6	9140	26050	3870	0	0	0	0	0	0	1
7	12757	26805	2700	0	0	0	0	0	0	1
7	10760	27160	3870	0	0	0	0	0	0	1
7	480	20130	-0	1	1	0	0	0	1	0
8	5320	14280	3870	0	0	0	0	0	0	1
8	16390	11820	-0	1	1	0	0	0	1	0
9	6940	15390	3870	0	0	0	0	0	0	1
9	16974	8979	-0	1	1	0	0	0	1	0
10	11327	9822	2200	0	0	0	0	0	0	1
10	17215	7804	-0	1	1	0	0	0	1	0
10	8550	16490	3870	0	0	0	0	0	0	1
11	17290	7440	-0	1	1	0	0	0	1	0

Nodo	X	Y	Z	Tx	Ty	Tz	Rx	Ry	Rz	Impalcato
11	10170	17600	3870	0	0	0	0	0	0	1
11	13001	10483	2200	0	0	0	0	0	0	1
12	10230	4650	0	1	1	0	0	0	1	0
12	11790	18700	3870	0	0	0	0	0	0	1
13	13410	19810	3870	0	0	0	0	0	0	1
13	12360	1890	-0	1	1	0	0	0	1	0
14	13848	24303	2200	0	0	0	0	0	0	1
14	7420	8280	0	1	1	0	0	0	1	0
15	14088	23128	2200	0	0	0	0	0	0	1
15	11180	27440	-0	1	1	0	0	0	1	0
15	9000	8900	3870	0	0	0	0	0	0	1
16	10850	9650	3870	0	0	0	0	0	0	1
16	11644	27253	-0	1	1	0	0	0	1	0
17	12757	26805	-0	1	1	0	0	0	1	0
17	12730	10380	3870	0	0	0	0	0	0	1
18	14600	11110	3870	0	0	0	0	0	0	1
18	14290	22141	2200	0	0	0	0	0	0	1
18	13390	26550	-0	1	1	0	0	0	1	0
19	14490	21161	2200	0	0	0	0	0	0	1
19	11327	9822	0	1	1	0	0	0	1	0
20	13001	10483	0	1	1	0	0	0	1	0
21	14600	20620	-0	1	1	0	0	0	1	0
22	14759	19836	2200	0	0	0	0	0	0	1
22	13848	24303	-0	1	1	0	0	0	1	0
23	14088	23128	-0	1	1	0	0	0	1	0
23	15198	17680	2200	0	0	0	0	0	0	1
24	14290	22141	-0	1	1	0	0	0	1	0
25	14330	21940	3870	0	0	0	0	0	0	1
25	14490	21161	-0	1	1	0	0	0	1	0
26	15258	17386	2200	0	0	0	0	0	0	1
26	14759	19836	-0	1	1	0	0	0	1	0
26	15340	16980	3870	0	0	0	0	0	0	1
27	15198	17680	-0	1	1	0	0	0	1	0
27	15736	15034	2200	0	0	0	0	0	0	1
28	15258	17386	-0	1	1	0	0	0	1	0
29	15736	15034	-0	1	1	0	0	0	1	0
30	15796	14740	-0	1	1	0	0	0	1	0
30	15796	14740	2200	0	0	0	0	0	0	1
31	16274	12389	2200	0	0	0	0	0	0	1
31	16274	12389	-0	1	1	0	0	0	1	0
32	17370	7048	0	1	1	0	0	0	1	0
33	17609	5872	0	1	1	0	0	0	1	0
34	17970	4100	0	1	1	0	0	0	1	0
35	11625	5201	-0	1	1	0	0	0	1	0
36	12369	5495	-0	1	1	0	0	0	1	0
38	11625	5201	2100	0	0	0	0	0	0	1
39	12369	5495	2100	0	0	0	0	0	0	1
101	12360	1890	2370	0	0	0	0	0	0	1
102	10230	4650	2990	0	0	0	0	0	0	1
103	7420	8280	3870	0	0	0	0	0	0	1
104	3660	13150	3870	0	0	0	0	0	0	1
105	174	17670	3870	0	0	0	0	0	0	1
106	2260	12150	-0	1	1	0	0	0	1	0
106	480	20130	3870	0	0	0	0	0	0	1
107	11180	27440	3870	0	0	0	0	0	0	1
108	13390	26550	3870	0	0	0	0	0	0	1
109	14600	20620	3870	0	0	0	0	0	0	1
110	16390	11820	3870	0	0	0	0	0	0	1
111	17290	7440	2990	0	0	0	0	0	0	1
112	17970	4100	2370	0	0	0	0	0	0	1
112	8830	3650	0	1	1	0	0	0	1	0
113	12810	490	-0	1	1	0	0	0	1	0
114	6020	7280	0	1	1	0	0	0	1	0
134	18470	2600	0	1	1	0	0	0	1	0

Nodo	X	Y	Z	Tx	Ty	Tz	Rx	Ry	Rz	Impalcato
206	2260	12150	200	1	1	0	0	0	1	1
212	8830	3650	2500	1	1	0	0	0	1	1
213	12810	490	2500	1	1	0	0	0	1	1
213	11560	-10	-0	1	1	0	0	0	1	0
214	6020	7280	1500	1	1	0	0	0	1	1
234	18470	2600	2500	1	1	0	0	0	1	1
313	11560	-10	2500	1	1	0	0	0	1	0

Input - Aste - Tabella sezioni tipo

Tipo	Nome	Area	Ix	Iy	It	Fx	Fy	Lx	Lx
G		mq	m ⁴	m ⁴	m ⁴			cm	cm
	HE 260 B	0.0	1.492E-04	5.135E-05	1.238E-06	1.000	1.000	26	26

Tipo	Nome	Base	Altezza	Larg.mag.
R		cm	cm	cm
	12x20	12	20	0
	50x60	60	50	100
	trave 30x30	30	30	0

Aste - Geometria e vincoli

	Ni	Nf	Vinc.	Sez.	Mat.	Crit.pr.	Rot.	f.f.	xi	yi	zi	xf	yf	zf	Tipo	L2	L3
							°		cm							cm	
101	13	26	I-I	HE 260 B	Acciaio	Acciaio_P ressflessione	0	5050	0	0	0	0	0	0	Trave	343	343
101	6	13	CC-I	HE 260 B	Acciaio	Acciaio_P ressflessione	0	5050	0	0	0	0	0	0	Trave	756	756
102	12	110	I-I	HE 260 B	Acciaio	Acciaio_P ressflessione	0	5050	0	0	0	0	0	0	Trave	828	828
102	5	12	CC-I	HE 260 B	Acciaio	Acciaio_P ressflessione	0	5050	0	0	0	0	0	0	Trave	756	756
103	11	18	I-I	HE 260 B	Acciaio	Acciaio_P ressflessione	0	5050	0	0	0	0	0	0	Trave	786	786
103	4	11	CC-I	HE 260 B	Acciaio	Acciaio_P ressflessione	0	5050	0	0	0	0	0	0	Trave	756	756
104	3	6	I-CC	HE 260 B	Acciaio	Acciaio_P ressflessione	0	5050	0	0	0	0	0	0	Trave	350	350
104	17	3	I-I	HE 260 B	Acciaio	Acciaio_P ressflessione	0	5050	0	0	0	0	0	0	Trave	460	460
104	10	17	I-I	HE 260 B	Acciaio	Acciaio_P ressflessione	0	5050	0	0	0	0	0	0	Trave	740	740
104	3	10	CC-I	HE 260 B	Acciaio	Acciaio_P ressflessione	0	5050	0	0	0	0	0	0	Trave	756	756
105	2	5	I-CC	HE 260 B	Acciaio	Acciaio_P ressflessione	0	5050	0	0	0	0	0	0	Trave	350	350
105	16	2	I-I	HE 260 B	Acciaio	Acciaio_P ressflessione	0	5050	0	0	0	0	0	0	Trave	462	462
105	9	16	I-I	HE 260 B	Acciaio	Acciaio_P ressflessione	0	5050	0	0	0	0	0	0	Trave	695	695
105	2	9	CC-I	HE 260 B	Acciaio	Acciaio_P ressflessione	0	5050	0	0	0	0	0	0	Trave	756	756
106	1	4	I-CC	HE 260 B	Acciaio	Acciaio_P ressflessione	0	5050	0	0	0	0	0	0	Trave	350	350

	Ni	Nf	Vinc.	Sez.	Mat.	Crit.pr.	Rot.	f.f.	xi	yi	zi	xf	yf	zf	Tipo	L2	L3
106	15	1	I-I	HE 260 B	Acciaio	Acciaio_P ressflessi one	0	5050	0	0	0	0	0	0	Trave	460	460
106	8	15	I-I	HE 260 B	Acciaio	Acciaio_P ressflessi one	0	5050	0	0	0	0	0	0	Trave	652	652
106	1	8	CC-I	HE 260 B	Acciaio	Acciaio_P ressflessi one	0	5050	0	0	0	0	0	0	Trave	756	756
107	7	25	CC-I	HE 260 B	Acciaio	Acciaio_P ressflessi one	0	5050	0	0	0	0	0	0	Trave	632	632
108	102	1	I-I	12x20	Legno_is otroppo	Legno_Ar careccio	0	5050	0	0	0	0	0	0	Trave	141	141
108	1	2	I-I	12x20	Legno_is otroppo	Legno_Ar careccio	0	5050	0	0	0	0	0	0	Trave	201	201
108	2	3	I-I	12x20	Legno_is otroppo	Legno_Ar careccio	0	5050	0	0	0	0	0	0	Trave	201	201
108	3	111	I-I	12x20	Legno_is otroppo	Legno_Ar careccio	0	5050	0	0	0	0	0	0	Trave	216	216
109	101	4	I-I	12x20	Legno_is otroppo	Legno_Ar careccio	0	5050	0	0	0	0	0	0	Trave	121	121
109	4	5	I-I	12x20	Legno_is otroppo	Legno_Ar careccio	0	5050	0	0	0	0	0	0	Trave	201	201
109	5	6	I-I	12x20	Legno_is otroppo	Legno_Ar careccio	0	5050	0	0	0	0	0	0	Trave	201	201
109	6	112	I-I	12x20	Legno_is otroppo	Legno_Ar careccio	0	5050	0	0	0	0	0	0	Trave	79	79
110	111	112	I-I	12x20	Legno_is otroppo	Legno_Ar careccio	0	5050	0	0	0	0	0	0	Trave	346	346
110	110	111	I-I	12x20	Legno_is otroppo	Legno_Ar careccio	0	5050	0	0	0	0	0	0	Trave	456	456
110	26	110	I-I	12x20	Legno_is otroppo	Legno_Ar careccio	0	5050	0	0	0	0	0	0	Trave	527	527
110	109	26	I-I	12x20	Legno_is otroppo	Legno_Ar careccio	0	5050	0	0	0	0	0	0	Trave	371	371
110	25	109	I-I	12x20	Legno_is otroppo	Legno_Ar careccio	0	5050	0	0	0	0	0	0	Trave	135	135
110	108	25	I-I	12x20	Legno_is otroppo	Legno_Ar careccio	0	5050	0	0	0	0	0	0	Trave	470	470
111	102	101	I-I	12x20	Legno_is otroppo	Legno_Ar careccio	0	5050	0	0	0	0	0	0	Trave	354	354
111	103	102	I-I	12x20	Legno_is otroppo	Legno_Ar careccio	0	5050	0	0	0	0	0	0	Trave	467	467
111	104	103	I-I	12x20	Legno_is otroppo	Legno_Ar careccio	0	5050	0	0	0	0	0	0	Trave	615	615
111	105	104	I-I	12x20	Legno_is otroppo	Legno_Ar careccio	0	5050	0	0	0	0	0	0	Trave	571	571
112	107	108	I-I	12x20	Legno_is otroppo	Legno_Ar careccio	0	5050	0	0	0	0	0	0	Trave	238	238
113	104	8	I-I	12x20	Legno_is otroppo	Legno_Ar careccio	0	5050	0	0	0	0	0	0	Trave	201	201
113	8	9	I-I	12x20	Legno_is otroppo	Legno_Ar careccio	0	5050	0	0	0	0	0	0	Trave	196	196
113	9	10	I-I	12x20	Legno_is otroppo	Legno_Ar careccio	0	5050	0	0	0	0	0	0	Trave	195	195
113	10	11	I-I	12x20	Legno_is otroppo	Legno_Ar careccio	0	5050	0	0	0	0	0	0	Trave	196	196
113	11	12	I-I	12x20	Legno_is otroppo	Legno_Ar careccio	0	5050	0	0	0	0	0	0	Trave	196	196
113	12	13	I-I	12x20	Legno_is otroppo	Legno_Ar careccio	0	5050	0	0	0	0	0	0	Trave	196	196
113	13	109	I-I	12x20	Legno_is otroppo	Legno_Ar careccio	0	5050	0	0	0	0	0	0	Trave	144	144
114	103	15	I-I	12x20	Legno_is otroppo	Legno_Ar careccio	0	5050	0	0	0	0	0	0	Trave	170	170
114	15	16	I-I	12x20	Legno_is otroppo	Legno_Ar careccio	0	5050	0	0	0	0	0	0	Trave	200	200
114	16	17	I-I	12x20	Legno_is otroppo	Legno_Ar careccio	0	5050	0	0	0	0	0	0	Trave	202	202
114	17	18	I-I	12x20	Legno_is otroppo	Legno_Ar careccio	0	5050	0	0	0	0	0	0	Trave	201	201
114	18	110	I-I	12x20	Legno_is otroppo	Legno_Ar careccio	0	5050	0	0	0	0	0	0	Trave	193	193
115	106	1	I-I	12x20	Legno_is otroppo	Legno_Ar careccio	0	5050	0	0	0	0	0	0	Trave	69	69
115	1	2	I-I	12x20	Legno_is otroppo	Legno_Ar careccio	0	5050	0	0	0	0	0	0	Trave	196	196
115	2	3	I-I	12x20	Legno_is otroppo	Legno_Ar careccio	0	5050	0	0	0	0	0	0	Trave	196	196
115	3	4	I-I	12x20	Legno_is otroppo	Legno_Ar careccio	0	5050	0	0	0	0	0	0	Trave	196	196
115	4	5	I-I	12x20	Legno_is otroppo	Legno_Ar careccio	0	5050	0	0	0	0	0	0	Trave	196	196

	Ni	Nf	Vinc.	Sez.	Mat.	Crit.pr.	Rot.	f.f.	xi	yi	zi	xf	yf	zf	Tipo	L2	L3
115	5	6	I-I	12x20	Legno_is otroto	Legno_Ar careccio	0	5050	0	0	0	0	0	0	Trave	195	195
115	6	7	I-I	12x20	Legno_is otroto	Legno_Ar careccio	0	5050	0	0	0	0	0	0	Trave	196	196
115	7	107	I-I	12x20	Legno_is otroto	Legno_Ar careccio	0	5050	0	0	0	0	0	0	Trave	50	50
116	106	105	I-I	12x20	Legno_is otroto	Legno_Ar careccio	0	5050	0	0	0	0	0	0	Trave	248	248
8000	313	213	I-I	trave 30x30	C30/37	CLS_Trav iAlte	0	8080	0	-0	0	0	-0	0	Trave	135	135
8000	213	234	I-I	trave 30x30	C30/37	CLS_Trav iAlte	0	8080	0	-0	0	0	0	-0	Trave	604	604
8001	212	313	I-I	trave 30x30	C30/37	CLS_Trav iAlte	0	8080	0	0	0	0	0	0	Trave	457	457
8001	214	212	I-I	trave 30x30	C30/37	CLS_Trav iAlte	0	8080	0	0	0	0	0	0	Trave	470	470
8001	206	214	I-I	trave 30x30	C30/37	CLS_Trav iAlte	0	8080	0	0	0	-0	0	0	Trave	629	629
9001	12	13	I-I	50x60	C25/30	CLS_Trav iFondazio ne_Rett	0	8585	0	0	0	0	0	0	Fond.	349	349
9001	14	12	I-I	50x60	C25/30	CLS_Trav iFondazio ne_Rett	0	8585	0	0	0	0	0	0	Fond.	459	459
9001	6	14	I-I	50x60	C25/30	CLS_Trav iFondazio ne_Rett	0	8585	0	0	0	0	0	0	Fond.	615	615
9001	5	6	I-I	50x60	C25/30	CLS_Trav iFondazio ne_Rett	0	8585	0	0	0	0	0	0	Fond.	571	571
9002	7	5	I-I	50x60	C25/30	CLS_Trav iFondazio ne_Rett	0	8585	0	0	0	0	0	0	Fond.	248	248
9003	134	34	I-I	50x60	C30/37	CLS_Trav iFondazio ne	0	8080	0	-0	-0	0	-0	-0	Fond.	158	158
9003	33	34	I-I	50x60	C25/30	CLS_Trav iFondazio ne_Rett	0	8585	0	0	0	0	0	0	Fond.	181	181
9003	32	33	I-I	50x60	C25/30	CLS_Trav iFondazio ne_Rett	0	8585	0	0	0	0	0	0	Fond.	120	120
9003	11	32	I-I	50x60	C25/30	CLS_Trav iFondazio ne_Rett	0	8585	0	0	0	0	0	0	Fond.	40	40
9003	10	11	I-I	50x60	C25/30	CLS_Trav iFondazio ne_Rett	0	8585	0	0	0	0	0	0	Fond.	37	37
9003	9	10	I-I	50x60	C25/30	CLS_Trav iFondazio ne_Rett	0	8585	0	0	0	0	0	0	Fond.	120	120
9003	8	9	I-I	50x60	C25/30	CLS_Trav iFondazio ne_Rett	0	8585	0	0	0	0	0	0	Fond.	290	290
9003	31	8	I-I	50x60	C25/30	CLS_Trav iFondazio ne_Rett	0	8585	0	0	0	0	0	0	Fond.	58	58
9003	30	31	I-I	50x60	C25/30	CLS_Trav iFondazio ne_Rett	0	8585	0	0	0	0	0	0	Fond.	240	240
9003	29	30	I-I	50x60	C25/30	CLS_Trav iFondazio ne_Rett	0	8585	0	0	0	0	0	0	Fond.	30	30
9003	28	29	I-I	50x60	C25/30	CLS_Trav iFondazio ne_Rett	0	8585	0	0	0	0	0	0	Fond.	240	240
9003	27	28	I-I	50x60	C25/30	CLS_Trav iFondazio	0	8585	0	0	0	0	0	0	Fond.	30	30

	Ni	Nf	Vinc.	Sez.	Mat.	Crit.pr. ne_Rett	Rot.	f.f.	xi	yi	zi	xf	yf	zf	Tipo	L2	L3
9003	26	27	I-I	50x60	C25/30	CLS_Trav iFondazio ne_Rett	0	8585	0	0	0	0	0	0	Fond.	220	220
9003	21	26	I-I	50x60	C25/30	CLS_Trav iFondazio ne_Rett	0	8585	0	0	0	0	0	0	Fond.	80	80
9003	25	21	I-I	50x60	C25/30	CLS_Trav iFondazio ne_Rett	0	8585	0	0	0	0	0	0	Fond.	55	55
9003	24	25	I-I	50x60	C25/30	CLS_Trav iFondazio ne_Rett	0	8585	0	0	0	0	0	0	Fond.	100	100
9003	23	24	I-I	50x60	C25/30	CLS_Trav iFondazio ne_Rett	0	8585	0	0	0	0	0	0	Fond.	101	101
9003	22	23	I-I	50x60	C25/30	CLS_Trav iFondazio ne_Rett	0	8585	0	0	0	0	0	0	Fond.	120	120
9003	18	22	I-I	50x60	C25/30	CLS_Trav iFondazio ne_Rett	0	8585	0	0	0	0	0	0	Fond.	229	229
9004	7	15	I-I	50x60	C25/30	CLS_Trav iFondazio ne_Rett	0	8585	0	0	0	0	0	0	Fond.	1296	1296
9005	15	16	I-I	50x60	C25/30	CLS_Trav iFondazio ne_Rett	0	8585	0	0	0	0	0	0	Fond.	50	50
9005	16	17	I-I	50x60	C25/30	CLS_Trav iFondazio ne_Rett	0	8585	0	0	0	0	0	0	Fond.	120	120
9005	17	18	I-I	50x60	C25/30	CLS_Trav iFondazio ne_Rett	0	8585	0	0	0	0	0	0	Fond.	68	68
9006	14	19	I-I	50x60	C25/30	CLS_Trav iFondazio ne_Rett	0	8585	0	0	0	0	0	0	Fond.	420	420
9006	19	20	I-I	50x60	C25/30	CLS_Trav iFondazio ne_Rett	0	8585	0	0	0	0	0	0	Fond.	180	180
9006	20	8	I-I	50x60	C25/30	CLS_Trav iFondazio ne_Rett	0	8585	0	0	0	0	0	0	Fond.	364	364
9007	6	106	I-I	50x60	C30/37	CLS_Trav iFondazio ne	0	8080	0	0	0	-0	0	0	Fond.	172	172
9007	6	21	I-I	50x60	C25/30	CLS_Trav iFondazio ne_Rett	0	8585	0	0	0	0	0	0	Fond.	1325	1325
9008	12	35	I-I	50x60	C25/30	CLS_Trav iFondazio ne_Rett	0	8585	0	0	0	0	0	0	Fond.	150	150
9008	35	36	I-I	50x60	C25/30	CLS_Trav iFondazio ne_Rett	0	8585	0	0	0	0	0	0	Fond.	80	80
9008	36	11	I-I	50x60	C25/30	CLS_Trav iFondazio ne_Rett	0	8585	0	0	0	0	0	0	Fond.	529	529
9009	13	34	I-I	50x60	C25/30	CLS_Trav iFondazio ne_Rett	0	8585	0	0	0	0	0	0	Fond.	603	603
9010	112	213	I-I	50x60	C30/37	CLS_Trav iFondazio ne	0	8080	0	0	0	0	0	0	Fond.	457	457
9010	114	112	I-I	50x60	C30/37	CLS_Trav iFondazio	0	8080	0	0	0	0	0	0	Fond.	459	459

	Ni	Nf	Vinc.	Sez.	Mat.	Crit.pr. ne	Rot.	f.f.	xi	yi	zi	xf	yf	zf	Tipo	L2	L3
9010	106	114	I-I	50x60	C30/37	CLS_Trav iFondazio ne	0	8080	0	0	0	-0	0	0	Fond.	615	615
9011	213	113	I-I	50x60	C30/37	CLS_Trav iFondazio ne	0	8080	0	-0	0	0	-0	0	Fond.	135	135
9011	113	134	I-I	50x60	C30/37	CLS_Trav iFondazio ne	0	8080	0	-0	0	0	0	-0	Fond.	604	604
9012	13	213	I-I	50x60	C30/37	CLS_Trav iFondazio ne	0	8080	0	0	0	0	0	0	Fond.	206	206

Aste - Carichi

Descrizione carichi aste

UnifG	Uniforme globale
UnifL	Uniforme locale
VarG	Variabile lineare globale
VarL	Variabile lineare locale
PolG	Poligonale globale
Termico	Distorsione termica
Torcente	Carico torcente
Precomp.	Carico da precompressione
PolL	Poligonale locale

Sezione	Ni	Nf	Cond.	Tipo c.	Xi cm	QXi car. dist. kg/m coppie torc. kg*m/m	QYi	QZi	Xf cm	QXf car. dist. kg/m coppie torc. kg*m/m	QYf	QZf
Trave 101												
HE 260 B	6	13	Peso Proprio	UnifG	0	0	0	93	756	0	0	93
HE 260 B	6	13	QP Solai	PolG	0	0	0	59	15	0	0	117
					15	0	0	117	617	0	0	118
					617	0	0	118	745	0	0	102
					745	0	0	102	756	0	0	59
HE 260 B	6	13	QFissi Solai	PolG	0	0	0	353	15	0	0	704
					15	0	0	704	617	0	0	706
					617	0	0	706	745	0	0	613
					745	0	0	613	756	0	0	353
HE 260 B	6	13	QV Solai	PolG	0	0	0	491	15	0	0	978
					15	0	0	978	617	0	0	981
					617	0	0	981	745	0	0	851
					745	0	0	851	756	0	0	491
HE 260 B	13	26	Peso Proprio	UnifG	0	0	0	93	343	0	0	93
HE 260 B	13	26	QP Solai	PolG	0	0	0	42	15	0	0	99
					15	0	0	99	343	0	0	60
HE 260 B	13	26	QFissi Solai	PolG	0	0	0	251	15	0	0	594
					15	0	0	594	343	0	0	359
HE 260 B	13	26	QV Solai	PolG	0	0	0	349	15	0	0	824
					15	0	0	824	343	0	0	498
Trave 102												
HE 260 B	5	12	Peso Proprio	UnifG	0	0	0	93	756	0	0	93
HE 260 B	5	12	QP Solai	PolG	0	0	0	59	15	0	0	117
					15	0	0	117	741	0	0	118
					741	0	0	118	756	0	0	59
HE 260 B	5	12	QFissi Solai	PolG	0	0	0	351	15	0	0	705
					15	0	0	705	741	0	0	706
					741	0	0	706	756	0	0	352
HE 260 B	5	12	QV Solai	PolG	0	0	0	488	15	0	0	979
					15	0	0	979	741	0	0	981
					741	0	0	981	756	0	0	490
HE 260 B	12	110	Peso Proprio	UnifG	0	0	0	93	828	0	0	93
HE 260 B	12	110	QP Solai	PolG	-0	0	0	59	14	0	0	118
					14	0	0	118	327	0	0	118

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
					327	0	0	118	800	0	0	60
					800	0	0	60	828	0	0	0
HE 260 B	12	110	QFissi Solai	PolG	-0	0	0	354	14	0	0	706
					14	0	0	706	327	0	0	706
					327	0	0	706	800	0	0	359
					800	0	0	359	828	0	0	0
HE 260 B	12	110	QV Solai	PolG	-0	0	0	491	14	0	0	981
					14	0	0	981	327	0	0	981
					327	0	0	981	800	0	0	499
					800	0	0	499	828	0	0	0
Trave 103												
HE 260 B	4	11	Peso Proprio	UnifG	0	0	0	93	756	0	0	93
HE 260 B	4	11	QP Solai	PolG	0	0	0	59	15	0	0	118
					15	0	0	118	741	0	0	118
					741	0	0	118	756	0	0	59
HE 260 B	4	11	QFissi Solai	PolG	0	0	0	353	15	0	0	707
					15	0	0	707	741	0	0	706
					741	0	0	706	756	0	0	353
HE 260 B	4	11	QV Solai	PolG	0	0	0	491	15	0	0	982
					15	0	0	982	741	0	0	980
					741	0	0	980	756	0	0	491
HE 260 B	11	18	Peso Proprio	UnifG	0	0	0	93	786	0	0	93
HE 260 B	11	18	QP Solai	PolG	0	0	0	59	15	0	0	118
					15	0	0	118	755	0	0	115
					755	0	0	115	786	0	0	56
HE 260 B	11	18	QFissi Solai	PolG	0	0	0	352	15	0	0	705
					15	0	0	705	755	0	0	691
					755	0	0	691	786	0	0	339
HE 260 B	11	18	QV Solai	PolG	0	0	0	489	15	0	0	980
					15	0	0	980	755	0	0	960
					755	0	0	960	786	0	0	470
Trave 104												
HE 260 B	3	10	Peso Proprio	UnifG	0	0	0	93	756	0	0	93
HE 260 B	3	6	Peso Proprio	UnifG	0	0	0	93	350	0	0	93
HE 260 B	3	6	QP Solai	PolG	-0	0	0	59	33	0	0	122
					33	0	0	122	320	0	0	87
					320	0	0	87	350	0	0	25
HE 260 B	3	10	QP Solai	PolG	0	0	0	59	14	0	0	118
					14	0	0	118	740	0	0	117
					740	0	0	117	756	0	0	59
HE 260 B	3	10	QFissi Solai	PolG	0	0	0	353	14	0	0	706
					14	0	0	706	740	0	0	705
					740	0	0	705	756	0	0	351
HE 260 B	3	6	QFissi Solai	PolG	-0	0	0	353	33	0	0	732
					33	0	0	732	320	0	0	523
					320	0	0	523	350	0	0	148
HE 260 B	3	10	QV Solai	PolG	0	0	0	491	14	0	0	980
					14	0	0	980	740	0	0	979
					740	0	0	979	756	0	0	488
HE 260 B	3	6	QV Solai	PolG	-0	0	0	294	33	0	0	610
					33	0	0	610	320	0	0	436
					320	0	0	436	350	0	0	124
HE 260 B	10	17	Peso Proprio	UnifG	0	0	0	93	740	0	0	93
HE 260 B	10	17	QP Solai	PolG	0	0	0	59	15	0	0	117
					15	0	0	117	709	0	0	118
					709	0	0	118	740	0	0	59
HE 260 B	10	17	QFissi Solai	PolG	0	0	0	353	15	0	0	704
					15	0	0	704	709	0	0	706
					709	0	0	706	740	0	0	352
HE 260 B	10	17	QV Solai	PolG	0	0	0	491	15	0	0	978
					15	0	0	978	709	0	0	980
					709	0	0	980	740	0	0	489
HE 260 B	17	3	Peso Proprio	UnifG	0	0	0	93	460	0	0	93
HE 260 B	17	3	QP Solai	PolG	0	0	0	174	430	0	0	125

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
					430	0	0	125	460	0	0	63
HE 260 B	17	3	QFissi Solai	PolG	0	0	0	1042	430	0	0	753
					430	0	0	753	460	0	0	379
HE 260 B	17	3	QV Solai	PolG	0	0	0	869	430	0	0	627
					430	0	0	627	460	0	0	316
Trave 105												
HE 260 B	2	5	Peso Proprio	UnifG	0	0	0	93	350	0	0	93
HE 260 B	2	9	Peso Proprio	UnifG	0	0	0	93	756	0	0	93
HE 260 B	2	9	QP Solai	PolG	-0	0	0	59	15	0	0	118
					15	0	0	118	741	0	0	117
					741	0	0	117	756	0	0	59
HE 260 B	2	5	QP Solai	PolG	-0	0	0	59	30	0	0	118
					30	0	0	118	320	0	0	118
					320	0	0	118	350	0	0	59
HE 260 B	2	9	QFissi Solai	PolG	-0	0	0	352	15	0	0	706
					15	0	0	706	741	0	0	704
					741	0	0	704	756	0	0	353
HE 260 B	2	5	QFissi Solai	PolG	-0	0	0	353	30	0	0	706
					30	0	0	706	320	0	0	706
					320	0	0	706	350	0	0	353
HE 260 B	2	9	QV Solai	PolG	-0	0	0	489	15	0	0	980
					15	0	0	980	741	0	0	978
					741	0	0	978	756	0	0	491
HE 260 B	2	5	QV Solai	PolG	-0	0	0	294	30	0	0	589
					30	0	0	589	320	0	0	589
					320	0	0	589	350	0	0	294
HE 260 B	9	16	Peso Proprio	UnifG	0	0	0	93	695	0	0	93
HE 260 B	9	16	QP Solai	PolG	-0	0	0	59	15	0	0	117
					15	0	0	117	667	0	0	117
					667	0	0	117	695	0	0	59
HE 260 B	9	16	QFissi Solai	PolG	-0	0	0	351	15	0	0	705
					15	0	0	705	667	0	0	705
					667	0	0	705	695	0	0	354
HE 260 B	9	16	QV Solai	PolG	-0	0	0	488	15	0	0	979
					15	0	0	979	667	0	0	979
					667	0	0	979	695	0	0	491
HE 260 B	16	2	Peso Proprio	UnifG	0	0	0	93	462	0	0	93
HE 260 B	16	2	QP Solai	PolG	0	0	0	59	31	0	0	118
					31	0	0	118	432	0	0	118
					432	0	0	118	462	0	0	59
HE 260 B	16	2	QFissi Solai	PolG	0	0	0	351	31	0	0	705
					31	0	0	705	432	0	0	707
					432	0	0	707	462	0	0	353
HE 260 B	16	2	QV Solai	PolG	0	0	0	293	31	0	0	588
					31	0	0	588	432	0	0	589
					432	0	0	589	462	0	0	294
Trave 106												
HE 260 B	1	4	Peso Proprio	UnifG	0	0	0	93	350	0	0	93
HE 260 B	1	8	Peso Proprio	UnifG	0	0	0	93	756	0	0	93
HE 260 B	1	8	QP Solai	PolG	-0	0	0	80	204	0	0	129
					204	0	0	129	741	0	0	120
					741	0	0	120	756	0	0	60
HE 260 B	1	4	QP Solai	PolG	-0	0	0	41	30	0	0	99
					30	0	0	99	331	0	0	94
					331	0	0	94	350	0	0	59
HE 260 B	1	8	QFissi Solai	PolG	-0	0	0	478	204	0	0	773
					204	0	0	773	741	0	0	718
					741	0	0	718	756	0	0	363
HE 260 B	1	4	QFissi Solai	PolG	-0	0	0	246	30	0	0	596
					30	0	0	596	331	0	0	566
					331	0	0	566	350	0	0	353
HE 260 B	1	4	QV Solai	PolG	-0	0	0	205	30	0	0	496
					30	0	0	496	331	0	0	472
					331	0	0	472	350	0	0	294

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
HE 260 B	1	8	QV Solai	PolG	-0	0	0	664	204	0	0	1074
					204	0	0	1074	741	0	0	997
					741	0	0	997	756	0	0	504
HE 260 B	8	15	Peso Proprio	UnifG	0	0	0	93	652	0	0	93
HE 260 B	8	15	QP Solai	PolG	0	0	0	59	15	0	0	119
					15	0	0	119	626	0	0	108
					626	0	0	108	652	0	0	59
HE 260 B	8	15	QFissi Solai	PolG	0	0	0	353	15	0	0	715
					15	0	0	715	626	0	0	649
					626	0	0	649	652	0	0	351
HE 260 B	8	15	QV Solai	PolG	0	0	0	491	15	0	0	993
					15	0	0	993	626	0	0	901
					626	0	0	901	652	0	0	488
HE 260 B	15	1	Peso Proprio	UnifG	0	0	0	93	460	0	0	93
HE 260 B	15	1	QP Solai	PolG	-0	0	0	49	28	0	0	107
					28	0	0	107	439	0	0	100
					439	0	0	100	460	0	0	59
HE 260 B	15	1	QFissi Solai	PolG	-0	0	0	295	28	0	0	644
					28	0	0	644	439	0	0	601
					439	0	0	601	460	0	0	353
HE 260 B	15	1	QV Solai	PolG	-0	0	0	246	28	0	0	537
					28	0	0	537	439	0	0	501
					439	0	0	501	460	0	0	294
Trave 107												
HE 260 B	7	25	Peso Proprio	UnifG	0	0	0	93	632	0	0	93
HE 260 B	7	25	QP Solai	PolG	0	0	0	16	15	0	0	78
					15	0	0	78	185	0	0	114
					185	0	0	114	632	0	0	59
HE 260 B	7	25	QFissi Solai	PolG	0	0	0	95	15	0	0	468
					15	0	0	468	185	0	0	682
					185	0	0	682	632	0	0	353
HE 260 B	7	25	QV Solai	PolG	0	0	0	132	15	0	0	650
					15	0	0	650	185	0	0	947
					185	0	0	947	632	0	0	491
Trave 108												
12x20	1	2	Peso Proprio	UnifG	0	0	0	17	201	0	0	17
12x20	1	2	QP Solai	PolG	-0	0	0	9	201	0	0	9
12x20	1	2	QFissi Solai	PolG	-0	0	0	53	201	0	0	53
12x20	1	2	QV Solai	PolG	-0	0	0	44	201	0	0	44
12x20	2	3	Peso Proprio	UnifG	0	0	0	17	201	0	0	17
12x20	2	3	QP Solai	PolG	-0	0	0	9	201	0	0	9
12x20	2	3	QFissi Solai	PolG	-0	0	0	53	201	0	0	53
12x20	2	3	QV Solai	PolG	-0	0	0	44	201	0	0	44
12x20	3	111	Peso Proprio	UnifG	0	0	0	17	216	0	0	17
12x20	3	111	QP Solai	PolG	-0	0	0	0	216	0	0	10
12x20	3	111	QFissi Solai	PolG	-0	0	0	0	216	0	0	61
12x20	3	111	QV Solai	PolG	-0	0	0	0	216	0	0	50
12x20	102	1	Peso Proprio	UnifG	0	0	0	17	141	0	0	17
12x20	102	1	QP Solai	PolG	0	0	0	6	141	0	0	6
12x20	102	1	QFissi Solai	PolG	0	0	0	37	141	0	0	36
12x20	102	1	QV Solai	PolG	0	0	0	31	141	0	0	30
Trave 109												
12x20	4	5	Peso Proprio	UnifG	0	0	0	17	201	0	0	17
12x20	4	5	QP Solai	PolG	-0	0	0	9	201	0	0	0
12x20	4	5	QFissi Solai	PolG	-0	0	0	53	201	0	0	0
12x20	4	5	QV Solai	PolG	-0	0	0	44	201	0	0	0
12x20	5	6	Peso Proprio	UnifG	0	0	0	17	201	0	0	17
12x20	5	6	QP Solai	PolG	-0	0	0	9	201	0	0	0
12x20	5	6	QFissi Solai	PolG	-0	0	0	53	201	0	0	0
12x20	5	6	QV Solai	PolG	-0	0	0	44	201	0	0	0
12x20	6	112	Peso Proprio	UnifG	0	0	0	17	79	0	0	17
12x20	6	112	QP Solai	PolG	0	0	0	4	79	0	0	0
12x20	6	112	QFissi Solai	PolG	0	0	0	23	79	0	0	0
12x20	6	112	QV Solai	PolG	0	0	0	19	79	0	0	0

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
12x20	101	4	Peso Proprio	UnifG	0	0	0	17	121	0	0	17
12x20	101	4	QP Solai	PolG	0	0	0	5	121	0	0	0
12x20	101	4	QFissi Solai	PolG	0	0	0	33	121	0	0	0
12x20	101	4	QV Solai	PolG	0	0	0	27	121	0	0	0
Trave 110												
12x20	25	109	Peso Proprio	UnifG	0	0	0	17	135	0	0	17
12x20	25	109	QP Solai	PolG	-0	0	0	56	135	0	0	41
12x20	25	109	QFissi Solai	PolG	-0	0	0	336	135	0	0	247
12x20	25	109	QV Solai	PolG	-0	0	0	467	135	0	0	342
12x20	26	110	Peso Proprio	UnifG	0	0	0	17	527	0	0	17
12x20	26	110	QP Solai	PolG	-0	0	0	57	527	0	0	0
12x20	26	110	QFissi Solai	PolG	-0	0	0	341	527	0	0	0
12x20	26	110	QV Solai	PolG	-0	0	0	474	527	0	0	0
12x20	108	25	Peso Proprio	UnifG	0	0	0	17	470	0	0	17
12x20	108	25	QP Solai	PolG	0	0	0	52	470	0	0	0
12x20	108	25	QFissi Solai	PolG	0	0	0	313	470	0	0	0
12x20	108	25	QV Solai	PolG	0	0	0	434	470	0	0	0
12x20	109	26	Peso Proprio	UnifG	0	0	0	17	371	0	0	17
12x20	109	26	QP Solai	PolG	0	0	0	0	11	0	0	40
					11	0	0	40	371	0	0	0
12x20	109	26	QFissi Solai	PolG	0	0	0	0	11	0	0	239
					11	0	0	239	371	0	0	0
12x20	109	26	QV Solai	PolG	0	0	0	0	11	0	0	332
					11	0	0	332	371	0	0	0
12x20	110	111	Peso Proprio	UnifG	0	0	0	17	456	0	0	17
12x20	110	111	QP Solai	PolG	0	0	0	116	456	0	0	64
12x20	110	111	QFissi Solai	PolG	0	0	0	698	456	0	0	384
12x20	110	111	QV Solai	PolG	0	0	0	582	456	0	0	320
12x20	111	112	Peso Proprio	UnifG	0	0	0	17	346	0	0	17
12x20	111	112	QP Solai	PolG	-0	0	0	60	334	0	0	24
					334	0	0	24	346	0	0	0
12x20	111	112	QFissi Solai	PolG	-0	0	0	360	334	0	0	141
					334	0	0	141	346	0	0	0
12x20	111	112	QV Solai	PolG	-0	0	0	300	334	0	0	118
					334	0	0	118	346	0	0	0
Trave 111												
12x20	102	101	Peso Proprio	UnifG	0	0	0	17	354	0	0	17
12x20	102	101	QP Solai	PolG	0	0	0	0	21	0	0	41
					21	0	0	41	354	0	0	35
12x20	102	101	QFissi Solai	PolG	0	0	0	0	21	0	0	244
					21	0	0	244	354	0	0	212
12x20	102	101	QV Solai	PolG	0	0	0	0	21	0	0	203
					21	0	0	203	354	0	0	176
12x20	103	102	Peso Proprio	UnifG	0	0	0	17	467	0	0	17
12x20	103	102	QP Solai	PolG	0	0	0	0	26	0	0	49
					26	0	0	49	467	0	0	41
12x20	103	102	QFissi Solai	PolG	0	0	0	0	26	0	0	294
					26	0	0	294	467	0	0	246
12x20	103	102	QV Solai	PolG	0	0	0	0	26	0	0	245
					26	0	0	245	467	0	0	205
12x20	104	103	Peso Proprio	UnifG	0	0	0	17	615	0	0	17
12x20	104	103	QP Solai	PolG	0	0	0	60	615	0	0	49
12x20	104	103	QFissi Solai	PolG	0	0	0	359	615	0	0	296
12x20	104	103	QV Solai	PolG	0	0	0	499	615	0	0	411
12x20	105	104	Peso Proprio	UnifG	0	0	0	17	571	0	0	17
12x20	105	104	QP Solai	PolG	0	0	0	70	556	0	0	60
					556	0	0	60	571	0	0	0
12x20	105	104	QFissi Solai	PolG	0	0	0	417	556	0	0	361
					556	0	0	361	571	0	0	0
12x20	105	104	QV Solai	PolG	0	0	0	580	556	0	0	501
					556	0	0	501	571	0	0	0
Trave 112												
12x20	107	108	Peso Proprio	UnifG	0	0	0	17	238	0	0	17
12x20	107	108	QP Solai	PolG	-0	0	0	0	4	0	0	12

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
					4	0	0	12	238	0	0	43
12x20	107	108	QFissi Solai	PolG	-0	0	0	0	4	0	0	75
					4	0	0	75	238	0	0	260
12x20	107	108	QV Solai	PolG	-0	0	0	0	4	0	0	104
					4	0	0	104	238	0	0	361
Trave 113												
12x20	8	9	Peso Proprio	UnifG	0	0	0	17	196	0	0	17
12x20	8	9	QP Solai	PolG	0	0	0	5	196	0	0	5
12x20	8	9	QFissi Solai	PolG	0	0	0	27	196	0	0	27
12x20	8	9	QV Solai	PolG	0	0	0	38	196	0	0	38
12x20	9	10	Peso Proprio	UnifG	0	0	0	17	195	0	0	17
12x20	9	10	QP Solai	PolG	0	0	0	4	195	0	0	4
12x20	9	10	QFissi Solai	PolG	0	0	0	27	195	0	0	27
12x20	9	10	QV Solai	PolG	0	0	0	37	195	0	0	37
12x20	10	11	Peso Proprio	UnifG	0	0	0	17	196	0	0	17
12x20	10	11	QP Solai	PolG	0	0	0	5	196	0	0	5
12x20	10	11	QFissi Solai	PolG	0	0	0	27	196	0	0	27
12x20	10	11	QV Solai	PolG	0	0	0	38	196	0	0	38
12x20	11	12	Peso Proprio	UnifG	0	0	0	17	196	0	0	17
12x20	11	12	QP Solai	PolG	0	0	0	4	196	0	0	4
12x20	11	12	QFissi Solai	PolG	0	0	0	26	196	0	0	26
12x20	11	12	QV Solai	PolG	0	0	0	36	196	0	0	36
12x20	12	13	Peso Proprio	UnifG	0	0	0	17	196	0	0	17
12x20	12	13	QP Solai	PolG	-0	0	0	5	196	0	0	5
12x20	12	13	QFissi Solai	PolG	-0	0	0	27	196	0	0	27
12x20	12	13	QV Solai	PolG	-0	0	0	38	196	0	0	38
12x20	13	109	Peso Proprio	UnifG	0	0	0	17	144	0	0	17
12x20	13	109	QP Solai	PolG	-0	0	0	3	144	0	0	3
12x20	13	109	QFissi Solai	PolG	-0	0	0	19	144	0	0	19
12x20	13	109	QV Solai	PolG	-0	0	0	26	144	0	0	27
12x20	104	8	Peso Proprio	UnifG	0	0	0	17	201	0	0	17
12x20	104	8	QP Solai	PolG	-0	0	0	4	201	0	0	4
12x20	104	8	QFissi Solai	PolG	-0	0	0	27	201	0	0	27
12x20	104	8	QV Solai	PolG	-0	0	0	37	201	0	0	37
Trave 114												
12x20	15	16	Peso Proprio	UnifG	0	0	0	17	200	0	0	17
12x20	15	16	QP Solai	PolG	0	0	0	8	200	0	0	8
12x20	15	16	QFissi Solai	PolG	0	0	0	49	200	0	0	50
12x20	15	16	QV Solai	PolG	0	0	0	68	200	0	0	41
12x20	16	17	Peso Proprio	UnifG	0	0	0	17	202	0	0	17
12x20	16	17	QP Solai	PolG	0	0	0	9	202	0	0	9
12x20	16	17	QFissi Solai	PolG	0	0	0	54	202	0	0	55
12x20	16	17	QV Solai	PolG	0	0	0	75	202	0	0	46
12x20	17	18	Peso Proprio	UnifG	0	0	0	17	201	0	0	17
12x20	17	18	QP Solai	PolG	0	0	0	10	201	0	0	0
12x20	17	18	QFissi Solai	PolG	0	0	0	57	201	0	0	2
12x20	17	18	QV Solai	PolG	0	0	0	77	201	0	0	2
12x20	18	110	Peso Proprio	UnifG	0	0	0	17	193	0	0	17
12x20	18	110	QP Solai	PolG	0	0	0	9	193	0	0	0
12x20	18	110	QFissi Solai	PolG	0	0	0	53	193	0	0	0
12x20	18	110	QV Solai	PolG	0	0	0	72	193	0	0	0
12x20	103	15	Peso Proprio	UnifG	0	0	0	17	170	0	0	17
12x20	103	15	QP Solai	PolG	-0	0	0	7	170	0	0	7
12x20	103	15	QFissi Solai	PolG	-0	0	0	45	170	0	0	45
12x20	103	15	QV Solai	PolG	-0	0	0	62	170	0	0	37
Trave 115												
12x20	1	2	Peso Proprio	UnifG	0	0	0	17	196	0	0	17
12x20	1	2	QP Solai	PolG	-0	0	0	5	196	0	0	0
12x20	1	2	QFissi Solai	PolG	-0	0	0	27	196	0	0	0
12x20	1	2	QV Solai	PolG	-0	0	0	38	196	0	0	0
12x20	2	3	Peso Proprio	UnifG	0	0	0	17	196	0	0	17
12x20	2	3	QP Solai	PolG	0	0	0	4	196	0	0	0
12x20	2	3	QFissi Solai	PolG	0	0	0	26	196	0	0	0
12x20	2	3	QV Solai	PolG	0	0	0	36	196	0	0	0

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
12x20	3	4	Peso Proprio	UnifG	0	0	0	17	196	0	0	17
12x20	3	4	QP Solai	PolG	-0	0	0	5	196	0	0	0
12x20	3	4	QFissi Solai	PolG	-0	0	0	27	196	0	0	0
12x20	3	4	QV Solai	PolG	-0	0	0	38	196	0	0	0
12x20	4	5	Peso Proprio	UnifG	0	0	0	17	196	0	0	17
12x20	4	5	QP Solai	PolG	-0	0	0	5	196	0	0	0
12x20	4	5	QFissi Solai	PolG	-0	0	0	27	196	0	0	0
12x20	4	5	QV Solai	PolG	-0	0	0	38	196	0	0	0
12x20	5	6	Peso Proprio	UnifG	0	0	0	17	195	0	0	17
12x20	5	6	QP Solai	PolG	-0	0	0	4	195	0	0	0
12x20	5	6	QFissi Solai	PolG	-0	0	0	27	195	0	0	0
12x20	5	6	QV Solai	PolG	-0	0	0	37	195	0	0	0
12x20	6	7	Peso Proprio	UnifG	0	0	0	17	196	0	0	17
12x20	6	7	QP Solai	PolG	0	0	0	5	196	0	0	0
12x20	6	7	QFissi Solai	PolG	0	0	0	27	196	0	0	0
12x20	6	7	QV Solai	PolG	0	0	0	38	196	0	0	0
12x20	7	107	Peso Proprio	UnifG	0	0	0	17	50	0	0	17
12x20	7	107	QP Solai	PolG	-0	0	0	1	50	0	0	0
12x20	7	107	QFissi Solai	PolG	-0	0	0	6	50	0	0	0
12x20	7	107	QV Solai	PolG	-0	0	0	9	50	0	0	0
12x20	106	1	Peso Proprio	UnifG	0	0	0	17	69	0	0	17
12x20	106	1	QP Solai	PolG	-0	0	0	2	69	0	0	0
12x20	106	1	QFissi Solai	PolG	-0	0	0	10	69	0	0	0
12x20	106	1	QV Solai	PolG	-0	0	0	13	69	0	0	0
Trave 116												
12x20	106	105	Peso Proprio	UnifG	0	0	0	17	248	0	0	17
12x20	106	105	QP Solai	PolG	0	0	0	17	248	0	0	56
12x20	106	105	QFissi Solai	PolG	0	0	0	99	248	0	0	336
12x20	106	105	QV Solai	PolG	0	0	0	138	248	0	0	466
Trave 8000												
trave 30x30	213	234	Peso Proprio	UnifG	0	0	0	225	604	0	0	225
trave 30x30	313	213	Peso Proprio	UnifG	0	0	0	225	135	0	0	225
Trave 8001												
trave 30x30	206	214	Peso Proprio	UnifG	0	0	0	225	629	0	0	225
trave 30x30	212	313	Peso Proprio	UnifG	0	0	0	225	457	0	0	225
trave 30x30	214	212	Peso Proprio	UnifG	0	0	0	225	470	0	0	225
Fondazione 9001												
50x60	5	6	Peso Proprio	UnifG	0	0	0	750	571	0	0	750
50x60	6	14	Peso Proprio	UnifG	0	0	0	750	615	0	0	750
50x60	12	13	Peso Proprio	UnifG	0	0	0	750	349	0	0	750
50x60	14	12	Peso Proprio	UnifG	0	0	0	750	459	0	0	750
Fondazione 9002												
50x60	7	5	Peso Proprio	UnifG	0	0	0	750	248	0	0	750
Fondazione 9003												
50x60	8	9	Peso Proprio	UnifG	0	0	0	750	290	0	0	750
50x60	9	10	Peso Proprio	UnifG	0	0	0	750	120	0	0	750
50x60	10	11	Peso Proprio	UnifG	0	0	0	750	37	0	0	750
50x60	11	32	Peso Proprio	UnifG	0	0	0	750	40	0	0	750
50x60	18	22	Peso Proprio	UnifG	0	0	0	750	229	0	0	750
50x60	21	26	Peso Proprio	UnifG	0	0	0	750	80	0	0	750
50x60	22	23	Peso Proprio	UnifG	0	0	0	750	120	0	0	750
50x60	23	24	Peso Proprio	UnifG	0	0	0	750	101	0	0	750
50x60	24	25	Peso Proprio	UnifG	0	0	0	750	100	0	0	750
50x60	25	21	Peso Proprio	UnifG	0	0	0	750	55	0	0	750
50x60	26	27	Peso Proprio	UnifG	0	0	0	750	220	0	0	750
50x60	27	28	Peso Proprio	UnifG	0	0	0	750	30	0	0	750
50x60	28	29	Peso Proprio	UnifG	0	0	0	750	240	0	0	750
50x60	29	30	Peso Proprio	UnifG	0	0	0	750	30	0	0	750
50x60	30	31	Peso Proprio	UnifG	0	0	0	750	240	0	0	750

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
50x60	31	8	Peso Proprio	UnifG	0	0	0	750	58	0	0	750
50x60	32	33	Peso Proprio	UnifG	0	0	0	750	120	0	0	750
50x60	33	34	Peso Proprio	UnifG	0	0	0	750	181	0	0	750
50x60	134	34	Peso Proprio	UnifG	0	0	0	750	158	0	0	750
Fondazione 9004												
50x60	7	15	Peso Proprio	UnifG	0	0	0	750	1296	0	0	750
Fondazione 9005												
50x60	15	16	Peso Proprio	UnifG	0	0	0	750	50	0	0	750
50x60	16	17	Peso Proprio	UnifG	0	0	0	750	120	0	0	750
50x60	17	18	Peso Proprio	UnifG	0	0	0	750	68	0	0	750
Fondazione 9006												
50x60	14	19	Peso Proprio	UnifG	0	0	0	750	420	0	0	750
50x60	19	20	Peso Proprio	UnifG	0	0	0	750	180	0	0	750
50x60	20	8	Peso Proprio	UnifG	0	0	0	750	364	0	0	750
Fondazione 9007												
50x60	6	21	Peso Proprio	UnifG	0	0	0	750	1325	0	0	750
50x60	6	106	Peso Proprio	UnifG	0	0	0	750	172	0	0	750
Fondazione 9008												
50x60	12	35	Peso Proprio	UnifG	0	0	0	750	150	0	0	750
50x60	35	36	Peso Proprio	UnifG	0	0	0	750	80	0	0	750
50x60	36	11	Peso Proprio	UnifG	0	0	0	750	529	0	0	750
Fondazione 9009												
50x60	13	34	Peso Proprio	UnifG	0	0	0	750	603	0	0	750
Fondazione 9010												
50x60	106	114	Peso Proprio	UnifG	0	0	0	750	615	0	0	750
50x60	112	213	Peso Proprio	UnifG	0	0	0	750	457	0	0	750
50x60	114	112	Peso Proprio	UnifG	0	0	0	750	459	0	0	750
Fondazione 9011												
50x60	113	134	Peso Proprio	UnifG	0	0	0	750	604	0	0	750
50x60	213	113	Peso Proprio	UnifG	0	0	0	750	135	0	0	750
Fondazione 9012												
50x60	13	213	Peso Proprio	UnifG	0	0	0	750	206	0	0	750

Pareti - geometria e vincoli

Parete	Nodi	Tipo	Materiale	Criterio	N.P.	N.P.X	N.P.Y	Spess. cm
1	15-7-5-6-21-25-24-23-22-18-17-16	Platea	C30/37	CLS_Platee	439			25
1	13-34-112-6-5-4-101	Discreto	Pannello XLAM 12	Criterio di verifica XLAM 0	168			12
2	21-6-14-19-20-8-31-30-29-28-27-26	Platea	C30/37	CLS_Platee	449			25
2	12-35-38-39-36-11-111-3-2-1-102	Discreto	Pannello XLAM 12	Criterio di verifica XLAM 0	222			12
3	8-20-19-14-12-35-36-11-10-9	Platea	C30/37	CLS_Platee	206			25
3	14-19-10-11-20-8-110-18-17-16-15-103	Discreto	Pannello XLAM 12	Criterio di verifica XLAM 0	370			12
4	6-21-109-13-12-11-10-9-8-104	Discreto	Pannello XLAM 12	Criterio di verifica XLAM 0	568			12
4	11-36-35-12-13-34-33-32	Platea	C30/37	CLS_Platee	130			25
5	7-15-107-7-6-5-4-3-2-1-106	Discreto	Pannello XLAM 12	Criterio di verifica XLAM 0	378			12
5	6-106-114-112-213-13-12-14	Platea	C30/37	CLS_Platee	104			25
6	15-16-6-7-17-18-108-107	Discreto	Pannello XLAM 12	Criterio di verifica XLAM 0	60			12
6	13-213-113-134-34	Platea	C30/37	CLS_Platee	59			25
7	12-13-101-102	Discreto	Pannello XLAM 12	Criterio di verifica XLAM 0	100			12
7	106-114-214-206	Discreto	C30/37	CLS_Muri	16	4	4	30

Parete	Nodi	Tipo	Materiale	Criterio	N.P.	N.P.X	N.P.Y	Spess.
8	114-112-212-214	Discreto	C30/37	CLS_Muri	16	4	4	30
8	11-32-2-3-33-34-112-111	Discreto	Pannello XLAM 12	Criterio di verifica XLAM 0	65			12
9	112-213-313-212	Discreto	C30/37	CLS_Muri	16	4	4	30
9	14-12-102-103	Discreto	Pannello XLAM 12	Criterio di verifica XLAM 0	136			12
10	213-113-213-313	Discreto	C30/37	CLS_Muri	16	4	4	30
10	8-9-2-3-10-11-111-110	Discreto	Pannello XLAM 12	Criterio di verifica XLAM 0	121			12
11	6-14-103-104	Discreto	Pannello XLAM 12	Criterio di verifica XLAM 0	164			12
11	113-134-234-213	Discreto	C30/37	CLS_Muri	16	4	4	30
12	5-6-104-105	Discreto	Pannello XLAM 12	Criterio di verifica XLAM 0	260			12
13	21-26-22-23-27-28-26-27- 29-30-30-31-31-8-110-26- 109	Discreto	Pannello XLAM 12	Criterio di verifica XLAM 0	229			12
14	7-5-105-106	Discreto	Pannello XLAM 12	Criterio di verifica XLAM 0	72			12
15	18-22-14-15-23-24-18-19- 25-21-109-25-108	Discreto	Pannello XLAM 12	Criterio di verifica XLAM 0	191			12

Muri - Carichi

Shell	Indice dello shell
Cond.	Condizione di carico
Tipo	Tipologia di spinta
γ	Peso specifico: terreno o acqua
Ht	Quota del piano di campagna
$\emptyset$	Angolo di attrito interno
c	Coesione
δ	Angolo di attrito terreno paramento shell
β	Angolo di inclinazione del piano di campagna
k0	Coefficiente di spinta a riposo (quando richiesto)
β_m	Coefficiente di riduzione dell'accelerazione massima attesa al sito (quando richiesto)
Ag	Accelerazione del sito a meno di 'g': quando richiesto, rappresenta il valore della accelerazione dello spettro per T=0, quindi comprensiva dei coefficienti di amplificazione topografica (S_T) e stratigrafica (S_s)
Q	Valore del carico uniforme
Vert.1	Valore del carico nel primo vertice ⁽¹⁾
Vert.2	Valore del carico nel secondo vertice ⁽¹⁾
Vert.3	Valore del carico nel terzo vertice ⁽¹⁾
Vert.4	Valore del carico nel quarto vertice ⁽¹⁾
Hw	Altezza del pelo libero dell'acqua

⁽¹⁾: Per shell con numero di vertici maggiori 4, per carichi trapezoidali, il valore del carico nei vertici e' stampato a gruppi di 4 secondo l'ordine con cui i vertici sono stati definiti

Shell	Cond.	Tipo	Ht	γ	$\emptyset$	c	δ	β	k0	β_m	Ag
			cm	kg/ mc	°	kg/c mq	°	°			
7	Spinta terreno	Terreno - Attivo - Dir.Pos.	250	2000	20	0.00	0	0	--	--	--
8	Spinta terreno	Terreno - Attivo - Dir.Pos.	250	2000	20	0.00	0	0	--	--	--
9	Spinta terreno	Terreno - Attivo - Dir.Pos.	250	2000	20	0.00	0	0	--	--	--
10	Spinta terreno	Terreno - Attivo - Dir.Pos.	250	2000	20	0.00	0	0	--	--	--
11	Spinta terreno	Terreno - Attivo - Dir.Pos.	250	200	20	0.00	0	0	--	--	--

Shel I	Cond.	Tipo	Ht	γ	$\emptyset$	c	δ	β	k0	βm	Ag
				0							

She II	Cond.	Tipo	Q	Vert.1	Vert.2	Vert.3	Vert.4	Hw	γ
			kg/mq	kg/mq	kg/mq	kg/mq	kg/mq	cm	kg/mc
1	Peso Proprio	Peso Proprio kg	600						
1	Peso Proprio	Peso Proprio kg	68773						
2	Peso Proprio	Peso Proprio kg	52075						
2	Peso Proprio	Peso Proprio kg	883						
3	Peso Proprio	Peso Proprio kg	23733						
3	Peso Proprio	Peso Proprio kg	1401						
4	Peso Proprio	Peso Proprio kg	14271						
4	Peso Proprio	Peso Proprio kg	2153						
5	Peso Proprio	Peso Proprio kg	15953						
5	Peso Proprio	Peso Proprio kg	1460						
6	Peso Proprio	Peso Proprio kg	6365						
6	Peso Proprio	Peso Proprio kg	251						
7	Peso Proprio	Peso Proprio kg	3922						
7	Peso Proprio	Peso Proprio kg	392						
8	Peso Proprio	Peso Proprio kg	6886						
8	Peso Proprio	Peso Proprio kg	273						
9	Peso Proprio	Peso Proprio kg	534						
9	Peso Proprio	Peso Proprio kg	8561						
10	Peso Proprio	Peso Proprio kg	439						
10	Peso Proprio	Peso Proprio kg	2524						
11	Peso Proprio	Peso Proprio kg	599						
11	Peso Proprio	Peso Proprio kg	11326						
12	Peso Proprio	Peso Proprio kg	928						
13	Peso Proprio	Peso Proprio kg	813						
14	Peso Proprio	Peso Proprio kg	305						
15	Peso Proprio	Peso Proprio kg	780						

Tabella solai tipo

Sol.N°	Descrizione	Spessore	QP	QF	QVar.	ψ_0	ψ_1	ψ_2	Luce netta	Def	%QX	%QY
		cm	kg/mq	kg/mq	kg/mq							
1	Copertura in legno	10	60	360	500	0.00	0.00	0.00	No	No	100	0
2	Copertura in legno_D	20	60	360	300	0.00	0.00	0.00	No	Si	100	0

Dati solai

Solaio n°	Nodi	Tipo
1	6-13-109-25-7	Copertura in legno
1	5-12-13-6	Copertura in legno
1	12-110-26-13	Copertura in legno
1	4-11-12-5	Copertura in legno
1	11-18-110-12	Copertura in legno
1	3-10-11-4	Copertura in legno
1	10-17-18-11	Copertura in legno
1	2-9-10-3	Copertura in legno
1	9-16-17-10	Copertura in legno
1	1-8-9-2	Copertura in legno
1	8-15-16-9	Copertura in legno
1	7-25-108-107	Copertura in legno
1	13-26-109	Copertura in legno
1	104-103-15-8	Copertura in legno

Solaio n°	Nodi	Tipo
1	105-104-8-1-106	Copertura in legno
2	15-1-2-16	Copertura in legno_D
2	1-4-5-2	Copertura in legno_D
2	16-2-3-17	Copertura in legno_D
2	102-101-4-1	Copertura in legno_D
2	103-102-1-15	Copertura in legno_D
2	3-6-112-111	Copertura in legno_D
2	2-5-6-3	Copertura in legno_D
3	17-3-111-110-18	Copertura in legno_D

Tabulati di verifica

L'esito di ogni elaborazione viene sintetizzato nei disegni e schemi grafici allegati, che evidenziano i valori numerici nei punti e/o nelle sezioni significative, ai fini della valutazione del comportamento complessivo della struttura, e quelli necessari ai fini delle verifiche di misura della sicurezza.

Di seguito si riportano le tabelle relative a:

- Forze sismiche e masse
- Spostamenti Relativi dei nodi (SLD)
- Fattori di partecipazione e masse modali
- Massime tensioni sul terreno aste
- Massime tensioni sul terreno platee
- Massimi spostamenti dei nodi
- Massimi spostamenti degli impalcati
- Massime sollecitazioni muri Discretizzati

Risultati Analisi Dinamica - Baricentri masse e masse

Scenario di calcolo: **Set_NT_SLV_SLD_A2_STR/GEO_2018**

Combinazione masse 1

Piano	Rigido	Massa	X	Y	Z
		kg	cm	cm	cm
0	No	0	0	0	0
1	Si	143584	1020	1222	346

Combinazione masse 2

Piano	Rigido	Massa	X	Y	Z
		kg	cm	cm	cm
0	No	0	0	0	0
1	Si	143584	1091	1346	346

Combinazione masse 3

Piano	Rigido	Massa	X	Y	Z
		kg	cm	cm	cm
0	No	0	0	0	0
1	Si	143584	1020	1469	346

Combinazione masse 4

Piano	Rigido	Massa	X	Y	Z
		kg	cm	cm	cm
0	No	0	0	0	0
1	Si	143584	949	1346	346

Verifica Degli Spostamenti Relativi

Scenario di calcolo: **Set_NT_SLV_SLD_A2_STR/GEO_2018**

Interp.	Comb.	ηX_v mm	ηX_h mm	ηY_v mm	ηY_h mm	Nodo1	Nodo2	η mm	ηA_{mm} mm	Cs
0-1	(25+26)-V-3	0.02	1.46	0.02	0.53	5	105	1.47	19.35	13
0-1	(25+26)-VIII-4	0.01	0.53	0.02	1.33	6	104	1.35	19.35	14
0-1	(25+26)-V-3	0.02	1.62	0.02	0.52	7	106	1.64	19.35	12
0-1	(25+26)-VI-3	0.01	1.02	0.04	1.90	8	110	1.95	19.35	9.9
0-1	(25+26)-VII-4	0.10	1.56	0.01	0.36	9	2	1.65	11.00	6.7
0-1	(25+26)-VI-3	0.01	0.46	0.01	1.34	10	3	1.35	11.00	8.1
0-1	(25+26)-VI-3	0.00	0.53	0.00	1.54	11	111	1.54	14.95	9.7
0-1	(25+26)-IV-3	0.02	0.36	0.00	1.02	12	102	1.02	14.95	15
0-1	(25+26)-IV-3	0.00	0.25	0.02	0.72	13	101	0.73	11.85	16
0-1	(25+26)-VIII-4	0.00	0.43	0.03	1.39	14	103	1.42	19.35	14
0-1	(25+26)-V-3	0.03	2.14	0.03	0.59	15	107	2.17	19.35	8.9
0-1	(25+26)-V-3	0.05	1.82	0.10	1.23	16	6	1.87	13.50	7.2
0-1	(25+26)-V-3	0.03	1.83	0.02	1.16	17	7	1.86	13.50	7.2
0-1	(25+26)-V-3	0.03	2.08	0.04	1.47	18	108	2.11	19.35	9.2
0-1	(25+26)-VI-3	0.14	0.58	0.40	0.97	19	10	1.37	11.00	8.0
0-1	(25+26)-VI-3	0.31	0.59	0.66	1.02	20	11	1.68	11.00	6.5
0-1	(25+26)-VI-3	0.02	1.58	0.04	1.79	21	109	1.82	19.35	11
0-1	(25+26)-V-3	0.52	1.09	0.15	1.12	22	14	1.60	11.00	6.9
0-1	(25+26)-V-3	0.78	1.05	0.20	1.18	23	15	1.83	11.00	6.0
0-1	(25+26)-V-3	0.66	1.08	0.18	1.19	24	18	1.75	11.00	6.3
0-1	(25+26)-VI-3	0.19	1.14	0.06	1.38	25	19	1.44	11.00	7.6
0-1	(25+26)-VI-3	0.10	1.00	0.00	1.44	26	22	1.44	11.00	7.6
0-1	(25+26)-VI-3	0.40	0.93	0.06	1.60	27	23	1.66	11.00	6.6
0-1	(25+26)-VI-3	0.42	0.93	0.06	1.61	28	26	1.67	11.00	6.6
0-1	(25+26)-VI-3	0.40	0.92	0.05	1.60	29	27	1.65	11.00	6.7
0-1	(25+26)-VI-3	0.38	0.93	0.04	1.60	30	30	1.64	11.00	6.7
0-1	(25+26)-VI-3	0.13	0.78	0.01	1.43	31	31	1.44	11.00	7.6
0-1	(25+26)-VI-3	0.00	0.49	0.01	1.35	32	2	1.36	11.00	8.1
0-1	(25+26)-VI-3	0.03	0.75	0.02	1.30	33	3	1.32	11.00	8.3
0-1	(25+26)-VI-3	0.01	0.55	0.01	1.32	34	112	1.34	11.85	8.9
0-1	(25+26)-IV-3	0.00	0.36	0.03	1.03	35	38	1.06	10.50	9.9
0-1	(25+26)-VIII-3	0.02	0.39	0.02	1.14	36	39	1.16	10.50	9.1
0-1	(25+26)-VIII-4	0.00	0.00	0.00	0.00	106	206	0.00	1.00	>100
0-1	(25+26)-VIII-4	0.00	0.00	0.00	0.00	112	212	0.00	12.50	>100
0-1	(25+26)-VIII-4	0.00	0.00	0.00	0.00	113	213	0.00	12.50	>100
0-1	(25+26)-VIII-4	0.00	0.00	0.00	0.00	114	214	0.00	7.50	>100
0-1	(25+26)-VIII-4	0.00	0.00	0.00	0.00	134	234	0.00	12.50	>100
0-0	(25+26)-VIII-4	0.00	0.00	0.00	0.00	213	313	0.00	12.50	>100
Minimo										
0-1	(25+26)-V-3	0.78	1.05	0.20	1.18	23	15	1.83	11.00	6.0

Periodi di vibrazione e Masse modali

Scenario di calcolo: **Set_NT_SLV_SLD_A2_STR/GEO_2018**

Posizione masse 1

Numero di Frequenze calcolate =15, filtrate=9

N	T s	Coeff. Partecipazione		Masse Modali kgm*g		Percentuali	
		Dir=0°	Dir=90°	Dir=0°	Dir=90°	Dir=0°	Dir=90°
1(1)	0.1778	29.616	-1.088	8601	12	6.46	0.01
2(2)	0.1613	56.582	-91.465	31396	82041	23.58	61.61
3(3)	0.1513	30.770	2.295	9285	52	6.97	0.04
4(4)	0.1262	-74.378	-62.107	54251	37827	40.74	28.41
5(5)	0.1035	29.473	14.370	8519	2025	6.40	1.52
6(6)	0.1002	-20.663	5.093	4187	254	3.14	0.19
7(7)	0.0907	7.650	1.070	574	11	0.43	0.01
8(8)	0.0861	-14.787	-3.312	2144	108	1.61	0.08
9(15)	0.0491	-19.141	-7.204	3593	509	2.70	0.38
Somma delle Masse Modali [kgm*g]				122551	122839		
Masse strutturali libere [kgm*g]				133165	133165		
Percentuale				92.03	92.25	92.03	92.25

Masse e coefficienti di partecipazione rotazionali:

N	T(s)	Coeff. Partecipazione		Masse Modali kgm*g		Percentuali	
1	0.1778	96.851		91988		1.15	
2	0.1613	-79.958		62697		0.78	
3	0.1513	67.784		45059		0.56	
4	0.1262	93.258		85288		1.07	
5	0.1035	-53.846		28434		0.36	
6	0.1002	-626.009		3843103		48.03	
7	0.0907	57.268		32163		0.40	
8	0.0861	-17.563		3025		0.04	
9	0.0686	-91.510		82122		1.03	
10	0.0591	83.228		67929		0.85	
11	0.0571	23.262		5306		0.07	
12	0.0561	3.146		97		0.00	
13	0.0557	1.101		12		0.00	
14	0.0496	-29.025		8261		0.10	
15	0.0491	-273.093		731380		9.14	

Posizione masse 2

Numero di Frequenze calcolate =15, filtrate=9

N	T s	Coeff. Partecipazione		Masse Modali kgm*g		Percentuali	
		Dir=0°	Dir=90°	Dir=0°	Dir=90°	Dir=0°	Dir=90°
1(1)	0.1964	25.818	2.593	6537	66	4.91	0.05
2(2)	0.1693	63.290	-88.238	39281	76354	29.50	57.34
3(3)	0.1318	77.783	63.204	59333	39175	44.56	29.42
4(4)	0.1221	-14.861	-21.399	2166	4490	1.63	3.37
5(5)	0.1031	-0.357	23.076	1	5222	0.00	3.92
6(6)	0.0985	-29.820	-0.769	8720	6	6.55	0.00
7(7)	0.0893	25.185	4.996	6220	245	4.67	0.18
8(9)	0.0730	5.790	1.934	329	37	0.25	0.03
9(15)	0.0486	-4.334	-2.117	184	44	0.14	0.03
Somma delle Masse Modali [kgm*g]				122771	125638		
Masse strutturali libere [kgm*g]				133165	133165		
Percentuale				92.20	94.35	92.20	94.35

Masse e coefficienti di partecipazione rotazionali:

N	T(s)	Coeff. Partecipazione	Masse Modali kgm*g	Percentuali
1	0.1964	63.191	39159	0.49
2	0.1693	-230.243	519869	6.51
3	0.1318	-83.012	67578	0.85
4	0.1221	154.188	233144	2.92
5	0.1031	-374.778	1377425	17.26
6	0.0985	-368.747	1333451	16.71
7	0.0893	209.987	432421	5.42
8	0.0771	-43.655	18689	0.23
9	0.0730	-79.809	62464	0.78
10	0.0622	-7.716	584	0.01
11	0.0583	-0.246	1	0.00
12	0.0565	-18.560	3378	0.04
13	0.0530	-6.244	382	0.00
14	0.0502	7.197	508	0.01
15	0.0486	-129.514	164497	2.06

Posizione masse 3

Numero di Frequenze calcolate =15, filtrate=8

N	T	Coeff. Partecipazione		Masse Modali		Percentuali	
	s			kgm*g			
		Dir=0°	Dir=90°	Dir=0°	Dir=90°	Dir=0°	Dir=90°
1(1)	0.1739	66.838	-46.772	43810	21453	32.90	16.11
2(2)	0.1704	39.642	-65.129	15411	41598	11.57	31.24
3(3)	0.1369	70.325	79.471	48500	61935	36.42	46.51
4(4)	0.1125	7.978	-7.085	624	492	0.47	0.37
5(5)	0.1037	-25.872	9.590	6564	902	4.93	0.68
6(6)	0.0831	-27.771	-8.449	7563	700	5.68	0.53
7(7)	0.0768	16.574	5.170	2694	262	2.02	0.20
8(11)	0.0627	5.198	1.456	265	21	0.20	0.02
Somma delle Masse Modali [kgm*g]				125431	127363		
Masse strutturali libere [kgm*g]				133165	133165		
Percentuale				94.19	95.64	94.19	95.64

Masse e coefficienti di partecipazione rotazionali:

N	T(s)	Coeff. Partecipazione	Masse Modali kgm*g	Percentuali
1	0.1739	-130.998	168286	2.13
2	0.1704	-229.739	517596	6.56
3	0.1369	-262.148	673927	8.54
4	0.1125	183.082	328709	4.16
5	0.1037	-381.869	1430041	18.12
6	0.0831	-243.020	579170	7.34
7	0.0768	112.018	123054	1.56
8	0.0710	-4.037	160	0.00
9	0.0657	43.752	18772	0.24
10	0.0639	7.986	625	0.01
11	0.0627	-80.083	62893	0.80
12	0.0603	-1.944	37	0.00
13	0.0525	-6.841	459	0.01
14	0.0521	-5.725	321	0.00
15	0.0470	0.828	7	0.00

Posizione masse 4

Numero di Frequenze calcolate =15, filtrate=7

N	T	Coeff. Partecipazione	Masse Modali	Percentuali
	s		kgm*g	

N	T	Coeff. Partecipazione		Masse Modali		Percentuali	
		Dir=0°	Dir=90°	Dir=0°	Dir=90°	Dir=0°	Dir=90°
1(1)	0.1635	-72.887	82.220	52098	66294	39.12	49.78
2(2)	0.1508	-21.190	-29.930	4403	8785	3.31	6.60
3(3)	0.1429	30.346	17.499	9031	3003	6.78	2.26
4(4)	0.1320	-63.977	-67.669	40140	44906	30.14	33.72
5(5)	0.1038	-19.913	-1.006	3889	10	2.92	0.01
6(6)	0.0898	-31.129	-9.809	9503	944	7.14	0.71
7(7)	0.0786	16.340	4.169	2618	170	1.97	0.13
Somma delle Masse Modali [kgm*g]				121681	124112		
Masse strutturali libere [kgm*g]				133165	133165		
Percentuale				91.38	93.20	91.38	93.20

Masse e coefficienti di partecipazione rotazionali:

N	T(s)	Coeff. Partecipazione	Masse Modali kgm*g	Percentuali
1	0.1635	77.077	58260	0.74
2	0.1508	-89.368	78322	0.99
3	0.1429	-19.571	3756	0.05
4	0.1320	309.404	938796	11.86
5	0.1038	-459.978	2074886	26.22
6	0.0898	-274.747	740263	9.35
7	0.0786	76.579	57510	0.73
8	0.0722	55.745	30475	0.39
9	0.0671	-7.221	511	0.01
10	0.0587	-3.389	113	0.00
11	0.0584	-25.337	6295	0.08
12	0.0583	68.003	45350	0.57
13	0.0554	77.588	59035	0.75
14	0.0529	8.284	673	0.01
15	0.0518	2.082	43	0.00

Risultati Analisi Dinamica - Massime tensioni sul terreno aste

Scenario di calcolo: **Set_NT_SLV_SLD_A2_STR/GEO_2018**

Asta	N.in.	N.fin.	0/5	1/5	2/5	3/5	4/5	5/5
			kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq
9001	5	6	0.26(8-II-3)	0.21(8-II-3)	0.19(2)	0.19(2)	0.21(2)	0.22(2)
9001	6	14	0.22(2)	0.19(2)	0.16(2)	0.15(2)	0.16(2)	0.18(2)
9001	14	12	0.18(2)	0.18(2)	0.17(2)	0.17(2)	0.17(2)	0.17(2)
9001	12	13	0.17(2)	0.17(2)	0.16(2)	0.16(2)	0.17(2)	0.17(2)
9002	7	5	0.31(2)	0.29(2)	0.27(9-I-2)	0.27(9-I-2)	0.26(9-I-2)	0.27(8-II-3)
9003	9	10	0.19(2)	0.18(2)	0.18(2)	0.18(2)	0.18(2)	0.17(2)
9003	8	9	0.21(2)	0.21(2)	0.21(2)	0.20(2)	0.20(2)	0.19(2)
9003	26	27	0.25(2)	0.24(2)	0.22(2)	0.20(2)	0.18(2)	0.17(2)
9003	24	25	0.22(2)	0.23(2)	0.23(2)	0.24(2)	0.25(2)	0.25(2)
9003	33	34	0.16(2)	0.16(2)	0.16(2)	0.16(2)	0.16(2)	0.17(2)
9003	11	32	0.17(2)	0.17(2)	0.17(2)	0.17(2)	0.17(2)	0.17(2)
9003	29	30	0.15(2)	0.15(2)	0.15(2)	0.15(2)	0.15(2)	0.15(2)
9003	32	33	0.17(2)	0.17(2)	0.16(2)	0.16(2)	0.16(2)	0.16(2)
9003	21	26	0.26(2)	0.26(2)	0.26(2)	0.26(2)	0.26(2)	0.25(2)
9003	134	34	0.18(2)	0.18(2)	0.17(2)	0.17(2)	0.17(2)	0.17(2)
9003	23	24	0.20(2)	0.21(2)	0.21(2)	0.21(2)	0.22(2)	0.22(2)
9003	27	28	0.17(2)	0.17(2)	0.16(2)	0.16(2)	0.16(2)	0.16(2)
9003	22	23	0.18(2)	0.18(2)	0.19(2)	0.19(2)	0.20(2)	0.20(2)
9003	18	22	0.23(9-I-3)	0.21(9-I-3)	0.19(9-I-3)	0.18(2)	0.18(2)	0.18(2)
9003	31	8	0.20(2)	0.21(2)	0.21(2)	0.21(2)	0.21(2)	0.21(2)
9003	28	29	0.16(2)	0.15(2)	0.14(2)	0.14(2)	0.14(2)	0.15(2)

Asta	N.in.	N.fin.	0/5	1/5	2/5	3/5	4/5	5/5
9003	25	21	0.25(2)	0.25(2)	0.26(2)	0.26(2)	0.26(2)	0.26(2)
9003	30	31	0.15(2)	0.16(2)	0.17(2)	0.18(2)	0.19(2)	0.20(2)
9003	10	11	0.17(2)	0.17(2)	0.17(2)	0.17(2)	0.17(2)	0.17(2)
9004	7	15	0.32(2)	0.29(2)	0.32(2)	0.33(2)	0.27(2)	0.31(2)
9005	16	17	0.28(2)	0.27(2)	0.26(9-I-3)	0.26(9-I-3)	0.26(9-I-3)	0.25(9-I-3)
9005	15	16	0.30(2)	0.30(2)	0.29(2)	0.29(2)	0.28(2)	0.28(2)
9005	17	18	0.25(9-I-3)	0.25(9-I-3)	0.25(9-I-3)	0.25(9-I-3)	0.25(9-I-3)	0.25(9-I-3)
9006	14	19	0.18(2)	0.19(2)	0.21(2)	0.22(2)	0.23(2)	0.22(2)
9006	20	8	0.22(2)	0.23(2)	0.22(2)	0.22(2)	0.22(2)	0.22(2)
9006	19	20	0.22(2)	0.22(2)	0.22(2)	0.22(2)	0.22(2)	0.22(2)
9007	6	106	0.21(2)	0.20(2)	0.19(2)	0.18(2)	0.18(2)	0.17(2)
9007	6	21	0.21(2)	0.31(2)	0.36(2)	0.37(2)	0.33(2)	0.25(2)
9008	12	35	0.17(2)	0.17(2)	0.17(2)	0.17(2)	0.17(2)	0.17(2)
9008	35	36	0.17(2)	0.17(2)	0.17(2)	0.17(2)	0.17(2)	0.17(2)
9008	36	11	0.17(2)	0.18(2)	0.18(2)	0.18(2)	0.17(2)	0.17(2)
9009	13	34	0.17(2)	0.17(2)	0.17(2)	0.17(2)	0.17(2)	0.17(2)
9010	106	114	0.17(2)	0.17(2)	0.17(2)	0.17(2)	0.17(2)	0.17(2)
9010	114	112	0.17(2)	0.18(2)	0.18(2)	0.18(2)	0.18(2)	0.18(2)
9010	112	213	0.18(2)	0.18(2)	0.18(2)	0.18(2)	0.18(2)	0.18(2)
9011	113	134	0.18(2)	0.18(2)	0.18(2)	0.18(2)	0.18(2)	0.18(2)
9011	213	113	0.18(2)	0.18(2)	0.18(2)	0.18(2)	0.18(2)	0.18(2)
9012	13	213	0.17(2)	0.17(2)	0.17(2)	0.18(2)	0.18(2)	0.18(2)

Risultati Analisi Dinamica - Sollecitazioni massime - Sigma terreno platea

Scenario di calcolo: **Set_NT_SLV_SLD_A2_STR/GEO_2018**

Muro	Cx mm	Cy mm	Cz mm	Sigma kg/cm ²
1	174	17670	0	0.23(8-II-3)
1	480	20130	-0	0.29(2)
1	11180	27440	-0	0.28(2)
1	14600	20620	-0	0.25(2)
1	3660	13150	-0	0.21(2)
1	14290	22141	-0	0.22(2)
1	14088	23128	-0	0.20(2)
1	13848	24303	-0	0.17(2)
1	13390	26550	-0	0.22(9-I-3)
1	11644	27253	-0	0.26(2)
1	12757	26805	-0	0.22(9-I-3)
1	14490	21161	-0	0.24(2)
1	225	18080	-0	0.23(9-I-2)
1	276	18490	-0	0.23(9-I-2)
1	327	18900	-0	0.23(9-I-2)
1	378	19310	-0	0.25(2)
1	429	19720	-0	0.27(2)
1	10846	27212	-0	0.28(2)
1	10512	26983	-0	0.27(2)
1	10177	26755	-0	0.26(2)
1	9843	26526	-0	0.25(2)
1	9508	26298	-0	0.25(2)
1	9174	26070	-0	0.24(2)
1	8840	25841	-0	0.24(2)
1	8505	25613	-0	0.24(2)
1	8171	25384	-0	0.25(2)
1	7836	25156	-0	0.26(2)
1	7502	24927	-0	0.27(2)
1	7168	24699	-0	0.28(2)

Muro	Cx	Cy	Cz	Sigma
1	6833	24470	-0	0.29(2)
1	6499	24242	-0	0.30(2)
1	6165	24014	-0	0.31(2)
1	5830	23785	-0	0.31(2)
1	5496	23557	-0	0.30(2)
1	5161	23328	-0	0.29(2)
1	4827	23100	-0	0.28(2)
1	4493	22871	-0	0.27(2)
1	4158	22643	-0	0.26(2)
1	3824	22414	-0	0.25(2)
1	3489	22186	-0	0.25(2)
1	3155	21958	-0	0.24(2)
1	2821	21729	-0	0.25(2)
1	2486	21501	-0	0.25(2)
1	2152	21272	-0	0.26(2)
1	1818	21044	-0	0.27(2)
1	1483	20815	-0	0.28(2)
1	1149	20587	-0	0.28(2)
1	814	20358	-0	0.28(2)
1	14278	20400	-0	0.26(2)
1	13956	20181	-0	0.27(2)
1	13635	19961	-0	0.28(2)
1	13313	19741	-0	0.30(2)
1	12991	19521	-0	0.31(2)
1	12669	19302	-0	0.32(2)
1	12348	19082	-0	0.33(2)
1	12026	18862	-0	0.34(2)
1	11704	18643	-0	0.35(2)
1	11382	18423	-0	0.35(2)
1	11061	18203	-0	0.36(2)
1	10739	17984	-0	0.36(2)
1	10417	17764	-0	0.37(2)
1	10095	17544	-0	0.37(2)
1	9773	17324	-0	0.37(2)
1	9452	17105	-0	0.37(2)
1	9130	16885	-0	0.37(2)
1	8808	16665	-0	0.37(2)
1	8486	16446	-0	0.36(2)
1	8165	16226	-0	0.36(2)
1	7843	16006	-0	0.36(2)
1	7521	15787	-0	0.35(2)
1	7199	15567	-0	0.35(2)
1	6878	15347	-0	0.34(2)
1	6556	15127	-0	0.33(2)
1	6234	14908	-0	0.32(2)
1	5912	14688	-0	0.31(2)
1	5591	14468	-0	0.30(2)
1	5269	14249	-0	0.28(2)
1	4947	14029	-0	0.27(2)
1	4625	13809	-0	0.25(2)
1	4303	13589	-0	0.23(2)
1	3982	13370	-0	0.22(2)
1	14189	22634	-0	0.21(2)
1	13772	24678	-0	0.17(2)
1	13695	25052	-0	0.17(2)
1	13619	25427	-0	0.18(2)
1	13543	25801	-0	0.18(2)
1	13466	26176	-0	0.20(9-I-3)
1	3411	13473	-0	0.21(2)
1	3162	13796	-0	0.20(2)
1	2913	14119	-0	0.20(2)
1	2664	14441	-0	0.20(2)
1	2415	14764	-0	0.19(2)
1	2166	15087	-0	0.19(2)

Muro	Cx	Cy	Cz	Sigma
1	1917	15410	-0	0.18(2)
1	1668	15733	-0	0.18(2)
1	1419	16056	-0	0.18(2)
1	1170	16379	-0	0.18(2)
1	921	16701	-0	0.19(8-II-3)
1	672	17024	-0	0.20(8-II-3)
1	423	17347	-0	0.22(8-II-3)
1	11412	27347	-0	0.27(2)
1	12200	27029	-0	0.23(2)
1	13073	26678	-0	0.22(9-I-3)
1	13968	23715	-0	0.18(2)
1	14390	21651	-0	0.23(2)
1	14545	20891	-0	0.25(2)
1	812	19927	-0	0.26(2)
1	725	19601	-0	0.25(2)
1	636	19254	-0	0.23(2)
1	602	18888	-0	0.22(2)
1	558	18521	-0	0.21(9-I-1)
1	607	18128	-0	0.21(9-I-1)
1	556	17755	-0	0.21(8-II-3)
1	697	17460	-0	0.20(8-II-3)
1	914	17163	-0	0.19(8-II-3)
1	1157	16854	-0	0.18(2)
1	1406	16543	-0	0.17(2)
1	1651	16250	-0	0.17(2)
1	1945	15990	-0	0.17(2)
1	2222	15634	-0	0.18(2)
1	2451	15276	-0	0.18(2)
1	2683	14941	-0	0.19(2)
1	2922	14616	-0	0.20(2)
1	3163	14303	-0	0.20(2)
1	3421	14014	-0	0.21(2)
1	3748	13753	-0	0.22(2)
1	4130	13888	-0	0.23(2)
1	4451	14080	-0	0.25(2)
1	4767	14298	-0	0.26(2)
1	5097	14528	-0	0.28(2)
1	5440	14754	-0	0.29(2)
1	5763	14920	-0	0.30(2)
1	6054	15128	-0	0.31(2)
1	6370	15363	-0	0.32(2)
1	6716	15612	-0	0.33(2)
1	7089	15859	-0	0.34(2)
1	7421	16012	-0	0.35(2)
1	7722	16213	-0	0.35(2)
1	8002	16456	-0	0.36(2)
1	8337	16632	-0	0.36(2)
1	8619	16844	-0	0.36(2)
1	8862	17099	-0	0.36(2)
1	9230	17368	-0	0.36(2)
1	9596	17584	-0	0.36(2)
1	9942	17791	-0	0.36(2)
1	10278	17998	-0	0.36(2)
1	10605	18198	-0	0.36(2)
1	10903	18396	-0	0.36(2)
1	11176	18635	-0	0.35(2)
1	11515	18872	-0	0.34(2)
1	11858	19098	-0	0.33(2)
1	12193	19323	-0	0.32(2)
1	12520	19548	-0	0.31(2)
1	12846	19748	-0	0.30(2)
1	13158	19956	-0	0.29(2)
1	13463	20180	-0	0.28(2)
1	13787	20397	-0	0.27(2)

Muro	Cx	Cy	Cz	Sigma
1	14095	20578	-0	0.26(2)
1	14324	20700	-0	0.25(2)
1	14256	20904	-0	0.25(2)
1	14160	21211	-0	0.24(2)
1	14054	21636	-0	0.23(2)
1	13946	22109	-0	0.22(2)
1	13845	22596	-0	0.20(2)
1	13739	23072	-0	0.19(2)
1	13564	23571	-0	0.17(2)
1	13455	24165	-0	0.17(2)
1	13453	24602	-0	0.17(2)
1	13398	24992	-0	0.17(2)
1	13331	25384	-0	0.17(2)
1	13264	25765	-0	0.18(2)
1	13213	26110	-0	0.19(2)
1	13186	26367	-0	0.20(9-I-3)
1	12940	26426	-0	0.20(9-I-3)
1	12564	26518	-0	0.20(2)
1	12014	26656	-0	0.22(2)
1	11591	26934	-0	0.24(2)
1	11320	27087	-0	0.25(2)
1	11147	27187	-0	0.27(2)
1	10950	27019	-0	0.26(2)
1	10686	26791	-0	0.25(2)
1	10385	26538	-0	0.24(2)
1	10057	26273	-0	0.23(2)
1	9703	26021	-0	0.22(2)
1	9348	25787	-0	0.22(2)
1	9000	25561	-0	0.21(2)
1	8653	25338	-0	0.22(2)
1	8309	25123	-0	0.22(2)
1	7971	24918	-0	0.24(2)
1	7663	24718	-0	0.25(2)
1	7385	24476	-0	0.25(2)
1	7043	24234	-0	0.26(2)
1	6719	23995	-0	0.27(2)
1	6430	23685	-0	0.27(2)
1	6065	23303	-0	0.25(2)
1	5575	23186	-0	0.26(2)
1	5261	23142	-0	0.27(2)
1	5064	22900	-0	0.26(2)
1	4698	22617	-0	0.24(2)
1	4335	22425	-0	0.23(2)
1	4015	22201	-0	0.23(2)
1	3696	21960	-0	0.22(2)
1	3378	21708	-0	0.22(2)
1	3051	21439	-0	0.22(2)
1	2674	21185	-0	0.23(2)
1	2316	21019	-0	0.24(2)
1	1996	20810	-0	0.25(2)
1	1668	20588	-0	0.25(2)
1	1347	20369	-0	0.26(2)
1	1050	20154	-0	0.26(2)
1	6467	22530	-0	0.17(2)
1	7345	21741	-0	0.09(2)
1	7974	21076	-0	0.08(4)
1	8618	20450	-0	0.10(2)
1	8624	19615	-0	0.15(2)
1	8998	19116	-0	0.21(2)
1	9304	18660	-0	0.26(2)
1	9592	18357	-0	0.31(2)
1	9775	18066	-0	0.34(2)
1	13672	21577	-0	0.22(2)
1	13205	21458	-0	0.22(2)

Muro	Cx	Cy	Cz	Sigma
1	12631	21266	-0	0.20(2)
1	11885	21063	-0	0.19(2)
1	10891	20974	-0	0.15(2)
1	9739	20451	-0	0.14(2)
1	12844	20654	-0	0.25(2)
1	13229	20412	-0	0.27(2)
1	13946	20820	-0	0.26(2)
1	13791	21147	-0	0.24(2)
1	13587	20652	-0	0.26(2)
1	13357	20978	-0	0.24(2)
1	11159	20067	-0	0.23(2)
1	11470	19675	-0	0.28(2)
1	11671	19370	-0	0.31(2)
1	12976	20170	-0	0.28(2)
1	12687	19987	-0	0.29(2)
1	12347	19848	-0	0.30(2)
1	12025	19596	-0	0.31(2)
1	12114	20279	-0	0.26(2)
1	12537	20201	-0	0.27(2)
1	12786	20342	-0	0.27(2)
1	11870	19850	-0	0.28(2)
1	9792	18943	-0	0.27(2)
1	10313	19166	-0	0.28(2)
1	10757	19255	-0	0.29(2)
1	11134	19436	-0	0.29(2)
1	10296	19726	-0	0.22(2)
1	10683	19557	-0	0.26(2)
1	10992	19686	-0	0.26(2)
1	9599	19399	-0	0.21(2)
1	9321	19821	-0	0.17(2)
1	10419	18753	-0	0.32(2)
1	10481	18439	-0	0.34(2)
1	10130	18267	-0	0.34(2)
1	9983	18580	-0	0.31(2)
1	11303	19134	-0	0.32(2)
1	10884	18866	-0	0.33(2)
1	10756	18567	-0	0.34(2)
1	8823	25045	-0	0.19(2)
1	9042	24736	-0	0.16(2)
1	9397	24391	-0	0.13(2)
1	9318	23683	-0	0.10(2)
1	9689	23021	-0	0.08(2)
1	10042	22355	-0	0.08(4)
1	10394	21682	-0	0.10(2)
1	8149	22241	-0	0.09(2)
1	8936	22617	-0	0.08(2)
1	8586	21596	-0	0.08(4)
1	9288	21966	-0	0.08(4)
1	9587	21300	-0	0.10(2)
1	8930	21115	-0	0.09(2)
1	7723	23016	-0	0.14(2)
1	7398	23557	-0	0.19(2)
1	7259	23957	-0	0.23(2)
1	6802	23393	-0	0.22(2)
1	6926	23782	-0	0.24(2)
1	8790	24192	-0	0.15(2)
1	8309	24006	-0	0.16(2)
1	7847	23825	-0	0.18(2)
1	8605	23240	-0	0.11(2)
1	8442	23647	-0	0.14(2)
1	8004	23496	-0	0.15(2)
1	8850	23841	-0	0.13(2)
1	8097	24667	-0	0.21(2)
1	8173	24361	-0	0.19(2)

Muro	Cx	Cy	Cz	Sigma
1	8613	24533	-0	0.17(2)
1	8460	24842	-0	0.20(2)
1	7694	24233	-0	0.21(2)
1	7818	24539	-0	0.22(2)
1	13050	23317	-0	0.16(2)
1	12276	23237	-0	0.12(2)
1	11493	23081	-0	0.10(2)
1	10755	22740	-0	0.09(2)
1	12499	21881	-0	0.17(2)
1	12377	22522	-0	0.14(2)
1	11698	22359	-0	0.12(2)
1	11839	21727	-0	0.15(2)
1	11030	22096	-0	0.10(2)
1	11253	21599	-0	0.13(2)
1	13551	22064	-0	0.20(2)
1	13067	22002	-0	0.19(2)
1	13462	22563	-0	0.19(2)
1	12989	22601	-0	0.17(2)
1	13417	22984	-0	0.18(2)
1	11170	23945	-0	0.10(2)
1	10289	24591	-0	0.12(2)
1	10136	25272	-0	0.16(2)
1	9918	25692	-0	0.19(2)
1	9710	25138	-0	0.16(2)
1	9361	24968	-0	0.16(2)
1	9536	25471	-0	0.19(2)
1	9180	25262	-0	0.19(2)
1	10409	23403	-0	0.08(2)
1	10005	23892	-0	0.10(2)
1	9842	24820	-0	0.14(2)
1	9533	24726	-0	0.14(2)
1	12904	24166	-0	0.15(2)
1	12110	24002	-0	0.12(2)
1	12672	24756	-0	0.15(2)
1	12560	25270	-0	0.16(2)
1	12516	25738	-0	0.17(2)
1	12512	26150	-0	0.19(2)
1	12983	25332	-0	0.17(2)
1	13055	24912	-0	0.16(2)
1	13137	24560	-0	0.16(2)
1	12921	25739	-0	0.18(2)
1	12896	26106	-0	0.19(2)
1	11401	26698	-0	0.23(2)
1	11221	26410	-0	0.21(2)
1	10986	26047	-0	0.19(2)
1	10653	25624	-0	0.17(2)
1	10648	26295	-0	0.22(2)
1	10319	25971	-0	0.20(2)
1	11146	26853	-0	0.24(2)
1	10925	26587	-0	0.23(2)
1	11961	25219	-0	0.14(2)
1	11167	25172	-0	0.14(2)
1	12058	24645	-0	0.13(2)
1	11465	24587	-0	0.12(2)
1	12033	26209	-0	0.19(2)
1	11988	25746	-0	0.17(2)
1	11591	26249	-0	0.20(2)
1	11669	26534	-0	0.21(2)
1	11433	25803	-0	0.17(2)
1	7570	19109	-0	0.13(2)
1	6637	18152	-0	0.15(2)
1	5901	17439	-0	0.16(2)
1	5220	16956	-0	0.16(2)
1	4539	16592	-0	0.15(2)

Muro	Cx	Cy	Cz	Sigma
1	4058	16081	-0	0.17(2)
1	3605	15660	-0	0.17(2)
1	3281	15343	-0	0.18(2)
1	2975	15132	-0	0.19(2)
1	7032	16289	-0	0.32(2)
1	6413	16733	-0	0.25(2)
1	8018	18020	-0	0.24(2)
1	8415	17310	-0	0.33(2)
1	8816	18269	-0	0.27(2)
1	8461	18831	-0	0.20(2)
1	8972	17703	-0	0.33(2)
1	9408	17877	-0	0.34(2)
1	9272	18168	-0	0.31(2)
1	7747	16773	-0	0.33(2)
1	7204	17420	-0	0.24(2)
1	7355	16230	-0	0.34(2)
1	7608	16405	-0	0.34(2)
1	8173	16794	-0	0.35(2)
1	8402	16983	-0	0.35(2)
1	4418	15567	-0	0.20(2)
1	4657	15159	-0	0.24(2)
1	4906	14843	-0	0.26(2)
1	5637	16368	-0	0.22(2)
1	5900	15924	-0	0.27(2)
1	6165	15633	-0	0.30(2)
1	6549	15927	-0	0.31(2)
1	6287	16195	-0	0.28(2)
1	5516	15565	-0	0.27(2)
1	5298	15133	-0	0.27(2)
1	5844	15362	-0	0.30(2)
1	5635	15138	-0	0.29(2)
1	5020	15894	-0	0.22(2)
1	4992	15395	-0	0.24(2)
1	3201	14802	-0	0.20(2)
1	3519	14990	-0	0.20(2)
1	3948	15177	-0	0.20(2)
1	3662	14665	-0	0.21(2)
1	3841	14406	-0	0.22(2)
1	4010	14167	-0	0.23(2)
1	3409	14497	-0	0.21(2)
1	3615	14238	-0	0.22(2)
1	3791	14053	-0	0.22(2)
1	4565	14586	-0	0.25(2)
1	4276	14357	-0	0.24(2)
1	4312	14880	-0	0.23(2)
1	4080	14612	-0	0.23(2)
1	3897	14818	-0	0.21(2)
1	3867	17470	-0	0.10(2)
1	3235	18313	-0	0.10(2)
1	2767	18935	-0	0.12(2)
1	2296	19495	-0	0.16(2)
1	2088	20007	-0	0.19(2)
1	1870	20328	-0	0.22(2)
1	2275	18569	-0	0.13(2)
1	1780	18274	-0	0.15(2)
1	1315	18094	-0	0.17(2)
1	1109	17790	-0	0.18(2)
1	928	17584	-0	0.19(8-II-3)
1	1246	19944	-0	0.24(2)
1	1398	19669	-0	0.21(2)
1	1612	19356	-0	0.19(2)
1	1926	19040	-0	0.16(2)
1	1722	19848	-0	0.21(2)
1	1877	19567	-0	0.18(2)

Muro	Cx	Cy	Cz	Sigma
1	1546	20122	-0	0.23(2)
1	871	17952	-0	0.19(9-I-1)
1	785	17763	-0	0.20(8-II-3)
1	926	18863	-0	0.20(2)
1	1274	19114	-0	0.20(2)
1	1054	19479	-0	0.22(2)
1	1038	19783	-0	0.24(2)
1	872	19199	-0	0.22(2)
1	1530	18734	-0	0.17(2)
1	1159	18507	-0	0.18(2)
1	885	18335	-0	0.19(2)
1	790	18573	-0	0.20(2)
1	1024	18127	-0	0.18(2)
1	2633	18035	-0	0.11(2)
1	2031	17712	-0	0.14(2)
1	1703	17288	-0	0.15(2)
1	1416	17044	-0	0.17(2)
1	1380	17544	-0	0.16(2)
1	1160	17334	-0	0.17(2)
1	1575	17784	-0	0.15(2)
1	3176	16087	-0	0.15(2)
1	2946	16782	-0	0.13(2)
1	2498	17235	-0	0.13(2)
1	3701	16546	-0	0.14(2)
1	3000	17580	-0	0.11(2)
1	2270	16392	-0	0.15(2)
1	2033	16906	-0	0.15(2)
1	1676	16732	-0	0.16(2)
1	1866	16458	-0	0.16(2)
1	2769	15474	-0	0.18(2)
1	2609	15897	-0	0.16(2)
1	3075	15635	-0	0.17(2)
1	5842	18653	-0	0.10(2)
1	5530	19353	-0	0.08(4)
1	5167	19951	-0	0.08(4)
1	4788	20512	-0	0.10(2)
1	4433	21038	-0	0.13(2)
1	4195	21444	-0	0.16(2)
1	3932	21714	-0	0.19(2)
1	6838	21152	-0	0.09(2)
1	6311	20678	-0	0.08(4)
1	5738	20299	-0	0.08(4)
1	6848	20009	-0	0.08(2)
1	6161	19703	-0	0.08(4)
1	6524	19155	-0	0.10(2)
1	7376	20566	-0	0.08(4)
1	7855	20042	-0	0.10(2)
1	4951	22244	-0	0.20(2)
1	5553	21858	-0	0.15(2)
1	5888	21263	-0	0.11(2)
1	6397	21648	-0	0.11(2)
1	5514	22715	-0	0.22(2)
1	4967	21385	-0	0.13(2)
1	5345	20865	-0	0.10(2)
1	4249	21980	-0	0.20(2)
1	4590	21763	-0	0.17(2)
1	4511	22216	-0	0.21(2)
1	2841	19873	-0	0.14(2)
1	3318	20303	-0	0.14(2)
1	3842	20775	-0	0.14(2)
1	2853	20744	-0	0.19(2)
1	3630	21443	-0	0.19(2)
1	3344	21100	-0	0.18(2)
1	3889	21221	-0	0.16(2)

Muro	Cx	Cy	Cz	Sigma
1	2494	20300	-0	0.18(2)
1	2203	20558	-0	0.22(2)
1	2457	20773	-0	0.21(2)
1	4631	19623	-0	0.08(4)
1	4129	19242	-0	0.08(2)
1	3656	18813	-0	0.09(2)
1	5319	17938	-0	0.11(2)
1	4708	18200	-0	0.09(2)
1	4450	18721	-0	0.08(4)
1	3991	18335	-0	0.09(2)
1	4802	17455	-0	0.12(2)
1	4948	19088	-0	0.08(4)
1	5166	18647	-0	0.08(2)
1	3739	19771	-0	0.10(2)
1	4250	20170	-0	0.10(2)
1	3251	19348	-0	0.11(2)
2	16390	11820	-0	0.21(2)
2	13001	10483	0	0.22(2)
2	11327	9822	0	0.22(2)
2	7420	8280	0	0.18(2)
2	14600	20620	-0	0.25(2)
2	3660	13150	-0	0.21(2)
2	14759	19836	-0	0.24(2)
2	15198	17680	-0	0.17(2)
2	15258	17386	-0	0.16(2)
2	15736	15034	-0	0.14(2)
2	15796	14740	-0	0.15(2)
2	16274	12389	-0	0.20(2)
2	16051	11686	-0	0.21(2)
2	15712	11553	-0	0.21(2)
2	15373	11419	-0	0.22(2)
2	15034	11285	-0	0.22(2)
2	14696	11151	-0	0.22(2)
2	14357	11018	-0	0.22(2)
2	14018	10884	-0	0.22(2)
2	13679	10750	-0	0.22(2)
2	13340	10616	-0	0.22(2)
2	10936	9668	-0	0.22(2)
2	10545	9513	-0	0.22(2)
2	10155	9359	-0	0.22(2)
2	9764	9205	-0	0.22(2)
2	9373	9051	-0	0.21(2)
2	8983	8897	-0	0.21(2)
2	8592	8743	-0	0.20(2)
2	8201	8588	-0	0.19(2)
2	7811	8434	-0	0.18(2)
2	14278	20400	-0	0.26(2)
2	13956	20181	-0	0.27(2)
2	13635	19961	-0	0.28(2)
2	13313	19741	-0	0.30(2)
2	12991	19521	-0	0.31(2)
2	12669	19302	-0	0.32(2)
2	12348	19082	-0	0.33(2)
2	12026	18862	-0	0.34(2)
2	11704	18643	-0	0.35(2)
2	11382	18423	-0	0.35(2)
2	11061	18203	-0	0.36(2)
2	10739	17984	-0	0.36(2)
2	10417	17764	-0	0.37(2)
2	10095	17544	-0	0.37(2)
2	9773	17324	-0	0.37(2)
2	9452	17105	-0	0.37(2)
2	9130	16885	-0	0.37(2)
2	8808	16665	-0	0.37(2)

Muro	Cx	Cy	Cz	Sigma
2	8486	16446	-0	0.36(2)
2	8165	16226	-0	0.36(2)
2	7843	16006	-0	0.36(2)
2	7521	15787	-0	0.35(2)
2	7199	15567	-0	0.35(2)
2	6878	15347	-0	0.34(2)
2	6556	15127	-0	0.33(2)
2	6234	14908	-0	0.32(2)
2	5912	14688	-0	0.31(2)
2	5591	14468	-0	0.30(2)
2	5269	14249	-0	0.28(2)
2	4947	14029	-0	0.27(2)
2	4625	13809	-0	0.25(2)
2	4303	13589	-0	0.23(2)
2	3982	13370	-0	0.22(2)
2	14680	20228	-0	0.25(2)
2	12583	10317	-0	0.22(2)
2	12164	10152	-0	0.21(2)
2	11745	9987	-0	0.22(2)
2	7185	8584	-0	0.18(2)
2	6950	8889	-0	0.17(2)
2	6715	9193	-0	0.16(2)
2	6480	9498	-0	0.16(2)
2	6245	9802	-0	0.15(2)
2	6010	10106	-0	0.15(2)
2	5775	10411	-0	0.15(2)
2	5540	10715	-0	0.15(2)
2	5305	11019	-0	0.15(2)
2	5070	11324	-0	0.16(2)
2	4835	11628	-0	0.17(2)
2	4600	11933	-0	0.17(2)
2	4365	12237	-0	0.18(2)
2	4130	12541	-0	0.19(2)
2	3895	12846	-0	0.20(2)
2	14833	19477	-0	0.23(2)
2	14906	19117	-0	0.22(2)
2	14979	18758	-0	0.20(2)
2	15052	18399	-0	0.19(2)
2	15125	18040	-0	0.18(2)
2	15228	17533	-0	0.16(2)
2	15338	16994	-0	0.15(2)
2	15417	16602	-0	0.14(2)
2	15497	16210	-0	0.14(2)
2	15577	15818	-0	0.14(2)
2	15656	15426	-0	0.14(2)
2	15766	14887	-0	0.14(2)
2	15876	14348	-0	0.15(2)
2	15955	13956	-0	0.16(2)
2	16035	13564	-0	0.17(2)
2	16115	13173	-0	0.18(2)
2	16195	12781	-0	0.19(2)
2	16332	12104	-0	0.21(2)
2	4402	12773	-0	0.20(2)
2	4628	12470	-0	0.19(2)
2	4865	12163	-0	0.18(2)
2	5108	11849	-0	0.17(2)
2	5355	11540	-0	0.16(2)
2	5604	11227	-0	0.15(2)
2	5843	10898	-0	0.15(2)
2	6074	10564	-0	0.15(2)
2	6282	10246	-0	0.15(2)
2	6491	9961	-0	0.15(2)
2	6759	9710	-0	0.16(2)
2	7046	9406	-0	0.16(2)

Muro	Cx	Cy	Cz	Sigma
2	7315	9077	-0	0.17(2)
2	7568	8748	-0	0.18(2)
2	7957	8923	-0	0.19(2)
2	8357	9105	-0	0.19(2)
2	8759	9288	-0	0.20(2)
2	9133	9533	-0	0.20(2)
2	9603	9630	-0	0.21(2)
2	10054	9778	-0	0.21(2)
2	10478	9854	-0	0.22(2)
2	10878	9983	-0	0.22(2)
2	11245	10084	-0	0.21(2)
2	11579	10285	-0	0.21(2)
2	11905	10660	-0	0.20(2)
2	12442	10682	-0	0.21(2)
2	12874	10781	-0	0.21(2)
2	13250	10890	-0	0.22(2)
2	13598	10996	-0	0.22(2)
2	13914	11110	-0	0.22(2)
2	14213	11271	-0	0.22(2)
2	14572	11413	-0	0.21(2)
2	14929	11543	-0	0.21(2)
2	15270	11677	-0	0.21(2)
2	15601	11823	-0	0.21(2)
2	15930	12028	-0	0.21(2)
2	15951	12385	-0	0.20(2)
2	15906	12748	-0	0.19(2)
2	15834	13130	-0	0.18(2)
2	15760	13524	-0	0.17(2)
2	15681	13931	-0	0.15(2)
2	15614	14335	-0	0.15(2)
2	15588	14700	-0	0.14(2)
2	15630	14876	-0	0.14(2)
2	15528	15036	-0	0.14(2)
2	15429	15379	-0	0.13(2)
2	15333	15733	-0	0.13(2)
2	15190	16083	-0	0.13(2)
2	15081	16510	-0	0.14(2)
2	14994	16954	-0	0.15(2)
2	15043	17294	-0	0.16(2)
2	15041	17503	-0	0.16(2)
2	14980	17698	-0	0.17(2)
2	14877	17991	-0	0.18(2)
2	14799	18338	-0	0.19(2)
2	14711	18693	-0	0.21(2)
2	14624	19046	-0	0.22(2)
2	14496	19392	-0	0.24(2)
2	14408	20140	-0	0.26(2)
2	14263	19784	-0	0.26(2)
2	13815	19661	-0	0.28(2)
2	13465	19488	-0	0.29(2)
2	13147	19285	-0	0.30(2)
2	12858	19051	-0	0.31(2)
2	12604	18723	-0	0.31(2)
2	12209	18571	-0	0.33(2)
2	11876	18385	-0	0.34(2)
2	11549	18178	-0	0.34(2)
2	11223	17966	-0	0.35(2)
2	10904	17748	-0	0.35(2)
2	10584	17529	-0	0.36(2)
2	10266	17307	-0	0.36(2)
2	9944	17087	-0	0.36(2)
2	9624	16863	-0	0.36(2)
2	9303	16640	-0	0.36(2)
2	8982	16411	-0	0.36(2)

Muro	Cx	Cy	Cz	Sigma
2	8652	16187	-0	0.35(2)
2	8320	15968	-0	0.35(2)
2	7990	15759	-0	0.35(2)
2	7666	15551	-0	0.34(2)
2	7350	15333	-0	0.34(2)
2	7032	15109	-0	0.33(2)
2	6705	14890	-0	0.32(2)
2	6381	14679	-0	0.31(2)
2	6082	14469	-0	0.30(2)
2	5812	14211	-0	0.29(2)
2	5461	13962	-0	0.27(2)
2	5118	13747	-0	0.26(2)
2	4798	13528	-0	0.24(2)
2	4492	13301	-0	0.23(2)
2	4193	13072	-0	0.21(2)
2	8801	10212	-0	0.17(2)
2	8321	11172	-0	0.13(2)
2	7897	11993	-0	0.12(2)
2	7439	12598	-0	0.14(2)
2	7116	13147	-0	0.18(2)
2	6844	13643	-0	0.22(2)
2	6632	14082	-0	0.26(2)
2	6528	14419	-0	0.29(2)
2	6201	11103	-0	0.14(2)
2	6640	11325	-0	0.14(2)
2	7198	11593	-0	0.13(2)
2	7836	10072	-0	0.15(2)
2	7401	9689	-0	0.16(2)
2	8112	9525	-0	0.18(2)
2	8558	9675	-0	0.18(2)
2	7696	9303	-0	0.17(2)
2	6867	10814	-0	0.14(2)
2	6930	10408	-0	0.14(2)
2	7031	10016	-0	0.15(2)
2	7497	10822	-0	0.13(2)
2	7267	10467	-0	0.14(2)
2	7378	10185	-0	0.15(2)
2	6578	10367	-0	0.15(2)
2	6430	10712	-0	0.14(2)
2	6700	10115	-0	0.15(2)
2	5407	12102	-0	0.17(2)
2	5732	12383	-0	0.18(2)
2	6091	12671	-0	0.18(2)
2	6573	12862	-0	0.18(2)
2	6330	11766	-0	0.15(2)
2	5999	12059	-0	0.16(2)
2	5674	11790	-0	0.16(2)
2	5952	11471	-0	0.15(2)
2	6764	12227	-0	0.15(2)
2	6285	12319	-0	0.16(2)
2	5454	12724	-0	0.20(2)
2	5181	12970	-0	0.21(2)
2	4986	13242	-0	0.23(2)
2	5155	12427	-0	0.19(2)
2	4911	12719	-0	0.20(2)
2	4698	13009	-0	0.21(2)
2	6330	13390	-0	0.22(2)
2	6133	13919	-0	0.26(2)
2	6248	14269	-0	0.29(2)
2	5664	13615	-0	0.25(2)
2	5295	13447	-0	0.24(2)
2	5790	13117	-0	0.21(2)
2	5422	13178	-0	0.22(2)
2	11550	11304	-0	0.16(2)

Muro	Cx	Cy	Cz	Sigma
2	10896	12253	-0	0.11(2)
2	10302	13137	-0	0.10(2)
2	9916	13878	-0	0.12(2)
2	9580	14541	-0	0.17(2)
2	9324	15120	-0	0.23(2)
2	9059	15553	-0	0.29(2)
2	8843	15891	-0	0.33(2)
2	7607	13466	-0	0.18(2)
2	8010	13768	-0	0.19(2)
2	8451	13958	-0	0.18(2)
2	8932	14304	-0	0.19(2)
2	7823	15292	-0	0.32(2)
2	7984	15010	-0	0.29(2)
2	8128	14703	-0	0.26(2)
2	8220	14354	-0	0.22(2)
2	8671	15335	-0	0.29(2)
2	8311	15168	-0	0.29(2)
2	8844	14898	-0	0.24(2)
2	8454	14818	-0	0.25(2)
2	8535	14492	-0	0.22(2)
2	8152	15476	-0	0.32(2)
2	8497	15667	-0	0.32(2)
2	7317	13919	-0	0.23(2)
2	7059	14301	-0	0.27(2)
2	6875	14616	-0	0.30(2)
2	7694	14820	-0	0.29(2)
2	7431	14557	-0	0.28(2)
2	7768	14240	-0	0.23(2)
2	7863	14588	-0	0.26(2)
2	7518	15075	-0	0.32(2)
2	7214	14839	-0	0.31(2)
2	8628	12575	-0	0.11(2)
2	9524	12829	-0	0.10(2)
2	9254	13599	-0	0.13(2)
2	7972	13008	-0	0.14(2)
2	8636	13381	-0	0.14(2)
2	8206	13386	-0	0.15(2)
2	9090	11645	-0	0.12(2)
2	9911	11997	-0	0.11(2)
2	10141	11272	-0	0.14(2)
2	10483	10741	-0	0.17(2)
2	10827	10367	-0	0.20(2)
2	10969	11060	-0	0.17(2)
2	10668	11528	-0	0.14(2)
2	11378	10469	-0	0.20(2)
2	11156	10687	-0	0.19(2)
2	11433	10877	-0	0.18(2)
2	11572	10669	-0	0.20(2)
2	11150	10307	-0	0.21(2)
2	9504	10854	-0	0.15(2)
2	9987	10312	-0	0.19(2)
2	9464	10051	-0	0.19(2)
2	10430	10178	-0	0.20(2)
2	15452	13486	-0	0.16(2)
2	15105	13450	-0	0.15(2)
2	14706	13439	-0	0.14(2)
2	14188	13497	-0	0.12(2)
2	13679	13157	-0	0.12(2)
2	13119	12955	-0	0.12(2)
2	12504	12759	-0	0.11(2)
2	11794	12513	-0	0.11(2)
2	14385	12863	-0	0.15(2)
2	14591	12468	-0	0.17(2)
2	14710	12133	-0	0.19(2)

Muro	Cx	Cy	Cz	Sigma
2	14811	11827	-0	0.20(2)
2	15610	12709	-0	0.18(2)
2	15295	12646	-0	0.18(2)
2	14943	12573	-0	0.18(2)
2	15381	12322	-0	0.19(2)
2	15462	12057	-0	0.20(2)
2	15661	12391	-0	0.19(2)
2	15684	12159	-0	0.20(2)
2	15050	12240	-0	0.19(2)
2	15148	11950	-0	0.20(2)
2	15190	13034	-0	0.16(2)
2	15521	13090	-0	0.17(2)
2	14806	12977	-0	0.16(2)
2	13991	11570	-0	0.20(2)
2	13938	12024	-0	0.18(2)
2	13922	12553	-0	0.15(2)
2	14346	12050	-0	0.19(2)
2	14430	11715	-0	0.20(2)
2	14287	12357	-0	0.17(2)
2	13535	11260	-0	0.21(2)
2	13537	11572	-0	0.19(2)
2	13478	11952	-0	0.17(2)
2	13316	12377	-0	0.15(2)
2	13813	11313	-0	0.21(2)
2	12754	12051	-0	0.15(2)
2	12750	11503	-0	0.18(2)
2	12803	11114	-0	0.20(2)
2	12100	11808	-0	0.15(2)
2	12411	11023	-0	0.19(2)
2	12311	11383	-0	0.17(2)
2	12100	10960	-0	0.19(2)
2	11987	11216	-0	0.18(2)
2	13148	11522	-0	0.19(2)
2	13184	11196	-0	0.20(2)
2	13127	11842	-0	0.17(2)
2	10163	14840	-0	0.17(2)
2	10700	15134	-0	0.16(2)
2	11082	15468	-0	0.17(2)
2	11509	15766	-0	0.17(2)
2	12008	15855	-0	0.15(2)
2	12479	16019	-0	0.14(2)
2	12763	16329	-0	0.15(2)
2	13091	16539	-0	0.15(2)
2	13446	16744	-0	0.15(2)
2	13747	16979	-0	0.16(2)
2	14070	17143	-0	0.16(2)
2	14343	17301	-0	0.16(2)
2	14627	17398	-0	0.16(2)
2	14774	17617	-0	0.17(2)
2	14322	14287	-0	0.11(2)
2	13806	15047	-0	0.10(2)
2	13816	15755	-0	0.11(2)
2	13746	16356	-0	0.13(2)
2	11706	15222	-0	0.13(2)
2	11804	14684	-0	0.10(2)
2	12018	14101	-0	0.09(2)
2	12359	13513	-0	0.09(2)
2	10855	13567	-0	0.10(2)
2	11431	13877	-0	0.09(2)
2	11683	13232	-0	0.09(2)
2	11145	13017	-0	0.10(2)
2	10525	14222	-0	0.12(2)
2	11157	14603	-0	0.12(2)
2	11315	15098	-0	0.13(2)

Muro	Cx	Cy	Cz	Sigma
2	13250	14976	-0	0.10(2)
2	12779	14931	-0	0.10(2)
2	12305	14821	-0	0.10(2)
2	13473	13631	-0	0.11(2)
2	13386	14081	-0	0.10(2)
2	13289	14520	-0	0.09(2)
2	13793	14179	-0	0.10(2)
2	13629	14582	-0	0.10(2)
2	13818	13769	-0	0.11(2)
2	12452	14326	-0	0.09(2)
2	12872	14443	-0	0.09(2)
2	12980	13524	-0	0.10(2)
2	12959	13998	-0	0.09(2)
2	12590	13946	-0	0.09(2)
2	12966	16060	-0	0.13(2)
2	13073	15751	-0	0.12(2)
2	13107	15411	-0	0.11(2)
2	13301	16186	-0	0.13(2)
2	13407	15778	-0	0.12(2)
2	13440	15412	-0	0.11(2)
2	12172	15348	-0	0.12(2)
2	12672	15490	-0	0.12(2)
2	12831	15730	-0	0.12(2)
2	12759	15936	-0	0.13(2)
2	14835	15852	-0	0.13(2)
2	14322	15804	-0	0.12(2)
2	14263	16346	-0	0.13(2)
2	14266	16825	-0	0.14(2)
2	13920	16720	-0	0.14(2)
2	14655	16822	-0	0.14(2)
2	14709	16383	-0	0.13(2)
2	14635	17109	-0	0.15(2)
2	14415	17078	-0	0.15(2)
2	14853	17328	-0	0.16(2)
2	14889	17483	-0	0.16(2)
2	14827	17130	-0	0.15(2)
2	15172	15297	-0	0.13(2)
2	14819	15306	-0	0.12(2)
2	14370	15236	-0	0.11(2)
2	15113	15627	-0	0.13(2)
2	15021	13891	-0	0.14(2)
2	14886	14341	-0	0.13(2)
2	14887	14821	-0	0.12(2)
2	14526	14781	-0	0.11(2)
2	14683	13872	-0	0.13(2)
2	15296	14842	-0	0.13(2)
2	15364	13916	-0	0.15(2)
2	15290	14359	-0	0.14(2)
2	11402	17709	-0	0.33(2)
2	11595	17430	-0	0.30(2)
2	11798	17125	-0	0.26(2)
2	12006	16800	-0	0.22(2)
2	12225	16442	-0	0.18(2)
2	10132	16826	-0	0.34(2)
2	10337	16540	-0	0.30(2)
2	10557	16219	-0	0.26(2)
2	10792	15859	-0	0.21(2)
2	9443	15815	-0	0.29(2)
2	9713	16098	-0	0.30(2)
2	10017	16314	-0	0.30(2)
2	9501	16371	-0	0.33(2)
2	9819	16594	-0	0.33(2)
2	9192	16122	-0	0.33(2)
2	10385	15616	-0	0.22(2)

Muro	Cx	Cy	Cz	Sigma
2	10219	16002	-0	0.26(2)
2	9846	15450	-0	0.23(2)
2	9926	15850	-0	0.26(2)
2	10657	16767	-0	0.30(2)
2	10966	16996	-0	0.30(2)
2	11279	17211	-0	0.30(2)
2	10769	17270	-0	0.33(2)
2	11088	17485	-0	0.33(2)
2	10456	17043	-0	0.34(2)
2	10885	16455	-0	0.26(2)
2	11183	16693	-0	0.26(2)
2	11487	16908	-0	0.26(2)
2	11879	16263	-0	0.19(2)
2	11694	16593	-0	0.22(2)
2	11147	16120	-0	0.21(2)
2	11405	16389	-0	0.22(2)
2	11598	16140	-0	0.19(2)
2	13545	17325	-0	0.18(2)
2	13296	17772	-0	0.22(2)
2	12772	18178	-0	0.28(2)
2	12972	17453	-0	0.22(2)
2	12653	17224	-0	0.22(2)
2	12330	17008	-0	0.22(2)
2	12874	16883	-0	0.18(2)
2	12548	16666	-0	0.18(2)
2	13209	17101	-0	0.18(2)
2	12059	18123	-0	0.32(2)
2	12301	17873	-0	0.28(2)
2	12452	17539	-0	0.25(2)
2	12732	17723	-0	0.25(2)
2	12347	18291	-0	0.31(2)
2	11936	17641	-0	0.29(2)
2	11737	17913	-0	0.32(2)
2	12129	17328	-0	0.25(2)
2	13772	17834	-0	0.20(2)
2	14178	17957	-0	0.19(2)
2	14571	17891	-0	0.18(2)
2	14231	17586	-0	0.18(2)
2	13904	17472	-0	0.18(2)
2	14476	17625	-0	0.17(2)
2	13320	19045	-0	0.29(2)
2	13513	18765	-0	0.26(2)
2	13565	18438	-0	0.24(2)
2	13681	18153	-0	0.22(2)
2	13226	18331	-0	0.26(2)
2	13401	18085	-0	0.23(2)
2	13046	18860	-0	0.29(2)
2	13175	18618	-0	0.28(2)
2	12930	18503	-0	0.28(2)
2	12860	18695	-0	0.30(2)
2	14406	18619	-0	0.22(2)
2	14186	18433	-0	0.22(2)
2	13970	18263	-0	0.22(2)
2	14522	18267	-0	0.20(2)
2	14295	18219	-0	0.20(2)
2	14040	18625	-0	0.23(2)
2	13926	18815	-0	0.24(2)
2	13767	18994	-0	0.26(2)
2	13614	19231	-0	0.28(2)
2	13833	18507	-0	0.23(2)
2	13758	18696	-0	0.25(2)
2	14359	18961	-0	0.23(2)
2	14128	18914	-0	0.24(2)
2	14191	18719	-0	0.23(2)

Muro	Cx	Cy	Cz	Sigma
2	13899	19381	-0	0.27(2)
2	14014	19136	-0	0.25(2)
2	14253	19243	-0	0.24(2)
2	14138	19469	-0	0.26(2)
3	16974	8979	-0	0.18(2)
3	16390	11820	-0	0.21(2)
3	10230	4650	0	0.17(2)
3	7420	8280	0	0.18(2)
3	13001	10483	0	0.22(2)
3	11327	9822	0	0.22(2)
3	17290	7440	-0	0.17(2)
3	12369	5495	-0	0.17(2)
3	11625	5201	-0	0.17(2)
3	17215	7804	-0	0.17(2)
3	16901	9334	-0	0.19(2)
3	16828	9690	-0	0.19(2)
3	16755	10045	-0	0.20(2)
3	16682	10400	-0	0.20(2)
3	16609	10755	-0	0.21(2)
3	16536	11110	-0	0.21(2)
3	16463	11465	-0	0.21(2)
3	9996	4953	-0	0.17(2)
3	9762	5255	-0	0.16(2)
3	9527	5558	-0	0.16(2)
3	9293	5860	-0	0.16(2)
3	9059	6162	-0	0.17(2)
3	8825	6465	-0	0.17(2)
3	8591	6767	-0	0.17(2)
3	8357	7070	-0	0.17(2)
3	8122	7372	-0	0.18(2)
3	7888	7675	-0	0.18(2)
3	7654	7977	-0	0.18(2)
3	16051	11686	-0	0.21(2)
3	15712	11553	-0	0.21(2)
3	15373	11419	-0	0.22(2)
3	15034	11285	-0	0.22(2)
3	14696	11151	-0	0.22(2)
3	14357	11018	-0	0.22(2)
3	14018	10884	-0	0.22(2)
3	13679	10750	-0	0.22(2)
3	13340	10616	-0	0.22(2)
3	10936	9668	-0	0.22(2)
3	10545	9513	-0	0.22(2)
3	10155	9359	-0	0.22(2)
3	9764	9205	-0	0.22(2)
3	9373	9051	-0	0.21(2)
3	8983	8897	-0	0.21(2)
3	8592	8743	-0	0.20(2)
3	8201	8588	-0	0.19(2)
3	7811	8434	-0	0.18(2)
3	16939	7301	-0	0.17(2)
3	16587	7162	-0	0.17(2)
3	16236	7023	-0	0.17(2)
3	15884	6884	-0	0.17(2)
3	15533	6745	-0	0.17(2)
3	15181	6606	-0	0.18(2)
3	14830	6467	-0	0.18(2)
3	14478	6329	-0	0.18(2)
3	14127	6190	-0	0.18(2)
3	13775	6051	-0	0.18(2)
3	13424	5912	-0	0.18(2)
3	13072	5773	-0	0.18(2)
3	12721	5634	-0	0.17(2)
3	11276	5063	-0	0.17(2)

Muro	Cx	Cy	Cz	Sigma
3	10928	4926	-0	0.17(2)
3	10579	4788	-0	0.17(2)
3	11745	9987	-0	0.22(2)
3	12164	10152	-0	0.21(2)
3	12583	10317	-0	0.22(2)
3	11997	5348	-0	0.17(2)
3	17253	7622	-0	0.17(2)
3	17094	8392	-0	0.18(2)
3	13178	10097	-0	0.21(2)
3	12838	9821	-0	0.21(2)
3	12374	9595	-0	0.21(2)
3	11870	9437	-0	0.21(2)
3	11418	9394	-0	0.22(2)
3	11004	9289	-0	0.22(2)
3	10624	9219	-0	0.22(2)
3	10264	9085	-0	0.22(2)
3	9882	8925	-0	0.22(2)
3	9493	8746	-0	0.21(2)
3	9105	8559	-0	0.20(2)
3	8717	8350	-0	0.20(2)
3	7916	8151	-0	0.18(2)
3	8292	8041	-0	0.19(2)
3	8422	7574	-0	0.18(2)
3	8597	7251	-0	0.17(2)
3	8837	6987	-0	0.17(2)
3	9087	6666	-0	0.17(2)
3	9339	6350	-0	0.16(2)
3	9595	6036	-0	0.16(2)
3	9855	5719	-0	0.16(2)
3	10107	5404	-0	0.16(2)
3	10346	5091	-0	0.16(2)
3	10705	5239	-0	0.17(2)
3	11087	5393	-0	0.17(2)
3	11495	5542	-0	0.17(2)
3	11911	5662	-0	0.17(2)
3	12272	5739	-0	0.17(2)
3	12598	5864	-0	0.17(2)
3	12938	6011	-0	0.17(2)
3	13291	6169	-0	0.17(2)
3	13663	6323	-0	0.17(2)
3	14041	6474	-0	0.17(2)
3	14419	6614	-0	0.17(2)
3	14778	6748	-0	0.17(2)
3	15124	6924	-0	0.17(2)
3	15477	6997	-0	0.17(2)
3	15816	7110	-0	0.17(2)
3	16142	7240	-0	0.17(2)
3	16455	7412	-0	0.17(2)
3	16850	7544	-0	0.17(2)
3	16740	7847	-0	0.17(2)
3	16655	8344	-0	0.17(2)
3	16598	8871	-0	0.18(2)
3	16600	9264	-0	0.19(2)
3	16545	9617	-0	0.19(2)
3	16472	9979	-0	0.20(2)
3	16388	10339	-0	0.20(2)
3	16301	10690	-0	0.21(2)
3	16216	11030	-0	0.21(2)
3	16132	11363	-0	0.21(2)
3	15799	11257	-0	0.21(2)
3	15461	11146	-0	0.22(2)
3	15121	11029	-0	0.22(2)
3	14783	10898	-0	0.22(2)
3	14444	10765	-0	0.22(2)

Muro	Cx	Cy	Cz	Sigma
3	14109	10631	-0	0.22(2)
3	13802	10489	-0	0.22(2)
3	13521	10287	-0	0.22(2)
3	12597	8953	-0	0.18(2)
3	12847	8220	-0	0.16(2)
3	13088	7545	-0	0.16(2)
3	13342	7039	-0	0.16(2)
3	13523	6650	-0	0.17(2)
3	11904	8745	-0	0.19(2)
3	12199	7973	-0	0.16(2)
3	12441	7216	-0	0.16(2)
3	12872	6803	-0	0.16(2)
3	13116	6470	-0	0.17(2)
3	11667	7032	-0	0.16(2)
3	11203	6466	-0	0.16(2)
3	10642	6150	-0	0.16(2)
3	10220	5915	-0	0.16(2)
3	11363	5944	-0	0.16(2)
3	10890	5762	-0	0.16(2)
3	10481	5580	-0	0.16(2)
3	12556	6529	-0	0.16(2)
3	12220	6309	-0	0.16(2)
3	11877	6044	-0	0.16(2)
3	11980	6617	-0	0.16(2)
3	11687	6376	-0	0.16(2)
3	12325	6787	-0	0.16(2)
3	12766	6273	-0	0.17(2)
3	12447	6098	-0	0.17(2)
3	12199	5960	-0	0.17(2)
3	10026	8617	-0	0.21(2)
3	10205	8267	-0	0.19(2)
3	10391	7858	-0	0.18(2)
3	10555	7406	-0	0.17(2)
3	10688	6905	-0	0.16(2)
3	11343	8356	-0	0.18(2)
3	10846	8083	-0	0.18(2)
3	11560	7739	-0	0.16(2)
3	11023	7599	-0	0.17(2)
3	11126	7179	-0	0.16(2)
3	11024	8829	-0	0.20(2)
3	11449	8989	-0	0.20(2)
3	10618	8499	-0	0.20(2)
3	10399	8793	-0	0.21(2)
3	10682	8947	-0	0.21(2)
3	9388	6898	-0	0.17(2)
3	9755	7111	-0	0.17(2)
3	10130	7293	-0	0.17(2)
3	9936	6251	-0	0.16(2)
3	9660	6570	-0	0.16(2)
3	10311	6521	-0	0.16(2)
3	9996	6796	-0	0.16(2)
3	10271	6998	-0	0.16(2)
3	9635	8418	-0	0.20(2)
3	9794	8058	-0	0.19(2)
3	9963	7673	-0	0.18(2)
3	9112	7295	-0	0.17(2)
3	9554	7489	-0	0.17(2)
3	9253	8228	-0	0.20(2)
3	9402	7873	-0	0.19(2)
3	8709	7648	-0	0.18(2)
3	9028	7718	-0	0.18(2)
3	8904	8052	-0	0.19(2)
3	8635	7914	-0	0.19(2)
3	8806	7398	-0	0.18(2)

Muro	Cx	Cy	Cz	Sigma
3	13221	9268	-0	0.19(2)
3	13446	8477	-0	0.16(2)
3	13662	7801	-0	0.16(2)
3	13836	7248	-0	0.16(2)
3	13944	6825	-0	0.17(2)
3	16160	8283	-0	0.17(2)
3	15599	8214	-0	0.17(2)
3	14948	8217	-0	0.16(2)
3	14260	8008	-0	0.16(2)
3	15047	7395	-0	0.17(2)
3	14380	7395	-0	0.16(2)
3	14370	6960	-0	0.17(2)
3	14732	7034	-0	0.17(2)
3	16212	7721	-0	0.17(2)
3	15651	7666	-0	0.17(2)
3	15735	7356	-0	0.17(2)
3	16029	7439	-0	0.17(2)
3	15420	7249	-0	0.17(2)
3	14612	8866	-0	0.17(2)
3	14406	9478	-0	0.18(2)
3	14258	9983	-0	0.20(2)
3	14205	10345	-0	0.21(2)
3	13859	9337	-0	0.18(2)
3	14044	8672	-0	0.16(2)
3	13786	9931	-0	0.21(2)
3	13395	9765	-0	0.20(2)
3	13931	10255	-0	0.21(2)
3	16163	9897	-0	0.19(2)
3	15818	9792	-0	0.19(2)
3	15414	9709	-0	0.19(2)
3	14933	9696	-0	0.19(2)
3	16134	8899	-0	0.18(2)
3	15932	9363	-0	0.18(2)
3	15509	9232	-0	0.18(2)
3	15614	8757	-0	0.17(2)
3	15067	9119	-0	0.17(2)
3	15210	8698	-0	0.17(2)
3	16246	9527	-0	0.19(2)
3	16327	9230	-0	0.18(2)
3	15218	10744	-0	0.21(2)
3	15315	10427	-0	0.21(2)
3	15395	10092	-0	0.20(2)
3	14550	10469	-0	0.21(2)
3	14885	10608	-0	0.21(2)
3	14683	10117	-0	0.20(2)
3	14997	10299	-0	0.20(2)
3	15108	10029	-0	0.20(2)
3	16071	10261	-0	0.20(2)
3	15735	10170	-0	0.20(2)
3	15556	10844	-0	0.21(2)
3	15649	10516	-0	0.21(2)
3	15978	10604	-0	0.21(2)
3	15887	10934	-0	0.21(2)
4	17970	4100	0	0.16(2)
4	17609	5872	0	0.16(2)
4	17290	7440	-0	0.17(2)
4	12369	5495	-0	0.17(2)
4	11625	5201	-0	0.17(2)
4	10230	4650	0	0.17(2)
4	12360	1890	-0	0.17(2)
4	17370	7048	0	0.17(2)
4	17880	4543	-0	0.16(2)
4	17790	4986	-0	0.16(2)
4	17699	5429	-0	0.16(2)

Muro	Cx	Cy	Cz	Sigma
4	16939	7301	-0	0.17(2)
4	16587	7162	-0	0.17(2)
4	16236	7023	-0	0.17(2)
4	15884	6884	-0	0.17(2)
4	15533	6745	-0	0.17(2)
4	15181	6606	-0	0.18(2)
4	14830	6467	-0	0.18(2)
4	14478	6329	-0	0.18(2)
4	14127	6190	-0	0.18(2)
4	13775	6051	-0	0.18(2)
4	13424	5912	-0	0.18(2)
4	13072	5773	-0	0.18(2)
4	12721	5634	-0	0.17(2)
4	11276	5063	-0	0.17(2)
4	10928	4926	-0	0.17(2)
4	10579	4788	-0	0.17(2)
4	17619	3961	-0	0.16(2)
4	17269	3823	-0	0.16(2)
4	16918	3685	-0	0.16(2)
4	16568	3547	-0	0.16(2)
4	16217	3409	-0	0.16(2)
4	15866	3271	-0	0.16(2)
4	15516	3133	-0	0.16(2)
4	15165	2995	-0	0.16(2)
4	14814	2857	-0	0.16(2)
4	14464	2719	-0	0.16(2)
4	14113	2581	-0	0.16(2)
4	13762	2443	-0	0.16(2)
4	13412	2304	-0	0.16(2)
4	13061	2166	-0	0.16(2)
4	12710	2028	-0	0.16(2)
4	11997	5348	-0	0.17(2)
4	12094	2235	-0	0.16(2)
4	11827	2580	-0	0.16(2)
4	11561	2925	-0	0.16(2)
4	11295	3270	-0	0.16(2)
4	11029	3615	-0	0.16(2)
4	10762	3960	-0	0.16(2)
4	10496	4305	-0	0.17(2)
4	17490	6460	-0	0.16(2)
4	17330	7244	-0	0.17(2)
4	16620	6905	-0	0.17(2)
4	16267	6766	-0	0.17(2)
4	15921	6593	-0	0.17(2)
4	15589	6512	-0	0.17(2)
4	15289	6386	-0	0.17(2)
4	15010	6206	-0	0.17(2)
4	14647	6020	-0	0.17(2)
4	14294	5797	-0	0.17(2)
4	13884	5714	-0	0.17(2)
4	13495	5599	-0	0.17(2)
4	13151	5523	-0	0.17(2)
4	12843	5356	-0	0.17(2)
4	12535	5031	-0	0.17(2)
4	12100	5010	-0	0.17(2)
4	11762	4883	-0	0.17(2)
4	11458	4661	-0	0.17(2)
4	10702	4498	-0	0.17(2)
4	11040	4401	-0	0.17(2)
4	11362	3956	-0	0.16(2)
4	11634	3517	-0	0.16(2)
4	11896	3096	-0	0.16(2)
4	12144	2736	-0	0.16(2)
4	12442	2420	-0	0.16(2)

Muro	Cx	Cy	Cz	Sigma
4	12820	2717	-0	0.16(2)
4	13292	2656	-0	0.16(2)
4	13648	2741	-0	0.16(2)
4	13976	2921	-0	0.16(2)
4	14394	3079	-0	0.16(2)
4	14756	3146	-0	0.16(2)
4	15094	3262	-0	0.16(2)
4	15441	3397	-0	0.16(2)
4	15790	3536	-0	0.16(2)
4	16137	3682	-0	0.16(2)
4	16487	3826	-0	0.16(2)
4	16812	3976	-0	0.16(2)
4	17119	4183	-0	0.16(2)
4	17499	4373	-0	0.16(2)
4	17360	4803	-0	0.16(2)
4	17246	5288	-0	0.16(2)
4	17148	5790	-0	0.16(2)
4	17062	6307	-0	0.16(2)
4	17012	6758	-0	0.17(2)
4	16975	7052	-0	0.17(2)
4	12122	4716	-0	0.17(2)
4	12173	4386	-0	0.16(2)
4	12404	3986	-0	0.16(2)
4	12705	3366	-0	0.15(2)
4	12250	3275	-0	0.16(2)
4	12404	2909	-0	0.16(2)
4	12013	3769	-0	0.16(2)
4	11777	4285	-0	0.16(2)
4	11887	4628	-0	0.17(2)
4	12779	4445	-0	0.16(2)
4	13083	3742	-0	0.15(2)
4	13280	3271	-0	0.15(2)
4	13291	2947	-0	0.16(2)
4	12360	4766	-0	0.17(2)
4	12437	4533	-0	0.16(2)
4	13036	2938	-0	0.16(2)
4	13007	3192	-0	0.15(2)
4	15013	3548	-0	0.16(2)
4	14885	3876	-0	0.15(2)
4	14871	4451	-0	0.15(2)
4	14534	5259	-0	0.16(2)
4	14384	3567	-0	0.15(2)
4	13756	3332	-0	0.15(2)
4	13565	3007	-0	0.16(2)
4	14717	3420	-0	0.16(2)
4	14180	4188	-0	0.15(2)
4	13590	3950	-0	0.15(2)
4	13552	5216	-0	0.17(2)
4	13902	4800	-0	0.16(2)
4	13990	5396	-0	0.17(2)
4	13363	4538	-0	0.16(2)
4	13011	5167	-0	0.17(2)
4	13207	4939	-0	0.17(2)
4	12928	4806	-0	0.16(2)
4	12825	5002	-0	0.17(2)
4	13238	5302	-0	0.17(2)
4	16636	5669	-0	0.16(2)
4	16040	5548	-0	0.16(2)
4	15358	5360	-0	0.16(2)
4	15961	6191	-0	0.17(2)
4	15308	5944	-0	0.17(2)
4	14830	5741	-0	0.17(2)
4	15649	6308	-0	0.17(2)
4	15415	6212	-0	0.17(2)

Muro	Cx	Cy	Cz	Sigma
4	16573	6196	-0	0.16(2)
4	16624	6598	-0	0.17(2)
4	16284	6519	-0	0.17(2)
4	16185	4958	-0	0.15(2)
4	16348	4483	-0	0.15(2)
4	16397	4123	-0	0.16(2)
4	16858	4560	-0	0.16(2)
4	16731	5119	-0	0.15(2)
4	16689	4220	-0	0.16(2)
4	15266	3976	-0	0.15(2)
4	15586	4110	-0	0.15(2)
4	15886	4313	-0	0.15(2)
4	15552	4686	-0	0.15(2)
4	15199	4258	-0	0.15(2)
4	15446	4351	-0	0.15(2)
4	15695	3822	-0	0.16(2)
4	15354	3686	-0	0.16(2)
4	16029	3985	-0	0.15(2)
5	6020	7280	0	0.17(2)
5	8830	3650	0	0.18(2)
5	11560	-10	-0	0.18(2)
5	12360	1890	-0	0.17(2)
5	10230	4650	0	0.17(2)
5	7420	8280	0	0.18(2)
5	3660	13150	-0	0.21(2)
5	2260	12150	-0	0.17(2)
5	6722	6372	-0	0.18(2)
5	7425	5465	-0	0.18(2)
5	8127	4558	-0	0.18(2)
5	9512	2735	-0	0.18(2)
5	10195	1820	-0	0.18(2)
5	10877	905	-0	0.18(2)
5	12094	2235	-0	0.16(2)
5	11827	2580	-0	0.16(2)
5	11561	2925	-0	0.16(2)
5	11295	3270	-0	0.16(2)
5	11029	3615	-0	0.16(2)
5	10762	3960	-0	0.16(2)
5	10496	4305	-0	0.17(2)
5	9996	4953	-0	0.17(2)
5	9762	5255	-0	0.16(2)
5	9527	5558	-0	0.16(2)
5	9293	5860	-0	0.16(2)
5	9059	6162	-0	0.17(2)
5	8825	6465	-0	0.17(2)
5	8591	6767	-0	0.17(2)
5	8357	7070	-0	0.17(2)
5	8122	7372	-0	0.18(2)
5	7888	7675	-0	0.18(2)
5	7654	7977	-0	0.18(2)
5	7185	8584	-0	0.18(2)
5	6950	8889	-0	0.17(2)
5	6715	9193	-0	0.16(2)
5	6480	9498	-0	0.16(2)
5	6245	9802	-0	0.15(2)
5	6010	10106	-0	0.15(2)
5	5775	10411	-0	0.15(2)
5	5540	10715	-0	0.15(2)
5	5305	11019	-0	0.15(2)
5	5070	11324	-0	0.16(2)
5	4835	11628	-0	0.17(2)
5	4600	11933	-0	0.17(2)
5	4365	12237	-0	0.18(2)
5	4130	12541	-0	0.19(2)

Muro	Cx	Cy	Cz	Sigma
5	3895	12846	-0	0.20(2)
5	12226	1574	-0	0.17(2)
5	12093	1257	-0	0.17(2)
5	11960	940	-0	0.18(2)
5	11826	624	-0	0.18(2)
5	11693	307	-0	0.18(2)
5	3200	10933	-0	0.17(2)
5	4140	9715	-0	0.17(2)
5	5080	8498	-0	0.17(2)
5	3310	12900	-0	0.19(2)
5	2960	12650	-0	0.18(2)
5	2610	12400	-0	0.17(2)
5	4609	10211	-0	0.16(2)
5	5720	8996	-0	0.16(2)
5	6519	7689	-0	0.17(2)
5	7204	6694	-0	0.17(2)
5	7874	5796	-0	0.17(2)
5	8541	4902	-0	0.17(2)
5	9249	3986	-0	0.17(2)
5	10049	2952	-0	0.17(2)
5	11276	978	-0	0.18(2)
5	11257	1723	-0	0.17(2)
5	11741	1319	-0	0.17(2)
5	11896	1402	-0	0.17(2)
5	11846	1637	-0	0.17(2)
5	11990	1867	-0	0.17(2)
5	11736	2068	-0	0.17(2)
5	11560	2428	-0	0.16(2)
5	11319	2778	-0	0.16(2)
5	11029	3155	-0	0.16(2)
5	10750	3549	-0	0.16(2)
5	10628	3850	-0	0.16(2)
5	10366	4056	-0	0.17(2)
5	10034	4487	-0	0.17(2)
5	9897	4796	-0	0.17(2)
5	9650	4968	-0	0.17(2)
5	9306	5385	-0	0.17(2)
5	9096	5734	-0	0.17(2)
5	8866	6040	-0	0.17(2)
5	8608	6322	-0	0.17(2)
5	8406	6642	-0	0.17(2)
5	8175	6937	-0	0.17(2)
5	7903	7225	-0	0.17(2)
5	7613	7653	-0	0.18(2)
5	7516	7919	-0	0.18(2)
5	7292	8123	-0	0.18(2)
5	6973	8558	-0	0.17(2)
5	6843	8807	-0	0.17(2)
5	6636	8995	-0	0.17(2)
5	6209	9313	-0	0.16(2)
5	6010	9640	-0	0.16(2)
5	5793	9950	-0	0.15(2)
5	5547	10268	-0	0.15(2)
5	5291	10597	-0	0.15(2)
5	5072	10945	-0	0.16(2)
5	4912	11232	-0	0.16(2)
5	4597	11418	-0	0.16(2)
5	4442	11763	-0	0.17(2)
5	4153	11922	-0	0.18(2)
5	3842	12150	-0	0.18(2)
5	3584	12541	-0	0.19(2)
5	3359	12260	-0	0.18(2)
5	3607	11580	-0	0.17(2)
5	8946	5304	-0	0.17(2)

Muro	Cx	Cy	Cz	Sigma
5	9636	4470	-0	0.17(2)
5	10310	3613	-0	0.17(2)
5	11308	2255	-0	0.17(2)
5	11086	2611	-0	0.17(2)
5	10748	3041	-0	0.17(2)
5	10970	2373	-0	0.17(2)
5	10571	2785	-0	0.17(2)
5	8352	6138	-0	0.17(2)
5	8917	5660	-0	0.17(2)
5	8712	5946	-0	0.17(2)
5	7173	7787	-0	0.18(2)
5	6723	8537	-0	0.17(2)
5	7736	6930	-0	0.17(2)
5	8269	6528	-0	0.17(2)
5	8060	6798	-0	0.17(2)
5	5000	10463	-0	0.16(2)
5	5775	9474	-0	0.16(2)
5	5592	9780	-0	0.16(2)
5	5318	10119	-0	0.16(2)
5	5481	9580	-0	0.16(2)
5	5167	9925	-0	0.16(2)
5	4784	10928	-0	0.16(2)
5	4078	11505	-0	0.17(2)
5	4490	10881	-0	0.16(2)
6	12810	490	-0	0.18(2)
6	18470	2600	0	0.18(2)
6	17970	4100	0	0.16(2)
6	12360	1890	-0	0.17(2)
6	11560	-10	-0	0.18(2)
6	14225	1018	-0	0.18(2)
6	15640	1545	-0	0.18(2)
6	17055	2072	-0	0.18(2)
6	17619	3961	-0	0.16(2)
6	17269	3823	-0	0.16(2)
6	16918	3685	-0	0.16(2)
6	16568	3547	-0	0.16(2)
6	16217	3409	-0	0.16(2)
6	15866	3271	-0	0.16(2)
6	15516	3133	-0	0.16(2)
6	15165	2995	-0	0.16(2)
6	14814	2857	-0	0.16(2)
6	14464	2719	-0	0.16(2)
6	14113	2581	-0	0.16(2)
6	13762	2443	-0	0.16(2)
6	13412	2304	-0	0.16(2)
6	13061	2166	-0	0.16(2)
6	12710	2028	-0	0.16(2)
6	11693	307	-0	0.18(2)
6	11826	624	-0	0.18(2)
6	11960	940	-0	0.18(2)
6	12093	1257	-0	0.17(2)
6	12226	1574	-0	0.17(2)
6	11872	115	-0	0.18(2)
6	12185	240	-0	0.18(2)
6	12497	365	-0	0.18(2)
6	18345	2975	-0	0.18(2)
6	18220	3350	-0	0.17(2)
6	18095	3725	-0	0.17(2)
6	12506	741	-0	0.18(2)
6	13005	1130	-0	0.18(2)
6	14075	1689	-0	0.17(2)
6	15455	2040	-0	0.18(2)
6	17072	2382	-0	0.18(2)
6	17767	3179	-0	0.17(2)

Muro	Cx	Cy	Cz	Sigma
6	17717	3596	-0	0.17(2)
6	17381	3508	-0	0.17(2)
6	17064	3361	-0	0.17(2)
6	16697	3229	-0	0.17(2)
6	16319	3100	-0	0.17(2)
6	15949	2988	-0	0.16(2)
6	15605	2904	-0	0.16(2)
6	15314	2741	-0	0.16(2)
6	15048	2526	-0	0.17(2)
6	14634	2442	-0	0.17(2)
6	14246	2303	-0	0.17(2)
6	13885	2111	-0	0.17(2)
6	13473	2010	-0	0.17(2)
6	13082	1876	-0	0.17(2)
6	12745	1776	-0	0.17(2)
6	12507	1716	-0	0.17(2)
6	12434	1491	-0	0.17(2)
6	12327	1202	-0	0.17(2)
6	12207	907	-0	0.18(2)
6	11894	327	-0	0.18(2)
6	12124	568	-0	0.18(2)
6	12612	1187	-0	0.17(2)
6	12441	945	-0	0.18(2)
6	15487	2493	-0	0.17(2)
6	17259	3007	-0	0.17(2)
6	17469	3231	-0	0.17(2)
6	15705	2685	-0	0.17(2)
6	15946	2652	-0	0.17(2)
6	16416	2831	-0	0.17(2)
6	16837	2908	-0	0.17(2)
6	16883	2626	-0	0.17(2)
6	16515	2692	-0	0.17(2)
6	14817	2185	-0	0.17(2)
6	14379	2059	-0	0.17(2)
6	12713	1502	-0	0.17(2)
6	13082	1565	-0	0.17(2)
6	13543	1755	-0	0.17(2)
Massimo assoluto				
1	9773	17324	-0	0.37(2)
Minimo assoluto				
1	5530	19353	-0	0.08(4)

Risultati Analisi Dinamica - Spostamenti massimi - Nodi

Scenario di calcolo: **Set_NT_SLV_SLD_A2_STR/GEO_2018**

la tripletta (Cb [-SubC-Cbm]) indica la Combinazione - SottoCombinazione sismica - Posizione Masse, nel caso non sismico mancano SubC-Cbm

Nodo	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
	mm	mm	mm	mrاد	mrاد	mrاد
1	-4.24(8-II-3)	3.49(9-I-4)	-1.92(2)	-0.46(9-I-4)	0.69(9-II-2)	0.19(9-I-2)
1	1.61(8-I-1)	4.36(9-I-1)	-1.37(2)	-0.20(9-I-1)	0.15(2)	0.41(8-II-1)
2	1.52(8-I-1)	-3.55(9-II-2)	-0.94(2)	0.49(8-I-3)	-1.49(8-II-2)	-2.01(8-II-2)
2	4.43(8-I-2)	3.69(9-I-2)	-1.10(2)	1.42(8-II-2)	7.01(8-I-2)	-2.50(8-I-2)
2	1.64(8-I-1)	-4.55(9-II-1)	-1.34(2)	-0.09(8-I-2)	-0.13(8-II-1)	-0.35(8-I-1)
2	-4.43(8-II-3)	3.53(9-I-4)	-3.60(2)	-1.23(9-I-1)	1.05(9-II-1)	0.19(9-I-2)
3	-3.47(8-II-2)	-3.40(9-II-2)	-0.89(2)	-0.82(8-I-2)	-3.19(8-II-2)	-0.53(8-II-1)
3	1.78(8-I-3)	-3.61(9-II-2)	-0.98(2)	-0.51(9-I-3)	-1.90(8-II-2)	-2.11(8-I-2)
3	1.67(8-I-4)	-4.72(9-II-1)	-1.33(2)	-0.17(8-II-2)	-0.18(8-II-1)	-0.37(8-I-2)
3	-4.63(8-II-3)	3.58(9-I-4)	-3.95(2)	1.50(9-II-2)	-1.08(9-I-1)	0.19(9-I-2)
4	-1.44(9-I-1)	-3.98(9-II-1)	-0.93(2)	2.45(9-II-1)	0.89(9-II-1)	-1.28(9-II-1)

Nodo	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
4	-4.83(8-II-3)	3.64(9-I-4)	-2.14(2)	1.41(9-II-2)	-1.11(9-I-2)	0.19(9-I-2)
5	0.00(1)	0.00(1)	-1.17(8-II-3)	-0.07(2)	-0.30(8-II-3)	0.00(1)
5	1.58(9-II-1)	-4.22(9-II-1)	-0.94(2)	2.44(9-II-1)	0.95(9-II-1)	-0.27(8-I-3)
5	-5.03(8-II-3)	3.72(9-I-1)	-3.48(2)	-1.75(9-I-2)	1.09(9-II-2)	0.19(9-I-2)
6	0.00(1)	0.00(1)	-1.03(2)	-0.12(2)	0.09(2)	0.00(1)
6	4.67(8-I-3)	3.87(9-I-2)	-1.47(2)	0.74(9-II-3)	-0.69(8-II-3)	-0.27(9-II-2)
6	1.73(9-II-2)	-4.34(9-II-1)	-0.91(2)	2.18(9-II-1)	1.02(9-II-1)	1.31(9-II-1)
6	-5.23(8-II-3)	3.86(9-I-1)	-4.05(2)	1.27(9-II-2)	-0.96(9-I-2)	0.19(9-I-2)
7	0.00(1)	0.00(1)	-1.43(2)	-0.26(2)	-0.34(8-II-3)	0.00(1)
7	4.69(8-I-3)	3.61(9-I-2)	-1.40(9-I-2)	-0.84(9-I-2)	-0.46(8-II-3)	0.16(8-II-3)
7	-5.43(8-II-3)	4.12(9-I-2)	-1.88(2)	0.59(9-II-2)	-0.60(8-II-3)	0.19(9-I-2)
8	0.00(1)	0.00(1)	-1.06(2)	0.10(9-II-2)	0.12(8-I-2)	0.00(1)
8	-3.18(8-II-3)	3.62(9-I-4)	-2.72(2)	-2.79(2)	-1.79(2)	0.19(9-I-2)
9	0.00(1)	0.00(1)	-0.92(2)	-0.08(8-I-1)	0.08(8-I-1)	0.00(1)
9	-3.36(8-II-3)	3.69(9-I-4)	-3.05(2)	-2.11(2)	-1.44(2)	0.19(9-I-2)
10	0.00(1)	0.00(1)	-0.86(2)	-0.05(8-I-1)	0.06(8-I-1)	0.00(1)
10	1.89(8-I-1)	-2.97(9-II-2)	-1.87(2)	-1.45(9-I-2)	0.83(9-II-1)	-0.62(2)
10	-3.55(8-II-3)	3.81(9-I-1)	-3.21(2)	-1.64(2)	-1.15(2)	0.19(9-I-2)
11	0.00(1)	0.00(1)	-0.85(2)	-0.04(8-I-2)	0.06(8-I-1)	0.00(1)
11	2.11(8-I-4)	-3.31(9-II-2)	-2.00(2)	1.65(9-II-2)	-0.97(2)	-0.22(8-I-3)
11	-3.73(8-II-3)	4.02(9-I-2)	-3.38(2)	0.27(2)	0.18(8-I-3)	0.19(9-I-2)
12	0.00(1)	0.00(1)	-0.83(2)	0.07(9-II-1)	-0.03(8-II-1)	0.00(1)
12	-3.92(8-II-3)	4.29(9-I-2)	-3.16(2)	-0.57(2)	-0.65(2)	0.19(9-I-2)
13	0.00(1)	0.00(1)	-0.83(2)	0.06(9-I-1)	-0.01(8-II-1)	0.00(1)
13	-4.12(8-II-3)	4.57(9-I-2)	-2.61(2)	-3.57(2)	-2.77(2)	0.19(9-I-2)
14	0.00(1)	0.00(1)	-0.89(2)	0.03(9-II-3)	0.06(2)	0.00(1)
14	3.27(8-I-3)	3.58(9-I-2)	-0.99(2)	0.57(9-II-3)	1.51(8-I-3)	0.82(2)
15	0.00(1)	0.00(1)	-1.40(2)	-0.31(9-I-3)	-0.16(9-II-3)	0.00(1)
15	3.44(8-I-3)	3.81(9-I-2)	-1.21(2)	-0.27(9-I-3)	1.42(8-I-3)	-0.10(9-I-4)
15	-2.74(8-II-1)	3.84(9-I-1)	-1.73(2)	-0.78(2)	-0.23(2)	0.19(9-I-2)
16	0.00(1)	0.00(1)	-1.28(2)	-0.31(9-I-3)	-0.15(9-II-3)	0.00(1)
16	-2.76(8-II-1)	4.14(9-I-2)	-2.20(2)	-1.56(2)	-0.21(2)	0.19(9-I-2)
17	0.00(1)	0.00(1)	-1.12(9-I-3)	-0.30(9-I-2)	-0.12(9-II-3)	0.00(1)
17	-2.78(8-II-1)	4.46(9-I-2)	-2.84(2)	-1.38(2)	-1.02(2)	0.19(9-I-2)
18	0.00(1)	0.00(1)	-1.09(9-I-3)	-0.32(9-I-2)	0.12(8-I-3)	0.00(1)
18	3.39(8-I-3)	3.81(9-I-2)	-1.44(2)	0.40(9-II-3)	1.63(8-I-3)	-0.70(2)
18	-2.85(8-II-4)	4.78(9-I-2)	-1.61(2)	-8.39(2)	-3.59(2)	0.19(9-I-2)
19	0.00(1)	0.00(1)	-1.10(2)	0.04(2)	-0.02(2)	0.00(1)
19	3.09(8-I-3)	3.71(9-I-2)	-1.43(2)	-0.56(9-I-2)	1.25(8-I-3)	-0.99(2)
20	0.00(1)	0.00(1)	-1.09(2)	0.03(9-II-2)	0.04(2)	0.00(1)
21	0.00(1)	0.00(1)	-1.25(2)	0.06(9-II-3)	-0.16(8-II-3)	0.00(1)
22	0.00(1)	0.00(1)	-0.87(2)	0.09(9-II-3)	0.15(8-I-3)	0.00(1)
22	-2.71(8-II-3)	3.81(9-I-2)	-1.31(2)	0.70(9-II-2)	-1.17(8-II-3)	-0.48(9-II-2)
23	0.00(1)	0.00(1)	-0.98(2)	0.10(2)	0.16(8-I-3)	0.00(1)
23	-2.73(9-I-2)	-4.30(9-II-2)	-1.03(2)	-0.29(8-I-3)	1.00(8-I-3)	-0.31(8-I-3)
24	0.00(1)	0.00(1)	-1.10(2)	0.12(2)	0.15(8-I-3)	0.00(1)
25	0.00(1)	0.00(1)	-1.22(2)	0.10(2)	-0.14(8-II-3)	0.00(1)
25	-4.49(8-II-3)	4.73(9-I-2)	-1.73(2)	0.99(2)	-11.33(2)	0.19(9-I-2)
26	0.00(1)	0.00(1)	-1.20(2)	-0.10(9-I-3)	-0.15(8-II-3)	0.00(1)
26	-2.77(9-I-2)	-4.31(9-II-2)	-1.02(2)	-0.22(8-I-3)	1.00(8-I-3)	-0.32(8-I-2)
26	-3.63(8-II-3)	4.91(9-I-2)	-1.06(2)	-0.23(8-I-3)	1.91(2)	0.19(9-I-2)
27	0.00(1)	0.00(1)	-0.83(2)	-0.14(8-I-3)	-0.08(8-II-3)	0.00(1)
27	-2.91(9-I-3)	-4.25(9-II-2)	-1.10(2)	-0.17(9-I-3)	0.99(8-I-3)	0.39(8-II-2)
28	0.00(1)	0.00(1)	-0.79(2)	-0.13(8-I-3)	-0.07(8-II-3)	0.00(1)
29	0.00(1)	0.00(1)	-0.71(2)	0.08(9-I-2)	0.12(8-I-2)	0.00(1)
30	0.00(1)	0.00(1)	-0.73(2)	0.07(9-I-2)	0.13(8-I-2)	0.00(1)
30	-2.95(9-I-3)	-4.23(9-II-2)	-1.12(2)	0.16(8-II-2)	0.95(8-I-3)	0.38(8-II-2)
31	0.00(1)	0.00(1)	-1.01(2)	0.10(2)	0.13(8-I-2)	0.00(1)
31	-2.23(9-I-1)	-3.78(9-II-2)	-1.39(2)	-1.27(9-I-2)	-0.92(9-I-1)	1.22(8-I-2)
32	0.00(1)	0.00(1)	-0.84(2)	-0.05(8-I-1)	0.05(8-I-1)	0.00(1)
33	0.00(1)	0.00(1)	-0.80(2)	0.06(8-II-2)	0.04(8-I-1)	0.00(1)
34	0.00(1)	0.00(1)	-0.82(2)	0.09(8-II-1)	0.04(9-II-2)	0.00(1)
35	0.00(1)	0.00(1)	-0.84(2)	0.05(9-II-1)	0.01(2)	0.00(1)
36	0.00(1)	0.00(1)	-0.86(2)	0.04(9-II-1)	0.02(2)	0.00(1)

Nodo	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
38	-1.17(8-II-1)	-2.94(9-II-1)	-1.23(2)	-2.06(9-I-1)	0.74(9-II-1)	-0.65(9-II-1)
39	1.24(8-I-1)	-3.30(9-II-1)	-1.08(2)	1.73(9-II-1)	-0.67(9-I-1)	-0.27(9-II-2)
101	-0.66(9-I-1)	-2.03(9-II-1)	-0.97(9-II-1)	0.79(9-II-1)	0.19(8-I-1)	1.95(8-II-1)
102	1.39(8-I-1)	3.04(9-I-1)	-0.86(2)	-0.59(9-I-1)	0.30(8-I-1)	3.68(8-II-1)
103	-2.72(8-II-1)	3.71(9-I-1)	-1.16(2)	-0.57(9-I-4)	-0.44(9-I-1)	0.19(9-I-2)
104	-3.05(8-II-4)	3.56(9-I-4)	-1.26(2)	0.50(9-II-4)	0.34(8-I-3)	0.19(9-I-2)
105	-3.75(8-II-3)	3.47(9-I-4)	-1.40(9-I-1)	-0.25(9-I-3)	0.75(9-II-1)	0.19(9-I-2)
106	0.00(1)	0.00(1)	-0.85(2)	0.05(9-I-3)	0.03(2)	0.00(1)
106	-4.17(8-II-3)	3.47(9-I-4)	-1.53(2)	-0.29(9-I-4)	0.71(8-I-3)	0.19(9-I-2)
107	-5.48(8-II-3)	4.19(9-I-2)	-1.58(2)	0.51(9-II-3)	-0.49(8-II-3)	0.19(9-I-2)
108	-5.32(8-II-3)	4.57(9-I-2)	-1.26(9-I-3)	0.48(9-II-2)	-0.46(8-II-3)	0.19(9-I-2)
109	-4.26(8-II-3)	4.78(9-I-2)	-1.41(2)	-0.30(9-I-2)	-0.67(8-II-3)	0.19(9-I-2)
110	-2.92(8-II-4)	5.09(9-I-2)	-1.33(2)	-3.11(2)	-3.35(2)	0.19(9-I-2)
111	-1.62(8-II-3)	-4.09(9-II-2)	-0.95(2)	-0.40(9-I-2)	0.53(8-I-3)	-4.97(8-I-2)
112	0.00(1)	0.00(1)	-0.89(2)	0.02(9-II-4)	-0.02(8-II-1)	0.00(1)
112	-1.46(9-I-2)	-3.51(9-II-2)	-1.05(9-II-2)	0.75(9-II-2)	-0.82(9-I-2)	1.79(8-II-2)
113	0.00(1)	0.00(1)	-0.90(2)	0.03(9-I-1)	0.01(9-I-1)	0.00(1)
114	0.00(1)	0.00(1)	-0.87(2)	0.02(9-II-1)	-0.02(9-II-1)	0.00(1)
134	0.00(1)	0.00(1)	-0.90(2)	0.08(8-II-3)	0.02(8-II-1)	0.00(1)
206	0.00(1)	0.00(1)	-0.85(2)	0.06(9-I-3)	0.02(2)	0.00(1)
212	0.00(1)	0.00(1)	-0.90(2)	0.00(8-I-4)	0.00(8-I-4)	0.00(1)
213	0.00(1)	0.00(1)	-0.91(2)	-0.00(8-I-3)	0.00(8-I-3)	0.00(1)
213	0.00(1)	0.00(1)	-0.91(2)	0.02(9-I-1)	-0.01(9-I-1)	0.00(1)
214	0.00(1)	0.00(1)	-0.87(2)	0.00(8-I-3)	0.00(8-I-3)	0.00(1)
234	0.00(1)	0.00(1)	-0.91(2)	0.00(8-II-3)	-0.00(9-I-2)	0.00(1)
313	0.00(1)	0.00(1)	-0.91(2)	0.00(8-I-4)	0.00(8-I-3)	0.00(1)

Risultati Analisi Dinamica - Spostamenti massimi - Impalcati

Scenario di calcolo: **Set_NT_SLV_SLD_A2_STR/GEO_2018**

la tripletta (Cb [-SubC-Cbm]) indica la Combinazione - SottoCombinazione sismica - Posizione Masse, nel caso non sismico mancano SubC-Cbm

Piano	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
	mm	mm	mm	mrad	mrad	mrad
1	2.44(8-I-3)	-2.81(9-II-1)	-1.54(2-1)	0.00(1-1)	0.00(1-1)	-0.20(8-I-3)

Risultati Analisi Dinamica - Sollecitazioni Massime - Muri discretizzati

Scenario di calcolo: **Set_NT_SLV_SLD_A2_STR/GEO_2018**

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
		kg/cmq	kg/cmq	kg/cmq	kg*m/m	kg*m/m	kg*m/m
1	1	0.69(9-II-1)	-2.54(2)	-1.61(8-I-3)	-216(8-II-3)	-216(8-II-3)	295(2)
1	2	-1.23(9-I-1)	-3.38(2)	-1.45(8-I-3)	-301(8-II-3)	-162(8-II-3)	386(2)
1	3	-1.82(9-I-1)	-3.72(2)	-1.24(8-I-3)	-261(8-II-3)	105(8-I-3)	420(2)
1	4	-2.06(9-I-1)	-3.59(2)	-1.33(2)	-253(2)	198(9-II-1)	405(2)
1	5	-1.78(9-I-1)	-3.27(2)	-1.36(9-II-1)	-283(9-I-1)	294(9-II-1)	341(2)
1	6	-1.31(9-I-1)	-3.07(2)	-1.56(9-II-1)	-317(9-I-1)	339(2)	244(2)
1	7	-1.37(9-I-1)	-3.19(2)	-1.58(9-II-1)	-419(9-I-1)	320(2)	122(9-II-1)
1	8	-1.52(9-I-1)	-3.17(2)	-1.81(9-II-1)	-596(2)	269(2)	142(9-II-1)
1	9	-1.46(9-I-1)	-3.08(2)	-1.86(9-II-1)	-697(2)	234(2)	-153(9-I-1)
1	10	-1.35(2)	-2.93(2)	-1.79(9-II-1)	-747(2)	202(2)	-184(9-I-1)
1	11	-1.41(2)	-2.73(2)	-1.68(9-II-1)	-764(2)	184(8-II-3)	-205(9-I-1)
1	12	-1.38(2)	-2.50(2)	-1.56(9-II-1)	-742(2)	190(8-II-3)	-222(9-I-2)
1	13	-1.41(2)	-2.14(2)	-1.50(9-II-1)	-696(2)	179(8-II-3)	-233(2)
1	14	-1.38(2)	-1.84(8-II-3)	-1.46(9-II-1)	-659(2)	152(8-II-3)	-286(2)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
1	15	-1.27(2)	-1.55(9-I-2)	-1.46(9-II-1)	-596(2)	114(9-I-2)	-336(2)
1	16	-1.21(2)	-1.32(9-I-1)	-1.48(9-II-1)	-485(2)	-117(9-II-1)	-377(2)
1	17	-1.17(2)	1.26(9-II-1)	-1.47(9-II-1)	-322(2)	-176(9-II-1)	-406(2)
1	18	-1.16(2)	1.90(9-II-4)	-1.34(9-II-1)	-252(9-II-4)	-272(9-II-4)	-411(2)
1	19	-1.29(9-I-4)	2.56(9-II-4)	-0.96(9-II-1)	293(9-I-4)	-421(2)	-377(2)
1	20	-2.85(9-I-3)	3.38(9-II-4)	0.66(8-II-3)	375(9-I-3)	-636(2)	-180(2)
1	21	-2.10(9-I-3)	1.91(9-II-1)	1.22(2)	281(9-I-3)	-1013(2)	-229(2)
1	22	-1.51(9-I-4)	1.29(9-II-1)	1.65(2)	-142(9-II-3)	-1503(2)	-192(2)
1	23	-0.85(9-I-4)	-1.24(9-I-1)	1.72(2)	-279(2)	-1935(2)	-167(2)
1	24	0.87(2)	-1.41(9-I-1)	1.56(2)	-415(2)	-2303(2)	-139(2)
1	25	1.24(2)	-1.57(2)	1.28(9-I-1)	-499(2)	-2620(2)	-110(2)
1	26	1.39(2)	-1.86(2)	1.14(9-I-1)	-543(2)	-2906(2)	-78(2)
1	27	1.38(2)	-2.02(2)	1.00(9-I-1)	-574(2)	-3131(2)	-58(2)
1	28	1.35(2)	-2.12(2)	0.89(9-I-1)	-590(2)	-3266(2)	-51(2)
1	29	1.30(2)	-2.20(2)	0.78(9-I-1)	-597(2)	-3367(2)	-46(2)
1	30	1.19(2)	-2.25(2)	0.71(8-II-3)	-593(2)	-3486(2)	-31(2)
1	31	1.04(2)	-2.25(2)	0.67(8-II-3)	-595(2)	-3653(2)	-18(2)
1	32	0.90(2)	-2.26(2)	0.65(8-II-3)	-598(2)	-3767(2)	-17(8-I-3)
1	33	0.86(2)	-2.26(2)	0.66(8-II-3)	-589(2)	-3825(2)	-26(2)
1	34	0.87(2)	-2.25(2)	0.65(8-II-3)	-600(2)	-3871(2)	13(8-II-3)
1	35	0.85(2)	-2.25(2)	0.61(8-II-3)	-619(2)	-3903(2)	-16(8-I-3)
1	36	0.81(2)	-2.26(2)	0.61(8-II-3)	-592(2)	-3844(2)	13(8-II-3)
1	37	0.81(2)	-2.28(2)	0.61(8-II-3)	-572(2)	-3748(2)	-12(8-I-3)
1	38	0.92(2)	-2.30(2)	0.59(8-II-3)	-593(2)	-3762(2)	-14(8-I-3)
1	39	1.11(2)	-2.30(2)	0.55(8-II-3)	-634(2)	-3823(2)	-16(8-I-3)
1	40	1.23(2)	-2.31(2)	0.48(8-II-3)	-656(2)	-3867(2)	-18(8-I-3)
1	41	1.24(2)	-2.31(2)	-0.50(8-I-3)	-652(2)	-3881(2)	22(8-II-3)
1	42	1.22(2)	-2.30(2)	-0.50(8-I-3)	-644(2)	-3854(2)	27(8-II-3)
1	43	1.25(2)	-2.28(2)	-0.49(9-I-3)	-634(2)	-3761(2)	30(8-II-3)
1	44	1.30(2)	-2.23(2)	-0.50(9-I-3)	-630(2)	-3636(2)	37(8-II-3)
1	45	1.27(2)	-2.15(2)	-0.68(2)	-620(2)	-3534(2)	47(8-II-3)
1	46	1.28(8-II-3)	-2.01(2)	-0.87(2)	-580(2)	-3419(2)	57(8-II-3)
1	47	1.27(8-II-3)	-1.82(2)	-0.98(2)	-523(2)	-3266(2)	66(8-II-3)
1	48	1.19(8-II-3)	-1.56(2)	-1.06(2)	-478(2)	-3095(2)	79(8-II-3)
1	49	1.05(8-II-3)	-1.20(2)	-1.13(2)	-425(2)	-2886(2)	91(8-II-3)
1	50	0.77(8-II-3)	-0.77(9-I-2)	-1.16(2)	-345(2)	-2600(2)	115(2)
1	51	-0.61(8-I-3)	-0.38(8-II-3)	-1.17(8-II-3)	-229(2)	-2236(2)	142(2)
1	52	-0.71(2)	1.05(2)	-1.10(8-II-3)	-98(2)	-1805(2)	140(2)
1	53	-1.13(2)	2.70(2)	1.05(8-I-3)	90(8-II-3)	-1344(2)	112(9-I-2)
1	54	-1.06(2)	4.08(2)	1.70(9-I-3)	136(9-II-3)	-969(2)	218(2)
1	55	-0.73(2)	2.25(9-I-2)	1.97(9-I-3)	-221(9-I-3)	-857(2)	372(2)
1	56	-0.92(9-II-2)	0.58(9-I-2)	2.10(9-I-3)	-375(2)	-677(2)	489(2)
1	57	-1.00(9-II-2)	-1.53(9-I-3)	1.79(2)	-572(2)	-525(2)	546(2)
1	58	-0.70(2)	-2.14(9-I-3)	1.93(2)	-734(2)	-450(2)	519(2)
1	59	-0.80(9-II-2)	-2.70(2)	2.04(2)	-810(2)	-293(2)	448(2)
1	60	-1.23(9-II-2)	-3.95(2)	1.67(2)	-724(2)	-132(9-II-3)	399(2)
1	61	-1.14(9-II-2)	-5.03(9-I-2)	1.07(2)	-607(2)	472(9-I-2)	368(2)
1	62	-0.89(8-I-3)	-5.40(9-I-2)	2.35(9-II-2)	-701(9-II-2)	633(9-I-2)	336(2)
1	63	-1.41(9-I-3)	-4.29(2)	3.12(9-II-2)	-700(9-II-2)	531(9-I-2)	328(9-I-2)
1	64	-1.95(9-I-3)	-4.15(2)	3.19(9-II-2)	-576(2)	374(9-I-2)	293(9-I-3)
1	65	-2.23(9-I-3)	-4.03(2)	2.91(9-II-2)	-533(2)	259(2)	248(9-I-3)
1	66	-2.20(9-I-3)	-3.87(2)	2.46(9-II-2)	-454(2)	302(2)	181(9-I-2)
1	67	-1.66(9-I-3)	-3.67(2)	1.90(9-II-2)	-311(2)	346(2)	89(9-I-2)
1	68	-1.47(9-I-3)	-3.58(2)	2.11(9-II-2)	-336(9-I-2)	492(9-II-2)	-104(2)
1	69	-1.77(9-I-3)	-3.83(2)	2.01(9-II-2)	-411(9-I-2)	577(9-II-2)	-207(2)
1	70	-2.03(9-I-2)	-4.19(2)	1.06(9-II-2)	-321(2)	491(9-II-2)	-288(2)
1	71	-1.82(9-I-2)	-3.85(2)	0.78(8-II-3)	-341(2)	165(2)	-318(2)
1	72	1.29(9-II-3)	-3.13(2)	-1.14(8-I-3)	-321(8-I-3)	-196(8-I-3)	-276(2)
1	73	0.97(9-II-3)	-2.26(2)	-1.16(8-I-3)	-239(8-I-3)	-175(8-I-3)	-197(2)
1	74	0.87(2)	-2.73(2)	1.34(8-II-3)	-190(2)	-395(2)	-121(2)
1	75	2.10(9-II-3)	-2.98(2)	1.33(9-II-3)	-323(8-II-3)	-618(2)	-128(2)
1	76	3.15(8-II-3)	-2.92(2)	-1.07(9-I-3)	-505(8-II-3)	-656(2)	-100(9-II-3)
1	77	-3.67(9-I-3)	-2.64(2)	-1.17(9-I-2)	-532(8-II-3)	-552(2)	-107(9-II-2)
1	78	-3.88(9-I-3)	-2.22(2)	-1.71(8-II-3)	481(9-I-3)	-401(2)	-134(9-II-2)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
1	79	-3.71(9-I-3)	-1.81(2)	-1.99(8-II-3)	438(9-I-3)	-274(2)	-137(9-II-2)
1	80	-3.93(2)	-1.55(2)	2.14(8-I-3)	446(2)	-198(2)	-137(9-II-2)
1	81	-4.15(2)	-1.43(2)	2.50(8-I-3)	477(2)	-175(2)	-134(9-II-2)
1	82	-3.89(2)	-1.47(2)	2.76(8-I-3)	445(2)	-265(8-I-3)	-128(9-II-2)
1	83	-3.17(2)	-1.68(2)	2.90(8-I-3)	348(2)	-393(8-I-3)	-118(9-II-2)
1	84	-3.02(8-II-3)	-2.07(2)	3.28(2)	381(8-II-3)	-551(8-I-3)	-116(2)
1	85	-3.18(8-II-3)	-2.33(2)	3.53(2)	-508(8-I-3)	-736(8-I-3)	-143(2)
1	86	4.00(8-I-3)	-2.95(2)	3.16(2)	-676(8-I-3)	-874(2)	-130(2)
1	87	3.88(8-I-3)	-3.38(2)	2.21(2)	-642(8-I-3)	-1007(2)	-97(9-II-3)
1	88	3.79(2)	-3.53(2)	1.83(8-II-3)	-663(2)	-1001(2)	-115(8-II-3)
1	89	3.54(2)	-3.49(2)	-1.55(8-I-3)	-650(2)	-896(2)	131(8-I-3)
1	90	3.29(2)	-3.36(2)	-1.56(8-I-3)	-630(2)	-881(2)	125(8-I-3)
1	91	4.12(8-II-3)	-3.11(2)	-2.22(2)	-620(8-II-3)	-1004(2)	77(8-I-3)
1	92	3.89(8-II-3)	-3.00(2)	-2.96(2)	-566(8-II-3)	-811(2)	86(2)
1	93	-2.57(9-I-3)	-2.22(2)	-3.13(2)	-349(9-II-3)	-518(2)	117(2)
1	94	-2.38(2)	-1.57(2)	-2.67(2)	297(9-I-3)	-332(2)	88(2)
1	95	-3.47(2)	-1.40(2)	-2.58(8-II-3)	385(2)	-218(9-II-4)	71(9-II-1)
1	96	-3.96(2)	-1.22(2)	-2.38(8-II-3)	458(2)	-189(9-II-2)	76(9-II-1)
1	97	-3.98(2)	-1.21(2)	-2.01(8-II-3)	463(2)	-238(8-I-3)	79(9-II-1)
1	98	-3.64(8-II-3)	-1.36(2)	1.74(9-I-3)	454(8-II-3)	-327(8-I-3)	81(9-II-1)
1	99	-4.19(8-II-3)	-1.72(2)	1.64(9-I-3)	532(8-II-3)	-438(8-I-3)	-87(9-I-1)
1	100	-4.66(8-II-3)	-2.18(2)	1.33(2)	594(8-II-3)	-575(8-I-3)	-95(9-I-1)
1	101	4.52(8-I-3)	-2.46(2)	1.05(2)	-694(8-I-3)	-714(2)	109(8-I-3)
1	102	4.08(8-I-3)	-2.76(2)	1.51(8-II-3)	-615(8-I-3)	-809(2)	146(8-I-3)
1	103	2.91(8-I-3)	-2.86(2)	-2.14(8-I-3)	-424(8-I-3)	-777(2)	156(8-I-3)
1	104	1.52(8-I-3)	-2.78(2)	-2.36(8-I-3)	-210(2)	-628(2)	161(2)
1	105	0.49(9-II-1)	-2.61(2)	-1.94(8-I-3)	-81(2)	-366(2)	198(2)
1	106	-0.79(2)	0.22(2)	1.01(8-I-2)	-94(9-I-2)	-560(2)	510(2)
1	107	-0.80(2)	1.14(2)	0.99(8-I-2)	52(9-II-3)	-840(2)	464(2)
1	108	-0.71(2)	1.76(2)	0.94(8-I-3)	62(8-II-3)	-1132(2)	338(2)
1	109	-0.50(2)	0.72(2)	-0.80(8-II-3)	-20(2)	-1291(2)	378(2)
1	110	-0.52(8-I-3)	-0.40(8-II-3)	-0.86(8-II-3)	-103(2)	-1491(2)	350(2)
1	111	-0.58(8-I-3)	-0.77(2)	-0.50(9-I-2)	190(8-I-3)	-238(2)	443(2)
1	112	-0.54(8-I-3)	-0.53(9-I-2)	-0.65(9-I-2)	109(8-I-3)	-802(2)	447(2)
1	113	-0.67(2)	-0.31(9-I-4)	0.56(8-I-3)	139(8-I-3)	-405(2)	498(2)
1	114	-0.55(2)	0.29(8-I-2)	-0.57(8-II-3)	75(8-I-3)	-802(2)	493(2)
1	115	1.05(8-II-3)	-1.90(2)	-0.73(2)	-412(2)	-2224(2)	134(2)
1	116	1.01(8-II-3)	-1.75(2)	-0.84(2)	-353(2)	-2118(2)	163(2)
1	117	-0.63(8-I-3)	-0.79(2)	-0.92(2)	-207(2)	-1754(2)	281(2)
1	118	0.83(8-II-3)	-1.18(2)	-0.96(2)	-290(2)	-1968(2)	225(2)
1	119	0.94(8-II-3)	-1.50(2)	-0.91(2)	-319(2)	-2054(2)	199(2)
1	120	-0.54(8-I-3)	-1.27(2)	-0.58(9-I-2)	181(8-I-3)	-100(9-I-2)	340(2)
1	121	0.67(8-II-3)	-1.19(2)	-0.83(2)	-171(2)	-1289(2)	308(2)
1	122	-0.54(8-I-3)	-1.26(2)	-0.69(2)	-119(8-II-3)	-675(2)	349(2)
1	123	-0.56(8-I-3)	-0.96(2)	-0.74(2)	-115(8-II-3)	-1017(2)	389(2)
1	124	0.71(8-II-3)	-1.50(2)	-0.75(2)	-154(8-II-3)	-1071(2)	248(2)
1	125	0.83(8-II-3)	-1.81(2)	-0.62(2)	-254(2)	-1241(2)	187(2)
1	126	0.77(8-II-3)	-1.67(2)	-0.69(2)	-157(8-II-3)	-1053(2)	251(2)
1	127	0.63(8-II-3)	-1.76(2)	-0.55(2)	-118(8-II-3)	-374(2)	248(2)
1	128	-0.46(8-I-3)	-1.63(2)	-0.52(9-I-2)	140(8-I-3)	322(2)	221(2)
1	129	-0.40(9-I-3)	-1.82(2)	-0.39(9-I-2)	91(8-I-3)	654(2)	128(2)
1	130	0.62(8-II-3)	-1.92(2)	-0.40(2)	-176(2)	-467(2)	132(2)
1	131	0.49(8-II-3)	-1.90(2)	-0.38(9-I-3)	-81(8-II-3)	97(2)	149(2)
1	132	0.63(8-II-3)	-1.89(2)	-0.48(2)	-119(8-II-3)	-384(2)	188(2)
1	133	0.56(2)	-1.98(2)	-0.35(9-I-3)	-104(2)	-114(2)	81(2)
1	134	0.48(2)	-2.00(2)	-0.30(9-I-3)	-63(8-II-3)	180(2)	71(2)
1	135	0.47(2)	-2.04(2)	-0.25(8-I-2)	-53(2)	293(2)	38(8-II-3)
1	136	0.30(9-II-3)	-1.95(2)	-0.18(8-I-2)	36(8-I-3)	766(2)	37(2)
1	137	0.34(9-II-3)	-1.90(2)	-0.28(9-I-3)	52(8-I-3)	711(2)	81(2)
1	138	-0.39(9-I-3)	-1.88(2)	-0.19(9-I-2)	85(2)	961(2)	37(2)
1	139	1.07(2)	-2.23(2)	-0.43(8-I-3)	-492(2)	-2682(2)	29(2)
1	140	1.02(2)	-2.23(2)	-0.42(8-I-3)	-484(2)	-2575(2)	20(8-II-3)
1	141	0.85(2)	-2.17(2)	-0.37(8-I-3)	-320(2)	-1441(2)	32(8-II-3)
1	142	0.67(2)	-2.11(2)	-0.31(8-I-2)	-171(2)	-459(2)	37(8-II-3)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
1	143	0.71(2)	-2.09(2)	-0.33(9-I-3)	-196(2)	-630(2)	62(2)
1	144	0.90(2)	-2.16(2)	-0.37(8-I-2)	-334(2)	-1585(2)	50(2)
1	145	0.81(8-II-3)	-1.95(2)	-0.55(2)	-285(2)	-1245(2)	138(2)
1	146	1.02(8-II-3)	-2.04(2)	-0.60(2)	-448(2)	-2280(2)	100(2)
1	147	0.81(2)	-2.02(2)	-0.43(2)	-297(2)	-1222(2)	106(2)
1	148	1.04(2)	-2.13(2)	-0.46(2)	-450(2)	-2310(2)	72(2)
1	149	1.08(2)	-2.20(2)	-0.44(9-I-3)	-456(2)	-2560(2)	69(2)
1	150	0.96(2)	-2.17(2)	-0.40(9-I-3)	-362(2)	-1866(2)	74(2)
1	151	1.09(2)	-2.23(2)	-0.44(9-I-3)	-509(2)	-2808(2)	41(2)
1	152	0.78(2)	-2.08(2)	-0.37(9-I-3)	-258(2)	-974(2)	80(2)
1	153	-0.79(9-I-1)	-1.79(2)	0.26(8-I-3)	51(2)	991(2)	-44(8-II-3)
1	154	-0.84(9-I-3)	-1.83(2)	0.35(9-II-2)	113(2)	951(2)	-57(2)
1	155	-0.92(9-I-3)	-1.96(2)	0.46(9-II-2)	209(2)	882(2)	-61(8-I-3)
1	156	-0.78(9-I-3)	-1.84(2)	0.40(9-II-2)	197(2)	909(2)	-33(8-I-3)
1	157	-0.57(9-I-3)	-1.78(2)	-0.38(9-I-2)	159(2)	902(2)	68(2)
1	158	-0.67(9-I-4)	-1.79(2)	0.20(9-II-2)	94(2)	1004(2)	10(8-I-3)
1	159	-0.57(9-I-3)	-1.80(2)	-0.27(9-I-2)	113(2)	986(2)	29(2)
1	160	-0.73(9-I-3)	-1.80(2)	0.30(9-II-2)	132(2)	964(2)	-10(9-II-1)
1	161	-0.81(9-I-1)	-1.80(2)	0.34(8-I-3)	-84(2)	934(2)	-100(8-II-3)
1	162	2.42(8-I-3)	-2.70(2)	1.58(2)	-546(8-I-3)	-323(8-I-3)	-164(2)
1	163	2.11(2)	-2.66(2)	0.85(2)	-497(2)	-223(9-II-2)	-197(8-II-3)
1	164	1.48(9-II-2)	-2.41(2)	0.99(2)	-381(8-I-3)	281(2)	-191(8-II-3)
1	165	1.66(2)	-2.52(2)	0.28(8-II-3)	-381(2)	323(2)	204(8-I-3)
1	166	0.93(9-II-2)	-2.08(2)	0.37(2)	-218(2)	735(2)	-183(8-II-3)
1	167	-1.04(9-I-3)	-2.11(2)	0.54(9-II-2)	229(2)	858(2)	-124(2)
1	168	-0.93(9-I-2)	-1.95(2)	0.42(8-I-3)	129(8-II-3)	926(2)	-125(2)
1	169	-1.00(9-I-2)	-2.16(2)	0.63(2)	-241(8-I-3)	705(2)	-195(2)
1	170	-1.02(9-I-2)	-2.08(2)	0.54(8-I-3)	198(8-II-3)	824(2)	-203(2)
1	171	-1.21(9-I-2)	-2.18(2)	0.77(2)	265(8-II-3)	678(2)	-238(2)
1	172	-1.30(9-I-2)	-2.28(2)	0.80(8-I-3)	252(2)	692(2)	-216(2)
1	173	-1.13(9-I-2)	-2.23(2)	0.63(8-I-3)	237(2)	802(2)	-185(2)
1	174	-1.32(9-I-3)	-2.32(2)	0.79(8-I-3)	352(2)	743(2)	-181(8-I-3)
1	175	-1.52(9-I-2)	-2.37(2)	1.09(8-I-3)	398(2)	581(2)	-203(8-I-3)
1	176	-1.51(9-I-2)	-2.32(2)	1.07(2)	292(2)	526(2)	-227(2)
1	177	-2.30(9-I-2)	-2.03(2)	2.14(8-I-3)	359(2)	-224(8-I-3)	-194(2)
1	178	-1.85(9-I-2)	-2.22(2)	1.50(2)	333(2)	291(2)	-222(2)
1	179	-2.72(2)	-1.96(2)	2.08(8-I-3)	457(2)	194(9-I-2)	-184(9-II-2)
1	180	-1.89(2)	-2.25(2)	1.52(8-I-3)	435(2)	359(2)	-205(8-I-3)
1	181	1.31(9-II-2)	-2.26(2)	1.16(2)	-377(8-I-3)	369(2)	-245(2)
1	182	2.29(8-I-3)	-2.52(2)	2.02(2)	-527(8-I-3)	-294(8-I-3)	-247(2)
1	183	-2.35(8-II-3)	-2.22(2)	2.39(2)	376(8-II-3)	-328(8-I-3)	-226(2)
1	184	-2.26(8-II-3)	-2.40(2)	2.28(2)	403(8-II-3)	-340(8-I-3)	-248(2)
1	185	-1.78(9-I-2)	-2.28(2)	1.80(2)	362(8-II-3)	248(9-I-2)	-265(2)
1	186	-1.44(9-I-2)	-2.31(2)	1.21(2)	318(8-II-3)	439(2)	-266(2)
1	187	-0.97(9-I-3)	-1.94(2)	0.79(9-II-2)	336(2)	622(2)	92(8-II-3)
1	188	-0.77(9-I-3)	-1.60(2)	0.63(9-II-2)	334(2)	557(2)	167(2)
1	189	-0.61(8-I-3)	-1.37(2)	-0.49(9-I-2)	278(2)	413(2)	281(2)
1	190	-0.76(9-I-3)	-1.69(2)	0.56(9-II-2)	317(2)	714(2)	124(2)
1	191	-0.68(9-I-3)	-1.73(2)	-0.44(9-I-2)	253(2)	828(2)	102(2)
1	192	-0.59(9-I-3)	-1.59(2)	-0.51(9-I-2)	231(2)	641(2)	187(2)
1	193	-0.86(9-I-3)	-1.86(2)	0.52(9-II-2)	274(2)	834(2)	62(8-II-3)
1	194	-0.94(9-I-3)	-1.90(2)	0.66(9-II-2)	336(2)	741(2)	81(8-II-3)
1	195	-0.82(2)	-0.89(9-I-3)	1.21(2)	-147(2)	-346(2)	478(2)
1	196	-0.67(2)	-1.08(2)	0.50(9-II-2)	263(2)	159(8-I-3)	357(2)
1	197	-0.81(2)	-0.84(2)	0.64(8-I-3)	160(8-I-3)	-117(2)	418(2)
1	198	-0.79(2)	-1.66(9-I-3)	1.44(2)	-256(2)	-204(2)	384(2)
1	199	-0.85(2)	-1.54(2)	0.67(9-II-2)	265(2)	335(2)	223(2)
1	200	-0.89(2)	-1.53(2)	0.94(2)	148(9-I-3)	141(8-I-3)	291(2)
1	201	-0.82(2)	-2.95(2)	1.29(2)	-300(2)	217(9-I-3)	225(2)
1	202	-0.91(2)	-2.31(2)	1.13(2)	-143(9-II-3)	214(2)	189(2)
1	203	-0.82(9-II-2)	-2.41(2)	1.48(2)	-366(2)	-159(8-II-3)	297(2)
1	204	-0.97(2)	-2.11(2)	0.88(9-II-2)	243(9-I-3)	433(2)	109(2)
1	205	-2.81(9-I-3)	-2.18(2)	1.33(8-I-3)	442(9-I-3)	123(9-I-4)	-176(9-II-2)
1	206	-2.15(9-I-3)	-2.39(2)	1.12(8-I-3)	422(9-I-3)	441(2)	-188(9-II-2)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
1	207	-2.11(9-I-3)	-2.33(2)	1.31(8-I-3)	457(2)	404(2)	-197(9-II-2)
1	208	-2.08(2)	-2.25(2)	1.46(8-I-3)	470(2)	386(2)	-201(9-II-2)
1	209	-2.94(2)	-1.95(2)	1.93(8-I-3)	493(2)	168(9-I-2)	-183(9-II-2)
1	210	-2.80(2)	-2.05(2)	1.67(8-I-3)	470(2)	139(9-I-1)	-181(9-II-2)
1	211	-1.12(9-I-3)	-2.16(2)	0.73(9-II-2)	346(2)	760(2)	-111(9-II-2)
1	212	-1.02(9-I-3)	-2.04(2)	0.58(9-II-2)	295(2)	820(2)	-87(8-I-3)
1	213	-1.14(9-I-3)	-2.25(2)	0.65(9-II-2)	324(2)	812(2)	-132(9-II-2)
1	214	-1.27(9-I-3)	-2.37(2)	0.78(9-II-2)	367(2)	785(2)	-155(9-II-2)
1	215	-1.34(9-I-3)	-2.41(2)	0.79(9-II-2)	372(2)	762(2)	-173(9-II-2)
1	216	-1.78(9-I-3)	-2.45(2)	1.08(8-I-3)	438(2)	572(2)	-200(9-II-2)
1	217	-1.51(9-I-3)	-2.47(2)	0.96(8-I-3)	417(2)	684(2)	-194(9-II-2)
1	218	-1.69(9-I-3)	-2.36(2)	1.09(8-I-3)	442(2)	588(2)	-198(9-II-2)
1	219	-1.70(9-I-3)	-2.47(2)	0.98(8-I-3)	409(2)	665(2)	-194(9-II-2)
1	220	-0.87(2)	-3.42(2)	1.24(9-II-2)	-225(9-II-3)	456(9-I-2)	179(2)
1	221	-1.10(9-I-3)	-2.70(2)	1.09(9-II-2)	258(9-I-3)	528(2)	137(9-I-2)
1	222	-1.17(9-I-3)	-2.32(2)	0.89(9-II-2)	328(2)	685(2)	-131(9-II-2)
1	223	-1.28(9-I-3)	-3.54(2)	1.51(9-II-2)	-291(9-II-3)	493(9-I-2)	305(9-I-2)
1	224	-1.08(9-I-3)	-3.85(2)	1.75(9-II-2)	-356(9-II-3)	573(9-I-2)	305(9-I-2)
1	225	-1.40(9-I-3)	-3.95(2)	2.10(9-II-2)	-464(9-II-2)	499(9-I-2)	352(9-I-2)
1	226	-1.40(9-I-3)	-3.59(2)	1.56(9-II-2)	-326(9-II-3)	547(2)	292(9-I-2)
1	227	-1.61(9-I-3)	-3.91(2)	2.21(9-II-2)	-426(9-II-2)	390(2)	316(9-I-2)
1	228	-1.71(9-I-3)	-3.87(2)	2.12(9-II-2)	-326(9-II-2)	437(2)	253(9-I-2)
1	229	-1.43(9-I-3)	-3.63(2)	1.55(9-II-2)	-305(9-II-3)	590(2)	-277(9-II-2)
1	230	-1.57(9-I-3)	-3.82(2)	1.90(9-II-2)	-287(2)	462(2)	-160(9-II-2)
1	231	-1.52(9-I-3)	-3.86(2)	1.66(9-II-2)	-225(2)	532(2)	-208(9-II-2)
1	232	-1.63(9-I-3)	-3.85(2)	1.96(9-II-2)	-292(2)	473(2)	-200(9-II-2)
1	233	-1.44(9-I-3)	-3.70(2)	1.53(9-II-2)	-236(9-II-3)	596(2)	-244(9-II-2)
1	234	-2.80(9-I-3)	-2.36(2)	0.94(8-I-3)	474(9-I-3)	106(9-I-3)	166(9-I-2)
1	235	-2.08(9-I-3)	-2.46(2)	0.93(9-II-2)	446(9-I-3)	481(2)	-164(9-II-2)
1	236	-2.60(9-I-3)	-2.54(2)	-0.70(9-I-2)	443(9-I-3)	76(9-I-3)	-121(9-II-2)
1	237	-1.99(9-I-3)	-2.53(2)	0.79(9-II-2)	414(9-I-3)	449(2)	-137(9-II-3)
1	238	-1.33(9-I-3)	-2.92(2)	0.70(9-II-3)	-168(9-II-2)	91(8-II-3)	-247(2)
1	239	1.27(9-II-3)	-2.75(2)	0.93(8-II-3)	-171(2)	-159(2)	-223(2)
1	240	-1.82(9-I-3)	-2.65(2)	0.64(9-II-2)	312(9-I-3)	335(2)	-158(9-II-3)
1	241	-2.14(9-I-3)	-2.71(2)	0.56(9-II-4)	-399(9-II-3)	-97(8-II-3)	-144(9-II-3)
1	242	1.68(9-II-3)	-2.82(2)	0.73(9-II-3)	-257(9-II-3)	-131(2)	-191(2)
1	243	-1.57(9-I-3)	-2.79(2)	0.56(9-II-3)	-215(9-II-3)	194(2)	-211(2)
1	244	-1.36(9-I-3)	-3.19(2)	1.18(9-II-2)	358(9-I-3)	677(2)	-279(9-II-2)
1	245	-1.28(9-I-3)	-3.07(2)	1.16(9-II-2)	313(9-I-3)	607(2)	-234(9-II-2)
1	246	-1.39(9-I-3)	-2.53(2)	0.89(9-II-2)	382(9-I-3)	785(2)	-190(9-II-2)
1	247	-1.30(9-I-3)	-2.63(2)	0.96(9-II-2)	360(9-I-3)	728(2)	-201(9-II-2)
1	248	-1.40(9-I-3)	-2.81(2)	0.98(9-II-2)	397(9-I-3)	766(2)	-229(9-II-2)
1	249	-1.43(9-I-3)	-3.41(2)	1.17(9-II-2)	-268(9-II-3)	660(2)	-211(9-II-2)
1	250	-1.57(9-I-3)	-3.61(2)	1.10(9-II-2)	-211(9-II-2)	531(2)	-186(2)
1	251	-1.39(9-I-3)	-3.29(2)	1.18(9-II-2)	344(9-I-3)	700(2)	-262(9-II-2)
1	252	-1.60(9-I-3)	-3.25(2)	0.75(9-II-2)	-245(9-II-2)	502(2)	-187(2)
1	253	-1.49(9-I-3)	-3.27(2)	0.59(9-II-3)	-235(9-II-2)	298(2)	-240(2)
1	254	-1.57(9-I-3)	-2.93(2)	0.63(9-II-1)	-223(9-II-3)	407(2)	-200(2)
1	255	-1.53(9-I-3)	-3.05(2)	0.91(9-II-2)	330(9-I-3)	658(2)	-154(9-II-3)
1	256	-1.47(9-I-3)	-2.90(2)	0.97(9-II-2)	401(9-I-3)	757(2)	-202(9-II-2)
1	257	-1.63(9-I-3)	-2.53(2)	0.91(9-II-2)	412(9-I-3)	727(2)	-176(9-II-2)
1	258	-1.66(9-I-3)	-2.62(2)	0.90(9-II-2)	411(9-I-3)	696(2)	-157(9-II-3)
1	259	-1.64(9-I-3)	-2.77(2)	0.79(9-II-2)	326(9-I-3)	564(2)	-155(9-II-3)
1	260	0.28(9-II-4)	-1.99(2)	0.20(8-II-2)	47(2)	844(2)	17(8-II-3)
1	261	0.40(2)	-2.07(2)	0.29(8-II-4)	27(9-II-1)	577(2)	-46(2)
1	262	0.47(2)	-2.05(2)	0.25(8-II-2)	-56(2)	316(2)	-23(8-I-3)
1	263	0.77(2)	-2.25(2)	0.53(8-II-3)	-363(2)	-2121(2)	-22(2)
1	264	0.65(2)	-2.19(2)	0.42(8-II-3)	-149(2)	-571(2)	-44(2)
1	265	0.65(2)	-2.13(2)	0.31(8-II-2)	-175(2)	-445(2)	-24(8-I-3)
1	266	0.73(2)	-2.18(2)	0.38(8-II-3)	-208(2)	-950(2)	-49(2)
1	267	0.80(2)	-2.18(2)	0.36(8-II-3)	-316(2)	-1371(2)	-24(8-I-3)
1	268	0.95(2)	-2.24(2)	0.44(8-II-3)	-462(2)	-2453(2)	-17(8-I-3)
1	269	0.85(2)	-2.26(2)	0.48(8-II-3)	-396(2)	-2245(2)	-18(8-I-3)
1	270	0.32(2)	-2.01(2)	0.52(8-II-3)	45(9-II-3)	545(2)	-102(2)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
1	271	0.88(2)	-2.22(2)	0.64(8-II-3)	-482(2)	-2875(2)	-48(2)
1	272	0.82(2)	-2.20(2)	0.63(8-II-3)	-345(2)	-1941(2)	-58(2)
1	273	0.84(2)	-2.25(2)	0.60(8-II-3)	-392(2)	-2556(2)	-16(2)
1	274	0.92(2)	-2.23(2)	0.65(8-II-3)	-394(2)	-2432(2)	-98(2)
1	275	0.66(2)	-2.14(2)	0.58(8-II-3)	-157(2)	-598(2)	-91(2)
1	276	0.32(2)	-2.07(2)	0.38(8-II-4)	49(2)	700(2)	-33(9-I-3)
1	277	0.81(2)	-2.23(2)	0.59(8-II-3)	-494(2)	-2923(2)	-10(8-I-3)
1	278	0.75(2)	-2.21(2)	0.57(8-II-3)	-338(2)	-1927(2)	-53(2)
1	279	0.79(2)	-2.25(2)	0.55(8-II-3)	-377(2)	-2425(2)	31(2)
1	280	0.80(2)	-2.25(2)	0.61(8-II-3)	-393(2)	-2586(2)	-62(2)
1	281	0.62(2)	-2.17(2)	0.50(8-II-3)	-147(2)	-529(2)	-51(2)
1	282	0.96(2)	-2.18(2)	0.68(8-II-3)	-403(2)	-2118(2)	-87(2)
1	283	1.05(2)	-2.10(2)	0.76(9-I-1)	-429(2)	-2094(2)	-114(2)
1	284	-0.34(9-I-2)	-1.86(2)	0.60(8-II-3)	74(9-II-3)	488(2)	-179(2)
1	285	0.80(2)	-1.98(2)	0.74(9-I-1)	-266(2)	-1080(2)	-151(2)
1	286	0.75(2)	-2.08(2)	0.66(8-II-3)	-190(2)	-831(2)	-83(2)
1	287	0.54(2)	-1.92(2)	0.67(9-I-1)	-88(2)	-201(2)	-184(2)
1	288	0.79(2)	-1.86(2)	0.82(9-I-1)	-249(2)	-1076(2)	-213(2)
1	289	1.09(2)	-1.99(2)	0.86(9-I-1)	-427(2)	-2106(2)	-137(2)
1	290	0.80(2)	-1.46(9-I-1)	1.07(9-I-1)	-326(2)	-1519(2)	-279(2)
1	291	1.11(2)	-1.87(2)	0.94(9-I-1)	-433(2)	-2130(2)	-158(2)
1	292	0.83(2)	-1.75(2)	0.90(9-I-1)	-257(2)	-1236(2)	-258(2)
1	293	1.03(2)	-1.72(2)	1.02(9-I-1)	-360(2)	-1833(2)	-225(2)
1	294	-0.56(9-I-1)	-1.41(2)	0.70(9-I-1)	185(8-II-3)	436(2)	-363(2)
1	295	-0.45(9-I-1)	-1.66(2)	0.67(9-I-1)	136(8-II-3)	486(2)	-276(2)
1	296	0.44(2)	-1.75(2)	0.75(9-I-1)	57(9-II-3)	-148(2)	-277(2)
1	297	0.45(2)	-1.41(9-I-1)	0.92(9-I-1)	-153(2)	-692(2)	-382(2)
1	298	0.48(2)	-1.57(2)	0.84(9-I-1)	-106(2)	-428(2)	-309(2)
1	299	-0.43(9-I-1)	-1.40(9-I-1)	0.81(9-I-1)	108(8-II-3)	-27(2)	-414(2)
1	300	-1.09(2)	-1.39(9-I-1)	-1.18(9-II-1)	-162(9-II-1)	107(9-I-1)	-439(2)
1	301	-0.63(9-I-1)	-1.41(9-I-1)	0.72(9-I-1)	211(8-II-3)	319(2)	-458(2)
1	302	-0.70(2)	-1.42(9-I-1)	-0.73(9-II-1)	199(8-II-3)	214(2)	-500(2)
1	303	-0.92(2)	-1.42(9-I-1)	-0.94(9-II-1)	151(9-I-1)	125(8-II-3)	-489(2)
1	304	-0.99(2)	-1.31(9-I-1)	-1.09(9-II-1)	-147(9-II-1)	-128(9-II-1)	-492(2)
1	305	-0.80(2)	-1.37(9-I-1)	-0.82(9-II-1)	156(9-I-1)	-84(9-II-1)	-548(2)
1	306	-1.03(9-I-4)	1.49(9-II-1)	0.78(9-I-1)	176(9-I-4)	-468(2)	-536(2)
1	307	-1.16(9-I-4)	1.96(9-II-1)	-0.73(9-II-1)	227(9-I-4)	-464(2)	-498(2)
1	308	-1.46(9-I-4)	1.68(9-II-1)	0.93(2)	208(9-I-4)	-709(2)	-453(2)
1	309	-0.89(2)	1.65(9-II-1)	-0.91(9-II-1)	179(9-I-4)	-252(2)	-516(2)
1	310	-0.80(9-I-4)	1.35(9-II-1)	0.72(9-I-1)	166(9-I-1)	-237(2)	-568(2)
1	311	-0.81(9-I-4)	-1.29(9-I-1)	1.24(2)	-153(2)	-1165(2)	-401(2)
1	312	0.52(2)	-1.38(9-I-1)	1.19(2)	-254(2)	-1348(2)	-346(2)
1	313	-1.19(9-I-4)	1.24(9-II-1)	1.14(2)	130(9-I-4)	-951(2)	-433(2)
1	314	-0.56(9-I-1)	-1.40(9-I-1)	0.80(9-I-1)	134(8-II-3)	26(9-I-1)	-507(2)
1	315	-0.51(9-I-4)	-1.38(9-I-1)	0.94(9-I-1)	-85(2)	-612(2)	-464(2)
1	316	-0.72(9-I-4)	-1.34(9-I-1)	0.91(9-I-1)	83(9-I-1)	-576(2)	-517(2)
1	317	-0.91(9-I-4)	-1.30(9-I-1)	0.86(9-I-1)	133(9-I-4)	-533(2)	-539(2)
1	318	-0.75(9-I-4)	-1.35(9-I-1)	0.78(9-I-1)	147(9-I-1)	-242(2)	-574(2)
1	319	-0.65(9-I-4)	-1.39(9-I-1)	0.79(9-I-1)	134(9-I-1)	-145(2)	-546(2)
1	320	-0.66(9-I-1)	-1.39(9-I-1)	0.75(9-I-1)	163(9-I-1)	68(9-I-1)	-561(2)
1	321	-1.49(8-II-3)	-2.05(2)	-0.75(9-II-2)	420(8-II-3)	776(2)	197(8-I-3)
1	322	-1.67(8-II-3)	-2.27(2)	-0.90(8-I-3)	317(8-II-3)	485(2)	268(8-I-3)
1	323	-1.63(8-II-3)	-2.17(2)	-0.80(9-II-2)	387(8-II-3)	676(2)	243(8-I-3)
1	324	-1.82(8-II-3)	-2.14(2)	-0.77(9-II-2)	394(8-II-3)	586(2)	242(8-I-3)
1	325	1.52(8-I-3)	-2.57(2)	-1.53(8-I-3)	-227(8-I-3)	-128(2)	253(8-I-3)
1	326	2.25(8-I-3)	-2.49(2)	-1.31(8-I-3)	-403(8-I-3)	-191(8-I-3)	248(8-I-3)
1	327	-2.00(8-II-3)	-2.26(2)	-0.89(8-I-3)	357(8-II-3)	299(2)	258(8-I-3)
1	328	-1.69(8-II-3)	-2.39(2)	-1.11(8-I-3)	255(8-II-3)	242(2)	275(8-I-3)
1	329	-1.35(9-I-1)	-3.12(2)	-1.36(9-II-1)	-207(2)	444(2)	222(2)
1	330	-1.38(9-I-1)	-3.04(2)	-1.43(9-II-1)	-285(2)	403(2)	169(2)
1	331	-1.36(9-I-1)	-2.96(2)	-1.29(9-II-1)	-145(2)	483(2)	183(9-II-1)
1	332	-1.12(8-II-3)	-2.54(2)	-1.61(8-I-3)	-88(9-II-1)	-83(2)	281(2)
1	333	-1.18(9-I-1)	-2.73(2)	-1.39(8-I-3)	100(9-I-4)	56(2)	306(2)
1	334	-1.41(8-II-3)	-2.52(2)	-1.25(8-I-3)	178(9-I-1)	201(2)	272(2)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
1	335	-1.50(8-II-3)	-2.46(2)	-1.03(8-I-3)	253(9-I-1)	432(2)	253(8-I-3)
1	336	-1.59(9-I-1)	-3.16(2)	-1.16(8-I-3)	-142(9-II-4)	289(2)	324(2)
1	337	-1.45(9-I-1)	-2.76(2)	-1.12(8-I-3)	196(9-I-1)	389(2)	269(2)
1	338	-1.40(9-I-1)	-2.88(2)	-1.27(8-I-3)	-133(9-II-4)	180(2)	315(2)
1	339	-1.52(8-II-3)	-2.37(2)	-0.89(9-II-2)	334(9-I-1)	629(2)	236(8-I-3)
1	340	-1.44(8-II-3)	-2.26(2)	-0.86(9-II-2)	386(8-II-3)	717(2)	211(8-I-3)
1	341	-1.43(8-II-3)	-2.68(2)	-1.00(8-I-3)	259(9-I-1)	554(2)	218(2)
1	342	-1.38(8-II-3)	-2.56(2)	-0.99(9-II-2)	305(9-I-1)	641(2)	198(8-I-3)
1	343	-1.52(9-I-1)	-3.19(2)	-1.20(9-II-2)	-132(2)	415(2)	282(2)
1	344	-1.47(9-I-1)	-2.97(2)	-1.08(8-I-3)	148(9-I-1)	495(2)	252(2)
1	345	-1.61(9-I-1)	-3.25(2)	-1.11(8-I-3)	-106(9-II-4)	363(2)	317(2)
1	346	-1.34(9-I-1)	-2.87(2)	-1.14(9-II-2)	117(8-II-4)	546(2)	188(9-II-1)
1	347	-1.36(9-I-1)	-2.84(2)	-1.09(9-II-2)	177(9-I-1)	562(2)	204(2)
1	348	-1.37(9-I-1)	-3.03(2)	-1.20(9-II-2)	-105(2)	484(2)	232(2)
1	349	-1.37(8-II-3)	-2.60(2)	-1.29(9-II-1)	-138(8-I-3)	447(2)	203(9-II-1)
1	350	-1.42(9-I-1)	-2.83(2)	-1.55(9-II-1)	-361(2)	337(2)	189(9-II-1)
1	351	-1.42(9-I-1)	-2.97(2)	-1.49(9-II-1)	-326(2)	371(2)	184(9-II-1)
1	352	-1.35(9-I-1)	-2.80(2)	-1.29(9-II-1)	-119(2)	470(2)	198(9-II-1)
1	353	-1.31(8-II-3)	-1.94(2)	-0.74(9-II-1)	417(8-II-3)	779(2)	149(8-I-3)
1	354	-1.34(8-II-3)	-2.66(2)	-1.13(9-II-1)	195(8-II-3)	556(2)	202(9-II-2)
1	355	-1.34(8-II-3)	-2.41(2)	-1.11(9-II-1)	274(8-II-3)	558(2)	204(9-II-2)
1	356	-1.35(8-II-3)	-2.42(2)	-1.00(9-II-1)	324(8-II-3)	629(2)	202(9-II-2)
1	357	-1.35(8-II-3)	-2.14(2)	-0.87(9-II-1)	407(8-II-3)	705(2)	184(8-I-3)
1	358	-0.79(8-II-3)	-1.39(9-I-1)	-0.71(9-II-1)	277(8-II-3)	505(2)	-357(2)
1	359	-0.75(9-I-2)	-1.54(2)	-0.59(9-II-1)	330(2)	700(2)	-257(2)
1	360	-0.95(8-II-3)	-1.50(2)	-0.75(9-II-1)	333(8-II-3)	643(2)	-219(2)
1	361	-1.25(8-II-3)	-1.95(2)	-0.89(9-II-1)	400(8-II-3)	651(2)	-161(9-I-2)
1	362	-1.09(8-II-3)	-1.72(2)	-0.80(9-II-1)	367(8-II-3)	662(2)	-172(9-I-1)
1	363	-1.14(8-II-3)	-1.79(2)	-0.72(9-II-1)	386(8-II-3)	758(2)	-138(9-I-2)
1	364	-1.30(8-II-3)	-2.14(2)	-1.08(9-II-1)	318(8-II-3)	545(2)	185(9-II-2)
1	365	-1.25(2)	-1.88(2)	-1.07(9-II-1)	302(8-II-3)	498(2)	-212(9-I-1)
1	366	-1.40(2)	-2.46(2)	-1.51(9-II-1)	-401(2)	268(2)	-216(9-I-1)
1	367	-1.39(2)	-2.18(2)	-1.41(9-II-1)	-297(2)	281(2)	-239(9-I-1)
1	368	-1.34(2)	-2.14(2)	-1.33(9-II-1)	-152(8-I-3)	371(2)	-219(9-I-1)
1	369	-1.36(9-I-2)	-2.65(2)	-1.55(9-II-1)	-382(2)	303(2)	-193(9-I-1)
1	370	-1.34(8-II-3)	-2.38(2)	-1.30(9-II-1)	-149(8-I-3)	416(2)	192(9-II-1)
1	371	-1.19(2)	-1.49(9-I-1)	-1.24(9-II-1)	-217(2)	150(8-II-3)	-377(2)
1	372	-1.37(2)	-1.82(2)	-1.33(9-II-1)	-197(2)	271(2)	-246(9-I-1)
1	373	-1.31(2)	-1.59(9-I-2)	-1.27(9-II-1)	-216(2)	208(2)	-306(2)
1	374	-1.22(2)	-1.56(2)	-1.05(9-II-1)	267(8-II-3)	438(2)	-239(9-I-1)
1	375	-1.05(2)	-1.47(9-I-1)	-1.03(9-II-1)	148(8-II-3)	215(2)	-414(2)
1	376	-0.93(2)	-1.44(9-I-1)	-0.87(9-II-1)	237(8-II-3)	360(2)	-401(2)
1	377	-1.10(2)	-1.49(9-I-1)	-1.04(9-II-1)	198(8-II-3)	331(2)	-331(2)
1	378	-0.67(9-I-2)	-1.99(2)	0.30(9-I-1)	163(2)	940(2)	-29(9-I-3)
1	379	-0.48(9-I-1)	-1.98(2)	0.33(8-II-4)	119(2)	957(2)	-31(9-I-3)
1	380	-0.60(9-I-2)	-1.94(2)	0.22(8-II-4)	132(2)	995(2)	19(9-II-3)
1	381	-0.82(9-I-2)	-2.02(2)	-0.28(9-II-1)	191(2)	897(2)	44(9-II-3)
1	382	-0.76(9-I-2)	-1.96(2)	0.18(9-I-1)	143(2)	936(2)	48(2)
1	383	-0.75(9-I-1)	-1.89(2)	0.11(9-I-4)	97(2)	971(2)	53(2)
1	384	-0.76(9-I-1)	-1.78(2)	0.18(8-I-3)	53(2)	999(2)	46(8-I-3)
1	385	-0.61(9-I-1)	-1.84(2)	0.11(9-II-2)	83(2)	1018(2)	21(2)
1	386	-0.58(9-I-1)	-1.89(2)	0.12(8-II-1)	98(2)	1015(2)	20(2)
1	387	-0.45(9-I-1)	-1.90(2)	0.11(8-II-2)	83(2)	1003(2)	20(2)
1	388	-0.83(9-I-1)	-1.94(2)	0.14(9-I-4)	102(8-I-3)	948(2)	102(2)
1	389	-0.80(9-I-1)	-1.87(2)	0.20(8-I-3)	78(8-I-3)	978(2)	101(8-I-3)
1	390	-0.80(9-I-1)	-1.97(2)	-0.24(9-II-3)	-158(8-II-3)	854(2)	148(2)
1	391	2.42(9-II-3)	-2.53(2)	-1.72(2)	-513(8-II-3)	-268(2)	187(2)
1	392	-1.55(9-I-3)	-2.26(2)	-1.72(2)	-334(8-II-3)	-139(9-II-4)	239(2)
1	393	-0.84(9-I-4)	-2.15(2)	-0.58(2)	-243(8-II-3)	563(2)	215(2)
1	394	1.41(9-II-3)	-2.45(2)	-0.75(2)	-365(8-II-3)	314(2)	185(8-I-3)
1	395	-0.88(9-I-1)	-2.02(2)	-0.19(9-II-4)	162(2)	902(2)	100(2)
1	396	-0.95(9-I-2)	-2.11(2)	-0.31(9-II-1)	235(2)	856(2)	74(9-II-3)
1	397	-1.10(9-I-1)	-2.19(2)	-0.40(9-II-4)	301(2)	778(2)	110(9-II-3)
1	398	-0.96(9-I-1)	-2.11(2)	-0.31(9-II-4)	194(2)	817(2)	158(2)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
1	399	-1.08(9-I-4)	-2.20(2)	-0.65(9-II-3)	235(2)	592(2)	199(2)
1	400	-2.38(2)	-1.85(2)	-1.87(8-II-3)	398(2)	141(9-I-4)	130(2)
1	401	-1.42(9-I-4)	-2.06(2)	-1.26(8-II-3)	334(2)	305(2)	180(2)
1	402	-1.69(9-I-3)	-2.04(2)	-1.65(2)	295(9-I-3)	155(9-I-4)	178(2)
1	403	-1.28(9-I-1)	-2.20(2)	-0.67(9-II-3)	369(2)	624(2)	135(9-II-3)
1	404	-1.81(2)	-2.03(2)	-1.13(9-II-3)	428(2)	391(2)	134(9-II-3)
1	405	-2.74(2)	-1.71(2)	-1.75(8-II-3)	466(2)	165(9-I-1)	111(9-II-4)
1	406	-2.10(8-II-3)	-2.09(2)	-0.58(9-II-4)	434(8-II-3)	562(2)	-138(9-I-4)
1	407	-1.94(2)	-2.05(2)	-1.00(9-II-3)	453(2)	413(2)	117(9-II-4)
1	408	-2.04(8-II-3)	-2.05(2)	-0.75(9-II-3)	424(2)	500(2)	-116(9-I-4)
1	409	-1.53(9-I-2)	-2.17(2)	-0.67(9-II-3)	403(2)	604(2)	114(9-II-4)
1	410	-3.04(8-II-3)	-1.96(2)	0.72(9-I-3)	507(8-II-3)	251(8-II-3)	-143(9-I-4)
1	411	-2.75(8-II-3)	-1.82(2)	-1.06(9-II-3)	429(2)	241(8-II-3)	-113(9-I-4)
1	412	-2.78(2)	-1.73(2)	-1.44(9-II-3)	478(2)	198(9-I-2)	103(9-II-4)
1	413	-2.07(8-II-3)	-2.03(2)	-0.58(9-II-1)	470(8-II-3)	618(2)	-144(9-I-1)
1	414	-1.91(8-II-3)	-2.03(2)	-0.66(9-II-2)	445(8-II-3)	662(2)	177(8-I-3)
1	415	-2.34(8-II-3)	-2.16(2)	-0.69(9-II-2)	451(8-II-3)	346(2)	195(8-I-3)
1	416	-2.84(8-II-3)	-2.38(2)	-0.88(8-I-3)	-550(8-I-3)	-245(8-I-3)	198(8-I-3)
1	417	-3.37(8-II-3)	-2.23(2)	0.66(9-I-2)	-607(8-I-3)	-283(8-I-3)	-142(8-II-3)
1	418	-2.67(8-II-3)	-2.12(2)	-0.53(9-II-1)	522(8-II-3)	318(2)	-152(9-I-1)
1	419	-3.38(8-II-3)	-2.07(2)	0.60(9-I-4)	571(8-II-3)	233(8-II-3)	-150(9-I-1)
1	420	-1.02(9-I-2)	-1.90(2)	-0.54(9-II-1)	296(2)	841(2)	-87(9-I-1)
1	421	-1.05(8-II-3)	-1.76(2)	-0.60(9-II-1)	327(8-II-3)	799(2)	-117(9-I-1)
1	422	-0.90(9-I-2)	-1.81(2)	-0.53(9-II-1)	298(2)	829(2)	-94(9-I-1)
1	423	-0.55(9-I-2)	-1.80(2)	0.52(8-II-3)	174(2)	834(2)	-149(2)
1	424	-0.75(9-I-2)	-1.79(2)	0.47(9-I-2)	276(2)	874(2)	-127(2)
1	425	-0.67(9-I-2)	-1.65(2)	0.55(9-I-2)	235(2)	771(2)	-207(2)
1	426	-0.96(9-I-2)	-1.97(2)	-0.47(9-II-1)	265(2)	853(2)	-67(9-I-4)
1	427	-0.89(9-I-2)	-2.02(2)	-0.38(9-II-1)	232(2)	870(2)	-48(9-I-4)
1	428	-0.50(9-I-2)	-1.93(2)	0.44(8-II-3)	146(2)	902(2)	-82(2)
1	429	-0.83(9-I-2)	-1.91(2)	-0.43(9-II-1)	243(2)	877(2)	-64(9-I-4)
1	430	-0.70(9-I-2)	-1.88(2)	0.40(8-II-3)	206(2)	901(2)	-71(2)
1	431	-0.75(9-I-2)	-1.95(2)	-0.35(9-II-1)	209(2)	911(2)	-44(9-I-4)
1	432	-1.46(8-II-3)	-2.11(2)	-0.53(9-II-1)	341(8-II-3)	768(2)	-109(9-I-4)
1	433	-1.27(9-I-2)	-2.18(2)	-0.47(9-II-4)	343(2)	759(2)	93(9-II-4)
1	434	-1.14(9-I-2)	-2.05(2)	-0.50(9-II-1)	290(2)	834(2)	-81(9-I-4)
1	435	-1.05(9-I-2)	-2.10(2)	-0.42(9-II-1)	277(2)	836(2)	66(9-II-4)
1	436	-1.21(8-II-3)	-1.95(2)	-0.58(9-II-1)	332(8-II-3)	838(2)	-100(9-I-1)
1	437	-1.26(8-II-3)	-1.91(2)	-0.65(9-II-1)	386(8-II-3)	822(2)	-118(9-I-2)
1	438	-1.53(8-II-3)	-1.96(2)	-0.67(9-II-1)	425(8-II-3)	800(2)	145(8-I-3)
1	439	-1.53(8-II-3)	-2.01(2)	-0.60(9-II-1)	400(8-II-3)	796(2)	-122(9-I-1)
1	1	-0.21(8-II-1)	-0.34(9-I-2)	0.97(9-I-2)	-561(8-I-2)	-20(9-I-2)	12(8-I-4)
1	2	1.50(8-I-2)	-2.35(2)	-0.44(8-II-1)	320(9-II-1)	34(9-II-1)	7(9-II-1)
1	3	0.90(8-I-2)	-3.91(2)	0.44(8-I-1)	188(8-I-4)	28(9-II-1)	11(9-II-1)
1	4	-1.43(9-I-2)	-0.68(2)	-0.37(8-II-1)	205(9-II-1)	18(9-II-1)	-1(9-I-1)
1	5	0.94(9-II-2)	-0.74(2)	-0.51(8-II-1)	130(9-II-1)	18(9-II-1)	-2(9-I-1)
1	6	-1.69(9-I-1)	-0.50(8-I-1)	0.29(8-I-1)	65(9-II-1)	9(9-II-1)	-4(9-II-1)
1	7	-1.62(9-I-2)	-0.51(8-II-1)	-0.30(8-II-1)	130(9-II-1)	10(9-II-1)	-3(9-II-1)
1	8	0.89(9-II-1)	-0.13(8-I-1)	-0.44(8-II-1)	87(9-II-1)	11(9-II-1)	-2(8-I-1)
1	9	-1.72(9-I-1)	-0.90(2)	0.37(8-I-1)	21(9-I-4)	-3(8-I-2)	-4(9-II-1)
1	10	0.82(9-II-1)	-0.19(8-II-1)	0.42(8-I-1)	48(8-I-1)	-2(8-I-2)	-5(9-II-1)
1	11	1.81(9-II-1)	-3.01(2)	0.47(8-I-1)	-109(9-II-1)	-10(9-II-1)	-2(8-I-1)
1	12	0.76(9-II-1)	-1.00(2)	0.52(8-I-1)	12(9-I-2)	-5(9-II-1)	-4(9-II-1)
1	13	0.58(8-I-2)	-1.36(2)	0.55(9-I-2)	127(8-I-4)	-21(9-I-2)	14(9-II-1)
1	14	-0.20(8-II-2)	-1.35(9-II-2)	1.08(9-I-2)	-201(8-I-2)	17(9-II-2)	16(9-II-1)
1	15	0.72(9-II-2)	-1.89(9-II-2)	1.39(9-I-2)	95(8-II-2)	13(9-II-2)	12(9-II-1)
1	16	0.43(8-I-2)	-1.20(2)	-0.52(8-II-1)	118(9-II-1)	-18(8-I-2)	5(9-II-1)
1	17	-0.92(9-I-2)	-2.98(2)	-0.47(8-II-1)	73(8-II-2)	-27(8-I-2)	7(9-II-1)
1	18	-0.65(9-II-2)	-3.33(9-II-2)	1.15(9-I-2)	-84(8-I-2)	-10(8-I-2)	9(9-II-1)
1	19	0.94(9-I-2)	-1.89(9-II-2)	-0.47(8-II-1)	63(8-II-2)	-29(9-II-1)	5(9-II-1)
1	20	-0.82(9-I-2)	-1.52(2)	0.58(9-I-1)	40(8-II-2)	-20(9-II-1)	4(9-II-1)
1	21	-0.32(9-I-2)	-1.74(2)	-0.49(8-II-1)	24(8-II-2)	-39(9-II-1)	2(9-II-1)
1	22	-0.46(8-II-2)	-0.66(2)	-0.45(8-II-1)	97(9-II-1)	-15(8-I-2)	0
1	23	0.32(9-II-2)	-0.42(2)	-0.50(8-II-1)	46(8-II-1)	-21(8-I-2)	-2(9-I-1)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
1	24	-0.36(9-II-2)	-1.00(2)	-0.50(8-II-1)	46(8-II-1)	-36(9-II-1)	-1(9-I-1)
1	25	-0.57(9-I-1)	-0.70(2)	0.44(8-I-1)	37(8-I-1)	-13(9-II-1)	-2(9-II-1)
1	26	0.28(8-I-2)	-0.08(9-I-2)	-0.43(8-II-1)	36(8-I-1)	-16(9-II-1)	-1(9-II-2)
1	27	0.47(9-II-1)	-1.62(2)	0.52(8-I-1)	12(9-I-2)	-9(9-II-1)	-2(9-II-1)
1	28	0.26(2)	-0.52(2)	0.49(8-I-1)	19(8-I-1)	-11(9-II-1)	-2(9-II-1)
1	29	-0.51(2)	-3.69(2)	0.44(8-I-1)	7(8-I-2)	-6(9-II-3)	-1(8-I-1)
1	30	-0.29(2)	-0.74(2)	-0.44(8-II-1)	36(8-I-1)	-34(9-II-1)	0
1	31	0.15(2)	-0.38(2)	-0.47(8-II-1)	21(8-I-1)	-38(9-II-1)	0
1	32	-1.27(9-I-1)	-0.77(2)	-0.38(8-II-1)	-32(9-II-1)	-9(9-II-1)	-3(9-I-1)
1	33	1.26(9-II-2)	-1.44(2)	-0.49(8-II-1)	-119(9-II-1)	-9(9-II-1)	-3(9-I-1)
1	34	-1.05(9-I-1)	-4.89(2)	-0.46(8-II-1)	-20(9-II-1)	-7(9-II-1)	-2(8-I-1)
1	35	0.90(2)	-2.02(2)	-0.49(8-II-1)	-18(9-II-1)	-10(9-II-2)	-1(8-I-1)
1	36	-1.34(9-I-1)	-0.51(8-I-1)	0.32(8-I-1)	-116(9-I-1)	-3(9-I-1)	4(9-II-1)
1	37	-1.30(9-I-1)	-0.51(8-II-1)	-0.30(8-II-1)	-53(9-I-1)	-4(9-I-1)	4(9-II-1)
1	38	0.79(9-II-1)	-0.11(2)	-0.44(8-II-1)	-23(9-I-1)	-3(9-II-1)	-5(9-I-1)
1	39	-1.42(9-I-1)	-0.82(2)	0.39(8-I-1)	-186(9-I-1)	-9(9-I-1)	0
1	40	0.77(9-II-1)	-0.19(8-II-1)	0.45(8-I-1)	-70(9-I-1)	-5(9-I-1)	2(9-II-4)
1	41	1.48(9-II-1)	-2.33(2)	0.49(8-I-1)	-267(9-I-1)	-15(9-I-1)	5(9-I-1)
1	42	0.62(9-II-1)	-0.82(2)	0.56(8-I-1)	-100(9-I-1)	-8(9-I-1)	2(8-II-1)
1	43	-1.19(8-I-1)	-0.74(8-I-1)	-0.37(8-II-1)	-154(8-II-1)	-14(9-I-1)	-13(9-II-1)
1	44	1.32(8-II-1)	-1.42(2)	-0.47(8-II-1)	-230(9-I-1)	-14(9-I-1)	-13(9-II-1)
1	45	-0.90(9-I-1)	-4.36(2)	-0.45(8-II-1)	-83(9-I-1)	-10(9-I-1)	8(9-I-1)
1	46	-0.82(8-I-1)	-0.83(9-II-1)	-0.35(8-II-1)	-372(8-II-1)	-22(8-II-1)	-13(9-II-1)
1	47	1.12(9-II-1)	-0.26(2)	-0.46(8-II-1)	-106(8-II-1)	-14(8-II-1)	-15(9-II-1)
1	48	-0.22(8-II-1)	-0.64(9-II-1)	0.60(9-II-1)	633(8-I-1)	11(8-I-1)	-12(8-I-1)
1	49	0.76(9-II-1)	-0.66(9-II-1)	-0.64(9-I-4)	174(8-I-1)	-15(8-II-1)	-14(9-II-1)
1	50	-0.68(9-I-1)	-0.86(2)	-0.47(8-II-1)	-23(9-I-1)	-13(9-II-1)	-2(9-I-1)
1	51	0.22(8-I-2)	-1.22(2)	-0.50(8-II-1)	-7(9-I-4)	-9(9-II-2)	-1(9-I-4)
1	52	-0.46(9-I-1)	-0.72(2)	0.45(8-I-1)	-77(9-I-1)	-21(9-II-1)	0
1	53	0.28(2)	-0.06(8-II-1)	-0.45(8-II-1)	-29(9-I-1)	-20(9-II-1)	-1(9-I-4)
1	54	0.13(8-I-2)	-1.40(2)	-0.49(8-II-1)	-7(9-I-4)	27(9-I-1)	0
1	55	-0.32(2)	-0.78(2)	-0.45(8-II-1)	-31(9-I-1)	34(9-I-1)	0
1	56	0.19(9-I-2)	-0.71(2)	-0.47(8-II-1)	-12(9-I-1)	31(9-I-1)	0
1	57	0.20(9-I-1)	-0.55(2)	0.44(8-I-1)	-16(9-I-1)	44(9-I-1)	-1(9-II-2)
1	58	0.20(9-I-1)	-0.56(2)	0.48(8-I-1)	-17(9-I-1)	44(9-I-1)	-1(9-II-2)
1	59	-0.29(8-I-1)	-1.40(2)	0.54(8-I-1)	-100(9-I-1)	-27(9-II-1)	2(9-I-2)
1	60	0.20(2)	-0.44(2)	0.51(8-I-1)	-46(9-I-1)	-30(9-II-1)	-1(9-II-2)
1	61	-0.18(2)	-1.05(2)	0.50(8-I-1)	-45(9-I-1)	43(9-I-1)	-2(9-II-2)
1	62	0.79(2)	-1.90(2)	-0.46(8-II-1)	-90(9-I-1)	-24(9-II-1)	7(9-I-1)
1	63	-0.37(2)	-2.95(2)	0.48(8-I-1)	-45(9-I-1)	-34(9-II-1)	-4(9-II-1)
1	64	-0.65(9-II-1)	-1.60(9-II-1)	-0.47(8-II-1)	-128(8-II-1)	-13(9-II-1)	-9(9-II-1)
1	65	-0.25(9-I-1)	-1.40(2)	-0.47(8-II-1)	-51(8-II-1)	-22(9-II-1)	8(9-I-1)
1	66	-0.51(9-II-1)	-2.76(9-II-1)	-0.76(9-I-1)	180(8-I-1)	4(9-I-1)	-9(9-II-1)
1	67	0.94(9-II-1)	-0.78(9-II-1)	-0.58(9-I-4)	-89(8-II-1)	-15(9-II-1)	10(9-I-1)
1	68	0.54(2)	-1.69(2)	0.48(8-I-1)	-46(9-I-1)	-42(9-II-1)	4(9-I-1)
1	69	0.09(9-I-1)	-1.55(2)	0.50(8-I-1)	-16(9-I-1)	47(9-I-1)	-3(9-II-2)
1	70	0.45(9-I-1)	-1.38(2)	-0.46(8-II-1)	-52(8-II-1)	-35(9-II-1)	6(9-I-1)
1	71	-0.12(2)	-2.16(2)	0.44(8-I-1)	-20(8-II-1)	42(9-I-1)	5(9-I-1)
1	72	-0.70(9-I-2)	-4.45(9-II-2)	1.25(9-I-2)	-53(8-I-2)	6(9-I-2)	10(9-II-1)
1	73	0.76(9-I-2)	-7.17(9-II-2)	1.26(9-I-2)	-51(8-I-2)	8(9-I-2)	9(9-II-1)
1	74	1.49(9-I-2)	-3.33(9-II-2)	0.52(9-I-1)	39(8-II-2)	-27(9-II-1)	3(9-II-1)
1	75	-1.11(9-I-2)	-3.28(9-II-2)	0.81(9-I-2)	-16(8-I-2)	41(9-I-2)	5(9-II-1)
1	76	0.79(9-I-2)	-1.29(2)	-0.48(8-II-1)	24(8-II-2)	-45(9-II-1)	2(9-II-1)
1	77	-0.13(9-II-2)	-1.69(2)	-0.47(8-II-1)	15(8-II-2)	-38(9-II-1)	2(8-I-1)
1	78	-0.20(2)	-1.15(2)	0.49(8-I-1)	18(8-I-1)	28(9-I-1)	-2(9-II-2)
1	79	0.22(9-I-2)	-0.40(2)	0.45(8-I-1)	17(8-I-1)	-32(9-II-1)	-1(9-II-2)
1	80	-0.15(9-II-2)	-2.34(2)	-0.46(8-II-1)	9(9-II-1)	24(9-I-2)	0
1	81	0.71(2)	-1.96(2)	0.44(8-I-1)	7(8-I-2)	25(9-I-1)	-1(8-I-3)
1	82	-0.16(9-II-2)	-2.02(2)	0.48(8-I-1)	11(8-I-1)	25(9-I-1)	-1(9-II-2)
1	83	-0.47(9-II-2)	-0.92(2)	-0.47(8-II-1)	20(8-I-1)	-50(9-II-1)	0
1	84	0.28(9-I-2)	-1.03(2)	-0.47(8-II-1)	15(9-I-2)	-50(9-II-1)	1(8-I-1)
1	85	-0.37(9-II-2)	-0.94(2)	0.45(8-I-1)	17(8-I-1)	50(9-I-1)	0
1	86	0.38(9-I-2)	-0.49(2)	-0.44(8-II-1)	12(9-I-2)	-51(9-II-1)	0
1	87	0.37(9-I-2)	-1.59(2)	0.46(8-I-1)	11(8-I-1)	49(9-I-1)	-1(8-I-3)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
1	88	0.34(9-I-2)	-1.19(2)	0.45(8-I-1)	8(8-I-1)	49(9-I-1)	0
1	89	1.70(9-I-2)	-5.05(9-II-2)	0.72(9-I-2)	-15(8-I-2)	33(9-I-2)	4(9-II-1)
1	90	-0.51(9-I-2)	-8.92(9-II-2)	0.81(9-I-2)	-15(9-I-2)	21(9-I-2)	3(9-II-1)
1	91	0.79(9-I-2)	-1.60(9-II-2)	-0.46(8-II-1)	15(8-II-2)	65(9-I-2)	2(9-I-2)
1	92	0.09(9-I-2)	-2.13(9-II-2)	-0.45(8-II-1)	14(9-I-2)	59(9-I-2)	2(9-I-2)
1	93	0.56(9-I-2)	-1.11(2)	-0.46(8-II-1)	15(9-I-2)	66(9-I-1)	1(9-I-2)
1	94	0.30(9-I-2)	-1.36(2)	-0.45(8-II-1)	14(9-I-2)	64(9-I-1)	1(9-I-2)
1	95	1.23(9-I-2)	-5.98(9-II-2)	0.62(9-I-2)	-15(9-I-2)	112(9-I-2)	2(9-II-1)
1	96	-0.10(9-I-2)	13.83(9-I-2)	-0.32(8-I-1)	0	85(9-I-2)	1(9-I-2)
1	97	0.95(9-I-2)	-2.19(9-II-2)	-0.45(8-II-1)	15(9-I-2)	103(9-I-2)	3(9-I-2)
1	98	0.10(9-I-2)	-4.12(9-II-2)	-0.31(8-II-1)	0	117(9-I-2)	2(9-I-2)
1	99	0.64(9-I-2)	-1.27(2)	-0.45(8-II-1)	14(9-I-2)	93(9-I-2)	2(9-I-2)
1	100	0.05(9-I-2)	-1.50(9-II-2)	-0.30(8-II-1)	0	96(9-I-2)	1(9-I-2)
1	101	-0.48(9-II-2)	-0.89(2)	-0.44(8-II-1)	12(9-I-2)	68(9-I-1)	0
1	102	0.36(9-I-2)	-0.83(2)	-0.44(8-II-1)	10(9-I-2)	68(9-I-1)	1(9-I-2)
1	103	0.38(9-I-2)	-1.19(2)	0.44(8-I-1)	7(9-I-2)	69(9-I-1)	0
1	104	0.33(9-I-2)	-0.84(2)	-0.42(8-II-1)	6(9-I-2)	68(9-I-1)	0
1	105	0.30(9-I-2)	-1.58(2)	0.43(8-I-1)	2(9-I-2)	72(9-I-1)	0
1	106	0.22(9-I-2)	-1.69(2)	0.42(8-I-1)	2(8-I-1)	72(9-I-1)	0
1	107	-0.43(9-II-2)	-0.99(2)	-0.44(8-II-1)	10(9-I-2)	89(9-I-2)	1(9-I-2)
1	108	0.05(8-I-1)	-1.12(2)	-0.30(8-II-1)	0	91(9-I-2)	0
1	109	-0.33(9-II-2)	-0.96(2)	-0.42(8-II-1)	6(9-I-2)	87(9-I-1)	0
1	110	0.07(9-II-2)	-0.87(2)	-0.29(8-II-1)	0	87(9-I-1)	0
1	111	0.25(9-I-2)	-1.30(2)	0.41(8-I-1)	3(9-I-2)	87(9-I-1)	0
1	112	0.09(9-II-2)	-1.11(2)	-0.28(8-II-1)	0	87(9-I-1)	0
1	113	0.29(9-I-2)	-1.76(2)	0.41(8-I-1)	2(8-I-1)	87(9-I-1)	0
1	114	0.07(9-II-2)	-1.66(2)	-0.27(8-II-1)	0	88(9-I-1)	0
1	115	0.38(9-I-2)	-1.71(2)	-0.45(8-II-1)	9(9-II-1)	47(9-I-1)	0
1	116	-0.25(9-II-2)	-2.17(2)	0.43(8-I-1)	6(8-I-1)	47(9-I-1)	0
1	117	0.47(9-I-2)	-1.77(2)	-0.42(8-II-1)	7(8-I-1)	68(9-I-1)	0
1	118	-0.25(9-II-2)	-1.18(2)	-0.47(8-II-1)	-12(9-I-1)	49(9-I-1)	0
1	119	0.26(9-I-1)	-1.55(2)	-0.46(8-II-1)	7(9-II-1)	48(9-I-1)	0
1	120	-0.26(9-II-1)	-0.85(2)	-0.43(8-II-1)	-15(9-I-1)	53(9-I-1)	0
1	121	0.30(9-I-1)	-0.75(2)	-0.44(8-II-1)	6(9-II-1)	52(9-I-1)	-1(9-II-2)
1	122	-0.27(9-II-1)	-1.01(2)	0.48(8-I-1)	-15(9-I-1)	56(9-I-1)	-2(9-II-2)
1	123	0.34(9-I-1)	-0.56(2)	0.45(8-I-1)	-4(8-II-1)	56(9-I-1)	-2(9-II-2)
1	124	0.28(9-II-1)	-3.45(9-II-1)	-0.65(9-I-1)	-43(8-II-1)	8(9-I-1)	8(9-I-1)
1	125	-0.91(9-II-1)	-2.52(9-II-1)	-0.56(9-I-4)	-90(8-II-1)	-12(9-II-1)	8(9-I-1)
1	126	0.35(9-II-1)	-0.76(2)	-0.45(8-II-1)	-30(8-II-1)	-28(9-II-1)	6(9-I-1)
1	127	0.33(9-I-1)	-1.43(2)	0.49(8-I-1)	-17(9-I-1)	53(9-I-1)	-3(9-II-2)
1	128	0.28(9-I-1)	-1.18(2)	0.47(8-I-1)	-6(8-II-1)	56(9-I-1)	-2(9-II-2)
1	129	0.51(9-I-1)	-1.56(2)	0.44(8-I-1)	-20(8-II-1)	46(9-I-1)	4(9-I-1)
1	130	-0.19(9-II-1)	-1.84(2)	0.46(8-I-1)	-10(8-II-1)	52(9-I-1)	-3(9-II-2)
1	131	0.66(9-I-1)	-1.57(9-II-1)	-0.43(8-II-1)	-30(8-II-1)	35(9-I-1)	5(9-I-1)
1	132	0.05(9-I-1)	-1.49(2)	0.43(8-I-1)	-12(8-II-1)	41(9-I-1)	3(9-I-1)
1	133	0.60(9-I-1)	-3.09(9-II-1)	-0.55(9-I-4)	-42(8-II-1)	17(9-I-1)	7(9-I-1)
1	134	0.40(9-II-1)	-1.91(9-II-1)	0.42(8-I-1)	-14(8-I-1)	27(9-I-1)	4(9-I-1)
1	135	-0.23(9-I-1)	-4.88(9-II-1)	0.54(9-II-4)	-16(8-II-1)	7(9-I-1)	6(9-I-1)
1	136	0.37(9-I-1)	-1.48(2)	-0.44(8-II-1)	7(9-II-1)	67(9-I-1)	0
1	137	0.21(9-I-1)	-1.86(2)	-0.43(8-II-1)	2(8-I-1)	67(9-I-1)	0
1	138	-0.34(9-II-1)	-1.03(2)	-0.44(8-II-1)	6(9-II-1)	67(9-I-1)	-1(9-II-2)
1	139	0.23(9-I-1)	-1.20(2)	-0.43(8-II-1)	2(9-II-1)	67(9-I-1)	0
1	140	-0.36(9-II-1)	-0.90(2)	0.44(8-I-1)	-4(8-II-1)	67(9-I-1)	-1(9-II-2)
1	141	0.26(9-I-1)	-0.74(2)	0.42(8-I-1)	1(8-I-1)	67(9-I-1)	-1(9-II-2)
1	142	0.38(9-I-1)	-1.24(2)	0.46(8-I-1)	-6(8-II-1)	64(9-I-1)	-2(9-II-2)
1	143	0.28(9-I-1)	-0.94(2)	0.44(8-I-1)	3(8-I-1)	66(9-I-1)	-1(9-II-2)
1	144	0.30(9-I-2)	-1.68(2)	-0.42(8-II-1)	2(9-II-1)	86(9-I-1)	0
1	145	0.09(9-II-2)	-1.83(2)	-0.27(8-II-1)	0	87(9-I-1)	0
1	146	0.25(9-I-1)	-1.26(2)	-0.42(8-II-1)	2(9-II-1)	83(9-I-1)	0
1	147	0.10(9-II-1)	-1.52(2)	-0.28(8-II-1)	0	85(9-I-1)	0
1	148	-0.25(9-II-1)	-0.92(2)	0.41(8-I-1)	1(8-I-1)	80(9-I-1)	0
1	149	0.09(9-II-1)	-1.01(2)	-0.27(8-II-1)	0	82(9-I-1)	0
1	150	0.26(9-I-1)	-1.06(2)	0.43(8-I-1)	3(8-I-1)	76(9-I-1)	0
1	151	0.08(9-II-2)	-0.87(2)	0.28(8-I-1)	0	78(9-I-1)	0

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
1	152	0.51(9-I-1)	-1.55(2)	0.45(8-I-1)	-9(8-II-1)	59(9-I-1)	-2(9-II-2)
1	153	0.28(9-I-1)	-1.52(2)	0.44(8-I-1)	5(9-I-1)	63(9-I-1)	-1(9-II-2)
1	154	0.63(9-I-1)	-1.39(2)	0.43(8-I-1)	-12(8-II-1)	51(9-I-1)	-2(9-II-1)
1	155	0.28(9-I-1)	-1.65(2)	0.43(8-I-1)	7(9-I-1)	56(9-I-1)	-1(9-II-2)
1	156	0.39(9-I-1)	-2.93(9-II-1)	0.44(8-I-1)	-8(8-I-1)	34(9-I-1)	5(9-I-1)
1	157	0.79(9-I-1)	-2.82(9-II-1)	0.42(8-I-1)	-13(8-II-1)	28(9-I-1)	3(9-I-1)
1	158	0.16(9-I-1)	-1.46(9-II-1)	0.42(8-I-1)	12(9-I-1)	43(9-I-1)	0
1	159	0.12(9-II-1)	-5.58(9-II-1)	0.43(8-I-1)	-8(9-I-1)	13(9-I-1)	3(9-I-1)
1	160	0.35(9-I-1)	-1.45(2)	0.43(8-I-1)	4(9-I-1)	72(9-I-1)	0
1	161	0.07(9-II-2)	-1.26(2)	0.28(8-I-1)	0	74(9-I-1)	0
1	162	0.43(9-I-1)	-1.55(2)	0.42(8-I-1)	7(9-I-1)	67(9-I-1)	0
1	163	0.04(8-II-1)	-1.60(2)	0.28(8-I-1)	0	70(9-I-1)	0
1	164	0.50(9-I-1)	-1.63(9-II-1)	0.42(8-I-1)	-7(9-II-1)	64(9-I-1)	0
1	165	0.10(9-I-1)	-1.44(2)	0.29(8-I-1)	0	65(9-I-1)	0
1	166	0.54(9-I-1)	-3.55(9-II-1)	0.42(8-I-1)	-5(8-I-1)	61(9-I-1)	-1(9-II-1)
1	167	0.21(9-I-1)	-2.56(9-II-1)	0.30(8-I-1)	0	63(9-I-1)	0
1	168	0.24(9-I-1)	7.91(9-I-1)	0.29(8-I-1)	0	44(9-I-1)	0
2	1	-1.38(9-I-3)	1.56(9-II-1)	0.99(9-II-3)	393(9-I-4)	-179(9-II-1)	379(2)
2	2	-1.10(9-I-3)	-1.09(9-I-1)	1.04(9-II-4)	288(9-I-4)	150(9-I-1)	359(2)
2	3	-0.97(9-I-3)	-1.09(8-II-4)	0.96(9-II-4)	-207(9-II-3)	209(2)	307(2)
2	4	-0.92(9-I-3)	-1.65(2)	0.82(9-II-4)	-231(9-II-3)	257(2)	242(2)
2	5	-0.89(8-I-2)	-2.02(2)	0.67(9-II-4)	-276(2)	279(2)	173(2)
2	6	-0.89(8-I-2)	-2.24(2)	-0.54(9-I-1)	-354(2)	282(2)	104(2)
2	7	-0.90(8-I-2)	-2.31(2)	-0.58(9-I-1)	-407(2)	268(2)	37(2)
2	8	-0.92(8-I-2)	-2.25(2)	-0.64(9-I-1)	-438(2)	238(2)	-28(2)
2	9	-0.93(8-I-2)	-2.03(2)	-0.75(8-II-1)	-439(2)	198(2)	-89(2)
2	10	-0.97(8-I-1)	-1.64(2)	-0.92(8-II-1)	-395(2)	148(2)	-144(2)
2	11	-0.99(8-I-1)	-1.03(2)	-1.07(8-II-1)	-343(8-II-1)	118(9-II-1)	-194(2)
2	12	-1.04(8-I-1)	-0.97(9-II-1)	-1.10(8-II-1)	-335(8-II-1)	-148(9-I-1)	-236(2)
2	13	-1.19(8-I-1)	1.35(8-II-1)	-0.92(8-II-1)	-295(8-II-1)	-266(8-II-1)	-267(2)
2	14	-1.80(8-I-1)	2.06(8-II-1)	1.03(8-I-1)	279(8-I-1)	-442(2)	-206(2)
2	15	-1.12(8-I-1)	-0.82(8-I-1)	1.20(8-I-1)	-188(8-II-1)	-719(2)	-273(2)
2	16	-0.56(8-I-1)	-0.75(8-I-1)	1.23(8-I-1)	-214(2)	-944(2)	-304(2)
2	17	0.81(2)	-0.78(8-I-1)	1.08(8-I-1)	-304(2)	-1126(2)	-311(2)
2	18	1.04(2)	-0.83(2)	0.88(8-I-1)	-365(2)	-1263(2)	-308(2)
2	19	1.28(2)	-0.88(2)	0.61(8-I-1)	-404(2)	-1370(2)	-323(2)
2	20	1.45(2)	-0.78(2)	0.32(8-I-1)	-473(2)	-1523(2)	-321(2)
2	21	1.56(2)	-0.64(8-I-1)	-0.50(2)	-534(2)	-1669(2)	-325(2)
2	22	1.59(8-I-1)	-0.40(8-I-1)	-1.00(2)	-563(2)	-1782(2)	-316(2)
2	23	1.26(8-I-1)	0.13(2)	-1.30(2)	-460(2)	-1800(2)	-298(2)
2	24	-0.97(8-II-1)	0.29(8-I-2)	-1.38(8-I-2)	-197(8-I-1)	-1620(2)	-296(2)
2	25	-1.27(2)	-0.36(8-II-2)	-1.02(8-I-2)	34(9-I-1)	-1389(2)	-295(2)
2	26	-1.59(8-I-2)	-0.63(8-II-2)	0.87(8-II-2)	-74(8-II-2)	-1345(2)	-350(2)
2	27	-1.91(8-I-2)	-0.76(8-II-2)	0.71(8-II-2)	-258(8-II-2)	-1494(2)	-388(2)
2	28	2.26(8-II-2)	-0.72(8-II-2)	0.41(2)	-410(2)	-1676(2)	-355(2)
2	29	2.18(8-II-2)	-0.57(8-II-2)	0.52(8-I-2)	-481(2)	-1790(2)	-317(2)
2	30	1.77(8-II-2)	-0.43(9-II-2)	-0.86(8-II-2)	-457(2)	-1785(2)	-306(2)
2	31	1.31(8-II-2)	-0.40(9-II-2)	-1.05(8-II-2)	-387(2)	-1689(2)	-292(2)
2	32	0.86(8-II-2)	-0.37(9-II-2)	-1.11(8-II-2)	-316(2)	-1566(2)	-269(2)
2	33	-0.57(8-I-2)	0.50(9-I-2)	-1.13(8-II-2)	-251(2)	-1442(2)	-246(2)
2	34	-0.28(8-I-2)	0.78(9-I-2)	-1.12(8-II-2)	-190(2)	-1303(2)	-216(2)
2	35	-0.24(9-II-2)	1.25(9-I-2)	1.10(8-I-2)	-128(2)	-1133(2)	-175(2)
2	36	-0.47(8-II-2)	2.10(9-I-2)	1.28(8-I-2)	-87(8-I-1)	-915(2)	-130(8-I-4)
2	37	-0.83(8-II-2)	3.68(9-I-2)	1.73(8-I-2)	-155(9-I-2)	-694(2)	-100(8-I-1)
2	38	0.54(8-I-1)	3.19(9-I-2)	2.26(9-I-2)	-275(9-I-2)	-689(9-I-2)	69(8-II-2)
2	39	0.62(8-I-2)	1.98(9-I-2)	2.69(9-I-2)	-453(9-I-2)	-528(9-I-2)	135(2)
2	40	0.65(9-I-2)	-1.35(9-II-2)	2.49(9-I-2)	-397(9-I-2)	-331(9-I-2)	213(2)
2	41	0.63(9-I-2)	-1.75(2)	2.02(9-I-2)	-351(9-I-2)	-191(9-I-2)	250(2)
2	42	-0.53(9-II-2)	-2.21(2)	1.56(9-I-2)	-319(9-I-2)	-107(8-II-3)	263(2)
2	43	-0.57(9-II-2)	-2.38(2)	1.17(9-I-2)	-302(9-I-2)	110(8-I-4)	260(2)
2	44	-0.54(9-II-2)	-2.35(2)	0.90(9-I-2)	-337(2)	105(8-I-2)	250(2)
2	45	-0.44(9-II-2)	-2.29(2)	0.87(9-I-2)	-393(2)	104(8-I-1)	231(2)
2	46	-0.51(9-II-2)	-2.43(2)	0.98(9-I-2)	-401(2)	154(8-I-3)	216(2)
2	47	-0.64(9-II-2)	-2.78(2)	-1.05(9-II-2)	-373(2)	179(8-I-4)	192(2)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
2	48	-0.81(9-II-2)	-3.02(2)	-1.15(9-II-2)	-296(2)	269(2)	170(2)
2	49	-0.95(9-II-2)	-2.93(2)	-1.22(9-II-2)	-243(2)	350(2)	137(2)
2	50	-1.14(9-II-2)	-2.59(2)	-1.23(9-II-2)	-207(2)	399(2)	96(9-II-2)
2	51	-1.28(9-II-2)	-2.05(2)	-1.34(2)	-185(2)	414(2)	84(9-II-2)
2	52	-1.32(9-II-2)	-1.78(9-I-2)	-1.47(2)	-201(2)	389(2)	73(9-II-2)
2	53	-1.33(8-I-3)	-1.47(9-I-2)	-1.54(2)	-206(2)	363(2)	-53(8-II-3)
2	54	-1.38(8-I-3)	-1.21(9-I-2)	-1.55(2)	-193(2)	363(2)	-85(2)
2	55	-1.53(8-I-3)	-1.13(9-I-2)	-1.57(2)	-141(2)	375(2)	-135(2)
2	56	-1.75(8-I-3)	1.41(9-II-2)	-1.54(2)	-94(9-II-3)	373(2)	-203(2)
2	57	-1.90(8-I-3)	2.10(9-II-2)	-1.45(2)	92(9-I-2)	323(2)	-284(2)
2	58	-2.03(8-I-3)	2.92(9-II-2)	-1.19(2)	169(9-I-2)	300(9-I-2)	-362(2)
2	59	-1.96(8-I-3)	3.72(9-II-2)	-0.82(9-I-3)	256(9-I-2)	340(9-I-2)	-428(2)
2	60	-1.53(8-I-3)	4.24(2)	-0.76(9-I-3)	278(9-I-2)	-506(9-II-2)	-452(2)
2	61	-1.09(9-I-3)	5.35(2)	1.39(9-II-2)	370(9-I-2)	-559(9-II-2)	-423(2)
2	62	-1.27(2)	6.17(2)	1.50(2)	201(9-I-2)	-785(2)	-238(2)
2	63	-0.50(2)	4.17(2)	1.07(2)	-38(9-II-2)	-1172(2)	-234(9-II-2)
2	64	-0.66(8-I-3)	2.94(2)	0.97(2)	-74(2)	-1395(2)	-202(9-II-2)
2	65	0.83(8-II-3)	1.83(9-II-2)	1.05(2)	-244(2)	-1856(2)	-137(9-II-2)
2	66	1.11(8-II-3)	1.32(9-II-2)	1.01(2)	-341(2)	-2197(2)	-99(9-II-2)
2	67	1.27(8-II-3)	0.95(9-II-2)	0.98(2)	-401(2)	-2425(2)	-74(9-II-2)
2	68	1.32(8-II-3)	-0.74(9-I-2)	0.96(2)	-443(2)	-2539(2)	-65(2)
2	69	1.34(8-II-3)	-0.76(9-I-2)	0.88(2)	-475(2)	-2691(2)	-89(2)
2	70	1.46(2)	-0.75(9-I-2)	0.78(2)	-549(2)	-2974(2)	-62(2)
2	71	1.49(2)	-0.73(9-I-2)	0.65(2)	-572(2)	-3161(2)	-44(2)
2	72	1.43(2)	-0.82(2)	0.54(2)	-574(2)	-3279(2)	-32(2)
2	73	1.38(2)	-0.88(2)	0.52(8-I-2)	-579(2)	-3367(2)	-28(2)
2	74	1.40(2)	-0.91(2)	0.50(8-I-2)	-595(2)	-3433(2)	-23(2)
2	75	1.39(2)	-0.91(2)	0.45(8-I-2)	-604(2)	-3474(2)	-18(9-II-3)
2	76	1.28(2)	-0.88(2)	0.40(8-I-2)	-590(2)	-3484(2)	-14(9-II-3)
2	77	1.10(2)	-0.84(2)	-0.41(8-II-2)	-560(2)	-3472(2)	14(9-I-3)
2	78	0.99(2)	-0.81(2)	-0.41(8-II-2)	-539(2)	-3450(2)	14(9-I-3)
2	79	0.98(2)	-0.80(2)	-0.39(8-II-2)	-538(2)	-3421(2)	16(9-I-3)
2	80	1.01(2)	-0.79(2)	-0.39(8-II-2)	-544(2)	-3390(2)	19(9-I-3)
2	81	1.03(2)	-0.78(2)	-0.40(8-II-2)	-542(2)	-3361(2)	20(2)
2	82	1.02(2)	-0.77(2)	-0.40(8-II-2)	-532(2)	-3330(2)	24(2)
2	83	1.07(2)	-0.78(2)	-0.38(8-II-2)	-533(2)	-3292(2)	25(2)
2	84	1.21(2)	-0.79(2)	-0.38(8-II-1)	-547(2)	-3240(2)	28(2)
2	85	1.36(2)	-0.80(2)	-0.43(9-I-1)	-561(2)	-3161(2)	34(2)
2	86	1.45(2)	-0.81(2)	-0.55(2)	-561(2)	-3058(2)	42(2)
2	87	1.49(2)	-0.81(2)	-0.74(2)	-549(2)	-2940(2)	46(2)
2	88	1.50(2)	-0.80(2)	-0.93(2)	-534(2)	-2789(2)	51(2)
2	89	1.48(2)	-0.77(2)	-1.16(2)	-502(2)	-2558(2)	63(2)
2	90	1.29(2)	-0.62(2)	-1.44(2)	-464(2)	-2287(2)	82(2)
2	91	0.89(2)	-0.59(9-I-1)	-1.69(2)	-388(2)	-2022(2)	94(2)
2	92	-0.87(9-I-4)	-0.60(9-I-1)	-1.83(2)	-259(2)	-1711(2)	100(2)
2	93	-1.59(9-I-4)	0.93(9-II-1)	-1.73(2)	152(9-I-4)	-1357(2)	102(2)
2	94	-2.34(9-I-3)	1.57(9-II-1)	-1.44(9-I-3)	291(9-I-3)	-992(2)	102(2)
2	95	-3.28(9-I-3)	2.93(2)	-0.98(9-I-3)	459(9-I-3)	-565(2)	151(2)
2	96	-1.95(9-I-3)	2.27(9-II-4)	-0.86(9-I-3)	475(9-I-4)	-333(9-II-4)	345(2)
2	97	0.52(2)	-0.57(2)	0.50(8-I-1)	-172(2)	-294(2)	-222(2)
2	98	-0.42(8-I-1)	-0.47(2)	0.42(8-I-1)	-72(2)	121(9-II-1)	-244(2)
2	99	0.42(2)	-0.57(2)	0.70(8-I-1)	-193(2)	-386(2)	-301(2)
2	100	-1.07(8-I-1)	-0.73(8-I-1)	0.80(8-I-1)	-166(8-II-1)	-248(8-II-1)	-330(2)
2	101	-0.71(8-I-1)	-0.61(8-I-1)	0.78(8-I-1)	-135(2)	-302(2)	-330(2)
2	102	-0.73(8-I-1)	-0.54(9-II-1)	0.46(8-I-1)	89(8-I-1)	149(9-II-1)	-285(2)
2	103	-0.91(8-I-1)	-0.73(9-II-1)	0.57(8-I-1)	155(8-I-1)	140(9-II-1)	-294(2)
2	104	-0.71(2)	-0.59(2)	-0.23(9-I-1)	159(2)	637(2)	65(9-I-1)
2	105	-0.59(8-I-2)	-0.31(2)	-0.11(9-I-4)	177(2)	769(2)	61(9-I-1)
2	106	-0.55(8-I-1)	-0.36(2)	0.20(9-II-1)	101(8-II-2)	510(2)	-110(2)
2	107	-0.76(8-I-1)	-0.78(2)	-0.29(8-II-1)	115(8-I-1)	380(2)	-133(2)
2	108	-0.70(8-I-1)	-0.51(2)	0.26(9-II-1)	117(9-II-1)	460(2)	-128(2)
2	109	-0.72(8-I-1)	-0.61(2)	0.34(8-I-1)	105(8-I-1)	312(2)	-209(2)
2	110	-0.70(8-I-1)	-0.71(2)	-0.25(9-I-1)	112(9-II-1)	497(2)	-75(9-II-1)
2	111	-0.85(8-I-2)	-1.59(2)	-0.53(9-I-1)	-188(2)	337(2)	-27(9-II-1)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
2	112	-0.83(8-I-2)	-1.59(2)	-0.49(9-I-1)	-136(2)	384(2)	63(2)
2	113	-0.80(2)	-1.02(2)	-0.37(9-I-1)	100(8-I-1)	505(2)	68(2)
2	114	-0.78(8-I-2)	-1.05(2)	-0.38(9-I-1)	98(8-I-1)	436(2)	-50(9-II-1)
2	115	-0.87(8-I-1)	-0.74(2)	-0.55(8-II-1)	-148(8-II-1)	196(2)	-218(2)
2	116	-0.86(8-I-1)	-1.49(2)	-0.58(8-II-1)	-224(2)	281(2)	-84(2)
2	117	-0.85(8-I-1)	-1.18(2)	-0.60(8-II-1)	-178(2)	254(2)	-147(2)
2	118	-0.81(8-I-1)	-1.03(2)	-0.44(8-II-1)	106(8-I-1)	342(2)	-111(2)
2	119	-0.83(9-I-3)	-1.11(2)	-0.55(9-I-4)	128(9-I-3)	366(2)	329(2)
2	120	-0.75(9-I-3)	-0.74(2)	-0.47(9-I-4)	119(9-I-3)	466(2)	382(2)
2	121	-0.74(2)	-0.87(2)	-0.41(9-I-4)	104(1)	537(2)	291(2)
2	122	-0.79(2)	-0.96(2)	-0.38(9-I-1)	101(1)	547(2)	185(2)
2	123	-0.82(8-I-2)	-1.52(2)	-0.47(9-I-1)	-87(2)	410(2)	154(2)
2	124	-0.81(8-I-2)	-1.36(2)	-0.50(9-I-4)	89(9-I-3)	406(2)	244(2)
2	125	-0.48(9-I-3)	-0.33(9-I-1)	-0.50(2)	148(2)	780(2)	283(2)
2	126	-0.55(8-I-2)	-0.30(2)	-0.28(2)	195(2)	847(2)	183(2)
2	127	-0.68(2)	-0.54(2)	-0.27(9-I-1)	189(2)	709(2)	197(2)
2	128	-0.62(9-I-3)	-0.56(2)	-0.42(2)	158(2)	654(2)	308(2)
2	129	-0.57(9-I-3)	-0.44(9-I-1)	-0.52(2)	149(2)	653(2)	342(2)
2	130	-0.67(9-I-3)	-0.55(9-I-1)	-0.50(2)	128(2)	540(2)	389(2)
2	131	-0.89(9-I-3)	-0.91(9-I-1)	-0.60(9-I-4)	176(9-I-3)	287(2)	401(2)
2	132	-0.81(9-I-3)	-0.75(9-I-1)	-0.54(9-I-4)	136(9-I-4)	335(2)	450(2)
2	133	-1.04(9-I-3)	-0.95(9-I-1)	-0.65(9-I-4)	224(9-I-4)	158(9-I-1)	445(2)
2	134	-0.95(9-I-3)	-0.78(9-I-1)	-0.62(9-I-4)	152(9-I-4)	147(9-I-1)	476(2)
2	135	-1.80(9-I-3)	1.48(9-II-1)	-0.97(9-I-3)	285(9-I-3)	-428(2)	338(2)
2	136	-1.32(9-I-3)	1.13(9-II-1)	-0.74(9-I-3)	263(9-I-4)	-189(9-II-1)	436(2)
2	137	-1.38(9-I-3)	0.88(9-II-1)	-1.17(2)	160(9-I-4)	-675(2)	324(2)
2	138	-1.14(9-I-3)	-0.77(9-I-1)	-0.83(2)	162(9-I-4)	-219(9-II-1)	441(2)
2	139	-0.37(9-I-3)	-0.35(9-I-1)	-0.69(2)	94(9-II-3)	462(2)	319(2)
2	140	1.18(2)	-0.64(2)	-0.90(2)	-411(2)	-1854(2)	144(2)
2	141	1.05(2)	-0.60(2)	-1.06(2)	-333(2)	-1492(2)	204(2)
2	142	0.83(2)	-0.53(2)	-0.90(2)	-268(2)	-988(2)	226(2)
2	143	0.44(2)	-0.40(2)	-0.84(2)	-127(2)	-188(2)	294(2)
2	144	-0.94(9-I-4)	-0.62(9-I-1)	-1.32(2)	-148(2)	-900(2)	306(2)
2	145	0.77(2)	-0.49(9-I-1)	-1.19(2)	-297(2)	-1158(2)	244(2)
2	146	-0.54(9-I-4)	-0.53(9-I-1)	-1.31(2)	-240(2)	-1044(2)	285(2)
2	147	-0.53(9-I-3)	-0.44(9-I-1)	-0.74(2)	85(9-II-3)	366(2)	389(2)
2	148	-0.70(9-I-3)	-0.59(9-I-1)	-0.65(2)	91(1)	336(2)	442(2)
2	149	-0.90(9-I-3)	-0.65(9-I-1)	-1.02(2)	83(9-I-4)	-343(2)	412(2)
2	150	-0.78(9-I-3)	-0.63(9-I-1)	-0.84(2)	84(9-I-4)	112(9-I-1)	453(2)
2	151	-0.65(9-I-4)	-0.55(9-I-1)	-1.01(2)	-88(2)	-303(2)	376(2)
2	152	-0.41(9-I-4)	-0.45(9-I-1)	-0.95(2)	-117(2)	-233(2)	354(2)
2	153	0.64(2)	-0.57(2)	-0.26(8-II-1)	-70(2)	-44(9-II-2)	77(2)
2	154	0.43(2)	-0.46(2)	-0.22(8-II-1)	42(2)	657(2)	90(2)
2	155	0.37(2)	-0.40(2)	-0.27(2)	57(9-II-3)	664(2)	133(2)
2	156	0.49(2)	-0.45(2)	-0.25(8-II-1)	39(9-II-3)	483(2)	95(2)
2	157	0.53(2)	-0.47(2)	-0.31(2)	-45(2)	246(2)	126(2)
2	158	0.70(2)	-0.55(2)	-0.31(8-II-1)	-135(2)	-321(2)	108(2)
2	159	0.67(2)	-0.57(2)	-0.28(8-II-1)	-98(2)	-156(2)	90(2)
2	160	0.86(2)	-0.64(2)	-0.34(8-II-1)	-250(2)	-1125(2)	91(2)
2	161	0.99(2)	-0.72(2)	-0.36(8-II-1)	-384(2)	-2133(2)	60(2)
2	162	0.92(2)	-0.73(2)	-0.35(8-II-2)	-369(2)	-2063(2)	48(2)
2	163	0.94(2)	-0.72(2)	-0.35(8-II-2)	-370(2)	-2088(2)	56(2)
2	164	0.80(2)	-0.66(2)	-0.31(8-II-2)	-210(2)	-940(2)	65(2)
2	165	0.82(2)	-0.66(2)	-0.32(8-II-1)	-225(2)	-1022(2)	80(2)
2	166	1.18(2)	-0.68(2)	-0.75(2)	-404(2)	-1879(2)	125(2)
2	167	-0.24(9-I-3)	-0.33(2)	-0.60(2)	87(9-II-3)	513(2)	254(2)
2	168	0.52(2)	-0.44(2)	-0.70(2)	-109(2)	-98(2)	242(2)
2	169	0.85(2)	-0.56(2)	-0.75(2)	-254(2)	-909(2)	194(2)
2	170	0.30(2)	-0.36(2)	-0.49(2)	71(9-II-3)	519(2)	202(2)
2	171	0.58(2)	-0.47(2)	-0.56(2)	-108(2)	-87(2)	195(2)
2	172	0.71(2)	-0.54(2)	-0.38(2)	-162(2)	-420(2)	128(2)
2	173	0.67(2)	-0.51(2)	-0.46(2)	-123(2)	-255(2)	175(2)
2	174	0.54(2)	-0.47(2)	-0.40(2)	-57(2)	138(2)	153(2)
2	175	0.35(2)	-0.38(2)	-0.38(2)	60(9-II-3)	581(2)	166(2)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
2	176	1.06(2)	-0.71(2)	-0.38(8-II-4)	-400(2)	-2112(2)	70(2)
2	177	0.89(2)	-0.63(2)	-0.38(2)	-271(2)	-1151(2)	104(2)
2	178	0.87(2)	-0.58(2)	-0.61(2)	-254(2)	-932(2)	162(2)
2	179	1.16(2)	-0.70(2)	-0.60(2)	-408(2)	-1927(2)	108(2)
2	180	1.12(2)	-0.71(2)	-0.46(2)	-409(2)	-2017(2)	87(2)
2	181	0.89(2)	-0.61(2)	-0.49(2)	-264(2)	-1046(2)	128(2)
2	182	-0.27(8-I-3)	-0.33(2)	-0.17(8-II-1)	113(2)	990(2)	97(2)
2	183	-0.37(8-I-2)	-0.23(2)	-0.12(8-II-1)	153(2)	1042(2)	100(2)
2	184	-0.46(8-I-2)	-0.24(8-II-3)	-0.25(2)	175(2)	964(2)	160(2)
2	185	-0.37(8-I-2)	-0.26(9-I-2)	-0.44(2)	125(9-II-3)	850(2)	227(2)
2	186	-0.29(8-I-2)	-0.28(2)	-0.38(2)	106(9-II-3)	860(2)	190(2)
2	187	-0.38(8-I-2)	-0.23(8-II-3)	-0.25(2)	144(2)	1005(2)	154(2)
2	188	-0.27(8-I-2)	-0.28(2)	-0.31(2)	99(2)	897(2)	153(2)
2	189	-0.27(8-I-2)	-0.30(2)	-0.21(2)	107(2)	955(2)	126(2)
2	190	-0.39(8-I-2)	-0.21(9-I-2)	-0.15(2)	150(2)	1040(2)	121(2)
2	191	-0.50(8-I-2)	-0.23(8-II-3)	-0.06(8-II-4)	162(2)	890(2)	76(2)
2	192	-0.44(8-I-2)	-0.22(8-II-4)	-0.06(8-II-1)	140(2)	925(2)	94(2)
2	193	-0.42(8-I-2)	-0.19(2)	0.09(8-I-1)	146(2)	885(2)	100(2)
2	194	-0.34(8-I-2)	-0.28(2)	-0.07(2)	130(2)	375(2)	87(2)
2	195	-0.38(8-I-2)	-0.24(8-II-4)	0.07(8-I-1)	107(2)	614(2)	87(2)
2	196	-0.22(8-I-3)	-0.28(8-II-2)	0.10(9-II-3)	112(8-II-1)	247(2)	63(2)
2	197	-0.31(9-I-1)	-0.37(8-II-2)	-0.38(8-I-2)	86(8-II-1)	-582(2)	-69(8-II-1)
2	198	-0.40(8-I-2)	-0.36(2)	-0.28(8-I-2)	93(2)	-421(2)	-65(8-II-1)
2	199	-0.55(8-I-2)	-0.38(8-II-2)	-0.61(8-I-2)	52(8-II-1)	-878(2)	-168(2)
2	200	-0.34(8-I-2)	-0.32(2)	-0.21(8-I-3)	73(8-II-1)	-201(2)	-57(8-II-1)
2	201	-0.21(9-I-1)	-0.29(8-II-2)	-0.19(9-I-3)	-129(8-I-1)	-238(2)	41(8-I-1)
2	202	-0.60(8-II-1)	-0.25(8-II-2)	-0.76(8-I-2)	-166(8-I-1)	-1166(2)	-154(2)
2	203	-0.35(8-II-1)	-0.26(8-II-2)	-0.46(8-I-2)	-153(8-I-1)	-740(2)	-69(8-II-1)
2	204	-0.66(8-II-1)	-0.19(8-II-2)	-0.69(8-I-2)	-272(8-I-1)	-1126(2)	-139(2)
2	205	-0.40(8-I-4)	-0.22(2)	0.12(9-II-4)	115(8-II-2)	578(2)	-45(8-I-1)
2	206	-0.37(8-I-2)	-0.25(8-II-4)	0.08(8-I-4)	122(8-II-1)	659(2)	56(2)
2	207	0.79(2)	-0.43(2)	0.17(9-II-1)	-312(2)	-611(2)	-183(2)
2	208	0.32(2)	-0.31(2)	0.17(9-II-1)	-127(2)	89(2)	-102(2)
2	209	0.66(2)	-0.54(2)	0.33(8-I-1)	-224(2)	-329(2)	-223(2)
2	210	0.18(2)	-0.24(8-II-2)	0.11(9-II-3)	-125(8-I-1)	192(2)	22(8-II-1)
2	211	0.75(8-I-1)	-0.18(2)	-0.56(2)	-370(2)	-1017(2)	-146(2)
2	212	0.38(2)	-0.22(8-II-2)	-0.20(9-I-3)	-212(8-I-1)	-383(2)	-50(2)
2	213	0.83(2)	-0.33(2)	-0.32(2)	-355(2)	-785(2)	-176(2)
2	214	-0.13(9-II-2)	1.23(9-I-2)	1.17(9-I-2)	119(2)	-320(9-I-2)	160(9-II-2)
2	215	0.21(8-I-2)	1.62(9-I-2)	1.72(9-I-2)	208(9-II-2)	-416(9-I-2)	153(9-II-2)
2	216	-0.31(8-II-2)	1.75(9-I-2)	1.12(9-I-2)	63(8-II-1)	-697(2)	91(8-II-2)
2	217	-0.26(8-II-2)	2.04(9-I-2)	1.54(9-I-2)	129(9-II-2)	-570(9-I-2)	112(8-II-2)
2	218	-0.17(9-II-2)	1.47(9-I-2)	1.13(9-I-2)	86(2)	-496(2)	128(8-II-2)
2	219	-0.36(8-I-2)	0.67(9-I-2)	-0.60(9-II-2)	143(2)	-227(2)	165(8-II-2)
2	220	-0.22(8-I-3)	0.93(9-I-2)	0.81(9-I-2)	151(2)	-259(2)	163(8-II-2)
2	221	-0.15(8-I-3)	1.09(9-I-2)	0.80(9-I-2)	85(2)	-509(2)	132(8-II-2)
2	222	-0.17(9-II-2)	1.19(9-I-2)	0.88(8-I-2)	50(9-I-2)	-797(2)	-98(8-I-2)
2	223	-0.25(8-I-2)	0.77(9-I-2)	-0.88(8-II-2)	-75(9-II-2)	-881(2)	-118(8-I-2)
2	224	-0.30(8-I-2)	0.74(9-I-2)	-0.69(8-II-2)	91(9-I-2)	-523(2)	134(8-II-2)
2	225	-0.25(9-II-2)	-0.91(8-I-3)	1.19(9-I-2)	159(9-II-2)	128(8-I-3)	193(2)
2	226	-0.31(9-II-2)	-1.15(8-I-3)	1.59(9-I-2)	-202(9-I-2)	-114(8-II-3)	212(2)
2	227	-0.22(9-II-2)	-1.19(9-II-2)	1.74(9-I-2)	217(9-II-2)	-226(9-I-2)	184(2)
2	228	-0.17(9-II-2)	-1.00(9-II-2)	1.21(9-I-2)	151(9-II-2)	-169(9-I-2)	183(2)
2	229	-0.44(8-I-2)	-0.62(9-II-2)	0.57(9-I-2)	209(2)	115(8-I-3)	177(8-II-2)
2	230	-0.49(8-I-2)	-0.55(8-I-3)	0.60(9-I-2)	259(2)	258(2)	165(9-II-2)
2	231	-0.36(8-I-2)	-0.73(8-I-3)	0.87(9-I-2)	207(2)	157(8-I-1)	177(2)
2	232	-0.31(8-I-2)	-0.80(9-II-2)	0.84(9-I-2)	192(2)	-116(8-II-3)	180(2)
2	233	-0.49(8-I-2)	-0.49(9-II-2)	-0.85(8-II-2)	-110(9-II-2)	-941(2)	-131(8-I-2)
2	234	0.76(8-II-2)	-0.38(9-II-2)	-0.77(8-II-2)	-168(2)	-982(2)	-138(8-I-2)
2	235	-0.65(8-I-2)	-0.37(9-II-2)	-0.51(8-II-2)	-105(8-II-2)	-474(2)	129(8-II-2)
2	236	-0.47(8-I-2)	-0.51(9-II-2)	-0.63(8-II-2)	94(9-I-2)	-523(2)	132(8-II-2)
2	237	-0.56(8-I-2)	-0.41(8-I-3)	0.39(9-I-2)	235(2)	319(2)	156(8-II-2)
2	238	-0.53(8-I-2)	-0.47(9-II-2)	-0.44(9-II-2)	182(2)	118(8-I-4)	172(8-II-2)
2	239	-0.59(8-I-2)	-0.39(9-II-2)	-0.41(9-II-2)	141(8-I-2)	-90(8-II-4)	158(8-II-2)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
2	240	-0.49(8-I-2)	-0.52(9-II-2)	-0.51(9-II-2)	125(9-I-3)	-204(2)	163(8-II-2)
2	241	-0.61(8-I-2)	-0.29(8-I-3)	-0.27(9-II-2)	179(2)	365(2)	138(8-II-2)
2	242	-0.66(8-I-2)	-0.28(8-I-3)	-0.31(9-II-2)	147(8-I-2)	97(8-I-4)	146(8-II-2)
2	243	1.40(8-II-2)	-0.33(9-II-2)	-0.55(8-II-2)	-336(2)	-1235(2)	-172(2)
2	244	1.11(8-II-2)	-0.35(9-II-2)	-0.70(8-II-2)	-242(2)	-1119(2)	-146(8-I-2)
2	245	1.01(8-II-2)	-0.28(9-II-2)	-0.44(8-II-2)	-209(8-II-2)	-768(2)	-134(8-I-2)
2	246	-0.77(8-I-2)	-0.27(9-II-2)	-0.38(9-II-2)	-141(8-II-2)	-352(2)	123(8-II-2)
2	247	-0.47(8-I-2)	-0.26(2)	-0.13(2)	130(2)	453(2)	37(9-II-1)
2	248	-0.56(8-I-2)	-0.19(8-I-2)	-0.17(2)	135(8-I-2)	454(2)	54(9-II-2)
2	249	-0.80(8-I-2)	-0.30(2)	-0.20(8-I-3)	127(8-I-2)	-347(2)	-160(2)
2	250	-0.73(8-I-2)	-0.36(2)	-0.23(8-I-3)	85(8-I-2)	-364(2)	-147(2)
2	251	-0.56(8-I-2)	-0.29(2)	-0.21(2)	116(8-I-2)	-28(9-I-3)	-43(2)
2	252	-0.88(8-I-2)	-0.34(8-II-2)	0.41(8-II-2)	114(8-I-2)	-737(2)	-213(2)
2	253	-0.70(8-I-2)	-0.18(2)	-0.21(2)	144(8-I-2)	90(2)	-41(9-I-2)
2	254	-0.92(8-I-2)	-0.21(2)	-0.15(9-II-2)	-170(8-II-2)	-384(2)	-147(2)
2	255	-1.32(8-I-2)	-0.39(8-II-2)	0.29(8-II-3)	-232(8-II-2)	-902(2)	-278(2)
2	256	1.36(8-II-2)	-0.38(8-II-2)	0.24(9-I-2)	-325(8-II-2)	-1003(2)	-246(2)
2	257	1.51(8-II-2)	-0.34(9-II-2)	0.32(9-I-2)	-346(2)	-1131(2)	-195(2)
2	258	-1.02(8-I-2)	-0.19(9-II-2)	-0.19(9-II-2)	-225(8-II-2)	-474(2)	-123(2)
2	259	-1.01(8-I-2)	-0.22(9-II-2)	-0.28(9-II-2)	-237(8-II-2)	-610(2)	-130(8-I-2)
2	260	-0.61(8-I-2)	-0.21(8-I-3)	-0.19(9-II-2)	150(8-I-2)	424(2)	100(8-II-2)
2	261	-0.70(8-I-2)	-0.20(8-I-3)	-0.23(9-II-2)	144(8-I-2)	140(2)	107(8-II-2)
2	262	-0.79(8-I-2)	-0.16(8-I-3)	-0.20(2)	-145(8-II-2)	-34(8-II-4)	-81(8-I-2)
2	263	-0.83(8-I-2)	-0.19(8-I-3)	-0.27(9-II-2)	-165(8-II-2)	-221(2)	-100(8-I-2)
2	264	-0.50(8-I-2)	-0.21(8-I-2)	-0.12(9-II-2)	183(2)	701(2)	77(2)
2	265	-0.48(8-I-3)	-0.24(8-I-2)	0.15(9-I-2)	198(2)	860(2)	59(2)
2	266	-0.42(8-I-2)	-0.21(2)	0.11(8-I-2)	166(2)	889(2)	79(2)
2	267	-0.43(8-I-2)	-0.21(2)	-0.10(8-II-2)	164(2)	761(2)	87(2)
2	268	-0.44(8-I-3)	-0.22(2)	0.12(8-I-2)	180(2)	903(2)	70(2)
2	269	-0.37(8-I-3)	-0.25(2)	-0.11(8-II-2)	160(2)	1033(2)	76(2)
2	270	-0.29(8-I-3)	-0.35(2)	-0.14(8-II-1)	127(2)	1019(2)	67(2)
2	271	-0.44(8-I-3)	-0.29(2)	0.17(8-I-2)	196(2)	982(2)	27(2)
2	272	-0.40(8-I-3)	-0.28(2)	0.14(8-I-2)	172(2)	1014(2)	52(2)
2	273	-0.32(8-I-3)	-0.38(2)	0.16(8-I-2)	139(2)	1026(2)	37(2)
2	274	-0.33(8-I-3)	-0.40(2)	0.20(2)	142(2)	1002(2)	16(8-I-3)
2	275	-0.40(8-I-3)	-0.36(2)	0.21(2)	173(2)	1025(2)	-15(9-I-2)
2	276	-0.36(8-I-3)	-0.44(2)	0.28(2)	139(2)	978(2)	-28(2)
2	277	-0.59(8-I-3)	-0.46(8-I-2)	0.41(9-I-2)	275(2)	661(2)	80(9-II-2)
2	278	-0.61(8-I-3)	-0.64(2)	0.52(9-I-2)	253(2)	595(2)	83(9-II-2)
2	279	-0.65(8-I-3)	-0.54(8-I-2)	0.43(9-I-2)	274(2)	721(2)	-75(9-I-2)
2	280	-0.59(8-I-2)	-0.39(8-I-3)	0.40(9-I-2)	267(2)	485(2)	125(9-II-2)
2	281	-0.58(8-I-3)	-0.49(8-I-2)	0.52(9-I-2)	272(2)	499(2)	114(9-II-2)
2	282	-0.59(8-I-2)	-0.40(8-I-2)	0.42(9-I-2)	275(2)	598(2)	101(9-II-2)
2	283	-0.55(8-I-3)	-0.38(8-I-2)	0.28(9-I-2)	243(2)	874(2)	-42(9-I-2)
2	284	-0.50(8-I-3)	-0.32(8-I-2)	0.22(9-I-2)	219(2)	930(2)	30(9-II-2)
2	285	-0.60(8-I-3)	-0.44(8-I-2)	0.35(9-I-2)	261(2)	807(2)	-59(9-I-2)
2	286	-0.58(8-I-2)	-0.30(8-I-3)	0.26(9-I-2)	237(2)	554(2)	111(9-II-2)
2	287	-0.56(8-I-2)	-0.24(8-I-2)	0.18(9-I-2)	209(2)	642(2)	85(9-II-2)
2	288	-0.56(8-I-3)	-0.34(8-I-2)	0.27(9-I-2)	247(2)	796(2)	55(9-II-2)
2	289	-0.53(8-I-3)	-0.29(8-I-2)	0.21(9-I-2)	225(2)	831(2)	51(9-II-2)
2	290	-0.54(8-I-3)	-0.29(8-I-2)	0.23(9-I-2)	230(2)	733(2)	71(9-II-2)
2	291	-0.58(8-I-3)	-0.39(8-I-2)	0.34(9-I-2)	266(2)	731(2)	67(9-II-2)
2	292	-0.58(8-I-2)	-0.34(8-I-2)	0.31(9-I-2)	259(2)	659(2)	89(9-II-2)
2	293	-0.60(8-I-3)	-0.67(9-I-2)	0.38(2)	199(2)	920(2)	-166(2)
2	294	-0.69(8-I-3)	-0.79(9-I-2)	0.35(9-I-2)	223(8-I-3)	881(2)	-190(2)
2	295	-0.64(8-I-3)	-0.62(2)	0.43(9-I-2)	259(2)	795(2)	-82(9-I-2)
2	296	-0.70(8-I-3)	-0.69(2)	0.44(9-I-2)	238(2)	784(2)	-90(9-I-2)
2	297	-0.65(8-I-3)	-0.60(9-I-2)	0.39(9-I-2)	245(2)	876(2)	-98(2)
2	298	-0.63(8-I-3)	-0.65(9-I-2)	0.36(9-I-2)	225(2)	908(2)	-133(2)
2	299	-0.71(8-I-3)	-0.77(9-I-2)	0.40(9-I-2)	222(8-I-3)	846(2)	-138(2)
2	300	-0.46(8-I-3)	-0.37(8-I-2)	0.26(2)	200(2)	995(2)	-31(9-I-2)
2	301	-0.41(8-I-3)	-0.45(2)	0.33(2)	162(2)	987(2)	-57(2)
2	302	-0.59(8-I-3)	-0.49(8-I-2)	0.35(9-I-2)	249(2)	886(2)	-67(9-I-2)
2	303	-0.53(8-I-3)	-0.43(8-I-2)	0.29(9-I-2)	225(2)	949(2)	-50(9-I-2)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
2	304	-0.48(8-I-3)	-0.49(9-I-2)	0.36(2)	193(2)	979(2)	-87(2)
2	305	-0.58(8-I-3)	-0.60(9-I-2)	0.36(2)	220(2)	937(2)	-123(2)
2	306	-0.55(8-I-3)	-0.53(9-I-2)	0.36(2)	217(2)	964(2)	-109(2)
2	307	-0.54(8-I-3)	-0.60(9-I-2)	0.40(2)	192(2)	944(2)	-136(2)
2	308	-0.57(8-I-3)	-0.55(9-I-2)	0.35(9-I-2)	226(2)	925(2)	-97(2)
2	309	-0.80(8-I-3)	-0.96(2)	0.44(9-I-2)	230(8-I-3)	754(2)	-118(2)
2	310	-0.90(8-I-3)	-1.04(9-I-2)	0.32(9-I-2)	239(8-I-3)	763(2)	-221(2)
2	311	-0.80(8-I-3)	-0.90(9-I-2)	0.34(9-I-2)	240(8-I-3)	835(2)	-211(2)
2	312	-0.85(8-I-3)	-1.04(9-I-2)	0.38(9-I-2)	237(8-I-3)	768(2)	-167(2)
2	313	-1.00(9-II-2)	-1.95(2)	-0.90(9-II-2)	-168(8-II-3)	509(2)	78(9-II-2)
2	314	-1.09(9-II-2)	-1.60(2)	-0.87(8-I-3)	-158(8-II-3)	534(2)	-71(9-I-2)
2	315	-0.88(9-II-2)	-1.41(2)	-0.61(9-II-2)	201(8-I-3)	622(2)	-91(9-I-2)
2	316	-0.96(8-I-3)	-1.26(9-I-2)	-0.58(9-II-2)	211(8-I-3)	658(2)	-115(2)
2	317	-1.01(8-I-3)	-1.16(9-I-2)	-0.45(8-I-3)	226(8-I-3)	700(2)	-213(2)
2	318	-1.04(8-I-3)	-1.29(9-I-2)	-0.60(8-I-3)	203(8-I-3)	642(2)	-156(2)
2	319	-1.12(8-I-3)	-1.25(9-I-2)	-0.65(8-I-3)	187(8-I-3)	617(2)	-197(2)
2	320	-1.30(8-I-3)	-1.34(9-I-2)	-0.96(2)	-127(8-II-3)	509(2)	-166(2)
2	321	-1.32(8-I-3)	-1.48(9-I-2)	-1.21(2)	-138(8-II-2)	429(2)	-98(2)
2	322	-1.38(8-I-3)	-1.32(9-I-2)	-1.25(2)	-128(8-II-2)	442(2)	-139(2)
2	323	-1.14(8-I-3)	-1.44(9-I-2)	-0.84(8-I-3)	146(8-I-3)	538(2)	-98(2)
2	324	-1.22(8-I-3)	-1.52(9-I-2)	-1.12(2)	-146(8-II-3)	469(2)	-77(2)
2	325	-1.20(8-I-3)	-1.34(9-I-2)	-0.86(8-I-3)	143(8-I-3)	544(2)	-151(2)
2	326	-0.72(8-I-3)	-0.96(2)	0.51(9-I-2)	212(2)	679(2)	-96(9-I-2)
2	327	-0.81(9-II-2)	-2.43(2)	-0.96(9-II-2)	-225(8-II-3)	353(2)	107(9-II-2)
2	328	-0.89(9-II-2)	-2.28(2)	-0.96(9-II-2)	-193(8-II-3)	446(2)	95(9-II-2)
2	329	-0.80(9-II-2)	-1.93(2)	-0.81(9-II-2)	-159(8-II-3)	450(2)	93(9-II-2)
2	330	-0.80(9-II-2)	-1.42(2)	-0.63(9-II-2)	187(8-I-3)	558(2)	-89(9-I-2)
2	331	-0.68(9-II-2)	-1.35(2)	0.69(9-I-2)	176(8-I-3)	476(2)	82(9-II-2)
2	332	-0.64(8-I-3)	-0.93(2)	0.61(9-I-2)	239(2)	565(2)	-84(9-I-2)
2	333	-0.55(9-II-2)	-1.16(2)	0.75(9-I-2)	175(8-I-3)	415(2)	99(9-II-2)
2	334	-0.40(8-I-3)	-0.79(8-I-3)	0.87(9-I-2)	196(2)	243(2)	156(2)
2	335	-0.48(8-I-3)	-0.93(2)	0.81(9-I-2)	200(2)	353(2)	122(9-II-2)
2	336	-0.51(8-I-3)	-0.64(8-I-3)	0.67(9-I-2)	258(2)	370(2)	136(9-II-2)
2	337	-0.68(9-II-2)	-1.82(2)	-0.80(9-II-2)	-139(8-II-3)	354(2)	94(9-II-2)
2	338	-0.67(9-II-2)	-2.30(2)	-0.92(9-II-2)	-224(9-I-2)	255(2)	110(2)
2	339	-0.40(9-II-2)	-1.55(2)	1.36(9-I-2)	-190(9-I-2)	133(8-I-4)	217(2)
2	340	-0.34(9-II-2)	-1.06(2)	1.11(9-I-2)	151(9-II-2)	170(8-I-2)	184(2)
2	341	-0.46(9-II-2)	-1.83(2)	1.14(9-I-2)	-186(9-I-2)	159(8-I-2)	205(2)
2	342	-0.43(9-II-2)	-1.37(2)	1.01(9-I-2)	141(9-II-2)	230(2)	152(2)
2	343	-0.54(9-II-2)	-1.62(2)	0.89(9-I-2)	130(8-I-3)	276(2)	104(2)
2	344	-0.56(9-II-2)	-2.28(2)	0.91(9-I-2)	-236(2)	173(8-I-4)	160(2)
2	345	-0.51(9-II-2)	-2.05(2)	0.98(9-I-2)	-197(9-I-2)	167(8-I-2)	169(2)
2	346	1.03(2)	-0.80(2)	0.33(8-I-2)	-396(2)	-2202(2)	15(9-I-3)
2	347	0.96(2)	-0.78(2)	-0.33(8-II-2)	-375(2)	-2173(2)	18(9-I-3)
2	348	0.91(2)	-0.74(2)	0.30(8-I-2)	-249(2)	-1122(2)	19(9-I-3)
2	349	0.87(2)	-0.72(2)	-0.27(8-II-2)	-236(2)	-1097(2)	24(9-I-3)
2	350	0.80(2)	-0.68(2)	-0.30(8-II-2)	-205(2)	-924(2)	48(2)
2	351	0.92(2)	-0.74(2)	-0.35(8-II-2)	-368(2)	-2069(2)	31(2)
2	352	0.93(2)	-0.77(2)	-0.34(8-II-2)	-367(2)	-2118(2)	22(9-I-3)
2	353	0.83(2)	-0.71(2)	-0.29(8-II-2)	-216(2)	-1010(2)	30(2)
2	354	0.76(2)	-0.67(2)	0.28(8-I-2)	-118(2)	-266(2)	-22(9-II-3)
2	355	0.41(2)	-0.50(2)	0.22(8-I-2)	79(2)	803(2)	19(8-I-3)
2	356	0.60(2)	-0.59(2)	0.24(8-I-2)	17(8-I-3)	388(2)	-23(8-II-3)
2	357	0.44(2)	-0.48(2)	-0.18(8-II-2)	54(2)	717(2)	58(2)
2	358	0.64(2)	-0.60(2)	-0.24(8-II-2)	-57(2)	52(9-I-2)	53(2)
2	359	0.74(2)	-0.66(2)	0.24(8-I-2)	-121(2)	-297(2)	27(9-I-3)
2	360	0.70(2)	-0.63(2)	-0.22(8-II-2)	-70(2)	-99(2)	60(2)
2	361	0.60(2)	-0.59(2)	0.21(8-I-2)	-12(9-I-1)	313(2)	28(9-I-3)
2	362	0.42(2)	-0.49(2)	0.18(8-I-2)	63(2)	770(2)	32(2)
2	363	1.24(2)	-0.80(2)	0.47(2)	-418(2)	-2148(2)	-70(2)
2	364	1.05(2)	-0.73(2)	0.49(2)	-269(2)	-1110(2)	-103(2)
2	365	1.22(2)	-0.83(2)	0.44(8-I-2)	-428(2)	-2186(2)	-54(2)
2	366	1.03(2)	-0.75(2)	0.40(2)	-273(2)	-1134(2)	-75(2)
2	367	0.95(2)	-0.75(2)	0.34(8-I-2)	-263(2)	-1131(2)	-25(8-II-3)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
2	368	1.11(2)	-0.81(2)	0.37(8-I-2)	-420(2)	-2212(2)	-16(9-II-3)
2	369	1.18(2)	-0.82(2)	0.41(8-I-2)	-432(2)	-2205(2)	-30(2)
2	370	1.00(2)	-0.75(2)	0.37(8-I-2)	-272(2)	-1139(2)	-47(2)
2	371	0.85(2)	-0.66(2)	0.49(2)	-136(2)	-290(2)	-122(2)
2	372	0.82(2)	-0.68(2)	0.35(2)	-134(2)	-286(2)	-58(2)
2	373	0.78(2)	-0.68(2)	0.31(8-I-2)	-125(2)	-263(2)	-32(8-II-3)
2	374	0.84(2)	-0.68(2)	0.42(2)	-138(2)	-299(2)	-90(2)
2	375	0.63(2)	-0.60(2)	0.49(2)	-69(8-II-3)	308(2)	-133(2)
2	376	0.50(8-II-3)	-0.57(9-I-2)	0.47(2)	103(8-I-3)	691(2)	-133(2)
2	377	-0.43(8-I-3)	-0.54(9-I-2)	0.42(2)	144(2)	911(2)	-117(2)
2	378	0.40(2)	-0.52(2)	0.30(2)	81(2)	798(2)	-34(2)
2	379	0.60(2)	-0.60(2)	0.29(2)	27(8-I-3)	384(2)	-33(8-II-3)
2	380	0.63(2)	-0.61(2)	0.36(2)	-41(8-II-3)	341(2)	-63(2)
2	381	0.64(2)	-0.62(2)	0.43(2)	-56(8-II-3)	306(2)	-97(2)
2	382	0.47(8-II-3)	-0.56(2)	0.42(2)	80(8-I-3)	671(2)	-98(2)
2	383	0.44(2)	-0.54(2)	0.37(2)	74(2)	736(2)	-58(2)
2	384	0.39(8-II-3)	-0.51(2)	0.39(2)	120(2)	885(2)	-83(2)
2	385	-0.55(8-I-3)	-0.68(9-I-2)	0.44(2)	181(8-I-3)	866(2)	-192(2)
2	386	-0.50(8-I-3)	-0.60(9-I-2)	0.44(2)	154(8-I-3)	896(2)	-152(2)
2	387	0.53(8-II-3)	-0.62(9-I-2)	0.49(2)	127(8-I-3)	696(2)	-170(2)
2	388	0.56(8-II-3)	-0.68(9-I-2)	0.50(2)	155(8-I-3)	690(2)	-211(2)
2	389	-0.64(8-I-3)	-0.83(9-I-2)	0.42(2)	203(8-I-3)	650(2)	-295(2)
2	390	-0.73(8-I-3)	-0.86(9-I-2)	0.30(2)	229(8-I-3)	805(2)	-259(2)
2	391	0.59(8-II-3)	-0.74(9-I-2)	0.48(2)	182(8-I-3)	674(2)	-251(2)
2	392	-0.62(8-I-3)	-0.77(9-I-2)	0.40(2)	208(8-I-3)	842(2)	-228(2)
2	393	0.74(8-II-3)	-0.76(9-I-2)	0.54(2)	-146(8-II-3)	211(2)	-320(2)
2	394	0.82(8-II-3)	-0.72(9-I-2)	0.61(2)	-153(8-II-3)	-128(2)	-253(2)
2	395	0.69(8-II-3)	-0.73(9-I-2)	0.54(2)	147(8-I-3)	367(2)	-263(2)
2	396	1.20(2)	-0.72(9-I-2)	0.72(2)	-400(2)	-1827(2)	-150(2)
2	397	0.95(8-II-3)	-0.72(9-I-2)	0.67(2)	-232(2)	-826(2)	-217(2)
2	398	1.08(8-II-3)	-0.73(9-I-2)	0.74(2)	-264(2)	-1274(2)	-240(2)
2	399	1.25(2)	-0.74(2)	0.57(2)	-412(2)	-2067(2)	-88(2)
2	400	1.25(2)	-0.71(9-I-2)	0.65(2)	-405(2)	-1951(2)	-111(2)
2	401	1.01(2)	-0.69(9-I-2)	0.63(2)	-244(2)	-929(2)	-170(2)
2	402	1.05(2)	-0.67(2)	0.57(2)	-262(2)	-1048(2)	-131(2)
2	403	0.67(8-II-3)	-0.68(9-I-2)	0.55(2)	117(8-I-3)	349(2)	-216(2)
2	404	0.63(8-II-3)	-0.63(9-I-2)	0.53(2)	91(8-I-3)	324(2)	-172(2)
2	405	0.84(2)	-0.65(9-I-2)	0.56(2)	-128(2)	-254(2)	-160(2)
2	406	0.81(2)	-0.68(9-I-2)	0.60(2)	-135(8-II-3)	-214(2)	-202(2)
2	407	-0.78(8-I-3)	-0.92(9-I-2)	0.24(2)	222(8-I-3)	644(2)	-328(2)
2	408	-0.87(8-I-3)	-0.98(9-I-2)	0.26(9-I-2)	238(8-I-3)	755(2)	-279(2)
2	409	-0.98(8-I-3)	-1.03(9-I-2)	-0.24(8-I-3)	220(8-I-3)	630(2)	-336(2)
2	410	-1.03(8-I-3)	-1.09(9-I-2)	-0.35(8-I-3)	226(8-I-3)	696(2)	-276(2)
2	411	-1.43(8-I-3)	-1.21(9-I-2)	-1.11(2)	-112(8-II-3)	478(2)	-211(2)
2	412	-1.16(8-I-3)	-1.19(9-I-2)	-0.57(8-I-3)	191(8-I-3)	621(2)	-253(2)
2	413	-1.27(8-I-3)	-1.23(9-I-2)	-0.74(8-I-3)	145(8-I-3)	546(2)	-240(2)
2	414	-1.23(8-I-3)	-1.13(9-I-2)	-0.52(8-I-3)	185(8-I-3)	591(2)	-308(2)
2	415	0.79(8-II-3)	0.86(9-II-2)	0.42(2)	176(8-I-3)	146(9-I-2)	-361(2)
2	416	0.80(8-II-3)	-0.79(9-I-2)	0.52(2)	-164(8-II-3)	113(9-I-2)	-311(2)
2	417	-0.75(8-I-3)	-0.89(9-I-2)	0.36(2)	203(8-I-3)	428(2)	-368(2)
2	418	0.98(8-II-3)	0.75(9-II-2)	0.74(2)	-199(8-II-3)	-863(2)	-254(2)
2	419	1.00(8-II-3)	-0.74(9-I-2)	0.70(2)	-229(2)	-995(2)	-212(2)
2	420	1.11(8-II-3)	-0.74(9-I-2)	0.81(2)	-297(2)	-1477(2)	-217(2)
2	421	0.91(8-II-3)	-0.77(9-I-2)	0.65(2)	-179(8-II-3)	-459(2)	-319(2)
2	422	0.93(8-II-3)	0.98(9-II-2)	0.69(2)	-191(8-II-3)	-738(2)	-300(2)
2	423	1.07(8-II-3)	0.97(9-II-2)	0.84(2)	-272(2)	-1522(2)	-203(2)
2	424	0.84(8-II-3)	0.94(9-II-2)	0.53(2)	-178(8-II-3)	-207(2)	-343(2)
2	425	-0.95(8-I-3)	1.02(9-II-2)	0.17(8-II-3)	211(8-I-3)	503(2)	-379(2)
2	426	-1.56(8-I-3)	1.84(9-II-2)	-0.81(2)	117(8-I-3)	381(2)	-344(2)
2	427	-1.54(8-I-3)	1.36(9-II-2)	-0.95(2)	107(8-I-3)	464(2)	-278(2)
2	428	-1.12(8-I-3)	1.25(9-II-2)	-0.28(8-I-3)	197(8-I-3)	470(2)	-379(2)
2	429	-1.28(8-I-3)	1.25(9-II-2)	-0.51(8-I-3)	175(8-I-3)	521(2)	-340(2)
2	430	-1.26(8-I-3)	1.54(9-II-2)	-0.44(8-I-3)	161(8-I-3)	413(2)	-382(2)
2	431	0.95(8-II-3)	1.33(9-II-2)	0.83(2)	-225(2)	-1339(2)	-221(2)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
2	432	0.84(8-II-3)	1.34(9-II-2)	0.61(2)	-179(8-II-3)	-632(2)	-322(2)
2	433	-1.01(8-I-3)	1.38(9-II-2)	0.17(9-II-3)	191(8-I-3)	307(2)	-405(2)
2	434	-0.83(8-I-3)	1.10(9-II-2)	0.26(2)	193(8-I-3)	266(2)	-393(2)
2	435	0.81(8-II-3)	1.42(9-II-2)	0.42(2)	-161(8-II-3)	-206(9-II-2)	-377(2)
2	436	0.80(8-II-3)	1.19(9-II-2)	0.39(2)	-169(8-II-3)	-129(9-II-2)	-371(2)
2	437	-0.86(8-I-3)	1.43(9-II-2)	0.23(2)	177(8-I-3)	188(9-I-2)	-402(2)
2	438	-1.53(8-I-3)	2.36(9-II-2)	-0.59(8-I-3)	127(2)	299(9-I-2)	-397(2)
2	439	-1.01(8-I-3)	1.71(9-II-2)	0.22(9-II-3)	167(8-I-3)	219(9-I-2)	-415(2)
2	440	-1.17(8-I-3)	1.65(9-II-2)	-0.28(9-I-3)	171(8-I-3)	298(2)	-408(2)
2	441	-1.20(8-I-3)	1.95(9-II-2)	-0.31(9-I-3)	152(8-I-3)	268(9-I-2)	-423(2)
2	442	-0.96(8-I-3)	2.29(9-II-2)	0.37(9-II-3)	117(8-I-3)	-366(2)	-382(2)
2	443	-1.07(8-I-3)	3.13(2)	0.50(9-II-2)	95(2)	-437(9-II-2)	-405(2)
2	444	-0.61(8-I-3)	2.51(2)	0.55(2)	-101(8-II-3)	-735(2)	-308(2)
2	445	-1.35(8-I-3)	2.83(9-II-2)	-0.48(9-I-3)	149(2)	297(9-I-2)	-426(2)
2	446	-1.06(8-I-3)	2.20(9-II-2)	0.29(9-II-3)	136(8-I-3)	-243(9-II-2)	-420(2)
2	447	-0.90(8-I-3)	1.77(9-II-2)	0.29(2)	149(8-I-3)	-227(9-II-2)	-400(2)
2	448	-0.77(8-I-3)	1.79(9-II-2)	0.50(2)	-149(8-II-3)	-518(2)	-347(2)
2	449	0.76(8-II-3)	1.81(9-II-2)	0.75(2)	-156(2)	-1088(2)	-255(2)
2	1	-1.16(8-II-2)	-1.23(8-II-1)	-0.63(8-II-1)	-1099(8-I-2)	-11(9-I-2)	-23(8-I-2)
2	2	-2.49(8-II-2)	-0.84(8-II-1)	-0.67(8-II-1)	-718(8-I-2)	36(8-II-2)	7(9-II-1)
2	3	1.07(8-I-2)	-1.26(8-II-2)	-0.81(8-II-1)	-468(8-I-2)	34(8-II-2)	11(8-II-2)
2	4	-2.12(8-II-2)	-0.89(8-I-1)	0.73(8-I-1)	-413(8-I-2)	38(9-II-3)	7(8-I-1)
2	5	0.63(8-I-2)	-0.67(8-II-1)	-0.85(8-II-1)	-481(8-I-2)	37(9-II-3)	7(8-I-3)
2	6	-2.39(8-II-2)	-0.91(2)	0.83(8-I-1)	177(8-II-2)	43(9-II-1)	-10(8-II-2)
2	7	0.77(8-I-2)	-0.22(8-II-1)	1.04(8-I-1)	-206(8-I-2)	36(9-II-2)	12(8-I-1)
2	8	-2.85(8-II-1)	-1.93(2)	1.07(8-I-1)	162(8-I-1)	74(8-I-3)	-8(8-II-2)
2	9	0.93(8-I-2)	-0.83(2)	1.29(8-I-1)	60(8-II-2)	46(9-II-1)	13(8-I-2)
2	10	2.95(8-I-1)	-4.37(2)	1.43(2)	425(8-I-1)	72(8-I-3)	-8(9-II-1)
2	11	2.80(8-I-2)	-8.59(2)	-1.34(8-II-1)	124(8-II-1)	99(9-II-1)	7(9-II-2)
2	12	-1.86(2)	-13.84(2)	1.26(8-I-1)	79(8-I-4)	117(9-II-1)	-5(8-I-1)
2	13	-2.06(8-II-2)	-2.66(2)	-1.06(8-II-1)	73(8-II-2)	57(9-II-1)	3(9-II-1)
2	14	0.76(8-I-2)	-3.23(2)	-1.46(8-II-1)	57(8-I-3)	70(9-II-1)	-3(8-I-1)
2	15	-1.92(8-II-2)	-1.18(8-I-1)	0.80(8-I-1)	35(9-II-1)	44(9-II-1)	2(8-II-3)
2	16	-2.01(8-II-2)	-1.18(8-II-1)	-0.84(8-II-1)	43(9-II-2)	44(9-II-1)	2(8-I-2)
2	17	0.94(8-I-1)	-0.54(8-I-1)	-1.23(8-II-1)	28(8-I-1)	50(9-II-1)	-2(8-I-2)
2	18	1.00(8-I-1)	-0.42(8-II-1)	1.19(8-I-1)	-18(8-II-1)	47(9-II-1)	-2(8-I-3)
2	19	-0.59(8-II-2)	-0.74(8-II-2)	-0.88(8-II-1)	-273(8-I-2)	43(8-I-2)	11(8-II-2)
2	20	-0.44(8-I-2)	-1.66(8-I-3)	-0.80(8-II-1)	-486(8-I-2)	10(9-II-2)	-20(8-I-2)
2	21	-0.39(8-II-2)	-0.86(2)	-0.94(8-II-1)	-249(8-I-2)	48(9-II-2)	-9(8-I-2)
2	22	-0.79(2)	-1.18(2)	1.12(8-I-1)	-216(8-I-2)	29(9-II-2)	4(8-I-4)
2	23	0.34(8-I-2)	-0.50(8-II-2)	1.07(8-I-1)	-123(8-I-2)	50(8-I-3)	4(9-II-1)
2	24	-0.77(8-II-2)	-2.72(2)	1.36(8-I-1)	98(8-II-2)	38(9-II-2)	6(8-I-1)
2	25	0.51(2)	-0.42(2)	1.27(8-I-1)	77(8-II-2)	33(9-II-2)	5(8-I-3)
2	26	0.35(8-I-1)	-1.32(8-I-3)	-0.90(8-II-1)	-109(8-I-2)	60(9-II-2)	-14(8-I-2)
2	27	-0.58(8-I-3)	-1.14(2)	1.12(8-I-1)	-115(8-I-2)	28(8-I-3)	3(9-II-1)
2	28	-0.56(2)	-2.00(2)	1.31(8-I-1)	78(8-II-2)	17(8-I-3)	4(8-I-1)
2	29	0.28(2)	-0.61(2)	1.23(8-I-1)	46(8-II-2)	30(8-I-3)	3(9-II-1)
2	30	0.17(8-II-1)	-2.38(2)	1.35(8-I-1)	39(8-II-2)	14(9-II-2)	3(8-I-1)
2	31	2.35(2)	-5.61(2)	1.34(8-I-1)	60(8-I-3)	43(9-II-2)	-3(8-II-2)
2	32	-0.30(8-I-1)	-4.03(2)	1.37(8-I-1)	34(8-II-2)	41(9-II-2)	5(8-I-3)
2	33	0.38(8-II-1)	-4.00(2)	1.39(8-I-1)	35(8-II-2)	14(8-I-2)	4(8-I-1)
2	34	0.65(8-I-1)	-4.75(2)	-1.43(8-II-1)	56(8-I-3)	43(9-II-1)	0
2	35	-1.47(2)	-9.98(2)	-1.16(8-II-1)	25(8-I-1)	44(9-II-1)	-2(8-II-2)
2	36	-1.06(8-II-1)	-2.31(2)	-1.23(8-II-1)	34(8-I-2)	38(9-II-1)	-1(8-I-3)
2	37	0.57(8-II-1)	-1.89(2)	-1.33(8-II-1)	23(8-I-1)	40(9-II-1)	-1(9-II-2)
2	38	-1.10(8-I-1)	-2.39(2)	1.21(8-I-1)	-16(8-II-1)	38(9-II-1)	-2(8-I-3)
2	39	0.76(8-II-1)	-0.49(2)	-1.14(8-II-1)	17(8-I-1)	37(9-II-1)	-1(8-I-3)
2	40	1.70(2)	-5.27(2)	-1.19(8-II-1)	25(8-I-1)	17(8-II-2)	-2(8-II-2)
2	41	-0.59(2)	-6.53(2)	1.29(8-I-1)	24(8-II-2)	18(8-II-2)	3(8-I-1)
2	42	-0.74(8-I-1)	-3.57(2)	-1.39(8-II-1)	23(8-I-1)	14(8-II-2)	-1(9-II-3)
2	43	-0.45(2)	-5.66(2)	-1.32(8-II-1)	14(8-I-1)	17(8-II-2)	-1(8-II-1)
2	44	-1.06(2)	-2.62(2)	1.22(8-I-1)	17(8-I-1)	14(9-II-1)	-1(8-I-3)
2	45	0.44(8-II-1)	-1.53(2)	-1.30(8-II-1)	12(8-I-1)	14(9-II-1)	0
2	46	0.49(8-II-1)	-1.69(2)	1.33(8-I-1)	11(8-I-1)	15(9-II-1)	0

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
2	47	-2.08(8-II-1)	-2.72(2)	1.02(8-I-1)	-69(8-II-1)	53(9-II-1)	4(9-I-1)
2	48	2.58(8-I-2)	-4.50(2)	-1.41(2)	125(8-II-1)	-64(9-I-1)	-8(9-I-1)
2	49	-2.45(8-II-2)	-2.55(2)	-0.90(8-II-1)	68(9-II-2)	-68(9-I-1)	-5(9-I-1)
2	50	-0.90(8-I-2)	-12.30(2)	-1.24(8-II-1)	42(9-II-2)	-101(9-I-1)	-5(9-I-2)
2	51	2.52(8-II-1)	-10.92(2)	1.32(8-I-1)	-137(9-II-2)	-98(9-I-1)	7(9-I-1)
2	52	-0.96(8-I-1)	-3.91(2)	1.42(8-I-1)	-14(8-II-1)	63(9-II-1)	2(8-I-1)
2	53	-1.94(2)	-1.94(2)	0.75(8-I-1)	47(9-II-1)	42(9-II-1)	-3(9-I-1)
2	54	1.13(8-II-2)	-0.79(2)	-0.97(8-II-1)	24(9-II-2)	44(9-II-1)	-3(9-I-1)
2	55	-2.11(8-I-1)	-0.44(8-II-1)	1.25(8-I-1)	-51(9-I-1)	43(9-II-1)	-2(8-II-1)
2	56	1.34(8-I-2)	-0.58(8-I-1)	1.36(8-I-1)	-38(9-I-1)	38(9-II-1)	-3(8-II-1)
2	57	-1.92(8-I-1)	-2.48(8-I-1)	1.54(8-I-1)	-69(8-II-1)	42(9-II-1)	-2(9-II-2)
2	58	-1.25(8-I-1)	-1.21(8-I-1)	0.58(8-I-1)	979(8-I-1)	20(9-II-4)	17(8-II-1)
2	59	2.41(8-II-1)	-3.66(2)	1.40(8-I-1)	-119(8-II-1)	94(9-II-1)	-5(9-II-1)
2	60	-1.39(8-I-1)	-1.18(2)	1.96(8-I-1)	-61(9-I-1)	74(9-II-1)	-3(9-I-4)
2	61	-2.58(8-I-1)	-1.79(2)	-1.01(8-II-1)	181(8-I-1)	87(9-II-1)	9(8-I-1)
2	62	2.25(8-II-1)	-4.76(2)	-1.50(2)	-439(9-I-1)	88(9-II-1)	9(8-I-1)
2	63	-2.45(2)	-12.98(2)	-1.33(8-II-1)	-82(9-I-4)	130(9-II-1)	7(9-II-2)
2	64	0.47(8-II-1)	-0.80(8-I-1)	-0.78(8-II-1)	393(8-I-1)	35(8-I-1)	8(9-I-2)
2	65	-1.97(8-I-1)	-1.32(2)	-0.73(8-II-1)	516(8-I-1)	46(8-I-1)	5(9-I-1)
2	66	1.14(8-II-1)	-0.67(2)	-1.09(8-II-1)	-170(8-II-1)	47(9-II-1)	12(9-I-1)
2	67	-0.43(8-I-1)	-0.57(9-II-1)	-0.72(8-II-1)	-288(8-II-1)	11(9-II-1)	13(8-II-1)
2	68	-1.56(2)	-4.13(2)	-1.07(8-II-1)	-26(9-I-2)	46(9-II-1)	1(8-II-1)
2	69	1.16(8-II-1)	-3.64(2)	-1.28(8-II-1)	-19(9-I-1)	48(9-II-1)	1(8-II-4)
2	70	0.98(8-II-1)	-5.07(2)	1.38(8-I-1)	-14(8-II-1)	42(9-II-1)	-1(8-I-4)
2	71	0.80(8-II-1)	-2.04(2)	1.31(8-I-1)	-13(8-II-1)	40(9-II-1)	0
2	72	-0.92(8-I-1)	-3.61(2)	1.41(8-I-1)	-13(8-II-1)	14(9-II-1)	0
2	73	-1.49(8-I-1)	-6.66(2)	-1.26(8-II-1)	-19(9-I-1)	40(9-II-1)	0
2	74	-1.25(8-I-1)	-9.29(2)	1.22(8-I-1)	-12(8-II-3)	42(9-II-1)	-1(8-I-3)
2	75	-1.84(8-I-1)	-3.57(8-I-1)	1.38(8-I-1)	-34(9-I-1)	32(9-II-2)	-2(8-I-1)
2	76	1.71(8-II-1)	-1.03(2)	0.95(8-I-1)	-25(9-I-1)	35(9-II-1)	-1(8-I-3)
2	77	0.99(8-II-1)	0.65(2)	1.85(8-I-1)	-69(9-I-1)	13(9-II-1)	-2(9-I-1)
2	78	1.99(8-II-1)	-0.97(8-I-1)	1.91(8-I-1)	-73(9-I-1)	26(9-II-1)	-4(8-I-1)
2	79	0.75(8-II-1)	-4.08(2)	-1.38(8-II-1)	-12(8-II-3)	21(9-II-1)	-2(8-I-3)
2	80	-1.13(8-I-1)	-7.82(2)	-1.30(8-II-1)	-8(8-I-1)	14(9-II-1)	0
2	81	1.24(8-II-1)	-5.47(2)	1.35(8-I-1)	-12(8-II-3)	14(9-II-1)	0
2	82	-0.54(8-I-1)	-5.06(2)	1.40(8-I-1)	9(8-I-1)	14(9-II-1)	0
2	83	-3.04(8-I-1)	-3.58(2)	1.10(8-I-1)	-30(9-I-1)	26(8-I-4)	-2(9-II-2)
2	84	-1.06(8-I-1)	-2.69(2)	-1.26(8-II-1)	-7(8-I-1)	22(9-II-1)	-1(8-I-3)
2	85	-1.31(8-I-1)	-5.42(8-I-1)	1.32(8-I-1)	-8(9-I-1)	29(8-I-1)	-2(9-II-2)
2	86	3.18(2)	-6.17(2)	-1.26(8-II-1)	-75(9-I-4)	37(9-II-1)	3(8-I-1)
2	87	1.31(8-I-2)	-4.82(2)	1.51(8-I-1)	-85(8-II-1)	28(9-II-2)	4(9-II-4)
2	88	-0.92(2)	-3.39(2)	-1.11(8-II-1)	-210(8-II-1)	23(8-I-1)	4(8-I-1)
2	89	1.33(2)	-5.16(2)	-1.16(8-II-1)	-71(8-II-1)	28(8-I-1)	4(8-I-1)
2	90	-0.44(8-I-1)	-0.95(2)	-0.87(8-II-1)	-198(8-II-1)	20(9-II-1)	9(8-II-1)
2	91	0.88(2)	-0.71(8-I-1)	-1.06(8-II-1)	-120(8-II-1)	18(9-II-1)	3(9-I-2)
2	92	0.58(8-I-2)	-0.88(9-II-1)	0.90(8-I-1)	-153(8-II-1)	4(8-II-4)	-11(8-I-1)
2	93	-1.21(8-II-1)	-6.03(2)	-1.31(8-II-1)	-72(8-II-1)	26(8-I-1)	4(9-I-1)
2	94	-0.47(8-II-1)	-9.95(2)	-1.23(8-II-1)	-6(8-I-1)	40(8-I-1)	-4(8-II-1)
2	95	0.24(8-II-1)	-0.57(2)	-1.13(8-II-1)	-92(9-II-1)	24(8-II-1)	-8(8-I-1)
2	96	-0.59(8-II-1)	-2.12(2)	-1.25(8-II-1)	-117(8-II-1)	10(8-II-1)	4(9-I-2)
2	97	0.46(8-I-1)	-3.22(2)	-1.33(8-II-1)	-27(8-II-1)	12(8-II-1)	-4(9-II-1)
2	98	-0.13(8-II-1)	-0.92(8-II-1)	1.09(8-I-1)	-61(9-II-1)	13(9-I-1)	-9(8-I-1)
2	99	0.17(8-I-2)	-0.64(2)	-1.05(8-II-1)	-44(8-I-2)	38(8-I-3)	4(8-II-2)
2	100	-0.36(8-I-1)	-1.18(8-I-1)	-0.97(8-II-1)	-80(8-II-2)	41(8-I-3)	7(8-II-2)
2	101	0.31(8-I-1)	-1.77(8-I-3)	-0.94(8-II-1)	-17(8-II-2)	24(9-II-2)	8(9-II-1)
2	102	-0.43(8-I-1)	-1.15(2)	1.11(8-I-1)	-33(8-II-2)	15(8-I-2)	3(8-II-2)
2	103	-0.43(2)	-1.60(2)	1.25(8-I-1)	47(8-II-2)	14(8-I-2)	2(9-II-1)
2	104	0.13(2)	-0.80(2)	1.20(8-I-1)	24(8-II-3)	19(8-I-2)	2(8-II-2)
2	105	-0.23(8-I-1)	-3.07(2)	1.37(8-I-1)	40(8-II-2)	13(9-I-1)	2(8-I-1)
2	106	0.18(2)	-1.66(2)	1.30(8-I-1)	29(8-II-3)	13(8-I-2)	1(8-I-1)
2	107	-0.42(8-I-1)	-2.00(8-I-1)	-0.93(8-II-1)	-26(8-II-2)	3(9-II-2)	7(9-II-1)
2	108	-0.05(8-I-3)	-1.16(8-I-1)	-1.05(8-II-1)	-18(8-I-3)	13(9-I-3)	3(8-II-2)
2	109	0.27(8-I-1)	-1.24(8-I-1)	-1.00(8-II-1)	-5(9-II-2)	13(9-I-3)	6(9-II-1)
2	110	-0.33(8-I-1)	-1.24(2)	1.20(8-I-1)	24(8-II-3)	18(9-I-1)	2(8-II-2)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
2	111	-0.17(8-I-1)	-1.12(2)	1.11(8-I-1)	-18(9-II-2)	18(9-I-1)	2(8-II-2)
2	112	-0.29(8-I-1)	-2.33(2)	1.29(8-I-1)	29(8-II-3)	-35(9-II-2)	1(8-I-1)
2	113	0.15(8-II-1)	-1.35(2)	1.21(8-I-1)	21(9-I-2)	-29(9-II-1)	2(8-II-3)
2	114	-0.06(8-I-1)	-3.04(2)	1.28(8-I-1)	18(8-II-3)	-37(9-II-1)	1(9-II-2)
2	115	0.86(2)	-4.61(2)	1.30(8-I-1)	25(8-II-2)	15(9-I-1)	2(8-I-1)
2	116	-0.19(2)	-4.34(2)	1.34(8-I-1)	26(8-II-3)	-15(9-II-1)	2(8-I-1)
2	117	0.28(2)	-3.94(2)	1.32(8-I-1)	27(8-II-3)	-38(9-II-1)	1(8-II-1)
2	118	0.55(2)	-4.44(2)	-1.31(8-II-1)	14(8-I-1)	18(8-II-3)	-1(8-II-1)
2	119	-0.43(2)	-5.96(2)	1.22(8-I-1)	19(8-II-3)	-18(8-I-3)	2(8-I-1)
2	120	-0.65(2)	-3.13(2)	-1.31(8-II-1)	12(8-I-1)	17(8-II-3)	0
2	121	0.08(8-II-1)	-3.55(2)	-1.31(8-II-1)	11(8-II-3)	19(8-II-3)	-1(8-II-1)
2	122	-0.65(2)	-3.17(2)	1.36(8-I-1)	11(8-I-1)	14(8-II-3)	0
2	123	0.35(2)	-1.90(2)	1.27(8-I-1)	7(8-I-1)	16(8-II-3)	0
2	124	0.63(2)	-4.55(2)	1.22(8-I-1)	19(8-II-3)	-39(9-II-1)	1(8-I-1)
2	125	-0.22(2)	-5.06(2)	1.26(8-I-1)	15(8-II-3)	-39(9-II-1)	0
2	126	-0.10(8-I-1)	-3.82(2)	-1.28(8-II-1)	10(8-II-3)	-38(9-II-1)	-1(8-II-1)
2	127	-0.16(2)	-4.71(2)	-1.23(8-II-1)	11(8-II-3)	-39(9-II-1)	1(8-I-1)
2	128	-0.50(2)	-3.11(2)	1.25(8-I-1)	7(8-I-1)	-37(9-II-1)	0
2	129	0.14(2)	-2.81(2)	-1.23(8-II-1)	6(8-II-3)	-38(9-II-1)	0
2	130	0.16(2)	-2.81(2)	1.29(8-I-1)	3(8-I-1)	37(9-I-1)	0
2	131	0.35(8-I-1)	-1.33(8-I-1)	-1.02(8-II-1)	12(9-I-2)	-49(9-II-2)	2(9-II-1)
2	132	-0.32(8-I-1)	-2.36(8-I-1)	-0.94(8-II-1)	-5(8-II-2)	16(9-I-2)	5(9-II-1)
2	133	-0.37(8-I-1)	-1.64(8-I-1)	1.06(8-I-1)	-14(9-II-2)	-40(9-II-2)	2(9-II-1)
2	134	-0.22(2)	-1.68(2)	1.21(8-I-1)	20(9-I-2)	-65(9-II-2)	2(8-II-3)
2	135	0.10(2)	-1.07(2)	1.12(8-I-1)	-17(9-II-2)	-61(9-II-2)	2(8-II-3)
2	136	0.21(8-I-1)	-2.34(8-I-1)	-0.94(8-II-1)	-3(9-II-2)	-41(9-II-2)	2(9-II-1)
2	137	-0.43(8-I-1)	-2.68(8-I-1)	0.99(8-I-1)	-3(9-II-2)	-110(9-II-2)	1(9-II-1)
2	138	0.08(2)	-1.96(8-I-1)	0.69(8-I-1)	0	-89(9-II-2)	2(9-I-2)
2	139	-0.36(8-I-1)	-1.44(2)	1.10(8-I-1)	-17(9-II-2)	-103(9-II-2)	3(9-I-2)
2	140	0.08(2)	-1.20(2)	0.74(8-I-1)	0	-115(9-II-2)	1(9-I-2)
2	141	0.12(8-II-1)	-3.09(2)	1.26(8-I-1)	18(8-II-3)	-63(9-II-2)	1(9-I-2)
2	142	0.12(8-II-1)	-2.14(2)	1.14(8-I-1)	-11(9-II-2)	-62(9-II-2)	1(8-II-3)
2	143	-0.13(8-I-1)	-1.95(2)	1.10(8-I-1)	11(9-I-2)	-93(9-II-2)	1(8-II-3)
2	144	0.07(8-I-1)	-1.67(2)	0.78(8-I-1)	0	-94(9-II-2)	0
2	145	0.06(8-I-1)	-3.10(8-I-1)	0.78(8-I-1)	0	-90(9-II-2)	0
2	146	0.05(8-I-1)	-3.03(2)	0.79(8-I-1)	0	-90(9-II-2)	0
2	147	0.37(2)	-4.37(2)	1.24(8-I-1)	15(8-II-3)	-62(9-II-1)	0
2	148	0.04(8-I-1)	-4.05(2)	1.17(8-I-1)	6(8-II-3)	-62(9-II-2)	0
2	149	0.14(2)	-4.17(2)	1.14(8-I-1)	6(8-II-3)	-85(9-II-2)	0
2	150	0.27(2)	-4.26(2)	-1.20(8-II-1)	11(8-II-3)	-61(9-II-1)	0
2	151	-0.10(2)	-4.83(2)	1.17(8-I-1)	5(8-II-3)	-61(9-II-1)	0
2	152	-0.21(2)	-3.38(2)	-1.21(8-II-1)	6(8-II-3)	-61(9-II-1)	0
2	153	0.15(8-I-1)	-3.81(2)	1.15(8-I-1)	3(8-II-3)	-61(9-II-1)	0
2	154	0.24(2)	-4.47(2)	1.16(8-I-1)	5(8-II-3)	-83(9-II-1)	0
2	155	-0.07(8-II-1)	-4.42(2)	0.80(8-I-1)	0	-83(9-II-2)	0
2	156	0.13(8-II-1)	-3.89(2)	1.15(8-I-1)	3(8-II-3)	-83(9-II-1)	0
2	157	-0.07(8-II-1)	-4.35(2)	0.80(8-I-1)	0	-83(9-II-1)	0
2	158	-0.22(2)	-3.39(2)	1.27(8-I-1)	3(8-I-1)	-62(9-II-1)	0
2	159	0.09(8-I-1)	-2.86(2)	1.15(8-I-1)	2(8-II-1)	-62(9-II-1)	0
2	160	-0.16(2)	-3.16(2)	1.12(8-I-1)	1(8-II-3)	-83(9-II-1)	0
2	161	-0.07(8-II-1)	-3.42(2)	0.81(8-I-1)	0	-83(9-II-1)	0
2	162	-0.06(8-II-1)	-3.34(2)	0.81(8-I-1)	0	-86(9-II-1)	0
2	163	-0.06(8-II-1)	-3.28(2)	0.81(8-I-1)	0	-86(9-II-1)	0
2	164	0.32(8-II-1)	-4.51(2)	1.42(8-I-1)	9(8-I-1)	13(9-I-1)	0
2	165	0.08(2)	-3.50(2)	1.38(8-I-1)	6(8-I-1)	13(9-I-1)	0
2	166	-0.13(2)	-3.89(2)	1.35(8-I-1)	6(8-I-1)	36(9-I-1)	0
2	167	0.64(2)	-4.97(2)	-1.33(8-II-1)	-7(8-I-1)	8(9-I-1)	0
2	168	-0.54(2)	-6.42(2)	1.31(8-I-1)	5(8-II-1)	12(9-I-1)	0
2	169	-0.43(8-II-1)	-3.74(2)	1.07(8-I-1)	4(9-I-1)	10(8-I-1)	0
2	170	-0.47(8-I-1)	-3.72(2)	-1.19(8-II-1)	-6(8-II-3)	10(8-I-1)	-1(9-II-2)
2	171	0.42(8-II-1)	-4.33(2)	-1.28(8-II-1)	-3(8-I-1)	7(9-I-1)	0
2	172	-0.58(8-I-1)	-4.76(2)	0.91(8-I-1)	0	8(8-I-1)	-1(9-II-2)
2	173	0.57(2)	-4.85(2)	1.26(8-I-1)	5(8-I-1)	34(9-I-1)	0
2	174	-0.20(2)	-5.02(2)	1.31(8-I-1)	2(8-I-1)	36(9-I-1)	0

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
2	175	-0.49(8-II-1)	-4.61(2)	0.86(8-I-1)	0	18(9-I-1)	0
2	176	0.21(8-II-1)	-3.90(2)	0.96(8-I-1)	0	26(9-I-1)	0
2	177	-0.30(8-II-1)	-4.33(2)	-1.22(8-II-1)	3(8-I-1)	28(9-I-1)	0
2	178	-0.15(2)	-5.13(2)	-1.24(8-II-1)	2(8-II-1)	32(9-I-1)	0
2	179	0.25(8-II-1)	-9.09(2)	-1.11(8-II-1)	-16(8-II-1)	31(8-I-1)	-4(9-II-1)
2	180	-0.34(2)	-4.36(2)	-1.38(8-II-1)	-31(8-II-1)	23(9-I-1)	-4(9-II-1)
2	181	-0.27(8-II-1)	-5.90(2)	-1.17(8-II-1)	-3(9-II-1)	24(9-I-1)	-4(9-II-1)
2	182	-0.29(9-II-1)	-1.44(2)	-1.25(8-II-1)	-37(8-I-1)	12(8-II-1)	-7(8-I-1)
2	183	0.13(8-I-1)	-2.18(2)	-1.39(8-II-1)	-12(9-II-2)	19(9-I-4)	-4(8-I-1)
2	184	0.36(8-II-1)	-1.15(8-II-1)	-1.15(8-II-1)	-18(8-I-1)	6(9-I-1)	-7(8-I-1)
2	185	-0.23(8-I-1)	-7.69(2)	-0.98(8-II-1)	-5(9-II-1)	34(9-I-1)	-4(9-II-2)
2	186	-0.05(2)	-6.11(2)	-1.17(8-II-1)	-1(9-I-1)	31(9-I-1)	-3(9-II-2)
2	187	-0.25(2)	-3.64(2)	-1.43(8-II-1)	-14(9-II-2)	27(9-I-1)	-3(8-I-1)
2	188	0.18(8-I-1)	-4.70(2)	-1.27(8-II-1)	-4(8-I-1)	28(9-I-1)	-3(8-I-1)
2	189	-0.55(9-II-1)	-1.49(2)	-1.25(8-II-1)	-18(8-I-1)	12(9-I-4)	-6(8-I-1)
2	190	0.24(8-II-1)	-1.86(2)	-1.37(8-II-1)	-11(8-I-1)	21(9-I-1)	-3(8-I-1)
2	191	-0.29(8-I-1)	-1.58(8-II-1)	-1.15(8-II-1)	-12(9-I-1)	7(9-I-1)	-5(8-I-1)
2	192	0.23(2)	-4.47(2)	1.29(8-I-1)	3(8-I-1)	-59(9-II-1)	0
2	193	0.08(8-I-1)	-3.92(2)	1.20(8-I-1)	0	-61(9-II-1)	0
2	194	-0.17(8-II-1)	-4.13(2)	1.17(8-I-1)	1(8-I-1)	-84(9-II-1)	0
2	195	0.25(2)	-4.73(2)	-1.23(8-II-1)	2(8-II-1)	-57(9-II-1)	0
2	196	-0.13(2)	-5.12(2)	1.22(8-I-1)	0	-58(9-II-1)	0
2	197	0.04(8-I-1)	-4.42(2)	-1.18(8-II-1)	0	-57(9-II-1)	0
2	198	-0.14(8-II-1)	-4.36(2)	0.79(8-I-1)	1(8-I-3)	41(9-I-1)	0
2	199	-0.20(8-II-1)	-4.33(2)	0.99(8-I-1)	0	-58(9-II-1)	0
2	200	0.30(8-I-1)	-4.71(2)	1.20(8-I-1)	0	-83(9-II-1)	0
2	201	-0.08(2)	-4.49(2)	0.82(8-I-1)	0	-83(9-II-1)	0
2	202	0.24(8-I-1)	-4.64(2)	-1.16(8-II-1)	0	-83(9-II-1)	0
2	203	-0.09(8-II-1)	-4.86(2)	0.82(8-I-1)	0	-83(9-II-1)	0
2	204	0.46(8-II-1)	-5.21(8-II-1)	0.85(8-I-1)	0	-62(9-II-1)	0
2	205	0.55(8-I-1)	-5.10(8-II-1)	0.98(8-I-1)	0	-83(9-II-1)	0
2	206	-0.09(8-II-1)	-4.37(2)	0.80(8-I-1)	0	-83(9-II-1)	0
2	207	0.11(8-I-1)	-6.77(8-II-1)	0.74(8-I-1)	0	-83(9-II-1)	0
2	208	-0.57(8-II-1)	-5.85(2)	-1.05(8-II-1)	-8(9-II-2)	37(9-I-1)	-3(8-I-1)
2	209	0.12(2)	-7.74(2)	-0.89(8-II-1)	-3(9-II-1)	43(9-I-1)	-3(8-I-1)
2	210	0.37(8-II-1)	-5.18(2)	-1.17(8-II-1)	-2(8-I-1)	41(9-I-1)	-2(8-I-1)
2	211	-0.44(9-II-1)	-1.42(2)	-1.25(8-II-1)	-11(8-I-1)	31(9-I-1)	-4(8-I-1)
2	212	-0.32(8-II-1)	-2.32(2)	-1.35(8-II-1)	-9(8-I-1)	21(9-I-1)	-3(8-I-1)
2	213	-0.17(9-II-1)	-4.02(2)	-1.30(8-II-1)	-8(8-I-1)	36(9-I-1)	2(8-II-1)
2	214	0.28(8-II-1)	-1.55(8-II-1)	-1.11(8-II-1)	-12(9-I-1)	8(9-I-1)	-3(8-I-1)
2	215	-0.59(8-II-1)	-6.94(2)	-0.94(8-II-1)	-2(8-I-1)	51(9-I-1)	-2(8-I-1)
2	216	0.64(8-II-1)	-5.63(8-I-1)	-1.03(8-II-1)	0	54(9-I-1)	1(8-II-1)
2	217	0.10(8-II-1)	-7.92(8-I-1)	-0.74(8-II-1)	0	57(8-II-1)	0
2	218	0.13(8-II-1)	-3.50(2)	-1.23(8-II-1)	-4(8-I-1)	-55(9-II-1)	1(8-II-1)
2	219	0.07(8-II-1)	-5.17(2)	-0.81(8-II-1)	0	53(9-I-1)	0
2	220	-0.43(8-II-1)	-2.41(8-II-1)	-1.16(8-II-1)	-8(9-I-1)	-52(9-II-1)	2(8-II-1)
2	221	0.08(9-I-1)	-2.14(2)	-0.84(8-II-1)	0	-56(9-II-1)	0
2	222	0.12(8-I-1)	-1.03(8-II-1)	-0.76(8-II-1)	0	-32(9-II-1)	0
3	1	-1.65(8-I-2)	-0.34(9-II-3)	-1.01(8-II-2)	-206(8-II-2)	-1328(2)	77(2)
3	2	-1.16(8-I-2)	0.33(2)	-1.01(8-II-2)	113(8-I-2)	-1198(2)	53(8-II-1)
3	3	-0.89(2)	0.28(2)	0.98(8-I-2)	70(9-I-1)	-1202(2)	-60(8-I-1)
3	4	-1.07(8-II-1)	-0.40(8-I-4)	0.95(8-I-2)	-178(8-I-1)	-1332(2)	-99(2)
3	5	1.60(8-I-1)	-0.47(8-I-1)	0.88(2)	-363(2)	-1544(2)	-58(2)
3	6	1.80(2)	-0.61(8-I-1)	0.43(2)	-463(2)	-1697(2)	19(8-I-1)
3	7	1.82(2)	-0.63(8-I-1)	-0.61(8-I-1)	-450(2)	-1710(2)	25(8-I-1)
3	8	1.55(2)	-0.55(8-I-1)	-0.91(8-I-1)	-388(2)	-1611(2)	27(8-I-1)
3	9	1.24(2)	-0.46(8-I-1)	-1.09(8-I-1)	-327(2)	-1464(2)	31(8-I-1)
3	10	0.93(2)	-0.36(8-I-1)	-1.21(8-I-1)	-267(2)	-1283(2)	41(2)
3	11	0.53(2)	0.41(8-II-1)	-1.25(8-I-1)	-187(2)	-1061(2)	63(2)
3	12	-0.97(8-I-1)	0.79(2)	-1.19(8-I-1)	114(8-I-1)	-781(2)	94(2)
3	13	-1.66(8-I-1)	1.36(2)	-1.14(8-I-1)	181(8-I-1)	-650(2)	70(9-II-1)
3	14	-2.22(8-I-1)	2.65(2)	-0.93(8-I-1)	306(8-I-1)	-405(2)	127(2)
3	15	-1.35(8-I-1)	1.86(2)	-0.84(8-I-1)	327(8-I-1)	-171(8-II-2)	255(2)
3	16	-1.07(8-I-1)	1.21(2)	-0.74(8-I-1)	299(8-I-1)	81(8-I-2)	258(2)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
3	17	-0.92(8-I-4)	0.73(2)	0.75(8-II-1)	265(8-I-1)	116(2)	223(2)
3	18	-0.87(8-I-4)	0.23(8-II-1)	0.68(8-II-2)	210(8-I-1)	170(2)	164(2)
3	19	-0.82(8-I-4)	-0.31(8-II-1)	0.61(9-II-3)	-225(8-II-1)	180(2)	106(8-I-1)
3	20	-0.79(8-I-1)	-0.62(9-II-1)	0.55(9-II-3)	-255(8-II-4)	165(2)	69(8-I-1)
3	21	-0.76(8-I-1)	-0.88(9-II-1)	0.46(9-II-3)	-272(8-II-4)	167(9-II-1)	-69(8-II-1)
3	22	-0.74(8-I-1)	-1.04(9-II-1)	0.33(8-II-1)	-258(8-II-4)	165(9-II-1)	-80(8-II-1)
3	23	-0.72(8-I-1)	-0.96(9-II-1)	0.31(8-I-1)	-207(8-II-1)	-131(9-I-4)	-108(2)
3	24	-0.72(8-I-1)	-0.75(9-II-4)	0.36(8-I-1)	135(8-I-1)	-121(8-II-1)	-120(2)
3	25	-0.96(8-I-1)	0.60(8-II-1)	0.43(8-I-1)	128(8-I-1)	-140(8-II-1)	-62(2)
3	26	-0.55(8-I-1)	-0.52(9-II-4)	0.50(8-I-1)	53(8-I-1)	-280(2)	-96(9-I-1)
3	27	-0.49(8-II-1)	-0.43(9-II-4)	0.41(8-I-1)	49(8-II-1)	-389(2)	-90(9-I-1)
3	28	-0.64(8-II-1)	-0.32(9-II-4)	0.29(8-II-1)	80(8-II-1)	-456(2)	-61(9-I-1)
3	29	-0.56(9-II-1)	-0.23(9-II-4)	0.45(8-II-1)	58(8-II-1)	-511(2)	-44(8-II-4)
3	30	-0.75(8-I-1)	-0.17(9-II-4)	0.59(8-II-1)	76(8-I-1)	-585(2)	-39(8-II-4)
3	31	-0.92(8-I-1)	-0.14(9-II-1)	0.56(8-II-1)	-126(8-II-1)	-680(2)	-34(9-I-1)
3	32	-0.75(8-I-1)	-0.20(8-II-1)	0.47(8-II-1)	-147(8-II-1)	-744(2)	-28(9-I-1)
3	33	0.64(8-II-1)	-0.22(8-II-1)	0.43(8-II-1)	-170(2)	-776(2)	26(9-II-1)
3	34	0.60(8-II-1)	-0.22(8-II-1)	0.38(8-II-1)	-172(2)	-784(2)	27(9-II-1)
3	35	0.54(8-II-1)	-0.22(8-II-1)	-0.35(8-I-1)	-155(2)	-780(2)	29(9-II-1)
3	36	0.53(8-II-1)	-0.24(8-I-1)	-0.41(8-I-1)	-140(2)	-773(2)	31(9-II-1)
3	37	0.54(8-II-1)	-0.26(8-I-1)	-0.48(8-I-1)	-138(2)	-762(2)	36(9-II-1)
3	38	0.54(8-II-1)	-0.31(8-I-1)	-0.58(8-I-1)	-132(2)	-735(2)	45(9-II-1)
3	39	0.51(8-II-1)	-0.32(8-II-3)	-0.69(2)	-118(2)	-702(2)	58(9-II-1)
3	40	-0.55(8-I-1)	-0.36(8-I-1)	-0.85(2)	-83(8-II-3)	-638(2)	70(9-II-1)
3	41	-0.63(8-I-1)	-0.39(8-I-1)	-0.93(2)	-56(8-II-3)	-531(2)	87(2)
3	42	-0.66(8-I-1)	-0.49(8-II-1)	-0.94(8-I-1)	57(9-II-1)	-380(2)	107(2)
3	43	-0.66(8-I-1)	-0.64(8-II-1)	-0.96(8-II-1)	66(8-I-1)	-310(9-I-1)	118(2)
3	44	-0.69(2)	-1.28(9-II-1)	-0.91(8-II-1)	87(8-II-1)	-237(9-I-1)	97(2)
3	45	-0.59(8-I-1)	-1.04(8-II-1)	-1.07(9-II-1)	83(8-II-1)	-214(9-I-1)	152(2)
3	46	-0.81(8-I-4)	-0.80(8-II-1)	-1.35(9-II-1)	-114(8-I-1)	112(8-II-1)	176(2)
3	47	-1.02(8-I-4)	-1.67(9-I-2)	-1.27(8-I-1)	-254(9-II-2)	233(9-I-2)	160(2)
3	48	-1.07(8-I-4)	-1.98(9-I-2)	-1.23(8-I-1)	-392(9-II-2)	323(9-I-2)	137(9-I-2)
3	49	-1.07(8-I-1)	1.43(9-II-2)	-1.44(9-I-2)	-378(9-II-2)	-203(9-II-2)	123(9-I-2)
3	50	-1.12(8-I-1)	0.99(9-II-1)	-1.45(9-I-2)	-317(2)	-93(9-II-1)	-96(9-II-2)
3	51	-1.18(8-I-1)	1.13(9-II-1)	-1.40(9-I-2)	-226(2)	-96(9-II-1)	-108(8-II-2)
3	52	-1.21(8-I-1)	1.60(9-II-1)	-1.45(9-I-2)	-196(9-II-2)	-172(9-II-1)	-146(2)
3	53	-1.12(8-I-2)	2.29(2)	-1.55(9-I-2)	-177(9-II-1)	-263(9-II-1)	-179(2)
3	54	-0.79(8-I-2)	3.03(2)	-1.51(9-I-2)	143(8-II-4)	-341(2)	-181(2)
3	55	-0.62(2)	3.98(2)	1.19(9-II-2)	102(8-II-1)	-572(2)	-111(9-II-2)
3	56	-0.18(8-I-1)	2.40(2)	1.13(9-II-2)	-50(8-I-2)	-779(2)	-160(9-II-2)
3	57	-0.44(8-I-2)	1.62(2)	1.07(9-II-2)	-82(2)	-959(2)	-140(9-II-2)
3	58	-0.71(8-I-2)	1.12(2)	0.99(9-II-2)	-128(2)	-1144(2)	-118(9-II-2)
3	59	0.98(8-II-2)	0.77(2)	0.88(9-II-2)	-181(2)	-1318(2)	-99(9-II-2)
3	60	1.33(8-II-2)	0.61(8-I-2)	0.75(9-II-2)	-241(2)	-1470(2)	-83(9-II-2)
3	61	1.68(8-II-2)	0.53(8-I-2)	0.57(8-II-2)	-306(2)	-1594(2)	-69(9-II-2)
3	62	2.02(8-II-2)	-0.52(8-II-2)	-0.33(8-I-1)	-366(2)	-1673(2)	-57(9-II-2)
3	63	2.20(8-II-2)	-0.51(8-II-2)	-0.35(8-II-1)	-386(8-II-2)	-1646(2)	-43(9-II-2)
3	64	1.97(8-II-2)	0.40(8-I-2)	-0.72(8-II-1)	-374(8-II-2)	-1508(2)	43(9-I-2)
3	65	-0.47(8-I-1)	-0.14(8-II-1)	0.31(8-II-1)	-99(2)	-298(2)	34(8-II-1)
3	66	-0.48(8-I-1)	0.15(2)	0.25(8-II-1)	60(8-I-1)	133(2)	-40(8-I-1)
3	67	-0.46(8-I-1)	0.20(2)	-0.21(8-I-1)	76(8-I-1)	487(2)	-42(8-I-1)
3	68	-0.34(9-I-2)	-0.25(9-II-2)	-0.29(8-II-2)	91(8-II-1)	-215(2)	-84(8-I-1)
3	69	-0.36(8-I-2)	-0.18(9-II-3)	-0.16(8-II-1)	102(2)	438(2)	-59(8-I-1)
3	70	-0.43(8-I-1)	0.20(2)	-0.20(8-I-1)	96(2)	647(2)	-43(8-I-1)
3	71	-0.54(8-I-1)	-0.31(9-II-1)	0.22(8-II-1)	124(8-II-1)	258(2)	-78(9-I-1)
3	72	-0.43(8-II-1)	-0.33(9-II-1)	0.28(8-II-1)	103(8-II-1)	-102(8-II-1)	-84(9-I-1)
3	73	-0.63(8-I-1)	-0.51(9-II-4)	0.29(8-I-1)	87(8-I-1)	-109(8-II-4)	-142(2)
3	74	-0.48(8-I-1)	-0.43(9-II-4)	0.28(2)	78(8-II-1)	-97(8-II-1)	-122(9-I-1)
3	75	-0.59(8-I-1)	-0.42(9-II-4)	0.22(8-II-1)	107(2)	180(9-II-1)	-103(9-I-1)
3	76	-0.64(8-I-1)	-0.60(9-II-4)	0.25(8-II-1)	112(8-I-1)	156(9-II-1)	-109(2)
3	77	-0.50(8-I-1)	-0.19(9-II-3)	0.16(8-II-1)	122(2)	460(2)	-51(2)
3	78	-0.51(8-I-1)	-0.23(9-II-4)	0.23(8-II-1)	101(8-II-2)	225(2)	-68(8-II-1)
3	79	-0.52(8-I-1)	-0.17(9-II-4)	0.22(8-II-1)	88(8-I-1)	206(2)	-62(2)
3	80	-0.49(8-I-1)	0.19(2)	0.19(8-II-1)	86(8-I-1)	404(2)	-39(9-I-1)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
3	81	-0.47(8-I-1)	0.19(2)	-0.17(8-I-1)	95(8-II-1)	516(2)	-48(2)
3	82	-0.51(8-I-1)	0.16(2)	0.21(8-II-1)	90(8-I-1)	275(2)	-54(2)
3	83	-0.47(8-I-1)	-0.25(9-II-4)	0.31(8-II-1)	78(8-II-2)	-132(8-II-1)	-68(8-II-1)
3	84	-0.52(8-I-1)	0.15(2)	0.26(8-II-1)	72(8-I-1)	112(9-II-1)	-45(9-I-1)
3	85	-0.55(8-I-1)	-0.12(8-II-1)	0.34(8-II-1)	-102(8-II-1)	-313(2)	-39(9-I-1)
3	86	-0.68(8-I-1)	-0.14(9-II-4)	0.38(8-II-1)	103(8-I-1)	-344(2)	-55(2)
3	87	-0.55(8-I-1)	-0.15(9-II-4)	0.29(8-II-1)	93(8-I-1)	-105(9-I-1)	-67(2)
3	88	-0.60(8-I-1)	-0.17(9-II-4)	0.35(8-II-1)	92(8-I-1)	-234(2)	-65(8-II-1)
3	89	-0.55(8-I-1)	0.13(2)	0.27(8-II-1)	89(8-I-1)	87(9-II-1)	-57(2)
3	90	-0.64(8-I-1)	-0.12(9-II-4)	0.37(8-II-1)	-104(8-II-1)	-332(2)	-48(9-I-1)
3	91	-0.27(8-I-1)	0.20(2)	-0.20(9-II-1)	121(8-II-1)	460(2)	-36(2)
3	92	-0.41(8-I-1)	0.22(2)	-0.18(8-I-1)	107(8-II-1)	643(2)	-32(2)
3	93	-0.49(8-I-1)	0.22(2)	-0.14(8-I-1)	132(8-II-1)	554(2)	-34(8-II-1)
3	94	-0.40(8-I-1)	0.24(2)	-0.17(9-II-1)	135(8-II-1)	617(2)	25(8-I-1)
3	95	-0.42(8-I-1)	0.24(2)	-0.17(9-II-1)	142(8-II-1)	573(2)	58(8-I-1)
3	96	-0.30(8-I-1)	0.25(2)	-0.23(9-II-1)	126(8-II-1)	460(2)	77(2)
3	97	-0.27(8-I-1)	0.25(2)	-0.22(9-II-1)	130(8-II-1)	477(2)	31(8-I-1)
3	98	0.68(8-I-1)	-0.25(9-II-1)	0.20(2)	-262(8-I-1)	-679(2)	-62(2)
3	99	0.33(2)	-0.21(9-II-3)	-0.22(9-II-1)	-137(8-I-1)	40(8-II-1)	-47(2)
3	100	-0.43(8-II-1)	-0.23(9-II-1)	-0.26(8-II-2)	143(8-II-1)	-393(2)	-112(2)
3	101	0.37(2)	0.23(2)	-0.30(9-II-1)	97(8-II-1)	158(2)	97(2)
3	102	0.41(2)	0.23(2)	-0.26(9-II-1)	-135(8-I-1)	81(2)	45(8-I-1)
3	103	0.71(2)	-0.26(9-II-1)	-0.41(9-II-1)	-182(2)	-306(2)	103(2)
3	104	1.13(2)	-0.38(8-I-4)	-0.62(8-I-1)	-291(2)	-916(2)	81(2)
3	105	1.25(2)	-0.37(8-I-4)	-0.42(9-II-1)	-347(2)	-1009(2)	60(8-I-1)
3	106	0.74(2)	-0.26(9-II-1)	-0.32(9-II-1)	-221(2)	-424(2)	62(8-I-1)
3	107	1.08(2)	-0.36(8-I-4)	-0.24(9-II-1)	-320(2)	-851(2)	-33(8-II-1)
3	108	-0.68(8-I-1)	-0.65(9-II-1)	0.24(8-II-1)	127(8-I-4)	206(9-II-1)	-61(8-II-1)
3	109	-0.69(8-I-1)	-0.60(9-II-1)	0.27(9-II-3)	137(8-I-4)	251(2)	53(8-I-1)
3	110	-0.68(8-I-1)	-0.47(9-II-1)	0.30(9-II-3)	145(8-I-4)	285(2)	106(2)
3	111	-0.56(8-I-1)	-0.29(9-II-1)	0.15(8-II-1)	147(2)	445(2)	-47(9-I-1)
3	112	-0.62(8-I-1)	-0.42(9-II-1)	0.19(8-II-1)	125(2)	307(2)	-58(9-I-1)
3	113	-0.62(8-I-1)	-0.42(9-II-1)	0.17(8-II-1)	129(9-II-4)	373(2)	67(8-I-1)
3	114	-0.58(8-I-1)	-0.37(9-II-1)	-0.20(8-I-1)	131(9-II-4)	383(2)	135(2)
3	115	-0.50(8-I-1)	-0.30(9-II-1)	-0.19(8-I-1)	119(9-II-3)	453(2)	127(2)
3	116	-0.53(8-I-1)	-0.31(9-II-1)	-0.14(8-I-1)	127(2)	479(2)	73(8-I-1)
3	117	-0.45(8-I-1)	-0.25(9-II-1)	-0.17(8-I-1)	132(8-II-2)	522(2)	88(2)
3	118	0.92(2)	-0.35(8-I-4)	-0.77(8-I-1)	-234(2)	-789(2)	109(2)
3	119	-0.35(8-I-1)	0.25(2)	-0.24(9-II-1)	112(8-II-2)	428(2)	132(2)
3	120	0.28(2)	0.23(2)	-0.34(9-II-1)	79(8-II-1)	186(2)	155(2)
3	121	0.59(2)	-0.26(9-II-1)	-0.51(8-I-1)	-135(2)	-226(2)	149(2)
3	122	-0.44(8-I-1)	-0.27(9-II-1)	-0.26(8-I-1)	100(9-II-3)	387(2)	178(2)
3	123	-0.54(8-I-1)	-0.29(9-II-1)	-0.28(8-I-1)	124(9-II-1)	340(2)	204(2)
3	124	-0.67(8-I-4)	-0.30(9-II-1)	0.34(8-II-2)	158(8-I-4)	278(2)	179(2)
3	125	0.67(2)	-0.31(8-I-1)	-0.85(8-I-1)	-178(2)	-639(2)	138(2)
3	126	-0.34(8-I-1)	0.25(9-I-1)	-0.37(8-I-1)	68(9-II-3)	204(2)	204(2)
3	127	0.40(2)	0.26(8-II-4)	-0.57(8-I-1)	-87(2)	-139(2)	190(2)
3	128	-0.68(8-I-1)	0.52(2)	-0.59(8-I-1)	122(8-I-1)	44(9-I-3)	245(2)
3	129	-0.92(8-I-1)	0.62(2)	-0.78(8-I-1)	111(8-I-1)	-281(2)	199(2)
3	130	-0.85(8-I-1)	0.85(8-II-1)	-0.64(8-I-1)	187(8-I-1)	60(8-I-2)	255(2)
3	131	-0.48(8-I-1)	0.35(8-II-1)	-0.58(8-I-1)	63(9-II-1)	-61(2)	223(2)
3	132	-0.48(8-I-1)	0.39(8-II-1)	-0.86(8-I-1)	-117(2)	-482(2)	167(2)
3	133	-0.70(8-I-4)	0.28(8-II-1)	0.41(8-II-1)	177(8-I-1)	219(2)	223(2)
3	134	-0.65(8-I-1)	0.38(8-II-1)	-0.43(8-I-1)	148(8-I-1)	176(2)	249(2)
3	135	-0.76(8-I-1)	0.52(8-II-1)	-0.49(8-I-1)	205(8-I-1)	136(2)	250(2)
3	136	-0.50(8-I-1)	0.28(9-I-1)	-0.40(8-I-1)	103(9-II-1)	210(2)	239(2)
3	137	-0.66(8-I-2)	-0.20(9-II-2)	-0.30(8-II-2)	133(8-I-2)	-212(2)	69(8-II-1)
3	138	-0.50(8-I-2)	0.16(2)	-0.14(8-II-1)	125(2)	432(2)	-53(8-I-1)
3	139	-0.47(8-I-2)	0.22(2)	-0.20(8-I-1)	111(2)	646(2)	45(8-II-1)
3	140	0.44(8-II-1)	-0.16(8-II-1)	-0.31(8-I-1)	-84(2)	-294(2)	40(8-II-1)
3	141	-0.47(8-I-1)	0.21(2)	-0.25(8-I-1)	84(8-I-1)	495(2)	50(8-II-1)
3	142	-0.46(8-I-1)	0.15(2)	-0.28(8-I-1)	59(8-I-1)	148(2)	50(8-II-1)
3	143	-0.50(8-I-1)	0.23(2)	-0.29(8-I-1)	107(8-I-1)	475(2)	62(8-II-1)
3	144	-0.56(8-I-1)	0.26(2)	-0.38(8-I-1)	129(8-I-1)	396(2)	79(8-II-1)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
3	145	-0.48(8-I-1)	-0.24(9-I-2)	-0.53(8-I-1)	-71(8-II-1)	-238(2)	77(2)
3	146	-0.50(8-I-1)	-0.16(9-I-2)	-0.44(8-I-1)	77(8-I-1)	101(9-II-1)	70(8-II-1)
3	147	-0.44(8-I-1)	-0.20(8-II-3)	-0.45(8-I-1)	-84(8-II-1)	-330(2)	49(8-II-1)
3	148	0.43(8-II-1)	-0.18(8-I-1)	-0.38(8-I-1)	-79(8-II-1)	-303(2)	44(8-II-1)
3	149	-0.47(8-I-1)	0.15(2)	-0.35(8-I-1)	69(8-I-1)	135(2)	59(8-II-1)
3	150	-0.71(8-I-4)	-0.59(8-II-1)	-0.91(8-I-1)	81(2)	-175(9-I-1)	190(2)
3	151	-0.76(8-I-1)	-0.53(8-II-3)	-0.88(8-I-1)	97(2)	99(2)	207(2)
3	152	-0.64(8-I-1)	0.23(2)	-0.51(8-I-1)	149(8-I-1)	302(2)	122(2)
3	153	-0.72(8-I-1)	-0.36(8-II-3)	-0.69(8-I-1)	150(2)	185(2)	176(2)
3	154	-0.65(8-I-1)	-0.44(8-I-1)	-0.82(8-I-1)	85(8-I-1)	-200(9-I-1)	177(2)
3	155	-0.66(8-I-1)	-0.36(8-II-3)	-0.72(8-I-1)	104(8-I-1)	-92(9-I-1)	184(2)
3	156	-0.61(8-I-1)	-0.37(8-II-3)	-0.79(8-I-1)	70(8-I-4)	-269(2)	147(2)
3	157	-0.57(8-I-1)	-0.31(8-II-3)	-0.72(8-I-1)	-63(8-II-4)	-312(2)	121(2)
3	158	-0.58(8-I-1)	-0.27(8-II-3)	-0.63(8-I-1)	95(8-I-1)	-90(9-I-1)	143(2)
3	159	-0.53(8-I-1)	-0.27(9-I-2)	-0.60(8-I-1)	-68(8-II-1)	-230(2)	91(2)
3	160	-0.54(8-I-2)	0.28(2)	-0.22(8-I-1)	143(8-I-1)	635(2)	51(8-II-1)
3	161	-0.63(8-I-2)	0.35(2)	-0.27(8-I-1)	180(8-I-1)	600(2)	58(8-II-1)
3	162	-0.63(8-I-2)	0.28(2)	0.15(8-I-1)	171(8-I-2)	453(2)	43(8-II-1)
3	163	-0.71(8-I-2)	0.40(2)	-0.20(8-II-1)	201(8-I-2)	482(2)	-55(9-II-2)
3	164	-1.00(8-I-2)	0.26(2)	-0.32(8-II-1)	197(8-I-2)	-390(2)	82(2)
3	165	-0.83(8-I-2)	0.32(2)	-0.20(8-II-1)	191(8-I-2)	55(9-I-1)	44(9-I-2)
3	166	-1.19(8-I-2)	0.35(2)	-0.34(8-II-1)	-284(8-II-2)	-664(2)	53(9-I-2)
3	167	1.53(8-II-2)	0.40(2)	-0.27(8-I-1)	-295(8-II-2)	-1020(2)	-95(9-II-2)
3	168	1.47(8-II-2)	0.36(2)	-0.27(8-II-1)	-309(8-II-2)	-833(2)	-62(9-II-2)
3	169	1.09(8-II-2)	0.46(2)	-0.24(8-II-1)	-243(8-II-2)	-452(2)	-101(9-II-2)
3	170	-0.86(8-I-2)	0.45(2)	-0.20(8-II-1)	191(8-I-2)	94(9-I-1)	-85(9-II-2)
3	171	-0.93(8-I-2)	0.64(9-II-1)	-0.54(8-I-1)	182(8-I-2)	305(2)	-153(9-II-2)
3	172	-0.83(8-I-1)	0.44(9-II-2)	-0.65(8-I-1)	180(2)	313(2)	123(8-I-1)
3	173	-0.91(8-I-2)	0.58(9-II-2)	-0.60(8-I-1)	182(8-I-2)	340(2)	-90(9-II-2)
3	174	-0.83(8-I-2)	0.46(2)	-0.43(8-I-1)	216(8-I-2)	456(2)	-74(8-II-1)
3	175	-0.75(8-I-2)	0.41(2)	-0.34(8-I-1)	213(8-I-1)	547(2)	68(8-I-1)
3	176	-0.74(8-I-2)	0.35(2)	-0.46(8-I-1)	195(8-I-1)	452(2)	96(8-I-1)
3	177	-0.86(8-I-2)	0.58(2)	-0.38(8-I-1)	212(8-I-2)	375(2)	-136(9-II-2)
3	178	-0.79(8-I-2)	0.52(2)	-0.26(8-I-1)	213(8-I-2)	433(2)	-101(9-II-2)
3	179	-0.88(8-I-1)	-0.76(9-I-2)	-0.90(8-I-1)	93(8-I-2)	247(9-I-2)	147(8-I-1)
3	180	-1.02(8-I-2)	0.88(9-II-1)	-0.73(8-I-1)	131(9-I-2)	208(2)	-159(9-II-2)
3	181	-1.10(8-I-1)	1.04(9-II-1)	-1.05(9-I-2)	-175(9-II-2)	141(9-I-1)	-144(9-II-2)
3	182	-1.00(8-I-1)	0.82(9-II-2)	-0.81(8-I-1)	124(9-I-2)	260(9-I-2)	-116(9-II-2)
3	183	-0.97(8-I-1)	1.10(9-II-2)	-0.95(8-I-1)	-122(9-II-2)	298(9-I-2)	131(9-I-2)
3	184	-1.05(8-I-1)	1.18(9-II-2)	-1.02(8-I-1)	-192(9-II-2)	218(9-I-2)	-134(9-II-2)
3	185	1.35(8-II-2)	0.45(8-I-2)	0.38(9-II-2)	-240(8-II-2)	-960(2)	-120(9-II-2)
3	186	0.87(8-II-2)	0.76(2)	0.69(9-II-2)	-140(8-II-2)	-797(2)	-161(9-II-2)
3	187	1.12(8-II-2)	0.56(2)	0.55(9-II-2)	-188(8-II-2)	-885(2)	-142(9-II-2)
3	188	1.01(8-II-2)	0.52(2)	-0.27(9-I-2)	-198(8-II-2)	-372(2)	-142(9-II-2)
3	189	-0.90(8-I-2)	0.61(2)	0.40(9-II-2)	-157(8-II-2)	-366(2)	-171(9-II-2)
3	190	-0.83(8-I-2)	0.76(2)	0.54(9-II-2)	121(8-I-2)	-353(2)	-196(2)
3	191	-0.86(8-I-2)	0.55(2)	-0.25(8-II-1)	192(8-I-2)	120(2)	-137(9-II-2)
3	192	-0.84(8-I-2)	0.75(2)	0.44(9-II-2)	153(8-I-2)	-75(9-II-1)	-205(2)
3	193	-0.87(8-I-2)	0.61(2)	-0.34(9-I-2)	181(8-I-2)	92(9-I-1)	-171(9-II-2)
3	194	-0.86(8-I-2)	0.68(2)	-0.38(9-I-2)	188(8-I-2)	199(2)	-177(9-II-2)
3	195	-1.10(8-I-2)	1.11(9-II-1)	-1.08(9-I-2)	-132(9-II-2)	127(9-I-1)	-166(2)
3	196	-0.92(8-I-2)	0.79(2)	-0.52(9-I-2)	160(8-I-2)	191(2)	-197(2)
3	197	-1.01(8-I-2)	0.95(9-II-1)	-0.76(9-I-2)	111(9-I-2)	160(9-I-1)	-200(2)
3	198	-0.76(8-I-2)	1.00(2)	0.64(9-II-2)	96(8-I-2)	-296(2)	-220(2)
3	199	-0.85(8-I-2)	0.92(2)	-0.54(9-I-2)	130(8-I-2)	90(9-I-1)	-230(2)
3	200	-0.70(8-I-2)	1.06(2)	0.79(9-II-2)	-92(8-II-2)	-680(2)	-180(9-II-2)
3	201	-0.91(8-I-2)	1.13(2)	-0.75(9-I-2)	82(8-I-2)	114(9-I-1)	-237(2)
3	202	-1.04(8-I-2)	1.36(2)	-1.07(9-I-2)	-85(9-II-2)	-138(9-II-1)	-208(2)
3	203	-0.76(8-I-2)	1.34(2)	0.73(9-II-2)	57(8-I-2)	-225(2)	-232(2)
3	204	-0.58(8-I-2)	1.50(2)	0.86(9-II-2)	-41(8-II-2)	-546(2)	-195(9-II-2)
3	205	-0.86(8-I-2)	1.79(2)	-1.01(9-I-2)	-46(9-II-2)	-217(9-II-1)	-219(2)
3	206	-0.60(8-I-2)	2.21(2)	0.93(9-II-2)	-27(9-II-1)	-428(2)	-191(9-II-2)
3	1	18.30(2)	-15.05(2)	0.68(8-I-1)	0	306(2)	28(8-II-2)
3	2	0.29(8-II-1)	-4.46(2)	1.35(8-I-1)	0	313(2)	-35(2)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
3	3	-1.50(2)	0.97(8-I-1)	1.16(8-I-1)	0	240(2)	-19(2)
3	4	4.59(2)	-8.82(2)	-1.33(8-II-1)	1(2)	436(2)	31(2)
3	5	-2.79(2)	-13.64(2)	1.37(8-I-1)	144(2)	606(2)	-9(2)
3	6	1.32(2)	-4.65(2)	-1.11(8-II-1)	-520(8-II-2)	137(2)	-13(8-I-2)
3	7	-0.62(9-I-2)	-2.99(2)	-1.09(8-II-1)	0	135(2)	-12(2)
3	8	1.24(2)	-4.05(2)	-1.28(8-II-1)	-286(8-II-2)	133(2)	-14(8-I-2)
3	9	-0.76(2)	-2.15(2)	1.13(8-I-1)	36(8-I-2)	157(2)	-15(2)
3	10	1.94(2)	-0.24(8-II-1)	-1.29(8-II-1)	160(8-I-2)	137(2)	-11(2)
3	11	3.85(2)	-5.93(2)	0.94(8-I-1)	-419(8-II-2)	45(2)	-3(9-I-1)
3	12	2.29(2)	-4.30(2)	-1.20(8-II-1)	-297(8-II-2)	55(8-I-3)	-7(2)
3	13	-1.05(8-II-2)	-4.41(2)	1.01(8-I-1)	-407(8-II-2)	45(8-I-3)	-4(9-I-1)
3	14	2.41(2)	-6.51(2)	1.44(8-I-1)	148(2)	238(2)	-7(2)
3	15	1.74(2)	-3.30(2)	1.50(8-I-1)	135(2)	224(2)	-5(2)
3	16	-0.55(8-II-2)	-10.28(2)	-1.35(8-II-1)	175(2)	260(2)	-4(2)
3	17	-3.23(2)	-1.27(8-I-1)	1.04(8-I-1)	0	157(2)	14(2)
3	18	-2.58(2)	-2.30(2)	-1.04(8-II-1)	0	184(2)	21(2)
3	19	0.53(2)	-2.31(2)	-1.47(8-II-1)	88(2)	275(2)	8(2)
3	20	-0.70(2)	-4.49(2)	-1.40(8-II-1)	78(2)	211(2)	5(2)
3	21	1.24(2)	-2.61(8-I-1)	-2.05(8-II-1)	0	-48(9-I-2)	2(2)
3	22	11.06(2)	-5.85(2)	-2.21(8-II-1)	0	-48(9-I-2)	4(9-II-2)
3	23	-0.43(2)	-1.16(2)	-2.68(8-II-1)	-33(2)	-29(9-I-2)	3(2)
3	24	-1.39(2)	-2.50(2)	1.40(8-I-1)	-22(2)	109(2)	10(2)
3	25	2.74(2)	-1.30(2)	1.35(8-I-1)	104(2)	183(2)	-2(8-II-2)
3	26	-2.98(2)	-6.15(2)	2.84(2)	0	45(2)	10(2)
3	27	-5.70(2)	-1.21(8-II-1)	1.92(2)	0	44(2)	12(2)
3	28	3.07(2)	-1.06(2)	1.91(8-I-1)	24(2)	93(2)	5(2)
3	29	-4.65(2)	-27.52(2)	2.12(8-I-1)	-31(2)	-81(9-I-2)	4(2)
3	30	10.24(2)	-13.25(2)	4.10(2)	-1(2)	-59(9-I-2)	10(2)
3	31	2.36(2)	-4.52(2)	3.89(2)	-31(2)	44(9-II-2)	6(2)
3	32	0.77(8-II-2)	-9.35(2)	3.49(2)	-23(2)	54(2)	3(2)
3	33	7.95(2)	-6.09(2)	2.04(8-I-1)	-39(2)	37(9-II-2)	3(2)
3	34	-3.02(2)	-17.34(2)	2.67(8-I-1)	-17(8-I-2)	42(9-II-2)	1(8-I-2)
3	35	1.34(2)	-0.32(2)	-2.53(8-II-1)	-33(2)	30(9-II-2)	3(2)
3	36	-1.96(2)	-7.90(2)	-2.17(8-II-1)	-31(2)	34(9-II-2)	2(2)
3	37	1.14(8-I-2)	-3.77(2)	-0.95(8-II-1)	-372(8-II-2)	14(9-II-2)	6(8-I-3)
3	38	-0.69(8-I-2)	-3.06(2)	-1.24(8-II-1)	137(8-I-2)	85(2)	-6(2)
3	39	0.86(8-I-2)	-2.27(2)	-1.24(8-II-1)	-214(8-II-2)	80(8-I-3)	-4(9-I-1)
3	40	0.79(8-II-2)	-3.42(2)	-1.30(8-II-1)	-204(8-II-2)	61(8-I-3)	-3(9-I-2)
3	41	0.40(8-I-2)	-3.98(2)	-1.17(8-II-1)	-301(8-II-2)	47(8-I-3)	6(8-I-3)
3	42	0.83(2)	-3.86(2)	1.50(8-I-1)	130(2)	120(2)	-3(2)
3	43	1.17(2)	-1.53(2)	1.38(8-I-1)	126(8-I-2)	115(2)	-2(9-I-1)
3	44	2.28(2)	-5.71(2)	1.35(8-I-1)	175(2)	127(2)	-4(2)
3	45	0.55(8-I-2)	-6.90(2)	1.49(8-I-1)	136(2)	122(2)	-2(2)
3	46	-0.73(8-I-2)	-3.23(2)	1.39(8-I-1)	125(8-I-2)	67(8-I-3)	2(9-II-1)
3	47	0.55(2)	-2.36(2)	-1.35(8-II-1)	134(8-I-2)	67(8-I-3)	3(9-II-1)
3	48	0.43(8-II-2)	-3.39(2)	-1.09(8-II-1)	-200(8-II-2)	-39(9-I-2)	11(8-I-3)
3	49	-0.85(8-I-2)	-3.26(2)	-1.46(8-II-1)	130(8-I-2)	40(8-I-3)	3(2)
3	50	1.47(2)	-4.72(2)	1.49(8-I-1)	129(2)	63(2)	-1(9-I-1)
3	51	0.56(8-II-2)	-3.75(2)	1.47(8-I-1)	96(8-I-2)	63(8-I-3)	2(8-II-2)
3	52	0.67(8-II-2)	-5.96(2)	1.48(8-I-1)	98(2)	56(2)	-2(8-I-2)
3	53	1.44(8-II-2)	-5.69(2)	-1.47(8-II-1)	87(2)	56(2)	-2(2)
3	54	0.83(8-II-2)	-3.64(2)	1.56(8-I-1)	93(8-I-2)	38(8-I-3)	3(2)
3	55	-0.21(8-I-2)	-2.86(2)	-1.54(8-II-1)	84(8-I-2)	38(8-I-3)	4(2)
3	56	1.26(8-II-2)	-4.73(2)	1.62(8-I-1)	83(2)	33(8-I-3)	1(8-II-2)
3	57	-0.79(8-I-2)	-4.33(2)	1.65(8-I-1)	63(8-I-2)	33(8-I-3)	2(8-II-3)
3	58	-1.01(8-I-2)	-5.19(2)	-1.61(8-II-1)	90(2)	38(2)	-2(2)
3	59	-1.42(8-I-2)	-5.86(2)	1.67(8-I-1)	50(2)	32(8-I-3)	-1(8-I-3)
3	60	-0.77(2)	-4.50(2)	1.38(8-I-1)	89(2)	121(2)	-4(2)
3	61	1.35(2)	-5.29(2)	-1.35(8-II-1)	122(2)	125(2)	-5(2)
3	62	0.73(8-II-2)	-5.35(2)	-1.38(8-II-1)	125(2)	77(2)	-5(2)
3	63	3.17(2)	-2.67(2)	2.64(2)	16(2)	77(2)	-1(8-II-2)
3	64	-1.99(2)	-6.49(2)	1.93(8-I-1)	-16(2)	88(2)	2(8-I-2)
3	65	3.25(2)	-1.34(2)	1.65(8-I-1)	70(2)	120(2)	-4(2)
3	66	-1.27(2)	-6.44(2)	1.62(8-I-1)	67(2)	86(2)	-5(2)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
3	67	2.19(2)	-3.31(2)	1.49(8-I-1)	75(2)	81(2)	-5(2)
3	68	-1.69(2)	-11.81(2)	2.63(2)	13(8-II-3)	71(2)	-3(2)
3	69	4.18(2)	-3.47(2)	1.81(8-I-1)	48(2)	86(2)	-6(2)
3	70	5.40(2)	-6.71(2)	2.64(8-I-1)	-18(2)	41(2)	-1(9-II-3)
3	71	2.25(2)	-10.63(2)	3.07(2)	26(2)	62(2)	-5(2)
3	72	4.76(2)	0.61(2)	-2.05(8-II-1)	-32(2)	18(2)	2(9-I-3)
3	73	-3.11(2)	-9.79(2)	2.38(8-I-1)	13(8-II-1)	33(2)	-2(9-II-2)
3	74	-0.69(2)	-2.37(2)	-2.27(8-II-1)	-14(9-I-3)	19(9-II-1)	2(2)
3	75	-1.43(8-I-2)	-5.80(2)	1.58(8-I-1)	79(2)	57(2)	-5(2)
3	76	-1.94(8-I-2)	-4.57(2)	1.68(8-I-1)	44(2)	40(2)	-2(2)
3	77	-1.94(8-I-2)	-10.33(2)	1.78(8-I-1)	47(2)	70(2)	-6(2)
3	78	2.67(8-II-2)	-4.47(2)	1.80(8-I-1)	32(2)	61(2)	-4(2)
3	79	2.43(8-II-2)	-13.36(2)	2.90(2)	21(2)	61(2)	-6(2)
3	80	4.70(8-II-2)	-10.40(2)	1.91(8-I-1)	31(2)	67(2)	-7(2)
3	81	7.26(2)	2.50(2)	2.13(8-I-1)	13(8-II-1)	-1(9-I-1)	-3(2)
3	82	6.40(8-II-2)	-7.55(2)	2.69(8-I-1)	66(2)	37(2)	-10(2)
3	83	4.35(2)	0.93(2)	-1.98(8-II-2)	-14(9-I-3)	3(2)	1(2)
3	84	5.25(2)	-2.93(2)	-1.43(8-II-1)	64(2)	8(2)	-1(9-II-2)
3	85	-0.72(2)	0.14(8-II-1)	-2.04(8-II-1)	0	28(9-II-2)	1(2)
3	86	-2.57(2)	-2.31(8-II-2)	-1.86(8-II-1)	0	30(9-II-2)	1(9-I-1)
3	87	0.32(2)	0.30(8-II-1)	-2.63(8-II-1)	-22(2)	26(9-II-2)	2(2)
3	88	4.86(2)	-6.65(2)	1.48(8-I-1)	0	39(9-II-2)	4(9-I-1)
3	89	-3.28(2)	-5.46(2)	-1.34(8-II-1)	0	39(9-II-2)	2(9-I-1)
3	90	1.52(2)	-1.27(2)	-2.04(8-II-1)	-6(8-II-2)	30(9-II-2)	0
3	91	-4.14(2)	-2.29(2)	-1.42(8-II-1)	0	34(9-II-2)	4(2)
3	92	0.38(8-I-1)	-0.68(8-II-2)	-2.52(8-II-1)	-22(2)	30(9-II-1)	2(2)
3	93	-0.24(8-II-3)	-0.15(2)	-2.62(8-II-1)	-29(2)	29(9-II-1)	3(2)
3	94	1.71(2)	0.66(2)	-2.54(8-II-1)	-29(2)	18(9-II-1)	3(2)
3	95	0.81(2)	-9.15(2)	-1.86(8-II-1)	12(8-I-1)	51(2)	3(2)
3	96	-1.65(2)	-5.06(2)	-1.94(8-II-1)	-6(8-II-2)	39(9-II-1)	1(2)
3	97	1.65(2)	-0.88(2)	-2.46(8-II-1)	-15(2)	34(9-II-1)	3(2)
3	98	1.81(2)	-1.70(2)	-2.19(2)	15(2)	38(9-II-2)	3(2)
3	99	2.21(2)	-11.10(2)	-2.81(2)	0	54(9-II-2)	4(8-I-4)
3	100	-1.10(2)	-22.83(2)	-1.55(8-II-1)	38(2)	62(9-II-2)	4(2)
3	101	2.97(2)	-10.85(2)	-1.54(8-II-1)	39(2)	51(2)	3(2)
3	102	1.09(2)	-0.91(8-II-2)	-1.60(8-II-1)	-10(9-II-1)	31(9-II-1)	4(2)
3	103	-0.40(8-II-1)	-2.18(2)	-1.71(8-II-2)	8(9-I-1)	43(9-II-1)	2(2)
3	104	-0.21(8-I-2)	-4.82(2)	-2.04(8-II-2)	11(2)	43(9-II-1)	2(2)
3	105	-3.04(2)	-1.08(8-II-1)	1.29(8-I-1)	0	33(9-II-2)	3(2)
3	106	-0.46(8-II-1)	-1.53(2)	1.36(8-I-1)	-7(8-I-4)	32(9-II-1)	3(2)
3	107	2.35(2)	-8.41(2)	1.71(8-I-1)	0	63(8-I-1)	3(9-I-2)
3	108	1.28(2)	-1.16(8-I-1)	1.89(8-I-1)	-7(2)	34(9-II-2)	3(2)
3	109	4.07(2)	-9.10(2)	-2.05(2)	0	62(8-I-1)	6(8-I-1)
3	110	-3.98(2)	-22.32(2)	-1.32(8-II-1)	-22(9-I-1)	89(8-I-1)	2(2)
3	111	-2.36(2)	-2.37(2)	-1.28(8-II-1)	0	30(8-I-1)	3(9-II-1)
3	112	1.40(2)	-0.84(2)	-1.89(8-II-1)	-49(8-I-1)	36(8-I-1)	2(2)
3	113	-2.06(2)	-1.32(2)	-0.89(8-II-1)	0	22(8-I-1)	6(8-II-1)
3	114	1.00(2)	0.39(8-II-1)	-1.39(8-II-1)	-116(8-I-1)	19(8-I-1)	4(8-II-1)
3	115	-1.01(8-II-1)	-1.72(8-II-1)	0.79(8-I-1)	0	4(8-II-4)	19(8-II-1)
3	116	0.82(8-II-2)	-0.48(9-I-3)	1.02(8-I-1)	-259(8-I-1)	7(9-II-4)	12(8-II-1)
3	117	-0.79(8-II-1)	-5.28(2)	1.86(8-I-1)	-7(2)	39(9-II-1)	3(2)
3	118	1.98(2)	-0.66(2)	1.63(8-I-1)	-17(2)	37(9-II-1)	3(2)
3	119	4.92(2)	-9.30(2)	-1.40(8-II-1)	-23(9-I-1)	42(9-II-1)	2(8-I-1)
3	120	-1.36(2)	-11.99(2)	1.66(8-I-1)	-17(2)	41(9-II-1)	2(2)
3	121	-0.79(2)	-4.88(2)	-1.83(8-II-1)	-49(8-I-1)	42(9-II-1)	2(8-I-1)
3	122	-1.19(2)	-11.05(2)	-1.73(8-II-1)	-40(8-I-1)	42(9-II-1)	2(2)
3	123	-1.02(2)	-2.08(2)	-1.40(8-II-1)	-122(8-I-1)	39(9-II-1)	1(2)
3	124	1.03(2)	-0.56(2)	-1.64(8-II-1)	-94(8-I-1)	42(9-II-1)	1(8-II-1)
3	125	-1.12(9-II-1)	-1.89(2)	1.03(8-I-1)	-285(8-I-1)	31(9-II-1)	3(8-II-1)
3	126	0.88(8-II-2)	0.07(9-II-4)	-1.28(8-II-1)	-187(8-I-1)	37(9-II-1)	3(8-II-1)
3	127	0.48(8-II-2)	-1.95(2)	1.00(8-I-2)	-311(8-I-1)	-4(8-I-4)	4(8-II-1)
3	128	1.70(2)	-5.01(2)	-2.04(8-II-2)	11(8-I-1)	34(2)	4(2)
3	129	0.69(8-I-1)	-4.02(2)	-2.46(8-II-1)	-12(2)	34(2)	4(2)
3	130	0.49(8-I-1)	-0.69(8-II-2)	-2.58(8-II-2)	-15(8-II-1)	24(2)	5(2)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
3	131	2.00(2)	-9.17(2)	-1.85(8-II-2)	-13(8-II-1)	39(2)	4(2)
3	132	-0.52(8-II-1)	-12.29(2)	-1.94(8-II-2)	20(2)	47(2)	2(2)
3	133	1.54(2)	-12.40(2)	-1.62(8-II-2)	26(2)	48(2)	2(2)
3	134	1.04(8-I-1)	-10.96(2)	-1.51(8-II-2)	16(8-I-1)	39(2)	3(2)
3	135	-0.41(8-II-1)	-3.51(2)	-1.62(8-II-2)	-8(9-II-1)	36(9-II-1)	1(2)
3	136	0.91(8-I-1)	-4.58(2)	-1.71(8-II-2)	-7(8-II-1)	34(9-II-1)	0
3	137	2.18(2)	-6.41(2)	-1.85(8-II-2)	13(2)	34(9-II-1)	0
3	138	2.48(2)	0.70(2)	-2.34(8-II-2)	-16(8-II-1)	3(9-II-1)	4(2)
3	139	3.68(2)	-0.61(2)	-1.81(8-II-2)	43(2)	7(2)	3(2)
3	140	0.98(8-I-1)	-12.06(2)	-1.69(8-II-2)	9(8-I-1)	32(2)	1(2)
3	141	1.58(2)	-11.53(2)	-1.44(8-II-2)	-10(8-II-1)	33(2)	2(2)
3	142	2.84(8-I-1)	-10.78(2)	-1.49(8-II-2)	-12(8-II-1)	39(2)	3(2)
3	143	2.24(8-I-1)	-9.97(2)	-1.87(8-II-2)	-12(8-II-1)	47(2)	4(2)
3	144	5.23(8-I-1)	-3.61(2)	-2.49(8-II-2)	-19(8-II-1)	29(2)	9(2)
3	145	1.78(8-I-1)	-4.19(2)	-1.69(8-II-2)	-9(2)	27(9-II-1)	0
3	146	1.53(8-I-1)	-2.96(2)	-1.59(8-II-2)	-13(2)	28(9-II-1)	0
3	147	-1.36(8-II-1)	-6.36(2)	-1.83(8-II-2)	-10(2)	25(2)	0
3	148	3.03(8-I-1)	-7.10(2)	-1.86(8-II-2)	-19(2)	25(2)	0
3	149	-1.60(8-II-1)	-4.78(2)	-1.71(8-II-2)	-13(2)	19(2)	0
3	150	1.99(8-I-1)	-4.18(2)	-1.89(8-II-2)	-18(2)	20(2)	0
3	151	-1.06(2)	-3.84(2)	1.60(8-I-2)	-14(2)	36(9-II-1)	2(8-I-1)
3	152	1.18(2)	-1.10(2)	1.46(8-I-2)	-12(2)	37(9-II-1)	1(8-I-1)
3	153	-1.10(8-II-1)	-4.15(2)	1.57(8-I-2)	-15(2)	28(9-II-1)	0
3	154	2.29(2)	-7.10(2)	1.63(8-I-2)	-16(2)	37(9-II-1)	1(2)
3	155	0.73(8-I-1)	-5.36(2)	1.68(8-I-2)	-18(8-I-1)	36(9-II-1)	0
3	156	2.01(2)	-6.90(2)	-1.69(8-II-2)	-40(8-I-1)	40(9-II-1)	1(2)
3	157	-0.97(2)	-11.18(2)	-1.49(8-II-2)	-39(8-I-1)	38(9-II-1)	0
3	158	-0.92(2)	-3.78(2)	-1.64(8-II-2)	-94(8-I-1)	46(9-II-1)	1(8-II-1)
3	159	0.34(8-II-1)	-5.27(2)	-1.70(8-II-2)	-77(8-I-1)	43(9-II-1)	2(8-II-1)
3	160	-0.53(8-I-1)	-1.53(2)	1.15(8-I-2)	-304(8-I-1)	46(9-II-1)	4(9-I-4)
3	161	-0.90(9-I-1)	-2.15(2)	-1.28(8-II-2)	-185(8-I-1)	53(9-II-1)	2(9-I-2)
3	162	0.87(2)	-1.01(2)	-1.45(8-II-2)	-145(8-I-1)	50(9-II-1)	2(8-II-1)
3	163	0.44(8-II-2)	-2.51(2)	1.10(8-I-2)	-234(8-I-1)	31(9-II-1)	7(9-I-1)
3	164	0.79(8-I-1)	-5.53(2)	1.74(8-I-2)	-18(8-I-1)	28(9-II-1)	0
3	165	1.15(8-I-1)	-3.60(2)	1.72(8-I-2)	-16(8-I-1)	28(9-II-1)	0
3	166	2.10(2)	-6.77(2)	-1.54(8-II-2)	-39(8-I-1)	28(9-II-1)	0
3	167	-0.91(8-II-1)	-8.01(2)	1.69(8-I-2)	-30(8-I-1)	28(9-II-1)	0
3	168	0.70(8-I-1)	-5.22(2)	-1.73(8-II-2)	-77(8-I-1)	31(9-II-1)	0
3	169	-0.74(8-II-1)	-7.88(2)	-1.69(8-II-2)	-49(8-I-1)	30(9-II-1)	1(9-II-1)
3	170	-1.28(8-II-1)	-4.99(2)	1.83(8-I-2)	-16(8-I-1)	16(9-II-1)	0
3	171	1.20(8-I-1)	-3.76(2)	1.81(8-I-2)	-16(2)	17(2)	-1(8-I-4)
3	172	1.16(8-I-1)	-6.05(2)	1.79(8-I-2)	-30(8-I-1)	16(8-II-1)	-1(9-I-1)
3	173	-1.05(8-II-1)	-5.78(2)	1.86(8-I-2)	-22(8-I-1)	16(9-II-1)	-1(8-I-4)
3	174	1.05(8-I-1)	-5.84(2)	-1.78(8-II-2)	-49(8-I-1)	14(8-II-1)	-1(9-I-1)
3	175	-0.97(8-II-1)	-7.61(2)	-1.75(8-II-2)	-31(8-I-1)	16(8-II-1)	-1(9-I-1)
3	176	-0.75(8-II-1)	-2.91(2)	-1.51(8-II-2)	-138(8-I-1)	38(9-II-1)	0
3	177	0.37(2)	-3.10(2)	-1.68(8-II-2)	-73(8-I-1)	34(9-II-1)	1(9-II-1)
3	178	-0.79(8-II-1)	-2.51(2)	1.26(8-I-2)	-239(8-I-1)	65(9-II-1)	6(9-I-1)
3	179	0.53(2)	-1.44(2)	-1.44(8-II-2)	-101(8-I-1)	48(9-II-1)	3(8-I-1)
3	180	0.64(9-II-1)	-3.98(9-I-1)	1.24(8-I-2)	-114(8-I-1)	70(9-II-1)	9(8-I-1)
3	181	-0.86(8-II-1)	-4.21(2)	-1.76(8-II-2)	-72(8-I-1)	11(8-II-1)	-2(9-I-1)
3	182	-0.60(8-II-1)	-5.38(2)	-1.82(8-II-2)	-38(8-I-1)	12(8-II-1)	-1(9-I-1)
3	183	-0.50(9-II-1)	-2.23(2)	1.41(8-I-2)	-47(8-I-1)	6(9-II-1)	4(8-I-1)
3	184	-0.96(8-II-1)	-2.94(2)	-1.53(8-II-2)	-100(8-I-1)	15(9-II-1)	4(8-I-1)
3	185	0.20(2)	-2.65(2)	-1.67(8-II-2)	-42(9-I-1)	12(9-II-1)	3(9-II-4)
3	186	-0.28(9-I-1)	-3.60(2)	1.37(8-I-1)	-40(8-I-1)	-20(9-II-1)	-4(8-II-4)
3	187	-0.38(8-I-2)	-3.44(2)	-1.48(8-II-1)	88(8-I-2)	46(9-II-2)	5(2)
3	188	0.39(9-I-1)	-3.56(2)	-1.32(8-II-1)	-136(8-II-2)	60(9-II-2)	8(8-I-3)
3	189	-0.40(8-II-4)	-3.60(2)	-1.25(8-II-1)	-86(8-II-2)	36(9-II-2)	10(8-I-3)
3	190	-1.17(8-I-2)	-3.40(2)	1.63(8-I-1)	71(8-I-2)	19(9-II-2)	5(2)
3	191	-0.27(8-I-2)	-3.24(2)	-1.60(8-II-1)	79(8-I-2)	17(9-II-2)	5(9-I-2)
3	192	-0.23(8-I-2)	-3.42(2)	1.76(8-I-1)	57(8-I-2)	5(8-I-3)	4(2)
3	193	-1.07(8-I-2)	-4.17(2)	1.84(8-I-1)	62(8-I-2)	10(8-I-2)	3(2)
3	194	-0.30(8-I-1)	-3.56(2)	1.84(8-I-1)	43(8-I-2)	-6(8-II-3)	4(2)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
3	195	-1.16(8-I-2)	-5.04(2)	1.89(8-I-1)	50(2)	15(8-I-2)	2(8-II-3)
3	196	-0.47(2)	-4.94(2)	1.91(8-I-1)	36(8-I-2)	11(8-I-2)	2(2)
3	197	-0.43(8-I-2)	-3.68(2)	-1.58(8-II-1)	51(8-I-2)	18(9-II-2)	7(9-I-3)
3	198	-0.41(8-I-1)	-3.43(2)	-1.43(8-II-1)	-72(8-II-2)	28(9-II-2)	8(8-I-3)
3	199	-0.62(8-II-4)	-3.70(2)	-1.39(8-II-1)	-34(8-II-2)	4(9-II-2)	11(8-I-3)
3	200	-0.47(2)	-3.65(2)	1.78(8-I-1)	40(8-I-2)	-11(8-I-3)	5(2)
3	201	0.08(9-II-1)	-3.32(2)	1.71(8-I-1)	-36(8-II-2)	-11(8-I-3)	7(9-I-2)
3	202	-0.84(8-I-1)	-3.72(2)	1.42(8-I-1)	-38(8-II-2)	25(9-I-2)	11(8-I-3)
3	203	-0.52(2)	-3.94(2)	1.88(8-I-1)	43(8-I-2)	-16(9-II-2)	4(2)
3	204	-0.04(8-I-2)	-3.42(2)	1.85(8-I-1)	26(8-I-2)	-17(8-I-3)	4(2)
3	205	-0.43(8-I-2)	-4.64(2)	1.93(8-I-1)	37(8-I-2)	-17(9-II-2)	3(2)
3	206	-0.33(2)	-4.29(2)	1.91(8-I-1)	24(8-I-2)	-16(9-II-2)	4(2)
3	207	-0.43(2)	-5.14(2)	1.95(8-I-1)	18(8-I-2)	-17(9-II-2)	3(2)
3	208	-1.54(8-I-2)	-5.52(2)	1.98(8-I-1)	50(2)	23(2)	-2(8-I-3)
3	209	-0.34(8-I-1)	-5.21(2)	1.96(8-I-1)	27(9-I-3)	16(8-I-2)	2(8-II-3)
3	210	-0.72(2)	-5.30(2)	1.97(8-I-1)	28(9-I-3)	-17(9-II-2)	2(8-II-3)
3	211	-2.89(2)	-7.40(2)	2.20(8-I-1)	36(2)	40(2)	-3(2)
3	212	0.54(8-II-1)	-4.70(2)	2.12(8-I-1)	19(9-I-1)	29(2)	-1(8-I-2)
3	213	0.77(8-II-1)	-8.95(2)	2.26(8-I-1)	9(9-I-2)	49(2)	-2(2)
3	214	-5.29(2)	-21.77(2)	2.54(8-I-1)	27(2)	87(2)	-7(2)
3	215	0.83(2)	-12.43(2)	2.20(8-I-1)	-9(2)	51(2)	-3(2)
3	216	-0.78(2)	-20.60(2)	1.71(8-I-1)	10(2)	58(2)	-2(2)
3	217	-1.50(2)	-6.70(2)	2.08(8-I-1)	20(9-I-1)	19(9-I-1)	1(8-II-3)
3	218	-0.17(2)	-5.15(2)	2.02(8-I-1)	13(9-I-3)	-16(9-II-2)	2(2)
3	219	0.30(2)	-12.00(2)	1.79(8-I-1)	-3(2)	27(2)	0
3	220	-1.26(2)	-10.67(2)	2.11(8-I-1)	10(9-I-2)	25(9-I-1)	-1(8-I-3)
3	221	0.31(8-II-1)	-7.07(2)	2.08(8-I-1)	7(9-I-3)	21(9-I-1)	1(8-II-3)
3	222	-0.87(2)	-17.17(2)	1.42(8-I-1)	4(2)	31(9-I-2)	1(8-II-3)
3	223	-0.43(8-I-2)	-3.73(2)	1.69(8-I-1)	-28(8-II-2)	-36(9-II-2)	5(9-I-3)
3	224	0.32(8-I-4)	-3.47(2)	1.60(8-I-1)	-32(8-I-2)	-49(9-II-2)	8(8-I-3)
3	225	-0.48(8-I-1)	-3.89(2)	1.49(8-I-1)	-24(8-I-2)	31(9-I-2)	8(8-I-3)
3	226	-0.44(2)	-3.75(2)	1.85(8-I-1)	24(8-I-2)	-34(8-I-3)	4(2)
3	227	0.06(8-I-4)	-3.39(2)	1.77(8-I-1)	-23(8-I-2)	-33(8-I-3)	4(2)
3	228	-0.41(2)	-4.27(2)	1.91(8-I-1)	23(8-I-2)	-36(8-I-3)	4(2)
3	229	-0.16(2)	-3.80(2)	1.87(8-I-1)	-11(8-II-2)	-37(8-I-3)	3(2)
3	230	-0.42(2)	-5.00(2)	1.95(8-I-1)	18(8-I-2)	-37(9-II-2)	3(2)
3	231	-0.29(2)	-4.71(2)	1.91(8-I-1)	9(8-I-2)	-37(8-I-3)	3(2)
3	232	-0.38(2)	-3.67(2)	1.73(8-I-1)	-14(8-I-2)	-46(9-II-2)	3(2)
3	233	0.10(9-I-2)	-3.59(2)	1.68(8-I-1)	-23(8-I-2)	-45(9-II-2)	7(8-I-3)
3	234	-0.28(8-I-2)	-4.04(8-I-2)	1.53(8-I-1)	-19(8-II-3)	29(9-I-2)	5(8-I-3)
3	235	0.06(9-I-2)	-3.71(2)	1.74(8-I-1)	-19(9-II-1)	-59(9-II-2)	3(9-I-2)
3	236	-0.61(8-I-1)	-3.38(2)	1.52(8-I-1)	8(9-I-1)	-78(9-II-2)	1(9-I-3)
3	237	0.26(8-II-4)	-4.54(8-I-2)	1.62(8-I-1)	-14(9-I-2)	-74(9-II-2)	2(8-I-3)
3	238	0.10(2)	-3.59(2)	1.08(8-I-1)	0	51(9-I-2)	0
3	239	0.05(2)	-4.74(8-I-2)	1.12(8-I-1)	0	-84(9-II-2)	0
3	240	0.05(8-I-2)	-3.17(2)	1.12(8-I-1)	0	-84(9-II-2)	0
3	241	-0.31(2)	-3.93(2)	1.86(8-I-1)	-11(8-II-2)	-56(8-I-3)	3(2)
3	242	-0.37(8-I-1)	-3.61(2)	1.77(8-I-1)	7(9-I-1)	-56(9-II-2)	2(2)
3	243	-0.10(2)	-3.99(2)	1.65(8-I-1)	-7(9-II-1)	-79(9-II-2)	2(9-I-2)
3	244	-0.29(2)	-4.57(2)	1.87(8-I-1)	9(8-I-2)	-58(8-I-3)	3(2)
3	245	-0.26(2)	-4.19(2)	1.80(8-I-1)	4(9-I-1)	-57(8-I-3)	2(2)
3	246	-0.24(2)	-4.89(2)	1.84(8-I-1)	-3(9-II-1)	-62(8-I-3)	2(2)
3	247	-0.33(8-II-2)	-5.11(2)	1.88(8-I-1)	3(9-I-3)	-63(8-I-3)	2(2)
3	248	-0.17(2)	-4.21(2)	1.75(8-I-1)	-4(9-II-1)	-78(8-I-3)	1(2)
3	249	0.09(8-I-2)	-3.84(2)	1.18(8-I-1)	0	-78(9-II-2)	0
3	250	-0.24(2)	-4.57(2)	1.76(8-I-1)	4(9-I-3)	-80(8-I-3)	1(2)
3	251	0.12(8-I-2)	-4.59(2)	1.20(8-I-1)	0	-79(8-I-3)	0
3	252	-0.22(8-II-2)	-5.26(2)	1.80(8-I-1)	-2(8-II-2)	-81(8-I-3)	1(2)
3	253	-0.13(8-II-2)	-5.07(2)	1.16(8-I-1)	0	-81(8-I-3)	0
3	254	-0.81(2)	-6.06(2)	2.02(8-I-1)	13(8-I-2)	-35(9-II-2)	2(2)
3	255	-0.23(2)	-5.23(2)	1.97(8-I-1)	6(8-I-2)	-36(9-II-2)	3(2)
3	256	-0.43(2)	-5.50(2)	1.93(8-I-1)	6(8-I-2)	-57(8-I-3)	2(2)
3	257	-1.00(2)	-8.55(2)	2.07(8-I-1)	8(9-I-3)	-32(9-II-2)	2(2)
3	258	0.06(8-II-1)	-6.20(2)	2.05(8-I-1)	4(8-I-2)	-34(9-II-2)	2(2)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
3	259	0.57(8-I-1)	-12.29(2)	1.65(8-I-1)	-1(2)	-33(9-II-2)	2(2)
3	260	0.56(8-II-1)	-10.47(2)	1.98(8-I-1)	-1(9-II-3)	-32(9-II-2)	2(2)
3	261	-0.38(8-I-1)	-16.81(2)	1.33(8-I-1)	1(8-I-2)	-39(9-II-2)	1(2)
3	262	-0.65(2)	-7.27(2)	2.01(8-I-1)	4(8-I-2)	-55(9-II-2)	2(2)
3	263	-0.47(8-II-2)	-5.86(2)	1.91(8-I-1)	2(9-I-3)	-56(8-I-3)	2(2)
3	264	0.29(8-I-1)	-12.08(2)	1.58(8-I-1)	0	-51(9-II-2)	2(2)
3	265	-0.88(8-II-1)	-10.89(2)	1.94(8-I-1)	2(8-I-2)	-52(9-II-2)	2(2)
3	266	-0.20(8-II-2)	-8.42(2)	1.95(8-I-1)	0	-54(9-II-2)	2(2)
3	267	-0.37(2)	-6.37(2)	1.87(8-I-1)	-2(8-II-2)	-80(8-I-3)	1(2)
3	268	-0.20(8-II-2)	-5.50(2)	1.22(8-I-1)	0	-81(8-I-3)	0
3	269	-0.50(8-II-1)	-8.54(2)	1.94(8-I-1)	-2(2)	-79(8-I-3)	1(2)
3	270	-0.28(8-II-2)	-7.22(2)	1.28(8-I-1)	0	-80(8-I-3)	0
3	271	-0.37(8-II-2)	-11.07(2)	1.33(8-I-1)	0	-79(8-I-3)	0
3	272	-0.49(2)	-14.75(2)	1.37(8-I-1)	-2(2)	-59(9-II-2)	2(2)
3	273	0.57(8-I-1)	-11.48(2)	1.62(8-I-1)	1(2)	-79(8-I-3)	2(2)
3	274	-0.30(8-II-2)	-14.54(2)	1.20(8-I-1)	0	-83(2)	0
3	275	-1.81(8-II-1)	-10.72(2)	-1.98(8-II-2)	-11(2)	30(2)	0
3	276	-5.05(8-II-1)	-11.83(2)	-1.74(8-II-2)	-29(2)	33(2)	0
3	277	-2.27(8-II-2)	-17.05(2)	-2.14(8-II-2)	-5(2)	51(2)	-2(2)
3	278	-1.50(8-II-1)	-8.67(2)	-2.17(8-II-2)	-17(2)	18(2)	-1(2)
3	279	-1.53(8-II-1)	-5.84(2)	-2.09(8-II-2)	-15(2)	15(2)	-1(2)
3	280	-0.83(8-II-1)	-6.57(2)	-2.16(8-II-2)	-12(2)	17(2)	-2(2)
3	281	-1.39(8-II-1)	-5.00(2)	1.91(8-I-2)	-16(2)	13(8-II-1)	-1(8-I-1)
3	282	0.62(8-I-1)	-4.03(2)	-2.03(8-II-2)	-13(2)	13(8-II-1)	-1(2)
3	283	-0.87(8-II-2)	-11.53(2)	-2.08(8-II-2)	-8(2)	20(2)	-2(2)
3	284	-0.53(8-I-1)	-12.16(2)	-1.83(8-II-2)	-2(2)	20(2)	-2(2)
3	285	-0.93(8-II-2)	-16.33(2)	-1.52(8-II-2)	0	21(2)	-2(2)
3	286	0.82(8-II-2)	-15.41(2)	-1.40(8-II-2)	0	18(9-I-2)	-2(2)
3	287	-0.83(2)	-7.83(2)	-2.18(8-II-2)	-12(2)	16(9-I-2)	-2(2)
3	288	0.07(8-II-1)	-8.68(2)	-2.12(8-II-2)	-7(2)	15(9-I-2)	-2(2)
3	289	-1.11(2)	-5.53(2)	-2.06(8-II-2)	-13(2)	17(9-I-2)	-2(2)
3	290	-0.07(2)	-5.65(2)	-2.11(8-II-2)	-8(2)	16(9-I-2)	-2(2)
3	291	-0.98(8-II-1)	-5.50(2)	1.94(8-I-2)	-22(8-I-1)	13(8-II-1)	-1(8-I-1)
3	292	-0.52(8-II-1)	-4.85(2)	1.95(8-I-2)	-16(8-I-1)	13(8-II-1)	-1(8-I-1)
3	293	0.91(8-I-1)	-5.85(2)	-1.87(8-II-2)	-31(8-I-1)	11(8-II-1)	-1(8-I-4)
3	294	-0.59(8-II-1)	-6.50(2)	1.91(8-I-2)	-22(9-I-1)	12(8-II-1)	-1(8-I-1)
3	295	0.66(8-I-1)	-5.02(2)	-1.93(8-II-2)	-38(8-I-1)	12(9-I-4)	0
3	296	-0.55(2)	-6.31(2)	-1.95(8-II-2)	-28(9-I-1)	11(9-I-4)	0
3	297	-0.79(8-II-1)	-3.58(2)	-1.78(8-II-2)	-42(8-I-1)	25(9-I-1)	-2(8-II-4)
3	298	-0.13(8-II-2)	-4.02(2)	-1.92(8-II-2)	-32(9-I-1)	15(9-I-1)	0
3	299	-0.46(8-II-2)	-2.97(2)	1.52(8-I-2)	-25(8-I-1)	34(9-I-1)	-3(9-II-1)
3	300	0.18(8-II-2)	-2.58(2)	-1.75(8-II-2)	-28(9-I-1)	40(9-I-1)	-2(8-II-1)
3	301	-0.23(8-I-1)	-3.96(2)	1.44(8-I-1)	-28(9-II-3)	-62(9-II-1)	-6(9-II-1)
3	302	-0.61(8-II-2)	-5.24(2)	1.94(8-I-2)	-16(8-I-1)	17(9-I-2)	-1(2)
3	303	-0.11(2)	-4.62(2)	-2.00(8-II-2)	-10(8-I-1)	17(9-I-2)	-2(2)
3	304	0.41(8-I-2)	-5.63(2)	-1.93(8-II-2)	-22(9-I-1)	19(9-I-1)	-1(2)
3	305	-0.37(2)	-5.63(2)	-1.95(8-II-2)	-14(9-I-1)	18(9-I-1)	-1(2)
3	306	0.45(8-I-1)	-5.40(2)	-1.99(8-II-2)	-28(9-I-1)	22(9-I-1)	-1(9-II-2)
3	307	-0.48(2)	-6.25(2)	-1.97(8-II-2)	-16(9-I-1)	20(9-I-1)	-1(9-II-2)
3	308	-0.57(8-II-2)	-4.40(2)	-1.96(8-II-2)	-31(9-I-1)	27(9-I-1)	-1(9-II-1)
3	309	-0.29(2)	-5.13(2)	-1.99(8-II-2)	-16(9-I-1)	25(9-I-1)	-2(9-II-1)
3	310	-0.37(8-II-1)	-2.82(2)	-1.64(8-II-2)	-26(9-II-3)	47(9-I-1)	-7(9-II-1)
3	311	-0.74(8-II-2)	-3.44(2)	-1.82(8-II-2)	-25(8-II-1)	34(9-I-1)	-2(9-II-1)
3	312	0.06(8-I-1)	-3.50(2)	-1.91(8-II-2)	-16(8-II-1)	30(9-I-1)	-2(9-II-1)
3	313	-0.27(8-I-2)	-3.77(8-II-1)	-1.52(8-II-2)	-16(9-II-3)	21(9-I-1)	-6(9-II-1)
3	314	-0.46(2)	-10.79(2)	-1.97(8-II-2)	-5(2)	21(9-I-2)	-2(2)
3	315	-0.37(8-II-2)	-12.03(2)	-1.55(8-II-2)	-1(2)	21(9-I-2)	-2(2)
3	316	-0.47(8-I-2)	-14.40(2)	-1.28(8-II-2)	-2(2)	-33(9-II-1)	-2(2)
3	317	-0.07(8-II-2)	-8.44(2)	-2.05(8-II-2)	-2(2)	-30(9-II-1)	-2(2)
3	318	-0.67(2)	-6.46(2)	-2.07(8-II-2)	-8(2)	-28(9-II-1)	-2(2)
3	319	-0.27(2)	-7.65(2)	-2.06(8-II-2)	-4(2)	-29(9-II-1)	-2(2)
3	320	-0.61(2)	-5.32(2)	-1.98(8-II-2)	-10(8-I-1)	-28(9-II-1)	-2(2)
3	321	-0.15(2)	-5.17(2)	-2.00(8-II-2)	-5(8-I-1)	-28(9-II-1)	-2(2)
3	322	-0.26(8-I-1)	-13.93(2)	-1.16(8-II-2)	0	-73(9-II-1)	0

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
3	323	-0.50(8-I-2)	-10.83(2)	-1.96(8-II-2)	-4(2)	-43(9-II-1)	-2(2)
3	324	0.03(2)	-11.66(2)	-1.60(8-II-2)	0	-43(9-II-1)	-2(2)
3	325	-0.43(8-II-2)	-13.73(2)	-1.33(8-II-2)	-2(2)	-53(9-II-1)	-1(2)
3	326	0.64(8-II-2)	-11.46(2)	-1.59(8-II-2)	0	-68(9-II-1)	-1(2)
3	327	-0.37(8-I-2)	-7.35(2)	-2.01(8-II-2)	-3(2)	-47(9-II-1)	-2(2)
3	328	-0.19(2)	-8.30(2)	-1.92(8-II-2)	0	-47(9-II-1)	-2(2)
3	329	-0.49(2)	-5.68(2)	-1.96(8-II-2)	-5(8-I-1)	-45(9-II-1)	-2(2)
3	330	-0.35(8-I-1)	-6.24(2)	-1.91(8-II-2)	-2(8-I-1)	-46(9-II-1)	-1(2)
3	331	-0.30(8-I-2)	-8.51(2)	-1.90(8-II-2)	-2(2)	-65(9-II-1)	0
3	332	-0.31(2)	-10.88(2)	-1.30(8-II-2)	0	-67(9-II-1)	0
3	333	-0.25(2)	-6.22(2)	-1.86(8-II-2)	-2(8-I-1)	-62(9-II-1)	0
3	334	-0.25(2)	-7.30(2)	-1.26(8-II-2)	0	-63(9-II-1)	0
3	335	-0.20(2)	-5.65(2)	-1.24(8-II-2)	0	-60(9-II-1)	0
3	336	-0.18(8-II-2)	-5.42(2)	-1.94(8-II-2)	-14(9-I-1)	-29(9-II-1)	-1(2)
3	337	-0.23(2)	-5.15(2)	-1.94(8-II-2)	-7(8-I-1)	-29(9-II-1)	-1(2)
3	338	0.20(8-I-2)	-5.50(2)	-1.96(8-II-2)	-16(9-I-1)	-30(9-II-1)	-1(9-II-2)
3	339	-0.35(2)	-5.85(2)	-1.94(8-II-2)	-8(8-I-1)	-30(9-II-1)	-1(9-II-2)
3	340	-0.22(8-II-2)	-4.91(2)	-1.99(8-II-2)	-16(9-I-1)	31(9-I-1)	-2(9-II-1)
3	341	-0.31(2)	-5.62(2)	-1.97(8-II-2)	-8(8-II-1)	32(9-I-1)	-1(9-II-1)
3	342	-0.39(8-II-2)	-3.91(2)	-1.92(8-II-2)	-15(8-II-1)	32(9-I-1)	-2(9-II-1)
3	343	-0.13(8-II-1)	-4.35(2)	-1.97(8-II-2)	-9(8-II-1)	32(9-I-1)	-2(9-II-1)
3	344	-0.65(8-II-2)	-3.27(2)	-1.71(8-II-2)	-16(9-II-3)	25(9-I-1)	-5(9-II-1)
3	345	0.06(2)	-3.25(2)	-1.89(8-II-2)	-10(9-II-2)	32(9-I-1)	-3(9-II-1)
3	346	0.21(8-II-2)	-4.19(8-II-1)	-1.58(8-II-2)	-5(2)	19(9-I-1)	-5(9-II-1)
3	347	-0.31(2)	-5.30(2)	-1.91(8-II-2)	-7(8-I-1)	-43(9-II-1)	-1(2)
3	348	-0.23(2)	-5.19(2)	-1.88(8-II-2)	-2(8-I-1)	-44(9-II-1)	-1(2)
3	349	-0.27(2)	-5.33(2)	-1.84(8-II-2)	-2(8-I-1)	-59(9-II-1)	0
3	350	-0.10(8-II-2)	-5.47(2)	-1.90(8-II-2)	-8(8-I-1)	-42(9-II-1)	-1(9-II-2)
3	351	-0.26(2)	-5.48(2)	-1.87(8-II-2)	-2(8-I-1)	-43(9-II-1)	0
3	352	0.18(8-I-2)	-5.23(2)	-1.93(8-II-2)	-8(8-II-1)	-40(9-II-1)	-1(9-II-1)
3	353	-0.25(2)	-5.68(2)	-1.87(8-II-2)	-3(8-II-1)	-41(9-II-1)	-1(9-II-1)
3	354	-0.11(2)	-5.37(2)	-1.83(8-II-2)	-2(8-I-1)	-55(9-II-1)	0
3	355	-0.16(2)	-5.32(2)	-1.23(8-II-2)	0	-57(9-II-1)	0
3	356	0.07(8-I-2)	-5.42(2)	-1.83(8-II-2)	-3(8-II-1)	-51(9-II-1)	0
3	357	-0.12(2)	-5.58(2)	-1.23(8-II-2)	0	-53(9-II-1)	0
3	358	-0.07(2)	-5.33(2)	-1.23(8-II-2)	0	-48(9-II-1)	0
3	359	-0.33(8-II-2)	-4.48(2)	-1.94(8-II-2)	-9(8-II-1)	-36(9-II-1)	-2(9-II-1)
3	360	-0.34(8-II-2)	-4.98(2)	-1.88(8-II-2)	-5(9-II-3)	-39(9-II-1)	-1(9-II-1)
3	361	0.05(8-I-2)	-4.88(2)	-1.84(8-II-2)	-4(9-II-3)	-46(9-II-1)	0
3	362	-0.48(8-II-2)	-3.32(8-II-1)	-1.76(8-II-2)	-9(8-I-1)	-30(9-II-1)	-4(9-II-1)
3	363	-0.50(8-II-2)	-3.63(2)	-1.90(8-II-2)	-7(9-II-2)	-24(9-II-1)	-2(9-II-1)
3	364	0.28(8-I-2)	-3.91(2)	-1.86(8-II-2)	-8(9-II-1)	-32(9-II-1)	-1(9-II-1)
3	365	0.22(8-II-2)	-4.29(8-II-1)	-1.60(8-II-2)	-7(9-I-3)	11(9-I-1)	-2(9-II-1)
3	366	-0.25(8-II-2)	-4.18(2)	-1.84(8-II-2)	-5(9-II-4)	-42(9-II-1)	0
3	367	0.12(8-I-1)	-4.42(2)	-1.25(8-II-2)	0	-43(9-II-1)	0
3	368	-0.55(8-II-2)	-4.94(8-II-1)	-1.72(8-II-2)	-5(9-I-3)	-38(9-II-1)	-1(9-II-1)
3	369	0.25(8-I-1)	-3.28(2)	-1.29(8-II-2)	0	-41(9-II-1)	0
3	370	0.27(8-I-1)	-3.58(8-II-1)	-1.18(8-II-2)	0	24(9-I-3)	0
4	1	0.76(8-II-3)	-1.51(2)	1.07(9-I-3)	0	14(9-II-2)	0
4	2	4.84(2)	-10.77(2)	-3.07(2)	0	172(2)	17(2)
4	3	-4.68(2)	-2.63(2)	-1.51(9-II-3)	0	77(2)	9(2)
4	4	2.77(2)	1.23(9-II-3)	-2.16(9-II-3)	28(2)	135(2)	2(2)
4	5	-5.09(2)	-3.73(2)	1.84(9-I-3)	0	50(9-II-2)	6(2)
4	6	3.02(2)	0.86(2)	1.96(9-I-3)	-11(9-II-2)	52(2)	4(2)
4	7	3.57(2)	-0.36(9-I-3)	3.20(2)	-13(2)	49(9-II-2)	4(2)
4	8	-2.40(2)	-4.98(2)	1.76(2)	0	95(2)	-14(2)
4	9	-2.76(2)	1.38(9-I-3)	1.57(9-I-3)	0	87(2)	-10(2)
4	10	9.12(2)	-13.79(2)	3.50(2)	0	192(2)	-22(2)
4	11	-0.61(2)	-4.18(2)	2.48(2)	21(2)	155(2)	-6(2)
4	12	1.91(2)	-19.16(2)	-2.22(9-II-3)	83(2)	220(2)	10(2)
4	13	-2.65(2)	-30.47(2)	2.11(9-I-3)	98(2)	264(2)	-6(2)
4	14	-0.14(9-II-3)	-2.42(2)	1.79(9-I-3)	-84(2)	41(2)	-3(2)
4	15	0.57(2)	-0.81(9-II-3)	1.56(9-I-3)	-149(2)	39(2)	-1(9-I-2)
4	16	0.58(2)	-1.19(8-I-3)	1.52(9-I-3)	-195(2)	6(9-II-2)	3(9-II-2)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
4	17	1.20(2)	-5.84(2)	2.43(9-I-3)	-5(9-I-2)	58(2)	-2(9-I-2)
4	18	0.77(2)	-2.53(2)	2.11(9-I-3)	-77(2)	61(2)	-2(9-I-2)
4	19	-1.48(2)	-6.40(2)	-2.03(9-II-3)	29(2)	83(2)	0
4	20	1.02(2)	-4.36(2)	-2.27(9-II-3)	77(2)	99(2)	-4(2)
4	21	-2.30(2)	-4.91(2)	2.04(9-I-3)	-11(9-II-2)	54(9-II-2)	2(2)
4	22	2.68(2)	-0.08(2)	-1.85(9-II-3)	30(2)	73(2)	-1(2)
4	23	-2.02(2)	-9.91(2)	2.94(2)	-13(2)	53(9-II-2)	2(2)
4	24	3.02(2)	-0.04(2)	2.44(9-I-3)	8(9-I-2)	51(9-II-2)	0
4	25	5.20(2)	-17.44(2)	4.01(2)	0	77(9-II-2)	5(9-I-2)
4	26	6.82(2)	-17.75(2)	-3.77(2)	0	73(9-II-2)	5(9-II-2)
4	27	-8.81(2)	-46.35(2)	1.92(9-I-3)	-17(2)	102(9-II-2)	3(2)
4	28	-5.50(2)	-4.04(2)	-1.83(9-II-3)	0	40(9-II-2)	2(2)
4	29	3.48(2)	0.33(9-I-3)	-2.83(2)	-13(2)	44(9-II-2)	2(2)
4	30	-5.59(2)	-3.60(2)	1.82(9-I-3)	0	-35(9-I-2)	2(2)
4	31	2.97(2)	1.21(2)	-1.94(9-II-3)	-14(9-II-2)	30(9-II-2)	1(2)
4	32	3.10(2)	1.55(8-I-3)	2.65(9-I-3)	-16(2)	-48(9-I-2)	0
4	33	6.00(2)	-15.81(2)	4.40(2)	0	-63(9-I-2)	5(9-I-2)
4	34	-2.81(2)	-36.00(2)	2.61(8-I-3)	-13(2)	-96(9-I-2)	2(9-I-2)
4	35	6.15(2)	-14.26(2)	-4.31(2)	0	-59(9-I-2)	-6(2)
4	36	-1.61(2)	-33.33(2)	-2.69(9-II-3)	-14(2)	-94(9-I-2)	-3(2)
4	37	-5.81(2)	-2.74(2)	-1.85(8-II-3)	0	34(9-II-2)	-4(2)
4	38	2.98(2)	1.54(9-II-3)	-2.72(8-II-3)	-15(2)	-46(9-I-2)	-2(2)
4	39	10.89(2)	-19.39(2)	1.90(9-I-3)	-18(2)	53(9-II-2)	2(2)
4	40	-2.44(2)	-23.56(2)	2.53(9-I-3)	-13(2)	54(9-II-2)	0
4	41	-2.27(2)	-9.53(2)	-2.66(9-II-3)	-13(2)	45(9-II-2)	1(2)
4	42	-2.11(2)	-23.01(2)	-2.40(9-II-3)	-18(2)	49(9-II-2)	1(2)
4	43	-3.08(2)	-5.22(2)	-1.95(9-II-3)	-14(9-II-2)	37(9-II-2)	0
4	44	3.01(2)	-0.34(2)	-2.33(9-II-3)	-20(2)	39(9-II-2)	0
4	45	-3.02(2)	-6.72(2)	2.47(9-I-3)	-16(2)	36(9-II-2)	0
4	46	3.17(2)	-0.04(9-I-3)	2.18(9-I-3)	-23(2)	35(9-II-2)	0
4	47	5.69(2)	-15.51(2)	2.83(2)	-13(2)	42(9-II-2)	0
4	48	1.81(2)	-8.78(2)	2.71(9-I-3)	-23(2)	39(9-II-2)	0
4	49	4.85(2)	-15.43(2)	-3.12(2)	-13(2)	42(9-II-2)	-2(2)
4	50	-7.02(2)	-38.14(2)	-2.03(9-II-3)	-23(2)	-46(9-I-2)	0
4	51	-1.90(2)	-5.76(2)	-2.61(8-II-3)	-15(2)	37(9-II-2)	-1(2)
4	52	1.63(2)	-7.73(2)	-2.74(8-II-3)	-22(2)	39(9-II-2)	-1(2)
4	53	0.43(2)	0.88(8-I-3)	-2.05(8-II-3)	-10(9-II-2)	34(9-II-2)	-2(2)
4	54	1.66(2)	-1.72(2)	-2.24(8-II-3)	-20(2)	37(9-II-2)	-1(2)
4	55	6.48(2)	-12.69(2)	2.13(9-I-3)	92(2)	62(2)	-2(9-I-2)
4	56	-0.27(9-II-3)	-13.50(2)	2.32(9-I-3)	26(2)	61(2)	2(9-II-2)
4	57	0.84(2)	-2.75(2)	2.01(9-I-3)	-90(2)	23(9-II-2)	3(9-II-2)
4	58	0.57(2)	-1.73(2)	1.75(9-I-3)	-212(2)	22(9-II-2)	4(9-II-2)
4	59	1.24(2)	-1.26(2)	1.64(9-I-3)	-194(2)	-6(9-I-2)	5(9-II-2)
4	60	2.71(2)	-7.89(2)	2.30(9-I-3)	20(2)	33(9-II-2)	3(9-II-2)
4	61	0.65(2)	-5.53(2)	2.15(9-I-3)	-68(2)	32(9-II-2)	4(9-II-2)
4	62	0.84(2)	-10.59(2)	-2.16(9-II-3)	76(2)	56(2)	-3(2)
4	63	-1.68(2)	-18.45(2)	1.79(9-I-3)	65(2)	55(2)	-2(2)
4	64	-1.46(2)	-5.95(2)	1.86(9-I-3)	31(2)	47(9-II-2)	-2(2)
4	65	1.93(2)	-3.12(2)	-1.96(9-II-3)	53(2)	52(2)	-4(2)
4	66	-1.92(2)	-7.69(2)	2.45(9-I-3)	8(9-I-2)	43(9-II-2)	-1(9-I-1)
4	67	2.55(2)	-1.36(2)	2.14(9-I-3)	29(2)	46(9-II-2)	-2(2)
4	68	4.69(2)	-14.55(2)	2.42(9-I-3)	-13(2)	38(9-II-2)	0
4	69	0.37(2)	-11.34(2)	2.47(9-I-3)	12(9-I-2)	40(9-II-2)	-1(2)
4	70	-0.64(8-I-3)	-1.72(2)	1.64(9-I-3)	-195(2)	22(9-II-2)	5(9-II-2)
4	71	3.59(2)	-11.21(2)	1.85(9-I-3)	61(2)	31(9-II-2)	-2(9-I-2)
4	72	-1.03(2)	-14.68(2)	2.11(9-I-3)	11(9-I-2)	28(9-II-2)	2(9-II-2)
4	73	0.68(2)	-4.90(2)	2.07(9-I-3)	-57(2)	-43(9-I-2)	3(9-II-2)
4	74	0.90(2)	-2.47(2)	1.80(9-I-3)	-130(2)	-31(9-I-2)	6(9-II-2)
4	75	2.39(2)	-8.91(2)	2.10(9-I-3)	9(9-I-2)	-30(9-I-2)	2(9-II-2)
4	76	0.24(9-I-2)	-8.34(2)	2.11(9-I-3)	-40(2)	-33(9-I-2)	2(2)
4	77	-0.62(2)	-7.90(2)	-1.94(9-II-3)	52(2)	31(9-II-2)	-3(2)
4	78	-0.16(2)	-11.16(2)	-1.84(9-II-3)	36(2)	29(9-II-2)	-1(9-I-1)
4	79	-1.50(2)	-7.06(2)	2.15(9-I-3)	29(2)	30(9-II-2)	-2(2)
4	80	2.02(2)	-3.18(2)	1.93(9-I-3)	36(2)	31(9-II-2)	-2(2)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
4	81	1.25(2)	-11.09(2)	2.42(9-I-3)	12(9-I-2)	26(9-II-2)	-2(2)
4	82	1.34(2)	-6.60(2)	2.29(9-I-3)	24(9-I-2)	28(9-II-2)	-2(2)
4	83	1.62(2)	-9.54(2)	1.79(9-I-3)	34(2)	-20(9-I-2)	-1(9-I-1)
4	84	-0.72(2)	-12.71(2)	1.96(9-I-3)	24(9-I-2)	-24(9-I-2)	1(2)
4	85	-1.00(2)	-7.53(2)	1.93(9-I-3)	35(2)	14(9-II-2)	-2(2)
4	86	0.72(2)	-7.43(2)	1.85(9-I-3)	31(9-I-2)	-16(9-I-2)	0
4	87	-0.20(8-I-3)	-9.11(2)	2.26(9-I-3)	24(9-I-2)	11(9-II-2)	-2(2)
4	88	1.40(2)	-5.32(2)	2.10(9-I-3)	29(9-I-2)	12(9-II-2)	-1(2)
4	89	0.09(9-I-3)	-11.64(2)	2.23(9-I-3)	23(9-I-2)	11(2)	-1(2)
4	90	4.25(2)	-13.95(2)	-2.29(9-II-3)	-19(2)	35(9-II-2)	0
4	91	-2.12(2)	-23.06(2)	1.99(9-I-3)	-9(9-II-2)	35(9-II-2)	0
4	92	-2.29(2)	-7.81(2)	-2.31(9-II-3)	-20(2)	32(9-II-2)	0
4	93	0.68(2)	-10.86(2)	-2.31(9-II-3)	-16(2)	33(9-II-2)	0
4	94	-2.60(2)	-6.42(2)	2.16(9-I-3)	-23(2)	31(9-II-2)	0
4	95	2.52(2)	-1.97(2)	-2.03(9-II-3)	-21(2)	32(9-II-2)	0
4	96	-0.66(2)	-10.41(2)	2.61(9-I-3)	-23(2)	29(9-II-2)	0
4	97	2.13(2)	-4.39(2)	2.37(9-I-3)	-24(2)	30(9-II-2)	0
4	98	7.42(2)	-17.51(2)	1.98(9-I-3)	-23(2)	29(9-II-2)	0
4	99	-1.38(2)	-20.24(2)	2.40(9-I-3)	-25(2)	28(9-II-2)	0
4	100	-1.17(2)	-10.37(2)	-2.60(8-II-3)	-21(2)	30(9-II-2)	0
4	101	-1.60(2)	-20.35(2)	-2.37(8-II-3)	-23(2)	28(9-II-2)	0
4	102	-1.87(2)	-6.24(2)	-2.08(8-II-3)	-14(2)	32(9-II-2)	0
4	103	2.67(2)	-3.33(2)	-2.33(8-II-3)	-17(2)	31(9-II-2)	0
4	104	4.33(2)	-13.95(2)	1.99(9-I-3)	-10(9-II-2)	23(9-II-2)	0
4	105	-0.86(2)	-16.80(2)	2.22(9-I-3)	16(9-I-2)	24(9-II-2)	-2(2)
4	106	2.62(2)	-12.38(2)	2.19(9-I-3)	16(9-I-2)	12(2)	-1(2)
4	107	0.74(2)	-10.71(2)	-2.25(9-II-3)	-16(2)	21(9-II-2)	0
4	108	-0.51(2)	-16.07(2)	-2.06(9-II-3)	-12(9-II-2)	21(9-II-2)	-1(2)
4	109	-1.80(2)	-7.71(2)	-2.02(9-II-3)	-21(2)	20(9-II-2)	0
4	110	1.43(2)	-6.90(2)	-2.12(9-II-3)	-13(2)	21(9-II-2)	0
4	111	-1.28(2)	-8.80(2)	2.34(9-I-3)	-24(2)	19(9-II-2)	0
4	112	2.02(2)	-4.27(2)	2.11(9-I-3)	-18(2)	20(9-II-2)	0
4	113	2.21(2)	-12.06(2)	-2.02(9-II-3)	-12(9-II-2)	12(2)	-1(2)
4	114	-0.66(2)	-15.80(2)	2.01(9-I-3)	16(9-I-2)	13(2)	-1(2)
4	115	-0.37(2)	-9.38(2)	-2.09(9-II-3)	-13(2)	12(2)	0
4	116	0.41(2)	-11.19(2)	-2.05(9-II-3)	-12(9-II-2)	12(2)	0
4	117	-1.16(2)	-8.61(2)	2.11(9-I-3)	-18(2)	11(2)	0
4	118	1.41(2)	-6.32(2)	1.96(9-I-3)	-11(9-II-2)	12(2)	0
4	119	1.12(2)	-8.07(2)	2.20(9-I-3)	-14(2)	11(2)	0
4	120	3.29(2)	-13.38(2)	2.33(9-I-3)	-25(2)	18(9-II-2)	0
4	121	0.64(2)	-11.21(2)	2.34(9-I-3)	-21(2)	18(9-II-2)	0
4	122	0.69(2)	-10.93(2)	2.30(9-I-3)	-21(2)	11(2)	0
4	123	3.46(2)	-13.74(2)	-2.30(8-II-3)	-22(2)	18(9-II-2)	0
4	124	-1.57(2)	-20.44(2)	2.00(9-I-3)	-21(2)	17(9-II-2)	0
4	125	-1.65(2)	-8.43(2)	-2.31(8-II-3)	-16(2)	20(9-II-2)	0
4	126	0.62(2)	-10.79(2)	-2.32(8-II-3)	-17(2)	19(9-II-2)	0
4	127	2.13(2)	-3.55(2)	-2.05(8-II-3)	-10(2)	21(9-II-2)	0
4	128	3.38(2)	-13.50(2)	2.00(9-I-3)	-21(2)	11(2)	0
4	129	-0.38(2)	-15.21(2)	2.16(9-I-3)	-15(2)	12(2)	0
4	130	0.62(2)	-10.99(2)	-2.27(8-II-3)	-17(2)	12(2)	0
4	131	-0.54(2)	-15.35(2)	-2.12(8-II-3)	-15(2)	12(2)	0
4	132	-1.53(2)	-8.58(2)	-2.04(8-II-3)	-10(2)	14(2)	0
4	133	1.28(2)	-7.18(2)	-2.16(8-II-3)	-11(2)	13(2)	0
4	134	3.89(2)	-12.04(2)	3.81(2)	0	60(9-II-2)	-8(2)
4	135	-4.33(2)	1.89(8-I-3)	2.21(8-I-3)	0	50(9-II-2)	-5(2)
4	136	-1.28(2)	-3.89(2)	2.10(8-I-3)	-10(2)	38(9-II-2)	-4(2)
4	137	6.06(2)	-22.80(2)	-3.50(2)	0	92(9-II-1)	4(9-II-1)
4	138	-6.54(2)	-38.82(2)	2.30(8-I-3)	21(2)	111(9-II-1)	-3(2)
4	139	1.50(2)	-3.41(2)	-3.22(2)	8(2)	49(9-II-1)	0
4	140	-5.21(2)	-3.03(2)	-1.99(8-II-3)	0	48(9-II-1)	0
4	141	-5.10(2)	-3.41(2)	1.74(8-I-3)	0	42(9-II-1)	-3(2)
4	142	2.86(2)	1.18(8-I-3)	-2.08(8-II-3)	-9(9-II-1)	37(9-II-1)	-1(2)
4	143	4.30(2)	-13.54(2)	3.53(2)	0	74(2)	-6(2)
4	144	3.55(2)	1.16(8-I-3)	2.50(8-I-3)	3(9-I-1)	54(2)	-2(2)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
4	145	6.35(2)	-19.73(2)	-3.65(2)	0	94(2)	4(9-II-1)
4	146	-7.48(2)	-40.62(2)	2.16(8-I-3)	21(2)	118(2)	-1(2)
4	147	2.01(2)	-2.18(2)	-3.22(2)	7(2)	55(2)	0
4	148	7.02(2)	-16.03(2)	2.55(8-I-3)	21(2)	54(9-II-2)	-3(2)
4	149	1.49(2)	-7.50(2)	2.57(8-I-3)	8(2)	50(9-II-2)	-1(2)
4	150	-0.18(9-II-3)	-12.62(2)	-2.94(2)	8(2)	56(9-II-1)	0
4	151	-5.48(2)	-31.99(2)	-2.17(8-II-3)	21(2)	61(9-II-1)	-2(2)
4	152	-2.86(2)	-5.76(2)	-2.13(8-II-3)	-9(9-II-1)	46(2)	-1(2)
4	153	3.02(2)	-0.77(2)	-2.59(8-II-3)	8(2)	48(2)	-2(2)
4	154	-3.27(2)	-6.90(2)	2.35(8-I-3)	3(9-I-1)	52(2)	-1(2)
4	155	2.94(2)	0.46(2)	2.05(8-I-3)	6(9-I-1)	49(2)	0
4	156	8.88(2)	-17.18(2)	2.27(8-I-3)	21(2)	64(2)	-1(2)
4	157	0.06(9-I-1)	-12.13(2)	2.49(8-I-3)	14(2)	59(2)	0
4	158	-0.85(2)	-11.33(2)	-2.97(2)	7(2)	65(2)	0
4	159	-4.29(2)	-28.59(2)	-2.33(8-II-3)	22(2)	69(2)	0
4	160	-5.04(2)	-3.29(2)	-1.95(8-II-3)	0	55(2)	1(9-II-1)
4	161	-4.83(2)	-3.38(2)	1.67(8-I-3)	0	59(2)	-2(2)
4	162	2.71(2)	1.10(8-I-3)	-2.05(8-II-3)	-7(9-II-1)	49(2)	0
4	163	4.38(2)	-14.19(2)	3.28(2)	0	130(2)	-8(2)
4	164	3.46(2)	1.01(8-I-3)	2.42(8-I-3)	14(2)	83(2)	0
4	165	12.31(2)	-19.86(2)	-4.26(2)	2(2)	149(2)	16(2)
4	166	-8.99(2)	-42.69(2)	1.95(8-I-3)	39(2)	217(2)	2(2)
4	167	-3.27(2)	2.28(8-II-3)	-1.98(8-II-3)	0	56(2)	8(2)
4	168	-2.83(2)	-5.97(2)	-2.62(2)	0	57(2)	11(2)
4	169	1.37(2)	-4.73(2)	-3.68(2)	25(2)	99(2)	6(2)
4	170	-2.14(2)	-0.75(8-I-3)	-1.54(8-II-3)	0	25(9-II-1)	7(2)
4	171	1.84(2)	-0.92(8-II-3)	-2.24(8-II-3)	-8(9-II-1)	29(2)	6(2)
4	172	-1.07(8-II-3)	-1.64(8-I-3)	1.19(8-I-3)	0	21(9-II-1)	6(2)
4	173	-1.50(2)	-2.11(8-II-3)	-1.21(8-II-3)	0	25(9-II-1)	6(2)
4	174	0.65(2)	0.29(8-II-3)	-1.84(8-II-3)	-15(2)	22(9-II-1)	5(2)
4	175	-0.41(2)	-1.38(2)	1.27(8-I-3)	-24(2)	-15(9-I-1)	4(2)
4	176	-2.71(2)	-5.53(2)	-2.11(8-II-3)	-7(9-II-1)	57(2)	0
4	177	2.73(2)	-0.40(2)	-2.55(8-II-3)	13(2)	59(2)	0
4	178	-2.99(2)	-6.66(2)	2.28(8-I-3)	14(2)	64(2)	0
4	179	3.03(2)	0.52(2)	1.99(8-I-3)	16(2)	61(2)	1(2)
4	180	10.46(2)	-17.57(2)	2.00(8-I-3)	36(2)	76(2)	2(2)
4	181	-0.55(2)	-14.11(2)	2.34(8-I-3)	35(2)	72(2)	2(2)
4	182	-0.62(2)	-8.41(2)	-3.15(2)	21(2)	62(2)	5(2)
4	183	-3.92(2)	-25.75(2)	-2.52(8-II-3)	40(2)	79(2)	2(2)
4	184	-2.19(2)	-3.59(2)	-2.27(8-II-3)	-6(9-II-1)	35(2)	5(2)
4	185	1.65(2)	-1.40(2)	-2.62(8-II-3)	14(2)	47(2)	2(2)
4	186	-0.12(8-II-2)	-0.48(8-I-4)	-1.60(8-II-3)	-31(2)	17(9-II-1)	4(2)
4	187	-1.42(2)	-1.98(2)	-1.83(8-II-3)	-23(2)	23(9-II-1)	4(2)
4	188	1.43(2)	-0.10(8-I-3)	-2.11(8-II-3)	-16(2)	28(9-II-1)	3(2)
4	189	0.33(9-II-3)	-1.68(2)	-1.44(8-II-3)	-45(2)	9(9-II-1)	4(9-I-1)
4	190	-0.27(2)	-9.04(2)	2.41(8-I-3)	5(2)	35(9-II-2)	0
4	191	2.14(2)	-2.64(2)	2.21(8-I-3)	-6(2)	34(9-II-2)	0
4	192	-1.89(2)	-8.32(2)	2.19(8-I-3)	-6(2)	21(9-II-2)	0
4	193	6.91(2)	-15.63(2)	-2.01(8-II-3)	20(2)	36(9-II-2)	0
4	194	-0.93(2)	-17.49(2)	2.31(8-I-3)	7(2)	34(9-II-2)	0
4	195	-2.41(2)	-8.93(2)	-2.58(8-II-3)	8(2)	40(2)	-1(2)
4	196	-1.51(2)	-18.04(2)	-2.41(8-II-3)	12(2)	37(2)	0
4	197	-2.61(2)	-6.62(2)	2.02(8-I-3)	6(9-I-1)	44(2)	0
4	198	2.62(2)	-1.39(2)	-2.26(8-II-3)	10(2)	44(2)	0
4	199	1.18(2)	-11.03(2)	2.39(8-I-3)	14(2)	46(2)	0
4	200	1.72(2)	-4.71(2)	2.23(8-I-3)	13(2)	46(2)	0
4	201	6.12(2)	-14.67(2)	-2.21(8-II-3)	22(2)	49(2)	0
4	202	-1.88(2)	-19.55(2)	2.12(8-I-3)	19(2)	47(2)	0
4	203	-2.16(2)	-8.41(2)	-2.55(8-II-3)	13(2)	50(2)	0
4	204	-0.82(2)	-14.97(2)	-2.46(8-II-3)	22(2)	50(2)	0
4	205	2.64(2)	-12.15(2)	2.24(8-I-3)	7(2)	23(2)	0
4	206	0.71(2)	-9.62(2)	2.23(8-I-3)	-2(2)	21(9-II-2)	0
4	207	2.90(2)	-12.49(2)	-2.31(8-II-3)	12(2)	27(2)	0
4	208	-1.41(2)	-18.13(2)	-2.03(8-II-3)	6(2)	23(2)	0

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
4	209	-2.24(2)	-7.96(2)	-2.26(8-II-3)	10(2)	32(2)	0
4	210	0.56(2)	-9.56(2)	-2.32(8-II-3)	10(2)	30(2)	0
4	211	0.27(2)	-10.20(2)	2.19(8-I-3)	-2(2)	15(2)	0
4	212	1.22(2)	-7.05(2)	2.09(8-I-3)	-6(2)	14(2)	0
4	213	2.84(2)	-12.35(2)	-2.02(8-II-3)	6(2)	17(2)	0
4	214	-0.30(2)	-13.54(2)	2.10(8-I-3)	0	15(2)	0
4	215	0.29(2)	-10.20(2)	-2.27(8-II-3)	10(2)	20(2)	0
4	216	-0.45(2)	-13.86(2)	-2.16(8-II-3)	6(2)	18(2)	0
4	217	-1.08(2)	-8.60(2)	2.18(8-I-3)	13(2)	35(2)	0
4	218	1.96(2)	-3.62(2)	-2.02(8-II-3)	14(2)	35(2)	0
4	219	3.42(2)	-12.61(2)	2.08(8-I-3)	19(2)	36(2)	0
4	220	0.07(9-I-1)	-11.43(2)	2.16(8-I-3)	18(2)	35(2)	0
4	221	2.09(2)	-11.29(2)	-2.38(8-II-3)	22(2)	37(2)	0
4	222	-1.35(2)	-17.23(2)	-2.13(8-II-3)	22(2)	36(2)	0
4	223	-1.55(2)	-8.32(2)	-2.03(8-II-3)	14(2)	23(2)	0
4	224	1.20(2)	-6.72(2)	-2.16(8-II-3)	11(2)	22(2)	0
4	225	0.92(2)	-10.48(2)	2.12(8-I-3)	18(2)	24(2)	0
4	226	0.96(2)	-7.54(2)	2.05(8-I-3)	15(2)	24(2)	0
4	227	2.60(2)	-11.85(2)	-2.12(8-II-3)	22(2)	24(2)	0
4	228	-0.62(2)	-14.11(2)	1.98(8-I-3)	19(2)	24(2)	0
4	229	-0.20(2)	-12.42(2)	-2.21(8-II-3)	22(2)	24(2)	0
4	230	-2.59(2)	-6.38(2)	1.95(8-I-3)	16(2)	50(2)	1(2)
4	231	2.41(2)	-1.24(2)	-2.24(8-II-3)	24(2)	53(2)	0
4	232	2.08(2)	-10.89(2)	2.24(8-I-3)	35(2)	47(2)	2(2)
4	233	1.59(2)	-5.38(2)	2.14(8-I-3)	30(2)	50(2)	1(2)
4	234	5.62(2)	-12.89(2)	-2.41(8-II-3)	40(2)	41(2)	1(2)
4	235	-2.76(2)	-20.70(2)	-1.97(8-II-3)	35(2)	43(2)	1(2)
4	236	-1.58(2)	-6.58(2)	-2.60(8-II-3)	14(2)	31(2)	1(9-I-2)
4	237	-0.44(2)	-11.74(2)	-2.57(8-II-3)	25(2)	36(2)	1(9-I-2)
4	238	-1.28(2)	-2.71(2)	-2.12(8-II-3)	-17(2)	24(9-II-1)	2(2)
4	239	1.60(2)	-1.21(2)	-2.37(8-II-3)	10(9-I-1)	28(9-II-1)	1(9-I-2)
4	240	-0.53(9-II-3)	-1.81(2)	-1.68(8-II-3)	-45(2)	25(9-II-1)	4(9-I-1)
4	241	0.96(2)	-0.65(2)	-2.01(8-II-3)	-22(2)	20(9-II-1)	1(9-I-2)
4	242	0.34(9-II-3)	-2.22(2)	-1.50(8-II-3)	-48(2)	-17(9-I-1)	4(9-I-1)
4	243	-2.04(2)	-7.60(2)	-2.24(8-II-3)	24(2)	37(2)	0
4	244	0.67(2)	-8.11(2)	-2.33(8-II-3)	25(2)	38(2)	0
4	245	-0.12(9-II-4)	-9.29(2)	-2.29(8-II-3)	25(2)	24(2)	0
4	246	-0.80(2)	-8.53(2)	2.08(8-I-3)	30(2)	34(2)	0
4	247	1.70(2)	-3.70(2)	-2.02(8-II-3)	28(2)	37(2)	0
4	248	3.89(2)	-11.76(2)	-1.99(8-II-3)	35(2)	26(2)	0
4	249	-0.45(2)	-12.29(2)	2.03(8-I-3)	28(2)	29(2)	0
4	250	-1.45(2)	-7.90(2)	-2.02(8-II-3)	28(2)	22(2)	0
4	251	1.11(2)	-6.17(2)	-2.16(8-II-3)	24(2)	23(2)	0
4	252	1.49(2)	-10.11(2)	2.00(8-I-3)	30(2)	18(2)	0
4	253	0.70(2)	-7.69(2)	1.94(8-I-3)	24(2)	19(2)	0
4	254	-0.09(9-II-4)	-12.19(2)	-1.94(8-II-3)	21(2)	12(2)	0
4	255	-0.21(2)	-12.63(2)	-2.12(8-II-3)	19(2)	12(2)	0
4	256	1.71(2)	-9.40(2)	-2.49(8-II-3)	25(2)	20(2)	0
4	257	-1.41(2)	-15.79(2)	-2.24(8-II-3)	24(2)	21(2)	0
4	258	2.73(2)	-10.94(2)	-2.22(8-II-3)	22(2)	11(2)	0
4	259	-1.23(2)	-5.23(2)	-2.35(8-II-3)	9(9-I-1)	17(9-II-1)	0
4	260	0.34(2)	-6.34(2)	-2.41(8-II-3)	11(2)	18(9-II-1)	-1(9-II-2)
4	261	-0.24(9-II-3)	-1.43(2)	-1.72(8-II-3)	-39(2)	16(9-II-1)	3(9-I-1)
4	262	-1.01(2)	-2.76(2)	-2.00(8-II-3)	-24(2)	24(9-II-1)	0
4	263	0.94(2)	-1.79(2)	-2.13(8-II-3)	-9(9-I-4)	21(9-II-1)	-1(2)
4	264	0.50(9-II-3)	-2.51(2)	-1.53(8-II-3)	-38(2)	-14(9-I-1)	3(9-I-2)
4	265	-0.20(9-II-3)	-7.37(2)	-2.37(8-II-3)	11(2)	9(9-II-4)	-1(9-II-2)
4	266	-0.31(2)	-10.85(2)	-2.31(8-II-3)	12(2)	9(2)	-1(2)
4	267	-0.94(2)	-4.05(2)	-2.12(8-II-3)	-9(9-I-4)	6(2)	-1(2)
4	268	0.72(2)	-4.20(2)	-2.26(8-II-3)	4(9-II-4)	9(9-II-4)	-2(2)
4	269	-0.58(9-II-3)	-2.83(2)	-1.73(8-II-3)	-34(2)	-13(9-I-1)	-3(9-II-1)
4	270	0.67(2)	-1.75(2)	-2.00(8-II-3)	-14(2)	4(2)	-2(2)
4	271	0.60(9-II-3)	-2.91(9-II-3)	-1.58(8-II-3)	-28(2)	-4(9-II-4)	-5(9-II-1)
4	272	-0.71(8-I-3)	-3.30(2)	1.73(9-I-3)	-109(2)	-70(9-I-2)	-5(9-I-2)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
4	273	0.62(8-I-3)	-1.80(2)	1.59(9-I-3)	-85(2)	40(9-II-2)	-9(9-I-2)
4	274	0.97(2)	-6.08(2)	2.07(9-I-3)	-31(2)	-29(9-I-2)	2(2)
4	275	0.61(9-I-3)	-4.40(2)	1.91(9-I-3)	-47(2)	-31(9-I-2)	1(2)
4	276	-0.93(8-I-3)	-2.50(8-I-3)	1.60(9-I-3)	-88(2)	20(9-II-2)	-9(9-I-2)
4	277	0.32(2)	-7.67(2)	2.08(9-I-3)	-29(9-II-2)	-16(9-I-2)	2(2)
4	278	1.84(2)	-9.35(2)	1.97(9-I-3)	24(9-I-2)	-13(9-I-2)	1(2)
4	279	-0.21(2)	-9.82(2)	2.02(9-I-3)	-26(9-I-2)	-16(9-I-2)	2(2)
4	280	0.19(8-II-3)	-8.51(2)	1.87(9-I-3)	31(9-I-2)	-8(2)	0
4	281	-0.25(2)	-10.47(2)	1.90(9-I-3)	27(9-I-2)	-13(2)	1(9-I-2)
4	282	-0.71(2)	-8.31(2)	2.08(9-I-3)	29(9-I-2)	-4(9-II-2)	0
4	283	0.88(2)	-6.54(2)	1.96(9-I-3)	28(9-I-2)	-7(2)	0
4	284	1.05(2)	-10.75(2)	2.20(9-I-3)	23(9-I-2)	7(9-I-2)	-1(2)
4	285	0.57(2)	-8.60(2)	2.14(9-I-3)	24(9-I-2)	-5(9-II-2)	0
4	286	0.45(2)	-5.14(2)	1.96(9-I-3)	-22(2)	-26(9-I-2)	2(9-I-2)
4	287	0.47(8-II-3)	-4.60(2)	1.86(9-I-3)	-46(2)	-32(9-I-2)	1(9-I-2)
4	288	0.66(8-I-3)	-3.28(2)	1.71(9-I-3)	-35(2)	-4(9-I-3)	6(9-II-2)
4	289	-0.26(8-I-3)	-6.41(2)	1.98(9-I-3)	-23(2)	-8(9-II-2)	3(9-I-2)
4	290	-0.71(8-I-3)	-2.91(8-I-3)	1.61(9-I-3)	-30(2)	2(2)	-6(9-I-2)
4	291	1.02(2)	-8.46(2)	2.00(9-I-3)	-28(9-II-2)	-8(9-II-2)	2(9-I-2)
4	292	0.06(9-I-2)	-7.78(2)	2.00(9-I-3)	-25(9-II-2)	-5(2)	2(9-I-2)
4	293	0.96(2)	-9.00(2)	1.91(9-I-3)	28(9-I-2)	-15(9-II-2)	2(9-I-2)
4	294	-0.17(2)	-10.05(2)	1.96(9-I-3)	-27(9-II-2)	-12(9-II-2)	2(9-I-2)
4	295	-0.41(2)	-8.36(2)	1.96(9-I-3)	28(9-I-2)	-19(9-II-2)	1(9-I-2)
4	296	0.29(2)	-8.49(2)	1.93(9-I-3)	24(9-I-2)	-18(9-II-2)	2(9-I-2)
4	297	0.19(8-II-3)	-9.54(2)	2.12(9-I-3)	24(9-I-2)	-21(9-II-2)	-1(9-II-2)
4	298	0.64(2)	-7.64(2)	2.03(9-I-3)	21(9-I-2)	-21(9-II-2)	1(9-I-2)
4	299	0.04(8-II-4)	-11.03(2)	2.09(9-I-3)	16(9-I-2)	-21(9-II-2)	-1(9-II-2)
4	300	2.07(2)	-12.03(2)	2.01(9-I-3)	16(9-I-2)	10(9-I-2)	-1(2)
4	301	-0.35(2)	-13.47(2)	2.10(9-I-3)	19(9-I-2)	9(9-I-2)	0
4	302	1.36(2)	-11.36(2)	2.08(9-I-3)	19(9-I-2)	-21(9-II-2)	-1(9-II-2)
4	303	0.70(2)	-10.67(2)	-2.02(9-II-3)	-12(9-II-2)	11(9-I-2)	0
4	304	-0.11(2)	-13.03(2)	1.93(9-I-3)	13(9-I-2)	11(9-I-2)	0
4	305	-0.63(2)	-9.19(2)	1.97(9-I-3)	-11(9-II-2)	12(9-I-2)	0
4	306	0.73(2)	-8.94(2)	-1.97(9-II-3)	-9(9-II-2)	11(9-I-2)	0
4	307	-0.23(2)	-9.90(2)	2.17(9-I-3)	-14(2)	12(9-I-2)	0
4	308	0.99(2)	-7.72(2)	2.06(9-I-3)	-8(9-II-2)	12(9-I-2)	0
4	309	1.73(2)	-12.02(2)	2.14(9-I-3)	-15(2)	12(9-I-2)	0
4	310	0.33(2)	-11.41(2)	2.15(9-I-3)	-9(2)	12(9-I-2)	0
4	311	1.86(2)	-12.26(2)	-2.09(8-II-3)	-15(2)	12(9-I-2)	0
4	312	-0.49(2)	-14.97(2)	2.00(9-I-3)	-10(2)	12(9-I-2)	0
4	313	-0.52(2)	-9.71(2)	-2.13(8-II-3)	-11(2)	11(9-I-2)	0
4	314	0.28(2)	-11.21(2)	-2.12(8-II-3)	-9(2)	12(9-I-2)	0
4	315	-0.54(2)	-9.48(2)	2.07(8-I-3)	-6(2)	11(9-I-2)	0
4	316	1.10(2)	-7.34(2)	-2.02(8-II-3)	-6(2)	11(9-I-2)	0
4	317	1.12(2)	-11.25(2)	1.93(9-I-3)	13(9-I-2)	21(9-I-2)	0
4	318	-0.21(2)	-12.93(2)	2.00(9-I-3)	12(9-I-2)	-21(9-II-2)	0
4	319	0.11(8-II-3)	-9.98(2)	-1.95(9-II-3)	-9(9-II-2)	22(9-I-2)	0
4	320	0.23(2)	-10.87(2)	1.93(9-I-3)	8(9-I-2)	21(9-I-2)	0
4	321	-0.34(2)	-9.67(2)	2.05(9-I-3)	-8(9-II-2)	22(9-I-2)	0
4	322	0.64(2)	-8.65(2)	1.99(9-I-3)	-6(9-II-2)	22(9-I-2)	0
4	323	0.56(2)	-10.92(2)	2.13(9-I-3)	-9(2)	22(9-I-2)	0
4	324	0.50(2)	-9.68(2)	2.08(9-I-3)	-5(9-II-2)	22(9-I-2)	0
4	325	1.60(2)	-12.11(2)	2.00(9-I-3)	-10(2)	21(9-I-2)	0
4	326	-0.07(2)	-12.89(2)	2.06(9-I-3)	-5(2)	22(9-I-2)	0
4	327	0.57(2)	-10.95(2)	-2.09(8-II-3)	-9(2)	21(9-I-2)	0
4	328	-0.18(2)	-13.00(2)	-2.00(8-II-3)	-6(2)	21(9-I-2)	0
4	329	-0.54(2)	-9.59(2)	-2.01(8-II-3)	-6(2)	20(9-I-2)	0
4	330	0.58(2)	-9.28(2)	-2.05(8-II-3)	-5(2)	20(9-I-2)	0
4	331	0.25(8-II-3)	-4.39(2)	1.91(9-I-3)	-16(9-II-2)	10(9-I-2)	3(9-I-2)
4	332	0.15(8-I-3)	-4.16(2)	1.76(9-I-3)	-15(2)	9(9-I-2)	5(9-II-2)
4	333	0.22(8-II-3)	-3.41(9-I-3)	1.60(9-I-3)	-9(2)	14(9-I-2)	-5(9-I-2)
4	334	0.46(2)	-7.31(2)	1.98(9-I-3)	-25(9-II-2)	-27(9-II-2)	2(9-I-2)
4	335	-0.07(2)	-6.61(2)	1.93(9-I-3)	-24(9-II-2)	-20(9-II-2)	4(9-I-2)
4	336	0.84(2)	-8.75(2)	1.95(9-I-3)	-28(9-II-2)	-33(9-II-2)	3(9-I-2)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
4	337	-0.18(8-I-3)	-8.92(2)	1.95(9-I-3)	-25(9-II-2)	-31(9-II-2)	3(9-I-2)
4	338	0.29(8-II-3)	-8.66(2)	1.94(9-I-3)	24(9-I-2)	-36(9-II-2)	2(9-I-2)
4	339	0.10(8-II-3)	-9.26(2)	1.93(9-I-3)	-21(9-II-2)	-34(9-II-2)	3(9-I-2)
4	340	-0.25(8-I-3)	-8.84(2)	2.02(9-I-3)	21(9-I-2)	-37(9-II-2)	2(9-I-2)
4	341	0.33(2)	-8.05(2)	1.96(9-I-3)	15(9-I-2)	-36(9-II-2)	2(9-I-2)
4	342	0.65(2)	-10.52(2)	2.07(9-I-3)	17(9-I-2)	-36(9-II-2)	1(9-I-2)
4	343	0.21(2)	-9.39(2)	2.03(9-I-3)	11(9-I-2)	-36(9-II-2)	1(9-I-2)
4	344	0.41(8-II-3)	-5.18(2)	1.90(9-I-3)	-20(9-II-2)	39(9-I-2)	3(9-I-2)
4	345	-0.29(8-I-3)	-4.53(2)	1.78(9-I-3)	-10(8-I-3)	51(9-I-2)	3(9-II-2)
4	346	0.41(9-II-2)	-3.68(9-I-3)	1.59(9-I-3)	-4(9-I-3)	35(9-I-2)	-2(9-I-2)
4	347	0.50(2)	-7.98(2)	1.93(9-I-3)	-25(9-II-2)	-61(9-II-2)	3(9-I-2)
4	348	-0.19(8-I-3)	-7.43(2)	1.82(9-I-3)	-22(9-II-2)	-53(9-II-2)	5(9-I-2)
4	349	-0.90(8-I-3)	-4.84(2)	1.70(9-I-3)	-4(9-I-3)	-111(9-II-2)	0
4	350	0.22(2)	-2.70(2)	1.13(9-I-3)	0	-82(9-II-2)	-2(9-II-2)
4	351	0.39(8-II-3)	-6.05(2)	1.77(9-I-3)	-20(9-II-2)	-113(9-II-2)	-4(9-II-2)
4	352	0.17(2)	-5.22(2)	1.27(9-I-3)	0	-121(9-II-2)	-2(9-II-2)
4	353	0.08(8-I-3)	-8.92(2)	1.24(9-I-3)	0	-92(9-II-2)	1(9-I-2)
4	354	-0.10(8-II-3)	-7.56(2)	1.24(9-I-3)	0	-92(9-II-2)	1(9-I-2)
4	355	0.44(8-II-3)	-8.79(2)	1.93(9-I-3)	-21(9-II-2)	-58(9-II-2)	3(9-I-2)
4	356	0.05(8-II-3)	-9.08(2)	1.81(9-I-3)	-13(9-II-2)	-59(9-II-2)	2(9-I-2)
4	357	0.31(8-II-3)	-9.05(2)	1.79(9-I-3)	-12(9-II-2)	-81(9-II-2)	2(9-I-2)
4	358	-0.21(8-I-3)	-8.53(2)	1.97(9-I-3)	15(9-I-2)	-54(9-II-2)	2(9-I-2)
4	359	0.07(2)	-8.68(2)	1.86(9-I-3)	-8(9-II-2)	-55(9-II-2)	2(9-I-2)
4	360	0.28(8-II-3)	-9.56(2)	2.02(9-I-3)	11(9-I-2)	-52(9-II-2)	1(9-I-2)
4	361	0.10(9-II-3)	-8.71(2)	1.84(9-I-3)	-4(9-II-2)	-52(9-II-2)	1(9-I-2)
4	362	0.23(8-II-3)	-8.61(2)	1.85(9-I-3)	-8(9-II-2)	-74(9-II-2)	1(9-I-2)
4	363	-0.14(8-II-3)	-8.73(2)	1.29(9-I-3)	0	-77(9-II-2)	0
4	364	-0.16(8-I-3)	-8.31(2)	1.82(9-I-3)	5(9-I-2)	-69(9-II-2)	0
4	365	-0.16(8-II-3)	-8.95(2)	1.32(9-I-3)	0	-69(9-II-2)	0
4	366	-0.15(8-II-3)	-10.02(2)	1.31(9-I-3)	0	-66(9-II-2)	0
4	367	-0.15(8-II-3)	-9.03(2)	1.31(9-I-3)	0	-66(9-II-2)	0
4	368	1.03(2)	-11.28(2)	2.00(9-I-3)	12(9-I-2)	-35(9-II-2)	0
4	369	-0.12(2)	-11.88(2)	2.03(9-I-3)	8(9-I-2)	-35(9-II-2)	0
4	370	0.44(2)	-10.59(2)	1.93(9-I-3)	8(9-I-2)	-33(9-II-2)	0
4	371	-0.09(8-I-2)	-11.69(2)	1.96(9-I-3)	6(9-I-2)	-34(9-II-2)	0
4	372	-0.15(8-I-3)	-9.83(2)	1.98(9-I-3)	-6(9-II-2)	-32(9-II-2)	0
4	373	0.25(2)	-9.84(2)	1.95(9-I-3)	4(9-I-2)	-33(9-II-2)	0
4	374	0.11(8-II-3)	-10.32(2)	2.06(9-I-3)	-5(9-II-2)	-32(9-II-2)	0
4	375	0.34(2)	-9.35(2)	2.01(9-I-3)	-3(9-II-2)	-32(9-II-2)	0
4	376	0.85(2)	-11.47(2)	2.04(9-I-3)	-5(2)	-31(9-II-2)	0
4	377	0.11(2)	-11.16(2)	2.04(9-I-3)	-2(9-II-2)	-31(9-II-2)	0
4	378	0.95(2)	-11.63(2)	-1.98(8-II-3)	-6(2)	-31(9-II-2)	0
4	379	-0.17(2)	-12.81(2)	1.98(9-I-3)	-2(2)	-31(9-II-2)	0
4	380	-0.08(9-II-1)	-10.21(2)	-2.03(8-II-3)	-5(2)	-31(9-II-2)	0
4	381	0.14(2)	-11.10(2)	-1.99(8-II-3)	-3(2)	-31(9-II-2)	0
4	382	0.64(2)	-11.00(2)	2.02(9-I-3)	8(9-I-2)	-49(9-II-2)	0
4	383	-0.09(9-I-3)	-10.63(2)	1.90(9-I-3)	3(9-I-2)	-50(9-II-2)	0
4	384	0.24(2)	-10.86(2)	1.87(9-I-3)	2(9-I-2)	-62(9-II-2)	0
4	385	0.53(2)	-10.95(2)	1.95(9-I-3)	6(9-I-2)	-47(9-II-2)	0
4	386	-0.26(9-I-3)	-11.64(2)	1.94(9-I-3)	2(9-I-2)	-47(9-II-2)	0
4	387	0.17(8-II-3)	-10.16(2)	1.94(9-I-3)	4(9-I-2)	-45(9-II-2)	0
4	388	-0.10(9-I-3)	-10.70(2)	1.92(9-I-3)	2(9-I-2)	-46(9-II-2)	0
4	389	-0.12(8-I-3)	-10.01(2)	1.99(9-I-3)	-3(9-II-2)	-44(9-II-2)	0
4	390	0.05(9-II-2)	-9.67(2)	1.95(9-I-3)	1(9-I-2)	-45(9-II-2)	0
4	391	0.29(2)	-10.89(2)	2.01(9-I-3)	-2(9-II-2)	-44(9-II-2)	0
4	392	0.04(8-I-3)	-10.28(2)	1.98(9-I-3)	0	-44(9-II-2)	0
4	393	0.38(2)	-11.17(2)	1.93(9-I-3)	2(9-I-2)	-60(9-II-2)	0
4	394	-0.19(2)	-10.93(2)	1.34(9-I-3)	0	-61(9-II-2)	0
4	395	0.14(2)	-10.57(2)	1.93(9-I-3)	2(9-I-2)	-58(9-II-2)	0
4	396	-0.20(2)	-11.05(2)	1.32(9-I-3)	0	-59(9-II-2)	0
4	397	-0.06(2)	-9.94(2)	1.95(9-I-3)	1(9-I-2)	-57(9-II-2)	0
4	398	-0.18(2)	-10.13(2)	1.31(9-I-3)	0	-58(9-II-2)	0
4	399	0.06(8-II-3)	-10.38(2)	1.97(9-I-3)	0	-56(9-II-2)	0
4	400	-0.17(2)	-9.95(2)	1.32(9-I-3)	0	-57(9-II-2)	0

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
4	401	0.68(2)	-11.68(2)	1.96(9-I-3)	-2(2)	-43(9-II-2)	0
4	402	-0.11(2)	-11.84(2)	1.96(9-I-3)	0	-43(9-II-2)	0
4	403	0.22(2)	-11.11(2)	-1.95(8-II-3)	-2(2)	-43(9-II-2)	0
4	404	-0.10(2)	-12.00(2)	1.90(8-I-3)	0	-43(9-II-2)	0
4	405	0.04(2)	-10.32(2)	-1.93(8-II-3)	-1(2)	-46(9-II-2)	0
4	406	-0.08(2)	-10.09(2)	-1.94(8-II-3)	0	-46(9-II-2)	0
4	407	0.24(2)	-11.36(2)	1.96(9-I-3)	0	-56(9-II-2)	0
4	408	-0.18(2)	-10.98(2)	1.32(9-I-3)	0	-56(9-II-2)	0
4	409	0.24(2)	-11.60(2)	1.91(8-I-3)	0	-55(9-II-2)	0
4	410	-0.19(2)	-11.86(2)	1.32(8-I-3)	0	-56(9-II-2)	0
4	411	-0.12(8-I-3)	-10.92(2)	-1.88(8-II-3)	0	-55(9-II-2)	0
4	412	-0.17(2)	-11.43(2)	1.30(8-I-3)	0	-55(9-II-2)	0
4	413	-0.06(9-II-3)	-9.93(2)	-1.90(8-II-3)	0	-56(9-II-2)	0
4	414	-0.11(2)	-10.20(2)	-1.24(8-II-3)	0	-56(9-II-2)	0
4	415	1.42(2)	-11.19(2)	2.07(8-I-3)	0	11(9-I-2)	0
4	416	0.38(2)	-10.27(2)	2.08(8-I-3)	-3(2)	11(9-I-2)	1(2)
4	417	1.53(2)	-11.27(2)	-2.13(8-II-3)	6(2)	11(9-I-1)	0
4	418	-0.39(2)	-13.58(2)	-2.01(8-II-3)	1(2)	11(9-I-1)	0
4	419	-0.60(2)	-9.24(2)	-2.14(8-II-3)	11(2)	12(2)	0
4	420	0.31(2)	-10.28(2)	-2.14(8-II-3)	6(2)	11(9-I-1)	0
4	421	-0.33(2)	-9.33(2)	2.03(8-I-3)	15(2)	13(2)	0
4	422	0.99(2)	-7.23(2)	-2.03(8-II-3)	10(2)	12(2)	0
4	423	1.69(2)	-11.12(2)	-1.97(8-II-3)	19(2)	13(2)	0
4	424	0.14(2)	-10.76(2)	2.01(8-I-3)	14(2)	13(2)	0
4	425	1.17(2)	-10.44(2)	-2.19(8-II-3)	22(2)	12(2)	0
4	426	-0.39(2)	-13.08(2)	-2.08(8-II-3)	17(2)	12(2)	0
4	427	0.36(2)	-10.27(2)	2.06(8-I-3)	-3(2)	19(9-I-2)	0
4	428	0.57(2)	-8.93(2)	2.02(8-I-3)	-3(2)	19(9-I-2)	0
4	429	1.35(2)	-11.24(2)	-2.01(8-II-3)	1(2)	18(9-I-2)	0
4	430	-0.06(9-II-4)	-11.82(2)	2.01(8-I-3)	0	19(9-I-2)	0
4	431	0.40(2)	-10.21(2)	-2.12(8-II-3)	6(2)	18(9-I-1)	0
4	432	-0.11(2)	-11.89(2)	-2.06(8-II-3)	2(2)	18(9-I-1)	0
4	433	-0.49(2)	-9.24(2)	-2.03(8-II-3)	10(2)	18(9-I-1)	0
4	434	0.53(2)	-8.78(2)	-2.08(8-II-3)	5(2)	18(9-I-1)	0
4	435	0.61(2)	-10.18(2)	1.98(8-I-3)	14(2)	18(9-I-1)	0
4	436	0.46(2)	-9.00(2)	-1.99(8-II-3)	8(2)	18(9-I-1)	0
4	437	1.29(2)	-10.78(2)	-2.07(8-II-3)	17(2)	18(9-I-1)	0
4	438	-0.20(2)	-11.86(2)	-2.00(8-II-3)	10(2)	18(9-I-1)	0
4	439	0.13(9-I-3)	-11.01(2)	-2.11(8-II-3)	12(2)	17(9-I-1)	0
4	440	-0.56(2)	-8.63(2)	-2.14(8-II-3)	24(2)	11(2)	0
4	441	0.45(2)	-9.25(2)	-2.17(8-II-3)	18(2)	11(2)	0
4	442	0.22(2)	-9.45(2)	-2.15(8-II-3)	18(2)	17(9-I-1)	0
4	443	-0.16(9-II-3)	-8.78(2)	-1.97(8-II-3)	24(2)	9(9-I-1)	0
4	444	0.80(2)	-7.14(2)	-2.05(8-II-3)	19(2)	10(9-I-1)	0
4	445	1.15(2)	-10.11(2)	-1.93(8-II-3)	21(2)	9(9-I-1)	0
4	446	0.35(2)	-9.31(2)	-1.96(8-II-3)	17(2)	9(9-I-1)	0
4	447	1.41(2)	-10.53(2)	-2.14(8-II-3)	17(2)	7(9-I-1)	-1(2)
4	448	-0.67(2)	-12.55(2)	-2.04(8-II-3)	13(2)	8(9-I-1)	-1(2)
4	449	1.26(2)	-8.77(2)	-2.29(8-II-3)	11(2)	5(9-I-1)	-2(2)
4	450	-0.26(2)	-11.13(2)	-2.20(8-II-3)	10(2)	6(9-I-1)	-1(2)
4	451	-0.38(9-II-3)	-5.87(2)	-2.25(8-II-3)	4(9-II-4)	3(9-I-1)	-2(2)
4	452	0.17(2)	-7.36(2)	-2.25(8-II-3)	7(9-I-1)	4(9-I-1)	-2(2)
4	453	-0.76(2)	-3.72(2)	-2.03(8-II-3)	-14(2)	4(9-I-1)	-2(2)
4	454	0.56(2)	-3.59(2)	-2.14(8-II-3)	-7(8-I-3)	2(8-II-3)	-2(2)
4	455	-0.79(9-II-3)	-2.98(2)	-1.69(8-II-3)	-27(2)	-6(9-I-1)	-5(9-II-1)
4	456	0.56(9-II-3)	-2.35(2)	-1.93(8-II-3)	-14(8-I-3)	6(9-I-1)	-2(2)
4	457	0.41(9-II-3)	-3.93(9-II-3)	-1.59(8-II-3)	-21(9-I-3)	-3(9-II-1)	-6(9-II-1)
4	458	-0.28(2)	-8.73(2)	-2.05(8-II-3)	19(2)	16(9-I-1)	0
4	459	0.48(2)	-8.30(2)	-2.10(8-II-3)	12(2)	17(9-I-1)	0
4	460	0.34(2)	-9.39(2)	-1.97(8-II-3)	17(2)	-16(9-II-1)	0
4	461	0.40(2)	-8.36(2)	-2.01(8-II-3)	12(2)	-16(9-II-1)	0
4	462	1.23(2)	-10.35(2)	-2.03(8-II-3)	13(2)	-16(9-II-1)	-1(2)
4	463	0.15(9-I-3)	-10.55(2)	-1.99(8-II-3)	10(2)	-16(9-II-1)	-1(2)
4	464	1.03(2)	-9.50(2)	-2.18(8-II-3)	9(2)	-15(9-II-1)	-2(2)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
4	465	-0.35(2)	-11.41(2)	-2.10(8-II-3)	7(2)	-15(9-II-1)	-1(2)
4	466	0.36(9-I-3)	-7.32(2)	-2.22(8-II-3)	7(9-I-1)	-13(9-II-1)	-2(2)
4	467	0.16(9-I-3)	-8.98(2)	-2.18(8-II-3)	6(9-I-1)	-14(9-II-1)	-2(2)
4	468	-0.54(9-II-3)	-5.05(2)	-2.12(8-II-3)	-7(8-I-3)	-12(9-II-1)	-2(2)
4	469	0.24(2)	-5.67(2)	-2.16(8-II-3)	-4(9-II-1)	-13(9-II-1)	-2(2)
4	470	-0.45(9-II-3)	-2.79(9-II-3)	-1.76(8-II-3)	-21(9-I-3)	15(9-I-1)	-5(9-II-1)
4	471	-0.74(9-II-3)	-3.44(2)	-1.94(8-II-3)	-13(2)	-1(2)	-2(2)
4	472	0.39(2)	-3.46(2)	-2.02(8-II-3)	-6(2)	-7(9-II-1)	-2(2)
4	473	0.38(8-II-3)	-4.19(9-II-3)	-1.63(8-II-3)	-14(9-I-4)	-4(9-II-4)	-4(9-II-1)
4	474	-0.15(2)	-9.88(2)	2.00(8-I-3)	-3(2)	-30(9-II-2)	0
4	475	0.33(2)	-9.19(2)	-1.98(8-II-3)	-2(2)	-31(9-II-2)	0
4	476	-0.15(2)	-9.84(2)	-1.95(8-II-3)	-2(2)	-43(9-II-2)	0
4	477	0.68(2)	-10.74(2)	1.99(8-I-3)	0	-30(9-II-2)	0
4	478	0.16(9-I-3)	-10.35(2)	1.99(8-I-3)	-1(2)	-30(9-II-2)	0
4	479	0.75(2)	-10.75(2)	-2.04(8-II-3)	2(2)	-30(9-II-1)	0
4	480	-0.14(2)	-11.81(2)	-1.99(8-II-3)	0	-30(9-II-2)	0
4	481	-0.12(9-II-4)	-9.63(2)	-2.06(8-II-3)	5(2)	-30(9-II-1)	0
4	482	0.15(9-I-3)	-10.32(2)	-2.05(8-II-3)	2(2)	-30(9-II-1)	0
4	483	-0.13(9-II-3)	-9.62(2)	-2.00(8-II-3)	8(2)	-30(9-II-1)	0
4	484	0.33(2)	-8.89(2)	-2.03(8-II-3)	3(2)	-30(9-II-1)	0
4	485	0.84(2)	-10.50(2)	-2.00(8-II-3)	10(2)	-30(9-II-1)	0
4	486	0.07(9-I-1)	-10.40(2)	-1.98(8-II-3)	5(2)	-30(9-II-1)	0
4	487	0.61(2)	-10.05(2)	-2.09(8-II-3)	12(2)	-30(9-II-1)	0
4	488	-0.16(2)	-11.37(2)	-2.03(8-II-3)	6(2)	-30(9-II-1)	0
4	489	0.17(2)	-10.27(2)	1.97(8-I-3)	-1(2)	-43(9-II-2)	0
4	490	0.22(8-I-3)	-9.74(2)	1.91(8-I-3)	0	-43(9-II-2)	0
4	491	0.56(2)	-10.91(2)	-2.00(8-II-3)	0	-43(9-II-2)	0
4	492	-0.31(8-II-3)	-11.02(2)	-1.91(8-II-3)	0	-43(9-II-2)	0
4	493	0.18(2)	-10.22(2)	-2.04(8-II-3)	2(2)	-43(9-II-1)	0
4	494	-0.11(2)	-11.04(2)	-1.88(8-II-3)	0	-43(9-II-1)	0
4	495	-0.15(8-I-3)	-10.01(2)	-1.91(8-II-3)	0	-55(9-II-2)	0
4	496	-0.11(2)	-9.78(2)	-1.29(8-II-3)	0	-56(9-II-2)	0
4	497	0.28(8-II-3)	-10.65(2)	-1.92(8-II-3)	0	-55(9-II-2)	0
4	498	-0.12(2)	-10.34(2)	-1.33(8-II-3)	0	-55(9-II-2)	0
4	499	0.15(2)	-10.95(2)	-1.86(8-II-3)	0	-55(9-II-1)	0
4	500	-0.13(2)	-10.98(2)	-1.36(8-II-3)	0	-55(9-II-2)	0
4	501	-0.11(2)	-10.28(2)	-1.34(8-II-3)	0	-57(9-II-1)	0
4	502	-0.11(2)	-10.39(2)	-1.34(8-II-3)	0	-57(9-II-1)	0
4	503	-0.12(2)	-9.50(2)	-2.03(8-II-3)	3(2)	-43(9-II-1)	0
4	504	0.04(8-I-3)	-9.58(2)	-1.92(8-II-3)	0	-43(9-II-1)	0
4	505	-0.16(9-II-3)	-9.54(2)	-1.90(8-II-3)	0	-56(9-II-1)	0
4	506	0.30(2)	-10.07(2)	-2.00(8-II-3)	5(2)	-43(9-II-1)	0
4	507	0.07(8-I-3)	-9.59(2)	-1.93(8-II-3)	1(2)	-43(9-II-1)	0
4	508	0.53(2)	-10.40(2)	-2.03(8-II-3)	6(2)	-43(9-II-1)	0
4	509	-0.16(2)	-10.85(2)	-1.88(8-II-3)	2(2)	-43(9-II-1)	0
4	510	-0.05(2)	-9.69(2)	-1.94(8-II-3)	1(2)	-56(9-II-1)	0
4	511	-0.13(2)	-9.54(2)	-1.37(8-II-3)	0	-56(9-II-1)	0
4	512	0.24(2)	-10.47(2)	-1.86(8-II-3)	2(2)	-56(9-II-1)	0
4	513	-0.15(2)	-9.98(2)	-1.37(8-II-3)	0	-56(9-II-1)	0
4	514	-0.15(2)	-10.23(2)	-1.34(8-II-3)	0	-57(9-II-1)	0
4	515	-0.17(2)	-10.91(2)	-1.34(8-II-3)	0	-57(9-II-1)	0
4	516	-0.19(9-II-3)	-9.06(2)	-2.08(8-II-3)	12(2)	-29(9-II-1)	0
4	517	0.17(9-I-3)	-9.56(2)	-2.08(8-II-3)	6(2)	-29(9-II-1)	0
4	518	0.21(9-I-3)	-9.05(2)	-2.01(8-II-3)	12(2)	-29(9-II-1)	0
4	519	0.28(2)	-8.45(2)	-2.04(8-II-3)	6(2)	-29(9-II-1)	0
4	520	0.65(2)	-9.80(2)	-1.99(8-II-3)	10(2)	-28(9-II-1)	-1(2)
4	521	0.20(9-I-3)	-9.40(2)	-2.00(8-II-3)	5(2)	-29(9-II-1)	-1(2)
4	522	0.97(2)	-9.87(2)	-2.08(8-II-3)	7(2)	-27(9-II-1)	-1(2)
4	523	-0.21(9-II-3)	-10.78(2)	-2.03(8-II-3)	5(9-I-1)	-28(9-II-1)	-1(2)
4	524	0.55(2)	-8.40(2)	-2.16(8-II-3)	6(9-I-1)	-26(9-II-1)	-2(2)
4	525	-0.24(9-II-3)	-9.94(2)	-2.10(8-II-3)	5(9-I-1)	-27(9-II-1)	-1(2)
4	526	-0.31(9-II-3)	-6.24(2)	-2.14(8-II-3)	-4(9-II-1)	-24(9-II-1)	-2(2)
4	527	0.30(9-I-3)	-7.34(2)	-2.13(8-II-3)	4(9-I-1)	-25(9-II-1)	-2(2)
4	528	-0.50(9-II-3)	-4.30(2)	-2.03(8-II-3)	-6(2)	-24(9-II-1)	-2(2)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
4	529	0.29(9-I-3)	-4.76(2)	-2.09(8-II-3)	-3(9-II-1)	-22(9-II-1)	-2(2)
4	530	-0.69(9-II-3)	-3.51(9-II-3)	-1.80(8-II-3)	-14(9-I-4)	-15(9-II-1)	-4(9-II-1)
4	531	0.21(2)	-3.21(2)	-1.98(8-II-3)	-7(2)	-25(9-II-1)	-2(2)
4	532	0.21(8-II-3)	-5.03(9-II-3)	-1.68(8-II-3)	-10(9-I-1)	-24(9-II-1)	-5(9-II-1)
4	533	0.20(2)	-9.46(2)	-2.07(8-II-3)	6(2)	-42(9-II-1)	0
4	534	-0.12(2)	-10.37(2)	-1.93(8-II-3)	2(2)	-43(9-II-1)	0
4	535	0.36(9-I-3)	-9.69(2)	-1.91(8-II-3)	2(2)	-55(9-II-1)	0
4	536	0.17(9-I-3)	-8.98(2)	-2.02(8-II-3)	6(2)	-42(9-II-1)	0
4	537	0.18(8-II-3)	-9.02(2)	-1.98(8-II-3)	2(2)	-42(9-II-1)	0
4	538	0.29(9-I-3)	-9.38(2)	-1.98(8-II-3)	5(2)	-41(9-II-1)	0
4	539	0.08(9-I-4)	-8.97(2)	-1.97(8-II-3)	2(2)	-41(9-II-1)	0
4	540	0.63(2)	-9.85(2)	-2.00(8-II-3)	5(9-I-1)	-40(9-II-1)	-1(2)
4	541	0.14(9-I-3)	-9.99(2)	-1.97(8-II-3)	2(9-I-1)	-40(9-II-1)	0
4	542	0.56(2)	-9.17(2)	-2.06(8-II-3)	5(9-I-1)	-39(9-II-1)	-1(2)
4	543	-0.22(9-II-3)	-10.20(2)	-2.00(8-II-3)	2(9-I-1)	-40(9-II-1)	0
4	544	-0.40(9-II-3)	-9.04(2)	-1.97(8-II-3)	2(2)	-54(9-II-1)	0
4	545	-0.19(2)	-9.76(2)	-1.36(8-II-3)	0	-55(9-II-1)	0
4	546	0.26(9-I-3)	-9.06(2)	-1.96(8-II-3)	2(2)	-54(9-II-1)	0
4	547	-0.20(2)	-8.99(2)	-1.34(8-II-3)	0	-54(9-II-1)	0
4	548	0.30(9-I-3)	-9.67(2)	-1.96(8-II-3)	2(9-I-1)	-53(9-II-1)	0
4	549	-0.21(2)	-9.43(2)	-1.32(8-II-3)	0	-53(9-II-1)	0
4	550	0.34(9-I-3)	-9.67(2)	-1.98(8-II-3)	2(9-I-1)	-52(9-II-1)	0
4	551	-0.20(2)	-10.02(2)	-1.32(8-II-3)	0	-53(9-II-1)	0
4	552	0.40(9-I-3)	-7.32(2)	-2.09(8-II-3)	4(9-I-1)	-38(9-II-1)	-1(2)
4	553	0.32(9-I-3)	-8.56(2)	-2.03(8-II-3)	3(9-I-1)	-39(9-II-1)	-1(2)
4	554	-0.50(9-II-3)	-5.37(2)	-2.07(8-II-3)	-3(9-II-1)	-37(9-II-1)	-1(2)
4	555	0.49(9-I-3)	-6.15(2)	-2.02(8-II-3)	-4(9-II-1)	-38(9-II-1)	-1(2)
4	556	-0.54(9-II-3)	-3.59(9-II-3)	-1.85(8-II-3)	-12(8-II-4)	-40(9-II-1)	-5(9-II-1)
4	557	-0.67(9-II-3)	-3.81(2)	-1.98(8-II-3)	-5(2)	-29(9-II-1)	-1(2)
4	558	0.40(9-I-3)	-4.27(2)	-1.97(8-II-3)	-6(9-II-4)	-33(9-II-1)	-1(9-I-1)
4	559	0.20(9-I-1)	-5.01(9-II-3)	-1.69(8-II-3)	-8(9-I-1)	15(9-I-1)	-3(9-II-1)
4	560	0.31(9-I-3)	-8.34(2)	-1.99(8-II-3)	3(9-I-1)	-52(9-II-1)	0
4	561	-0.14(2)	-9.32(2)	-1.32(8-II-3)	0	-52(9-II-1)	0
4	562	0.21(9-I-3)	-6.32(2)	-1.98(8-II-3)	-4(9-II-1)	-52(9-II-1)	0
4	563	0.08(9-I-4)	-7.35(2)	-1.32(8-II-3)	0	-52(9-II-1)	0
4	564	-0.42(9-II-3)	-4.78(2)	-1.96(8-II-3)	-5(9-II-4)	-54(9-II-1)	-1(9-I-1)
4	565	0.19(9-I-4)	-5.20(2)	-1.32(8-II-3)	0	-52(9-II-1)	0
4	566	-0.61(9-II-3)	-5.21(9-II-3)	-1.81(8-II-3)	-6(8-II-4)	-53(9-II-1)	-2(9-II-1)
4	567	0.38(9-I-3)	-3.34(2)	-1.35(8-II-3)	0	-57(9-II-1)	0
4	568	0.44(9-I-3)	-4.47(9-II-4)	-1.23(8-II-3)	0	33(9-I-1)	0
4	1	-0.59(8-I-1)	-0.99(9-II-1)	-0.49(8-I-1)	43(8-I-1)	-410(2)	54(9-II-1)
4	2	-0.60(8-I-1)	-0.94(9-II-1)	0.48(8-II-1)	-61(8-II-1)	-552(2)	51(9-II-1)
4	3	-0.54(8-I-1)	-0.85(9-II-1)	0.43(8-II-1)	-88(2)	-682(2)	46(9-II-1)
4	4	0.48(8-II-1)	-0.75(8-II-1)	0.36(8-II-1)	-139(2)	-794(2)	41(8-I-4)
4	5	0.50(8-II-1)	-0.71(8-II-1)	0.29(8-II-1)	-154(2)	-835(2)	37(8-I-4)
4	6	0.47(8-II-1)	-0.68(8-II-1)	-0.24(8-I-1)	-151(2)	-820(2)	34(8-I-1)
4	7	0.45(8-II-1)	-0.66(8-II-1)	-0.25(8-I-1)	-149(2)	-813(2)	28(8-I-1)
4	8	0.47(8-II-1)	-0.64(8-II-1)	-0.27(8-I-1)	-162(2)	-828(2)	25(8-I-1)
4	9	0.53(8-II-1)	-0.63(8-II-1)	-0.30(8-II-1)	-185(2)	-865(2)	27(8-I-1)
4	10	0.59(8-II-1)	-0.61(8-II-1)	-0.37(9-I-1)	-187(2)	-893(2)	30(8-I-1)
4	11	-0.77(8-I-1)	-0.59(8-II-4)	-0.42(2)	-152(8-II-1)	-844(2)	36(8-I-4)
4	12	-0.87(8-I-1)	-0.57(8-II-4)	-0.43(2)	-102(8-II-1)	-687(2)	57(9-II-1)
4	13	-0.69(8-I-1)	-0.55(9-I-1)	-0.39(8-II-1)	73(8-I-1)	-607(2)	65(9-II-1)
4	14	-0.60(8-II-1)	-0.56(9-I-1)	-0.28(8-II-1)	59(9-II-1)	-560(2)	59(9-II-1)
4	15	-0.69(8-II-1)	-0.52(9-I-1)	-0.13(2)	79(8-II-1)	-470(2)	60(9-II-1)
4	16	-0.53(8-II-1)	-0.44(9-I-1)	-0.27(8-I-1)	49(8-II-1)	-325(2)	62(8-I-4)
4	17	-0.56(8-I-1)	-0.39(8-I-1)	-0.38(8-I-1)	43(9-I-1)	-251(2)	41(8-I-4)
4	18	-0.97(9-I-1)	0.77(8-II-1)	-0.34(8-I-1)	154(9-I-1)	-117(8-II-1)	54(2)
4	19	-0.69(9-I-1)	0.52(8-II-1)	0.27(8-II-1)	207(9-I-1)	63(8-I-1)	128(2)
4	20	-0.70(9-I-1)	-0.34(8-I-1)	0.37(8-II-1)	187(9-I-1)	112(9-I-1)	119(2)
4	21	-0.75(9-I-1)	-0.57(9-I-1)	0.48(8-II-1)	-205(9-II-1)	156(9-I-1)	92(9-I-1)
4	22	-0.81(9-I-1)	-0.82(9-I-1)	0.57(8-II-4)	-268(9-II-1)	179(9-I-1)	-76(9-II-1)
4	23	-0.85(9-I-1)	-1.12(9-I-1)	0.62(8-II-4)	-307(9-II-1)	206(9-I-1)	-103(9-II-1)
4	24	-1.04(9-I-1)	-1.46(9-I-1)	0.58(8-II-4)	-290(9-II-1)	242(9-I-1)	-114(9-II-1)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
4	25	-1.71(9-I-1)	-1.67(9-I-1)	0.38(8-II-4)	257(9-I-1)	243(9-I-1)	-98(9-II-1)
4	26	-1.33(9-I-1)	-1.11(9-I-1)	0.55(8-II-4)	184(9-I-1)	215(9-I-1)	-89(9-II-1)
4	27	-0.83(9-I-1)	-0.91(9-I-1)	0.63(9-I-1)	127(9-I-1)	-225(9-II-1)	-77(9-II-1)
4	28	-0.50(8-I-1)	-0.81(9-I-1)	0.65(9-I-1)	50(9-I-1)	-251(9-II-1)	-60(9-II-1)
4	29	-0.50(9-II-2)	-0.75(9-I-1)	0.57(8-II-4)	45(9-II-2)	-231(9-II-1)	-46(9-II-1)
4	30	-0.65(9-II-2)	-0.73(9-I-1)	0.48(8-II-4)	63(9-II-2)	-203(9-II-1)	-36(9-II-1)
4	31	-0.76(9-II-2)	-0.73(9-I-1)	0.39(8-II-1)	67(9-II-2)	-198(9-II-1)	-32(9-II-1)
4	32	-0.80(9-II-2)	-0.67(9-I-2)	0.33(8-II-1)	66(9-II-1)	-202(9-II-4)	-29(9-II-1)
4	33	-0.80(9-II-2)	-0.66(9-I-3)	0.29(8-II-2)	63(9-II-1)	-212(9-II-2)	-26(9-II-1)
4	34	-0.77(9-II-2)	-0.66(9-I-3)	-0.33(8-I-2)	58(9-II-2)	-231(9-II-2)	29(9-I-1)
4	35	-0.69(9-II-2)	-0.67(9-I-3)	-0.47(9-I-2)	48(9-II-4)	-263(9-II-2)	36(9-I-1)
4	36	-0.56(8-I-4)	-0.70(9-I-2)	-0.63(9-I-2)	39(8-I-1)	-310(9-II-2)	47(9-I-1)
4	37	-0.46(8-I-1)	-0.75(9-I-2)	-0.77(9-I-2)	51(9-I-2)	-371(9-II-2)	64(9-I-1)
4	38	-0.59(9-I-2)	-1.05(9-I-2)	-0.96(9-I-2)	114(9-I-2)	-432(9-II-2)	89(9-I-2)
4	39	-1.13(9-I-2)	-1.64(9-I-2)	-1.19(9-I-2)	161(9-I-2)	523(9-I-2)	109(9-I-2)
4	40	-1.04(9-I-2)	-3.82(9-I-2)	-1.64(9-I-2)	-180(9-II-2)	607(9-I-2)	75(9-I-1)
4	41	-1.03(9-I-2)	-1.42(9-I-2)	-2.24(9-I-2)	-114(9-II-2)	263(9-I-2)	149(9-I-2)
4	42	-1.11(9-I-2)	-2.12(9-II-2)	-1.86(9-I-2)	-116(9-I-2)	296(9-II-2)	119(9-I-2)
4	43	-0.89(9-I-2)	-3.24(9-II-2)	-0.79(8-I-2)	-242(9-I-2)	542(9-II-2)	-65(8-II-1)
4	44	-0.62(8-I-2)	-2.47(9-II-2)	-0.92(8-I-3)	-231(9-I-2)	398(9-II-2)	-125(8-II-3)
4	45	-0.59(8-I-1)	-1.22(8-II-1)	-0.99(8-I-3)	95(9-II-1)	141(8-II-1)	-99(8-II-3)
4	46	-0.58(2)	-1.28(8-II-1)	-0.68(8-I-4)	93(2)	-154(8-I-1)	-55(8-II-1)
4	47	-0.71(2)	1.25(8-I-1)	-0.55(8-I-1)	87(8-II-1)	-226(8-I-1)	35(8-I-1)
4	48	-0.60(2)	-1.03(8-II-1)	-0.60(8-I-1)	60(8-I-1)	-289(8-I-1)	40(8-I-1)
4	49	-0.77(9-I-1)	-1.11(9-I-1)	0.42(8-II-4)	199(9-I-1)	224(9-I-1)	-52(9-II-1)
4	50	-0.88(9-I-1)	-1.24(9-I-1)	0.39(8-II-1)	199(9-I-1)	246(9-I-1)	-89(9-II-1)
4	51	-0.74(9-I-1)	-1.02(9-I-1)	0.33(8-II-1)	162(9-I-1)	241(9-I-1)	-34(9-II-1)
4	52	-0.58(8-I-1)	-0.85(9-I-1)	0.22(8-II-1)	129(9-I-1)	269(2)	63(2)
4	53	-0.68(9-I-1)	-0.88(9-I-1)	0.36(8-II-1)	171(9-I-1)	199(2)	60(2)
4	54	-0.53(8-I-1)	-0.49(9-I-1)	-0.13(8-I-1)	75(8-II-1)	62(8-I-1)	121(2)
4	55	-0.60(8-I-1)	-0.67(9-I-1)	0.23(8-II-1)	120(9-I-1)	158(2)	118(2)
4	56	-0.45(8-II-1)	-0.59(9-I-1)	-0.17(2)	90(8-II-1)	-123(2)	91(9-II-1)
4	57	-0.51(8-I-1)	-0.61(9-I-1)	-0.15(2)	80(8-II-2)	57(8-I-1)	97(9-II-1)
4	58	-0.47(8-II-1)	-0.58(9-I-1)	-0.22(2)	74(9-II-1)	-264(2)	93(9-II-1)
4	59	-0.54(8-I-1)	-0.69(9-I-1)	-0.12(8-I-1)	99(8-II-1)	177(2)	110(2)
4	60	-0.51(8-I-1)	-0.67(9-I-1)	-0.18(2)	80(9-II-1)	54(8-I-1)	96(9-II-1)
4	61	-0.53(8-I-1)	-0.66(9-I-1)	-0.17(2)	87(8-I-1)	54(9-II-1)	87(9-II-1)
4	62	-0.52(8-I-1)	-0.71(9-I-1)	-0.13(8-I-2)	94(1)	148(2)	102(2)
4	63	-0.55(8-I-1)	-0.64(9-I-1)	-0.20(2)	70(8-I-1)	-226(2)	98(9-II-1)
4	64	-0.59(9-I-1)	-0.76(9-I-1)	0.31(8-II-1)	97(2)	263(2)	-28(9-II-2)
4	65	-0.65(9-I-1)	-0.92(9-I-1)	0.27(8-II-1)	116(9-I-1)	253(2)	-37(9-II-2)
4	66	-0.58(9-I-1)	-0.79(9-I-1)	0.25(8-II-1)	127(2)	330(2)	14(2)
4	67	-0.81(9-I-1)	-0.82(9-I-1)	0.41(8-II-4)	104(9-I-1)	230(9-I-1)	-44(9-II-1)
4	68	-0.52(8-I-1)	-0.76(9-I-1)	0.15(8-II-1)	109(1)	301(2)	65(2)
4	69	-0.53(9-I-1)	-0.78(9-I-1)	0.43(8-II-4)	63(8-II-1)	204(9-I-1)	-35(9-II-1)
4	70	-0.44(8-I-1)	-0.70(9-I-1)	0.39(8-II-4)	85(9-II-2)	201(9-I-1)	-20(8-II-2)
4	71	-0.49(8-I-1)	-0.74(9-I-1)	0.31(8-II-1)	90(9-II-2)	257(2)	-23(8-II-1)
4	72	-0.63(9-II-2)	-0.57(9-I-3)	0.29(8-II-1)	87(9-II-1)	152(9-I-1)	-28(9-II-1)
4	73	-0.50(8-I-3)	-0.55(1)	0.26(8-II-1)	102(9-II-1)	281(2)	-27(8-I-2)
4	74	-0.58(9-II-2)	-0.57(9-I-1)	0.29(8-II-1)	100(9-II-1)	178(9-I-1)	-27(8-I-2)
4	75	-0.47(9-II-2)	-0.63(9-I-1)	0.33(8-II-1)	97(9-II-2)	211(2)	-20(8-II-2)
4	76	-0.45(8-I-1)	-0.53(1)	0.21(8-II-1)	99(9-II-4)	408(2)	29(8-I-2)
4	77	-0.44(8-I-1)	-0.54(9-I-1)	0.21(8-II-1)	109(9-II-4)	384(2)	21(8-I-1)
4	78	-0.47(8-I-1)	-0.67(9-I-1)	0.22(8-II-1)	112(9-II-2)	363(2)	19(2)
4	79	-0.48(8-I-1)	-0.52(1)	-0.19(8-I-2)	60(8-I-1)	87(9-II-1)	45(8-I-1)
4	80	-0.46(8-I-1)	-0.58(8-II-1)	-0.21(8-I-1)	-74(2)	-232(2)	-40(8-II-1)
4	81	-0.50(8-I-1)	-0.56(8-II-4)	-0.24(9-I-1)	-114(2)	-373(2)	41(8-I-1)
4	82	-0.46(8-I-1)	-0.51(1)	-0.17(8-I-2)	82(8-I-1)	336(2)	37(8-I-1)
4	83	-0.46(8-I-1)	-0.53(9-I-1)	-0.14(8-I-2)	98(8-I-1)	348(2)	41(8-I-1)
4	84	-0.48(8-I-1)	-0.64(9-I-1)	0.13(8-II-2)	104(8-I-1)	320(2)	61(2)
4	85	-0.55(8-I-1)	-0.57(9-I-1)	-0.19(9-I-2)	91(8-I-1)	-124(2)	81(2)
4	86	-0.57(8-I-1)	-0.66(9-I-1)	-0.17(2)	103(8-I-1)	-49(9-I-1)	106(2)
4	87	-0.61(8-I-1)	-0.57(9-I-1)	-0.27(2)	90(8-I-1)	-334(2)	64(9-II-1)
4	88	-0.51(8-I-1)	-0.60(9-I-1)	-0.15(9-I-2)	99(8-I-1)	121(9-II-1)	76(2)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
4	89	-0.67(8-I-1)	-0.57(8-II-4)	-0.28(2)	-122(8-II-1)	-496(2)	51(8-I-4)
4	90	-0.55(8-I-1)	-0.56(9-I-1)	-0.22(9-I-1)	-79(8-II-1)	-206(2)	56(2)
4	91	-0.57(8-I-1)	-0.56(8-II-4)	-0.26(9-I-1)	-112(2)	-450(2)	45(8-I-1)
4	92	-0.50(8-I-1)	-0.54(9-I-1)	-0.16(9-I-2)	83(8-I-1)	121(9-II-1)	52(8-I-1)
4	93	-0.45(8-I-1)	-0.60(8-II-1)	-0.23(8-I-1)	-67(8-II-1)	-222(2)	36(8-I-1)
4	94	-0.45(8-I-1)	-0.61(8-II-1)	-0.23(8-I-1)	54(8-I-1)	112(9-II-1)	-55(8-II-1)
4	95	-0.45(8-I-1)	-0.64(8-II-1)	0.24(8-II-1)	-85(2)	-350(2)	-43(8-II-1)
4	96	-0.46(8-I-1)	-0.74(9-II-1)	0.32(8-II-1)	-97(2)	-495(2)	-54(8-II-4)
4	97	-0.47(8-I-1)	-0.73(9-II-1)	0.30(8-II-1)	-59(8-II-1)	-206(2)	-77(8-II-4)
4	98	-0.45(8-I-1)	-0.69(8-II-1)	0.28(8-II-1)	-87(2)	-416(2)	-43(8-II-1)
4	99	-0.48(8-I-1)	-0.89(9-II-1)	0.34(8-II-1)	-60(8-II-1)	-337(2)	-81(8-II-4)
4	100	-0.47(8-I-1)	-0.74(9-II-1)	-0.28(8-I-2)	68(8-I-1)	172(9-II-1)	-83(8-II-1)
4	101	-0.48(8-I-1)	-1.04(9-II-1)	-0.36(8-I-2)	84(8-I-2)	250(9-II-2)	-115(8-II-4)
4	102	-0.51(8-I-1)	-1.58(9-II-1)	-0.49(8-I-2)	88(8-I-3)	354(9-II-2)	-147(8-II-3)
4	103	-0.52(8-I-1)	-1.08(9-II-1)	-0.41(8-I-1)	60(8-I-4)	-211(2)	-95(9-I-2)
4	104	-0.52(8-I-1)	-0.98(9-II-1)	0.35(8-II-1)	53(8-I-1)	-261(2)	-97(9-I-2)
4	105	-0.46(8-I-1)	-1.17(9-II-1)	-0.36(8-I-2)	72(8-I-1)	-108(9-I-1)	-128(9-I-2)
4	106	-0.50(8-I-1)	-1.32(9-II-1)	-0.48(8-I-1)	95(9-II-2)	136(9-II-1)	-140(8-II-3)
4	107	-0.49(8-I-2)	-1.03(8-II-1)	-0.54(8-I-1)	81(9-II-1)	-159(8-I-1)	-81(8-II-4)
4	108	-0.48(8-I-1)	-0.78(8-II-1)	-0.40(8-I-2)	130(9-I-2)	319(2)	-110(9-II-2)
4	109	-0.50(8-I-1)	-0.90(9-II-1)	-0.38(8-I-2)	121(9-I-2)	357(9-II-2)	-82(8-II-2)
4	110	-0.53(8-II-2)	-0.99(9-II-1)	-0.71(9-I-2)	113(9-I-2)	273(9-II-2)	139(9-I-2)
4	111	-0.53(8-I-1)	-1.49(9-II-1)	-0.56(8-I-2)	83(2)	451(9-II-2)	-84(8-II-1)
4	112	-0.76(9-I-2)	-1.20(9-I-2)	-0.87(9-I-2)	133(9-I-2)	284(9-I-2)	177(9-I-2)
4	113	-0.47(8-I-2)	-0.71(8-II-1)	-0.57(9-I-2)	67(8-II-2)	284(9-I-2)	116(9-I-2)
4	114	-0.65(9-I-2)	-0.79(8-II-1)	-0.56(9-I-2)	108(9-I-2)	293(9-I-2)	148(9-I-2)
4	115	-0.50(8-II-2)	-0.73(8-II-1)	-0.46(9-I-2)	106(9-I-2)	247(2)	140(9-I-2)
4	116	-0.47(8-I-1)	-0.68(8-II-1)	-0.29(8-I-2)	96(8-I-2)	344(2)	-70(8-II-2)
4	117	-0.47(8-I-1)	-0.67(8-II-1)	-0.31(8-I-2)	99(8-I-1)	376(2)	-88(9-II-2)
4	118	-0.48(8-I-1)	-0.57(1)	-0.24(8-I-2)	87(8-I-4)	374(2)	-54(9-II-2)
4	119	-0.46(8-I-1)	-0.57(1)	-0.24(8-I-2)	89(8-I-1)	421(2)	-54(9-II-2)
4	120	-0.47(8-I-1)	-0.59(9-II-1)	-0.27(8-I-2)	90(8-I-1)	388(2)	-62(9-II-2)
4	121	-0.47(8-I-1)	-0.53(1)	0.22(8-II-2)	95(9-II-4)	406(2)	-45(9-II-2)
4	122	-0.46(8-I-1)	-0.55(8-II-1)	-0.22(8-I-1)	76(8-I-1)	334(2)	-50(8-II-2)
4	123	-0.62(9-II-2)	-0.58(1)	0.27(8-II-2)	83(9-II-1)	159(9-I-2)	31(9-I-1)
4	124	-0.50(8-I-3)	-0.56(1)	0.24(8-II-2)	93(9-II-4)	287(2)	36(9-I-2)
4	125	-0.49(8-I-1)	-0.58(1)	-0.26(8-I-2)	83(9-II-4)	277(2)	54(9-I-2)
4	126	-0.58(9-II-2)	-0.59(1)	-0.29(8-I-2)	76(9-II-4)	176(9-I-2)	45(9-I-2)
4	127	-0.47(8-I-1)	-0.65(8-II-1)	-0.35(8-I-2)	84(8-I-1)	277(2)	105(9-I-2)
4	128	-0.48(8-I-1)	-0.60(1)	-0.30(8-I-2)	80(8-I-1)	280(2)	74(9-I-2)
4	129	-0.52(8-I-4)	-0.62(1)	-0.36(8-I-2)	66(8-I-4)	203(9-I-2)	64(9-I-2)
4	130	-0.48(8-I-1)	-0.65(1)	-0.48(9-I-2)	63(8-I-1)	240(9-I-2)	90(9-I-2)
5	1	1.24(2)	-2.16(2)	0.92(2)	0	-16(9-I-2)	-3(9-I-2)
5	2	-5.78(2)	0.27(9-II-2)	2.20(2)	0	8(9-II-2)	-3(9-I-2)
5	3	-2.42(8-I-3)	-3.90(2)	3.55(2)	0	8(9-II-2)	-3(9-I-2)
5	4	1.16(2)	1.31(2)	4.51(2)	-6(9-II-2)	8(9-II-2)	-3(9-I-2)
5	5	6.23(2)	-3.00(2)	3.85(2)	0	6(2)	-2(9-I-2)
5	6	0.22(8-II-3)	-3.30(2)	4.91(2)	8(9-I-2)	8(9-II-2)	-2(9-I-2)
5	7	7.14(2)	-2.84(2)	-1.83(8-II-3)	0	4(9-II-2)	2(9-II-2)
5	8	-3.90(2)	-15.46(2)	2.71(8-I-3)	9(9-I-2)	8(2)	-2(9-I-2)
5	9	0.18(9-II-3)	-0.51(2)	-2.44(8-II-3)	7(9-I-2)	2(9-II-2)	1(9-II-2)
5	10	3.52(2)	-2.59(2)	1.23(2)	-3(8-II-3)	10(9-II-2)	-3(9-I-2)
5	11	-0.99(2)	-3.93(2)	-0.60(9-I-2)	0	11(9-II-2)	-3(9-I-2)
5	12	-3.40(2)	-7.74(2)	1.83(2)	-4(8-II-3)	20(9-II-2)	-3(9-I-2)
5	13	0.87(8-II-3)	-8.42(2)	-0.66(9-I-2)	-10(9-I-2)	14(9-II-2)	-3(9-I-2)
5	14	0.11(2)	-7.26(2)	0.72(9-II-2)	-20(9-I-2)	14(9-II-2)	-3(9-I-2)
5	15	1.38(8-II-3)	-2.17(9-II-2)	0.82(9-II-2)	-27(9-I-2)	8(9-II-3)	-3(9-I-2)
5	16	1.88(8-II-3)	-4.41(2)	4.05(2)	-5(9-II-2)	14(9-II-2)	-2(9-I-2)
5	17	5.76(2)	-1.04(2)	3.42(2)	-13(9-II-2)	16(9-II-2)	-2(9-I-2)
5	18	4.05(2)	0.21(2)	4.35(2)	9(9-I-2)	6(9-II-2)	-2(9-I-2)
5	19	2.25(2)	0.22(2)	4.60(2)	15(9-I-2)	9(9-II-2)	-2(9-I-2)
5	20	8.51(2)	-0.62(2)	2.50(8-I-3)	10(2)	5(2)	-2(9-I-2)
5	21	-1.09(8-I-3)	-8.02(2)	2.95(2)	14(9-I-2)	6(2)	-2(9-I-2)
5	22	4.08(2)	0.45(2)	-2.32(8-II-3)	7(9-I-2)	3(2)	-1(9-I-1)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
5	23	0.70(8-II-3)	-5.29(2)	2.05(8-I-3)	14(2)	5(2)	-1(9-I-1)
5	24	2.04(2)	-0.02(8-II-3)	-2.00(8-II-3)	0	2(9-II-2)	1(9-II-1)
5	25	1.75(2)	0.30(8-II-3)	-2.10(8-II-3)	0	2(9-II-2)	1(9-II-1)
5	26	0.79(2)	-0.32(2)	-2.64(8-II-3)	5(9-I-2)	2(9-II-2)	1(9-II-1)
5	27	5.34(2)	-1.29(2)	-2.13(8-II-3)	0	3(2)	0
5	28	0.39(2)	-0.92(2)	-2.73(8-II-3)	4(9-I-2)	2(8-I-3)	1(9-II-1)
5	29	-3.12(2)	-14.56(2)	-3.78(2)	7(2)	7(2)	1(9-II-1)
5	30	2.48(8-I-3)	-4.60(2)	-4.67(2)	0	7(2)	1(2)
5	31	-6.83(2)	-4.14(2)	-2.80(2)	0	5(2)	2(2)
5	32	3.70(2)	-1.71(2)	-4.97(2)	6(9-I-2)	6(2)	1(2)
5	33	-0.47(2)	-7.40(2)	1.09(2)	0	2(2)	1(2)
5	34	3.21(2)	0.24(2)	-2.50(8-II-3)	5(9-I-2)	1(2)	1(9-II-1)
5	35	2.39(2)	-0.14(2)	-2.33(8-II-3)	12(2)	2(2)	-1(9-I-1)
5	36	3.33(2)	0.38(2)	-2.60(8-II-3)	4(9-I-2)	2(2)	1(9-II-1)
5	37	2.29(2)	-0.12(2)	-2.45(8-II-3)	11(2)	2(2)	1(9-II-1)
5	38	6.71(2)	-0.28(2)	-3.33(2)	8(2)	5(2)	1(9-II-1)
5	39	0.48(8-I-3)	-4.30(2)	-2.67(8-II-3)	10(2)	5(2)	1(9-II-1)
5	40	-2.33(8-II-3)	-7.38(2)	-4.82(2)	6(9-I-2)	9(2)	1(2)
5	41	-0.77(2)	-7.54(2)	-4.56(2)	11(9-I-2)	7(2)	1(2)
5	42	-5.84(2)	-2.98(2)	-0.70(2)	0	4(2)	1(2)
5	43	4.47(2)	-0.35(2)	-2.10(2)	-5(9-II-2)	4(2)	1(2)
5	44	-0.74(2)	-3.81(2)	0.80(2)	-3(9-II-2)	3(2)	1(2)
5	45	1.76(2)	-0.54(2)	-0.49(8-II-3)	-6(9-II-2)	3(2)	1(2)
5	46	-0.53(2)	-11.70(2)	0.68(8-I-3)	-3(9-II-2)	2(2)	0
5	47	0.44(9-II-2)	-8.93(2)	0.71(8-I-3)	-6(9-II-2)	3(9-I-2)	0
5	48	-3.57(2)	-8.48(2)	-2.09(2)	-5(9-II-2)	8(2)	1(2)
5	49	6.03(2)	-1.65(2)	-3.55(2)	9(9-I-2)	8(2)	1(2)
5	50	3.36(2)	-4.30(2)	0.85(8-I-3)	-5(2)	27(9-II-2)	-3(9-I-2)
5	51	0.21(2)	-5.15(2)	-0.83(8-II-3)	-16(9-I-2)	26(9-II-2)	-3(9-I-2)
5	52	-4.26(8-I-3)	-12.46(2)	3.05(2)	-13(9-II-2)	28(9-II-2)	-2(9-I-2)
5	53	2.50(8-II-3)	-6.54(2)	1.30(8-I-3)	-15(9-II-2)	26(9-II-2)	-2(9-I-2)
5	54	4.42(8-II-3)	-6.70(2)	-1.34(8-II-3)	-10(2)	35(9-II-2)	-3(9-I-2)
5	55	0.17(8-II-3)	-6.14(2)	1.16(8-I-3)	-39(9-I-2)	35(9-II-2)	-5(9-I-2)
5	56	-0.28(9-I-3)	-3.08(9-II-2)	1.46(8-I-3)	-50(9-I-2)	22(9-II-2)	6(9-II-2)
5	57	4.26(8-II-3)	1.65(2)	4.02(2)	15(9-I-2)	0	-1(9-I-1)
5	58	-12.56(8-I-3)	-3.53(8-I-3)	3.84(2)	-27(9-II-2)	13(9-II-2)	-2(2)
5	59	8.81(2)	1.48(2)	2.40(8-I-3)	15(9-I-2)	0	-1(9-I-1)
5	60	10.88(8-II-3)	-2.43(2)	2.77(2)	19(9-I-2)	1(2)	-1(9-I-2)
5	61	8.69(2)	1.12(2)	1.59(8-I-3)	14(2)	0	-1(9-I-1)
5	62	11.13(2)	-3.50(2)	1.60(8-I-3)	18(2)	0	-1(9-I-1)
5	63	6.23(2)	0.28(2)	-1.82(8-II-3)	12(2)	0	0
5	64	11.57(2)	-1.05(2)	-1.38(8-II-3)	20(2)	1(2)	-1(9-I-1)
5	65	-1.46(8-I-3)	-5.24(8-I-3)	2.49(8-I-3)	-49(9-I-2)	73(9-II-2)	-6(9-I-2)
5	66	-10.25(8-I-3)	-9.25(2)	1.97(8-I-3)	-24(9-II-2)	35(9-II-2)	-2(9-I-2)
5	67	-0.21(9-II-3)	-4.25(2)	-2.01(8-II-3)	-9(2)	34(9-II-2)	-3(9-I-2)
5	68	-3.71(8-I-3)	-19.09(2)	3.03(8-I-3)	-12(9-II-2)	34(9-II-2)	2(9-II-2)
5	69	-4.24(8-I-3)	-6.84(2)	2.66(8-I-3)	-9(2)	-40(9-I-2)	-2(9-I-2)
5	70	-0.54(9-II-3)	-4.96(2)	2.88(8-I-3)	-8(9-I-2)	-38(9-I-2)	-2(9-I-2)
5	71	0.96(8-I-3)	-10.97(2)	2.73(8-I-3)	-3(9-I-2)	21(9-II-2)	1(9-II-2)
5	72	0.60(8-II-3)	-6.57(2)	2.97(8-I-3)	-10(9-II-2)	24(9-II-2)	0
5	73	-1.20(8-I-3)	-18.59(2)	2.30(8-I-3)	0	13(9-II-2)	0
5	74	5.51(2)	0.20(2)	-1.90(8-II-3)	11(2)	0	1(9-II-1)
5	75	10.09(2)	0.09(2)	-1.49(8-II-3)	19(2)	1(2)	0
5	76	6.33(2)	0.90(2)	-2.20(8-II-3)	10(2)	0	1(2)
5	77	8.08(2)	-0.83(2)	-1.63(8-II-3)	17(2)	1(2)	1(9-II-1)
5	78	5.60(2)	1.54(2)	-3.79(2)	10(9-I-2)	0	1(2)
5	79	9.26(8-I-3)	-3.22(2)	-2.14(8-II-3)	16(9-I-2)	1(2)	1(2)
5	80	-4.30(8-II-3)	-14.41(2)	-3.36(2)	8(9-I-2)	10(2)	0
5	81	-12.92(8-II-3)	-5.55(2)	-4.37(2)	16(9-I-2)	5(2)	2(2)
5	82	-1.77(2)	-5.01(2)	-0.71(8-II-3)	-5(9-II-2)	5(9-I-2)	0
5	83	3.40(8-I-3)	-1.12(2)	-1.00(8-II-3)	-10(9-II-2)	5(2)	0
5	84	0.71(2)	-6.15(2)	0.93(8-I-3)	-6(9-II-2)	6(9-I-2)	0
5	85	2.05(8-I-3)	-4.51(2)	1.07(8-I-3)	-9(9-II-2)	6(9-I-2)	0
5	86	-3.68(2)	-7.08(2)	-1.53(8-II-3)	-8(9-II-2)	8(9-I-2)	0

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
5	87	-8.03(8-II-3)	-4.61(2)	-1.95(8-II-3)	-14(9-II-2)	7(9-I-2)	0
5	88	-8.10(2)	-20.49(2)	-3.46(8-II-3)	-7(9-II-2)	11(9-I-2)	-1(9-II-2)
5	89	-2.86(2)	-5.25(2)	1.98(8-I-3)	-8(9-II-2)	9(9-I-2)	0
5	90	-6.27(8-II-3)	-3.66(2)	-2.27(8-II-3)	-9(9-II-2)	9(9-I-2)	0
5	91	-2.74(2)	-6.14(2)	2.53(8-I-3)	-5(9-II-2)	-9(9-II-2)	0
5	92	-3.39(2)	-6.68(2)	-3.19(8-II-3)	-5(9-II-2)	11(9-I-2)	0
5	93	0.90(2)	-7.20(2)	-3.04(8-II-3)	-1(2)	11(9-I-2)	-1(9-II-2)
5	94	-1.80(2)	-16.93(2)	-2.53(8-II-3)	0	14(9-I-2)	0
5	95	-0.23(8-II-3)	-5.34(2)	-3.23(8-II-3)	-2(2)	-14(9-II-2)	0
5	96	-2.45(2)	-6.29(2)	3.20(8-I-3)	-5(9-II-2)	-14(9-II-2)	0
5	97	-0.35(2)	-5.30(2)	3.26(8-I-3)	-1(9-II-2)	-13(9-II-2)	0
5	98	-0.83(2)	-4.98(2)	-0.67(2)	0	1(2)	0
5	99	0.22(9-II-4)	-9.74(2)	-0.54(8-II-3)	-3(9-II-2)	2(2)	0
5	100	-5.43(2)	-3.30(2)	1.46(2)	0	0	0
5	101	2.71(2)	0.12(8-II-3)	0.79(2)	-3(9-II-2)	1(2)	0
5	102	-3.14(2)	-4.31(2)	3.55(2)	0	0	0
5	103	4.07(2)	1.30(2)	3.15(2)	-3(2)	0	0
5	104	-0.33(2)	2.82(2)	4.94(2)	-5(2)	-2(2)	0
5	105	5.63(2)	-5.03(2)	4.95(2)	0	-1(2)	1(9-I-2)
5	106	-1.98(2)	-6.25(2)	4.46(2)	-8(2)	-4(2)	-1(9-II-2)
5	107	6.99(2)	-2.40(2)	1.78(8-I-3)	0	-1(2)	-1(9-II-2)
5	108	-1.38(2)	-10.81(2)	2.62(8-I-3)	-6(2)	-4(2)	-1(9-II-2)
5	109	1.90(2)	-0.72(8-II-3)	1.72(8-I-3)	0	0	-1(9-II-2)
5	110	-0.37(8-II-3)	-1.12(8-I-3)	2.23(8-I-3)	-3(9-II-4)	0	-1(9-II-2)
5	111	0.46(8-I-3)	-0.67(8-I-3)	-2.24(8-II-3)	-3(9-II-4)	1(9-II-1)	-1(9-II-2)
5	112	-2.56(2)	-6.91(2)	0.87(2)	-3(9-II-2)	-2(9-II-2)	0
5	113	1.19(2)	-2.51(2)	0.50(8-I-3)	-6(9-II-2)	2(9-I-2)	0
5	114	2.47(2)	-1.62(2)	4.43(2)	-6(2)	-2(2)	0
5	115	-4.06(2)	-7.29(2)	3.10(2)	-3(2)	-1(2)	0
5	116	4.66(2)	-1.00(2)	1.87(2)	-6(9-II-2)	-2(9-II-2)	0
5	117	-1.06(9-I-3)	-6.27(2)	4.52(2)	-8(2)	-2(2)	0
5	118	5.44(2)	0.44(2)	4.56(2)	-9(2)	-3(2)	0
5	119	1.30(2)	-0.83(2)	4.90(2)	-12(2)	-3(2)	0
5	120	5.96(2)	0.25(8-II-3)	2.32(8-I-3)	-7(2)	-2(2)	-1(9-II-2)
5	121	-2.45(2)	-9.42(2)	2.91(2)	-12(2)	-3(2)	0
5	122	3.55(2)	0.25(2)	2.06(8-I-3)	-3(9-II-4)	0	-1(9-II-2)
5	123	1.34(2)	-1.89(2)	2.14(8-I-3)	-7(2)	-2(2)	-1(9-II-2)
5	124	2.91(2)	0.22(2)	-2.13(8-II-3)	-3(9-II-4)	0	-1(9-II-2)
5	125	2.45(2)	-0.17(8-II-3)	-1.99(8-II-3)	-5(9-II-4)	0	-1(9-II-2)
5	126	1.91(2)	-0.47(8-II-3)	-1.81(8-II-3)	0	2(9-II-1)	-2(9-II-2)
5	127	6.32(2)	-2.80(2)	-1.89(8-II-3)	0	4(2)	-2(9-II-2)
5	128	-0.45(8-II-3)	-0.49(8-I-3)	-2.39(8-II-3)	5(9-I-4)	2(9-II-1)	-2(9-II-2)
5	129	3.08(2)	-4.50(2)	-4.39(2)	0	5(2)	2(9-I-2)
5	130	-4.03(2)	-14.68(2)	-3.43(2)	9(2)	7(2)	-2(9-II-2)
5	131	-5.56(2)	-4.18(2)	-2.83(2)	0	6(9-II-1)	2(9-I-1)
5	132	2.62(2)	-0.74(2)	-4.84(2)	7(9-I-1)	5(9-II-4)	2(9-I-2)
5	133	-5.46(2)	-3.11(2)	-0.61(2)	0	6(9-II-4)	2(9-I-1)
5	134	4.21(2)	0.08(2)	-2.22(2)	-4(9-II-1)	5(9-II-1)	2(9-I-1)
5	135	0.50(2)	-5.10(2)	1.25(2)	0	5(9-II-4)	2(9-I-1)
5	136	2.50(2)	0.28(9-I-3)	0.52(9-I-3)	-2(2)	5(9-II-4)	2(9-I-1)
5	137	0.57(2)	-4.70(2)	-1.02(2)	0	-7(9-I-3)	2(9-I-1)
5	138	-0.31(9-I-4)	1.14(9-I-4)	-0.84(2)	14(9-II-1)	-5(9-I-4)	1(9-I-1)
5	139	3.43(2)	0.53(2)	-2.27(8-II-3)	5(9-I-4)	3(2)	-1(9-II-2)
5	140	1.98(2)	-0.20(2)	-2.10(8-II-3)	7(9-I-4)	2(2)	-1(9-II-2)
5	141	6.93(2)	-0.31(2)	-3.11(2)	10(2)	5(2)	-1(9-II-2)
5	142	-1.74(8-II-3)	-6.35(2)	-2.46(8-II-3)	10(9-I-4)	5(2)	-1(9-II-2)
5	143	-2.59(8-II-3)	-6.76(2)	-4.53(2)	7(9-I-1)	6(9-II-1)	2(9-I-2)
5	144	-1.77(8-II-3)	-6.64(2)	-4.30(2)	12(9-I-1)	5(2)	-1(9-II-2)
5	145	-3.39(2)	-8.34(2)	-2.05(2)	-4(9-II-1)	10(9-II-1)	2(9-I-2)
5	146	6.69(2)	-1.39(2)	-3.28(2)	11(9-I-1)	7(9-II-1)	1(9-I-2)
5	147	-2.73(2)	-5.31(2)	0.60(9-I-3)	-2(2)	13(9-II-1)	2(9-I-1)
5	148	4.44(2)	-0.56(2)	-0.80(9-II-3)	-6(9-II-1)	11(9-II-1)	2(9-I-2)
5	149	-0.08(9-II-1)	-4.27(2)	-0.82(9-II-4)	22(9-II-1)	12(9-II-1)	2(9-I-1)
5	150	0.27(2)	-7.70(2)	-0.78(9-II-3)	-11(9-I-1)	9(9-II-4)	3(9-I-1)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
5	151	-0.54(8-II-3)	-11.72(2)	0.86(9-I-3)	-6(9-I-1)	8(9-II-4)	2(9-I-1)
5	152	0.85(2)	-4.63(2)	0.95(9-I-3)	-6(9-I-1)	13(9-II-1)	2(9-I-1)
5	153	1.21(8-I-3)	-1.81(2)	-0.89(9-II-3)	-26(9-I-1)	13(9-II-1)	2(9-I-1)
5	154	-0.85(9-I-3)	-6.37(2)	-0.72(8-II-3)	-7(9-II-2)	-6(9-II-2)	0
5	155	-1.28(2)	-8.49(2)	1.13(8-I-3)	-8(9-II-2)	-5(9-II-2)	0
5	156	-1.96(2)	-6.62(2)	2.07(8-I-3)	-8(9-II-2)	-10(9-II-2)	0
5	157	5.38(2)	-2.72(2)	3.01(2)	-10(2)	-4(9-II-2)	0
5	158	-2.77(2)	-10.27(2)	1.71(2)	-6(2)	-4(9-II-2)	0
5	159	3.66(8-II-3)	-2.60(2)	0.99(8-I-3)	-9(9-II-2)	-6(9-II-2)	0
5	160	-3.62(2)	-13.91(2)	2.98(2)	-9(2)	-4(9-II-2)	0
5	161	3.33(9-II-3)	1.22(2)	4.12(2)	-11(2)	0	0
5	162	-14.25(8-I-3)	-3.62(8-I-3)	4.30(2)	-16(2)	-3(9-II-2)	0
5	163	8.32(2)	1.35(2)	2.35(2)	-12(2)	0	0
5	164	8.36(8-II-3)	-2.68(2)	2.89(2)	-15(2)	0	0
5	165	6.41(2)	0.99(2)	1.57(8-I-3)	-7(2)	0	0
5	166	9.54(2)	-3.12(2)	1.50(8-I-3)	-11(2)	0	0
5	167	5.56(2)	0.17(8-II-3)	-1.52(8-II-3)	-5(9-II-4)	0	-1(9-II-2)
5	168	10.22(2)	-0.31(2)	-1.19(8-II-3)	-7(9-II-4)	0	0
5	169	5.72(2)	0.45(2)	-1.60(8-II-3)	7(9-I-4)	0	-1(9-II-2)
5	170	9.94(2)	0.16(8-I-3)	-1.24(8-II-3)	7(9-I-4)	0	-1(9-II-2)
5	171	-9.85(8-I-3)	-5.81(2)	2.29(8-I-3)	-8(9-II-1)	-8(9-II-2)	0
5	172	-4.32(2)	-7.50(2)	1.85(8-I-3)	-8(9-II-2)	-10(9-II-2)	0
5	173	-3.30(8-I-3)	-5.60(2)	2.43(8-I-3)	-4(9-II-2)	-10(9-II-2)	0
5	174	-3.77(2)	-18.62(2)	3.18(8-I-3)	-4(2)	-13(9-II-2)	0
5	175	-2.79(2)	-7.15(2)	3.13(8-I-3)	-4(9-II-2)	-14(9-II-2)	0
5	176	-0.50(8-I-3)	-6.05(2)	3.32(8-I-3)	-1(2)	-14(9-II-2)	0
5	177	1.17(8-I-3)	-9.06(2)	2.94(8-I-3)	1(2)	-15(9-II-2)	0
5	178	1.13(8-II-3)	-6.89(2)	3.13(8-I-3)	0	-14(9-II-2)	0
5	179	-1.27(8-I-3)	-17.67(2)	2.38(8-I-3)	0	-17(9-II-2)	0
5	180	7.64(2)	1.29(2)	-2.04(8-II-3)	10(9-I-4)	0	-1(9-II-2)
5	181	9.18(2)	-1.54(2)	-1.44(8-II-3)	10(9-I-4)	0	-1(9-II-2)
5	182	6.11(2)	1.97(2)	-3.70(2)	12(9-I-1)	0	1(9-I-2)
5	183	11.12(8-I-3)	-3.79(2)	-2.12(2)	14(9-I-4)	0	1(9-I-2)
5	184	-5.39(8-II-3)	-14.63(2)	-2.98(2)	11(9-I-1)	8(9-II-1)	1(9-I-2)
5	185	-12.86(8-II-3)	-5.09(2)	-4.24(2)	19(9-I-1)	4(9-II-1)	0
5	186	2.28(8-I-3)	-5.70(2)	1.21(9-I-3)	-6(9-I-1)	20(9-II-1)	2(9-I-1)
5	187	2.99(8-I-3)	-2.92(2)	1.30(9-I-3)	-8(9-II-4)	15(9-II-1)	1(9-I-2)
5	188	-2.95(8-II-3)	-7.11(2)	-0.92(9-II-3)	-6(9-II-4)	14(9-II-1)	2(9-I-2)
5	189	6.08(8-I-3)	-3.71(2)	-1.39(8-II-3)	11(9-I-4)	10(9-II-1)	1(9-I-2)
5	190	0.17(8-I-3)	-4.41(2)	-1.07(9-II-3)	-34(9-I-1)	27(9-II-1)	3(9-I-1)
5	191	-2.31(8-II-3)	-7.97(2)	1.33(9-I-3)	-13(9-I-1)	24(9-II-1)	2(9-I-2)
5	192	-1.34(8-II-3)	-2.68(9-II-4)	-1.29(9-II-3)	-44(9-I-1)	27(9-II-1)	-3(9-II-4)
5	193	-5.87(8-II-3)	-5.50(2)	2.11(8-I-3)	-6(9-II-4)	-16(9-I-1)	1(9-I-2)
5	194	-1.75(8-II-3)	-3.26(2)	-2.66(8-II-3)	-10(9-II-4)	-11(9-I-1)	0
5	195	-8.63(8-II-3)	-9.77(2)	-2.62(8-II-3)	10(9-I-1)	-9(9-I-1)	0
5	196	-1.13(8-II-3)	-20.85(2)	-2.90(8-II-3)	-1(9-I-1)	-6(9-I-1)	0
5	197	-1.26(2)	-18.48(2)	-2.34(8-II-3)	4(9-I-4)	-3(2)	0
5	198	1.81(8-I-3)	-5.10(2)	2.07(8-I-3)	-12(9-I-1)	-25(9-I-4)	1(9-I-2)
5	199	-1.88(8-II-3)	-5.45(2)	2.42(8-I-3)	-4(9-II-3)	-20(9-I-1)	0
5	200	0.85(9-II-1)	-3.63(2)	-2.06(9-II-3)	-46(9-I-1)	-38(9-I-4)	3(9-I-4)
5	201	-1.05(2)	-6.07(2)	-2.23(9-II-3)	-9(9-I-1)	-32(9-I-4)	0
5	202	-0.81(9-II-4)	-3.52(9-II-4)	-2.28(9-II-3)	-35(9-I-1)	-42(9-I-4)	-3(9-II-4)
5	203	-0.93(8-II-3)	-5.03(2)	-2.69(8-II-3)	-5(9-II-4)	-10(9-I-1)	1(9-II-4)
5	204	-1.90(2)	-5.71(2)	-2.81(8-II-3)	-2(8-II-3)	-11(9-I-1)	0
5	205	0.55(9-II-4)	-4.08(2)	-2.64(9-II-3)	-15(9-I-1)	-20(9-I-4)	0
5	206	0.99(8-I-3)	-4.45(2)	-2.58(8-II-3)	-12(9-I-1)	-23(9-I-4)	1(9-II-3)
5	207	-0.51(9-II-1)	-5.33(2)	-2.76(8-II-3)	-4(9-I-2)	-17(9-I-4)	2(9-II-4)
5	208	-0.77(9-II-1)	-2.04(8-II-3)	-2.70(9-II-3)	-14(9-I-1)	-17(9-I-4)	-1(9-II-3)
5	209	-1.23(9-I-3)	-4.28(2)	3.32(8-I-3)	-17(9-I-2)	-43(9-I-2)	1(9-II-2)
5	210	0.37(9-I-3)	-3.31(8-I-3)	3.52(8-I-3)	-10(8-II-3)	-28(9-I-2)	4(9-II-2)
5	211	-0.67(8-II-3)	-7.16(2)	3.20(8-I-3)	-4(9-I-2)	-16(9-I-2)	0
5	212	0.53(9-I-3)	-6.08(2)	3.41(8-I-3)	-3(8-II-3)	-18(9-I-2)	2(9-I-2)
5	213	-0.59(9-I-3)	-2.67(9-I-3)	3.59(8-I-3)	-14(9-I-2)	-13(9-I-2)	4(9-II-2)
5	214	1.08(8-I-3)	-16.33(2)	2.22(8-I-3)	1(9-I-2)	-2(9-II-3)	0

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
5	215	-1.70(8-I-3)	-10.54(2)	2.43(8-I-3)	0	-5(8-II-3)	1(9-I-2)
5	216	-0.68(8-I-3)	-8.38(2)	2.99(8-I-3)	-2(9-II-2)	-4(8-II-3)	1(9-I-2)
5	217	-0.63(9-I-2)	-5.12(2)	3.46(8-I-3)	-6(9-I-2)	-9(8-II-3)	2(9-I-2)
5	218	0.42(9-I-3)	-4.09(2)	3.59(8-I-3)	-2(9-II-2)	-6(2)	3(8-I-3)
5	219	-1.70(8-II-3)	-9.69(2)	2.64(8-I-3)	0	-12(9-II-2)	1(9-I-2)
5	220	-0.76(8-II-3)	-8.04(2)	3.17(8-I-3)	0	-11(9-II-2)	1(9-I-2)
5	221	-0.53(9-I-2)	-6.56(2)	3.36(8-I-3)	-2(8-I-3)	-6(9-II-4)	3(9-I-2)
5	222	-1.18(8-I-3)	-12.93(2)	2.25(8-I-3)	-2(8-I-3)	-22(9-II-2)	2(9-I-2)
5	223	-0.43(9-I-3)	-3.61(9-I-3)	3.58(8-I-3)	-5(9-I-2)	-7(9-II-3)	3(8-I-3)
5	224	1.78(8-I-3)	-9.93(2)	2.54(8-I-3)	0	-30(9-II-2)	3(9-I-2)
5	225	-1.21(2)	-7.61(2)	-3.22(8-II-3)	0	-17(9-II-2)	0
5	226	0.30(8-II-3)	-8.19(2)	-2.87(8-II-3)	0	-16(9-II-2)	0
5	227	-1.71(8-II-3)	-14.82(2)	-2.36(8-II-3)	0	-19(9-II-2)	0
5	228	-1.25(2)	-6.28(2)	3.28(8-I-3)	-2(2)	-19(9-II-2)	0
5	229	0.54(8-I-3)	-5.42(2)	-3.28(8-II-3)	0	-19(9-II-2)	0
5	230	-1.15(2)	-6.68(2)	3.31(8-I-3)	-2(2)	-19(9-II-2)	0
5	231	-0.41(2)	-6.11(2)	3.34(8-I-3)	-1(9-I-2)	-19(9-II-2)	0
5	232	1.34(8-II-3)	-10.22(2)	-2.64(8-II-3)	0	-24(9-II-2)	0
5	233	-1.32(8-II-3)	-15.50(2)	-2.29(8-II-3)	0	-25(9-II-2)	0
5	234	-0.85(2)	-6.68(2)	-3.25(8-II-3)	0	-24(9-II-2)	0
5	235	-0.94(8-II-3)	-7.22(2)	-3.10(8-II-3)	2(9-II-2)	-24(9-II-2)	0
5	236	-0.59(2)	-6.33(2)	3.32(8-I-3)	-1(9-I-2)	-24(9-II-2)	0
5	237	-0.25(8-II-3)	-5.73(2)	-3.31(8-II-3)	3(9-II-2)	-24(9-II-2)	0
5	238	-0.49(9-I-2)	-5.76(2)	3.39(8-I-3)	-2(9-I-2)	-19(9-II-2)	3(9-I-2)
5	239	0.24(9-I-2)	-4.53(2)	3.51(8-I-3)	-2(8-I-3)	-24(9-II-2)	2(8-I-3)
5	240	-0.52(8-II-3)	-4.72(9-I-3)	3.42(8-I-3)	-6(9-I-2)	-21(9-II-2)	1(9-I-3)
5	241	-0.33(8-I-3)	-15.15(8-II-3)	2.17(8-I-3)	0	-43(9-II-2)	3(9-I-2)
5	242	-1.28(8-I-3)	-9.85(2)	2.69(8-I-3)	1(9-II-4)	-44(9-II-2)	3(9-I-2)
5	243	-0.20(2)	-7.98(2)	2.87(8-I-3)	2(9-II-4)	-33(9-II-2)	2(9-I-2)
5	244	-0.20(9-II-2)	-7.30(2)	3.26(8-I-3)	-7(8-I-3)	-33(9-II-2)	4(9-I-2)
5	245	1.55(8-I-3)	-5.75(2)	3.02(8-I-3)	2(9-II-4)	-47(9-II-2)	4(9-I-2)
5	246	-0.18(9-I-2)	-4.95(2)	3.09(8-I-3)	-2(9-I-3)	-50(9-II-2)	2(9-I-2)
5	247	2.19(8-I-3)	-6.02(9-I-2)	2.78(8-I-3)	3(9-II-2)	-45(9-II-2)	2(9-I-2)
5	248	-7.45(8-II-3)	-17.95(8-II-3)	2.71(8-I-3)	13(8-II-3)	-71(9-II-2)	-6(9-II-2)
5	249	2.76(8-I-3)	-9.61(8-II-3)	2.69(8-I-3)	3(8-II-3)	-57(9-II-2)	4(9-I-2)
5	250	-2.58(8-II-3)	-7.85(2)	2.73(8-I-3)	8(8-II-3)	-55(9-II-2)	5(9-I-2)
5	251	0.84(9-II-2)	-5.36(2)	1.77(8-I-3)	-5(9-I-2)	-99(9-II-2)	3(9-I-2)
5	252	-0.13(2)	-9.79(9-I-2)	1.08(8-I-3)	0	-105(9-II-2)	-2(9-II-2)
5	253	3.40(8-I-3)	-7.23(2)	1.62(8-I-3)	10(8-II-3)	-84(9-II-2)	-4(9-II-2)
5	254	-0.35(8-II-3)	-5.16(2)	1.04(8-I-3)	0	-98(9-II-2)	-2(9-II-2)
5	255	2.80(8-I-3)	-9.27(8-II-3)	1.42(8-I-3)	7(8-II-3)	-62(9-II-2)	-5(9-II-2)
5	256	-0.54(8-II-3)	-8.71(2)	0.92(8-I-3)	0	-72(9-II-2)	-2(9-II-2)
5	257	8.40(8-I-3)	-7.15(8-II-3)	-2.13(8-II-3)	22(9-I-2)	-31(9-II-2)	-7(9-II-2)
5	258	-0.64(8-II-3)	-9.89(8-II-3)	-0.98(8-II-3)	0	-48(9-II-2)	-2(9-II-2)
5	259	5.95(8-I-3)	0.44(8-I-3)	1.14(8-I-3)	-21(9-II-2)	-2(9-II-2)	-1(9-II-2)
5	260	0.64(9-I-3)	1.09(8-II-3)	0.91(8-I-3)	0	-3(9-II-2)	-1(9-II-2)
5	261	3.77(8-I-3)	-0.46(8-II-3)	1.01(8-I-3)	-13(9-II-2)	0	0
5	262	0.59(9-I-3)	-0.36(8-I-3)	0.83(8-I-3)	0	0	0
5	263	1.82(2)	-0.39(8-II-3)	0.95(8-I-3)	-7(9-II-2)	0	0
5	264	0.63(2)	-0.40(8-I-3)	0.78(8-I-3)	0	0	0
5	265	1.32(8-II-3)	-15.47(8-I-3)	-2.21(8-II-3)	0	-31(9-II-2)	0
5	266	-1.51(8-I-3)	-7.62(2)	-3.02(8-II-3)	2(9-II-2)	-30(9-II-2)	0
5	267	-0.95(8-II-3)	-9.97(2)	2.66(8-I-3)	3(9-II-2)	-31(9-II-2)	0
5	268	-0.78(2)	-6.25(2)	3.19(8-I-3)	3(9-II-2)	-28(9-II-2)	0
5	269	-0.80(8-I-3)	-6.43(2)	-3.01(8-II-3)	5(9-II-2)	-29(9-II-2)	0
5	270	1.40(2)	0.36(8-I-3)	0.96(8-I-3)	-5(9-II-2)	0	0
5	271	0.67(2)	-0.48(8-I-3)	0.78(8-I-3)	0	0	0
5	272	0.64(2)	-0.69(8-I-3)	0.81(8-I-3)	0	0	0
5	273	2.98(8-II-3)	-0.53(8-I-3)	1.07(8-I-3)	-6(9-II-2)	0	0
5	274	0.52(2)	0.59(8-I-3)	0.82(8-I-3)	0	0	0
5	275	4.79(8-II-3)	0.54(8-II-3)	1.18(8-I-3)	-7(9-II-2)	-3(9-II-2)	0
5	276	0.49(8-II-3)	0.49(8-I-3)	0.90(8-I-3)	0	-1(9-II-2)	0
5	277	-2.94(8-I-3)	-9.32(2)	2.51(8-I-3)	3(9-II-2)	-35(9-II-2)	0
5	278	-8.25(8-I-3)	-18.17(8-I-3)	2.66(8-I-3)	8(9-II-2)	-45(9-II-2)	0

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
5	279	-1.28(8-I-3)	-6.74(2)	2.59(8-I-3)	5(9-II-2)	-33(9-II-2)	0
5	280	-3.69(8-I-3)	-7.53(2)	2.20(8-I-3)	6(9-II-2)	-34(9-II-2)	0
5	281	-1.23(8-I-3)	-6.13(2)	2.24(8-I-3)	5(9-II-2)	-32(9-II-2)	0
5	282	-7.31(8-I-3)	-9.34(8-I-3)	2.18(8-I-3)	0	-24(9-II-2)	3(9-II-2)
5	283	-0.56(8-I-3)	0.90(8-I-3)	0.99(8-I-3)	0	-3(9-II-2)	0
5	284	1.40(8-II-3)	-9.68(8-I-3)	1.34(8-I-3)	3(9-II-2)	-34(9-II-2)	0
5	285	-0.79(8-I-3)	-9.46(8-I-3)	1.04(8-I-3)	0	-30(9-II-2)	0
5	286	-1.33(8-I-3)	-7.53(2)	1.17(8-I-3)	6(9-II-2)	-36(9-II-2)	0
5	287	-0.63(8-I-3)	-8.80(2)	0.84(8-I-3)	0	-36(9-II-2)	0
5	288	-0.63(8-I-3)	-6.20(2)	1.26(8-I-3)	5(9-II-2)	-36(9-II-2)	0
5	289	-0.60(2)	-6.59(2)	0.76(8-I-3)	0	-36(9-II-2)	0
5	290	-0.79(8-II-3)	-8.73(2)	2.57(8-I-3)	0	-18(9-II-2)	0
5	291	-1.48(8-II-3)	-8.91(2)	3.06(8-I-3)	-1(2)	-19(9-II-2)	0
5	292	-0.73(8-I-3)	-6.88(2)	3.21(8-I-3)	0	-19(9-II-2)	0
5	293	-1.57(8-I-3)	-14.16(2)	2.18(8-I-3)	0	-20(9-II-2)	0
5	294	-0.74(8-II-3)	-7.43(2)	3.19(8-I-3)	0	-23(9-II-2)	0
5	295	-0.28(2)	-6.49(2)	3.31(8-I-3)	3(9-II-2)	-23(9-II-2)	0
5	296	1.32(8-II-3)	-14.30(2)	2.13(8-I-3)	0	-23(9-II-2)	0
5	297	1.59(8-I-3)	-9.67(2)	2.45(8-I-3)	0	-23(9-II-2)	0
5	298	-0.96(8-I-3)	-8.43(2)	3.04(8-I-3)	2(9-II-2)	-23(9-II-2)	0
5	299	-0.51(2)	-7.48(2)	-2.84(8-II-3)	3(9-I-4)	-5(2)	1(9-II-4)
5	300	0.30(8-I-3)	-9.35(2)	-2.42(8-II-3)	0	-5(2)	0
5	301	-0.56(2)	-15.98(2)	-1.97(8-II-3)	0	-8(9-II-1)	-1(9-I-4)
5	302	-0.30(2)	-6.30(2)	-2.94(8-II-3)	-2(9-I-2)	-7(9-II-4)	-1(9-I-4)
5	303	-0.39(9-I-2)	-5.03(2)	-2.86(8-II-3)	-4(9-I-2)	-8(2)	2(9-II-4)
5	304	-0.21(9-II-1)	-5.27(2)	-2.95(8-II-3)	4(9-II-1)	-7(2)	-2(9-I-4)
5	305	0.81(9-II-1)	-3.35(2)	-2.79(9-II-3)	-11(9-I-1)	-8(2)	0
5	306	-0.64(9-II-1)	-4.79(2)	-2.87(8-II-3)	-6(8-II-3)	-9(2)	-2(9-I-4)
5	307	-0.62(9-II-1)	-2.54(8-II-3)	-2.76(9-II-3)	-10(8-II-3)	-9(2)	-2(9-II-3)
5	308	-0.34(9-I-3)	-8.19(2)	-2.86(8-II-3)	4(9-II-4)	-14(9-II-1)	-1(9-I-4)
5	309	0.26(8-II-3)	-9.54(2)	-2.36(8-II-3)	1(9-II-1)	-13(9-II-1)	-1(9-I-4)
5	310	-1.31(8-II-3)	-14.30(2)	-1.98(8-II-3)	3(9-II-4)	-17(9-II-1)	-1(9-I-4)
5	311	-0.50(9-I-4)	-5.69(2)	-2.94(8-II-3)	-4(9-I-1)	-21(9-II-4)	-2(9-I-4)
5	312	-0.31(9-II-3)	-6.20(2)	-2.94(8-II-3)	6(9-II-1)	-19(9-II-4)	-1(9-I-4)
5	313	0.47(9-II-1)	-3.54(2)	-2.78(9-II-3)	-10(8-II-3)	-27(9-II-4)	0
5	314	0.68(9-II-1)	-4.15(2)	-2.87(8-II-3)	-7(8-II-3)	-20(9-II-4)	-2(9-I-4)
5	315	-0.28(9-II-2)	-5.01(2)	-2.91(8-II-3)	-9(9-I-1)	-20(9-II-4)	-2(9-I-4)
5	316	-0.50(9-II-2)	-3.87(9-I-1)	-2.71(9-II-3)	-21(8-II-3)	-28(9-II-4)	-1(9-II-3)
5	317	-0.65(8-II-3)	-6.61(2)	3.19(8-I-3)	3(9-II-2)	-28(9-II-2)	0
5	318	-0.86(2)	-6.16(2)	3.06(8-I-3)	5(9-II-2)	-28(9-II-2)	0
5	319	-0.90(2)	-6.21(2)	2.61(8-I-3)	5(9-II-2)	-31(9-II-2)	0
5	320	-1.14(8-II-3)	-9.49(2)	2.43(8-I-3)	0	-26(9-II-2)	0
5	321	-1.46(8-II-3)	-8.80(2)	2.97(8-I-3)	2(9-II-2)	-27(9-II-2)	0
5	322	-0.72(2)	-7.33(2)	3.01(8-I-3)	4(9-II-2)	-27(9-II-2)	0
5	323	-1.10(8-I-3)	-13.77(8-II-3)	-2.27(8-II-3)	2(9-II-2)	-28(9-II-2)	0
5	324	-0.87(8-II-3)	-7.40(2)	-2.65(8-II-3)	4(9-II-2)	-30(9-II-2)	0
5	325	-1.72(8-II-3)	-6.55(2)	-2.26(8-II-3)	4(9-II-2)	-31(9-II-2)	0
5	326	-7.93(8-II-3)	-20.22(8-II-3)	-2.76(8-II-3)	-4(9-I-1)	-38(9-II-2)	-1(9-II-2)
5	327	-2.26(8-II-3)	-10.52(8-II-3)	-2.41(8-II-3)	2(9-II-2)	-31(9-II-2)	0
5	328	-3.79(8-II-3)	-8.47(2)	-2.31(8-II-3)	4(9-II-1)	-30(9-II-2)	0
5	329	-0.65(9-II-3)	-6.60(2)	-1.27(8-II-3)	4(9-II-2)	-34(9-II-2)	0
5	330	-0.61(2)	-6.18(2)	-0.74(8-II-3)	0	-35(9-II-2)	0
5	331	1.39(8-I-3)	-8.19(2)	-1.22(8-II-3)	4(9-II-2)	-32(9-II-2)	0
5	332	-0.61(2)	-7.27(2)	-0.79(8-II-3)	0	-33(9-II-2)	0
5	333	1.37(8-I-3)	-9.84(8-II-3)	-1.44(8-II-3)	3(9-II-2)	-27(9-II-2)	-1(9-II-2)
5	334	-0.65(8-II-3)	-9.14(2)	-0.88(8-II-3)	0	-31(9-II-2)	0
5	335	-6.95(8-II-3)	-5.05(8-II-3)	-2.28(8-II-3)	-2(9-II-2)	-12(9-II-2)	-3(9-II-2)
5	336	-0.68(8-II-3)	-11.06(8-II-3)	-1.03(8-II-3)	0	-24(9-II-2)	0
5	337	4.33(8-I-3)	0.16(2)	-1.16(8-II-3)	-6(9-II-2)	-1(9-II-1)	0
5	338	0.45(9-I-3)	0.87(8-II-3)	-0.96(8-II-3)	0	-1(9-II-2)	0
5	339	2.54(8-I-3)	-0.30(8-II-3)	-1.06(8-II-3)	-5(9-II-2)	0	0
5	340	0.39(9-I-3)	-0.10(8-I-3)	-0.88(8-II-3)	0	0	0
5	341	1.28(2)	-0.29(8-II-3)	-0.97(8-II-3)	-4(9-II-1)	0	0
5	342	0.56(2)	0.21(8-II-3)	-0.81(8-II-3)	0	0	0

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
5	343	2.09(8-II-3)	-0.32(8-II-3)	-0.92(8-II-3)	-4(9-II-1)	0	0
5	344	0.64(2)	0.28(8-II-3)	-0.77(8-II-3)	0	0	0
5	345	1.23(8-II-3)	-10.34(2)	-2.25(8-II-3)	1(9-II-1)	-26(9-II-1)	0
5	346	-0.95(8-II-3)	-14.75(2)	-2.16(8-II-3)	0	-27(9-II-1)	0
5	347	1.75(8-II-3)	-18.38(8-I-3)	-2.54(8-II-3)	1(9-II-4)	-42(9-II-1)	0
5	348	-0.46(9-I-3)	-6.82(2)	-2.89(8-II-3)	8(9-II-4)	-28(9-II-1)	0
5	349	-0.45(2)	-8.40(2)	-2.79(8-II-3)	6(9-II-1)	-26(9-II-1)	0
5	350	-0.27(9-I-1)	-4.98(2)	-2.85(8-II-3)	-8(9-I-2)	-33(9-II-4)	-1(9-I-4)
5	351	-0.76(8-I-3)	-5.63(2)	-2.86(8-II-3)	-7(9-I-1)	-29(9-II-1)	0
5	352	-0.89(8-II-3)	-3.89(8-II-3)	-2.66(9-II-3)	-22(8-II-3)	-37(9-II-4)	-1(9-II-3)
5	353	-0.50(8-I-3)	-4.22(2)	-2.75(8-II-3)	-12(8-II-3)	-40(9-II-4)	0
5	354	-0.83(8-I-3)	-5.70(9-I-1)	-2.42(9-II-3)	-26(8-II-3)	-47(9-II-4)	-2(9-II-4)
5	355	4.09(8-II-3)	-0.34(8-II-3)	-0.92(8-II-3)	-6(9-II-1)	0	0
5	356	0.65(2)	0.37(8-II-3)	-0.78(8-II-3)	0	0	0
5	357	6.20(8-II-3)	-0.32(8-II-3)	-1.02(8-II-3)	-8(9-II-1)	-1(9-II-1)	0
5	358	0.59(8-II-3)	0.51(8-II-3)	-0.83(8-II-3)	0	0	0
5	359	0.69(8-II-3)	1.15(8-II-3)	-0.91(8-II-3)	0	-6(9-II-1)	0
5	360	8.42(8-II-3)	-9.39(8-I-3)	1.81(8-I-3)	4(8-II-3)	-30(9-II-1)	4(9-II-1)
5	361	0.78(8-II-3)	-0.48(8-II-3)	0.88(8-I-3)	0	-6(9-II-1)	0
5	362	2.29(8-II-3)	-7.73(2)	-2.63(8-II-3)	6(9-II-4)	-35(9-II-1)	0
5	363	-7.17(8-I-3)	-10.14(2)	-2.34(8-II-3)	6(9-II-4)	-39(9-II-1)	1(9-II-2)
5	364	-1.27(9-I-3)	-5.95(2)	-2.59(8-II-3)	-7(9-I-1)	-36(9-II-1)	0
5	365	3.55(8-II-3)	-6.82(2)	-2.26(8-II-3)	-4(9-I-1)	-36(9-II-1)	0
5	366	-0.57(8-II-3)	-4.26(8-II-3)	-2.27(9-II-3)	-24(8-II-3)	-40(9-II-1)	-3(9-II-4)
5	367	0.62(9-II-3)	-3.93(2)	-2.47(8-II-3)	-12(8-II-3)	-35(9-II-1)	0
5	368	1.39(8-II-3)	-5.01(2)	-2.27(8-II-3)	-6(9-II-3)	-36(9-II-1)	0
5	369	1.61(8-II-3)	-5.40(9-I-2)	-1.93(9-II-3)	-12(8-II-3)	-25(9-II-1)	-1(9-II-4)
5	370	3.06(8-II-3)	-8.31(2)	-1.33(8-II-3)	4(9-II-4)	-37(9-II-1)	1(9-II-1)
5	371	-0.83(8-I-3)	-7.63(2)	0.92(8-I-3)	0	-31(9-II-1)	0
5	372	2.61(8-II-3)	-6.95(2)	-1.41(8-II-3)	-4(9-I-1)	-41(9-II-1)	0
5	373	-0.62(8-I-3)	-8.57(2)	-0.86(8-II-3)	0	-40(9-II-1)	0
5	374	2.01(8-II-3)	-5.05(2)	-1.55(9-II-3)	-5(8-II-3)	-42(9-II-1)	0
5	375	-0.41(8-I-3)	-5.91(2)	-0.90(9-II-3)	0	-41(9-II-1)	0
5	376	0.43(9-II-2)	-5.74(8-II-3)	-1.46(9-II-3)	-11(8-II-3)	-41(9-II-1)	0
5	377	-0.20(8-I-3)	-3.55(2)	-0.99(9-II-3)	0	-43(9-II-1)	0
5	378	-0.07(8-II-3)	-6.20(9-I-1)	-0.93(9-II-3)	0	-36(9-II-2)	0
5	1	0.39(8-II-2)	-0.58(2)	-0.35(9-II-1)	-457(9-II-1)	-55(8-I-2)	-91(9-I-1)
5	2	0.71(8-II-1)	0.29(8-II-1)	0.36(2)	-599(8-I-1)	-56(1)	-94(2)
5	3	0.82(8-II-1)	0.32(8-II-1)	0.15(8-II-1)	-665(8-I-1)	-84(9-II-1)	-50(8-I-1)
5	4	0.69(8-II-2)	0.14(8-II-1)	-0.30(2)	-633(8-I-4)	-86(8-I-1)	67(8-II-1)
5	5	0.65(8-II-1)	-0.10(2)	-0.33(2)	-651(8-I-4)	-78(8-I-1)	-47(8-I-1)
5	6	0.61(8-II-1)	0.13(8-I-1)	0.35(9-II-1)	-620(8-I-1)	-72(8-I-4)	-80(9-II-1)
5	7	0.68(9-II-1)	0.11(8-II-1)	0.51(9-II-1)	-545(8-I-1)	-61(1)	-84(9-II-4)
5	8	0.81(9-II-1)	-0.26(9-I-1)	0.44(9-II-4)	-495(9-I-1)	-54(8-I-1)	-82(8-I-4)
5	9	0.74(9-II-1)	0.22(9-II-1)	0.38(8-II-1)	-539(9-I-1)	-56(9-I-1)	-38(8-I-1)
5	10	1.35(9-I-1)	-0.43(9-I-1)	0.55(9-I-1)	-354(9-I-1)	30(9-I-1)	-88(9-I-1)
5	11	1.00(9-I-1)	-0.76(9-I-1)	0.40(8-I-1)	-89(9-I-1)	111(9-I-1)	-177(9-I-1)
5	12	0.95(9-I-1)	-1.07(9-I-1)	0.31(8-II-1)	52(9-II-4)	139(9-I-1)	-174(9-I-1)
5	13	1.04(9-I-1)	-1.46(9-I-1)	0.31(9-II-4)	108(9-I-1)	185(9-I-1)	-211(9-I-1)
5	14	0.71(8-II-4)	-1.65(9-I-1)	0.37(9-II-1)	260(9-I-1)	232(9-I-1)	-142(9-I-1)
5	15	0.76(9-II-1)	-1.86(9-I-1)	0.59(9-II-1)	316(9-I-1)	219(9-I-1)	-86(9-I-1)
5	16	0.66(9-II-1)	-1.92(9-I-1)	0.51(9-II-1)	465(9-I-1)	269(9-I-1)	-51(9-II-4)
5	17	0.72(1)	-1.59(9-I-1)	0.58(9-II-4)	557(9-I-1)	256(9-I-1)	-63(9-II-1)
5	18	0.80(1)	-1.26(9-I-1)	0.63(9-II-4)	608(9-I-1)	212(9-I-1)	-61(9-II-1)
5	19	0.76(1)	-0.94(9-I-1)	-0.61(9-I-4)	599(9-I-1)	175(9-I-1)	62(9-I-1)
5	20	0.73(9-II-1)	-0.64(9-I-1)	-0.76(9-I-4)	571(9-I-1)	143(9-I-1)	78(9-I-1)
5	21	0.68(9-II-1)	-0.42(9-I-1)	-0.83(9-I-4)	551(9-I-1)	119(9-I-1)	82(9-I-1)
5	22	0.64(9-II-1)	0.37(9-II-1)	-0.80(9-I-1)	557(8-I-1)	93(8-I-1)	79(9-I-1)
5	23	0.59(9-II-1)	0.67(8-II-1)	-0.76(9-I-1)	631(8-I-1)	108(8-I-1)	62(9-I-1)
5	24	0.64(9-II-1)	0.74(8-II-1)	0.82(9-II-4)	671(8-I-1)	146(8-I-1)	-37(9-II-4)
5	25	0.79(9-II-1)	0.64(8-II-1)	0.87(9-II-1)	632(8-I-1)	148(8-I-1)	-38(9-II-4)
5	26	0.86(9-II-1)	-0.76(9-II-4)	0.71(9-II-1)	597(8-I-1)	172(9-II-4)	-38(9-II-1)
5	27	0.97(9-II-3)	-1.00(9-II-4)	0.39(9-II-1)	614(8-I-4)	210(9-II-4)	19(8-II-1)
5	28	0.98(9-II-3)	-1.00(9-II-1)	-0.30(8-II-1)	624(8-I-4)	197(9-II-1)	41(2)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
5	29	0.95(9-II-3)	-0.83(2)	-0.55(2)	623(8-I-4)	164(9-II-1)	66(2)
5	30	0.88(8-II-2)	-0.67(2)	-0.86(2)	633(8-I-4)	127(9-II-1)	86(2)
5	31	0.78(8-II-2)	-0.38(8-II-1)	-1.11(2)	662(8-I-1)	78(9-II-1)	97(2)
5	32	0.67(8-II-2)	0.31(8-I-1)	-1.27(2)	712(8-I-1)	61(8-I-1)	99(2)
5	33	-0.90(2)	1.04(2)	-1.30(2)	804(8-I-1)	-114(2)	105(2)
5	34	-1.69(2)	1.94(2)	-0.86(2)	943(8-I-1)	-209(8-II-1)	66(8-I-1)
5	35	-2.17(2)	2.70(2)	-0.34(9-I-1)	1138(8-I-1)	-369(8-II-1)	51(8-I-1)
5	36	-1.95(2)	2.50(8-II-1)	1.42(2)	1185(8-I-1)	-399(8-II-1)	-98(2)
5	37	-0.88(2)	1.80(8-II-1)	1.79(2)	1049(8-I-1)	-291(8-II-1)	-93(2)
5	38	0.63(9-II-4)	1.15(9-I-1)	2.00(2)	895(8-I-1)	200(9-II-1)	-100(2)
5	39	0.69(9-II-3)	-0.83(9-II-1)	1.68(2)	705(8-I-1)	168(9-II-1)	-115(2)
5	40	0.93(9-II-3)	-1.33(2)	1.34(2)	618(8-I-1)	201(2)	-82(2)
5	41	1.00(9-II-3)	-1.85(2)	0.92(8-II-1)	539(8-I-1)	261(2)	-45(9-I-1)
5	42	1.05(9-II-3)	-2.10(2)	0.69(9-I-1)	481(8-I-1)	298(2)	50(9-II-1)
5	43	1.04(9-II-3)	-2.24(2)	-0.69(9-II-1)	436(8-I-1)	320(2)	74(2)
5	44	0.99(9-II-3)	-2.26(2)	-0.93(9-II-1)	436(9-I-3)	323(2)	116(2)
5	45	0.94(9-II-3)	-2.22(2)	-1.36(2)	474(9-I-3)	307(2)	148(2)
5	46	0.82(9-II-3)	-1.91(2)	-1.90(2)	507(9-I-4)	237(2)	200(2)
5	47	-0.56(2)	-1.40(2)	-2.33(2)	535(9-I-4)	203(2)	235(2)
5	48	-1.02(2)	-0.95(9-I-1)	-2.64(2)	566(9-I-4)	164(9-I-1)	254(2)
5	49	-1.57(2)	1.06(9-II-1)	-2.64(2)	560(9-I-4)	172(9-I-1)	277(2)
5	50	-2.10(2)	1.94(9-II-4)	-2.41(2)	552(9-I-3)	-269(9-II-4)	247(2)
5	51	-3.26(9-I-3)	2.41(9-II-4)	-1.72(2)	514(9-I-3)	-337(9-II-4)	110(2)
5	52	-2.03(2)	1.11(9-II-1)	-1.66(2)	261(2)	-198(9-II-4)	140(2)
5	53	-1.93(2)	0.55(9-II-1)	-1.50(2)	354(2)	63(9-I-1)	216(2)
5	54	-1.75(2)	-0.41(2)	-1.41(2)	-343(9-I-4)	-62(9-I-3)	178(2)
5	55	-0.94(2)	-0.58(2)	-1.07(2)	-386(9-I-4)	-67(9-I-3)	141(2)
5	56	0.69(9-II-1)	-1.27(9-I-1)	0.41(9-II-4)	260(9-I-1)	214(9-I-1)	-94(8-I-1)
5	57	0.68(1)	-1.18(9-I-1)	0.39(9-II-4)	148(9-I-1)	157(9-I-1)	-150(9-I-1)
5	58	0.63(8-II-1)	0.22(8-I-1)	0.41(9-II-1)	72(2)	36(8-I-1)	-104(9-II-1)
5	59	0.76(9-II-1)	-0.44(9-II-4)	0.55(9-II-1)	362(8-I-1)	108(9-II-4)	-95(9-II-1)
5	60	0.67(9-II-1)	0.50(8-II-1)	0.71(9-II-1)	477(8-I-1)	109(8-I-1)	-83(9-II-1)
5	61	0.74(9-II-1)	-0.68(9-I-1)	0.52(9-II-4)	154(9-I-1)	86(9-I-1)	-89(9-II-4)
5	62	0.76(9-II-1)	-0.50(9-I-1)	0.48(9-II-4)	-109(9-I-1)	-31(8-I-4)	-98(8-I-4)
5	63	0.75(9-II-1)	-0.42(9-I-1)	0.54(9-II-1)	103(2)	47(9-I-1)	99(9-I-4)
5	64	0.73(9-II-1)	-0.67(9-I-1)	0.44(9-II-4)	142(9-I-1)	72(9-I-1)	-89(8-I-4)
5	65	0.72(1)	-1.09(9-I-1)	0.45(9-II-4)	289(9-I-1)	154(9-I-1)	-88(8-I-1)
5	66	0.72(9-II-1)	-0.48(9-I-1)	-0.62(9-I-1)	357(9-I-1)	98(9-I-1)	97(9-I-4)
5	67	0.73(9-II-1)	-0.79(9-I-1)	0.55(9-II-4)	375(9-I-1)	129(9-I-1)	-78(9-II-4)
5	68	0.72(1)	-1.03(9-I-1)	0.53(9-II-4)	383(9-I-1)	153(9-I-1)	-86(9-II-4)
5	69	0.69(9-II-1)	0.20(8-II-1)	0.55(9-II-1)	82(2)	-27(8-II-1)	-110(9-II-4)
5	70	0.70(9-II-1)	0.36(8-II-1)	0.65(9-II-1)	382(8-I-1)	81(8-I-1)	94(9-I-4)
5	71	0.69(9-II-1)	0.25(9-II-1)	-0.72(9-I-1)	423(8-I-1)	75(9-I-1)	99(9-I-1)
5	72	0.80(8-II-2)	-0.72(9-II-1)	-0.30(8-II-1)	483(8-I-4)	172(9-II-1)	48(8-II-1)
5	73	0.85(8-II-2)	-0.50(9-II-4)	-0.32(2)	312(8-I-4)	131(9-II-1)	61(8-II-1)
5	74	0.81(8-II-2)	-0.58(2)	-0.47(2)	447(8-I-4)	138(9-II-1)	72(2)
5	75	0.78(9-II-3)	-0.67(9-II-4)	0.28(9-II-1)	424(8-I-4)	166(9-II-4)	42(8-II-1)
5	76	0.65(8-II-2)	-0.28(2)	-0.33(2)	62(2)	60(9-II-3)	70(8-II-1)
5	77	0.64(9-II-3)	-0.57(9-II-1)	1.22(2)	391(8-I-1)	106(9-II-1)	-180(2)
5	78	-0.77(2)	0.67(8-II-1)	0.71(2)	235(2)	-133(8-II-1)	-152(2)
5	79	-0.82(2)	1.18(8-II-1)	1.66(2)	820(8-I-1)	188(9-II-1)	-157(2)
5	80	-1.53(2)	1.62(8-II-1)	0.91(2)	771(8-I-1)	-325(8-II-1)	-100(2)
5	81	0.71(8-II-2)	-0.21(2)	-0.95(2)	540(8-I-1)	80(2)	131(2)
5	82	0.73(8-II-2)	-0.12(2)	-0.78(2)	375(8-I-1)	72(2)	136(2)
5	83	0.57(8-II-2)	0.21(8-II-1)	-0.87(2)	517(8-I-1)	40(8-I-1)	124(2)
5	84	0.81(8-II-2)	-0.39(2)	-0.73(2)	458(8-I-4)	104(2)	108(2)
5	85	0.63(8-II-2)	0.14(9-I-1)	-0.50(2)	102(2)	40(8-II-1)	120(8-II-1)
5	86	-0.70(2)	0.64(2)	-0.20(2)	185(2)	-81(8-II-2)	100(8-II-1)
5	87	-1.47(2)	1.72(2)	-0.22(9-I-1)	819(8-I-1)	-264(8-II-1)	54(8-II-1)
5	88	-0.93(2)	0.94(2)	-0.69(2)	590(8-I-1)	-114(8-II-2)	136(2)
5	89	0.64(9-II-3)	-1.36(2)	0.48(9-I-1)	190(8-I-1)	180(2)	-102(9-I-1)
5	90	0.79(9-II-3)	-0.94(2)	0.44(9-I-1)	-54(8-II-2)	105(2)	-121(9-I-1)
5	91	0.59(9-II-3)	-1.31(2)	-0.56(9-II-1)	211(2)	192(2)	131(9-II-1)
5	92	0.73(9-II-3)	-1.03(2)	0.60(9-I-1)	203(8-I-1)	133(2)	-127(9-I-1)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
5	93	0.64(9-II-3)	-0.99(2)	0.73(2)	331(8-I-1)	157(2)	-132(8-II-1)
5	94	0.81(9-II-3)	-1.77(2)	-0.66(9-II-1)	339(2)	271(2)	114(9-II-1)
5	95	0.84(9-II-3)	-1.68(2)	0.56(9-I-1)	334(8-I-1)	238(2)	87(9-II-1)
5	96	0.81(9-II-3)	-1.42(2)	0.73(8-II-4)	382(8-I-1)	211(2)	-100(9-I-1)
5	97	0.78(9-II-3)	-1.77(2)	-0.90(2)	339(2)	276(2)	141(2)
5	98	0.75(9-II-3)	-1.71(2)	-1.48(2)	387(9-I-3)	255(2)	205(2)
5	99	-1.74(2)	0.82(9-II-1)	-1.72(2)	268(2)	110(9-I-1)	277(2)
5	100	-0.88(2)	-0.93(2)	-2.03(2)	386(9-I-4)	162(2)	299(2)
5	101	-1.47(2)	-0.64(9-I-1)	-1.87(2)	254(9-I-3)	106(9-I-1)	311(2)
5	102	-0.56(2)	-1.17(2)	-1.61(2)	267(9-I-3)	178(2)	262(2)
5	103	-0.61(2)	-0.82(2)	-1.39(2)	92(2)	115(2)	249(2)
5	104	0.56(9-II-3)	-1.27(2)	-0.97(2)	228(2)	194(2)	165(9-II-4)
6	1	0.83(1)	-0.33(8-II-4)	0.51(9-I-1)	-354(9-I-1)	-319(9-I-1)	-295(9-I-1)
6	2	0.94(9-II-1)	0.21(8-I-1)	0.41(1)	-320(9-I-1)	-337(9-I-1)	-269(9-I-1)
6	3	0.89(9-II-1)	0.51(9-I-1)	0.54(1)	-338(1)	-304(9-I-1)	-242(1)
6	4	0.90(8-II-1)	0.62(9-II-2)	0.55(9-II-1)	-403(1)	-349(1)	-290(1)
6	5	1.17(8-II-1)	1.01(9-II-2)	0.73(9-II-2)	-350(9-I-2)	-212(1)	-190(8-II-3)
6	6	1.13(8-II-1)	1.19(9-II-2)	0.80(9-II-2)	-155(8-II-3)	-146(9-II-2)	-88(8-II-3)
6	7	1.01(8-II-1)	-2.11(9-I-2)	-1.02(9-I-2)	256(9-I-2)	-174(9-II-2)	85(9-I-2)
6	8	-1.71(9-I-2)	-2.58(9-I-2)	-1.49(9-I-2)	447(9-I-2)	297(9-I-2)	216(9-I-2)
6	9	0.98(9-II-1)	-1.71(9-I-2)	0.61(9-II-2)	445(9-I-2)	388(9-I-2)	241(9-I-2)
6	10	0.77(8-II-1)	1.39(9-II-2)	0.61(9-II-2)	384(9-I-2)	341(9-I-2)	248(9-I-2)
6	11	0.79(8-II-1)	1.19(9-II-2)	0.77(9-II-2)	316(9-I-2)	297(9-I-2)	238(9-I-2)
6	12	0.80(8-II-1)	0.96(9-II-2)	0.89(9-II-2)	261(9-I-2)	252(9-I-2)	224(9-I-2)
6	13	0.81(8-II-1)	0.75(9-II-2)	0.97(9-II-2)	228(9-I-2)	215(9-I-2)	210(9-I-2)
6	14	0.79(8-II-1)	0.62(9-II-2)	1.03(9-II-2)	214(1)	193(8-II-3)	205(9-I-2)
6	15	0.75(8-II-1)	0.56(8-I-1)	1.01(9-II-2)	216(1)	199(1)	203(9-I-2)
6	16	0.74(8-II-1)	0.69(9-I-1)	0.98(9-II-1)	216(9-I-1)	209(1)	200(9-I-1)
6	17	0.85(9-II-1)	0.73(9-I-1)	0.94(9-II-2)	223(9-I-1)	217(1)	200(9-I-1)
6	18	1.01(9-II-1)	0.84(9-I-1)	0.89(9-II-2)	257(9-I-1)	226(1)	199(9-I-1)
6	19	1.21(9-II-1)	0.83(9-I-1)	0.75(9-II-2)	301(9-I-1)	233(8-II-4)	211(9-I-1)
6	20	1.37(9-II-1)	0.77(9-I-1)	0.62(1)	336(9-I-1)	271(9-I-1)	218(9-I-1)
6	21	1.54(9-II-1)	0.53(9-I-1)	0.73(9-I-1)	389(9-I-1)	352(9-I-1)	210(9-I-1)
6	22	1.58(9-II-1)	-0.14(8-II-1)	1.03(9-I-1)	423(9-I-1)	431(9-I-1)	188(9-I-1)
6	23	1.53(9-II-1)	-0.43(8-II-4)	1.24(9-I-1)	406(9-I-1)	460(9-I-1)	135(9-I-1)
6	24	1.44(9-II-1)	-0.21(8-II-4)	1.13(9-I-1)	249(9-I-1)	523(9-I-1)	74(9-I-1)
6	25	0.89(9-II-1)	-0.20(8-II-4)	1.49(9-I-1)	109(9-I-1)	565(9-I-1)	44(8-II-4)
6	26	0.66(1)	-0.29(9-I-1)	1.54(9-I-1)	-44(9-II-1)	558(9-I-1)	15(8-II-1)
6	27	1.22(9-I-1)	-0.43(9-I-1)	1.36(9-I-1)	-143(9-I-1)	464(9-I-1)	-43(9-I-1)
6	28	1.65(9-I-1)	-0.61(9-I-1)	1.16(9-I-1)	-197(9-I-1)	346(9-I-1)	-96(9-I-1)
6	29	1.75(9-I-1)	-0.85(9-I-1)	1.09(9-I-1)	-209(9-I-1)	116(9-I-1)	-138(9-I-1)
6	30	1.56(9-I-1)	-0.59(9-I-1)	0.95(9-I-1)	-329(9-I-1)	-70(9-I-1)	-235(9-I-1)
6	31	1.12(9-I-1)	-0.40(9-I-1)	0.80(9-I-1)	-358(9-I-1)	-215(9-I-1)	-274(9-I-1)
6	32	0.75(9-II-1)	-0.27(8-II-4)	1.03(9-I-1)	-68(8-II-1)	301(9-I-1)	-45(9-I-1)
6	33	0.87(1)	-0.32(8-II-4)	0.98(9-I-1)	-214(9-I-1)	140(9-I-1)	-124(9-I-1)
6	34	0.83(9-II-1)	-0.20(8-II-4)	0.65(9-I-1)	-159(9-I-1)	39(8-II-1)	-114(9-I-1)
6	35	0.96(8-II-1)	1.02(9-II-2)	0.77(9-II-2)	-124(8-II-3)	-182(9-II-2)	-81(1)
6	36	0.90(9-II-1)	1.25(9-II-2)	0.74(9-II-2)	239(9-I-2)	204(9-I-2)	115(9-I-2)
6	37	0.83(9-II-1)	1.09(9-II-2)	0.67(9-II-2)	167(9-I-2)	211(9-I-2)	132(9-I-2)
6	38	0.85(8-II-1)	0.57(9-II-2)	0.76(9-II-1)	-47(8-II-3)	-50(9-I-1)	-42(9-II-2)
6	39	0.83(8-II-1)	0.78(9-II-2)	0.70(9-II-1)	100(8-I-1)	-108(9-II-2)	-59(9-II-2)
6	40	0.78(8-II-1)	0.74(9-II-2)	0.72(9-II-2)	-156(8-II-3)	-162(9-II-2)	-104(9-II-1)
6	41	0.79(8-II-1)	0.73(9-II-2)	0.79(9-II-2)	-57(8-II-1)	-73(9-II-2)	-60(9-II-2)
6	42	0.90(8-II-1)	0.80(9-II-2)	0.66(9-II-2)	-107(8-II-3)	-174(9-II-2)	-74(9-II-1)
6	43	0.83(8-II-1)	1.04(9-II-2)	0.72(9-II-2)	140(8-I-1)	181(9-I-2)	123(9-I-2)
6	44	0.78(8-II-1)	0.84(9-II-2)	0.77(9-II-2)	144(8-I-1)	168(9-I-2)	128(9-I-2)
6	45	0.78(8-II-1)	0.55(8-I-1)	0.87(9-II-2)	139(8-I-1)	121(8-II-1)	139(9-I-2)
6	46	0.78(8-II-1)	0.72(9-II-2)	0.82(9-II-2)	140(8-I-1)	145(9-I-2)	135(9-I-2)
6	47	0.77(8-II-1)	0.64(9-II-2)	0.94(9-II-2)	149(8-I-1)	139(8-II-3)	142(9-I-2)
6	48	0.95(9-II-1)	0.68(9-I-1)	0.74(9-II-2)	170(9-I-1)	146(9-II-1)	115(9-I-1)
6	49	0.97(9-II-1)	0.50(9-I-1)	0.69(9-II-2)	-115(9-II-1)	-91(9-I-1)	-57(9-II-2)
6	50	1.02(9-II-1)	0.55(9-I-1)	0.62(9-II-2)	142(9-I-1)	143(9-II-1)	90(9-I-1)
6	51	0.85(9-II-1)	0.67(9-I-1)	0.78(9-II-2)	72(9-I-1)	82(9-II-1)	61(9-I-1)
6	52	0.77(8-II-1)	0.59(9-I-1)	0.76(9-II-1)	-38(8-II-3)	85(9-II-1)	68(9-I-2)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
6	53	1.01(9-II-1)	-0.17(8-II-4)	0.97(9-I-1)	-93(9-II-1)	359(9-I-1)	36(9-II-1)
6	54	1.28(9-II-1)	-0.31(8-II-4)	1.02(9-I-1)	237(9-I-1)	406(9-I-1)	62(8-II-4)
6	55	1.01(9-II-1)	-0.21(8-II-4)	0.68(9-I-1)	-121(9-II-1)	145(8-II-4)	32(9-II-1)
6	56	1.24(9-II-1)	-0.22(8-II-4)	0.85(9-I-1)	246(9-I-1)	295(9-I-1)	82(8-II-4)
6	57	1.28(9-II-1)	0.17(9-I-1)	0.65(9-I-1)	250(9-I-1)	188(8-II-4)	98(9-I-1)
6	58	1.07(9-II-1)	0.17(8-I-1)	0.48(8-I-1)	-145(9-II-1)	122(9-II-1)	-38(9-I-1)
6	59	1.17(9-II-1)	0.52(9-I-1)	0.57(1)	176(9-I-1)	137(9-II-1)	79(9-I-1)
6	1	0.78(8-II-3)	-1.02(9-II-2)	0.43(9-II-2)	0	-9(9-I-2)	-1(8-II-3)
6	2	0.47(8-I-3)	-1.55(8-II-3)	0.63(9-II-2)	55(8-II-3)	-5(9-I-3)	-2(9-I-2)
6	3	-2.89(8-I-3)	-1.21(8-I-3)	1.11(9-II-2)	0	-9(9-I-2)	0
6	4	1.92(8-I-3)	-0.83(2)	0.84(9-II-2)	19(8-II-3)	-5(9-I-2)	0
6	5	-1.40(8-I-3)	-3.84(8-I-3)	0.93(9-II-2)	20(8-II-3)	-13(9-I-2)	0
6	6	1.63(8-II-3)	-2.87(9-II-2)	1.92(9-II-2)	0	-9(9-I-2)	1(9-I-2)
6	7	3.01(8-I-3)	-0.75(2)	1.88(9-II-2)	33(8-II-3)	-6(9-I-3)	2(9-I-2)
6	8	-1.31(9-II-2)	-1.37(8-II-3)	0.97(9-II-2)	61(8-II-3)	-13(8-I-3)	-3(9-I-2)
6	9	0.84(9-II-2)	-1.39(9-I-2)	1.41(9-II-2)	65(8-II-3)	-15(9-I-3)	-3(9-I-2)
6	10	-5.61(9-II-2)	-0.58(2)	2.61(9-II-2)	62(8-II-3)	-39(8-I-3)	-5(9-I-2)
6	11	1.91(9-II-2)	-2.12(9-I-2)	3.52(9-II-2)	34(8-II-3)	-17(9-I-3)	-8(9-I-2)
6	12	-2.71(8-I-3)	-8.43(8-I-3)	2.21(9-II-2)	28(8-II-3)	-16(9-I-2)	0
6	13	-5.84(9-II-2)	-4.88(8-I-3)	1.87(9-II-2)	63(8-II-3)	-15(9-I-3)	-3(8-II-3)
6	14	-2.73(9-II-2)	-15.49(8-I-3)	3.41(9-II-2)	22(8-II-3)	-23(9-I-3)	-4(8-II-3)
6	15	1.03(9-I-2)	-4.62(8-I-3)	3.31(9-II-2)	6(8-II-3)	-21(8-I-3)	-5(9-I-2)
6	16	-1.38(9-I-2)	-0.83(9-I-2)	2.65(9-II-2)	5(2)	-3(2)	2(9-I-2)
6	17	1.74(9-I-2)	-3.92(9-II-2)	2.54(9-II-2)	5(2)	-6(9-I-2)	2(9-I-2)
6	18	0.52(9-II-2)	-1.42(9-II-2)	2.23(9-II-2)	0	-3(8-I-3)	1(9-I-2)
6	19	-1.81(9-I-2)	-0.46(9-I-2)	2.53(9-II-2)	-10(9-I-2)	-5(8-I-3)	1(9-I-2)
6	20	0.94(9-II-2)	2.96(9-II-2)	2.55(9-II-2)	-10(9-I-2)	9(8-II-3)	2(9-I-2)
6	21	-0.47(9-I-2)	-0.40(2)	3.08(9-II-2)	11(9-II-2)	-5(9-I-3)	3(9-I-2)
6	22	3.22(9-II-2)	-3.56(9-I-2)	1.52(9-II-2)	0	-8(8-I-3)	0
6	23	-1.79(9-I-2)	-1.28(8-II-3)	0.57(8-I-3)	0	-10(2)	0
6	24	1.98(9-I-2)	-0.46(2)	1.07(8-I-3)	-17(9-I-2)	-5(8-I-3)	0
6	25	-2.26(9-I-2)	-4.78(9-I-2)	1.03(8-I-3)	-18(9-I-2)	18(8-II-3)	0
6	26	-3.11(9-II-2)	-0.69(9-I-2)	2.16(9-II-2)	-37(9-I-2)	10(8-II-3)	2(8-II-3)
6	27	-0.44(9-II-2)	-1.66(2)	0.67(8-I-3)	-46(9-I-2)	13(8-II-3)	2(9-II-2)
6	28	0.54(9-II-2)	0.59(9-I-2)	3.02(9-II-2)	11(9-II-2)	-3(9-II-3)	2(8-II-3)
6	29	-6.93(9-II-2)	-1.60(9-II-2)	3.09(9-II-2)	39(8-II-3)	-4(9-I-3)	2(9-I-2)
6	30	0.11(9-II-2)	-3.12(9-I-2)	0.97(8-I-3)	-47(9-I-2)	21(8-II-3)	2(9-II-2)
6	31	2.62(9-II-2)	-7.85(9-I-2)	2.14(9-II-2)	-42(9-I-2)	26(8-II-3)	1(9-II-3)
6	32	1.90(9-II-2)	-2.41(9-I-2)	3.02(9-II-2)	-54(9-I-2)	9(9-II-3)	3(8-II-3)
6	33	1.72(9-I-2)	-1.50(8-II-3)	0.76(8-I-3)	-74(9-I-2)	-15(9-I-3)	4(9-II-2)
6	34	4.83(9-II-2)	-2.27(8-II-3)	2.26(8-I-3)	-74(9-I-2)	-47(9-I-2)	-4(9-I-2)
6	35	1.47(8-I-3)	-11.68(9-I-2)	2.93(8-I-3)	-23(9-I-2)	-35(9-I-3)	-7(9-I-2)
6	36	-1.07(8-I-3)	-1.58(2)	3.25(8-I-3)	-3(8-II-3)	-17(9-I-2)	4(8-I-3)
6	37	1.50(9-II-2)	-1.50(8-I-3)	3.71(9-II-2)	5(8-II-3)	-14(8-I-3)	-3(9-I-2)
6	38	-0.18(9-I-3)	-1.78(9-I-2)	3.79(9-II-2)	14(8-II-3)	-21(9-I-2)	-6(9-I-2)
6	39	-0.94(9-II-2)	-4.40(8-I-3)	3.32(9-II-2)	10(9-I-2)	20(9-II-3)	-3(9-I-2)
6	40	0.87(9-II-2)	-1.75(9-I-3)	4.07(9-II-2)	2(8-II-3)	-8(9-I-3)	2(9-II-1)
6	41	-0.38(9-II-2)	-2.89(9-I-2)	3.38(9-II-2)	5(9-II-3)	12(9-II-3)	2(9-II-1)
6	42	0.13(9-I-2)	-2.70(9-I-3)	4.13(9-II-2)	2(9-II-2)	-7(8-II-3)	3(9-II-3)
6	43	0.94(9-I-2)	-4.68(9-I-3)	3.90(9-II-2)	17(9-II-3)	16(8-I-3)	4(9-II-3)
6	44	1.08(9-II-2)	-6.97(9-I-3)	3.46(9-II-2)	13(9-II-3)	-43(9-II-3)	2(9-II-3)
6	45	0.52(9-II-2)	-7.43(9-I-2)	3.32(9-II-2)	5(9-II-2)	7(9-II-2)	3(9-II-3)
6	46	-1.60(9-II-2)	-3.83(9-I-3)	4.05(9-II-2)	7(9-II-3)	-9(8-II-3)	3(9-II-3)
6	47	1.67(9-II-2)	-9.22(9-I-2)	3.39(9-II-2)	8(9-II-3)	-18(8-II-3)	3(9-II-3)
6	48	-1.32(9-II-2)	-14.69(9-I-2)	3.10(9-II-2)	3(9-II-2)	-31(9-II-3)	3(9-I-2)
6	49	1.99(9-II-2)	-21.82(9-I-2)	3.03(9-II-2)	-2(9-II-2)	-58(9-II-3)	4(9-I-2)
6	50	0.54(9-II-2)	-9.99(9-I-2)	2.52(9-II-2)	0	-67(9-II-3)	2(9-I-2)
6	51	0.89(8-I-3)	-6.99(9-I-2)	2.95(9-II-2)	-4(9-I-2)	-33(9-I-2)	4(8-I-3)
6	52	-0.84(8-I-3)	-2.40(9-I-3)	3.48(8-I-3)	-1(8-II-3)	-12(9-I-2)	3(8-I-3)
6	53	0.32(8-I-3)	-2.86(9-I-3)	3.02(9-II-2)	-6(9-I-2)	-21(9-I-2)	3(8-I-3)
6	54	0.06(8-I-3)	-3.64(9-I-3)	3.52(8-I-3)	-2(9-II-2)	-9(2)	3(9-I-3)
6	55	-0.37(8-I-3)	-7.64(8-I-3)	2.99(9-II-2)	-5(9-I-2)	-18(8-II-3)	2(9-I-3)
6	56	0.90(8-I-3)	-5.00(9-I-3)	3.44(8-I-3)	-1(9-I-2)	-17(9-II-3)	2(9-I-3)
6	57	-0.84(8-I-3)	-13.43(8-I-3)	2.85(8-I-3)	6(9-II-2)	-26(9-II-3)	2(9-I-2)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
6	58	1.06(8-I-3)	-6.47(9-I-3)	3.12(8-I-3)	-6(9-I-2)	-28(9-II-3)	3(9-I-2)
6	59	-0.92(8-I-3)	-18.22(8-I-3)	2.46(8-I-3)	3(9-II-2)	55(9-I-3)	2(9-I-3)
6	60	0.25(8-II-3)	-7.86(8-I-3)	2.06(8-I-3)	0	52(9-I-2)	-2(9-II-2)
7	1	-0.08(2)	-0.69(9-I-4)	-2.89(9-I-3)	141(9-I-3)	1133(9-I-3)	-72(2)
7	2	-0.11(8-II-3)	-0.77(8-II-4)	-3.10(9-I-3)	85(9-I-3)	693(9-I-3)	-69(2)
7	3	-0.19(9-I-3)	-2.05(9-I-3)	-2.84(9-I-3)	50(9-I-3)	388(9-I-3)	-43(2)
7	4	-1.12(9-I-3)	-6.09(9-I-3)	-1.84(9-I-3)	-18(2)	124(9-I-3)	61(9-I-3)
7	5	-0.14(9-I-3)	-0.88(2)	-1.92(9-I-3)	75(9-I-3)	597(9-I-3)	-36(9-II-4)
7	6	-0.14(9-I-4)	-0.73(2)	-2.08(9-I-3)	40(9-I-3)	346(9-I-3)	-15(9-II-1)
7	7	-0.18(9-I-3)	-0.50(1)	-2.12(9-I-3)	22(9-I-4)	183(9-I-3)	26(2)
7	8	-0.39(9-I-3)	-2.46(9-I-3)	-1.94(9-I-3)	11(9-I-4)	-94(2)	34(9-II-4)
7	9	-0.09(2)	-0.94(2)	-1.57(9-I-3)	79(9-II-1)	628(9-II-1)	-24(9-II-1)
7	10	-0.05(9-II-4)	-0.73(2)	-1.64(9-I-3)	39(9-II-1)	284(9-II-1)	10(2)
7	11	-0.06(9-II-1)	-0.64(2)	-1.64(9-I-3)	17(9-II-1)	-107(2)	7(2)
7	12	-0.12(9-I-3)	-0.92(9-I-3)	-1.57(9-I-3)	4(9-II-1)	-50(2)	-19(9-I-1)
7	13	-0.09(1)	-0.73(9-II-1)	-1.34(9-I-3)	83(9-II-1)	643(9-II-1)	9(8-II-1)
7	14	-0.10(1)	-0.58(9-II-1)	-1.39(9-I-3)	13(9-II-1)	103(9-II-1)	-13(2)
7	15	-0.07(8-I-3)	-0.55(9-II-1)	-1.38(9-I-3)	-11(2)	-59(2)	-19(9-II-1)
7	16	-0.06(2)	-0.46(2)	-1.37(9-I-3)	-7(2)	-54(2)	-11(9-II-1)
7	1	-1.17(8-I-1)	-0.84(9-I-1)	-1.94(9-I-1)	187(8-II-1)	27(8-II-1)	-22(8-I-1)
7	2	2.63(9-I-1)	-1.22(9-I-1)	-2.02(9-I-1)	586(8-II-1)	32(8-II-1)	-5(8-II-1)
7	3	-2.25(9-I-1)	-2.54(9-II-1)	-1.72(9-I-1)	424(8-I-1)	18(8-I-1)	-20(8-I-1)
7	4	-1.07(9-I-1)	-2.92(9-II-1)	-2.34(9-I-1)	134(8-II-1)	41(8-I-1)	-24(8-I-1)
7	5	-1.08(9-I-1)	-0.51(9-I-1)	-2.20(9-I-1)	160(8-I-1)	40(8-I-1)	-23(8-I-1)
7	6	0.40(9-I-1)	-2.71(9-II-1)	-1.90(9-I-1)	114(8-II-1)	4(9-I-1)	-12(8-I-1)
7	7	-0.46(8-I-1)	-1.97(9-II-1)	-2.45(9-I-1)	-346(8-I-1)	11(8-II-1)	-11(8-II-1)
7	8	0.90(8-II-1)	-0.72(9-I-1)	-1.95(9-I-1)	481(8-II-1)	17(8-II-1)	-14(8-I-1)
7	9	-0.68(8-II-1)	-2.07(9-II-1)	-2.45(9-I-1)	-255(8-I-1)	26(8-I-1)	-23(8-I-1)
7	10	-0.48(8-I-1)	-0.91(9-II-1)	-2.69(9-I-1)	-333(8-I-1)	48(8-I-1)	-6(8-II-1)
7	11	-1.05(9-I-1)	-1.06(9-II-1)	-2.80(9-I-1)	-160(8-I-1)	67(8-I-1)	-12(8-I-1)
7	12	-0.87(9-I-1)	-1.22(9-II-1)	-2.64(9-I-1)	212(8-II-1)	50(8-I-1)	-16(8-I-1)
7	13	-1.12(9-I-1)	-0.65(9-II-1)	-2.67(9-I-1)	-83(9-II-1)	55(8-I-1)	-20(8-I-1)
7	14	-0.59(9-I-1)	-1.26(9-II-1)	-2.67(9-I-1)	-145(8-I-1)	73(8-I-1)	-8(8-I-1)
7	15	1.33(9-II-1)	-0.94(9-II-1)	-2.64(9-I-1)	-99(8-I-1)	91(8-I-1)	-4(8-I-1)
7	16	5.92(9-I-1)	-3.20(9-II-1)	-2.16(9-I-1)	-364(8-II-1)	44(8-II-1)	-19(8-II-1)
7	17	4.56(9-I-1)	-2.12(9-I-1)	-2.20(9-I-1)	-524(8-I-1)	45(8-II-1)	-16(8-II-1)
7	18	-1.49(9-II-4)	-2.20(9-II-1)	-2.43(9-I-1)	-339(8-I-1)	22(8-II-1)	-8(8-II-1)
7	19	8.50(9-I-1)	-1.57(8-II-1)	-2.20(9-I-1)	-592(8-II-1)	22(8-I-1)	-21(8-I-1)
7	20	7.24(9-I-1)	-2.58(9-II-1)	-2.19(9-I-1)	-277(8-II-1)	28(8-II-1)	-22(8-II-1)
7	21	-2.91(9-II-1)	-1.07(9-I-1)	-2.68(9-I-1)	-228(8-II-1)	28(8-II-1)	-24(8-II-1)
7	22	-7.12(9-II-1)	-2.97(9-II-1)	-2.66(9-I-1)	-312(8-II-1)	20(8-II-1)	-21(8-I-1)
7	23	-4.25(9-II-1)	-1.42(9-I-1)	-2.83(9-I-1)	-150(8-II-1)	22(8-II-1)	-23(8-II-1)
7	24	-2.57(9-II-1)	-0.58(8-II-1)	-3.11(9-I-1)	-181(8-II-1)	6(8-I-1)	-16(8-I-1)
7	25	-0.48(9-II-4)	-0.91(9-II-1)	-2.72(9-I-1)	-349(8-I-1)	37(8-I-1)	-6(8-II-1)
7	26	-1.10(9-I-1)	-1.14(9-II-1)	-2.85(9-I-1)	-211(8-I-1)	64(8-I-1)	-3(8-II-1)
7	27	-0.96(9-I-1)	-1.16(9-II-1)	-2.73(9-I-1)	-206(8-I-1)	75(8-I-1)	-2(8-I-1)
7	28	-1.68(9-II-1)	-1.53(9-II-1)	-2.83(9-I-1)	-232(8-II-1)	24(8-II-1)	-13(8-II-1)
7	29	-1.01(9-I-1)	-0.88(9-II-1)	-2.95(9-I-1)	-191(8-I-1)	44(8-II-1)	-9(8-II-1)
7	30	-1.14(9-I-1)	-1.28(9-II-1)	-2.81(9-I-1)	-193(8-I-1)	61(8-I-1)	-8(8-II-1)
7	31	-1.71(9-I-1)	-0.93(9-II-1)	-2.69(9-I-1)	-111(8-I-1)	82(8-I-1)	-4(8-II-1)
7	32	-0.41(8-II-1)	-1.22(9-II-1)	-3.11(9-I-1)	-140(8-II-1)	16(8-II-1)	15(8-II-1)
7	33	-1.88(9-II-1)	-1.40(9-II-1)	-3.03(9-I-1)	-150(8-II-1)	11(8-II-1)	-15(8-I-1)
7	34	-1.13(9-I-1)	-0.93(9-II-1)	-3.06(9-I-1)	-105(8-II-1)	24(8-II-1)	-14(8-II-1)
7	35	-1.26(9-I-1)	-1.02(9-II-1)	3.07(9-II-1)	-107(8-II-1)	7(8-II-1)	-13(8-I-1)
7	36	-1.56(9-I-1)	-1.41(9-II-1)	2.87(9-II-1)	-107(8-II-1)	39(8-II-1)	-12(8-II-1)
7	37	-2.15(9-I-1)	-1.26(9-II-1)	2.73(9-II-1)	-89(8-I-1)	59(8-II-1)	-9(8-II-1)
7	38	-3.60(9-I-1)	-0.87(9-II-1)	2.86(9-II-1)	-83(8-II-1)	20(8-II-1)	-13(8-I-1)
7	39	-2.72(9-I-1)	-1.61(9-II-1)	2.77(9-II-1)	49(8-I-1)	26(8-II-1)	-11(8-I-1)
7	40	-2.47(9-I-1)	-1.92(9-II-1)	2.59(9-II-1)	62(9-II-1)	7(9-I-1)	-11(8-I-1)
7	41	1.16(9-II-1)	-0.94(9-II-1)	-2.54(9-I-1)	-52(8-I-1)	74(8-I-1)	-10(8-I-1)
7	42	-0.18(9-I-4)	-1.76(9-II-1)	-2.49(9-I-1)	-80(9-II-1)	44(8-I-1)	-13(8-I-1)
7	43	-0.76(9-I-1)	-1.44(9-II-1)	-2.13(9-I-1)	-66(9-II-1)	34(8-I-1)	-11(8-I-1)
7	44	0.11(8-I-1)	-3.04(9-II-1)	-1.73(9-I-1)	-58(9-II-1)	6(9-I-1)	-8(8-I-1)
7	45	0.01(9-I-1)	-2.64(9-II-1)	-1.90(9-I-1)	-32(8-I-1)	32(8-I-1)	-7(8-I-1)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
7	46	0.36(9-II-1)	-4.04(9-II-1)	-1.61(9-I-1)	-14(9-II-2)	-2(9-II-1)	5(8-II-1)
7	47	-0.17(9-I-4)	-1.47(9-II-1)	-2.32(9-I-1)	-47(9-II-1)	60(8-I-1)	-8(8-I-1)
7	48	0.87(9-II-1)	-1.12(9-II-1)	-2.17(9-I-1)	-27(9-II-1)	34(8-I-1)	-6(8-I-1)
7	49	-1.00(9-I-1)	-1.16(9-II-1)	-2.40(9-I-1)	-97(8-I-1)	75(8-I-1)	-3(8-I-1)
7	50	1.04(9-II-1)	-0.89(9-II-1)	-2.30(9-I-1)	-33(8-I-1)	76(8-I-1)	-5(8-I-1)
7	51	-0.25(9-II-1)	-1.74(9-II-1)	-2.08(9-I-1)	-19(9-II-1)	44(8-I-1)	4(8-II-1)
7	52	-0.51(9-I-1)	-1.19(9-II-1)	-2.14(9-I-1)	-29(8-I-1)	56(8-I-1)	4(8-II-1)
7	53	0.32(9-II-1)	-1.01(9-II-1)	-2.07(9-I-1)	-14(9-II-1)	47(8-I-1)	3(8-II-1)
7	54	0.10(8-I-1)	-1.68(9-II-1)	-1.94(9-I-1)	-10(9-II-1)	22(8-I-1)	3(8-II-1)
7	55	0.28(9-I-1)	-3.03(9-II-1)	-1.73(9-I-1)	-10(8-II-1)	22(8-I-1)	3(8-II-1)
7	56	0.28(9-II-1)	-4.82(9-II-1)	-1.54(9-I-1)	-7(8-II-1)	9(9-I-1)	2(8-II-1)
7	57	0.56(9-I-1)	-4.69(9-II-1)	-1.63(9-I-1)	-10(9-I-1)	21(8-I-1)	0
7	58	0.22(9-I-1)	-5.18(9-II-1)	-1.19(9-I-1)	0	24(9-I-1)	0
7	59	0.08(8-I-1)	-1.24(9-II-1)	-1.94(9-I-1)	13(9-I-1)	37(8-I-1)	2(8-II-1)
7	60	0.22(9-I-1)	-1.64(9-II-1)	-1.86(9-I-1)	6(8-I-1)	33(8-I-1)	2(8-II-1)
7	61	0.18(9-I-1)	-1.09(9-II-1)	-1.84(9-I-1)	5(9-I-1)	42(8-I-1)	1(8-II-1)
7	62	0.20(9-I-1)	-2.01(9-II-1)	-1.79(9-I-1)	3(9-I-1)	25(8-I-1)	0
7	63	0.24(9-I-1)	-0.77(9-II-1)	-1.26(9-I-1)	0	22(8-I-1)	0
7	64	0.06(8-I-1)	-1.27(9-II-1)	-1.74(9-I-1)	5(9-I-1)	29(8-I-1)	0
7	65	0.16(9-I-1)	-0.98(9-II-1)	-1.19(9-I-1)	0	27(8-I-1)	0
7	66	-1.47(9-I-1)	-1.17(9-II-1)	2.42(9-II-1)	-112(8-I-1)	71(8-I-1)	-3(8-II-1)
7	67	1.25(9-II-1)	-1.01(9-II-1)	-2.32(9-I-1)	-45(8-I-1)	83(8-I-1)	-1(8-II-1)
7	68	-2.02(9-I-1)	-1.30(9-II-1)	2.43(9-II-1)	-91(8-I-1)	55(8-I-1)	-7(8-II-1)
7	69	1.54(9-II-1)	-1.21(9-II-1)	2.32(9-II-1)	-46(8-I-1)	71(8-I-1)	-3(8-II-1)
7	70	-0.96(9-I-1)	-1.12(9-II-1)	-2.14(9-I-1)	-45(8-I-1)	62(8-I-1)	1(8-I-1)
7	71	0.54(9-II-1)	-1.00(9-II-1)	-2.07(9-I-1)	-13(9-II-1)	64(8-I-1)	2(8-II-1)
7	72	-0.26(9-I-4)	-1.10(9-II-1)	-1.92(9-I-1)	-13(9-II-1)	45(8-I-1)	2(8-II-1)
7	73	1.33(9-II-1)	-1.19(9-II-1)	2.13(9-II-1)	-47(8-I-1)	56(8-I-1)	2(8-I-1)
7	74	0.75(9-II-1)	-1.14(9-II-1)	2.05(9-II-1)	-13(8-II-1)	64(8-I-1)	1(9-II-1)
7	75	3.94(9-II-1)	-0.75(9-II-1)	2.37(9-II-1)	65(9-II-1)	27(8-II-1)	-10(8-II-1)
7	76	-2.58(9-I-1)	-1.88(9-II-1)	2.42(9-II-1)	52(8-I-1)	26(8-II-1)	-9(8-II-1)
7	77	2.00(9-II-1)	-1.35(9-II-1)	2.30(9-II-1)	-34(8-I-1)	47(8-II-1)	-6(8-II-1)
7	78	1.81(9-II-1)	-1.68(9-II-1)	2.08(9-II-1)	45(9-II-1)	5(9-I-1)	-7(8-II-1)
7	79	1.69(9-II-1)	-1.29(9-II-1)	2.10(9-II-1)	-38(8-I-1)	40(8-I-1)	4(8-I-1)
7	80	0.97(9-II-1)	-1.32(9-II-1)	2.03(9-II-1)	-13(8-I-1)	53(8-I-1)	2(8-II-1)
7	81	-2.23(9-I-1)	-1.12(8-II-1)	2.07(9-II-1)	40(9-II-1)	21(8-II-1)	-6(8-II-1)
7	82	1.36(9-II-1)	-1.61(9-II-1)	2.00(9-II-1)	14(8-II-1)	30(8-I-1)	4(8-II-1)
7	83	-1.12(9-I-1)	-1.97(9-II-1)	1.86(9-II-1)	28(9-II-1)	5(9-I-1)	-5(8-II-1)
7	84	0.55(9-II-1)	-1.14(9-II-1)	1.91(9-II-1)	-13(8-II-1)	47(8-I-1)	1(9-II-1)
7	85	0.17(9-II-1)	-1.09(9-II-1)	1.82(9-II-1)	-4(9-II-1)	48(8-I-1)	1(8-II-1)
7	86	0.80(9-II-1)	-1.17(9-II-1)	1.90(9-II-1)	-14(8-I-1)	41(8-I-1)	1(8-II-1)
7	87	0.44(9-II-1)	-1.26(9-II-1)	1.81(9-II-1)	-3(9-II-1)	46(8-I-1)	1(9-II-1)
7	88	0.08(9-II-4)	-1.16(9-II-1)	1.73(9-II-1)	-4(9-II-1)	33(8-I-1)	0
7	89	0.11(9-I-1)	-1.01(9-II-1)	1.16(9-II-1)	0	31(8-I-1)	0
7	90	0.12(9-II-4)	-1.21(9-II-1)	1.72(9-II-1)	-3(9-II-1)	36(8-I-1)	0
7	91	0.08(9-I-1)	-1.12(9-II-1)	1.16(9-II-1)	0	35(8-I-1)	0
7	92	-1.29(9-I-1)	-1.03(8-II-1)	1.86(9-II-1)	20(9-II-1)	28(8-I-1)	-3(8-II-1)
7	93	1.00(9-II-1)	-1.78(9-II-1)	1.89(9-II-1)	18(8-II-1)	24(8-I-1)	2(8-II-1)
7	94	0.55(9-II-1)	-1.28(9-II-1)	1.78(9-II-1)	-1(8-II-1)	36(8-I-1)	1(9-II-1)
7	95	-0.45(9-I-1)	-2.33(9-II-1)	1.68(9-II-1)	15(8-II-1)	8(9-I-1)	-2(8-II-1)
7	96	0.31(9-II-1)	-0.79(9-II-1)	1.71(9-II-1)	-3(8-II-1)	38(8-I-1)	1(9-II-1)
7	97	0.05(9-I-1)	-1.51(9-II-1)	1.16(9-II-1)	0	37(8-I-1)	0
7	98	0.53(9-II-1)	-1.54(8-II-1)	1.66(9-II-1)	9(8-II-1)	-38(8-II-1)	0
7	99	-0.05(8-II-1)	-2.96(9-II-1)	1.18(9-II-1)	0	-40(8-II-1)	0
7	100	-0.09(8-II-1)	-4.56(9-II-1)	1.09(9-II-1)	0	-26(8-II-1)	0
8	1	-2.56(9-I-2)	2.85(9-I-2)	-1.96(9-I-2)	505(8-I-2)	-16(8-II-2)	17(8-II-2)
8	2	0.95(8-I-2)	-2.45(9-II-2)	-1.66(9-I-2)	434(8-II-2)	23(8-I-2)	-15(8-I-2)
8	3	2.31(9-II-2)	-2.68(9-I-2)	-1.97(9-I-2)	152(8-I-1)	25(8-I-2)	-19(8-I-2)
8	4	-3.20(9-II-2)	-3.76(9-II-2)	-2.85(9-I-2)	91(8-II-1)	-40(8-II-2)	21(8-II-2)
8	5	0.86(9-II-2)	-1.90(9-I-2)	-2.74(9-I-2)	221(8-I-2)	-39(8-II-2)	20(8-II-2)
8	6	-2.12(9-II-2)	-3.40(9-II-2)	-3.05(9-I-2)	117(8-I-2)	-3(8-II-2)	11(8-II-2)
8	7	2.24(9-I-2)	-4.21(9-I-2)	-2.34(9-I-2)	170(8-II-2)	26(8-I-2)	-9(8-I-2)
8	8	-4.92(9-II-2)	-1.58(9-II-2)	-3.54(9-I-2)	124(8-II-2)	-58(8-II-2)	-12(8-I-2)
8	9	0.66(9-II-2)	-1.98(9-I-2)	-3.71(9-I-2)	98(8-I-2)	-61(8-II-2)	15(8-II-2)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
8	10	-7.75(9-II-2)	-1.49(9-I-3)	-0.70(9-I-2)	-668(8-II-2)	25(8-I-2)	-27(8-I-2)
8	11	7.23(9-I-2)	-0.81(2)	-1.22(9-I-2)	-299(8-II-2)	41(8-II-2)	-29(8-II-2)
8	12	-3.89(9-II-2)	-3.03(9-I-2)	-1.80(9-I-2)	-387(8-II-2)	58(8-II-2)	-23(8-II-2)
8	13	-2.17(9-II-2)	-0.69(2)	-2.64(9-I-2)	-438(8-I-2)	42(8-II-2)	-28(8-II-2)
8	14	3.50(9-I-2)	-6.57(9-II-2)	2.20(9-II-2)	594(8-II-2)	-14(8-I-2)	-10(8-II-2)
8	15	2.57(9-I-2)	-1.06(9-I-2)	1.47(9-II-2)	563(8-II-2)	-9(8-I-2)	-8(8-II-2)
8	16	8.56(9-I-2)	-2.69(9-II-2)	1.98(9-II-2)	303(8-II-2)	24(8-I-2)	-7(8-II-2)
8	17	2.58(9-I-2)	0.32(2)	-3.03(9-I-2)	-313(8-II-2)	-17(8-I-2)	-12(8-II-2)
8	18	9.64(9-I-2)	-2.02(9-II-2)	3.54(9-II-2)	416(8-II-2)	9(8-II-2)	-14(8-II-2)
8	19	-3.93(9-II-2)	-6.87(9-II-2)	3.49(9-II-2)	118(8-II-2)	51(8-I-2)	-9(8-II-2)
8	20	3.48(9-I-2)	-1.20(8-I-3)	-0.87(9-I-2)	-169(8-II-2)	-6(8-II-1)	-24(8-I-2)
8	21	-0.94(8-II-2)	-5.98(9-I-2)	-1.44(9-I-2)	-292(8-II-2)	28(8-II-2)	-18(8-I-2)
8	22	-2.59(9-II-2)	-0.70(9-I-2)	-2.88(9-I-2)	-160(8-II-2)	20(8-II-2)	16(8-I-2)
8	23	-3.50(9-I-2)	-4.47(9-I-2)	-1.90(9-I-2)	-173(8-II-2)	8(9-I-2)	-22(8-I-2)
8	24	-0.79(9-I-2)	-10.89(9-I-2)	-2.54(9-I-2)	-36(8-II-2)	-50(8-I-2)	-20(8-II-2)
8	25	-0.79(9-II-2)	-1.85(9-I-1)	-2.97(9-I-2)	-8(8-II-2)	4(9-I-2)	-12(8-II-2)
8	26	-1.56(9-II-2)	-2.06(9-II-2)	-4.01(9-I-2)	42(8-I-1)	-31(8-II-2)	10(8-II-2)
8	27	0.30(9-II-1)	-1.43(9-II-2)	-3.60(9-I-2)	77(8-I-2)	-30(8-II-2)	10(8-II-2)
8	28	0.39(9-II-2)	-4.34(9-II-2)	-3.37(9-I-2)	52(8-I-2)	-6(9-I-2)	7(8-II-2)
8	29	0.70(9-I-2)	-4.27(9-II-2)	-3.63(9-I-2)	51(8-I-2)	-18(8-II-2)	6(8-II-2)
8	30	-1.16(9-I-2)	-6.59(9-II-2)	-3.50(9-I-2)	41(9-I-2)	-1(9-I-2)	4(8-II-1)
8	31	0.16(9-II-2)	-0.66(2)	-4.18(9-I-2)	32(8-I-2)	-56(8-II-2)	8(8-II-2)
8	32	0.49(9-II-2)	-1.24(9-I-2)	3.27(9-II-2)	24(8-I-2)	71(8-I-2)	-5(8-I-2)
8	33	-0.18(9-II-2)	-1.98(9-I-2)	-3.85(9-I-2)	29(8-I-1)	69(8-I-2)	-8(8-I-2)
8	34	0.59(9-I-2)	-0.76(2)	-4.03(9-I-2)	18(8-I-2)	-56(8-II-2)	8(8-II-2)
8	35	-0.44(9-I-2)	-1.16(9-I-2)	-4.01(9-I-2)	23(8-I-2)	-48(8-II-2)	8(8-II-2)
8	36	-0.12(9-I-1)	-0.74(2)	-4.14(9-I-2)	32(8-I-2)	-48(8-II-2)	8(8-II-2)
8	37	0.57(9-II-2)	-1.44(9-II-2)	-4.13(9-I-2)	17(8-I-2)	-22(8-II-2)	5(8-II-2)
8	38	1.69(9-I-2)	-1.30(9-I-2)	-3.86(9-I-2)	8(8-I-2)	-60(8-II-2)	6(8-II-2)
8	39	1.19(9-I-2)	-8.31(9-II-2)	-3.34(9-I-2)	45(9-I-2)	-13(9-I-2)	3(8-II-1)
8	40	-0.52(9-II-2)	-2.44(9-II-2)	-4.05(9-I-2)	27(8-I-2)	-24(8-II-2)	4(8-II-2)
8	41	1.13(9-II-2)	-4.14(9-II-2)	-3.56(9-I-2)	22(9-I-2)	-11(8-II-1)	2(8-II-2)
8	42	1.33(9-I-2)	-6.58(9-II-2)	-3.43(9-I-2)	23(9-I-2)	-21(9-I-2)	1(8-II-1)
8	43	0.65(9-I-2)	-7.11(9-II-2)	-2.44(9-I-2)	0	-28(9-I-2)	1(9-I-2)
8	44	-1.72(9-I-2)	-4.41(9-I-2)	-3.80(9-I-2)	15(8-I-2)	-44(8-II-2)	5(8-II-2)
8	45	0.57(9-I-2)	-0.88(9-I-2)	-3.87(9-I-2)	-6(9-II-2)	-31(8-II-2)	3(8-II-2)
8	46	-0.53(9-I-2)	-2.09(9-I-2)	-3.64(9-I-2)	-10(8-II-2)	-25(8-II-2)	2(8-II-2)
8	47	0.36(9-I-2)	-0.99(9-II-2)	-2.55(9-I-2)	0	-19(8-II-2)	0
8	48	0.35(9-II-2)	-1.15(2)	-2.54(9-I-2)	0	-33(8-II-2)	0
8	49	2.33(9-I-2)	-1.97(9-II-2)	2.89(9-II-2)	3(8-I-1)	58(8-I-2)	-6(8-I-2)
8	50	-1.90(9-I-2)	-5.27(9-I-2)	3.08(9-II-2)	3(8-I-1)	-58(8-II-2)	6(8-II-2)
8	51	1.14(9-I-2)	-3.17(9-I-2)	2.64(9-II-2)	-3(8-I-2)	61(8-I-2)	6(8-II-2)
8	52	1.09(9-II-2)	-5.95(9-I-2)	-2.80(9-I-2)	-7(8-I-2)	-45(8-II-2)	-8(8-II-2)
8	53	-1.07(9-II-2)	-1.94(8-I-1)	-3.05(9-I-2)	-2(8-II-2)	0	-6(8-II-2)
8	54	1.10(9-II-2)	-2.14(8-I-1)	2.88(9-II-2)	-2(9-I-1)	-24(8-II-2)	4(8-I-2)
8	55	-1.07(9-II-2)	-2.81(8-I-3)	3.01(9-II-2)	-2(8-I-2)	-4(9-I-2)	3(8-I-2)
8	56	1.41(9-II-2)	-9.39(9-I-2)	2.57(9-II-2)	-7(8-II-2)	-59(8-II-2)	4(8-II-2)
8	57	0.61(9-I-2)	-5.09(9-I-2)	-3.14(9-I-2)	0	-51(8-II-2)	4(8-II-2)
8	58	0.15(9-II-2)	-11.79(9-I-2)	2.57(9-II-2)	-9(8-II-2)	-50(8-II-2)	3(8-II-2)
8	59	-0.62(9-I-2)	-9.98(9-I-2)	3.07(9-II-2)	1(8-II-2)	-35(8-II-2)	2(8-II-2)
8	60	0.52(9-II-2)	-16.33(9-I-2)	2.26(9-II-2)	0	-46(8-II-2)	0
8	61	1.20(9-II-2)	-6.99(9-II-2)	2.90(9-II-2)	-4(9-I-1)	-12(8-II-2)	3(8-I-2)
8	62	-1.08(9-II-2)	-4.44(8-I-3)	2.89(9-II-2)	-3(8-I-1)	8(8-I-3)	2(8-I-2)
8	63	1.48(9-II-2)	-12.51(9-II-2)	2.72(9-II-2)	3(8-II-1)	13(8-I-1)	2(9-I-2)
8	64	-1.36(9-II-2)	-7.82(9-II-2)	2.53(9-II-2)	3(8-II-1)	23(8-I-1)	2(9-I-2)
8	65	-0.17(8-I-1)	-17.10(9-II-2)	2.00(9-II-2)	0	37(8-I-1)	1(9-I-2)
8	1	-0.06(9-II-4)	-0.71(9-II-1)	-1.27(8-I-3)	76(9-II-1)	598(9-II-1)	57(2)
8	2	-0.07(9-II-4)	-0.59(8-I-4)	-1.31(8-I-3)	35(2)	-107(2)	66(2)
8	3	-0.07(9-II-1)	-0.48(8-I-4)	-1.30(8-I-3)	53(2)	-134(2)	23(9-II-1)
8	4	-0.06(9-II-1)	-0.34(8-I-4)	-1.30(8-I-3)	43(2)	-78(2)	-83(2)
8	5	-0.09(1)	-0.70(9-II-1)	-1.19(8-I-4)	74(9-II-1)	592(9-II-1)	42(2)
8	6	-0.09(9-II-1)	-0.59(9-II-1)	-1.23(8-I-4)	-92(2)	-289(2)	53(2)
8	7	-0.05(2)	-0.47(9-II-1)	-1.23(8-I-4)	-92(2)	-354(2)	15(8-II-1)
8	8	-0.05(9-II-2)	-0.35(8-I-4)	-1.21(8-I-4)	-27(2)	-132(2)	-38(2)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
8	9	-0.08(2)	-0.73(9-II-4)	-1.10(8-I-4)	65(9-II-4)	559(9-II-4)	-53(2)
8	10	-0.05(1)	-0.58(9-II-1)	-1.13(8-I-4)	-116(2)	-287(2)	-11(2)
8	11	-0.05(8-I-4)	-0.47(9-II-1)	-1.14(8-I-4)	-141(2)	-320(2)	47(2)
8	12	-0.04(8-I-4)	-0.39(9-II-1)	-1.11(8-I-4)	-76(2)	-90(1)	82(2)
8	13	-0.11(9-II-1)	-0.69(9-II-4)	-1.03(8-I-4)	64(1)	431(9-II-4)	-62(2)
8	14	-0.09(9-II-1)	-0.54(9-II-4)	-1.04(8-I-4)	71(2)	-106(2)	-67(1)
8	15	-0.05(9-II-1)	-0.42(9-II-4)	-1.02(8-I-4)	52(2)	-83(2)	66(2)
8	16	-0.02(1)	-0.36(9-II-1)	-0.98(8-I-4)	13(2)	-24(1)	74(2)
9	1	9.30(9-I-4)	-0.90(9-I-1)	1.93(9-II-1)	1111(8-II-1)	-63(8-I-1)	19(8-I-1)
9	2	-9.43(9-II-4)	-0.54(9-I-1)	-1.83(9-I-1)	878(8-II-1)	-63(8-I-1)	32(8-I-1)
9	3	-8.56(9-II-1)	-1.29(9-II-1)	-2.18(9-I-1)	623(8-II-1)	-56(8-I-1)	26(8-I-1)
9	4	-9.81(9-II-1)	-0.48(9-I-1)	-1.82(9-I-1)	519(8-II-1)	-52(8-I-1)	39(8-I-1)
9	5	-8.07(9-II-1)	-1.02(9-II-1)	-2.19(9-I-1)	459(8-II-1)	-53(8-I-1)	38(8-I-1)
9	6	-9.96(9-II-1)	-0.51(2)	-1.78(9-I-1)	135(8-II-1)	-40(8-I-4)	39(8-I-1)
9	7	-7.79(9-II-1)	-0.84(9-II-1)	-2.14(9-I-1)	215(8-II-1)	-47(8-I-1)	42(8-I-1)
9	8	-9.82(9-II-1)	-0.61(2)	-1.70(9-I-1)	445(8-I-1)	-29(8-I-4)	31(8-I-1)
9	9	-7.55(9-II-1)	-0.71(9-II-1)	-2.04(9-I-1)	100(8-I-1)	-40(8-I-4)	39(8-I-1)
9	10	-11.41(9-II-1)	-1.62(9-I-1)	-0.97(9-I-1)	1520(8-I-1)	-13(8-I-2)	19(8-II-1)
9	11	5.81(9-I-1)	-1.00(9-I-1)	-1.08(9-I-1)	774(8-I-1)	-24(8-I-2)	9(8-I-4)
9	12	-9.56(9-II-1)	-1.30(9-I-1)	-1.51(9-I-1)	936(8-I-1)	-23(8-I-2)	15(8-I-4)
9	13	-7.11(9-II-1)	0.53(9-I-1)	-1.84(9-I-1)	400(8-I-1)	-35(8-I-4)	27(8-I-1)
9	14	8.36(9-I-1)	-2.07(2)	-0.51(9-I-1)	594(8-I-1)	-6(8-I-2)	4(9-I-1)
9	15	10.91(9-I-1)	-5.73(9-II-1)	1.82(9-II-1)	872(8-II-1)	-13(8-II-1)	21(8-II-1)
9	16	10.54(9-I-1)	-2.80(9-I-1)	1.46(9-II-1)	-493(8-I-1)	-14(8-I-1)	29(8-II-1)
9	17	9.36(9-I-1)	-1.12(9-II-1)	2.13(9-II-1)	1042(8-II-1)	-28(8-I-1)	8(8-II-4)
9	18	-19.12(9-II-1)	-0.44(9-II-4)	2.95(9-II-1)	466(8-II-1)	-18(8-I-1)	18(8-II-4)
9	19	8.48(9-I-1)	-0.32(9-II-1)	2.16(9-II-1)	692(8-II-1)	-24(8-I-1)	6(8-II-1)
9	20	15.24(9-I-1)	-0.41(9-II-1)	2.36(9-II-1)	622(8-II-1)	-22(8-I-1)	6(8-II-1)
9	21	8.44(9-I-4)	-3.10(9-II-1)	-1.91(9-I-1)	-926(8-II-1)	22(8-I-1)	-35(8-I-1)
9	22	12.93(9-I-1)	-1.47(9-II-1)	2.24(9-II-1)	99(8-II-1)	76(8-I-1)	46(8-II-1)
9	23	9.43(9-I-1)	-2.07(9-I-1)	-1.59(9-I-1)	-170(8-II-1)	80(8-I-1)	43(8-II-1)
9	24	-7.52(9-II-1)	-0.80(9-I-4)	-2.41(9-I-1)	-300(8-II-1)	68(8-I-1)	-44(8-I-1)
9	25	8.29(9-I-1)	0.19(2)	-1.80(9-I-1)	654(8-II-1)	-13(8-I-1)	15(8-I-1)
9	26	15.84(9-I-1)	-0.31(2)	1.78(9-II-1)	557(8-II-1)	-5(8-II-1)	11(8-I-1)
9	27	7.88(9-I-1)	0.29(9-I-1)	-1.68(9-I-1)	506(8-II-1)	-7(8-I-1)	22(8-I-1)
9	28	11.49(9-I-1)	-0.34(2)	-1.48(9-I-1)	475(8-II-1)	-2(8-II-4)	20(8-I-1)
9	29	7.06(9-I-1)	0.36(9-I-1)	-1.60(9-I-1)	266(8-II-1)	-6(8-I-1)	24(8-I-1)
9	30	8.07(9-I-1)	-0.37(2)	-1.33(9-I-1)	316(8-II-1)	-4(8-I-1)	25(8-I-1)
9	31	6.25(9-I-1)	0.34(9-I-1)	-1.52(9-I-1)	69(8-II-1)	-7(8-I-1)	22(8-I-1)
9	32	5.28(9-I-1)	-0.38(2)	-1.24(9-I-1)	113(8-II-1)	-10(8-I-1)	25(8-I-1)
9	33	-6.10(9-II-1)	0.21(9-I-1)	-1.35(9-I-1)	330(8-I-1)	-13(8-I-1)	14(8-I-4)
9	34	-3.79(9-II-4)	-0.43(2)	-1.20(9-I-1)	149(8-I-1)	-20(8-I-1)	18(8-I-1)
9	35	-5.50(9-II-1)	-3.75(2)	3.36(9-II-1)	-93(8-II-4)	174(8-I-1)	32(8-II-1)
9	36	-5.77(9-II-1)	-1.35(9-II-1)	3.07(9-II-1)	-238(8-II-1)	56(8-I-1)	-25(8-I-1)
9	37	-0.86(9-II-1)	-1.21(9-II-1)	3.17(9-II-1)	-164(8-II-1)	6(8-I-1)	-16(8-I-1)
9	38	0.27(2)	-1.80(9-I-1)	3.12(9-II-1)	-25(8-II-1)	101(8-I-1)	-26(8-I-1)
9	39	-0.41(8-II-1)	-0.84(8-II-1)	3.32(9-II-1)	74(8-I-4)	98(8-I-1)	-24(8-I-1)
9	40	-4.93(9-II-1)	-5.29(9-I-1)	-0.60(2)	515(8-I-1)	-39(8-I-4)	8(8-I-4)
9	41	-3.28(9-II-4)	-1.99(9-I-1)	-1.52(9-I-1)	426(8-I-1)	40(8-II-1)	9(8-I-4)
9	42	-4.16(9-II-1)	-4.13(9-I-1)	-0.51(2)	321(8-I-1)	-13(9-I-1)	12(8-I-4)
9	43	-3.19(2)	-7.08(9-I-1)	-2.97(9-I-1)	309(8-I-1)	26(9-II-1)	17(8-I-1)
9	44	-2.15(9-I-1)	-9.66(9-I-1)	-3.57(9-I-1)	63(8-I-1)	29(8-I-1)	17(8-I-1)
9	45	-1.76(9-I-1)	-0.49(2)	3.03(9-II-1)	-145(8-II-1)	7(8-II-1)	-14(8-I-1)
9	46	-3.62(9-I-1)	-7.09(9-I-1)	3.13(9-II-1)	-29(8-II-4)	193(8-I-1)	22(8-II-1)
9	47	-4.74(9-I-1)	-0.75(2)	2.95(9-II-1)	-24(8-I-1)	41(8-I-1)	18(8-II-1)
9	48	-2.99(9-I-1)	-2.06(9-II-1)	2.89(9-II-1)	-50(8-II-1)	37(9-I-1)	13(8-II-1)
9	49	-8.75(9-I-1)	-2.62(9-I-1)	2.51(9-II-1)	-101(8-I-1)	85(8-I-1)	11(8-II-1)
9	50	-3.95(9-I-1)	-1.47(9-II-1)	2.60(9-II-1)	-35(9-II-1)	71(8-I-1)	15(8-II-1)
9	51	4.94(9-II-1)	-1.14(9-II-1)	2.34(9-II-1)	-40(8-I-1)	28(9-I-1)	9(8-II-1)
9	52	-4.22(9-I-1)	-1.00(8-II-1)	2.50(9-II-1)	-34(8-II-1)	7(9-I-1)	9(8-II-1)
9	53	-3.71(9-I-1)	-1.16(8-II-1)	1.87(9-II-1)	-28(8-I-1)	26(8-I-1)	6(8-II-1)
9	54	2.31(9-II-1)	-1.11(8-II-1)	1.85(9-II-1)	29(9-II-1)	5(9-I-1)	4(8-II-1)
9	55	4.23(9-II-1)	-2.09(9-I-4)	1.78(9-II-1)	-35(8-II-1)	62(8-I-1)	7(8-II-1)
9	56	-2.56(9-I-1)	-1.12(8-II-4)	1.73(9-II-1)	24(8-I-1)	35(9-I-1)	4(8-II-1)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
9	57	9.04(9-II-1)	0.22(9-I-1)	-1.83(9-I-1)	70(8-II-1)	6(8-I-1)	2(9-I-1)
9	58	12.61(9-II-1)	-1.62(9-I-1)	-2.49(9-I-1)	107(8-II-1)	10(8-I-1)	10(8-I-1)
9	59	-4.38(9-I-1)	-6.10(9-I-1)	-2.06(9-I-1)	41(8-I-1)	84(8-I-1)	2(8-I-1)
9	60	5.73(9-II-1)	-0.23(9-II-1)	1.42(9-II-1)	42(8-I-1)	7(8-I-1)	3(8-I-1)
9	61	3.32(9-II-1)	-0.51(9-I-1)	-1.79(9-I-1)	37(8-II-1)	8(8-I-1)	2(9-I-1)
9	62	3.19(9-II-1)	-0.33(9-II-1)	1.31(9-II-1)	29(8-I-1)	3(8-I-2)	2(8-II-1)
9	63	2.80(9-II-1)	-0.39(9-I-1)	1.64(9-II-1)	29(8-I-1)	3(8-I-4)	2(8-II-1)
9	64	0.79(9-II-1)	-0.48(9-II-1)	1.33(9-II-1)	19(8-I-1)	2(8-I-2)	-2(8-I-1)
9	65	-2.43(9-I-1)	-0.39(9-I-1)	1.61(9-II-1)	22(8-I-1)	2(8-I-2)	2(8-II-1)
9	66	1.94(9-I-1)	-0.67(9-II-1)	1.48(9-II-1)	13(8-I-2)	1(9-I-1)	-2(8-I-1)
9	67	-2.09(9-I-1)	-0.34(9-I-1)	1.65(9-II-1)	15(8-I-1)	1(8-I-2)	-2(8-I-1)
9	68	-1.81(9-I-1)	0.63(9-II-1)	1.79(9-II-1)	10(8-I-3)	2(9-I-1)	-2(8-I-1)
9	69	2.12(9-I-1)	-3.84(2)	3.73(9-II-1)	-58(8-I-1)	-9(9-II-1)	8(8-I-1)
9	70	-1.04(9-II-3)	-11.72(9-II-1)	4.06(9-II-1)	44(9-II-1)	23(9-I-1)	-7(8-II-2)
9	71	-11.12(9-II-1)	-5.70(9-II-3)	2.61(9-II-1)	32(8-II-2)	22(9-I-1)	-6(8-II-2)
9	72	-1.33(9-II-1)	-7.35(9-II-1)	2.18(9-II-1)	36(9-II-3)	21(9-I-3)	-4(8-II-2)
9	73	-12.62(9-II-1)	-3.48(9-II-1)	2.88(9-II-1)	56(9-II-3)	6(8-II-1)	-2(8-II-1)
9	74	-6.65(9-II-1)	0.93(9-II-1)	2.23(9-II-1)	36(9-II-3)	0	-2(8-II-1)
9	75	-0.23(8-I-1)	-0.87(9-II-1)	1.92(9-II-1)	20(9-II-3)	2(9-I-2)	-2(8-I-1)
9	76	-1.97(9-I-1)	-4.15(9-II-3)	1.54(9-II-1)	41(9-II-3)	7(9-I-1)	-3(8-II-2)
9	77	-1.86(9-I-1)	-1.69(8-II-1)	1.73(9-II-1)	29(9-II-1)	6(9-I-1)	4(8-II-1)
9	78	2.27(9-II-1)	-1.78(8-II-4)	1.64(9-II-1)	21(8-I-1)	24(8-I-1)	3(8-II-1)
9	79	1.26(9-II-1)	-1.08(8-II-1)	1.66(9-II-1)	14(9-II-1)	18(9-I-1)	2(8-II-1)
9	80	1.51(9-II-1)	-2.72(9-I-1)	-2.01(9-I-1)	31(8-I-1)	27(8-I-1)	2(8-I-1)
9	81	-1.94(9-I-1)	-3.61(9-I-1)	-1.71(9-I-1)	15(9-I-1)	33(8-I-1)	2(8-I-1)
9	82	-3.01(9-I-1)	-1.08(9-I-1)	-2.02(9-I-1)	35(8-I-1)	18(8-I-4)	2(9-I-1)
9	83	1.86(9-II-1)	-1.88(9-I-1)	-2.01(9-I-1)	17(8-I-1)	24(8-I-1)	2(8-I-1)
9	84	-2.79(9-I-1)	-0.32(9-I-1)	1.89(9-II-1)	29(8-I-1)	12(8-I-2)	2(8-II-1)
9	85	1.81(9-II-1)	-0.16(9-I-1)	1.94(9-II-1)	18(8-I-1)	14(8-I-4)	2(8-II-1)
9	86	-2.52(9-I-1)	-0.07(9-I-1)	1.87(9-II-1)	22(8-I-1)	10(8-I-2)	2(8-II-1)
9	87	-2.03(9-I-1)	-0.08(9-I-1)	1.89(9-II-1)	-17(8-II-1)	10(8-I-2)	2(8-II-1)
9	88	-2.32(9-I-1)	-0.19(9-II-1)	1.88(9-II-1)	15(8-I-1)	9(8-I-2)	-2(8-I-1)
9	89	-2.31(9-I-1)	-0.10(9-II-1)	1.87(9-II-1)	-14(8-II-1)	9(8-I-2)	-2(8-I-1)
9	90	-3.21(9-I-1)	-2.94(9-II-1)	1.86(9-II-1)	25(9-II-3)	9(9-I-3)	-2(8-II-2)
9	91	-2.76(9-I-1)	-1.97(9-II-3)	2.15(9-II-1)	18(9-II-3)	6(9-I-1)	-2(8-I-1)
9	92	-3.32(9-I-1)	-0.36(9-II-1)	1.99(9-II-1)	-5(9-I-3)	5(9-I-2)	-3(8-I-1)
9	93	-2.19(9-I-1)	-0.70(9-II-1)	1.97(9-II-1)	10(8-I-3)	8(8-I-2)	-2(8-I-1)
9	94	-2.66(9-I-1)	-0.21(9-II-1)	1.89(9-II-1)	-9(8-II-1)	8(8-I-2)	-2(8-I-1)
9	95	-1.19(9-I-1)	-1.61(8-II-1)	1.58(9-II-1)	16(9-II-1)	11(9-I-1)	1(8-II-1)
9	96	0.62(9-II-1)	-2.05(8-II-1)	1.54(9-II-1)	25(9-II-1)	8(9-I-1)	1(8-II-1)
9	97	0.91(9-II-1)	-2.57(9-I-1)	-1.66(9-I-1)	14(9-I-1)	20(9-I-1)	2(8-I-1)
9	98	0.77(9-II-1)	-1.96(9-I-4)	1.54(9-II-1)	6(9-I-1)	17(9-I-1)	2(8-I-1)
9	99	-1.32(9-I-1)	-1.96(9-I-1)	-1.85(9-I-1)	17(8-I-1)	18(8-I-4)	2(8-I-1)
9	100	0.77(9-II-1)	-2.94(9-I-1)	-1.62(9-I-1)	10(9-I-1)	19(9-I-1)	-1(8-I-1)
9	101	0.39(9-II-1)	-1.99(9-II-1)	1.49(9-II-1)	24(9-II-1)	-32(8-II-1)	0
9	102	-0.09(8-II-1)	-3.48(8-II-1)	1.08(9-II-1)	0	-26(8-II-1)	0
9	103	0.31(9-II-4)	-1.74(8-II-4)	1.51(9-II-1)	6(9-I-1)	-27(8-II-1)	-2(8-II-1)
9	104	0.08(8-I-1)	-2.38(8-II-4)	1.06(9-II-1)	0	-33(8-II-1)	0
9	105	0.34(9-II-1)	-3.74(9-I-1)	-1.53(9-I-1)	9(9-I-1)	-21(8-II-1)	-1(8-II-1)
9	106	0.13(9-II-4)	-1.90(9-I-1)	1.09(9-II-1)	0	-22(8-II-1)	0
9	107	0.14(9-II-1)	-0.89(2)	1.09(9-II-1)	0	-20(8-II-2)	0
9	108	0.12(9-II-1)	-4.05(9-I-1)	1.10(9-II-1)	0	-20(8-II-2)	0
9	109	-1.87(9-I-1)	-0.63(9-I-1)	1.83(9-II-1)	18(8-I-1)	18(8-I-2)	1(8-II-1)
9	110	0.90(9-II-1)	-1.11(9-I-1)	1.69(9-II-1)	6(8-I-1)	19(8-I-4)	-1(8-I-2)
9	111	-0.80(9-I-1)	-0.48(2)	1.59(9-II-1)	-5(8-II-1)	-21(8-II-2)	0
9	112	-2.03(9-I-1)	-0.28(9-I-1)	1.76(9-II-1)	-17(8-II-1)	18(8-I-2)	2(8-II-1)
9	113	0.84(9-II-1)	-0.23(9-I-1)	1.70(9-II-1)	-6(8-II-1)	18(8-I-2)	-1(8-I-1)
9	114	-2.19(9-I-1)	-0.09(2)	1.72(9-II-1)	-14(8-II-1)	18(8-I-2)	-2(8-I-1)
9	115	1.08(9-II-1)	-0.06(2)	1.66(9-II-1)	-7(8-II-1)	18(8-I-2)	-1(8-I-1)
9	116	-2.39(9-I-1)	-0.24(9-II-1)	1.70(9-II-1)	-10(8-II-1)	-19(8-II-2)	-2(8-I-1)
9	117	-1.28(9-I-1)	-0.21(9-II-1)	1.63(9-II-1)	-7(8-II-1)	-19(8-II-2)	-2(8-I-1)
9	118	-2.75(9-I-1)	-0.83(9-II-3)	1.74(9-II-1)	-5(9-I-3)	-19(8-II-2)	-2(8-I-1)
9	119	-1.49(9-I-1)	-0.51(9-II-1)	1.60(9-II-1)	-6(8-II-1)	-18(8-II-2)	-2(8-I-1)
9	120	-1.61(9-I-1)	-2.47(9-II-1)	1.51(9-II-1)	-1(8-I-1)	17(8-I-2)	-2(8-I-1)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
9	121	-1.11(9-I-1)	-0.28(9-I-1)	1.64(9-II-1)	-6(8-II-1)	-23(8-II-2)	0
9	122	0.12(9-II-3)	-1.44(9-I-1)	1.12(9-II-1)	0	-21(8-II-2)	0
9	123	-1.04(9-I-1)	-0.18(9-I-1)	1.60(9-II-1)	-7(8-II-1)	-27(8-II-2)	0
9	124	0.10(2)	-0.34(9-I-1)	1.09(9-II-1)	0	-25(8-II-2)	0
9	125	-1.04(9-I-1)	-0.11(8-II-4)	1.56(9-II-1)	-7(8-II-1)	-31(8-II-2)	-1(8-I-1)
9	126	0.06(8-II-1)	-0.12(9-II-1)	1.06(9-II-1)	0	-29(8-II-2)	0
9	127	-1.10(9-I-1)	-0.19(9-II-3)	1.53(9-II-1)	-6(8-II-1)	-36(8-II-2)	-1(8-I-1)
9	128	-0.05(8-I-4)	-0.47(9-II-1)	1.02(9-II-1)	0	-34(8-II-2)	0
9	129	1.44(9-II-1)	-0.80(8-II-2)	1.43(9-II-1)	-2(8-I-1)	-43(8-II-2)	-2(8-I-1)
9	130	-0.15(2)	-1.58(9-II-1)	0.98(9-II-1)	0	-39(8-II-2)	0
9	131	-2.99(9-I-1)	-3.81(9-II-3)	1.49(9-II-1)	28(8-II-1)	5(9-I-1)	-2(9-II-1)
9	132	4.30(9-II-1)	-2.41(8-II-2)	1.43(9-II-1)	32(8-II-1)	11(8-I-2)	-2(8-II-2)
9	133	-1.24(9-I-1)	-4.83(8-II-2)	1.09(9-II-1)	23(8-II-1)	8(8-I-2)	-2(8-II-2)
9	134	1.40(9-II-1)	-2.76(8-II-1)	1.20(9-II-1)	22(8-II-1)	-50(8-II-2)	0
9	135	-0.27(2)	-3.32(9-II-3)	0.89(9-II-1)	0	-52(8-II-2)	0
9	136	-0.36(2)	-6.54(8-II-2)	-0.79(9-I-1)	0	-38(8-II-2)	0
9	1	-0.08(2)	-0.65(2)	-0.97(8-I-4)	77(1)	373(8-II-1)	68(2)
9	2	-0.07(9-I-1)	-0.51(1)	-0.96(8-I-4)	92(2)	-116(1)	97(1)
9	3	-0.05(2)	-0.34(2)	-0.94(8-I-4)	107(2)	-95(1)	-55(2)
9	4	-0.04(8-I-3)	-0.16(2)	-0.93(8-I-4)	46(2)	-39(1)	-103(2)
9	5	-0.09(2)	-0.70(2)	-0.86(8-I-4)	37(8-II-1)	457(1)	66(9-II-1)
9	6	-0.06(2)	-0.53(2)	-0.89(8-I-4)	-144(2)	-305(2)	45(2)
9	7	-0.04(2)	-0.36(2)	-0.89(8-I-4)	-163(2)	-350(2)	-24(9-II-1)
9	8	-0.02(2)	-0.18(2)	-0.88(8-I-4)	-66(2)	-113(2)	-82(2)
9	9	-0.06(2)	-0.76(2)	-0.78(8-I-4)	42(9-I-1)	462(9-I-1)	-65(2)
9	10	-0.04(2)	-0.55(2)	-0.80(8-I-4)	-143(2)	-304(2)	-44(2)
9	11	-0.05(9-II-4)	-0.37(2)	-0.80(8-I-4)	-161(2)	-349(2)	24(2)
9	12	-0.02(2)	-0.19(2)	-0.79(8-I-4)	-65(2)	-113(2)	82(2)
9	13	0.23(9-I-1)	-0.86(9-I-1)	-0.71(8-I-3)	68(2)	373(9-I-1)	-67(2)
9	14	-0.14(9-I-1)	-0.41(2)	-0.68(8-I-3)	91(2)	-111(2)	-93(1)
9	15	-0.06(1)	-0.31(2)	-0.67(8-I-3)	105(2)	-100(2)	54(2)
9	16	-0.03(2)	-0.17(2)	-0.66(8-I-3)	46(2)	-38(2)	103(2)
10	1	-8.16(9-II-2)	-1.93(9-I-2)	-1.35(9-I-2)	-1141(8-I-2)	-43(8-I-2)	21(8-II-2)
10	2	-9.67(9-II-2)	-2.07(9-I-2)	-0.68(9-I-2)	-1402(8-I-2)	-81(8-I-2)	14(8-I-2)
10	3	-10.38(9-II-2)	-2.35(2)	0.66(9-II-2)	-1372(8-I-2)	-61(8-I-2)	28(8-I-2)
10	4	8.02(9-I-2)	-1.43(2)	-0.54(9-I-2)	-905(8-I-2)	-41(8-I-2)	20(8-I-2)
10	5	6.52(9-I-2)	-5.21(9-II-2)	2.19(9-II-2)	319(8-II-2)	98(8-I-2)	-68(8-I-2)
10	6	8.80(9-I-2)	-0.97(8-I-3)	1.45(9-II-2)	1081(8-I-2)	99(8-I-2)	73(8-II-2)
10	7	3.88(9-I-2)	-2.14(8-I-3)	0.93(9-II-2)	485(8-I-2)	25(8-I-2)	43(8-II-2)
10	8	5.00(9-I-3)	-2.82(9-II-2)	2.39(9-II-2)	783(8-II-2)	37(8-I-2)	51(8-II-2)
10	9	4.14(9-I-2)	-1.21(9-I-2)	3.04(9-II-2)	282(8-I-2)	49(8-I-2)	-64(8-I-2)
10	10	4.90(9-I-2)	-5.32(9-II-2)	2.98(9-II-2)	173(8-I-2)	-59(8-II-2)	-47(8-I-2)
10	11	4.06(9-I-2)	-4.58(9-II-2)	1.57(9-II-2)	472(8-I-2)	-60(8-II-2)	-40(8-I-2)
10	12	2.29(9-II-2)	-2.43(9-II-2)	1.01(9-II-2)	191(8-I-2)	-6(8-II-1)	28(8-II-2)
10	13	-1.85(9-II-2)	-2.15(9-II-2)	3.47(9-II-2)	198(8-I-2)	41(8-I-2)	-46(8-I-2)
10	14	5.57(9-I-2)	-3.10(9-I-2)	-1.90(9-I-2)	-919(8-I-2)	-46(8-II-2)	32(8-II-2)
10	15	-5.98(9-II-2)	-1.05(2)	-3.07(9-I-2)	294(8-II-2)	-54(8-II-2)	-41(8-I-2)
10	16	3.50(9-I-2)	0.73(9-II-2)	3.23(9-II-2)	327(8-II-2)	-12(8-I-2)	-27(8-I-2)
10	17	6.06(9-I-2)	-3.23(9-I-2)	-0.68(9-I-2)	-913(8-I-2)	-90(8-II-2)	13(8-I-2)
10	18	8.17(9-I-2)	-1.86(9-I-2)	-1.54(9-I-2)	362(8-II-2)	-132(8-II-2)	12(8-II-2)
10	19	2.03(9-I-2)	-6.88(9-I-2)	-2.17(9-I-2)	382(8-II-2)	-136(8-II-2)	-7(8-II-2)
10	20	6.97(9-II-2)	-2.48(9-I-2)	-3.38(9-I-2)	103(8-I-2)	-123(8-II-2)	-7(8-I-2)
10	21	6.30(9-II-2)	-4.18(9-I-2)	-2.12(9-I-2)	132(8-II-2)	-186(8-II-2)	-8(8-II-2)
10	22	9.20(9-I-2)	-3.33(9-II-2)	1.51(9-II-2)	-1173(8-I-2)	-52(8-I-2)	42(8-I-2)
10	23	4.79(9-I-3)	-1.82(2)	1.15(9-II-2)	-871(8-I-2)	-43(8-I-2)	37(8-I-2)
10	24	6.71(9-I-2)	-0.90(9-I-2)	2.00(9-II-2)	-783(8-I-2)	-67(8-I-2)	50(8-I-2)
10	25	-5.45(9-II-2)	-2.16(9-II-2)	2.51(9-II-2)	-639(8-I-2)	-49(8-I-2)	46(8-I-2)
10	26	-5.87(9-II-3)	-0.93(2)	-1.96(9-I-2)	-337(8-II-2)	-70(8-I-2)	50(8-I-2)
10	27	-5.64(9-II-2)	-1.49(9-II-2)	-2.41(9-I-2)	-322(8-I-2)	-66(8-I-2)	52(8-I-2)
10	28	-9.49(9-II-2)	2.36(2)	-1.23(9-I-2)	1348(8-I-2)	-68(2)	-28(8-II-2)
10	29	-8.47(9-II-2)	-0.94(9-I-2)	-1.73(9-I-2)	-589(8-II-2)	-74(8-I-2)	-50(8-II-2)
10	30	-18.05(2)	22.35(2)	2.41(2)	-2110(8-II-2)	-194(2)	26(8-II-2)
10	31	7.57(9-I-2)	9.21(2)	1.30(9-II-2)	-1040(8-II-2)	-88(8-I-2)	-18(8-II-2)
10	32	4.31(9-I-3)	-1.56(9-I-2)	-1.83(9-I-2)	-669(8-II-2)	-76(8-I-2)	-40(8-II-2)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
10	33	-5.63(9-II-2)	-1.31(9-II-2)	-2.39(9-I-2)	-173(8-II-2)	-75(8-I-2)	-49(8-II-2)
10	34	-5.41(9-II-3)	3.46(9-II-2)	0.91(9-II-2)	-1039(8-II-2)	-66(8-I-2)	-14(8-II-2)
10	35	7.90(9-I-2)	5.01(2)	-1.36(9-I-2)	-484(8-II-2)	-119(8-I-2)	-33(8-II-2)
10	36	5.62(9-I-2)	-1.17(9-I-2)	1.70(2)	-753(8-II-2)	-40(2)	-9(8-II-3)
10	37	8.92(9-I-2)	-7.00(9-II-2)	1.08(9-II-2)	-901(8-I-2)	-67(8-II-2)	31(8-I-2)
10	38	8.50(9-I-2)	-2.28(9-II-2)	0.83(9-II-2)	-575(8-I-2)	-110(8-II-2)	19(8-I-2)
10	39	7.84(9-I-2)	0.23(2)	2.16(9-II-2)	-695(8-I-2)	7(8-II-2)	29(8-I-2)
10	40	14.19(9-I-2)	-3.48(9-II-2)	2.38(9-II-2)	-846(8-I-2)	-47(8-II-2)	28(8-I-2)
10	41	6.59(9-I-2)	0.50(9-I-2)	-1.93(9-I-2)	-385(8-I-2)	-7(8-I-2)	31(8-I-2)
10	42	10.51(9-I-2)	-0.61(2)	-1.63(9-I-2)	-517(8-I-2)	-7(8-I-2)	32(8-I-2)
10	43	-4.64(9-II-2)	-9.15(9-II-2)	1.87(9-II-2)	-378(8-I-2)	-121(8-II-2)	35(8-I-2)
10	44	0.11(9-II-3)	-4.26(9-II-2)	1.81(9-II-2)	48(8-I-2)	-184(8-II-2)	-10(8-II-2)
10	45	-4.14(9-I-2)	-6.06(9-II-2)	2.45(9-II-2)	-65(8-I-2)	-113(8-II-2)	-4(8-II-2)
10	46	4.98(9-I-2)	0.37(9-I-2)	-1.88(9-I-2)	-174(8-II-2)	-16(8-I-2)	-27(8-II-2)
10	47	7.29(9-I-2)	-0.83(2)	-1.57(9-I-2)	-177(8-I-2)	-17(8-I-2)	-30(8-II-2)
10	48	-3.57(9-II-3)	3.61(2)	0.81(2)	-673(8-II-2)	-84(8-I-2)	-21(8-II-2)
10	49	-3.97(9-II-3)	-5.28(9-I-2)	-0.98(9-I-2)	-459(8-II-2)	-65(8-I-2)	-24(8-II-2)
10	50	4.65(9-I-3)	1.30(9-II-2)	-1.70(9-I-2)	-341(8-II-2)	-48(8-I-2)	-23(8-II-2)
10	51	4.76(9-I-2)	-2.99(9-I-2)	0.97(2)	-449(8-II-2)	-8(8-I-3)	-17(8-II-2)
10	52	-1.28(2)	-5.63(9-I-2)	1.11(9-II-2)	-460(8-II-2)	-31(8-I-2)	-34(8-II-2)
10	53	1.88(9-I-2)	-5.96(9-I-2)	1.42(9-II-2)	-89(8-II-2)	-5(8-I-3)	-18(8-II-2)
10	54	-2.53(9-II-2)	-3.01(9-I-2)	3.36(9-II-2)	-89(8-II-2)	-74(8-II-2)	17(8-I-2)
10	55	0.66(9-II-2)	-6.58(9-I-2)	4.21(9-II-2)	-33(8-II-2)	-9(9-II-2)	11(8-I-2)
10	56	-7.30(9-II-2)	-6.53(9-II-2)	2.06(9-II-2)	181(8-I-2)	8(9-I-2)	-26(8-I-2)
10	57	-1.20(9-II-2)	-13.91(9-II-2)	2.88(9-II-2)	26(8-I-2)	-102(8-II-2)	-21(8-I-2)
10	58	-0.79(9-I-2)	-3.34(9-II-2)	3.12(9-II-2)	-10(8-I-2)	4(9-I-2)	-11(8-I-2)
10	59	1.06(9-I-2)	-8.18(9-II-2)	2.91(9-II-2)	4(8-II-2)	44(8-I-2)	7(8-II-2)
10	60	-1.03(9-I-2)	-2.06(8-I-1)	3.16(9-II-2)	3(8-II-2)	0	5(8-II-2)
10	61	-1.08(9-II-2)	-2.44(8-I-3)	2.97(9-II-2)	3(8-II-2)	18(8-I-2)	3(8-II-2)
10	62	-4.11(9-I-2)	-11.54(9-I-2)	-4.29(9-I-2)	9(8-I-2)	-268(8-II-2)	-7(8-I-2)
10	63	-0.18(9-II-2)	-3.15(9-II-2)	4.33(9-II-2)	10(8-I-2)	-180(8-II-2)	-10(8-I-2)
10	64	0.10(2)	-2.82(2)	-4.40(9-I-2)	-6(8-I-2)	-183(8-II-2)	-13(8-I-2)
10	65	-0.12(9-II-2)	-3.52(9-I-2)	-3.78(9-I-2)	7(8-I-2)	-178(8-II-2)	-14(8-I-2)
10	66	0.56(9-I-2)	-4.09(9-II-2)	4.10(9-II-2)	-4(8-I-2)	-153(8-II-2)	-15(8-I-2)
10	67	-5.38(9-I-2)	-5.81(9-II-2)	2.67(9-II-2)	-51(8-I-2)	-111(8-II-2)	-11(8-I-2)
10	68	-1.04(9-I-2)	-2.38(8-I-1)	3.07(9-II-2)	2(8-II-3)	-4(9-I-2)	3(8-II-2)
10	69	-1.19(9-II-2)	-6.18(9-I-2)	2.96(9-II-2)	-4(8-I-3)	-7(8-II-2)	3(8-II-3)
10	70	-1.07(9-I-2)	-4.29(9-I-1)	2.93(9-II-2)	-3(8-I-1)	8(8-I-3)	3(8-II-3)
10	71	-1.53(9-II-2)	-12.04(9-I-2)	2.77(9-II-2)	-3(8-I-1)	-10(8-II-1)	3(8-II-3)
10	72	1.40(9-II-2)	-8.52(9-I-2)	2.56(9-II-2)	-3(8-I-1)	23(8-I-1)	3(8-II-3)
10	73	0.24(9-II-1)	-16.95(9-I-2)	2.03(9-II-2)	0	-40(8-II-1)	-1(9-II-2)
10	74	1.75(9-I-2)	-6.81(9-II-2)	1.68(9-II-2)	8(8-I-2)	96(8-I-2)	-6(8-I-2)
10	75	0.68(9-II-2)	-10.56(9-II-2)	1.44(9-II-2)	-4(8-I-2)	66(8-I-2)	-2(8-I-1)
10	76	-0.71(9-II-2)	-14.25(9-II-2)	1.46(9-II-2)	2(8-I-2)	53(8-I-2)	-2(8-I-2)
10	77	-0.96(9-I-2)	-6.49(9-II-2)	2.05(9-II-2)	-1(8-II-2)	58(8-I-2)	-2(8-II-2)
10	78	-1.66(9-II-2)	-7.81(9-II-2)	2.14(9-II-2)	0	36(8-I-2)	-2(8-I-2)
10	79	0.34(9-I-2)	-15.98(9-II-2)	1.71(9-II-2)	0	33(8-I-2)	0
10	80	-1.35(9-II-2)	-4.29(9-I-2)	4.00(9-II-2)	-4(8-I-2)	-143(8-II-2)	-13(8-I-2)
10	81	-1.25(9-I-2)	-3.72(9-I-2)	4.36(9-II-2)	4(8-I-2)	-153(8-II-2)	-14(8-I-2)
10	82	-7.23(9-I-2)	-12.66(9-I-2)	-4.40(9-I-2)	-49(8-I-2)	195(8-I-2)	-11(8-I-2)
10	83	-2.99(9-II-2)	-4.15(9-II-2)	4.78(9-II-2)	-33(8-II-2)	-58(8-II-2)	11(8-I-2)
10	84	-1.15(9-I-2)	-3.02(2)	5.51(9-II-2)	-10(8-I-2)	-3(8-I-4)	8(8-I-2)
10	85	-3.03(9-II-2)	-10.45(9-II-2)	5.48(9-II-2)	-13(8-I-2)	-30(8-II-2)	8(8-I-2)
10	86	-8.62(9-II-2)	-3.62(8-I-4)	4.95(9-II-2)	-38(8-I-2)	-5(9-I-2)	5(8-I-2)
10	87	1.59(9-II-2)	-4.20(9-I-2)	-2.44(9-I-2)	-76(8-I-2)	97(8-I-2)	-2(8-II-2)
10	88	-0.76(9-I-2)	-3.00(2)	2.12(9-II-2)	-17(8-I-2)	106(8-I-2)	-4(8-I-2)
10	89	1.86(9-I-2)	-2.71(2)	2.13(9-II-2)	-10(8-I-2)	65(8-I-2)	-3(8-I-2)
10	90	0.51(9-II-1)	-0.58(9-II-2)	2.91(9-II-2)	-47(8-I-2)	11(8-I-2)	-4(8-II-2)
10	91	7.82(9-II-2)	-1.82(9-I-2)	-3.78(9-I-2)	-90(8-I-2)	5(8-I-2)	14(8-I-2)
10	92	-1.73(9-I-2)	-8.93(9-I-2)	-3.44(9-I-2)	-39(8-I-2)	109(8-I-2)	-4(8-II-2)
10	93	-6.07(9-II-2)	-1.58(9-II-2)	3.00(9-II-2)	-24(8-II-2)	7(8-I-2)	5(8-I-2)
10	94	-0.79(9-II-2)	0.73(9-II-2)	3.12(9-II-2)	-25(8-I-2)	8(8-I-2)	-4(8-II-2)
10	95	-0.57(9-II-2)	-1.41(9-I-2)	3.33(9-II-2)	-23(8-I-2)	28(8-I-2)	-4(8-II-2)
10	96	-0.39(9-II-2)	-1.31(9-I-2)	3.30(9-II-2)	-13(8-I-2)	33(8-I-2)	-2(8-I-2)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
10	97	-2.57(9-II-2)	-4.23(9-I-2)	-3.47(9-I-2)	-33(8-I-2)	51(8-I-2)	-5(8-II-2)
10	98	-0.51(9-I-2)	-6.79(9-I-2)	2.77(9-II-2)	-2(8-II-2)	73(8-I-2)	-2(8-I-2)
10	99	-1.74(9-II-2)	-3.80(9-I-2)	2.76(9-II-2)	-3(8-I-2)	39(8-I-2)	-1(8-I-2)
10	100	0.22(9-I-2)	-3.19(9-I-2)	1.85(9-II-2)	0	37(8-I-2)	0
10	101	-0.85(9-II-2)	-4.20(9-I-2)	3.07(9-II-2)	-12(8-I-2)	39(8-I-2)	-1(8-I-2)
10	102	-0.11(9-II-2)	-3.83(9-I-2)	2.00(9-II-2)	0	40(8-I-2)	0
10	103	-0.11(9-II-1)	-1.78(9-II-2)	2.03(9-II-2)	0	39(8-I-1)	0
10	104	-12.95(9-II-2)	-6.99(9-II-2)	4.63(9-II-2)	-44(2)	13(8-I-4)	-4(8-I-2)
10	105	-0.64(9-II-2)	1.37(9-II-2)	3.67(9-II-2)	-14(9-I-3)	2(8-I-1)	4(8-I-2)
10	106	-3.71(9-II-2)	-4.40(9-II-1)	3.21(9-II-2)	-36(8-I-2)	8(8-I-3)	5(8-I-1)
10	107	-3.50(9-II-2)	-11.13(9-II-2)	3.35(9-II-2)	-19(2)	26(8-I-4)	4(8-I-2)
10	108	-1.86(9-II-2)	-3.98(8-I-1)	2.83(9-II-2)	-34(8-I-2)	-6(9-I-2)	4(8-I-1)
10	109	-0.95(9-II-2)	-2.35(9-II-2)	3.70(9-II-2)	-14(9-I-3)	22(8-I-4)	-4(8-I-2)
10	110	-0.26(2)	-0.43(9-II-2)	3.12(9-II-2)	-14(8-I-2)	22(8-I-1)	-3(8-I-2)
10	111	-0.35(9-II-2)	2.89(9-II-2)	2.85(9-II-2)	-8(8-I-2)	39(8-I-1)	-2(8-I-2)
10	112	-0.16(9-II-1)	-5.74(9-II-2)	1.98(9-II-2)	0	39(8-I-1)	0
10	113	-0.25(9-II-1)	-0.71(9-I-2)	1.96(9-II-2)	0	39(8-I-1)	0
10	114	-0.82(9-I-2)	-4.74(9-II-2)	2.71(9-II-2)	-26(8-I-2)	21(8-I-4)	3(8-I-1)
10	115	-2.02(9-I-2)	-6.74(9-II-2)	3.13(9-II-2)	-21(2)	15(8-I-4)	3(8-I-2)
10	116	-0.36(2)	-5.79(9-II-2)	3.20(9-II-2)	-6(9-I-2)	21(8-I-4)	3(8-II-2)
10	117	-1.07(9-I-2)	-5.82(9-II-2)	2.90(9-II-2)	-9(9-I-3)	43(8-I-4)	2(8-II-2)
10	118	-0.93(9-I-2)	-4.44(8-I-1)	2.45(9-II-2)	-15(8-I-2)	-8(8-II-1)	2(8-I-2)
10	119	0.95(9-II-2)	-3.53(8-I-4)	2.47(9-II-2)	-14(8-I-2)	44(8-I-1)	1(8-I-2)
10	120	-0.46(2)	-7.27(9-II-2)	1.89(9-II-2)	0	46(8-I-1)	1(8-II-2)
10	121	-0.52(2)	-6.33(8-I-4)	-1.75(9-I-2)	0	35(8-I-1)	0
10	1	0.56(9-I-1)	0.27(9-I-1)	0.88(9-I-1)	32(2)	305(9-I-1)	20(9-II-1)
10	2	-0.38(9-I-1)	-0.44(2)	-0.56(9-II-2)	56(9-II-1)	-63(9-I-1)	41(9-I-1)
10	3	-0.06(9-I-1)	-0.33(2)	-0.56(8-I-3)	63(2)	3(2)	-17(2)
10	4	-0.07(2)	-0.18(2)	-0.54(8-I-3)	23(1)	-4(8-I-4)	-17(8-II-3)
10	5	0.46(9-I-1)	-0.87(9-I-1)	0.52(9-I-1)	60(9-I-1)	367(9-I-1)	-14(9-I-1)
10	6	-0.18(9-I-1)	-0.44(2)	-0.51(9-II-2)	-64(9-II-1)	-83(9-I-1)	27(9-I-1)
10	7	-0.05(9-I-1)	-0.35(2)	-0.52(8-I-3)	-66(2)	-26(9-I-1)	-9(9-II-1)
10	8	-0.05(9-I-1)	-0.17(2)	-0.52(8-I-3)	-24(1)	4(8-II-3)	-13(1)
10	9	0.14(9-I-1)	-0.99(9-I-1)	-0.47(9-II-2)	73(9-I-1)	407(9-I-1)	-16(9-II-1)
10	10	-0.05(9-II-1)	-0.55(2)	-0.47(9-II-2)	-62(9-II-1)	-92(9-I-1)	-18(9-I-1)
10	11	-0.02(2)	-0.35(2)	-0.48(9-II-2)	-65(2)	-24(9-I-1)	8(9-II-1)
10	12	-0.02(2)	-0.18(2)	-0.48(8-I-3)	-23(1)	2(8-II-3)	15(1)
10	13	-0.10(9-II-1)	-0.92(9-I-1)	-0.44(8-I-3)	45(1)	411(9-I-1)	-22(9-II-1)
10	14	0.04(9-I-1)	-0.61(9-I-1)	-0.45(8-I-3)	56(9-II-1)	-91(9-I-1)	-48(9-I-1)
10	15	-0.01(2)	-0.37(2)	-0.45(8-I-3)	66(2)	20(2)	20(2)
10	16	0.02(8-I-3)	-0.18(2)	-0.46(8-I-3)	23(1)	-4(2)	23(2)
11	1	-2.73(9-II-4)	-2.16(9-I-4)	1.08(9-II-1)	0	-13(8-I-2)	-21(8-I-1)
11	2	-1.51(9-II-1)	-2.49(9-II-1)	2.23(9-II-1)	0	-14(8-I-4)	-5(8-I-1)
11	3	-3.68(9-II-1)	1.77(9-II-1)	2.18(9-II-1)	0	-11(8-I-4)	-6(8-I-1)
11	4	1.11(9-I-1)	-1.42(9-II-1)	2.36(9-II-1)	0	-8(8-I-1)	-3(8-I-1)
11	5	-2.66(9-II-1)	1.18(9-II-1)	2.91(9-II-1)	-50(8-II-1)	-7(8-I-1)	-3(8-I-1)
11	6	1.35(2)	-1.39(9-II-1)	2.32(9-II-1)	0	8(8-II-1)	0
11	7	-1.99(9-II-1)	-1.09(9-I-1)	2.98(9-II-1)	-35(8-II-1)	6(8-II-1)	-2(8-I-1)
11	8	1.52(2)	-1.38(9-II-1)	2.23(9-II-1)	0	7(8-II-1)	0
11	9	-1.48(9-II-1)	-1.16(9-I-1)	2.91(9-II-1)	-25(8-II-1)	6(8-II-1)	0
11	10	1.60(2)	-1.01(9-II-1)	2.10(9-II-1)	0	-6(8-I-1)	-1(8-II-1)
11	11	1.09(9-I-1)	-1.05(9-I-1)	2.78(9-II-1)	-18(8-II-1)	5(8-II-1)	0
11	12	1.64(2)	-0.37(2)	1.98(9-II-1)	0	-4(8-I-1)	-2(8-II-1)
11	13	0.68(9-I-4)	-0.98(2)	2.62(9-II-1)	12(8-I-1)	-4(8-I-1)	-2(8-II-1)
11	14	1.54(2)	-1.56(9-I-1)	-1.95(9-I-1)	0	-3(8-I-1)	-2(8-II-1)
11	15	0.18(2)	-1.06(2)	2.47(9-II-1)	9(8-I-1)	-3(8-I-1)	-2(8-II-1)
11	16	-2.68(9-II-1)	-3.51(2)	2.10(9-II-1)	-82(8-II-1)	-16(8-II-1)	-11(8-I-1)
11	17	6.39(9-I-1)	-1.07(2)	1.15(9-II-1)	-333(8-II-1)	-14(8-II-1)	-11(8-I-1)
11	18	3.47(9-I-1)	-2.06(9-I-1)	0.66(2)	-189(8-II-1)	-6(8-I-2)	-4(8-I-1)
11	19	3.13(9-I-1)	-0.29(9-II-1)	2.59(9-II-1)	-56(8-II-1)	-9(8-II-1)	-5(8-I-1)
11	20	4.72(9-I-1)	-0.65(2)	2.40(9-II-1)	-162(8-II-1)	-18(8-II-1)	8(8-II-1)
11	21	3.03(9-I-1)	0.05(9-II-4)	2.62(9-II-1)	-35(8-II-1)	-2(8-II-1)	-3(8-I-1)
11	22	-4.31(9-II-1)	-0.76(2)	2.48(9-II-1)	-101(8-II-1)	-7(8-II-1)	-4(8-I-1)
11	23	2.66(9-I-1)	0.12(9-II-1)	2.56(9-II-1)	-25(8-II-1)	0	0

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
11	24	3.71(9-I-1)	-0.80(2)	2.41(9-II-1)	-71(8-II-1)	-2(8-II-1)	-2(8-I-1)
11	25	2.18(9-I-1)	0.23(9-II-1)	2.44(9-II-1)	-18(8-II-1)	2(8-II-1)	0
11	26	3.04(9-I-1)	-0.84(2)	2.31(9-II-1)	-51(8-II-1)	0	0
11	27	2.25(2)	0.20(9-II-1)	2.28(9-II-1)	12(8-I-1)	-2(8-I-1)	-2(8-II-1)
11	28	2.30(9-I-1)	-0.90(2)	2.18(9-II-1)	-36(8-II-1)	0	-1(8-II-1)
11	29	2.27(2)	0.21(2)	2.13(9-II-1)	9(8-I-1)	-1(8-I-1)	-2(8-II-1)
11	30	1.68(9-I-4)	-0.85(2)	1.99(9-II-1)	24(8-I-1)	0	-2(8-II-1)
11	31	-7.17(9-II-1)	-4.78(2)	0.80(2)	-186(8-II-1)	-42(8-II-1)	-3(8-I-1)
11	32	4.34(9-I-1)	-2.84(2)	0.55(9-II-1)	-84(8-II-1)	-13(9-I-1)	-4(8-II-1)
11	33	5.93(9-I-1)	-0.36(9-II-1)	1.80(9-II-1)	-141(8-II-1)	7(8-I-1)	5(8-II-1)
11	34	-12.80(9-II-1)	-5.98(9-II-1)	2.22(9-II-1)	-132(8-II-1)	-35(8-II-1)	9(8-II-1)
11	35	5.72(9-I-1)	0.18(2)	1.84(9-II-1)	-98(8-II-1)	-3(8-II-1)	-3(8-I-1)
11	36	-11.31(9-II-1)	-0.55(9-II-1)	1.58(9-II-1)	-119(8-II-1)	-9(8-II-1)	-4(8-I-1)
11	37	5.17(9-I-1)	0.24(2)	1.70(9-II-1)	-71(8-II-1)	0	-1(8-I-1)
11	38	9.46(9-I-1)	-0.46(2)	1.37(9-II-1)	-102(8-II-1)	-4(8-II-1)	-3(8-I-1)
11	39	4.38(9-I-1)	0.27(9-II-1)	1.56(9-II-1)	-51(8-II-1)	0	0
11	40	7.93(9-I-1)	-0.44(2)	1.23(9-II-1)	-81(8-II-1)	-2(8-II-1)	0
11	41	3.41(2)	0.38(9-II-1)	1.41(9-II-1)	-36(8-II-1)	0	-1(8-II-1)
11	42	6.28(9-I-1)	-0.47(2)	1.11(9-II-1)	-61(8-II-1)	-1(8-II-1)	0
11	43	4.03(2)	0.56(9-II-1)	1.22(9-II-1)	25(8-I-1)	0	-2(8-II-1)
11	44	5.75(2)	-0.84(9-II-1)	1.05(9-II-1)	-44(8-II-1)	0	-1(8-II-1)
11	45	6.50(2)	-0.64(9-II-1)	1.06(9-II-1)	31(8-I-1)	0	-2(8-II-1)
11	46	6.56(2)	-0.70(9-I-1)	-1.03(9-I-1)	23(8-I-1)	0	-2(8-II-1)
11	47	-6.97(9-II-1)	-4.72(9-II-1)	3.11(9-II-1)	-80(8-II-1)	26(9-II-1)	-9(8-II-1)
11	48	-1.52(9-II-1)	-8.74(2)	4.06(9-II-1)	-18(9-I-1)	28(8-I-1)	8(8-I-1)
11	49	1.31(2)	2.29(9-I-1)	-2.11(9-I-1)	0	-1(8-I-1)	-3(8-II-1)
11	50	1.44(2)	-2.80(9-I-1)	-2.06(9-I-1)	0	-1(8-I-1)	-3(8-II-1)
11	51	0.54(9-II-1)	-1.33(9-II-1)	-2.49(9-I-1)	4(8-I-1)	-2(8-I-1)	-3(8-II-1)
11	52	1.42(2)	1.55(9-I-1)	-2.15(9-I-1)	0	-1(2)	3(8-I-1)
11	53	0.18(2)	-1.76(9-I-1)	-2.62(9-I-1)	2(2)	-1(2)	-3(8-II-1)
11	54	1.17(9-II-1)	1.21(9-I-1)	-2.16(9-I-1)	0	-3(8-I-1)	3(8-I-1)
11	55	0.46(9-II-1)	-1.82(2)	-2.71(9-I-1)	4(8-II-1)	-2(8-I-1)	3(8-I-1)
11	56	0.72(9-II-1)	-1.90(9-I-1)	-2.69(9-I-1)	6(8-II-1)	-4(8-I-1)	3(8-I-1)
11	57	1.11(9-II-1)	-3.06(2)	-2.08(9-I-1)	0	-8(8-I-1)	2(8-I-1)
11	58	-1.44(9-I-1)	1.13(9-I-1)	-2.60(9-I-1)	9(8-II-1)	-4(8-I-1)	2(8-I-1)
11	59	-1.98(9-I-1)	1.47(9-I-1)	-1.84(9-I-1)	0	-8(8-I-1)	2(8-I-1)
11	60	-2.42(2)	-0.57(9-II-3)	-1.12(2)	0	-18(8-I-3)	3(8-I-2)
11	61	1.21(2)	-2.91(2)	-1.97(9-I-1)	12(8-II-1)	-16(8-I-3)	2(8-I-1)
11	62	1.13(9-II-1)	-1.60(2)	-1.18(9-I-1)	14(8-II-1)	15(8-II-3)	3(8-I-2)
11	63	2.20(2)	0.06(9-I-1)	-2.25(9-I-1)	5(8-I-1)	0	-3(8-II-1)
11	64	1.43(9-II-1)	-0.88(2)	-2.00(9-I-1)	14(8-I-1)	0	-3(8-II-1)
11	65	4.06(2)	0.45(9-I-1)	-1.27(9-I-1)	13(8-I-1)	0	-2(8-II-1)
11	66	1.90(2)	-0.09(9-I-1)	-2.37(9-I-1)	3(2)	0	-3(8-II-1)
11	67	1.85(9-II-1)	-1.00(2)	-2.22(9-I-1)	7(8-I-1)	0	-3(8-II-1)
11	68	2.06(9-II-1)	-0.12(9-I-1)	-2.47(9-I-1)	4(8-II-1)	0	3(8-I-1)
11	69	2.41(9-II-1)	-0.85(2)	-2.36(9-I-1)	7(2)	0	-3(8-II-1)
11	70	2.51(9-II-1)	-0.21(9-I-1)	-2.49(9-I-1)	8(8-II-1)	-2(8-I-1)	3(8-I-1)
11	71	2.91(9-II-1)	-0.62(2)	-2.44(9-I-1)	11(8-II-1)	-1(8-I-1)	3(8-I-1)
11	72	2.27(9-II-1)	-0.35(9-I-1)	-2.44(9-I-1)	10(8-II-1)	-3(8-I-1)	2(8-I-1)
11	73	3.45(9-II-1)	-0.66(2)	-2.50(9-I-1)	18(8-II-1)	-2(8-I-1)	3(8-I-1)
11	74	-2.22(9-I-1)	-1.68(2)	-1.36(9-I-1)	19(8-II-1)	5(8-II-1)	2(8-I-2)
11	75	-2.74(9-I-1)	-4.03(9-I-1)	-2.00(9-I-1)	12(8-II-1)	9(8-II-1)	2(8-I-1)
11	76	2.68(9-II-1)	-1.24(2)	-2.50(9-I-1)	23(8-II-1)	5(8-II-1)	3(8-I-1)
11	77	3.54(9-II-1)	-1.67(2)	-1.28(9-I-1)	33(8-II-1)	-2(8-I-3)	2(8-I-2)
11	78	3.47(2)	0.28(9-I-1)	-1.49(9-I-1)	6(8-I-1)	0	-3(8-II-1)
11	79	5.83(2)	-0.66(9-I-1)	-1.06(9-I-1)	13(8-I-1)	0	-3(8-II-1)
11	80	4.29(9-II-1)	0.10(2)	-1.67(9-I-1)	7(2)	0	-3(8-II-1)
11	81	7.18(9-II-1)	-0.40(2)	-1.18(9-I-1)	8(2)	0	-3(8-II-1)
11	82	5.15(9-II-1)	0.17(9-II-1)	-1.83(9-I-1)	11(8-II-1)	0	3(8-I-1)
11	83	9.11(9-II-1)	-0.26(2)	-1.34(9-I-1)	13(8-II-4)	0	3(8-I-1)
11	84	5.62(9-II-1)	0.11(2)	-2.06(9-I-1)	19(8-II-1)	0	2(8-I-1)
11	85	11.23(9-II-1)	-0.28(2)	-1.54(9-I-1)	23(8-II-1)	0	2(8-I-1)
11	86	5.70(9-II-1)	-0.22(9-I-1)	-2.30(9-I-1)	26(8-II-1)	1(8-I-4)	2(9-II-4)
11	87	-13.85(9-I-1)	-0.60(9-I-1)	-1.85(9-I-1)	37(8-II-1)	1(8-II-3)	2(8-I-1)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
11	88	-5.86(9-I-1)	-4.78(2)	-1.36(9-I-1)	33(8-II-1)	9(8-II-1)	2(8-I-2)
11	89	-15.93(9-I-1)	-5.41(9-I-1)	-2.69(9-I-1)	52(8-II-1)	6(8-II-1)	3(9-II-4)
11	90	-9.27(9-I-1)	-2.57(2)	-1.70(9-I-1)	39(8-II-1)	-1(9-I-4)	2(8-I-2)
11	91	-8.43(9-I-1)	-3.63(2)	-2.77(9-I-1)	39(8-II-1)	-3(2)	2(8-I-1)
11	92	-3.04(9-I-1)	-8.98(2)	-2.83(9-I-1)	7(9-II-1)	6(2)	3(8-I-1)
11	93	1.79(9-II-1)	-3.86(2)	4.17(9-II-1)	4(8-II-1)	-9(9-II-1)	-6(8-II-1)
11	94	-4.18(9-II-1)	-7.45(2)	3.39(9-II-1)	-19(8-I-1)	17(8-II-1)	-5(8-II-1)
11	95	1.82(9-I-1)	-6.23(9-I-1)	2.11(9-II-1)	0	22(9-I-1)	-4(8-II-1)
11	96	-2.06(9-II-1)	-10.83(9-I-1)	1.21(9-II-1)	-10(8-I-1)	23(8-II-1)	-4(8-I-1)
11	97	0.46(9-I-1)	-4.72(8-II-1)	0.94(9-II-1)	5(8-I-2)	7(9-I-1)	-4(8-I-1)
11	98	-3.51(9-I-1)	-13.04(9-I-1)	-1.39(9-I-1)	-24(8-I-1)	11(8-II-1)	-6(8-I-1)
11	99	-5.85(9-I-1)	-5.42(8-II-1)	1.14(9-II-1)	-57(8-I-1)	5(9-I-1)	-4(8-I-1)
11	100	3.34(9-II-1)	-5.52(8-II-1)	-0.91(9-I-1)	-48(8-I-1)	8(8-I-2)	-3(8-I-1)
11	101	7.44(9-II-1)	-4.85(9-I-1)	-2.09(9-I-1)	-36(8-I-1)	15(8-I-1)	4(8-I-2)
11	102	-2.45(9-I-1)	-7.59(9-I-1)	-1.15(9-I-1)	-21(8-I-1)	30(8-I-1)	0
11	103	4.12(9-II-1)	0.36(9-I-1)	-0.88(9-I-1)	14(8-I-2)	3(8-I-1)	2(8-I-2)
11	104	5.61(9-II-1)	-0.71(9-I-1)	-1.01(9-I-1)	-6(9-II-1)	3(8-I-1)	3(8-I-2)
11	105	1.02(9-II-1)	0.28(9-I-1)	-1.29(9-I-1)	-2(8-II-2)	6(8-I-1)	3(8-I-2)
11	106	0.82(2)	-5.07(8-II-1)	-1.18(9-I-1)	-21(8-I-1)	-42(8-II-2)	0
11	107	-0.32(8-II-1)	-7.45(8-II-1)	-0.82(9-I-1)	0	-38(8-II-2)	0
11	108	-1.72(9-I-1)	-3.45(9-I-1)	-1.45(9-I-1)	-2(8-II-1)	-38(8-II-1)	3(8-I-2)
11	109	-0.25(8-II-1)	-4.44(9-I-1)	-0.99(9-I-1)	0	-44(8-II-1)	0
11	110	-0.13(9-I-1)	1.26(9-I-1)	-0.92(9-I-1)	0	21(8-I-1)	0
11	111	0.13(2)	-1.10(9-I-1)	-0.92(9-I-1)	0	21(8-I-1)	0
11	112	2.83(9-II-1)	-0.20(9-II-1)	-0.73(9-I-1)	19(8-I-2)	3(8-I-1)	2(8-I-2)
11	113	1.16(9-II-1)	-0.20(9-I-1)	-0.90(9-I-1)	8(8-I-2)	3(8-I-1)	2(8-I-2)
11	114	0.83(9-II-1)	-0.32(9-II-1)	-1.21(9-I-1)	8(8-I-2)	13(8-I-1)	2(8-I-1)
11	115	1.60(9-II-1)	-0.08(9-II-1)	-0.66(9-I-1)	18(8-I-2)	1(8-I-1)	1(8-I-1)
11	116	0.68(9-II-1)	-0.16(9-I-1)	-0.87(9-I-1)	8(8-I-2)	1(8-I-1)	1(8-I-1)
11	117	1.21(2)	-0.20(9-I-1)	-0.64(9-I-1)	16(8-I-2)	0	0
11	118	0.67(2)	-0.02(9-II-1)	-0.83(9-I-1)	7(8-I-1)	0	0
11	119	2.86(9-I-1)	-0.49(9-II-1)	0.69(9-II-1)	14(8-I-2)	0	0
11	120	1.71(9-I-1)	-0.45(9-I-1)	-0.66(9-I-1)	14(8-I-2)	0	0
11	121	0.97(9-I-1)	-0.13(9-II-1)	-0.77(9-I-1)	6(8-I-2)	0	0
11	122	0.47(9-II-1)	-0.15(9-I-1)	-1.20(9-I-1)	8(8-I-2)	6(8-I-1)	1(8-I-1)
11	123	0.22(2)	-0.33(9-I-1)	-0.88(9-I-1)	0	9(8-I-1)	0
11	124	0.28(9-I-1)	-0.23(9-I-1)	-1.18(9-I-1)	7(8-I-1)	2(8-I-1)	0
11	125	0.28(2)	-0.12(9-II-1)	-0.86(9-I-1)	0	4(8-I-1)	0
11	126	0.61(9-I-1)	-0.66(9-I-1)	-1.14(9-I-1)	6(8-I-2)	0	0
11	127	0.31(2)	-0.61(9-II-1)	-0.86(9-I-1)	0	0	0
11	128	0.33(2)	-1.21(9-II-1)	-0.87(9-I-1)	0	2(8-II-2)	0
11	129	0.32(2)	-1.07(9-I-1)	0.88(9-II-1)	0	2(8-II-2)	0
11	130	2.03(9-I-1)	-3.38(9-II-3)	-2.34(9-I-1)	-2(9-II-1)	-1(9-II-3)	-2(8-II-1)
11	131	-1.11(9-I-1)	-7.31(2)	-1.95(9-I-1)	2(9-II-1)	4(8-II-2)	-3(8-II-1)
11	132	0.71(9-I-1)	-4.05(9-II-3)	-2.19(9-I-1)	-1(9-I-1)	0	-3(8-II-1)
11	133	-0.61(9-II-4)	-8.75(9-II-4)	-1.98(9-I-1)	6(8-II-4)	6(8-II-2)	-3(8-II-2)
11	134	1.92(9-II-1)	-4.69(9-II-3)	-2.53(9-I-1)	-5(8-II-2)	-3(9-II-4)	-4(8-II-2)
11	135	-4.44(9-II-1)	-13.68(9-II-4)	-2.89(9-I-1)	20(9-II-3)	-3(9-II-3)	-5(8-II-2)
11	136	-10.26(9-II-1)	-6.79(9-II-4)	-2.56(9-I-1)	51(8-II-2)	3(9-I-4)	-4(8-II-2)
11	137	4.17(9-I-1)	-0.37(9-II-1)	0.73(9-II-1)	15(8-I-2)	0	0
11	138	1.65(9-I-1)	-0.16(9-I-1)	0.85(9-II-1)	5(8-I-2)	0	0
11	139	1.18(9-I-1)	-0.68(9-II-1)	1.23(9-II-1)	5(8-I-2)	0	0
11	140	5.58(9-I-1)	-0.18(9-II-1)	0.80(9-II-1)	17(9-I-3)	0	0
11	141	2.41(9-I-1)	0.14(9-II-1)	0.99(9-II-1)	7(9-I-3)	0	0
11	142	7.17(9-I-1)	-0.19(9-II-1)	0.92(9-II-1)	18(9-I-3)	-2(9-II-3)	-1(9-I-3)
11	143	2.81(9-I-1)	-0.06(9-I-1)	1.12(9-II-1)	8(9-I-3)	0	-1(8-I-3)
11	144	9.00(9-I-1)	0.20(9-I-1)	1.08(9-II-1)	-16(9-II-3)	-4(9-II-3)	-2(9-I-3)
11	145	3.14(9-I-1)	-0.03(9-I-1)	1.27(9-II-1)	-9(9-II-3)	-2(9-II-3)	-2(9-I-3)
11	146	11.24(9-I-1)	-1.04(9-II-1)	1.47(9-II-1)	5(9-I-3)	-6(9-II-3)	-3(9-I-3)
11	147	3.31(9-I-1)	-0.09(9-I-1)	1.46(9-II-1)	-8(9-II-3)	-4(9-II-3)	-2(9-I-3)
11	148	14.19(9-I-1)	-6.27(9-II-4)	2.89(9-II-1)	28(8-II-2)	-14(9-II-3)	4(9-II-3)
11	149	3.09(9-I-1)	0.50(9-II-4)	2.02(9-II-1)	-3(9-II-4)	-5(9-II-3)	-3(9-I-3)
11	150	1.52(9-I-1)	-0.27(9-II-1)	1.35(9-II-1)	6(9-I-3)	1(9-I-3)	0
11	151	0.30(2)	-0.31(9-I-1)	0.94(9-II-1)	0	0	0

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
11	152	1.96(9-I-1)	-0.28(9-II-1)	1.45(9-II-1)	8(9-I-3)	-5(9-II-3)	0
11	153	0.25(2)	-0.10(9-II-1)	0.99(9-II-1)	0	-2(9-II-3)	0
11	154	2.30(9-I-1)	-0.29(9-II-1)	1.56(9-II-1)	-9(9-II-3)	-11(9-II-3)	-1(9-I-3)
11	155	0.17(2)	-0.19(9-II-1)	1.05(9-II-1)	0	-7(9-II-3)	0
11	156	2.61(9-I-1)	0.35(9-I-1)	1.66(9-II-1)	-8(9-II-3)	-20(9-II-3)	-2(9-I-3)
11	157	0.13(9-I-1)	-0.18(9-II-1)	1.11(9-II-1)	0	-15(9-II-3)	0
11	158	-3.01(9-II-1)	-2.84(9-II-1)	2.06(9-II-1)	-3(9-II-4)	-35(9-II-3)	-3(9-I-3)
11	159	-0.21(9-II-1)	0.33(9-I-1)	1.18(9-II-1)	0	-25(9-II-3)	0
11	160	5.95(9-I-1)	-6.47(9-II-3)	-1.74(9-I-1)	43(8-II-3)	8(9-I-3)	-3(8-II-2)
11	161	-3.96(9-II-1)	-8.22(9-II-4)	1.69(9-II-1)	20(8-II-3)	-29(9-II-3)	0
11	162	1.68(9-I-1)	-5.70(9-II-4)	1.63(9-II-1)	19(8-II-3)	-43(9-II-3)	0
11	163	-0.36(9-II-1)	-6.55(9-II-4)	1.25(9-II-1)	0	-45(9-II-3)	0
11	164	-0.43(2)	-8.62(9-II-3)	-1.13(9-I-1)	0	-39(9-II-3)	0
11	1	-0.10(1)	-0.73(2)	-0.38(8-I-3)	71(1)	453(9-I-1)	54(2)
11	2	-0.07(1)	-0.56(2)	-0.38(8-I-3)	46(2)	-134(2)	97(1)
11	3	-0.05(9-II-1)	-0.37(2)	-0.39(8-I-3)	56(2)	-132(2)	-43(2)
11	4	-0.02(2)	-0.19(2)	-0.40(8-I-3)	25(2)	-57(2)	-90(2)
11	5	-0.09(2)	-0.71(2)	-0.30(9-II-2)	54(8-II-1)	581(1)	46(2)
11	6	-0.07(9-I-1)	-0.54(2)	-0.31(9-II-2)	-102(2)	-307(2)	33(2)
11	7	-0.07(9-I-2)	-0.35(2)	-0.33(9-II-2)	-125(2)	-416(2)	-14(2)
11	8	-0.03(9-I-2)	-0.18(2)	-0.33(9-II-2)	-52(2)	-155(2)	-62(2)
11	9	-0.13(9-I-2)	-0.66(2)	0.32(9-I-2)	58(8-II-1)	605(1)	-54(2)
11	10	-0.15(9-I-2)	-0.52(2)	0.41(9-I-2)	-102(2)	-299(2)	-28(2)
11	11	-0.10(9-I-2)	-0.35(2)	0.42(9-I-2)	-122(2)	-418(2)	19(2)
11	12	-0.04(9-I-2)	-0.18(2)	0.42(9-I-2)	-51(2)	-158(2)	59(2)
11	13	-0.25(9-I-2)	-0.91(9-I-2)	0.80(9-I-2)	122(8-II-3)	833(8-II-3)	-76(2)
11	14	-0.09(9-II-2)	-0.94(9-I-2)	0.47(9-I-2)	47(2)	-150(1)	-110(1)
11	15	-0.07(9-II-2)	-0.61(9-I-2)	0.33(9-I-2)	55(2)	-130(2)	38(2)
11	16	-0.04(9-II-2)	-0.28(9-I-2)	0.28(9-I-2)	24(2)	-64(2)	130(2)
12	1	-1.41(2)	-1.79(9-II-1)	-1.14(9-I-1)	0	15(8-II-3)	3(8-II-3)
12	2	-0.49(9-II-4)	-2.07(9-I-1)	-1.49(9-I-1)	0	3(8-II-3)	1(8-II-3)
12	3	-0.99(9-I-1)	-1.69(9-II-1)	-1.66(9-I-1)	-5(2)	6(8-II-3)	1(8-II-3)
12	4	-0.66(9-II-4)	-1.99(9-I-1)	-1.44(9-I-1)	0	6(8-II-3)	2(8-II-3)
12	5	-2.02(9-I-1)	-1.24(2)	-1.89(9-I-1)	-9(2)	-4(8-I-2)	0
12	6	-2.41(9-I-1)	-1.21(2)	-2.08(9-I-1)	-9(2)	-4(8-I-2)	0
12	7	-1.62(9-I-1)	-1.70(9-II-1)	-1.68(9-I-1)	-10(2)	11(8-II-3)	1(8-II-3)
12	8	1.27(9-II-1)	-1.29(8-II-4)	-1.57(9-I-1)	-16(2)	11(8-II-3)	2(8-II-3)
12	9	-2.87(9-I-1)	-1.89(9-II-4)	-1.55(9-I-1)	-19(2)	-2(8-I-3)	3(8-II-3)
12	10	-2.60(9-I-1)	-1.45(9-II-4)	-2.04(9-I-1)	-12(2)	-4(8-I-2)	0
12	11	-3.20(9-I-1)	-1.30(2)	-2.02(9-I-1)	-17(2)	-4(8-I-2)	0
12	12	-0.25(9-II-3)	-2.23(9-II-1)	-1.43(9-I-1)	0	4(8-II-3)	1(8-II-3)
12	13	-0.17(9-II-3)	-1.21(2)	-1.46(9-I-1)	0	3(9-II-3)	0
12	14	-0.76(9-I-1)	-1.21(2)	-1.85(9-I-1)	-4(2)	3(9-II-3)	0
12	15	-1.42(9-I-1)	-1.22(2)	-1.93(9-I-1)	-4(2)	-3(8-I-2)	0
12	16	-0.16(8-II-3)	-1.25(2)	-1.48(9-I-1)	0	3(9-II-3)	0
12	17	-0.73(9-I-1)	-1.22(2)	-1.95(9-I-1)	-4(9-II-3)	3(9-II-3)	0
12	18	-0.18(8-II-3)	-1.28(2)	1.49(9-II-1)	0	4(9-II-3)	0
12	19	-0.69(9-I-1)	-1.22(2)	-1.98(9-I-1)	-5(9-II-3)	3(9-II-3)	0
12	20	-0.20(8-II-3)	-1.31(2)	1.50(9-II-1)	0	4(9-II-3)	0
12	21	-0.63(9-I-1)	-1.23(2)	2.00(9-II-1)	-6(9-II-3)	3(9-II-3)	0
12	22	-0.57(9-I-1)	-1.24(2)	2.02(9-II-1)	-6(9-II-3)	4(9-II-3)	0
12	23	-0.23(8-II-3)	-1.34(2)	1.51(9-II-1)	0	5(9-II-3)	-1(9-II-3)
12	24	-0.28(8-II-3)	-1.36(2)	1.52(9-II-1)	0	6(9-II-3)	-2(9-II-3)
12	25	-0.48(9-I-1)	-1.25(2)	2.03(9-II-1)	-6(9-II-3)	5(9-II-3)	-1(9-II-3)
12	26	-0.38(8-II-3)	-1.36(2)	1.51(9-II-1)	0	6(9-II-3)	-2(9-II-3)
12	27	0.37(9-II-1)	-1.28(2)	2.02(9-II-1)	-5(9-II-3)	5(9-II-3)	-2(9-II-3)
12	28	-0.56(9-I-1)	-1.29(2)	1.45(9-II-1)	0	5(9-II-3)	-2(9-II-3)
12	29	0.33(9-II-4)	-1.33(2)	1.96(9-II-1)	-3(8-II-3)	5(9-II-3)	-2(9-II-3)
12	30	0.88(9-II-1)	-1.73(9-II-4)	1.24(9-II-4)	0	3(8-II-3)	-2(9-II-3)
12	31	0.68(9-II-1)	-2.28(9-I-1)	1.34(9-II-4)	0	4(8-II-3)	-2(9-II-3)
12	32	0.17(9-II-3)	-1.42(2)	1.79(9-II-1)	7(9-II-4)	4(9-II-3)	-2(9-II-3)
12	33	-0.21(9-II-4)	-1.72(9-I-4)	1.32(9-II-4)	12(9-II-4)	3(8-II-3)	-1(9-II-3)
12	34	-1.28(9-I-1)	-1.26(2)	-2.01(9-I-1)	-4(9-II-3)	-3(9-I-3)	0
12	35	-2.25(9-I-1)	-1.23(2)	-2.13(9-I-1)	-7(9-II-3)	-3(9-I-3)	0

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
12	36	-1.12(9-I-1)	-1.31(2)	-2.04(9-I-1)	-5(9-II-3)	-3(9-I-3)	0
12	37	-1.92(9-I-1)	-1.25(2)	-2.15(9-I-1)	-9(9-II-3)	-3(9-I-3)	0
12	38	-0.99(9-I-1)	-1.36(2)	2.06(9-II-1)	-6(9-II-3)	-4(9-I-3)	0
12	39	-1.62(9-I-1)	-1.26(2)	-2.15(9-I-1)	-11(9-II-3)	-3(9-I-3)	0
12	40	-0.86(9-I-1)	-1.39(2)	2.07(9-II-1)	-6(9-II-3)	-5(9-I-3)	0
12	41	-1.34(9-I-1)	-1.28(2)	2.15(9-II-1)	-12(9-II-3)	-4(9-I-3)	0
12	42	-0.76(9-I-1)	-1.43(2)	2.07(9-II-1)	-6(9-II-3)	7(9-II-4)	-1(9-II-3)
12	43	-1.05(9-I-1)	-1.29(2)	2.16(9-II-1)	-13(9-II-3)	-5(9-I-4)	0
12	44	-0.68(9-I-1)	-1.46(2)	2.06(9-II-1)	-5(9-II-3)	9(9-II-4)	-2(9-II-3)
12	45	-0.79(9-I-1)	-1.30(2)	2.16(9-II-1)	-12(9-II-3)	7(9-II-4)	-1(9-II-3)
12	46	-0.57(9-I-1)	-1.46(2)	2.00(9-II-1)	-3(8-II-3)	12(9-II-4)	-2(9-II-3)
12	47	-0.51(9-I-1)	-1.32(2)	2.13(9-II-1)	-9(9-II-3)	10(9-II-4)	-2(9-II-3)
12	48	-0.52(9-I-1)	-1.38(2)	1.84(9-II-1)	7(9-II-4)	13(9-II-4)	-2(9-II-3)
12	49	-0.17(9-I-4)	-1.35(2)	2.06(9-II-1)	-5(8-II-3)	13(9-II-4)	-2(9-II-3)
12	50	0.48(9-II-1)	-1.26(2)	1.54(9-II-4)	16(9-II-4)	14(9-II-3)	-2(9-II-3)
12	51	-0.29(9-II-1)	-1.31(2)	1.92(9-II-1)	18(9-II-4)	13(9-II-3)	-2(9-II-3)
12	52	-0.30(9-II-4)	-2.35(9-I-4)	1.58(9-II-4)	26(9-II-4)	8(8-II-3)	-2(9-II-3)
12	53	-2.86(9-I-1)	-1.18(2)	-2.27(9-I-1)	-9(2)	-3(8-I-2)	0
12	54	-4.83(9-I-1)	-1.29(2)	-2.31(9-I-1)	-15(2)	-4(8-I-2)	0
12	55	-3.59(9-I-1)	-2.29(9-II-4)	-2.17(9-I-1)	-20(2)	-4(8-I-2)	0
12	56	-4.65(9-I-1)	-1.56(2)	-1.99(9-I-1)	-25(2)	-3(9-I-3)	3(8-II-3)
12	57	-7.80(9-I-1)	-2.88(9-II-4)	-2.10(9-I-1)	-36(2)	-1(9-I-4)	3(8-II-3)
12	58	-3.41(9-I-1)	-1.52(9-II-4)	-2.65(9-I-1)	-15(2)	-4(2)	0
12	59	-7.04(9-I-1)	-1.48(2)	-2.74(9-I-1)	-24(2)	-4(8-I-2)	0
12	60	-6.31(9-I-1)	-2.82(9-II-4)	-3.16(9-I-1)	-36(2)	-3(2)	3(8-II-3)
12	61	-3.62(9-I-1)	-1.29(2)	-2.92(9-I-1)	-15(2)	-4(2)	0
12	62	-2.92(9-I-1)	-1.82(9-II-3)	-3.27(9-I-1)	-22(2)	-3(2)	0
12	63	-2.35(9-I-1)	-1.60(2)	-3.35(9-I-1)	-32(2)	-8(8-II-3)	2(8-II-3)
12	64	-2.21(9-I-1)	-1.31(2)	-3.23(9-I-1)	-14(2)	-4(2)	0
12	65	-1.05(9-I-1)	-1.36(2)	-3.28(9-I-1)	-20(2)	-4(2)	0
12	66	-2.49(9-I-1)	-1.26(2)	-2.33(9-I-1)	-7(9-II-3)	-3(8-I-2)	0
12	67	-3.45(9-I-1)	-1.25(2)	-2.45(9-I-1)	-10(2)	-3(8-I-2)	0
12	68	-3.11(9-I-1)	-1.26(2)	-2.77(9-I-1)	-10(2)	-4(2)	0
12	69	-2.18(9-I-1)	-1.32(2)	-2.34(9-I-1)	-9(9-II-3)	-3(9-I-3)	0
12	70	-2.74(9-I-1)	-1.26(2)	-2.47(9-I-1)	-11(9-II-3)	-3(9-I-3)	0
12	71	-1.88(9-I-1)	-1.38(2)	-2.33(9-I-1)	-11(9-II-3)	-3(9-I-3)	0
12	72	-2.26(9-I-1)	-1.29(2)	-2.45(9-I-1)	-13(9-II-3)	-3(9-I-3)	0
12	73	-1.62(9-I-1)	-1.43(2)	2.30(9-II-1)	-12(9-II-3)	-4(9-I-4)	0
12	74	-1.87(9-I-1)	-1.33(2)	-2.42(9-I-1)	-15(9-II-3)	-3(9-I-4)	0
12	75	-1.38(9-I-1)	-1.48(2)	2.30(9-II-1)	-13(9-II-3)	-6(9-I-4)	0
12	76	-1.49(9-I-1)	-1.35(2)	2.38(9-II-1)	-17(9-II-3)	-5(9-I-4)	0
12	77	-1.15(9-I-1)	-1.51(2)	2.28(9-II-1)	-12(9-II-3)	9(9-II-4)	0
12	78	-1.15(9-I-1)	-1.36(2)	2.36(9-II-1)	-18(9-II-3)	-7(9-I-4)	0
12	79	-0.96(9-I-1)	-1.53(2)	2.25(9-II-1)	-9(9-II-3)	14(9-II-4)	-1(9-II-3)
12	80	-0.83(9-I-1)	-1.38(2)	2.34(9-II-1)	-17(9-II-3)	11(9-II-4)	0
12	81	-0.88(9-I-1)	-1.51(2)	2.16(9-II-1)	-5(8-II-3)	21(9-II-4)	-2(9-II-3)
12	82	-0.50(9-I-1)	-1.40(2)	2.28(9-II-1)	-13(9-II-3)	16(9-II-4)	0
12	83	0.29(9-II-4)	-1.21(2)	1.85(9-II-4)	35(9-II-4)	24(9-II-4)	-3(9-II-4)
12	84	-0.78(9-I-1)	-1.65(9-I-1)	2.02(9-II-1)	17(9-II-4)	28(9-II-4)	-2(9-II-3)
12	85	-0.18(9-I-3)	-1.36(2)	2.15(9-II-1)	-6(9-I-2)	24(9-II-4)	-1(9-II-3)
12	86	-0.22(9-I-4)	-3.12(9-I-4)	1.79(9-II-4)	41(9-II-4)	35(9-II-4)	-3(9-II-3)
12	87	-2.74(9-I-1)	-1.34(2)	-2.75(9-I-1)	-11(9-II-3)	-3(2)	0
12	88	-2.47(9-I-1)	-1.27(2)	-2.90(9-I-1)	-11(9-II-3)	-4(2)	0
12	89	-2.35(9-I-1)	-1.41(2)	-2.70(9-I-1)	-13(9-II-3)	-3(2)	0
12	90	-1.96(9-I-1)	-1.31(2)	-2.84(9-I-1)	-14(9-II-3)	-3(2)	0
12	91	-2.00(9-I-1)	-1.47(2)	-2.64(9-I-1)	-15(9-II-3)	-3(9-I-1)	0
12	92	-1.62(9-I-1)	-1.36(2)	-2.77(9-I-1)	-16(9-II-3)	-3(9-I-1)	0
12	93	-1.72(9-I-1)	-1.53(2)	-2.58(9-I-1)	-17(9-II-3)	-4(9-I-4)	0
12	94	-1.30(9-I-1)	-1.38(2)	-2.70(9-I-1)	-17(9-II-3)	-3(9-I-1)	0
12	95	-2.09(9-I-1)	-1.36(2)	-3.14(9-I-1)	-11(9-II-3)	-4(2)	0
12	96	-0.64(9-I-1)	-1.30(2)	-3.23(9-I-1)	-12(2)	-4(2)	0
12	97	-1.85(9-I-1)	-1.44(2)	-3.04(9-I-1)	-14(9-II-3)	-3(2)	0
12	98	-0.58(9-I-1)	-1.33(2)	-3.13(9-I-1)	-13(9-II-3)	-3(2)	0
12	99	-1.60(9-I-1)	-1.51(2)	-2.95(9-I-1)	-16(9-II-3)	-3(8-II-3)	0

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
12	100	-0.53(9-I-1)	-1.38(2)	-3.04(9-I-1)	-15(9-II-3)	-3(8-II-3)	0
12	101	-1.40(9-I-1)	-1.58(2)	-2.86(9-I-1)	-17(9-II-3)	-3(9-I-1)	0
12	102	-0.45(9-I-1)	-1.43(2)	-2.95(9-I-1)	-15(9-II-3)	-3(9-I-1)	0
12	103	-0.38(9-I-1)	-1.47(2)	-2.86(9-I-1)	-15(9-II-3)	-3(9-I-1)	0
12	104	-1.43(9-I-1)	-1.58(2)	2.52(9-II-1)	-18(9-II-3)	-6(9-I-4)	0
12	105	-1.03(9-I-1)	-1.42(2)	-2.63(9-I-1)	-18(9-II-3)	-5(9-I-4)	0
12	106	-1.20(9-I-1)	-1.63(2)	-2.77(9-I-1)	-18(9-II-3)	-3(9-I-1)	0
12	107	-1.16(9-I-1)	-1.60(2)	2.49(9-II-1)	-17(9-II-3)	9(9-II-4)	0
12	108	-0.78(9-I-1)	-1.45(2)	2.57(9-II-1)	-19(9-II-3)	7(9-II-4)	0
12	109	-0.92(9-I-1)	-1.60(2)	2.42(9-II-1)	-13(9-II-3)	16(9-II-4)	0
12	110	-0.52(9-I-1)	-1.46(2)	2.52(9-II-1)	-17(9-II-3)	12(9-II-4)	0
12	111	-0.69(9-I-1)	-1.49(2)	2.30(9-II-1)	-7(9-I-1)	26(9-II-4)	0
12	112	-0.24(9-I-4)	-1.45(2)	2.44(9-II-1)	-13(9-II-3)	20(9-II-4)	0
12	113	-0.67(9-II-3)	-1.59(9-I-1)	2.12(9-II-4)	40(9-II-4)	43(9-II-4)	-3(9-II-3)
12	114	0.33(8-II-3)	-1.38(2)	2.33(9-II-1)	-6(9-I-2)	35(9-II-4)	0
12	115	-0.44(9-I-3)	-4.29(9-I-4)	2.24(9-II-4)	33(9-II-4)	49(9-II-4)	-2(9-II-4)
12	116	-1.02(9-I-1)	-1.67(2)	-2.68(9-I-1)	-19(9-II-3)	-4(9-I-1)	0
12	117	-0.30(9-I-1)	-1.51(2)	-2.77(9-I-1)	-14(9-II-3)	-3(9-I-1)	0
12	118	-0.86(9-I-1)	-1.69(2)	2.62(9-II-1)	-17(9-II-3)	6(9-II-4)	1(9-II-4)
12	119	-0.21(9-I-1)	-1.53(2)	2.68(9-II-1)	-13(9-II-3)	5(9-II-4)	1(9-II-4)
12	120	-0.77(9-I-1)	-1.66(2)	2.54(9-II-1)	-12(9-II-3)	11(9-II-4)	1(9-II-4)
12	121	0.15(9-II-4)	-1.53(2)	2.62(9-II-1)	-10(9-II-3)	9(9-II-4)	2(9-II-4)
12	122	-0.41(9-II-3)	-1.54(9-I-1)	2.40(9-II-4)	12(9-II-4)	22(9-II-4)	0
12	123	-0.66(8-II-3)	-1.98(9-I-1)	2.44(9-II-1)	-8(9-I-1)	25(9-II-4)	1(9-II-4)
12	124	0.28(8-II-3)	-1.47(2)	2.52(9-II-1)	-5(8-II-3)	18(9-II-4)	3(9-II-4)
12	125	0.52(9-II-3)	-2.67(9-I-1)	2.48(9-II-4)	9(9-II-4)	16(9-II-4)	0
12	126	-0.81(2)	-2.51(9-II-3)	-3.22(9-I-1)	-28(2)	10(8-II-3)	-2(8-I-3)
12	127	-1.41(9-I-1)	-2.77(2)	-3.06(9-I-1)	-29(2)	-1(9-II-3)	-3(8-I-3)
12	128	-0.72(9-I-1)	-1.50(9-II-3)	-3.29(9-I-1)	-18(2)	-4(8-II-3)	0
12	129	-0.63(9-I-1)	-1.37(2)	-3.31(9-I-1)	-21(2)	-4(8-II-3)	0
12	130	-1.37(9-II-1)	-3.80(9-II-3)	-3.00(9-I-1)	-28(2)	0	-4(8-I-3)
12	131	-0.32(9-II-3)	-1.42(2)	-3.27(9-I-1)	-17(2)	-3(8-II-3)	0
12	132	-0.91(9-II-1)	-1.40(2)	-3.31(9-I-1)	-14(2)	-1(8-I-1)	0
12	133	-0.77(9-II-4)	-2.48(9-II-3)	-3.29(9-I-1)	-20(2)	-3(9-I-3)	0
12	134	-0.59(9-I-1)	-2.49(9-II-3)	-3.20(9-I-1)	-22(9-I-4)	-8(8-II-3)	-3(8-I-3)
12	135	-1.75(9-II-1)	-4.06(9-II-3)	-3.23(9-I-1)	-23(9-I-3)	-3(9-II-4)	-2(8-I-3)
12	136	-1.55(9-II-4)	-1.51(2)	-3.28(9-I-1)	-15(2)	-5(8-II-3)	0
12	137	-2.37(9-II-1)	-1.35(2)	-3.21(9-I-1)	-9(2)	-4(8-II-3)	0
12	138	-0.54(9-I-1)	-1.38(2)	-3.22(9-I-1)	-12(2)	-4(8-II-3)	0
12	139	-0.65(9-II-1)	-1.32(2)	-3.25(9-I-1)	-12(2)	-3(8-II-3)	0
12	140	-1.05(9-II-4)	-1.39(2)	-3.21(9-I-1)	-12(2)	-6(8-II-3)	0
12	141	-0.54(9-I-1)	-1.44(2)	-3.14(9-I-1)	-13(9-II-3)	-5(8-II-3)	0
12	142	-0.64(9-II-1)	-1.34(2)	-3.18(9-I-1)	-13(8-II-3)	-5(8-II-3)	0
12	143	-0.53(9-I-1)	-1.53(2)	-3.06(9-I-1)	-15(9-II-3)	-6(8-II-3)	0
12	144	-0.57(9-II-1)	-1.41(2)	-3.10(9-I-1)	-14(8-II-3)	-6(8-II-3)	0
12	145	-0.52(9-I-1)	-1.61(2)	-2.98(9-I-1)	-15(9-II-3)	-6(8-II-3)	0
12	146	-0.49(9-II-1)	-1.47(2)	-3.01(9-I-1)	-13(8-II-3)	-6(8-II-3)	0
12	147	-0.49(9-I-1)	-1.68(2)	-2.89(9-I-1)	-15(9-II-3)	-6(8-II-3)	0
12	148	-0.41(9-II-1)	-1.53(2)	-2.93(9-I-1)	-12(8-II-3)	-6(8-II-3)	0
12	149	-0.47(9-I-1)	-1.73(2)	-2.81(9-I-1)	-14(9-II-3)	-5(8-II-3)	0
12	150	0.33(9-I-1)	-1.57(2)	-2.85(9-I-1)	11(8-I-3)	-5(8-II-3)	0
12	151	-0.44(9-I-1)	-1.77(2)	-2.71(9-I-1)	-13(9-II-3)	4(9-I-3)	1(9-II-4)
12	152	0.29(9-I-1)	-1.61(2)	-2.76(9-I-1)	10(8-I-3)	-4(8-II-3)	1(9-II-4)
12	153	-0.41(9-I-1)	-1.77(2)	2.64(9-II-1)	-10(9-II-3)	4(9-I-3)	2(9-II-4)
12	154	0.25(9-I-1)	-1.62(2)	-2.67(9-I-1)	7(8-I-3)	3(8-I-3)	2(9-II-4)
12	155	-0.43(8-II-3)	-1.71(8-II-3)	2.55(9-II-1)	-4(8-II-3)	4(9-I-3)	3(9-II-4)
12	156	0.28(9-I-2)	-1.58(2)	2.61(9-II-1)	4(8-I-4)	2(8-I-3)	2(9-II-4)
12	157	-0.60(8-II-3)	-2.09(8-II-3)	2.49(9-II-4)	6(9-II-4)	4(9-II-4)	0
12	158	0.43(8-II-3)	-1.67(9-I-1)	2.54(9-II-1)	-2(9-II-1)	4(9-I-4)	3(9-II-4)
12	159	0.41(8-II-3)	-2.51(8-II-3)	2.55(9-II-4)	-7(9-II-1)	7(9-I-4)	1(9-I-2)
12	160	-0.82(9-II-4)	-1.44(2)	-3.13(9-I-1)	-13(8-II-3)	-8(8-II-3)	0
12	161	-2.02(9-II-1)	-1.37(2)	-3.12(9-I-1)	-12(8-II-3)	-7(8-II-3)	0
12	162	-0.71(9-II-4)	-1.54(2)	-3.05(9-I-1)	-14(8-II-3)	-9(8-II-3)	0
12	163	-1.77(9-II-1)	-1.42(2)	-3.04(9-I-1)	-12(8-II-3)	-9(8-II-3)	0

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
12	164	-0.61(9-II-4)	-1.64(2)	-2.96(9-I-1)	-13(8-II-3)	-10(8-II-3)	0
12	165	-1.49(9-II-1)	-1.50(2)	-2.95(9-I-1)	-11(8-II-3)	-9(8-II-3)	0
12	166	-0.51(9-II-4)	-1.72(2)	-2.88(9-I-1)	-12(8-II-3)	10(8-I-3)	0
12	167	1.25(9-I-1)	-1.57(2)	-2.87(9-I-1)	10(8-I-3)	10(8-I-3)	0
12	168	-0.42(9-II-4)	-1.79(2)	-2.80(9-I-1)	11(8-I-3)	10(9-I-3)	0
12	169	1.03(9-I-1)	-1.63(2)	-2.79(9-I-1)	9(8-I-3)	10(9-I-3)	0
12	170	-0.33(9-II-4)	-1.84(2)	-2.71(9-I-1)	10(8-I-3)	11(9-I-3)	1(9-II-3)
12	171	0.83(9-I-1)	-1.67(2)	-2.71(9-I-1)	9(9-II-1)	10(9-I-3)	0
12	172	-0.30(9-II-3)	-1.86(2)	-2.63(9-I-1)	7(8-I-3)	12(9-I-3)	2(9-II-4)
12	173	0.64(9-I-1)	-1.70(2)	-2.63(9-I-1)	10(9-II-1)	11(9-I-3)	1(9-II-3)
12	174	-0.39(8-II-3)	-1.83(2)	2.56(9-II-1)	3(8-I-3)	-16(9-II-4)	2(9-II-4)
12	175	0.45(9-I-1)	-1.69(2)	2.55(9-II-1)	9(9-II-1)	-13(9-II-3)	1(9-II-3)
12	176	-0.37(8-II-3)	-2.11(8-II-3)	2.47(9-II-1)	-10(9-II-1)	-23(9-II-4)	0
12	177	-0.59(8-II-3)	-2.38(8-II-3)	2.51(9-II-1)	-2(9-II-1)	17(9-I-4)	2(9-II-4)
12	178	0.28(8-II-3)	-1.61(2)	2.52(9-II-1)	5(9-II-3)	-16(9-II-4)	2(9-II-4)
12	179	0.42(8-II-3)	-3.25(8-II-3)	2.47(9-II-4)	-25(9-II-1)	-25(9-II-4)	1(9-I-2)
12	180	-2.76(9-II-1)	-1.96(9-II-3)	-3.24(9-I-1)	-10(9-I-3)	4(8-I-3)	0
12	181	-3.82(9-II-1)	-3.06(9-II-3)	-3.24(9-I-1)	-25(9-I-3)	1(9-I-3)	-2(8-I-3)
12	182	-4.27(9-II-1)	-3.96(9-II-3)	-2.91(9-I-1)	-30(9-I-3)	3(9-I-4)	-2(8-I-3)
12	183	-5.95(9-II-1)	-1.88(9-II-3)	-2.85(9-I-1)	-8(9-I-3)	10(9-I-3)	0
12	184	-3.43(9-II-1)	-1.41(2)	-2.91(9-I-1)	-10(8-II-3)	11(9-I-3)	0
12	185	-3.47(9-II-1)	-1.51(8-II-4)	-2.72(9-I-1)	-7(8-II-3)	10(9-I-3)	0
12	186	-3.52(9-II-1)	-2.74(8-II-3)	-2.41(9-I-1)	-8(9-I-3)	11(9-I-3)	0
12	187	7.25(9-I-1)	-3.48(9-II-3)	-2.36(9-I-1)	-31(9-I-3)	13(9-I-3)	-2(8-I-3)
12	188	-2.60(9-II-1)	-5.01(9-II-3)	-1.80(9-I-1)	-23(9-I-3)	8(9-I-3)	-2(8-I-3)
12	189	-3.66(9-II-1)	-1.41(2)	-2.38(9-I-1)	-7(8-II-3)	23(9-I-3)	0
12	190	-3.14(9-II-1)	-1.64(9-II-3)	-2.19(9-I-1)	-4(9-I-1)	20(9-I-3)	-2(8-II-2)
12	191	2.44(9-I-1)	-1.43(2)	-2.23(9-I-1)	-6(8-II-3)	23(9-I-3)	0
12	192	2.16(9-I-1)	-4.17(9-II-3)	-1.81(9-I-1)	-21(9-I-3)	-47(9-II-3)	0
12	193	-0.48(2)	-6.63(8-II-3)	-1.14(9-I-1)	0	-39(9-II-3)	0
12	194	2.05(9-I-1)	-1.87(9-II-3)	-1.95(9-I-1)	-4(8-II-4)	42(9-I-3)	-1(8-II-2)
12	195	-0.45(9-II-4)	-2.66(8-II-3)	-1.29(9-I-1)	0	-48(9-II-3)	0
12	196	1.77(9-I-1)	-1.34(2)	-2.00(9-I-1)	-6(8-II-3)	36(9-I-3)	0
12	197	-0.26(9-II-4)	-1.53(2)	-1.30(9-I-1)	0	38(9-I-3)	0
12	198	-2.52(9-II-1)	-1.42(2)	-2.88(9-I-1)	-12(8-II-3)	13(9-I-3)	0
12	199	-2.96(9-II-1)	-1.38(2)	-2.75(9-I-1)	-9(8-II-3)	12(9-I-3)	0
12	200	-3.11(9-II-1)	-1.39(2)	-2.42(9-I-1)	-10(8-II-3)	23(9-I-3)	0
12	201	-1.97(9-II-1)	-1.53(2)	-2.83(9-I-1)	-12(8-II-3)	15(9-I-3)	0
12	202	-2.52(9-II-1)	-1.43(2)	-2.73(9-I-1)	-9(8-II-3)	14(9-I-3)	0
12	203	-1.59(9-II-1)	-1.65(2)	-2.77(9-I-1)	-11(8-II-3)	15(9-I-3)	0
12	204	2.14(9-I-1)	-1.51(2)	-2.69(9-I-1)	-8(8-II-3)	15(9-I-3)	0
12	205	-1.28(9-II-1)	-1.75(2)	-2.70(9-I-1)	10(8-I-3)	16(9-I-3)	0
12	206	1.79(9-I-1)	-1.60(2)	-2.64(9-I-1)	7(8-I-3)	15(9-I-3)	0
12	207	-1.01(9-II-4)	-1.84(2)	-2.63(9-I-1)	9(8-I-3)	16(9-I-3)	0
12	208	1.46(9-I-1)	-1.67(2)	-2.58(9-I-1)	6(8-I-3)	16(9-I-3)	0
12	209	-0.77(9-II-4)	-1.90(2)	-2.57(9-I-1)	9(9-II-1)	17(9-I-3)	0
12	210	1.17(9-I-1)	-1.73(2)	-2.52(9-I-1)	7(9-II-1)	16(9-I-3)	0
12	211	-0.55(9-II-4)	-1.94(2)	-2.49(9-I-1)	10(9-II-1)	18(9-I-3)	0
12	212	0.89(9-I-1)	-1.77(2)	-2.45(9-I-1)	9(9-II-1)	17(9-I-3)	0
12	213	-0.36(9-II-4)	-1.95(2)	-2.42(9-I-1)	9(9-II-1)	21(9-I-3)	1(8-II-3)
12	214	0.63(9-I-1)	-1.78(2)	-2.39(9-I-1)	10(9-II-1)	19(9-I-3)	0
12	215	-0.28(9-II-3)	-2.01(8-II-3)	2.39(9-II-1)	-2(9-I-3)	-29(9-II-4)	2(9-II-3)
12	216	0.40(9-I-1)	-1.73(2)	2.36(9-II-1)	7(9-II-4)	-23(9-II-3)	1(8-II-3)
12	217	-0.64(9-I-1)	-2.95(8-II-3)	2.31(9-II-1)	-24(9-II-1)	-35(9-II-4)	1(9-I-1)
12	218	0.27(8-II-3)	-2.04(8-II-3)	2.34(9-II-1)	-9(9-II-1)	-37(9-II-4)	1(8-II-3)
12	219	0.45(9-I-1)	-4.61(8-II-3)	2.16(9-II-4)	-41(9-II-1)	-49(9-II-4)	-2(9-II-4)
12	220	-2.54(9-II-1)	-1.50(2)	-2.43(9-I-1)	-9(8-II-3)	23(9-I-3)	0
12	221	2.01(9-I-1)	-1.44(2)	-2.27(9-I-1)	-5(8-II-3)	22(9-I-3)	0
12	222	-2.06(9-II-1)	-1.64(2)	-2.42(9-I-1)	-8(8-II-3)	22(9-I-3)	0
12	223	1.70(9-I-1)	-1.52(2)	-2.30(9-I-1)	-4(8-II-3)	22(9-I-3)	0
12	224	-1.65(9-II-1)	-1.77(2)	-2.40(9-I-1)	7(8-I-3)	22(9-I-3)	0
12	225	1.42(9-I-1)	-1.62(2)	-2.30(9-I-1)	3(8-I-3)	22(9-I-3)	0
12	226	-1.30(9-II-1)	-1.87(2)	-2.36(9-I-1)	6(8-I-3)	23(9-I-3)	0
12	227	1.18(9-I-1)	-1.71(2)	-2.28(9-I-1)	3(8-I-3)	22(9-I-3)	0

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
12	228	-0.98(9-II-4)	-1.95(2)	-2.32(9-I-1)	7(9-II-1)	23(9-I-3)	0
12	229	0.96(9-I-1)	-1.78(2)	-2.25(9-I-1)	3(9-II-1)	23(9-I-3)	0
12	230	1.56(9-I-1)	-1.43(2)	-2.07(9-I-1)	-5(8-II-3)	33(9-I-3)	0
12	231	-0.16(9-II-1)	-1.45(2)	-1.35(9-I-1)	0	35(9-I-3)	0
12	232	1.30(9-I-1)	-1.59(2)	-2.11(9-I-1)	-4(8-II-3)	31(9-I-3)	0
12	233	0.14(9-I-1)	-1.53(2)	-1.38(9-I-1)	0	32(9-I-3)	0
12	234	1.06(9-I-1)	-1.74(2)	-2.13(9-I-1)	3(8-I-3)	29(9-I-3)	0
12	235	0.18(8-II-3)	-1.64(2)	-1.41(9-I-1)	0	30(9-I-3)	0
12	236	0.85(9-I-1)	-1.86(2)	-2.13(9-I-1)	3(8-I-3)	29(9-I-3)	0
12	237	0.22(8-II-3)	-1.75(2)	-1.41(9-I-1)	0	29(9-I-3)	0
12	238	0.65(9-I-1)	-1.96(2)	-2.11(9-I-1)	3(9-II-1)	30(9-I-3)	0
12	239	0.25(8-II-3)	-1.85(2)	-1.41(9-I-1)	0	29(9-I-3)	0
12	240	-0.71(9-II-4)	-2.01(2)	-2.27(9-I-1)	9(9-II-1)	24(9-I-3)	0
12	241	0.75(9-I-1)	-1.84(2)	-2.21(9-I-1)	4(9-II-1)	24(9-I-3)	0
12	242	-0.47(9-II-4)	-2.03(2)	-2.22(9-I-1)	10(9-II-1)	26(9-I-3)	0
12	243	0.52(9-I-1)	-1.87(2)	-2.16(9-I-1)	4(9-II-1)	25(9-I-3)	0
12	244	-0.34(9-II-3)	-2.04(2)	2.21(9-II-1)	6(9-II-4)	27(9-I-3)	1(9-I-2)
12	245	0.29(2)	-1.86(2)	-2.11(9-I-1)	3(9-II-1)	27(9-I-3)	-1(9-II-1)
12	246	0.68(9-II-1)	-3.00(8-II-3)	2.10(9-II-1)	-39(9-II-1)	-36(9-II-3)	-3(9-II-4)
12	247	-0.39(8-II-3)	-2.62(8-II-3)	2.21(9-II-1)	-11(9-II-1)	-31(9-II-3)	0
12	248	0.29(2)	-1.94(8-II-3)	2.11(9-II-1)	5(9-I-4)	28(9-I-3)	-2(9-II-1)
12	249	0.38(9-I-1)	-4.51(8-II-3)	1.90(9-II-1)	-25(9-II-1)	-23(9-II-3)	-1(9-II-4)
12	250	0.48(9-I-4)	-2.03(2)	-2.08(9-I-1)	4(9-II-1)	30(9-I-3)	0
12	251	0.26(8-II-3)	-1.93(2)	-1.39(9-I-1)	0	30(9-I-3)	0
12	252	0.36(9-I-4)	-2.08(2)	-2.03(9-I-1)	4(9-II-1)	31(9-I-3)	0
12	253	0.29(2)	-1.98(2)	-1.37(9-I-1)	0	31(9-I-3)	0
12	254	0.33(9-I-4)	-2.08(2)	-1.98(9-I-1)	3(9-II-1)	33(8-I-3)	0
12	255	0.31(2)	-2.00(2)	-1.34(9-I-1)	0	32(8-I-3)	0
12	256	0.26(9-I-3)	-2.39(9-I-1)	2.01(9-II-1)	4(9-I-4)	36(8-I-3)	-1(9-II-1)
12	257	0.33(2)	-1.97(2)	1.33(9-II-1)	0	34(8-I-3)	0
12	258	0.56(8-I-3)	-4.39(9-I-1)	1.91(9-II-1)	-24(9-II-1)	38(8-I-3)	-2(9-II-1)
12	259	0.39(2)	-2.22(9-II-3)	1.39(9-II-1)	0	38(8-I-3)	0
12	260	0.33(2)	-5.07(8-II-3)	1.32(9-II-1)	0	39(8-I-3)	0
13	1	39.30(2)	-22.41(2)	1.51(2)	0	-198(2)	-35(8-I-2)
13	2	5.70(2)	-8.47(2)	-1.26(9-I-2)	0	-89(2)	-17(8-I-2)
13	3	-4.06(9-II-2)	-8.46(2)	1.06(9-II-3)	450(8-I-2)	-91(2)	-20(8-I-2)
13	4	2.42(9-I-2)	-2.35(9-II-2)	-1.68(9-I-2)	0	-37(2)	-8(8-I-2)
13	5	2.42(9-I-3)	-2.70(2)	-1.70(9-I-2)	228(8-I-2)	-43(2)	-9(8-I-2)
13	6	1.58(9-I-2)	-1.07(9-II-2)	-1.96(9-I-2)	0	-18(2)	-4(2)
13	7	2.17(9-I-3)	-0.89(9-I-2)	-2.33(9-I-2)	120(8-I-2)	-21(2)	-5(8-I-2)
13	8	2.10(9-I-2)	-0.97(9-I-2)	-2.64(9-I-2)	65(8-I-2)	-11(2)	-2(2)
13	9	0.94(9-I-2)	0.75(9-I-2)	-2.09(9-I-2)	0	-9(2)	-3(2)
13	10	0.38(9-I-2)	0.69(9-I-2)	-2.16(9-I-2)	0	-5(8-II-2)	-2(2)
13	11	1.84(9-I-2)	-0.82(9-I-2)	-2.77(9-I-2)	35(8-I-2)	-6(8-II-2)	-2(2)
13	12	-0.44(9-I-2)	-0.43(2)	-2.10(9-I-2)	0	-3(8-II-2)	-2(8-II-2)
13	13	1.59(9-I-2)	-0.58(9-I-2)	-2.83(9-I-2)	19(8-I-2)	-4(8-II-2)	-2(2)
13	14	-0.95(9-I-2)	-1.70(9-I-2)	-1.86(9-I-2)	0	3(8-II-2)	-2(8-II-2)
13	15	1.69(9-I-2)	-0.60(2)	-2.63(9-I-2)	11(8-I-2)	3(8-I-2)	-2(8-II-2)
13	16	7.68(2)	-7.15(2)	1.31(2)	420(8-I-2)	-41(2)	-7(2)
13	17	5.55(9-I-2)	-4.96(2)	-1.11(9-I-2)	217(8-I-2)	-39(8-II-2)	-4(8-I-2)
13	18	-2.96(9-II-3)	-7.56(2)	0.81(2)	326(8-I-2)	-37(8-II-2)	-6(8-I-2)
13	19	4.49(9-I-2)	-2.07(9-II-2)	-1.89(9-I-2)	119(8-I-2)	-36(8-II-2)	-3(8-I-2)
13	20	1.60(9-I-3)	-1.69(2)	1.37(9-II-2)	183(8-I-2)	-41(8-II-2)	-4(8-I-2)
13	21	3.53(9-I-2)	-0.15(9-II-2)	-2.26(9-I-2)	65(8-I-2)	-26(8-II-2)	-2(2)
13	22	2.58(9-I-2)	-0.31(9-II-2)	-2.02(9-I-2)	112(8-I-2)	-32(8-II-2)	-3(8-I-2)
13	23	2.82(9-I-2)	-0.12(9-II-2)	-2.44(9-I-2)	35(8-I-2)	-17(8-II-2)	-1(2)
13	24	2.59(9-I-2)	-0.21(2)	-2.23(9-I-2)	70(8-I-2)	-22(8-II-2)	-2(8-I-3)
13	25	-0.88(2)	-2.21(9-I-2)	-1.62(9-I-2)	0	3(8-II-2)	-3(8-II-2)
13	26	1.07(9-I-3)	-0.73(9-II-2)	-2.18(9-I-2)	6(8-I-2)	3(8-II-2)	-2(8-II-2)
13	27	2.20(9-I-2)	-0.10(9-II-2)	-2.54(9-I-2)	19(8-I-2)	12(8-I-2)	-1(9-II-3)
13	28	2.48(9-I-2)	-0.29(2)	-2.37(9-I-2)	43(8-I-2)	-15(8-II-2)	-1(9-II-2)
13	29	1.38(9-I-2)	-1.73(9-I-2)	-2.42(9-I-2)	11(8-I-2)	11(8-I-2)	-2(8-II-2)
13	30	2.31(9-I-2)	-0.45(2)	-2.48(9-I-2)	26(8-I-2)	12(8-I-2)	-2(9-II-3)
13	31	-1.30(9-II-2)	-2.33(2)	-1.95(9-I-2)	7(8-I-2)	11(8-I-2)	-2(8-II-2)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
13	32	3.30(9-I-2)	-0.89(2)	-2.11(9-I-2)	17(8-I-2)	12(8-I-2)	-2(8-II-2)
13	33	1.30(9-I-3)	-0.88(2)	-1.82(9-I-2)	9(8-I-2)	10(8-I-2)	-2(8-II-2)
13	34	-0.38(2)	-2.32(9-II-2)	-1.63(9-I-2)	0	3(8-II-2)	-3(8-II-2)
13	35	0.61(9-I-2)	-1.32(9-II-2)	-1.65(9-I-2)	0	7(2)	-3(8-II-2)
13	36	0.81(9-I-3)	-0.97(9-I-2)	2.05(9-II-2)	2(8-I-3)	6(2)	-3(8-II-2)
13	37	0.98(9-I-2)	-1.05(9-II-2)	1.95(9-II-2)	3(8-I-3)	10(8-I-2)	-2(8-II-2)
13	38	0.81(2)	-0.51(2)	-1.72(9-I-2)	0	13(2)	-3(8-II-2)
13	39	-0.70(9-II-2)	-0.85(2)	-2.22(9-I-2)	3(8-II-2)	10(2)	-2(8-II-2)
13	40	1.05(2)	-0.63(2)	-1.77(9-I-2)	0	25(2)	-3(8-II-2)
13	41	-0.48(9-II-3)	-0.98(2)	-2.33(9-I-2)	7(2)	18(2)	-2(8-II-2)
13	42	1.18(2)	-0.33(8-II-3)	-1.80(9-I-2)	0	51(2)	-4(2)
13	43	-0.30(9-II-3)	-1.04(2)	-2.42(9-I-2)	19(2)	34(2)	-2(8-II-2)
13	44	-2.96(2)	0.64(9-II-3)	-1.55(9-I-2)	0	50(2)	5(2)
13	45	0.46(2)	1.41(2)	-2.35(9-I-2)	29(2)	69(2)	1(8-I-2)
13	46	-1.32(2)	-0.49(8-I-3)	1.49(9-II-2)	0	25(2)	4(2)
13	47	0.41(2)	0.28(2)	-2.01(9-I-2)	21(2)	34(2)	2(8-I-2)
13	48	-0.65(9-II-2)	-0.64(9-II-2)	1.68(9-II-2)	0	14(2)	3(2)
13	49	0.81(9-II-2)	-0.24(9-II-2)	2.10(9-II-2)	10(2)	18(2)	2(2)
13	50	-0.09(8-I-3)	-0.65(9-I-2)	1.82(9-II-2)	0	8(2)	3(2)
13	51	0.86(9-II-2)	-0.45(9-II-2)	2.36(9-II-2)	6(9-II-3)	10(2)	2(2)
13	52	1.03(9-II-2)	-2.09(9-II-2)	1.76(9-II-2)	0	5(9-I-3)	3(2)
13	53	0.25(9-II-2)	-2.10(9-I-2)	1.84(9-II-2)	0	5(9-I-3)	3(2)
13	54	-0.86(9-I-2)	-0.91(9-II-2)	2.36(9-II-2)	6(9-II-3)	6(8-II-3)	2(2)
13	55	0.69(9-I-3)	-0.17(2)	-2.06(9-I-2)	3(9-II-3)	12(2)	-2(8-II-2)
13	56	1.00(9-I-3)	-0.69(2)	2.00(9-II-2)	6(2)	11(2)	-2(8-II-2)
13	57	0.58(2)	-0.26(2)	-2.16(9-I-2)	7(2)	16(2)	-2(8-II-2)
13	58	-0.70(9-II-3)	-0.75(2)	-2.02(9-I-2)	11(2)	14(2)	-2(8-II-2)
13	59	0.35(2)	-0.15(2)	-2.25(9-I-2)	19(2)	22(2)	2(8-I-2)
13	60	-0.42(9-II-3)	-0.86(2)	-2.10(9-I-2)	19(2)	20(2)	2(8-I-2)
13	61	-0.59(2)	-0.60(9-I-2)	-2.17(9-I-2)	29(2)	25(2)	1(8-I-2)
13	62	0.15(8-II-3)	-0.16(8-II-3)	-2.14(9-I-2)	28(2)	24(2)	2(8-I-2)
13	63	-0.72(2)	-0.90(9-I-3)	-1.88(9-I-2)	21(2)	24(2)	1(8-I-2)
13	64	0.63(2)	0.66(2)	-1.93(9-I-2)	29(2)	25(2)	1(8-I-2)
13	65	-0.61(2)	-1.52(9-II-2)	1.97(9-II-2)	10(2)	19(2)	2(2)
13	66	1.07(9-II-2)	-0.38(8-I-3)	1.68(9-II-2)	24(2)	23(2)	1(8-I-2)
13	67	-0.30(2)	-0.64(9-II-2)	2.25(9-II-2)	6(9-II-3)	14(2)	2(2)
13	68	1.60(9-II-2)	-0.57(9-II-2)	2.10(9-II-2)	15(2)	17(2)	1(8-I-2)
13	69	0.64(9-II-2)	0.14(9-II-2)	2.27(9-II-2)	-6(9-I-3)	8(2)	2(2)
13	70	-1.23(9-I-2)	-0.28(2)	2.27(9-II-2)	12(9-II-3)	11(2)	1(2)
13	71	-1.39(9-I-2)	-0.39(2)	2.20(9-II-2)	11(9-II-3)	7(8-II-3)	2(2)
13	72	5.12(9-I-2)	-5.65(2)	0.84(2)	310(8-I-2)	26(8-I-2)	-4(2)
13	73	1.79(9-I-3)	-4.41(2)	0.98(2)	252(8-I-2)	-8(8-I-3)	-6(8-II-2)
13	74	5.32(9-I-2)	-5.74(9-II-2)	1.28(9-II-2)	181(8-I-2)	34(8-I-2)	-3(8-I-2)
13	75	0.79(9-I-3)	-5.89(2)	0.86(9-II-2)	160(8-I-2)	33(8-I-2)	-4(9-I-1)
13	76	4.12(9-I-2)	0.32(9-I-2)	-1.87(9-I-2)	112(8-I-2)	-24(8-II-2)	-3(8-I-2)
13	77	-3.57(9-II-2)	-1.29(9-II-2)	1.90(9-II-2)	129(8-I-2)	29(8-I-2)	-5(8-I-2)
13	78	3.68(9-I-2)	0.18(9-I-2)	-2.05(9-I-2)	70(8-I-2)	-16(8-II-2)	-2(8-I-2)
13	79	4.31(9-I-2)	-0.33(9-II-2)	-1.96(9-I-2)	104(8-I-2)	-22(8-II-2)	-4(8-I-2)
13	80	3.25(9-I-2)	0.11(9-I-2)	-2.16(9-I-2)	43(8-I-2)	11(8-I-2)	-1(8-I-3)
13	81	4.46(9-I-2)	-0.24(9-II-2)	-2.03(9-I-2)	80(8-I-2)	15(8-I-2)	-2(8-I-3)
13	82	2.76(9-I-2)	0.10(9-I-2)	-2.24(9-I-2)	26(8-I-2)	10(8-I-2)	-2(9-II-3)
13	83	4.24(9-I-2)	-0.26(2)	-2.06(9-I-2)	57(8-I-2)	12(8-I-2)	-1(9-II-2)
13	84	-1.31(9-II-3)	-4.43(9-I-2)	-1.87(9-I-2)	17(8-I-2)	21(8-I-2)	-2(9-II-3)
13	85	3.82(9-I-2)	-0.66(2)	-2.13(9-I-2)	34(8-I-2)	16(8-I-2)	2(9-I-3)
13	86	-2.33(9-II-2)	-2.84(9-II-2)	1.50(9-II-2)	9(8-I-2)	21(8-I-2)	-2(8-II-2)
13	87	4.56(9-I-2)	-1.61(2)	-1.04(9-I-2)	17(8-I-3)	21(8-I-2)	-2(9-II-3)
13	88	5.13(9-I-2)	-4.29(9-II-2)	0.86(9-II-2)	232(8-I-2)	-5(9-II-2)	-9(8-II-2)
13	89	7.79(9-I-2)	-8.54(9-II-2)	1.41(9-II-2)	157(8-I-2)	42(9-I-3)	-3(2)
13	90	4.59(9-I-2)	-5.91(2)	1.68(9-II-2)	61(2)	19(9-I-3)	-5(8-II-2)
13	91	7.10(9-I-2)	1.05(9-II-2)	2.19(9-II-2)	128(8-I-2)	-11(8-II-3)	-4(8-I-2)
13	92	21.22(9-I-2)	-6.02(9-II-2)	3.17(9-II-2)	92(8-I-2)	19(8-I-2)	-8(9-I-3)
13	93	6.75(9-I-2)	0.22(9-II-2)	-1.92(9-I-2)	104(8-I-2)	-4(8-II-2)	-3(8-I-2)
13	94	17.57(9-I-2)	-0.98(9-II-2)	-1.83(9-I-2)	114(8-I-2)	-7(8-II-2)	-4(8-I-2)
13	95	6.16(9-I-2)	0.11(9-II-2)	-1.75(9-I-2)	80(8-I-2)	-2(8-II-2)	-2(8-I-3)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
13	96	13.98(9-I-2)	-0.33(9-II-2)	-1.51(9-I-2)	110(8-I-2)	6(8-I-2)	-3(8-I-2)
13	97	5.38(9-I-2)	0.10(9-II-2)	-1.65(9-I-2)	57(8-I-2)	2(8-I-2)	-1(9-II-2)
13	98	10.72(9-I-2)	-0.22(9-II-2)	-1.36(9-I-2)	92(8-I-2)	5(8-I-2)	-2(8-I-3)
13	99	4.43(9-I-2)	0.22(2)	-1.66(9-I-2)	34(8-I-2)	-3(9-I-2)	3(9-I-3)
13	100	7.71(9-I-2)	-0.24(2)	-1.31(9-I-2)	65(8-I-2)	5(8-I-2)	-1(9-II-3)
13	101	-2.59(9-II-2)	-7.16(9-I-2)	-0.61(9-I-2)	18(8-I-3)	44(8-I-2)	-2(9-II-3)
13	102	-5.28(9-II-2)	-2.37(9-I-2)	-1.65(9-I-2)	28(8-I-2)	27(8-I-2)	6(9-I-3)
13	103	3.91(9-I-2)	-6.05(9-II-2)	0.13(9-I-2)	-10(8-II-3)	38(8-I-2)	-2(9-II-2)
13	104	-5.49(9-II-2)	-2.93(9-II-2)	1.21(9-II-2)	16(8-I-3)	31(8-I-2)	-4(2)
13	105	1.46(9-I-2)	0.09(2)	1.72(9-II-2)	6(2)	7(2)	-2(8-II-2)
13	106	1.51(9-I-2)	-0.81(2)	1.60(9-II-2)	9(2)	14(8-I-2)	-1(2)
13	107	3.06(9-I-2)	0.19(9-I-2)	1.12(9-II-2)	9(2)	0	-2(2)
13	108	0.96(9-I-3)	0.02(9-II-3)	-1.72(9-I-2)	11(2)	8(2)	1(8-I-2)
13	109	-1.13(9-II-2)	-0.52(2)	1.52(9-II-2)	18(2)	8(2)	-1(8-II-2)
13	110	0.50(8-II-3)	-0.04(2)	-1.82(9-I-2)	19(2)	9(2)	2(8-I-2)
13	111	-0.63(9-II-3)	-0.59(2)	-1.58(9-I-2)	25(2)	9(2)	2(8-I-2)
13	112	0.25(9-II-2)	0.06(9-I-2)	-1.88(9-I-2)	28(2)	11(2)	2(8-I-2)
13	113	-0.36(9-I-2)	-0.36(2)	-1.66(9-I-2)	28(2)	10(2)	2(8-I-2)
13	114	-1.05(9-I-2)	-1.89(9-I-2)	-1.70(9-I-2)	29(2)	17(2)	1(8-I-2)
13	115	-0.82(9-I-2)	0.40(9-II-2)	-1.73(9-I-2)	28(2)	13(2)	2(8-I-2)
13	116	-0.98(9-I-2)	-1.73(2)	1.41(9-II-2)	24(2)	22(2)	1(8-I-2)
13	117	0.73(9-II-2)	-0.70(9-I-3)	-1.26(9-I-2)	24(2)	19(2)	2(8-I-2)
13	118	-0.83(9-I-2)	-2.33(9-II-2)	1.92(9-II-2)	15(2)	16(2)	1(8-I-2)
13	119	3.84(9-II-2)	-1.18(9-II-2)	1.45(9-II-2)	20(8-II-2)	19(2)	0
13	120	1.55(9-II-2)	0.26(9-II-2)	2.09(9-II-2)	12(9-II-3)	8(2)	1(2)
13	121	-2.81(9-I-2)	-0.54(9-II-2)	2.00(9-II-2)	18(9-II-3)	12(2)	0
13	122	2.10(9-II-2)	0.16(9-II-2)	2.04(9-II-2)	11(9-II-3)	5(9-I-2)	2(2)
13	123	-3.25(9-I-2)	-0.26(2)	1.92(9-II-2)	18(9-II-3)	7(2)	1(2)
13	124	1.70(9-I-2)	0.14(2)	1.01(9-II-2)	18(2)	2(2)	-1(9-II-3)
13	125	-3.27(9-II-2)	-0.35(2)	0.80(9-II-2)	23(2)	4(8-I-2)	0
13	126	0.74(8-II-3)	0.12(2)	-1.03(9-I-2)	25(2)	1(2)	1(9-I-3)
13	127	-1.56(9-II-2)	-0.28(2)	-0.72(9-I-2)	33(2)	3(2)	1(9-I-3)
13	128	0.45(9-II-2)	0.08(2)	-1.10(9-I-2)	28(2)	2(2)	2(9-I-3)
13	129	-0.62(8-I-2)	-0.25(2)	-0.78(9-I-2)	36(2)	2(2)	2(9-I-3)
13	130	-1.46(9-I-2)	0.44(9-I-2)	-1.21(9-I-2)	28(2)	0	2(8-I-2)
13	131	-2.19(9-I-2)	-0.20(9-I-2)	-0.86(9-I-2)	33(2)	2(2)	2(8-I-2)
13	132	-3.18(9-I-2)	-5.76(9-I-2)	-0.77(9-I-2)	24(2)	32(2)	2(9-I-3)
13	133	-4.18(9-I-2)	-1.55(9-I-2)	-1.19(9-I-2)	24(8-II-2)	15(2)	5(2)
13	134	-1.63(9-I-2)	-7.56(9-II-2)	0.99(9-II-2)	20(2)	29(2)	0
13	135	3.14(9-II-2)	-1.21(2)	0.48(9-I-2)	13(8-II-2)	28(2)	0
13	136	-3.39(9-I-2)	0.63(9-II-2)	1.50(9-II-2)	18(9-II-3)	2(9-I-2)	0
13	137	-4.16(9-I-2)	-2.05(9-II-2)	1.51(9-II-2)	26(9-II-3)	14(2)	-3(2)
13	138	4.83(9-II-2)	0.46(9-II-2)	1.40(9-II-2)	18(9-II-3)	2(2)	0
13	139	-6.20(9-I-2)	-0.65(9-II-2)	1.20(9-II-2)	25(9-II-3)	3(2)	0
13	140	-8.73(9-I-2)	-0.71(9-II-2)	1.36(9-II-2)	23(9-II-3)	0	0
13	141	11.44(9-II-2)	0.79(9-II-2)	1.31(9-II-2)	23(9-II-3)	0	2(2)
13	142	1.38(9-II-2)	-0.36(2)	1.43(9-II-2)	0	-5(9-I-3)	3(2)
13	143	-0.32(2)	-0.74(9-I-2)	2.09(9-II-2)	5(9-II-3)	4(9-I-3)	3(2)
13	144	1.45(9-II-2)	0.61(9-II-2)	2.07(9-II-2)	5(9-II-3)	7(9-I-2)	2(2)
13	145	1.81(9-II-2)	-1.73(9-I-2)	-1.03(9-I-2)	0	-9(8-I-3)	4(2)
13	146	-0.29(9-II-3)	-0.55(2)	1.65(9-II-2)	9(2)	-6(8-I-3)	3(2)
13	147	-1.10(9-II-3)	-0.97(8-I-3)	-0.44(8-II-3)	0	-24(8-I-3)	6(2)
13	148	-1.25(9-I-2)	-1.89(9-I-2)	-0.54(9-I-2)	0	-27(8-I-3)	5(2)
13	149	-0.35(8-II-3)	-0.69(2)	-0.99(9-I-2)	17(2)	-11(8-I-3)	3(2)
13	150	-0.66(9-I-2)	0.56(8-I-3)	0.58(9-II-2)	19(2)	-24(2)	7(2)
13	151	1.86(9-II-2)	-2.19(9-I-2)	1.62(9-II-2)	7(2)	8(9-I-2)	2(2)
13	152	-1.08(9-I-2)	-0.47(2)	1.91(9-II-2)	10(9-II-3)	7(9-I-2)	2(2)
13	153	-0.87(9-I-2)	-0.81(2)	0.63(8-I-3)	38(2)	-8(8-I-3)	4(2)
13	154	-1.40(9-I-2)	-2.02(9-I-2)	0.90(9-II-2)	14(2)	-11(8-I-3)	3(2)
13	155	-0.29(8-II-3)	-0.79(9-I-2)	1.24(9-II-2)	23(2)	8(8-II-3)	2(2)
13	156	-1.43(9-I-2)	-0.46(8-I-3)	0.69(9-II-2)	42(2)	-8(2)	4(2)
13	157	-1.78(9-I-2)	-1.00(2)	0.61(8-I-3)	50(2)	7(8-II-3)	3(2)
13	158	2.79(9-II-2)	-1.27(8-I-3)	0.69(9-II-2)	41(2)	-3(9-II-2)	3(8-I-3)
13	159	2.40(9-II-2)	1.15(9-II-2)	1.82(9-II-2)	10(9-II-3)	8(9-I-2)	2(2)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
13	160	-3.83(9-I-2)	-0.49(9-I-2)	1.89(9-II-2)	17(9-II-2)	6(9-I-2)	2(2)
13	161	5.42(9-II-2)	0.17(9-I-2)	1.70(9-II-2)	17(9-II-3)	2(9-I-2)	2(2)
13	162	3.89(9-II-2)	-0.96(2)	0.65(9-II-2)	26(2)	18(9-I-3)	3(8-I-3)
13	163	2.79(9-II-2)	-0.70(2)	0.60(8-I-3)	29(2)	11(9-I-2)	2(9-II-2)
13	164	-2.81(9-I-2)	-4.18(9-I-2)	1.02(9-II-2)	19(2)	14(9-I-2)	2(2)
13	165	-1.63(9-I-2)	-1.28(9-I-2)	-1.61(9-I-2)	16(9-II-2)	10(9-I-2)	2(2)
13	166	6.84(9-II-2)	-1.98(9-I-2)	-1.74(9-I-2)	15(9-II-2)	6(9-I-2)	2(2)
13	167	13.43(9-II-2)	-0.77(9-I-2)	1.55(9-II-2)	24(9-II-2)	4(9-I-2)	2(2)
13	168	15.56(9-II-2)	-8.61(9-I-2)	-2.11(9-I-2)	-26(9-I-2)	23(9-I-2)	3(2)
13	169	-4.16(9-I-2)	-1.92(9-I-3)	0.71(9-II-2)	23(2)	-20(8-I-3)	2(9-II-2)
13	170	3.77(9-II-2)	-0.84(2)	-0.99(9-I-2)	16(9-II-2)	17(9-I-2)	1(9-II-1)
13	171	5.33(9-II-2)	-1.73(9-I-3)	0.99(9-II-2)	12(9-II-2)	-9(9-II-2)	4(8-I-3)
13	172	13.96(9-I-2)	-4.79(9-II-2)	3.93(9-II-2)	39(2)	-9(9-II-2)	6(8-I-2)
13	173	-3.73(9-II-2)	-8.61(9-II-2)	5.03(9-II-2)	20(8-II-3)	26(2)	5(8-I-2)
13	174	-1.48(9-I-2)	-4.03(2)	5.25(9-II-2)	9(8-II-2)	-3(8-I-4)	7(8-I-2)
13	175	-2.69(9-II-2)	-7.19(2)	4.41(9-II-2)	9(8-II-2)	14(8-II-3)	7(8-I-2)
13	176	-2.22(2)	-11.59(9-II-2)	-1.33(9-I-2)	-11(8-II-3)	76(8-I-2)	0
13	177	-0.39(9-II-2)	-16.31(9-I-2)	-1.36(9-I-2)	0	76(8-I-2)	2(9-II-1)
13	178	-0.49(9-I-2)	-7.61(2)	-2.11(9-I-2)	0	41(8-I-2)	2(8-II-3)
13	179	0.13(9-I-2)	-12.07(9-I-2)	-1.70(9-I-2)	0	42(8-I-2)	2(8-II-3)
13	180	1.52(9-II-2)	-5.99(9-I-2)	4.71(9-II-2)	-4(9-I-3)	-5(9-I-2)	6(9-I-3)
13	181	-4.48(9-II-2)	-8.13(9-I-2)	3.58(9-II-2)	-8(9-I-2)	-13(9-I-3)	6(9-I-3)
13	182	-0.09(9-I-2)	-7.97(2)	-2.00(9-I-2)	0	16(8-I-3)	2(8-II-3)
13	183	0.02(9-I-2)	-8.27(2)	-1.88(9-I-2)	0	17(8-I-3)	2(8-II-3)
13	184	-1.77(2)	-13.63(9-II-2)	1.06(9-II-2)	13(8-II-2)	56(2)	0
13	185	-0.36(9-II-2)	-10.43(9-I-2)	1.26(9-II-2)	0	54(2)	0
13	186	-0.45(9-I-2)	-9.75(9-II-2)	2.01(9-II-2)	0	30(2)	0
13	187	0.13(9-I-2)	-6.64(9-I-2)	1.66(9-II-2)	0	31(2)	-1(8-I-3)
13	188	-0.09(9-I-2)	-4.91(9-II-2)	1.94(9-II-2)	0	12(8-I-3)	-1(8-I-3)
13	189	0.01(9-I-2)	-4.54(2)	1.85(9-II-2)	0	12(8-I-3)	-1(8-I-3)
13	190	-0.94(9-I-2)	-6.89(9-I-2)	2.59(9-II-2)	-4(8-I-1)	-6(9-I-2)	5(8-I-2)
13	191	-1.29(9-II-2)	-11.93(9-I-2)	2.01(9-II-2)	-11(8-I-4)	-15(9-I-3)	4(8-II-2)
13	192	0.05(9-I-2)	-8.53(9-I-2)	-1.83(9-I-2)	0	-23(9-I-3)	2(8-II-3)
13	193	-0.12(9-I-2)	-7.95(2)	-2.05(9-I-2)	0	-23(9-I-3)	2(8-II-3)
13	194	1.10(9-II-2)	-7.26(9-I-2)	2.15(9-II-2)	10(9-I-1)	-8(8-II-4)	4(8-II-2)
13	195	-0.73(9-II-2)	-14.71(9-I-2)	-1.82(9-I-2)	14(9-I-2)	-29(9-I-1)	3(8-II-2)
13	196	-1.29(9-I-2)	-9.61(9-I-2)	-2.09(9-I-2)	14(9-I-2)	35(8-I-1)	3(8-II-2)
13	197	-0.59(9-I-2)	-17.00(9-I-2)	-1.70(9-I-2)	0	-63(8-II-1)	0
13	198	0.17(9-I-2)	-13.61(9-I-2)	-1.64(9-I-2)	0	-51(9-I-3)	2(8-II-3)
13	199	-0.39(9-I-2)	-9.07(9-II-2)	-2.17(9-I-2)	0	-50(8-I-2)	1(8-II-3)
13	200	0.35(9-I-2)	-18.12(9-I-2)	-1.33(9-I-2)	0	-73(8-I-2)	4(9-II-2)
13	201	0.18(2)	-13.38(9-II-2)	-1.65(9-I-2)	0	-73(8-I-2)	3(9-II-2)
13	202	-0.05(9-II-2)	-4.16(2)	1.77(9-II-2)	0	-22(8-II-3)	-1(8-I-3)
13	203	0.12(9-II-2)	-7.07(9-II-2)	2.02(9-II-2)	0	-22(8-II-3)	-1(8-I-3)
13	204	-0.17(9-II-2)	-8.58(9-I-2)	1.59(9-II-2)	0	-40(9-II-3)	-1(8-I-3)
13	205	0.39(9-II-2)	-12.02(9-II-2)	2.13(9-II-2)	0	-39(8-II-2)	0
13	206	-0.35(9-II-2)	-12.86(9-I-2)	1.28(9-II-2)	0	-57(9-II-3)	-2(9-I-2)
13	207	0.22(2)	-16.39(9-II-2)	1.62(9-II-2)	0	-59(9-I-3)	2(9-II-2)
13	208	4.44(9-II-2)	-4.81(9-II-2)	2.29(9-II-2)	13(9-II-2)	23(9-I-2)	-4(8-II-3)
13	209	-12.72(9-I-2)	-4.02(9-I-2)	-2.36(9-I-2)	-30(9-I-2)	23(9-I-2)	-2(9-I-1)
13	210	-2.89(9-I-2)	-8.69(9-I-2)	-3.42(9-I-2)	-14(9-I-2)	23(9-I-2)	-3(9-I-2)
13	211	-2.26(9-I-2)	-3.61(9-I-2)	3.06(9-II-2)	-14(9-I-2)	-18(9-II-2)	-5(8-II-3)
13	212	-0.82(8-II-3)	-2.85(9-I-3)	4.30(9-II-2)	-14(9-I-2)	-11(9-II-2)	-5(8-II-3)
13	213	-0.57(9-I-2)	-2.36(8-I-3)	4.64(9-II-2)	-20(9-I-2)	5(9-I-3)	-4(8-II-3)
13	214	-1.05(9-II-2)	-2.65(8-I-3)	3.66(9-II-2)	-2(9-II-2)	-7(9-II-2)	-3(2)
13	215	1.76(9-II-2)	-4.31(9-I-2)	3.23(9-II-2)	0	-4(2)	-2(2)
13	216	-1.96(9-II-2)	-4.15(9-II-2)	3.19(9-II-2)	-4(9-I-2)	-15(9-I-2)	-2(9-II-2)
13	217	0.56(9-I-2)	-2.85(8-I-3)	4.83(9-II-2)	-8(2)	-3(2)	-3(8-II-3)
13	218	-0.30(9-II-2)	-4.11(8-I-3)	4.77(9-II-2)	-11(9-I-3)	-9(9-I-2)	-3(8-II-3)
13	219	0.88(9-II-2)	-3.95(9-II-2)	3.61(9-II-2)	-1(9-I-3)	-11(9-I-2)	-2(9-II-2)
13	220	-0.88(9-II-2)	-10.16(9-II-2)	3.00(9-II-2)	-7(9-I-2)	-22(9-I-2)	-3(9-II-2)
13	221	-0.22(9-I-2)	-3.69(8-I-3)	4.78(9-II-2)	-12(9-I-3)	-6(9-I-2)	3(8-I-3)
13	222	0.20(8-I-3)	-4.19(8-I-3)	4.67(9-II-2)	-18(9-I-3)	-20(8-II-3)	2(9-I-3)
13	223	0.25(9-II-2)	-7.52(9-II-2)	3.68(9-II-2)	-3(8-I-3)	-20(8-II-3)	-3(9-II-2)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
13	224	-0.13(8-II-3)	-16.30(9-II-2)	2.98(9-II-2)	-6(8-II-3)	-30(8-II-3)	-3(9-II-2)
13	225	-0.52(9-I-2)	-5.17(8-I-3)	4.46(9-II-2)	-16(9-I-3)	-15(9-I-2)	2(9-I-3)
13	226	-0.62(9-II-2)	-3.08(8-I-3)	3.98(9-II-2)	-10(9-I-3)	56(8-I-3)	-2(9-II-2)
13	227	-0.34(9-II-2)	-12.69(9-II-2)	3.34(9-II-2)	-2(9-I-3)	56(8-I-3)	-3(9-II-2)
13	228	-0.62(9-II-2)	-21.49(9-II-2)	2.56(9-II-2)	0	53(8-I-3)	-2(9-II-2)
13	229	-0.74(2)	-8.62(8-I-3)	2.72(9-II-2)	0	51(8-I-3)	-2(9-II-2)
14	1	-0.68(9-II-3)	-1.01(2)	0.70(9-II-4)	0	-16(9-II-1)	0
14	2	0.19(9-I-1)	-1.28(2)	0.84(9-II-4)	17(9-II-4)	-10(9-II-1)	-2(9-II-4)
14	3	-0.23(8-II-3)	-1.11(2)	0.91(9-II-4)	17(9-II-4)	8(8-II-3)	-2(9-II-4)
14	4	-1.51(9-II-3)	-0.74(9-I-1)	1.19(9-II-4)	0	-7(9-II-1)	-1(9-I-4)
14	5	1.06(9-II-4)	-1.32(9-II-4)	1.12(9-II-4)	8(9-II-4)	-14(9-II-1)	-1(9-I-1)
14	6	0.47(9-I-3)	-2.31(9-II-4)	1.59(9-II-4)	0	-7(9-II-1)	-2(9-I-4)
14	7	-1.17(9-II-3)	-3.41(9-II-3)	1.37(9-II-4)	10(9-II-4)	9(9-I-2)	-2(9-I-1)
14	8	1.37(9-II-3)	-1.15(2)	1.01(9-II-4)	33(9-II-4)	8(9-II-3)	0
14	9	0.49(9-I-4)	-0.84(9-I-4)	1.92(9-II-4)	4(9-II-4)	-3(8-I-3)	-2(9-I-4)
14	10	-1.06(9-I-4)	-1.11(9-II-4)	2.07(9-II-4)	11(9-II-4)	7(9-I-2)	-2(9-I-1)
14	11	-1.03(9-II-3)	-2.99(9-II-3)	1.05(9-II-4)	33(9-II-4)	16(8-II-3)	0
14	12	0.97(9-I-1)	-1.17(9-I-1)	1.07(9-II-4)	49(9-II-4)	29(9-II-4)	-3(9-II-4)
14	13	-2.65(9-II-4)	-1.54(9-I-1)	2.23(9-II-4)	49(9-II-4)	38(9-II-4)	-3(9-II-4)
14	14	-1.19(9-II-4)	-5.23(9-II-3)	2.56(9-II-4)	17(9-II-4)	37(9-II-3)	-4(9-II-4)
14	15	0.62(9-I-4)	-0.18(9-II-4)	2.04(9-II-4)	11(9-II-4)	2(8-II-3)	-2(9-I-1)
14	16	-4.07(9-II-4)	-4.62(9-II-4)	2.33(9-II-4)	41(9-II-4)	13(8-II-3)	-3(8-II-3)
14	17	1.30(9-I-4)	-0.70(9-II-4)	1.84(9-II-4)	15(9-II-3)	3(8-II-3)	-2(9-I-4)
14	18	0.21(9-II-4)	-1.18(9-II-4)	1.97(9-II-4)	5(9-I-4)	-3(8-I-3)	-2(9-I-4)
14	19	1.00(9-II-4)	-1.82(9-I-4)	1.39(9-II-4)	0	-3(9-I-3)	-2(9-I-4)
14	20	-0.21(2)	-0.82(9-I-4)	2.03(9-II-4)	9(9-I-1)	-6(8-I-3)	-2(9-I-4)
14	21	0.54(9-II-4)	0.41(9-II-4)	1.99(9-II-4)	9(9-I-1)	2(8-II-3)	-2(9-I-4)
14	22	2.01(9-II-4)	-2.01(9-I-4)	-0.84(9-I-4)	0	6(9-II-3)	-1(9-I-4)
14	23	-1.06(9-II-4)	-0.59(9-II-4)	1.37(9-II-4)	12(9-I-1)	3(9-II-3)	-2(9-I-4)
14	24	0.87(9-II-4)	-2.07(9-I-4)	1.51(9-II-4)	12(9-I-1)	-6(8-I-3)	-2(9-I-4)
14	25	-0.90(9-I-4)	0.55(9-II-3)	0.41(9-II-3)	0	-4(9-I-3)	0
14	26	0.88(9-I-4)	-0.48(2)	0.65(9-II-3)	18(9-I-1)	4(9-II-3)	0
14	27	-1.31(9-I-4)	-1.87(9-I-4)	0.69(9-II-3)	18(9-I-1)	12(8-II-3)	0
14	28	-2.21(9-II-4)	-1.22(9-I-4)	-1.26(9-I-4)	29(9-I-1)	-10(8-I-3)	-1(9-I-4)
14	29	0.48(9-I-4)	-1.01(8-I-3)	0.65(9-II-3)	41(9-I-1)	12(9-I-2)	-1(9-II-3)
14	30	1.86(9-II-4)	0.41(9-I-4)	1.84(9-II-4)	29(9-I-1)	0	-2(9-I-4)
14	31	0.37(9-II-4)	-0.95(2)	0.77(9-II-3)	42(9-I-1)	-18(8-I-3)	-1(9-II-3)
14	32	2.00(9-II-4)	-6.28(9-I-4)	1.26(9-II-4)	34(9-I-1)	-21(8-I-3)	-1(8-I-3)
14	33	5.13(9-II-4)	-1.68(9-I-4)	2.14(9-II-4)	48(9-I-1)	6(8-II-3)	-3(8-I-3)
14	34	0.85(8-II-3)	-0.86(9-I-3)	0.90(9-II-3)	51(9-I-4)	24(9-I-2)	-2(9-II-4)
14	35	2.93(9-II-4)	-0.96(9-I-4)	2.09(9-II-4)	51(9-I-4)	34(9-I-1)	-2(9-II-1)
14	36	1.15(9-II-3)	-5.55(9-I-4)	2.49(9-II-4)	18(9-I-4)	36(9-I-1)	-4(9-II-4)
14	37	-0.89(9-II-3)	-1.67(8-II-3)	2.69(9-II-4)	5(9-I-4)	16(9-I-4)	-1(9-II-3)
14	38	0.85(9-II-4)	-2.38(9-I-1)	2.78(9-II-4)	5(9-II-4)	14(9-II-4)	2(9-I-2)
14	39	-0.65(9-II-4)	-3.04(8-II-3)	2.53(9-II-4)	2(9-II-3)	18(9-II-3)	2(9-I-2)
14	40	0.57(9-II-4)	-2.99(9-I-1)	2.92(9-II-4)	0	4(9-I-4)	2(8-II-3)
14	41	-0.07(9-II-1)	-5.60(9-I-1)	2.53(9-II-4)	-6(9-II-1)	-13(9-II-4)	2(9-I-2)
14	42	-0.15(9-II-4)	-3.57(9-I-1)	2.81(9-II-4)	-6(9-II-1)	-19(9-II-4)	3(9-I-2)
14	43	0.90(9-II-4)	-9.14(9-I-4)	2.46(9-II-4)	-25(9-II-4)	-31(9-II-3)	-4(9-II-1)
14	44	3.70(9-II-4)	-4.42(9-I-1)	1.79(9-II-4)	-40(9-II-1)	-37(9-II-4)	-3(9-II-1)
14	45	0.61(9-I-3)	-5.39(9-I-1)	1.16(9-II-4)	-33(9-II-1)	23(8-I-3)	1(9-I-2)
14	46	0.39(9-I-3)	-4.79(9-I-1)	-1.03(9-I-4)	-23(9-II-1)	-19(8-II-3)	1(9-I-1)
14	47	0.53(8-I-3)	-4.76(9-I-1)	-1.09(9-I-4)	-16(9-II-1)	52(9-II-1)	0
14	48	0.33(2)	-6.60(9-I-1)	-0.84(9-I-4)	0	50(9-II-1)	0
14	49	4.02(9-II-4)	-7.71(9-I-4)	2.03(9-II-4)	-16(9-II-4)	27(8-I-3)	3(8-I-3)
14	50	0.50(2)	-6.67(9-I-4)	0.90(9-II-4)	0	52(9-II-1)	1(9-II-4)
14	51	1.44(9-II-4)	-0.73(9-I-4)	1.38(9-II-4)	-25(8-II-3)	13(8-I-3)	2(9-II-4)
14	52	0.60(2)	-1.31(9-I-4)	1.69(9-II-4)	-9(8-II-3)	10(8-I-3)	3(9-II-1)
14	53	-0.81(8-II-3)	-2.77(9-I-4)	1.63(9-II-4)	-9(8-II-3)	42(9-II-2)	3(9-II-1)
14	54	0.67(9-II-3)	-3.08(9-I-1)	2.47(9-II-4)	5(9-I-2)	24(9-I-1)	-2(9-II-3)
14	55	-0.58(9-II-3)	-2.81(8-II-3)	2.83(9-II-4)	2(9-I-2)	10(2)	-2(8-II-3)
14	56	-0.08(8-I-3)	-4.92(9-II-3)	2.46(9-II-4)	6(8-II-3)	15(2)	-3(8-II-3)
14	57	0.12(9-II-3)	-3.90(8-II-3)	2.71(9-II-4)	6(9-II-3)	24(9-II-4)	-3(8-II-3)
14	58	1.52(9-I-4)	-0.35(9-II-4)	1.41(9-II-4)	26(9-II-2)	-9(8-II-3)	2(9-II-3)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
14	59	0.57(2)	-0.19(9-II-4)	1.51(9-II-4)	13(8-I-3)	9(8-I-3)	2(9-II-4)
14	60	-0.65(8-II-3)	-0.29(2)	1.53(9-II-4)	13(9-II-2)	35(8-I-3)	2(9-II-4)
14	61	0.53(2)	-0.48(9-I-4)	0.97(9-II-4)	0	35(8-I-3)	0
14	62	0.54(2)	-2.02(9-II-4)	1.03(9-II-4)	0	-35(8-II-3)	0
14	63	-4.01(9-II-4)	-0.84(9-II-4)	2.03(9-II-4)	20(9-II-1)	-3(8-II-3)	6(8-II-3)
14	64	-0.88(9-II-3)	-8.33(9-II-3)	2.40(9-II-4)	18(9-II-3)	32(9-II-1)	-3(8-II-3)
14	65	0.75(9-I-3)	-6.87(9-II-3)	1.64(9-II-4)	10(9-II-1)	-37(8-II-3)	3(8-II-3)
14	66	1.00(9-II-4)	-2.07(9-II-3)	1.58(9-II-4)	7(9-II-4)	-41(8-II-3)	3(8-II-3)
14	67	-3.57(9-II-4)	-5.18(8-II-3)	1.70(9-II-3)	31(8-II-3)	34(9-II-1)	-2(8-II-3)
14	68	0.82(9-II-4)	-4.77(8-II-3)	1.15(9-II-3)	24(9-II-3)	-28(8-II-3)	0
14	69	0.33(2)	-6.72(9-II-3)	0.91(9-II-4)	0	-57(8-II-3)	0
14	70	0.27(9-II-3)	-6.59(8-II-3)	1.05(9-II-3)	11(8-II-3)	28(8-I-3)	-1(8-II-3)
14	71	-0.47(9-I-1)	-4.62(8-II-3)	1.07(9-II-4)	9(8-II-3)	-56(8-II-3)	0
14	72	0.22(9-I-3)	-8.01(8-II-3)	0.84(9-II-4)	0	-45(8-II-3)	0
15	1	-2.21(9-II-2)	-1.48(9-II-2)	0.78(9-II-2)	0	-24(2)	17(2)
15	2	1.57(9-II-2)	-0.55(9-I-3)	1.32(9-II-2)	181(2)	-96(2)	13(2)
15	3	-2.49(9-II-2)	-2.60(9-II-2)	1.34(9-II-2)	0	-124(2)	28(2)
15	4	-3.09(2)	0.85(9-I-2)	1.82(9-II-2)	0	-276(2)	38(2)
15	5	2.09(9-II-2)	-0.14(8-I-3)	2.21(9-II-2)	14(2)	-193(2)	17(2)
15	6	18.17(2)	-18.32(2)	-1.88(9-I-2)	0	-742(2)	-35(2)
15	7	-12.34(2)	-3.23(9-I-2)	2.27(9-II-2)	0	-730(2)	53(2)
15	8	1.08(9-II-2)	0.81(9-I-2)	2.79(9-II-2)	-151(2)	-361(2)	14(2)
15	9	-0.51(9-II-3)	-1.40(9-II-2)	1.11(9-II-2)	193(2)	-8(2)	7(2)
15	10	0.57(9-II-3)	-4.04(2)	-1.57(9-I-2)	0	-280(2)	-21(2)
15	11	-0.77(9-II-2)	-6.48(2)	-2.24(9-I-2)	-181(2)	-328(2)	-1(9-II-2)
15	12	1.43(9-II-2)	-1.36(2)	-1.90(9-I-2)	-77(2)	-168(2)	-4(2)
15	13	-0.40(9-II-2)	-3.91(9-II-2)	2.14(9-II-2)	25(2)	-102(2)	11(2)
15	14	3.76(9-II-2)	-1.08(9-II-2)	1.48(9-II-2)	175(2)	-69(2)	2(8-II-3)
15	15	-1.02(9-I-2)	-1.17(2)	2.75(9-II-2)	-167(2)	-204(2)	12(2)
15	16	3.21(9-II-2)	0.81(9-I-2)	2.63(9-II-2)	-51(2)	-157(2)	2(9-I-2)
15	17	3.50(2)	-5.63(2)	-2.23(9-I-2)	-202(2)	-221(2)	2(9-I-2)
15	18	-1.65(2)	-8.78(2)	2.47(9-II-2)	-203(2)	-240(2)	5(2)
15	19	1.21(9-II-2)	-4.38(2)	-1.81(9-I-2)	-86(2)	-153(2)	2(9-I-2)
15	20	0.82(9-II-2)	-4.53(2)	-1.83(9-I-2)	-176(2)	-177(2)	8(2)
15	21	-1.66(9-II-2)	-1.95(9-II-2)	-1.52(9-I-2)	0	-133(2)	-15(2)
15	22	-1.79(9-I-2)	1.74(9-I-2)	-2.08(9-I-2)	0	-32(2)	-8(2)
15	23	-0.44(9-II-2)	-2.79(9-I-2)	-2.29(9-I-2)	0	-31(2)	-10(2)
15	24	-2.21(9-I-2)	-0.83(9-I-2)	-1.41(9-I-2)	0	-22(2)	-7(2)
15	25	0.74(9-I-2)	-1.49(9-I-2)	-2.33(9-I-2)	28(2)	-22(2)	-7(2)
15	26	-0.46(9-I-3)	-0.88(9-I-2)	0.90(9-II-2)	0	-11(8-I-3)	-5(2)
15	27	0.51(9-II-2)	-1.28(9-II-2)	1.01(9-II-2)	0	-7(2)	-4(2)
15	28	-0.27(9-I-3)	-1.08(9-I-2)	0.92(9-II-2)	0	-8(2)	-4(2)
15	29	0.63(9-II-2)	-1.19(9-II-2)	1.14(9-II-2)	10(2)	-10(8-I-3)	-4(2)
15	30	0.39(9-II-2)	-1.84(9-I-2)	0.72(9-II-2)	0	-8(9-II-2)	-2(8-II-3)
15	31	1.22(9-II-2)	-1.19(9-II-2)	-2.75(9-I-2)	14(8-I-3)	-54(2)	-8(2)
15	32	-1.71(9-II-2)	-0.69(2)	-1.89(9-I-2)	0	-66(2)	-12(2)
15	33	2.34(9-II-2)	-0.60(9-II-2)	-2.23(9-I-2)	-15(2)	-93(2)	-7(2)
15	34	0.32(2)	-3.83(9-II-2)	-2.22(9-I-2)	-11(8-II-3)	-96(2)	-2(2)
15	35	3.74(9-II-2)	-1.03(2)	-1.89(9-I-2)	-107(2)	-128(2)	4(2)
15	36	0.66(9-II-2)	-0.74(9-II-2)	-2.86(9-I-2)	28(2)	-56(2)	-5(2)
15	37	3.22(9-II-2)	-0.83(9-II-2)	-2.73(9-I-2)	-34(2)	-83(2)	0
15	38	-2.22(9-I-2)	-2.73(9-I-2)	-2.48(9-I-2)	19(2)	-38(2)	-5(2)
15	39	0.64(9-II-2)	-0.38(2)	-3.04(9-I-2)	23(8-I-3)	-46(2)	-3(2)
15	40	0.79(9-II-2)	-1.32(9-I-2)	-2.21(9-I-2)	28(8-I-3)	-31(2)	-4(2)
15	41	-1.40(9-I-2)	-0.91(2)	-1.04(9-I-2)	0	-16(2)	-6(2)
15	42	0.54(2)	-0.84(9-I-2)	-1.57(9-I-2)	23(2)	-17(2)	-5(2)
15	43	-1.79(9-I-2)	-2.09(9-I-2)	-1.71(9-I-2)	19(8-I-3)	-31(2)	-4(2)
15	44	-0.82(9-I-2)	-1.12(9-II-2)	-1.11(9-I-2)	8(8-I-3)	-16(8-I-3)	-4(2)
15	45	0.67(9-II-2)	-0.78(2)	-1.30(9-I-2)	22(2)	-14(8-I-3)	-5(2)
15	46	-0.80(9-I-2)	-1.00(2)	1.23(9-II-2)	11(2)	-20(8-I-3)	-4(2)
15	47	0.95(9-II-2)	-0.83(2)	1.34(9-II-2)	26(2)	-19(8-I-3)	-4(2)
15	48	0.18(9-I-2)	-0.95(2)	1.12(9-II-2)	22(8-II-3)	-12(8-I-3)	-3(8-II-3)
15	49	-0.51(9-I-2)	-1.39(9-I-2)	1.14(9-II-2)	11(2)	-13(8-I-3)	-3(2)
15	50	0.34(8-I-3)	-0.91(2)	1.38(9-II-2)	23(2)	-19(8-I-3)	-3(8-II-3)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
15	51	0.68(9-II-2)	-2.17(9-I-2)	1.15(9-II-2)	33(8-II-3)	-7(8-I-3)	-2(8-II-3)
15	52	-0.76(9-I-2)	-4.78(9-II-2)	1.38(9-II-2)	176(2)	-37(2)	2(9-II-3)
15	53	4.63(9-II-2)	-1.20(8-I-3)	0.96(9-II-2)	229(2)	-3(9-II-2)	-5(2)
15	54	1.42(9-II-2)	-4.15(9-II-2)	2.74(9-II-2)	-51(2)	-59(2)	1(9-I-2)
15	55	6.90(9-II-2)	-1.46(9-II-2)	2.22(9-II-2)	61(2)	-49(2)	-3(2)
15	56	4.40(9-II-2)	-4.24(9-I-2)	-2.60(9-I-2)	-202(2)	-72(2)	4(2)
15	57	-3.55(9-I-2)	-2.49(2)	3.14(9-II-2)	-91(2)	-59(2)	2(9-I-2)
15	58	3.92(9-II-2)	-6.35(9-I-2)	-1.84(9-I-2)	-176(2)	-86(2)	7(2)
15	59	-0.73(9-I-2)	-6.92(2)	-2.45(9-I-2)	-156(2)	-75(2)	4(2)
15	60	-1.70(9-I-2)	-4.79(9-II-2)	-1.73(9-I-2)	-107(2)	-90(2)	5(2)
15	61	3.11(9-II-2)	-3.50(2)	-1.41(9-I-2)	-160(2)	-94(2)	7(2)
15	62	2.92(9-II-2)	-2.76(9-II-2)	0.99(9-II-2)	233(2)	-9(9-II-2)	-6(2)
15	63	1.57(9-II-2)	-8.80(9-II-2)	2.31(9-II-2)	63(2)	-27(2)	-4(2)
15	64	6.44(9-II-2)	-3.37(9-II-2)	1.49(9-II-2)	146(2)	-14(9-II-3)	-8(2)
15	65	4.59(9-II-2)	1.08(2)	3.11(9-II-2)	-91(2)	-7(2)	-2(9-II-2)
15	66	1.68(9-II-2)	-2.89(9-II-2)	3.27(9-II-2)	70(9-I-2)	-10(2)	-2(2)
15	67	3.55(9-II-2)	-6.34(2)	-1.70(9-I-2)	-131(2)	-34(2)	2(2)
15	68	6.20(9-II-2)	-9.48(9-I-2)	-2.61(9-I-2)	-163(2)	-33(2)	3(9-I-2)
15	69	8.54(9-II-2)	-3.87(9-I-2)	-3.32(9-I-2)	-109(2)	-13(2)	-4(9-II-2)
15	70	6.66(9-II-2)	-4.93(2)	-1.72(9-I-2)	-99(2)	-52(2)	3(2)
15	71	1.28(9-II-2)	-4.04(9-II-2)	-2.85(9-I-2)	-30(2)	-52(2)	1(2)
15	72	6.64(9-II-2)	-2.31(9-II-2)	-2.17(9-I-2)	-108(2)	-80(2)	7(2)
15	73	1.96(9-II-2)	-2.56(9-I-2)	-2.51(9-I-2)	28(8-I-3)	-40(2)	-3(2)
15	74	2.76(9-II-2)	-2.84(9-I-2)	-3.11(9-I-2)	25(8-I-3)	-40(2)	-2(2)
15	75	-3.15(9-I-2)	-0.38(9-I-2)	-3.25(9-I-2)	-46(2)	-54(2)	0
15	76	2.04(9-II-2)	-2.57(9-I-2)	-2.21(9-I-2)	31(8-I-3)	-40(2)	-3(2)
15	77	-1.09(9-I-2)	-1.30(2)	-1.42(9-I-2)	17(8-I-3)	-25(2)	-4(2)
15	78	1.03(9-II-2)	-0.92(2)	-1.56(9-I-2)	29(8-I-3)	-26(2)	-4(2)
15	79	-2.11(9-I-2)	-2.31(9-I-2)	-1.66(9-I-2)	30(8-I-3)	-41(2)	-3(2)
15	80	-0.67(9-I-2)	-1.13(2)	1.46(9-II-2)	22(2)	-26(8-I-3)	-3(2)
15	81	1.79(9-II-2)	-0.92(2)	1.48(9-II-2)	29(8-I-3)	-24(8-I-3)	-3(2)
15	82	0.68(9-II-2)	-1.04(2)	1.53(9-II-2)	25(2)	-29(8-I-3)	-3(8-II-3)
15	83	1.45(9-II-2)	-0.93(2)	1.64(9-II-2)	31(2)	-27(8-I-3)	-2(8-II-3)
15	84	0.14(9-I-2)	-0.86(2)	1.45(9-II-2)	47(8-II-3)	-33(8-I-3)	-4(8-II-3)
15	85	0.38(8-I-3)	-0.95(9-I-2)	1.68(9-II-2)	34(2)	-29(8-I-3)	-3(8-II-3)
15	86	0.62(9-II-2)	-4.00(9-I-2)	1.61(9-II-2)	51(8-II-3)	-27(8-I-3)	-4(8-II-3)
15	87	-1.61(9-I-2)	-1.65(9-II-2)	1.73(9-II-2)	31(8-I-3)	-31(2)	-2(2)
15	88	4.61(9-II-2)	-1.13(2)	-1.76(9-I-2)	36(8-I-3)	-33(2)	-1(2)
15	89	2.20(9-II-2)	-8.20(9-II-2)	-2.35(9-I-2)	-105(2)	-54(2)	7(2)
15	90	0.54(2)	-5.16(9-II-2)	-1.79(9-I-2)	-79(2)	-46(2)	6(2)
15	91	4.74(9-II-2)	0.52(9-I-2)	-3.30(9-I-2)	-47(2)	5(2)	1(2)
15	92	3.87(9-II-2)	-1.07(9-II-2)	-3.14(9-I-2)	-139(2)	-41(2)	9(2)
15	93	-5.45(9-I-2)	-6.61(9-I-2)	-2.66(9-I-2)	30(8-I-3)	-51(2)	-2(2)
15	94	-12.42(9-I-2)	-3.00(9-I-2)	-3.52(9-I-2)	-53(2)	-32(2)	-4(2)
15	95	-1.40(9-I-2)	-1.25(8-I-3)	1.96(9-II-2)	31(2)	-29(8-I-3)	-2(2)
15	96	4.04(9-II-2)	-1.04(2)	2.09(9-II-2)	33(8-I-3)	-27(8-I-3)	0
15	97	0.49(9-I-2)	-0.83(2)	2.10(9-II-2)	43(8-II-3)	-38(8-I-3)	-4(8-II-3)
15	98	1.10(9-II-2)	-1.74(9-I-2)	2.06(9-II-2)	34(2)	-44(8-I-3)	-2(8-II-3)
15	99	2.10(9-II-2)	-1.02(2)	2.26(9-II-2)	32(2)	-35(8-I-3)	0
15	100	2.29(9-II-2)	-4.15(9-I-2)	2.41(9-II-2)	36(8-II-3)	-63(8-I-3)	-3(8-II-3)
15	101	-3.69(9-I-2)	-2.20(9-II-2)	-2.24(9-I-2)	35(8-I-3)	-43(2)	0
15	102	-9.29(9-I-2)	-2.80(9-I-2)	-2.47(9-I-2)	37(8-I-3)	-42(2)	0
15	103	-3.09(9-I-2)	-1.83(9-II-2)	2.74(9-II-2)	33(8-I-3)	-28(2)	0
15	104	-7.39(9-I-2)	-1.25(2)	-2.98(9-I-2)	30(8-I-3)	-32(2)	0
15	105	-2.39(9-I-2)	-1.26(2)	2.93(9-II-2)	33(2)	-23(8-I-3)	0
15	106	-3.76(9-I-2)	-1.10(2)	3.24(9-II-2)	29(2)	-24(8-I-3)	1(9-I-2)
15	107	-0.57(8-I-3)	-0.81(2)	3.02(9-II-2)	25(8-II-3)	-34(8-I-3)	0
15	108	-1.99(9-I-2)	-1.60(9-I-2)	3.31(9-II-2)	25(2)	-27(8-I-3)	1(9-I-2)
15	109	0.97(9-II-2)	-3.21(9-I-2)	3.46(9-II-2)	17(2)	-12(9-I-3)	5(9-II-2)
15	110	-4.13(9-II-2)	-4.70(9-II-2)	-2.44(9-I-2)	138(2)	-18(9-II-2)	-8(2)
15	111	-0.72(9-II-2)	-10.88(9-II-2)	3.45(9-II-2)	45(2)	36(9-I-2)	-12(2)
15	112	-0.56(9-I-2)	-3.29(8-I-3)	3.98(9-II-2)	8(2)	-11(9-II-2)	-6(2)
15	113	-1.54(9-I-2)	-12.44(9-I-2)	-3.47(9-I-2)	-31(2)	-23(2)	-3(2)
15	114	-1.66(9-II-2)	-6.20(9-II-2)	3.63(9-II-2)	11(9-I-2)	35(9-I-2)	-5(2)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
15	115	0.40(9-I-2)	-5.58(2)	-3.79(9-I-2)	4(2)	-25(2)	0
15	116	-2.01(9-I-2)	-8.33(2)	-3.48(9-I-2)	4(2)	-11(9-II-3)	0
15	117	-1.31(9-I-2)	-3.01(9-I-3)	-4.17(9-I-2)	4(9-I-2)	-3(2)	-4(8-I-3)
15	118	-2.00(9-II-2)	-3.89(2)	-3.58(9-I-2)	6(8-II-3)	21(9-I-2)	-4(8-I-3)
15	119	1.71(9-I-2)	-7.21(2)	-3.70(9-I-2)	-2(2)	14(8-I-3)	-2(2)
15	120	-1.17(9-I-2)	-5.28(2)	-4.12(9-I-2)	0	15(8-I-3)	-2(2)
15	121	-0.87(9-I-2)	-12.18(9-II-2)	-3.15(9-I-2)	-49(2)	-75(2)	7(2)
15	122	-0.20(9-II-2)	-4.08(2)	-3.81(9-I-2)	10(2)	-24(2)	0
15	123	-7.79(9-I-2)	-10.35(9-I-2)	-4.03(9-I-2)	24(8-I-3)	-60(2)	1(2)
15	124	1.65(9-I-2)	-6.69(9-II-2)	-3.57(9-I-2)	-2(2)	-35(2)	0
15	125	-1.11(9-I-2)	-4.84(2)	-4.11(9-I-2)	0	-15(8-II-3)	-1(2)
15	126	-2.61(9-I-2)	-2.18(9-II-2)	-3.99(9-I-2)	27(8-I-3)	-29(2)	2(2)
15	127	0.38(9-I-2)	-1.77(2)	-3.66(9-I-2)	7(2)	-32(2)	3(2)
15	128	-1.63(9-I-2)	-3.65(9-I-2)	-2.93(9-I-2)	7(8-I-3)	-24(2)	3(2)
15	129	-2.22(9-I-2)	-1.49(2)	3.98(9-II-2)	28(2)	-18(2)	2(9-I-2)
15	130	0.76(9-II-2)	-1.28(2)	-4.10(9-I-2)	14(2)	-23(2)	3(2)
15	131	-1.10(9-I-3)	-1.82(9-I-3)	3.97(9-II-2)	23(2)	-14(8-I-3)	2(9-I-2)
15	132	0.33(9-II-2)	-1.16(2)	4.13(9-II-2)	16(2)	-16(2)	2(8-II-3)
15	133	-0.48(9-I-3)	-2.10(9-I-3)	4.00(9-II-2)	15(9-II-3)	-6(9-I-3)	4(9-II-2)
15	134	0.86(8-I-3)	-1.13(9-I-3)	4.15(9-II-2)	12(2)	-20(9-I-2)	2(9-II-2)
15	135	1.72(9-I-2)	-4.19(2)	-3.69(9-I-2)	0	-18(8-II-3)	-2(2)
15	136	1.05(9-I-2)	-2.84(9-II-2)	-3.32(9-I-2)	2(2)	-20(8-II-3)	3(2)
15	137	-1.84(9-I-2)	-2.65(2)	-2.80(9-I-2)	1(8-I-3)	-24(8-II-3)	3(2)
15	138	-0.29(8-I-3)	-1.91(9-II-2)	-4.06(9-I-2)	14(2)	-14(8-II-3)	3(2)
15	139	1.35(9-II-2)	-1.58(2)	-3.93(9-I-2)	5(8-I-3)	-17(8-II-3)	3(2)
15	140	-0.29(9-I-3)	-1.52(2)	4.16(9-II-2)	15(2)	-15(9-I-2)	3(8-II-3)
15	141	0.30(9-II-2)	-1.28(2)	-4.20(9-I-2)	10(9-II-2)	-13(8-II-3)	3(2)
15	142	-0.89(9-I-3)	-2.24(9-I-3)	4.20(9-II-2)	10(2)	-9(9-II-2)	2(9-II-2)
15	143	0.42(8-I-3)	-1.11(2)	4.20(9-II-2)	12(9-II-2)	-15(9-I-2)	3(8-II-3)
15	144	0.57(9-I-3)	-2.28(9-I-3)	4.24(9-II-2)	10(9-II-2)	-11(8-II-3)	4(9-II-2)
15	145	-1.64(9-I-2)	-4.28(9-I-3)	-4.05(9-I-2)	-6(8-I-3)	-6(9-I-2)	-5(9-II-2)
15	146	-1.95(9-II-2)	-7.32(9-I-2)	-3.48(9-I-2)	-13(8-I-3)	7(2)	-5(9-II-2)
15	147	1.62(9-I-2)	-7.59(9-II-2)	-3.57(9-I-2)	1(2)	30(8-I-3)	-2(2)
15	148	-0.40(9-I-2)	-5.08(2)	-4.02(9-I-2)	1(2)	38(8-I-3)	-2(2)
15	149	-1.78(9-I-2)	-6.50(9-I-3)	-3.91(9-I-2)	-12(8-I-3)	-15(9-I-2)	-6(9-II-2)
15	150	-1.95(9-II-2)	-12.19(9-I-2)	-3.29(9-I-2)	-10(8-I-3)	30(8-I-3)	-5(9-II-2)
15	151	-1.79(9-I-2)	-10.63(9-I-3)	-3.39(9-I-2)	-10(8-I-3)	51(8-I-3)	-5(9-II-2)
15	152	-0.03(9-II-3)	-12.83(9-II-2)	-3.22(9-I-2)	0	47(8-I-3)	-2(2)
15	153	-0.55(2)	-16.22(9-I-2)	-2.57(9-I-2)	0	98(8-I-3)	-2(9-II-2)
15	154	0.28(9-I-2)	-8.75(9-II-2)	-3.55(9-I-2)	0	60(8-I-3)	-1(2)
15	155	-0.19(9-II-2)	-16.97(9-II-2)	-2.59(9-I-2)	0	63(8-I-3)	-1(2)
15	156	-2.01(9-I-2)	-7.34(9-I-2)	-3.45(9-I-2)	0	28(8-I-3)	-2(2)
15	157	0.62(9-I-2)	-5.29(2)	-3.97(9-I-2)	0	37(8-I-3)	-3(2)
15	158	1.44(9-I-2)	-8.00(9-II-2)	-2.79(9-I-2)	0	32(8-I-3)	3(2)
15	159	-1.61(9-II-2)	-3.78(9-II-2)	-3.98(9-I-2)	4(8-I-3)	29(8-I-3)	3(2)
15	160	2.06(9-II-2)	-2.99(9-II-2)	-3.38(9-I-2)	2(8-I-3)	30(8-I-3)	3(8-II-3)
15	161	-0.35(8-I-3)	-1.72(2)	-4.19(9-I-2)	10(9-II-2)	25(8-I-3)	3(8-II-3)
15	162	0.34(9-I-2)	-1.55(2)	-4.15(9-I-2)	7(8-I-3)	27(8-I-3)	3(8-II-3)
15	163	-0.50(8-I-3)	-1.75(9-I-3)	4.18(9-II-2)	12(9-II-2)	-26(8-II-3)	3(8-II-3)
15	164	0.31(9-I-2)	-1.35(2)	4.15(9-II-2)	13(9-II-2)	-24(8-II-3)	3(8-II-3)
15	165	-0.84(9-I-3)	-2.76(9-I-3)	4.22(9-II-2)	10(9-II-2)	-14(8-II-3)	4(9-II-2)
15	166	0.51(8-I-3)	-1.80(9-I-3)	4.16(9-II-2)	15(9-II-2)	-27(8-II-3)	3(8-II-3)
15	167	0.45(8-I-3)	-3.52(9-I-3)	4.18(9-II-2)	13(9-II-2)	-21(8-II-3)	5(9-II-2)
15	168	-0.09(9-I-2)	-12.65(9-I-2)	-3.19(9-I-2)	2(2)	47(8-I-3)	-2(2)
15	169	-0.26(9-I-2)	-9.31(9-I-2)	-3.54(9-I-2)	0	60(8-I-3)	-2(2)
15	170	0.15(8-I-3)	-17.05(9-I-2)	-2.58(9-I-2)	0	73(2)	-1(2)
15	171	0.81(9-I-2)	-16.37(9-II-2)	-2.61(9-I-2)	0	54(8-I-3)	0
15	172	-2.44(9-II-2)	-6.43(9-II-2)	-3.52(9-I-2)	1(8-I-3)	45(8-I-3)	3(8-II-3)
15	173	-1.57(9-I-2)	-10.93(9-II-2)	-3.03(9-I-2)	0	46(8-I-3)	2(8-II-3)
15	174	2.17(9-I-2)	-11.35(9-II-2)	-3.40(9-I-2)	0	58(8-I-3)	2(8-II-3)
15	175	-0.34(8-I-3)	-1.91(2)	-4.10(9-I-2)	7(8-I-3)	46(8-I-3)	3(8-II-3)
15	176	0.38(9-I-2)	-1.81(2)	-3.98(9-I-2)	3(9-II-2)	45(8-I-3)	2(8-II-3)
15	177	-0.43(8-I-3)	-1.73(2)	4.08(9-II-2)	13(9-II-2)	48(8-I-3)	3(8-II-3)
15	178	0.46(9-I-2)	-1.57(2)	-3.98(9-I-2)	8(9-II-2)	47(8-I-3)	2(8-II-3)

Muro	Pann.	Sxx	Syy	Sxy	Mxx	Myy	Mxy
15	179	-0.50(8-I-3)	-2.79(9-I-3)	4.09(9-II-2)	15(9-II-2)	48(8-I-3)	4(9-II-2)
15	180	-0.68(8-I-3)	-2.49(9-I-3)	4.10(9-II-2)	14(9-II-2)	37(8-I-3)	3(8-II-3)
15	181	0.34(9-I-2)	-1.65(9-I-3)	3.94(9-II-2)	16(9-II-2)	43(8-I-3)	3(8-II-3)
15	182	0.27(9-I-3)	-4.85(8-I-3)	3.98(9-II-2)	16(9-II-2)	24(8-I-3)	2(9-II-2)
15	183	-0.80(9-II-2)	-3.58(9-II-2)	-3.84(9-I-2)	3(8-I-3)	63(8-I-3)	2(8-II-3)
15	184	0.72(9-I-2)	-2.22(2)	-2.68(9-I-2)	0	59(8-I-3)	0
15	185	-0.42(8-I-3)	-1.84(2)	-3.84(9-I-2)	8(9-II-2)	68(8-I-3)	2(8-II-3)
15	186	0.57(9-I-2)	-1.92(9-I-3)	-2.63(9-I-2)	0	65(8-I-3)	0
15	187	-0.41(8-I-3)	-2.30(9-I-3)	3.86(9-II-2)	14(9-II-2)	76(8-I-3)	3(8-II-3)
15	188	0.40(9-I-2)	-1.65(2)	2.58(9-II-2)	0	70(8-I-3)	1(8-II-3)
15	189	-0.56(8-I-3)	-4.75(9-I-3)	3.81(9-II-2)	21(9-II-2)	82(8-I-3)	1(2)
15	190	0.38(2)	-3.63(8-I-3)	2.67(9-II-2)	0	84(8-I-3)	1(8-II-3)
15	191	0.29(2)	-8.76(8-I-3)	2.61(9-II-2)	0	71(8-I-3)	2(9-I-2)

Verifiche stato limite ultimo

Verifica delle travi di fondazione

Scenario di calcolo: **Set_NT_SLV_SLD_A2_STR/GEO_2018**

Simbologia:

Terreno	Nome della stratigrafia per travi Winkler
L [cm]	Lunghezza teorica elemento (distanza tra i nodi)
Ln [cm]	Lunghezza netta elemento (tiene conto dei conci rigidi)
L2,L3 [cm]	Lunghezze libere di inflessione
Sez. R: Sezione Rettangolare	
	By[cm]: Larghezza (asse locale y)
	Bz[cm]: Larghezza (asse locale z)
Sez. T: Sezione a T (rovescia e non)	
	Ba[cm]: Larghezza base inferiore
	Ha[cm]: Altezza inferiore
	Bs[cm]: Larghezza superiore
	Hs[cm]: Altezza superiore
Sez. L: Sezione ad L (rovescia e non)	
	Ba[cm]: Larghezza base inferiore
	Ha[cm]: Altezza inferiore
	Bs[cm]: Larghezza superiore
	Hs[cm]: Altezza superiore
Sez. C: Sezione circolare	
	R[cm]: Raggio
Sez. G: Sezione generica	
	B[cm]: Larghezza
	H[cm]: Altezza
Fatt.Ampl.Sisma	Fattore moltiplicativo di gruppo per le azioni sismiche (solo se diverso da 1.0)
X [cm]	Punto di verifica
ILN	Inizio luce netta
CAMP	Punto di massimo momento sia superiore che inferiore ad esclusione degli estremi
FLN	Fine luce netta
M- [kg*m]	Momento negativo massimo di calcolo ⁽¹⁾
N- [kg]	Sforzo normale corrispondente ad M-
M+ [kg*m]	Momento positivo massimo di calcolo ⁽¹⁾
N+ [kg]	Sforzo normale corrispondente ad M+
ΔM- [kg*m]	Incremento di M- per la traslazione del diagramma del momento a causa del taglio
ΔM+ [kg*m]	Incremento di M+ per la traslazione del diagramma del momento a causa del taglio
Afs [cmq]	Area di ferro superiore

Afi [cmq]	Area di ferro inferiore
ε_{SC-}	Deformazione nel cls per effetto di M-:N-(⁴)
ε_{SC+}	Deformazione nel cls per effetto di M+:N+(⁴)
ε_{sf-}	Deformazione nell'acciaio per effetto di M-:N-(⁴)
ε_{sf+}	Deformazione nell'acciaio per effetto di M+:N+(⁴)
C-	Combinazione di carico generatore di M-:N-
C+	Combinazione di carico generatore di M+:N+
x- [cm]	Profondità asse neutro per la combinazione C-(⁵)
d- [cm]	Altezza utile della sezione per la combinazione C-(⁶)
x+ [cm]	Profondità asse neutro per la combinazione C+(⁵)
d+ [cm]	Altezza utile della sezione per la combinazione C+(⁶)
Mr- [kg*m]	Momento resistente superiore
Mr+ [kg*m]	Momento resistente inferiore
Stato-	Stato della sezione per la combinazione C-(⁷)
Stato+	Stato della sezione per la combinazione C+(⁷)
Comb	Combinazione di carico: quando Comb non è sismica è individuata dal codice [C], quando è sismica è individuata dal codice [(Cx+Cy) Cm Sc].
- C	Individua la Combinazione di Carico non sismica (1, 2, ecc. come da scenario);
- Cx	Individua la Combinazione di Carico sismica in direzione x (SismaX, come da scenario);
- Cy	Individua la Combinazione di Carico sismica in direzione y (SismaY, come da scenario);
- Cm	Individua la Combinazione spostamento masse (I, II, III, IV, V, ecc. come da Combinazioni Sisma in Spostamento masse impalcato);
- Sc	Individua la sottocombinazione ottenuta mediante la permutazione dei segni (1, 2, 3, 4, 5, 6, 7, 8):
1)	$Sc = + SismaZ*fz + SismaX*fx + SismaY*fy$
2)	$Sc = + SismaZ*fz + SismaX*fx - SismaY*fy$
3)	$Sc = + SismaZ*fz - SismaX*fx + SismaY*fy$
4)	$Sc = + SismaZ*fz - SismaX*fx - SismaY*fy$
5)	$Sc = - SismaZ*fz + SismaX*fx + SismaY*fy$
6)	$Sc = - SismaZ*fz + SismaX*fx - SismaY*fy$
7)	$Sc = - SismaZ*fz - SismaX*fx + SismaY*fy$
8)	$Sc = - SismaZ*fz - SismaX*fx - SismaY*fy$
Le ultime quattro sono assenti quando non è richiesto il contributo del sisma in direzione verticale. Le combinazioni delle azioni sismiche così ottenute vengono combinate con i carichi verticali (come da scenario).	
Sez	Sezione di verifica [Sinistra/Destra]
Td [kg]	Taglio di verifica(²)
VRdns [kg]	Resistenza a taglio in assenza di armature
VRcd [kg]	Resistenza taglio-compressione calcestruzzo
VRsd [kg]	Resistenza taglio-trazione acciaio
VRd [kg]	Resistenza a taglio =min(VRcd,VRsd)
VRd,f [kg]	Resistenza a taglio dovuta alla resistenza a trazione del calcestruzzo ad alte prestazioni (quando presente)(cfr. eq 4.2 CNR204/2006), oppure resistenza rinforzo del composito (quando presente)(cfr. eq 4.19 CNR200/2013)
Mt [kg*m]	Momento torcente
Tpl [kg]	Taglio dovuto ai momenti resistenti alle estremità della trave
Mr [kg*m]	Momento resistente (ultimo) utilizzato per il calcolo di Tpl quando richiesto
Dx [cm]	Distanza dall'estremo da armare con staffe
Staffe [cmq]	Area delle staffe
cot(θ)	cot(θ) secondo il punto 4.1.2.1.3 delle Norme Tecniche
F.Par. [cmq]	Area armatura longitudinale di parete(³)
Cs	Coefficiente di sicurezza definito dal rapporto Fr/Fd (Fr=resistenza,Fd=azione)
ζ_E	Livello di sicurezza sismico definito come rapporto tra l'accelerazione sopportabile e l'accelerazione di progetto, quando richiesto dal criterio di verifica
Simbologia verifica travi collegamento:	
Comb	Combinazione più gravosa
Nsd [kg]	Azione verticale negli elementi collegati, nella combinazione specificata
α	Coefficiente in funzione della classe di terreno (NTC 7.2.5.1)
a/g	Punto di aggancio dello spettro di accelerazione [a/g=Sa(0)]
N	Sforzo normale di verifica $N=\alpha*Nsd*a/g$
Af [cmq]	Area di ferro complessiva nella sezione
NRd C [kg]	Resistenza a compressione della sezione

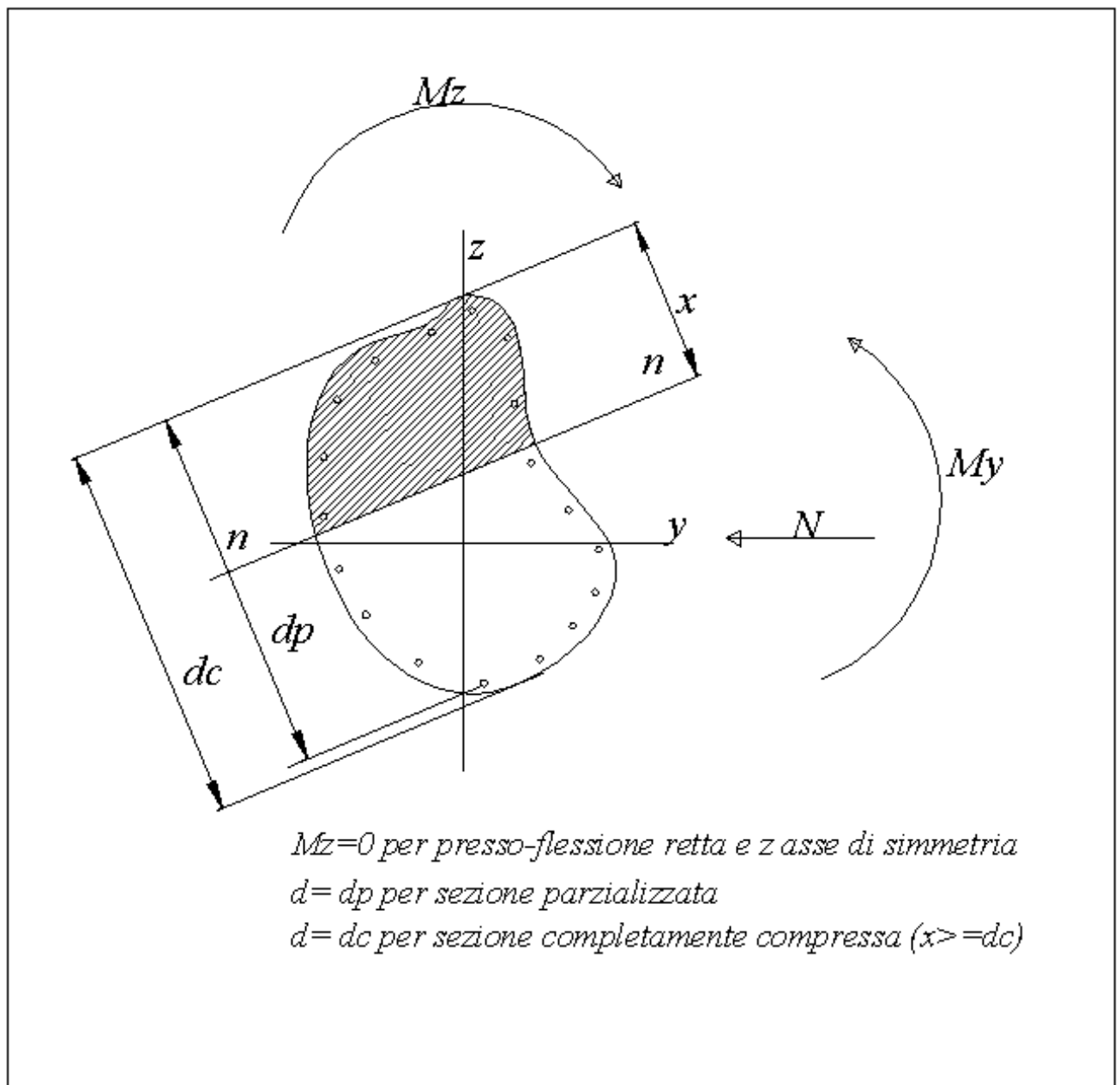
NRd T [kg] Resistenza a trazione della sezione

Verifiche duttilità (quando richieste):

Zona	Sezione di verifica dell'elemento
Comb.	Combinazione di verifica
Nmax [kg]	Sforzo Normale massimo
Dir	Direzione di flessione (pilastri=Y o Z, travi =Z, pareti= ortogonale alla base)
Mry [kg*m]	Momento di snervamento corrispondente a Nmax
MrU [kg*m]	Momento ultimo (resistente) corrispondente a Nmax sulla sezione depurata del calcestruzzo non confinato, considerando il confinamento
ϕ_y [1/m]	Curvatura allo snervamento ($\phi_y = MrU/Mry * \phi'_y$)
ϕ_u [1/m]	Curvatura allo corrispondente a MrU
μ	Capacità in duttilità della sezione
F.Conf	Fattore di confinamento adottato (= $f_{ck,c}/f_{ck}$)
μ_d	Richiesta in duttilità della sezione
Cs	Livello di sicurezza ($Cs = \mu/\mu_d$)

Note Verifica travi:

- (1) il valore del momento di verifica è dato da $M + \Delta M$
- (2) Td è il valore di verifica a taglio esso è calcolato in funzione della somma tra taglio da carichi verticali il valore di Tpl ovvero quando la trave è tozza amplificando il taglio di calcolo dovuto al sisma per il fattore di comportamento
- (3) armatura necessaria per la sola verifica a torsione
- (4) le deformazioni sono stampate a meno del fattore 10^{-3}
- (5) distanza tra la fibra di cls compressa più lontana e l'asse neutro in direzione ortogonale all'asse neutro
- (6) distanza tra le fibre sollecitate più lontane dall'asse neutro: nel caso di sezione parzializzata le due fibre sono quella di cls compresso e quella dell'acciaio teso più lontane da n-n, mentre nel caso di sezione completamente compressa le due fibre sono le due di cls compresso più lontane da n-n
- (7) Indica lo stato della sezione se: completamente compressa (Compr.),completamente tesa (Tesa), parzializzata (Parz.)



Schema geometrico verifica della sezione

Trave di fondazione: 9001 [12,13], Pilastrate [--,--] Sez. R: By=60.0 cm Bz=50.0 cm L=348.6 cm
Ln=348.6 cm Terreno=Terreno1 Criterio : CLS_TraviFondazione_Rett - Verifica a flessione: **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	185	578	--	--	6.03	6.03	10012	10012	(8+9)-III-2	(8+9)-III-3	17
34.9	134	367	30	125	6.03	6.03	10012	10012	(8+9)-III-2	(8+9)-III-3	20
CAMP	992	401	100	135	6.03	6.03	10012	10012	(8+9)-IV-3	(8+9)-IV-2	9.2
313.7	1160	629	--	--	6.03	6.03	10012	10012	(8+9)-IV-3	(8+9)-IV-2	8.6
FLN	956	589	--	--	6.03	6.03	10012	10012	(8+9)-IV-3	(8+9)-IV-2	10

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	9.6	45.9	0.209	9.6	45.9	0.210	10012	10012	(8+9)-III-2	(8+9)-III-3	Parz.	Parz.
34.9	9.6	45.9	0.209	9.6	45.9	0.209	10012	10012	(8+9)-III-2	(8+9)-III-3	Parz.	Parz.
CAMP	9.6	45.9	0.210	9.6	45.9	0.210	10012	10012	(8+9)-IV-3	(8+9)-IV-2	Parz.	Parz.
313.7	9.6	45.9	0.210	9.6	45.9	0.210	10012	10012	(8+9)-IV-3	(8+9)-IV-2	Parz.	Parz.
FLN	9.6	45.9	0.210	9.6	45.9	0.210	10012	10012	(8+9)-IV-3	(8+9)-IV-2	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500 Comb: Sin=(8+9)-III-3 Cen=(8+9)-III-3 Des=(8+9)-IV-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	702	--	60298	40627	40627	0	10012	50.0	10.05	58
Cen	778	--	60298	37716	37716	--	--	--	9.33	48
Des	618	--	60298	40627	40627	0	10012	50.0	10.05	66

Trave di fondazione: 9001 [14,12], Pilastrate [--,--] Sez. R: By=60.0 cm Bz=50.0 cm L=459.1 cm
Ln=459.1 cm Terreno=Terreno1 Criterio : CLS_TraviFondazione_Rett - Verifica a flessione: **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	468	1846	--	--	6.03	6.03	10012	10012	(8+9)-I-1	2	5.4
45.9	178	1319	130	237	6.03	6.03	10012	10012	(8+9)-I-1	2	6.4
CAMP	767	664	--	295	6.03	6.03	10012	10012	(8+9)-VIII-4	2	10
413.1	381	432	126	31	6.03	6.03	10012	10012	(8+9)-IV-2	(8+9)-III-3	20
FLN	345	501	40	--	6.03	6.03	10012	10012	(8+9)-III-2	(8+9)-III-3	20

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	9.6	45.9	0.209	9.7	45.9	0.210	10012	10012	(8+9)-I-1	2	Parz.	Parz.
45.9	9.6	45.9	0.209	9.6	45.9	0.210	10012	10012	(8+9)-I-1	2	Parz.	Parz.
CAMP	9.6	45.9	0.210	9.6	45.9	0.210	10012	10012	(8+9)-VIII-4	2	Parz.	Parz.
413.1	9.6	45.9	0.209	9.6	45.9	0.209	10012	10012	(8+9)-IV-2	(8+9)-III-3	Parz.	Parz.
FLN	9.6	45.9	0.209	9.6	45.9	0.209	10012	10012	(8+9)-III-2	(8+9)-III-3	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500 Comb: Sin=(8+9)-I-4 Cen=3 Des=(8+9)-IV-2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	2132	--	60298	40627	40627	0	10012	50.0	10.05	19
Cen	1855	--	60298	37419	37419	--	--	--	9.26	20
Des	927	--	60298	40627	40627	0	10012	50.0	10.05	44

Trave di fondazione: 9001 [6,14], Pilastrate [--,--] Sez. R: By=60.0 cm Bz=50.0 cm L=615.3 cm
Ln=615.3 cm Terreno=Terreno1 Criterio : CLS_TraviFondazione_Rett - Verifica a flessione: **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	283	2328	11	--	6.03	6.03	10012	10012	(8+9)-VIII-1	2	4.3
61.5	705	1511	--	42	6.03	6.03	10012	10012	(8+9)-VIII-3	(8+9)-VIII-2	6.4
CAMP	1266	655	--	288	6.03	6.03	10012	10012	2	(8+9)-VIII-2	7.9
553.7	672	1078	--	132	6.03	6.03	10012	10012	(8+9)-III-2	(8+9)-III-3	8.3
FLN	798	1950	--	--	6.03	6.03	10012	10012	(8+9)-I-1	(8+9)-I-4	5.1

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	9.6	45.9	0.209	9.7	45.9	0.211	10012	10012	(8+9)-VIII-1	2	Parz.	Parz.
61.5	9.6	45.9	0.210	9.6	45.9	0.210	10012	10012	(8+9)-VIII-3	(8+9)-VIII-2	Parz.	Parz.
CAMP	9.6	45.9	0.210	9.6	45.9	0.210	10012	10012	2	(8+9)-VIII-2	Parz.	Parz.
553.7	9.6	45.9	0.210	9.6	45.9	0.210	10012	10012	(8+9)-III-2	(8+9)-III-3	Parz.	Parz.
FLN	9.6	45.9	0.210	9.7	45.9	0.210	10012	10012	(8+9)-I-1	(8+9)-I-4	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500 Comb: Sin=3 Cen=3 Des=(8+9)-II-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	2346	--	60298	40627	40627	0	10012	50.0	10.05	17
Cen	2809	--	60298	37122	37122	--	--	--	9.19	13
Des	2072	--	60298	40627	40627	0	10012	50.0	10.05	20

Trave di fondazione: 9001 [5,6], Pilastrate [--,--] Sez. R: By=60.0 cm Bz=50.0 cm L=570.8 cm Ln=570.8 cm Terreno=Terreno1 Criterio : CLS_TraviFondazione_Rett - Verifica a flessione: **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	1523	197	--	--	6.03	6.03	10012	10012	2	(8+9)-VIII-3	6.6
57.1	1456	--	24	--	6.03	6.03	10012	10012	2	1	6.8
CAMP	1316	1101	50	299	6.03	6.03	10012	10012	2	(8+9)-VIII-4	7.1
513.7	668	1928	532	177	6.03	6.03	10012	10012	(8+9)-IV-3	(8+9)-VIII-4	4.8
FLN	574	2418	43	--	6.03	6.03	10012	10012	(8+9)-VIII-1	(8+9)-VIII-4	4.1

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	9.6	45.9	0.210	9.6	45.9	0.209	10012	10012	2	(8+9)-VIII-3	Parz.	Parz.
57.1	9.6	45.9	0.210	--	--	--	10012	10012	2	1	Parz.	--
CAMP	9.6	45.9	0.210	9.6	45.9	0.210	10012	10012	2	(8+9)-VIII-4	Parz.	Parz.
513.7	9.6	45.9	0.210	9.7	45.9	0.211	10012	10012	(8+9)-IV-3	(8+9)-VIII-4	Parz.	Parz.
FLN	9.6	45.9	0.210	9.7	45.9	0.211	10012	10012	(8+9)-VIII-1	(8+9)-VIII-4	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500 Comb: Sin=(8+9)-VI-2 Cen=(8+9)-V-2 Des=(8+9)-VII-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	1483	--	60298	40627	40627	0	10012	50.0	10.05	27
Cen	1628	--	60298	36933	36933	--	--	--	9.14	23
Des	1280	--	60298	40627	40627	0	10012	50.0	10.05	32

Trave di fondazione: 9002 [7,5], Pilastrate [--,--] Sez. R: By=60.0 cm Bz=50.0 cm L=247.9 cm Ln=247.9 cm Terreno=Terreno1 Criterio : CLS_TraviFondazione_Rett - Verifica a flessione: **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	956	743	181	--	6.03	6.03	10012	10012	(8+9)-VII-1	(8+9)-V-3	8.8
24.8	1117	587	293	129	6.03	6.03	10012	10012	(8+9)-VIII-1	(8+9)-VII-4	7.1

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
CAMP	1973	677	--	--	6.03	6.03	10012	10012	2	(8+9)-VIII-4	5.1
223.1	1454	342	246	168	6.03	6.03	10012	10012	2	(8+9)-VIII-3	5.9
FLN	1545	544	--	--	6.03	6.03	10012	10012	(8+9)-VIII-2	(8+9)-VIII-3	6.5

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	9.6	45.9	0.210	9.6	45.9	0.210	10012	10012	(8+9)-VII-1	(8+9)-V-3	Parz.	Parz.
24.8	9.6	45.9	0.210	9.6	45.9	0.210	10012	10012	(8+9)-VIII-1	(8+9)-VII-4	Parz.	Parz.
CAMP	9.7	45.9	0.210	9.6	45.9	0.210	10012	10012	2	(8+9)-VIII-4	Parz.	Parz.
223.1	9.7	45.9	0.210	9.6	45.9	0.209	10012	10012	2	(8+9)-VIII-3	Parz.	Parz.
FLN	9.6	45.9	0.210	9.6	45.9	0.210	10012	10012	(8+9)-VIII-2	(8+9)-VIII-3	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500 Comb: Sin=3 Cen=(8+9)-VIII-4 Des=(8+9)-VIII-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	2392	--	60298	40627	40627	0	10012	50.0	10.05	17
Cen	2668	--	60298	36933	36933	--	--	--	9.14	14
Des	2250	--	60298	40627	40627	0	10012	50.0	10.05	18

Trave di fondazione: 9003 [134,34], Pilastrate [--,--] Sez. R: By=60.0 cm Bz=50.0 cm L=158.1 cm Ln=158.1 cm Terreno=Terreno1 Criterio : CLS_TraviFondazione - Verifica a flessione: **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	256	1899	--	--	6.03	7.60	10019	12520	(8+9)-V-2	(8+9)-V-3	6.6
15.8	79	1387	177	512	6.03	7.60	10019	12520	(8+9)-V-2	(8+9)-V-3	6.6
CAMP	2500	1916	781	576	6.03	7.60	10019	12520	(8+9)-VI-3	(8+9)-VI-2	3.1
142.3	3098	2351	598	456	6.03	7.60	10019	12520	(8+9)-VI-3	(8+9)-VI-2	2.7
FLN	3696	2807	--	--	6.03	7.60	10019	12520	(8+9)-VI-3	(8+9)-VI-2	2.7

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	9.4	45.9	0.206	10.7	45.9	0.233	10019	12520	(8+9)-V-2	(8+9)-V-3	Parz.	Parz.
15.8	9.4	45.9	0.206	10.7	45.9	0.233	10019	12520	(8+9)-V-2	(8+9)-V-3	Parz.	Parz.
CAMP	9.5	45.9	0.208	10.7	45.9	0.234	10019	12520	(8+9)-VI-3	(8+9)-VI-2	Parz.	Parz.
142.3	9.5	45.9	0.208	10.7	45.9	0.234	10019	12520	(8+9)-VI-3	(8+9)-VI-2	Parz.	Parz.
FLN	9.5	45.9	0.208	10.7	45.9	0.234	10019	12520	(8+9)-VI-3	(8+9)-VI-2	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ = 2.500 Comb: (8+9)-VI-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	4047	--	60298	41494	41494	0	12520	158.1	10.27	10
Des							10019			

Trave di fondazione: 9003 [33,34], Pilastrate [--,--] Sez. R: By=60.0 cm Bz=50.0 cm L=180.9 cm Ln=180.9 cm Terreno=Terreno1 Criterio : CLS_TraviFondazione_Rett - Verifica a flessione: **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	3209	2512	--	--	6.03	6.03	10012	10012	(8+9)-VI-2	(8+9)-VI-3	3.1
18.1	2960	2217	249	294	6.03	6.03	10012	10012	(8+9)-VI-2	(8+9)-VI-3	3.1
CAMP	3039	2178	464	499	6.03	6.03	10012	10012	(8+9)-VI-3	(8+9)-VI-2	2.9
162.8	3445	2612	405	458	6.03	6.03	10012	10012	(8+9)-VI-3	(8+9)-VI-2	2.6
FLN	3851	3070	--	--	6.03	6.03	10012	10012	(8+9)-VI-3	(8+9)-VI-2	2.6

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	9.7	45.9	0.211	9.7	45.9	0.211	10012	10012	(8+9)-VI-2	(8+9)-VI-3	Parz.	Parz.
18.1	9.7	45.9	0.211	9.7	45.9	0.211	10012	10012	(8+9)-VI-2	(8+9)-VI-3	Parz.	Parz.
CAMP	9.7	45.9	0.212	9.7	45.9	0.211	10012	10012	(8+9)-VI-3	(8+9)-VI-2	Parz.	Parz.
162.8	9.7	45.9	0.212	9.7	45.9	0.211	10012	10012	(8+9)-VI-3	(8+9)-VI-2	Parz.	Parz.
FLN	9.7	45.9	0.212	9.7	45.9	0.211	10012	10012	(8+9)-VI-3	(8+9)-VI-2	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Des=2.500 Comb: Sin=(8+9)-VI-3 Des=(8+9)-VI-2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	4827	--	60298	37513	37513	0	10012	90.4	9.28	7.8
Des	4865	--	60298	40627	40627	0	10012	90.4	10.05	8.4

Trave di fondazione: 9003 [32,33], Pilastrate [--,--] Sez. R: By=60.0 cm Bz=50.0 cm L=120.0 cm Ln=120.0 cm Terreno=Terreno1 Criterio : CLS_TraviFondazione_Rett - Verifica a flessione: **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	887	861	--	--	6.03	6.03	10012	10012	(8+9)-I-3	(8+9)-I-2	11
12.0	726	583	161	278	6.03	6.03	10012	10012	(8+9)-I-3	(8+9)-I-2	11
CAMP	2251	1577	631	568	6.03	6.03	10012	10012	(8+9)-VI-2	(8+9)-VI-3	3.5
108.0	2619	1904	365	333	6.03	6.03	10012	10012	(8+9)-VI-2	(8+9)-VI-3	3.4
FLN	2984	2237	--	--	6.03	6.03	10012	10012	(8+9)-VI-2	(8+9)-VI-3	3.4

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	9.6	45.9	0.210	9.6	45.9	0.210	10012	10012	(8+9)-I-3	(8+9)-I-2	Parz.	Parz.
12.0	9.6	45.9	0.210	9.6	45.9	0.210	10012	10012	(8+9)-I-3	(8+9)-I-2	Parz.	Parz.
CAMP	9.7	45.9	0.211	9.7	45.9	0.211	10012	10012	(8+9)-VI-2	(8+9)-VI-3	Parz.	Parz.
108.0	9.7	45.9	0.211	9.7	45.9	0.211	10012	10012	(8+9)-VI-2	(8+9)-VI-3	Parz.	Parz.
FLN	9.7	45.9	0.211	9.7	45.9	0.211	10012	10012	(8+9)-VI-2	(8+9)-VI-3	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Des=2.500 Comb: Sin=(8+9)-VI-2 Des=(8+9)-VI-2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	3265	--	60298	40627	40627	0	10012	60.0	10.05	12
Des	3169	--	60298	37513	37513	0	10012	60.0	9.28	12

Trave di fondazione: 9003 [11,32], Pilastrate [--,--] Sez. R: By=60.0 cm Bz=50.0 cm L=40.0 cm Ln=40.0 cm Terreno=Terreno1 Criterio : CLS_TraviFondazione_Rett - Verifica a flessione: **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	640	981	175	--	6.03	6.03	10012	10012	(8+9)-I-3	(8+9)-III-1	10
4.0	634	940	195	41	6.03	6.03	10012	10012	(8+9)-I-3	(8+9)-III-1	10
CAMP	819	708	107	273	6.03	6.03	10012	10012	(8+9)-V-3	(8+9)-III-1	10
36.0	872	863	55	32	6.03	6.03	10012	10012	(8+9)-V-3	(8+9)-V-2	11
FLN	927	895	--	--	6.03	6.03	10012	10012	(8+9)-V-3	(8+9)-V-2	11

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	9.6	45.9	0.210	9.6	45.9	0.210	10012	10012	(8+9)-I-3	(8+9)-III-1	Parz.	Parz.
4.0	9.6	45.9	0.210	9.6	45.9	0.210	10012	10012	(8+9)-I-3	(8+9)-III-1	Parz.	Parz.
CAMP	9.6	45.9	0.210	9.6	45.9	0.210	10012	10012	(8+9)-V-3	(8+9)-III-1	Parz.	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
36.0	9.6	45.9	0.210	9.6	45.9	0.210	10012	10012	(8+9)-V-3	(8+9)-V-2	Parz.	Parz.
FLN	9.6	45.9	0.210	9.6	45.9	0.210	10012	10012	(8+9)-V-3	(8+9)-V-2	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$ Comb: (8+9)-VI-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	2200	--	60298	40627	40627	0	10012	40.0	10.05	18
Des							10012			

Trave di fondazione: 9003 [10,11], Pilastrate [--,--] Sez. R: By=60.0 cm Bz=50.0 cm L=37.2 cm Ln=37.2 cm Terreno=Terreno1 Criterio : CLS_TraviFondazione_Rett - Verifica a flessione: **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	1433	1197	--	--	6.03	6.03	10012	10012	(8+9)-II-2	(8+9)-II-3	7.0
3.7	1389	1156	44	42	6.03	6.03	10012	10012	(8+9)-II-2	(8+9)-II-3	7.0
CAMP	1155	980	278	217	6.03	6.03	10012	10012	(8+9)-II-2	(8+9)-II-3	7.0
33.5	476	330	808	731	6.03	6.03	10012	10012	(8+9)-II-2	(8+9)-II-3	7.8
FLN	-661	1046	1879	--	6.03	6.03	10012	10012	(8+9)-I-2	(8+9)-I-1	8.2

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	9.6	45.9	0.210	9.6	45.9	0.210	10012	10012	(8+9)-II-2	(8+9)-II-3	Parz.	Parz.
3.7	9.6	45.9	0.210	9.6	45.9	0.210	10012	10012	(8+9)-II-2	(8+9)-II-3	Parz.	Parz.
CAMP	9.6	45.9	0.210	9.6	45.9	0.210	10012	10012	(8+9)-II-2	(8+9)-II-3	Parz.	Parz.
33.5	9.6	45.9	0.210	9.6	45.9	0.210	10012	10012	(8+9)-II-2	(8+9)-II-3	Parz.	Parz.
FLN	9.6	45.9	0.210	9.6	45.9	0.210	10012	10012	(8+9)-I-2	(8+9)-I-1	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$ Comb: (8+9)-VI-2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	1719	--	60298	40627	40627	0	10012	37.2	10.05	24
Des							10012			

Trave di fondazione: 9003 [9,10], Pilastrate [--,--] Sez. R: By=60.0 cm Bz=50.0 cm L=120.0 cm Ln=120.0 cm Terreno=Terreno1 Criterio : CLS_TraviFondazione_Rett - Verifica a flessione: **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	1979	1777	--	--	6.03	6.03	10012	10012	(8+9)-VI-3	(8+9)-VI-2	5.1
12.0	1704	1405	274	372	6.03	6.03	10012	10012	(8+9)-VI-3	(8+9)-VI-2	5.1
CAMP	1432	1043	470	630	6.03	6.03	10012	10012	(8+9)-VI-3	(8+9)-VI-2	5.3
108.0	1158	758	287	313	6.03	6.03	10012	10012	(8+9)-II-2	(8+9)-II-3	6.9
FLN	1445	1071	--	--	6.03	6.03	10012	10012	(8+9)-II-2	(8+9)-II-3	6.9

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	9.7	45.9	0.210	9.7	45.9	0.210	10012	10012	(8+9)-VI-3	(8+9)-VI-2	Parz.	Parz.
12.0	9.7	45.9	0.210	9.7	45.9	0.210	10012	10012	(8+9)-VI-3	(8+9)-VI-2	Parz.	Parz.
CAMP	9.7	45.9	0.210	9.7	45.9	0.210	10012	10012	(8+9)-VI-3	(8+9)-VI-2	Parz.	Parz.
108.0	9.6	45.9	0.210	9.6	45.9	0.210	10012	10012	(8+9)-II-2	(8+9)-II-3	Parz.	Parz.
FLN	9.6	45.9	0.210	9.6	45.9	0.210	10012	10012	(8+9)-II-2	(8+9)-II-3	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Des=2.500 Comb: Sin=(8+9)-VI-2 Des=(8+9)-VI-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	3213	--	60298	37414	37414	0	10012	60.0	9.26	12
Des	2752	--	60298	40627	40627	0	10012	60.0	10.05	15

Trave di fondazione: 9003 [8,9], Pilastrate [--,--] Sez. R: By=60.0 cm Bz=50.0 cm L=290.0 cm Ln=290.0 cm Terreno=Terreno1 Criterio : CLS_TraviFondazione_Rett - Verifica a flessione: **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	1031	2853	--	--	6.03	6.03	10012	10012	(8+9)-II-4	(8+9)-II-1	3.5
29.0	435	1937	424	652	6.03	6.03	10012	10012	(8+9)-II-4	(8+9)-II-1	3.9
CAMP	1077	1623	538	356	6.03	6.03	10012	10012	(8+9)-VI-3	2	5.1
261.0	1833	1766	204	41	6.03	6.03	10012	10012	(8+9)-VI-3	(8+9)-VI-2	4.9
FLN	2119	1823	--	--	6.03	6.03	10012	10012	(8+9)-VI-3	(8+9)-VI-2	4.7

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	9.6	45.9	0.210	9.7	45.9	0.211	10012	10012	(8+9)-II-4	(8+9)-II-1	Parz.	Parz.
29.0	9.6	45.9	0.210	9.7	45.9	0.211	10012	10012	(8+9)-II-4	(8+9)-II-1	Parz.	Parz.
CAMP	9.6	45.9	0.210	9.7	45.9	0.210	10012	10012	(8+9)-VI-3	2	Parz.	Parz.
261.0	9.7	45.9	0.211	9.7	45.9	0.210	10012	10012	(8+9)-VI-3	(8+9)-VI-2	Parz.	Parz.
FLN	9.7	45.9	0.211	9.7	45.9	0.210	10012	10012	(8+9)-VI-3	(8+9)-VI-2	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Des=2.500 Comb: Sin=(8+9)-VI-1 Des=(8+9)-VI-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	4449	--	60298	40627	40627	0	10012	145.0	10.05	9.1
Des	2365	--	60298	37414	37414	0	10012	145.0	9.26	16

Trave di fondazione: 9003 [31,8], Pilastrate [--,--] Sez. R: By=60.0 cm Bz=50.0 cm L=58.0 cm Ln=58.0 cm Terreno=Terreno1 Criterio : CLS_TraviFondazione_Rett - Verifica a flessione: **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	2328	3624	--	--	6.03	6.03	10012	10012	(8+9)-VI-4	(8+9)-VI-1	2.8
5.8	2164	3510	164	115	6.03	6.03	10012	10012	(8+9)-VI-4	(8+9)-VI-1	2.8
CAMP	1854	3305	475	320	6.03	6.03	10012	10012	(8+9)-VI-4	(8+9)-VI-1	2.8
52.2	1203	3004	326	96	6.03	6.03	10012	10012	(8+9)-VI-4	(8+9)-VI-1	3.2
FLN	1135	3008	290	50	6.03	6.03	10012	10012	(8+9)-VI-4	(8+9)-VI-1	3.3

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	9.7	45.9	0.211	9.7	45.9	0.212	10012	10012	(8+9)-VI-4	(8+9)-VI-1	Parz.	Parz.
5.8	9.7	45.9	0.211	9.7	45.9	0.212	10012	10012	(8+9)-VI-4	(8+9)-VI-1	Parz.	Parz.
CAMP	9.7	45.9	0.211	9.7	45.9	0.212	10012	10012	(8+9)-VI-4	(8+9)-VI-1	Parz.	Parz.
52.2	9.6	45.9	0.210	9.7	45.9	0.211	10012	10012	(8+9)-VI-4	(8+9)-VI-1	Parz.	Parz.
FLN	9.6	45.9	0.210	9.7	45.9	0.211	10012	10012	(8+9)-VI-4	(8+9)-VI-1	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ =2.500 Comb: (8+9)-VI-2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	3514	--	60298	40627	40627	0	10012	58.0	10.05	12
Des							10012			

Trave di fondazione: 9003 [30,31], Pilastrate [--,--] Sez. R: By=60.0 cm Bz=50.0 cm L=240.0 cm Ln=240.0 cm Terreno=Terreno1 Criterio : CLS_TraviFondazione_Rett - Verifica a flessione: **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	937	198	40	--	6.03	6.03	10012	10012	2	(8+9)-I-4	10
24.0	983	131	65	58	6.03	6.03	10012	10012	2	(8+9)-I-4	9.6
CAMP	1408	1704	191	515	6.03	6.03	10012	10012	(8+9)-II-4	(8+9)-II-1	4.5
216.0	1713	2385	356	800	6.03	6.03	10012	10012	(8+9)-VI-4	(8+9)-VI-1	3.1
FLN	2127	3315	--	--	6.03	6.03	10012	10012	(8+9)-VI-4	(8+9)-VI-1	3.0

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	9.6	45.9	0.210	9.6	45.9	0.209	10012	10012	2	(8+9)-I-4	Parz.	Parz.
24.0	9.6	45.9	0.210	9.6	45.9	0.209	10012	10012	2	(8+9)-I-4	Parz.	Parz.
CAMP	9.6	45.9	0.210	9.7	45.9	0.211	10012	10012	(8+9)-II-4	(8+9)-II-1	Parz.	Parz.
216.0	9.7	45.9	0.211	9.7	45.9	0.211	10012	10012	(8+9)-VI-4	(8+9)-VI-1	Parz.	Parz.
FLN	9.7	45.9	0.211	9.7	45.9	0.211	10012	10012	(8+9)-VI-4	(8+9)-VI-1	Parz.	Parz.

Verifica a taglio: $\cot(\theta) \sin=2.500, \cot(\theta) \cos=2.500, \cot(\theta) \tan=2.500$ Comb: Sin=(8+9)-VI-1 Cen=(8+9)-VI-1 Des=(8+9)-VI-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	1021	--	60298	40627	40627	0	10012	50.0	10.05	40
Cen	2895	--	60298	37725	37725	--	--	--	9.34	13
Des	4096	--	60298	40627	40627	0	10012	50.0	10.05	9.9

Trave di fondazione: 9003 [29,30], Pilastrate [--,--] Sez. R: By=60.0 cm Bz=50.0 cm L=30.0 cm Ln=30.0 cm Terreno=Terreno1 Criterio : CLS_TraviFondazione_Rett - Verifica a flessione: **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	1207	571	--	--	6.03	6.03	10012	10012	(8+9)-V-2	(8+9)-V-3	8.3
3.0	1154	524	53	47	6.03	6.03	10012	10012	(8+9)-V-2	(8+9)-V-3	8.3
CAMP	905	287	302	284	6.03	6.03	10012	10012	(8+9)-V-2	(8+9)-V-3	8.3
27.0	586	6	509	466	6.03	6.03	10012	10012	(8+9)-V-2	(8+9)-V-3	9.1
FLN	562	-5	482	432	6.03	6.03	10012	10012	(8+9)-V-2	(8+9)-V-3	9.6

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	9.6	45.9	0.210	9.6	45.9	0.210	10012	10012	(8+9)-V-2	(8+9)-V-3	Parz.	Parz.
3.0	9.6	45.9	0.210	9.6	45.9	0.210	10012	10012	(8+9)-V-2	(8+9)-V-3	Parz.	Parz.
CAMP	9.6	45.9	0.210	9.6	45.9	0.210	10012	10012	(8+9)-V-2	(8+9)-V-3	Parz.	Parz.
27.0	9.6	45.9	0.210	9.6	45.9	0.209	10012	10012	(8+9)-V-2	(8+9)-V-3	Parz.	Parz.
FLN	9.6	45.9	0.210	9.6	45.9	0.209	10012	10012	(8+9)-V-2	(8+9)-V-3	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$ Comb: (8+9)-VI-2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	2222	--	60298	40627	40627	0	10012	30.0	10.05	18
Des							10012			

Trave di fondazione: 9003 [28,29], Pilastrate [--,--] Sez. R: By=60.0 cm Bz=50.0 cm L=240.0 cm Ln=240.0 cm Terreno=Terreno1 Criterio : CLS_TraviFondazione_Rett - Verifica a flessione: **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	1150	408	219	--	6.03	6.03	10012	10012	2	(8+9)-VI-4	7.3
24.0	1404	172	151	203	6.03	6.03	10012	10012	2	(8+9)-VI-4	6.4

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
CAMP	1796	241	--	64	6.03	6.03	10012	10012	2	(8+9)-V-3	5.6
216.0	1251	316	148	208	6.03	6.03	10012	10012	2	(8+9)-V-3	7.2
FLN	1204	557	2	--	6.03	6.03	10012	10012	(8+9)-V-2	(8+9)-V-3	8.3

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	9.6	45.9	0.210	9.6	45.9	0.209	10012	10012	2	(8+9)-VI-4	Parz.	Parz.
24.0	9.6	45.9	0.210	9.6	45.9	0.209	10012	10012	2	(8+9)-VI-4	Parz.	Parz.
CAMP	9.7	45.9	0.210	9.6	45.9	0.209	10012	10012	2	(8+9)-V-3	Parz.	Parz.
216.0	9.6	45.9	0.210	9.6	45.9	0.209	10012	10012	2	(8+9)-V-3	Parz.	Parz.
FLN	9.6	45.9	0.210	9.6	45.9	0.210	10012	10012	(8+9)-V-2	(8+9)-V-3	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500 Comb: Sin=(8+9)-VI-2 Cen=(8+9)-VI-3 Des=(8+9)-VI-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	1734	--	60298	40627	40627	0	10012	50.0	10.05	23
Cen	1250	--	60298	37725	37725	--	--	--	9.34	30
Des	1761	--	60298	40627	40627	0	10012	50.0	10.05	23

Trave di fondazione: 9003 [27,28], Pilastrate [--,--] Sez. R: By=60.0 cm Bz=50.0 cm L=30.0 cm Ln=30.0 cm Terreno=Terreno1 Criterio : CLS_TraviFondazione_Rett - Verifica a flessione: **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	908	108	153	172	8.04	8.04	13238	13238	2	(8+9)-VI-4	12
3.0	936	113	144	209	8.04	8.04	13238	13238	2	(8+9)-VI-4	12
CAMP	1037	326	113	88	8.04	8.04	13238	13238	(8+9)-VI-1	(8+9)-VI-4	12
27.0	1093	370	57	45	8.04	8.04	13238	13238	(8+9)-VI-1	(8+9)-VI-4	12
FLN	1150	414	--	--	8.04	8.04	13238	13238	(8+9)-VI-1	(8+9)-VI-4	12

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.7	45.9	0.233	10.7	45.9	0.233	13238	13238	2	(8+9)-VI-4	Parz.	Parz.
3.0	10.7	45.9	0.233	10.7	45.9	0.233	13238	13238	2	(8+9)-VI-4	Parz.	Parz.
CAMP	10.7	45.9	0.234	10.7	45.9	0.233	13238	13238	(8+9)-VI-1	(8+9)-VI-4	Parz.	Parz.
27.0	10.7	45.9	0.234	10.7	45.9	0.233	13238	13238	(8+9)-VI-1	(8+9)-VI-4	Parz.	Parz.
FLN	10.7	45.9	0.234	10.7	45.9	0.233	13238	13238	(8+9)-VI-1	(8+9)-VI-4	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ =2.500 Comb: (8+9)-VI-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	2209	--	60298	40627	40627	0	13238	30.0	10.05	18
Des							13238			

Trave di fondazione: 9003 [26,27], Pilastrate [--,--] Sez. R: By=60.0 cm Bz=50.0 cm L=220.0 cm Ln=220.0 cm Terreno=Terreno1 Criterio : CLS_TraviFondazione_Rett - Verifica a flessione: **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	1857	3590	--	--	6.03	6.03	10012	10012	(8+9)-VI-3	(8+9)-VI-2	2.8
22.0	1419	2692	411	843	6.03	6.03	10012	10012	(8+9)-VI-3	(8+9)-VI-2	2.8
CAMP	1172	2146	232	513	6.03	6.03	10012	10012	(8+9)-VI-3	(8+9)-VI-2	3.8
198.0	862	166	122	43	6.03	6.03	10012	10012	2	(8+9)-V-4	10
FLN	992	202	--	--	6.03	6.03	10012	10012	2	(8+9)-V-4	10

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	9.7	45.9	0.210	9.7	45.9	0.212	10012	10012	(8+9)-VI-3	(8+9)-VI-2	Parz.	Parz.
22.0	9.7	45.9	0.210	9.7	45.9	0.212	10012	10012	(8+9)-VI-3	(8+9)-VI-2	Parz.	Parz.
CAMP	9.6	45.9	0.210	9.7	45.9	0.211	10012	10012	(8+9)-VI-3	(8+9)-VI-2	Parz.	Parz.
198.0	9.6	45.9	0.210	9.6	45.9	0.209	10012	10012	2	(8+9)-V-4	Parz.	Parz.
FLN	9.6	45.9	0.210	9.6	45.9	0.209	10012	10012	2	(8+9)-V-4	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500 Comb: Sin=(8+9)-V-2 Cen=(8+9)-V-2 Des=(8+9)-VI-2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	4365	--	60298	40627	40627	0	10012	50.0	10.05	9.3
Cen	3244	--	60298	37241	37241	--	--	--	9.22	11
Des	1526	--	60298	40627	40627	0	10012	50.0	10.05	27

Trave di fondazione: 9003 [21,26], Pilastrate [--,--] Sez. R: By=60.0 cm Bz=50.0 cm L=80.0 cm Ln=80.0 cm Terreno=Terreno1 Criterio : CLS_TraviFondazione_Rett - Verifica a flessione: **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	433	3510	--	--	6.03	6.03	10012	10012	(8+9)-VII-4	2	2.9
8.0	387	3398	46	113	6.03	6.03	10012	10012	(8+9)-VII-4	2	2.9
CAMP	1602	3454	399	164	6.03	6.03	10012	10012	(8+9)-VI-3	(8+9)-VI-2	2.8
72.0	1796	3527	205	90	6.03	6.03	10012	10012	(8+9)-VI-3	(8+9)-VI-2	2.8
FLN	2000	3617	--	--	6.03	6.03	10012	10012	(8+9)-VI-3	(8+9)-VI-2	2.8

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	9.6	45.9	0.209	9.7	45.9	0.212	10012	10012	(8+9)-VII-4	2	Parz.	Parz.
8.0	9.6	45.9	0.209	9.7	45.9	0.212	10012	10012	(8+9)-VII-4	2	Parz.	Parz.
CAMP	9.7	45.9	0.210	9.7	45.9	0.212	10012	10012	(8+9)-VI-3	(8+9)-VI-2	Parz.	Parz.
72.0	9.7	45.9	0.210	9.7	45.9	0.212	10012	10012	(8+9)-VI-3	(8+9)-VI-2	Parz.	Parz.
FLN	9.7	45.9	0.210	9.7	45.9	0.212	10012	10012	(8+9)-VI-3	(8+9)-VI-2	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ =2.500 Comb: (8+9)-VI-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	4864	--	60298	40627	40627	0	10012	80.0	10.05	8.4
Des							10012			

Trave di fondazione: 9003 [25,21], Pilastrate [--,--] Sez. R: By=60.0 cm Bz=50.0 cm L=55.2 cm Ln=55.2 cm Terreno=Terreno1 Criterio : CLS_TraviFondazione_Rett - Verifica a flessione: **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	1560	2875	--	--	6.03	6.03	10012	10012	(8+9)-VI-4	(8+9)-VI-1	3.5
5.5	1438	2817	122	58	6.03	6.03	10012	10012	(8+9)-VI-4	(8+9)-VI-1	3.5
CAMP	1216	2931	345	253	6.03	6.03	10012	10012	(8+9)-VI-4	2	3.1
49.7	808	3055	174	129	6.03	6.03	10012	10012	(8+9)-VI-4	2	3.1
FLN	794	3184	123	--	6.03	6.03	10012	10012	(8+9)-VI-4	2	3.1

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	9.6	45.9	0.210	9.7	45.9	0.211	10012	10012	(8+9)-VI-4	(8+9)-VI-1	Parz.	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
5.5	9.6	45.9	0.210	9.7	45.9	0.211	10012	10012	(8+9)-VI-4	(8+9)-VI-1	Parz.	Parz.
CAMP	9.6	45.9	0.210	9.7	45.9	0.211	10012	10012	(8+9)-VI-4	2	Parz.	Parz.
49.7	9.6	45.9	0.210	9.7	45.9	0.211	10012	10012	(8+9)-VI-4	2	Parz.	Parz.
FLN	9.6	45.9	0.210	9.7	45.9	0.211	10012	10012	(8+9)-VI-4	2	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$ Comb: (8+9)-V-2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	3999	--	60298	40918	40918	0	10012	55.2	10.13	10
Des							10012			

Trave di fondazione: 9003 [24,25], Pilastrate [--,--] Sez. R: By=60.0 cm Bz=50.0 cm L=100.0 cm
Ln=100.0 cm Terreno=Terreno1 Criterio : CLS_TraviFondazione_Rett - Verifica a flessione: **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	1236	1307	--	--	6.03	6.03	10012	10012	(8+9)-VI-3	(8+9)-VI-2	7.7
10.0	860	975	376	332	6.03	6.03	10012	10012	(8+9)-VI-3	(8+9)-VI-2	7.7
CAMP	946	1767	528	867	6.03	6.03	10012	10012	(8+9)-VI-4	(8+9)-VI-1	3.8
90.0	1213	2198	262	436	6.03	6.03	10012	10012	(8+9)-VI-4	(8+9)-VI-1	3.8
FLN	1475	2634	--	--	6.03	6.03	10012	10012	(8+9)-VI-4	(8+9)-VI-1	3.8

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	9.6	45.9	0.210	9.6	45.9	0.210	10012	10012	(8+9)-VI-3	(8+9)-VI-2	Parz.	Parz.
10.0	9.6	45.9	0.210	9.6	45.9	0.210	10012	10012	(8+9)-VI-3	(8+9)-VI-2	Parz.	Parz.
CAMP	9.6	45.9	0.210	9.7	45.9	0.211	10012	10012	(8+9)-VI-4	(8+9)-VI-1	Parz.	Parz.
90.0	9.6	45.9	0.210	9.7	45.9	0.211	10012	10012	(8+9)-VI-4	(8+9)-VI-1	Parz.	Parz.
FLN	9.6	45.9	0.210	9.7	45.9	0.211	10012	10012	(8+9)-VI-4	(8+9)-VI-1	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$ Comb: (8+9)-VI-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	4388	--	60298	40627	40627	0	10012	100.0	10.05	9.3
Des							10012			

Trave di fondazione: 9003 [23,24], Pilastrate [--,--] Sez. R: By=60.0 cm Bz=50.0 cm L=100.7 cm
Ln=100.7 cm Terreno=Terreno1 Criterio : CLS_TraviFondazione_Rett - Verifica a flessione: **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	1379	910	--	--	6.03	6.03	10012	10012	(8+9)-V-2	(8+9)-V-3	7.3
10.1	1192	844	187	66	6.03	6.03	10012	10012	(8+9)-V-2	(8+9)-V-3	7.3
CAMP	996	737	383	738	6.03	6.03	10012	10012	(8+9)-V-2	(8+9)-VI-2	6.8
90.6	1136	1298	118	177	6.03	6.03	10012	10012	(8+9)-VI-3	(8+9)-VI-2	6.8
FLN	1254	1475	--	--	6.03	6.03	10012	10012	(8+9)-VI-3	(8+9)-VI-2	6.8

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	9.6	45.9	0.210	9.6	45.9	0.210	10012	10012	(8+9)-V-2	(8+9)-V-3	Parz.	Parz.
10.1	9.6	45.9	0.210	9.6	45.9	0.210	10012	10012	(8+9)-V-2	(8+9)-V-3	Parz.	Parz.
CAMP	9.6	45.9	0.210	9.6	45.9	0.210	10012	10012	(8+9)-V-2	(8+9)-VI-2	Parz.	Parz.
90.6	9.6	45.9	0.210	9.6	45.9	0.210	10012	10012	(8+9)-VI-3	(8+9)-VI-2	Parz.	Parz.
FLN	9.6	45.9	0.210	9.6	45.9	0.210	10012	10012	(8+9)-VI-3	(8+9)-VI-2	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$ Comb: (8+9)-VI-2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	2223	--	60298	40627	40627	0	10012	100.7	10.05	18
Des							10012			

Trave di fondazione: 9003 [22,23], Pilastrate [--,--] Sez. R: By=60.0 cm Bz=50.0 cm L=120.0 cm
 Ln=120.0 cm Terreno=Terreno1 Criterio : CLS_TraviFondazione_Rett - Verifica a flessione: **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	4400	3051	--	--	6.03	6.03	10012	10012	(8+9)-VI-3	(8+9)-VI-2	2.3
12.0	2683	1394	1717	1657	6.03	6.03	10012	10012	(8+9)-VI-3	(8+9)-VI-2	2.3
CAMP	3250	2029	857	746	6.03	6.03	10012	10012	(8+9)-II-3	(8+9)-II-2	2.4
108.0	952	544	300	342	6.03	6.03	10012	10012	(8+9)-VIII-1	(8+9)-V-3	8.0
FLN	1216	886	--	--	6.03	6.03	10012	10012	(8+9)-V-2	(8+9)-V-3	8.2

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	9.7	45.9	0.212	9.7	45.9	0.211	10012	10012	(8+9)-VI-3	(8+9)-VI-2	Parz.	Parz.
12.0	9.7	45.9	0.212	9.7	45.9	0.211	10012	10012	(8+9)-VI-3	(8+9)-VI-2	Parz.	Parz.
CAMP	9.7	45.9	0.212	9.7	45.9	0.211	10012	10012	(8+9)-II-3	(8+9)-II-2	Parz.	Parz.
108.0	9.6	45.9	0.210	9.6	45.9	0.210	10012	10012	(8+9)-VIII-1	(8+9)-V-3	Parz.	Parz.
FLN	9.6	45.9	0.210	9.6	45.9	0.210	10012	10012	(8+9)-V-2	(8+9)-V-3	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Des=2.500 Comb: Sin=(8+9)-VI-3 Des=(8+9)-VI-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	4656	--	60298	37477	37477	0	10012	60.0	9.27	8.0
Des	4681	--	60298	40627	40627	0	10012	60.0	10.05	8.7

Trave di fondazione: 9003 [18,22], Pilastrate [--,--] Sez. R: By=60.0 cm Bz=50.0 cm L=229.3 cm
 Ln=229.3 cm Terreno=Terreno1 Criterio : CLS_TraviFondazione_Rett - Verifica a flessione: **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	1392	447	--	--	6.03	6.03	10012	10012	(8+9)-VI-2	(8+9)-VI-3	7.2
22.9	1280	-229	135	609	6.03	6.03	10012	10012	2	(8+9)-VI-3	7.1
CAMP	4047	2982	395	300	6.03	6.03	10012	10012	(8+9)-VI-3	(8+9)-VI-2	2.3
206.4	4485	3315	--	--	6.03	6.03	10012	10012	(8+9)-VI-3	(8+9)-VI-2	2.2
FLN	4338	3221	--	--	6.03	6.03	10012	10012	(8+9)-VI-3	(8+9)-VI-2	2.3

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	9.6	45.9	0.210	9.6	45.9	0.209	10012	10012	(8+9)-VI-2	(8+9)-VI-3	Parz.	Parz.
22.9	9.6	45.9	0.210	9.6	45.9	0.209	10012	10012	2	(8+9)-VI-3	Parz.	Parz.
CAMP	9.7	45.9	0.212	9.7	45.9	0.211	10012	10012	(8+9)-VI-3	(8+9)-VI-2	Parz.	Parz.
206.4	9.7	45.9	0.212	9.7	45.9	0.211	10012	10012	(8+9)-VI-3	(8+9)-VI-2	Parz.	Parz.
FLN	9.7	45.9	0.212	9.7	45.9	0.211	10012	10012	(8+9)-VI-3	(8+9)-VI-2	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Des=2.500 Comb: Sin=(8+9)-VI-4 Des=(8+9)-VI-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	2833	--	60298	40627	40627	0	10012	114.7	10.05	14
Des	2736	--	60298	37477	37477	0	10012	114.7	9.27	14

Trave di fondazione: 9004 [7,15], Pilastrate [--,--] Sez. R: By=60.0 cm Bz=50.0 cm L=1295.9 cm

Ln=1295.9 cm Terreno=Terreno1 Criterio : CLS_TraviFondazione_Rett - Verifica a flessione: **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	908	727	--	--	6.03	6.03	10012	10012	(8+9)-V-2	(8+9)-V-3	11
129.6	1981	2679	144	--	6.03	6.03	10012	10012	(8+9)-V-3	(8+9)-V-2	3.7
CAMP	2885	3359	--	--	6.03	6.03	10012	10012	(8+9)-V-3	(8+9)-V-2	3.0
1166.3	-1858	2878	4599	--	6.03	6.03	10012	10012	(8+9)-V-3	(8+9)-VII-4	3.5
FLN	145	286	291	310	6.03	6.03	10012	10012	(8+9)-II-1	(8+9)-II-4	17

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	9.6	45.9	0.210	9.6	45.9	0.210	10012	10012	(8+9)-V-2	(8+9)-V-3	Parz.	Parz.
129.6	9.7	45.9	0.211	9.7	45.9	0.211	10012	10012	(8+9)-V-3	(8+9)-V-2	Parz.	Parz.
CAMP	9.7	45.9	0.211	9.7	45.9	0.211	10012	10012	(8+9)-V-3	(8+9)-V-2	Parz.	Parz.
1166.3	9.7	45.9	0.211	9.7	45.9	0.211	10012	10012	(8+9)-V-3	(8+9)-VII-4	Parz.	Parz.
FLN	9.6	45.9	0.209	9.6	45.9	0.210	10012	10012	(8+9)-II-1	(8+9)-II-4	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500 Comb: Sin=(8+9)-V-2 Cen=(8+9)-V-3 Des=(8+9)-VII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	3047	--	60298	40627	40627	0	10012	50.0	10.05	13
Cen	4446	--	60298	37029	37029	--	--	--	9.16	8.3
Des	2981	--	60298	40627	40627	0	10012	50.0	10.05	14

Trave di fondazione: 9005 [15,16], Pilastrate [--,--] Sez. R: By=60.0 cm Bz=50.0 cm L=50.0 cm Ln=50.0 cm Terreno=Terreno1 Criterio : CLS_TraviFondazione_Rett - Verifica a flessione: **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	635	708	609	251	6.03	6.03	10012	10012	(8+9)-V-3	(8+9)-V-2	8.0
5.0	776	755	616	336	6.03	6.03	10012	10012	(8+9)-V-3	(8+9)-V-2	7.2
CAMP	1853	1347	309	180	6.03	6.03	10012	10012	(8+9)-V-3	(8+9)-V-2	4.6
45.0	2009	1437	153	90	6.03	6.03	10012	10012	(8+9)-V-3	(8+9)-V-2	4.6
FLN	2162	1527	--	--	6.03	6.03	10012	10012	(8+9)-V-3	(8+9)-V-2	4.6

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	9.6	45.9	0.210	9.6	45.9	0.210	10012	10012	(8+9)-V-3	(8+9)-V-2	Parz.	Parz.
5.0	9.6	45.9	0.210	9.6	45.9	0.210	10012	10012	(8+9)-V-3	(8+9)-V-2	Parz.	Parz.
CAMP	9.7	45.9	0.211	9.6	45.9	0.210	10012	10012	(8+9)-V-3	(8+9)-V-2	Parz.	Parz.
45.0	9.7	45.9	0.211	9.6	45.9	0.210	10012	10012	(8+9)-V-3	(8+9)-V-2	Parz.	Parz.
FLN	9.7	45.9	0.211	9.6	45.9	0.210	10012	10012	(8+9)-V-3	(8+9)-V-2	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ =2.500 Comb: (8+9)-VI-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	3775	--	60298	40643	40643	0	10012	50.0	10.06	11
Des							10012			

Trave di fondazione: 9005 [16,17], Pilastrate [--,--] Sez. R: By=60.0 cm Bz=50.0 cm L=120.0 cm Ln=120.0 cm Terreno=Terreno1 Criterio : CLS_TraviFondazione_Rett - Verifica a flessione: **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
ILN	2049	1491	--	--	6.03	6.03	10012	10012	(8+9)-VI-3	(8+9)-VI-2	4.9
12.0	1757	990	292	500	6.03	6.03	10012	10012	(8+9)-VI-3	(8+9)-VI-2	4.9
CAMP	2195	800	973	913	6.03	6.03	10012	10012	(8+9)-VI-2	(8+9)-VI-3	3.2
108.0	2756	1321	571	543	6.03	6.03	10012	10012	(8+9)-VI-2	(8+9)-VI-3	3.0
FLN	3327	1864	--	--	6.03	6.03	10012	10012	(8+9)-VI-2	(8+9)-VI-3	3.0

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	9.7	45.9	0.211	9.6	45.9	0.210	10012	10012	(8+9)-VI-3	(8+9)-VI-2	Parz.	Parz.
12.0	9.7	45.9	0.211	9.6	45.9	0.210	10012	10012	(8+9)-VI-3	(8+9)-VI-2	Parz.	Parz.
CAMP	9.7	45.9	0.211	9.7	45.9	0.210	10012	10012	(8+9)-VI-2	(8+9)-VI-3	Parz.	Parz.
108.0	9.7	45.9	0.211	9.7	45.9	0.210	10012	10012	(8+9)-VI-2	(8+9)-VI-3	Parz.	Parz.
FLN	9.7	45.9	0.211	9.7	45.9	0.210	10012	10012	(8+9)-VI-2	(8+9)-VI-3	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$ Comb: (8+9)-VI-2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	4848	--	60298	40627	40627	0	10012	120.0	10.05	8.4
Des							10012			

Trave di fondazione: 9005 [17,18], Pilastrate [--,--] Sez. R: By=60.0 cm Bz=50.0 cm L=68.2 cm Ln=68.2 cm Terreno=Terreno1 Criterio : CLS_TraviFondazione_Rett - Verifica a flessione: **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	3333	2118	--	--	6.03	6.03	10012	10012	(8+9)-VI-2	(8+9)-VI-3	3.0
6.8	3184	1971	148	148	6.03	6.03	10012	10012	(8+9)-VI-2	(8+9)-VI-3	3.0
CAMP	2896	1696	436	423	6.03	6.03	10012	10012	(8+9)-VI-2	(8+9)-VI-3	3.0
61.4	2140	1227	243	142	6.03	6.03	10012	10012	(8+9)-VI-2	(8+9)-VI-3	4.2
FLN	2078	1204	218	107	6.03	6.03	10012	10012	(8+9)-VI-2	(8+9)-VI-3	4.4

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	9.7	45.9	0.211	9.7	45.9	0.211	10012	10012	(8+9)-VI-2	(8+9)-VI-3	Parz.	Parz.
6.8	9.7	45.9	0.211	9.7	45.9	0.211	10012	10012	(8+9)-VI-2	(8+9)-VI-3	Parz.	Parz.
CAMP	9.7	45.9	0.211	9.7	45.9	0.211	10012	10012	(8+9)-VI-2	(8+9)-VI-3	Parz.	Parz.
61.4	9.7	45.9	0.211	9.6	45.9	0.210	10012	10012	(8+9)-VI-2	(8+9)-VI-3	Parz.	Parz.
FLN	9.7	45.9	0.211	9.6	45.9	0.210	10012	10012	(8+9)-VI-2	(8+9)-VI-3	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$ Comb: (8+9)-V-2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	2329	--	60298	41699	41699	0	10012	68.2	10.32	18
Des							10012			

Trave di fondazione: 9006 [14,19], Pilastrate [--,--] Sez. R: By=60.0 cm Bz=50.0 cm L=420.0 cm Ln=420.0 cm Terreno=Terreno1 Criterio : CLS_TraviFondazione_Rett - Verifica a flessione: **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	1491	491	--	40	6.03	6.03	10012	10012	(8+9)-I-1	(8+9)-I-4	6.7
42.0	1315	572	86	--	6.03	6.03	10012	10012	(8+9)-I-1	(8+9)-I-4	7.1
CAMP	922	1284	194	220	6.03	6.03	10012	10012	(8+9)-I-1	(8+9)-I-1	6.7
378.0	949	1733	62	--	6.03	6.03	10012	10012	(8+9)-I-4	(8+9)-I-1	5.8
FLN	1076	1165	--	279	6.03	6.03	10012	10012	(8+9)-I-4	(8+9)-I-1	6.9

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	9.6	45.9	0.210	9.6	45.9	0.210	10012	10012	(8+9)-I-1	(8+9)-I-4	Parz.	Parz.
42.0	9.6	45.9	0.210	9.6	45.9	0.210	10012	10012	(8+9)-I-1	(8+9)-I-4	Parz.	Parz.
CAMP	9.6	45.9	0.210	9.6	45.9	0.210	10012	10012	(8+9)-I-1	(8+9)-I-1	Parz.	Parz.
378.0	9.6	45.9	0.210	9.7	45.9	0.210	10012	10012	(8+9)-I-4	(8+9)-I-1	Parz.	Parz.
FLN	9.6	45.9	0.210	9.6	45.9	0.210	10012	10012	(8+9)-I-4	(8+9)-I-1	Parz.	Parz.

Verifica a taglio: $\cot(\theta) \sin=2.500, \cot(\theta) \cos=2.500$ Comb: $\sin=(8+9)-I-1$ $\cos=3$

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	1494	--	60298	40627	40627	0	10012	210.0	10.05	27
Des	2653	--	60298	37169	37169	0	10012	210.0	9.20	14

Trave di fondazione: 9006 [19,20], Pilastrate [--,--] Sez. R: $B_y=60.0$ cm $B_z=50.0$ cm $L=180.0$ cm
 $L_n=180.0$ cm Terreno=Terreno1 Criterio : CLS_TraviFondazione_Rett - Verifica a flessione: **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	1173	1290	--	--	6.03	6.03	10012	10012	(8+9)-I-4	(8+9)-I-1	7.8
18.0	979	709	194	581	6.03	6.03	10012	10012	(8+9)-I-4	(8+9)-I-1	7.8
CAMP	1093	421	236	625	6.03	6.03	10012	10012	(8+9)-I-1	(8+9)-I-4	7.5
162.0	1300	964	197	557	6.03	6.03	10012	10012	(8+9)-I-1	(8+9)-I-4	6.6
FLN	1496	1521	--	--	6.03	6.03	10012	10012	(8+9)-I-1	(8+9)-I-4	6.6

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	9.6	45.9	0.210	9.6	45.9	0.210	10012	10012	(8+9)-I-4	(8+9)-I-1	Parz.	Parz.
18.0	9.6	45.9	0.210	9.6	45.9	0.210	10012	10012	(8+9)-I-4	(8+9)-I-1	Parz.	Parz.
CAMP	9.6	45.9	0.210	9.6	45.9	0.210	10012	10012	(8+9)-I-1	(8+9)-I-4	Parz.	Parz.
162.0	9.6	45.9	0.210	9.6	45.9	0.210	10012	10012	(8+9)-I-1	(8+9)-I-4	Parz.	Parz.
FLN	9.6	45.9	0.210	9.6	45.9	0.210	10012	10012	(8+9)-I-1	(8+9)-I-4	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$ Comb: (8+9)-I-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	3282	--	60298	37169	37169	0	10012	180.0	9.20	11
Des							10012			

Trave di fondazione: 9006 [20,8], Pilastrate [--,--] Sez. R: $B_y=60.0$ cm $B_z=50.0$ cm $L=364.3$ cm
 $L_n=364.3$ cm Terreno=Terreno1 Criterio : CLS_TraviFondazione_Rett - Verifica a flessione: **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	1387	1390	--	141	6.03	6.03	10012	10012	(8+9)-I-1	(8+9)-I-4	6.5
36.4	1155	1638	132	--	6.03	6.03	10012	10012	(8+9)-I-1	(8+9)-I-4	6.1
CAMP	947	1481	118	89	6.03	6.03	10012	10012	(8+9)-I-1	(8+9)-I-4	6.4
327.9	294	--	144	95	6.03	6.03	10012	10012	2	(8+9)-I-1	23
FLN	548	167	--	--	6.03	6.03	10012	10012	2	(8+9)-I-1	18

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	9.6	45.9	0.210	9.6	45.9	0.210	10012	10012	(8+9)-I-1	(8+9)-I-4	Parz.	Parz.
36.4	9.6	45.9	0.210	9.7	45.9	0.210	10012	10012	(8+9)-I-1	(8+9)-I-4	Parz.	Parz.
CAMP	9.6	45.9	0.210	9.6	45.9	0.210	10012	10012	(8+9)-I-1	(8+9)-I-4	Parz.	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
327.9	9.6	45.9	0.209	9.6	45.9	0.209	10012	10012	2	(8+9)-I-1	Parz.	Parz.
FLN	9.6	45.9	0.210	9.6	45.9	0.209	10012	10012	2	(8+9)-I-1	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Des=2.500 Comb: Sin=3 Des=(8+9)-II-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	1837	--	60298	37169	37169	0	10012	182.2	9.20	20
Des	1144	--	60298	40627	40627	0	10012	182.2	10.05	36

Trave di fondazione: 9007 [6,106], Pilastrate [--,--] Sez. R: By=60.0 cm Bz=50.0 cm L=172.0 cm
Ln=172.0 cm Terreno=Terreno1 Criterio : CLS_TraviFondazione - Verifica a flessione: **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	3139	1951	--	--	6.03	7.60	10019	12520	(8+9)-VIII-1	(8+9)-VIII-4	3.2
17.2	2633	1443	506	508	6.03	7.60	10019	12520	(8+9)-VIII-1	(8+9)-VIII-4	3.2
CAMP	2129	962	606	583	6.03	7.60	10019	12520	(8+9)-VIII-1	(8+9)-VIII-4	3.7
154.8	1226	988	7	433	6.03	7.60	10019	12520	2	(8+9)-VIII-1	8.1
FLN	1208	1421	18	--	6.03	7.60	10019	12520	2	(8+9)-VIII-1	8.2

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	9.5	45.9	0.207	10.7	45.9	0.233	10019	12520	(8+9)-VIII-1	(8+9)-VIII-4	Parz.	Parz.
17.2	9.5	45.9	0.207	10.7	45.9	0.233	10019	12520	(8+9)-VIII-1	(8+9)-VIII-4	Parz.	Parz.
CAMP	9.5	45.9	0.207	10.7	45.9	0.233	10019	12520	(8+9)-VIII-1	(8+9)-VIII-4	Parz.	Parz.
154.8	9.5	45.9	0.206	10.7	45.9	0.233	10019	12520	2	(8+9)-VIII-1	Parz.	Parz.
FLN	9.5	45.9	0.206	10.7	45.9	0.233	10019	12520	2	(8+9)-VIII-1	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ =2.500 Comb: (8+9)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	3031	--	60298	40627	40627	0	12520	172.0	10.05	13
Des							10019			

Trave di fondazione: 9007 [6,21], Pilastrate [--,--] Sez. R: By=60.0 cm Bz=50.0 cm L=1324.7 cm
Ln=1324.7 cm Terreno=Terreno1 Criterio : CLS_TraviFondazione_Rett - Verifica a flessione: **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	2483	723	--	--	6.03	6.03	10012	10012	(8+9)-VIII-1	(8+9)-VIII-4	4.0
132.5	462	207	315	80	6.03	6.03	10012	10012	(8+9)-VIII-1	(8+9)-VIII-4	13
CAMP	477	956	--	--	6.03	12.06	10032	19484	(8+9)-V-2	2	20
1192.2	531	533	--	13	6.03	6.03	10012	10012	(8+9)-V-1	(8+9)-VII-4	18
FLN	1222	6	--	31	6.03	6.03	10012	10012	2	(8+9)-VI-2	8.2

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	9.7	45.9	0.211	9.6	45.9	0.210	10012	10012	(8+9)-VIII-1	(8+9)-VIII-4	Parz.	Parz.
132.5	9.6	45.9	0.210	9.6	45.9	0.209	10012	10012	(8+9)-VIII-1	(8+9)-VIII-4	Parz.	Parz.
CAMP	9.0	45.9	0.196	13.1	45.9	0.285	10032	19484	(8+9)-V-2	2	Parz.	Parz.
1192.2	9.6	45.9	0.210	9.6	45.9	0.210	10012	10012	(8+9)-V-1	(8+9)-VII-4	Parz.	Parz.
FLN	9.6	45.9	0.210	9.6	45.9	0.209	10012	10012	2	(8+9)-VI-2	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500 Comb: Sin=3 Cen=3 Des=3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	2237	--	60298	40627	40627	0	10012	50.0	10.05	18
Cen	2344	--	60298	36933	36933	--	--	--	9.14	16
Des	1204	--	60298	40627	40627	0	10012	50.0	10.05	34

Trave di fondazione: 9008 [12,35], Pilastrate [--,--] Sez. R: By=60.0 cm Bz=50.0 cm L=150.0 cm
Ln=150.0 cm Terreno=Terreno1 Criterio : CLS_TraviFondazione_Rett - Verifica a flessione: **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	720	113	--	--	6.03	6.03	10012	10012	(8+9)-I-1	(8+9)-I-4	14
15.0	610	76	111	37	6.03	6.03	10012	10012	(8+9)-I-1	(8+9)-I-4	14
CAMP	495	313	156	--	6.03	6.03	10012	10012	(8+9)-I-1	(8+9)-I-1	15
135.0	533	279	2	--	6.03	6.03	10012	10012	(8+9)-I-4	(8+9)-I-1	19
FLN	535	250	--	--	6.03	6.03	10012	10012	(8+9)-I-4	(8+9)-I-1	19

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	9.6	45.9	0.210	9.6	45.9	0.209	10012	10012	(8+9)-I-1	(8+9)-I-4	Parz.	Parz.
15.0	9.6	45.9	0.210	9.6	45.9	0.209	10012	10012	(8+9)-I-1	(8+9)-I-4	Parz.	Parz.
CAMP	9.6	45.9	0.210	9.6	45.9	0.209	10012	10012	(8+9)-I-1	(8+9)-I-1	Parz.	Parz.
135.0	9.6	45.9	0.210	9.6	45.9	0.209	10012	10012	(8+9)-I-4	(8+9)-I-1	Parz.	Parz.
FLN	9.6	45.9	0.210	9.6	45.9	0.209	10012	10012	(8+9)-I-4	(8+9)-I-1	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$ Comb: (8+9)-I-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	1128	--	60298	40627	40627	0	10012	150.0	10.05	36
Des							10012			

Trave di fondazione: 9008 [35,36], Pilastrate [--,--] Sez. R: By=60.0 cm Bz=50.0 cm L=80.0 cm Ln=80.0 cm Terreno=Terreno1 Criterio : CLS_TraviFondazione_Rett - Verifica a flessione: **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	596	203	--	--	6.03	6.03	10012	10012	(8+9)-I-4	(8+9)-I-1	17
8.0	529	99	67	104	6.03	6.03	10012	10012	(8+9)-I-4	(8+9)-I-1	17
CAMP	486	27	133	246	6.03	6.03	10012	10012	(8+9)-III-1	(8+9)-III-4	16
72.0	552	147	67	125	6.03	6.03	10012	10012	(8+9)-III-1	(8+9)-III-4	16
FLN	619	272	--	--	6.03	6.03	10012	10012	(8+9)-III-1	(8+9)-III-4	16

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	9.6	45.9	0.210	9.6	45.9	0.209	10012	10012	(8+9)-I-4	(8+9)-I-1	Parz.	Parz.
8.0	9.6	45.9	0.210	9.6	45.9	0.209	10012	10012	(8+9)-I-4	(8+9)-I-1	Parz.	Parz.
CAMP	9.6	45.9	0.210	9.6	45.9	0.209	10012	10012	(8+9)-III-1	(8+9)-III-4	Parz.	Parz.
72.0	9.6	45.9	0.210	9.6	45.9	0.209	10012	10012	(8+9)-III-1	(8+9)-III-4	Parz.	Parz.
FLN	9.6	45.9	0.210	9.6	45.9	0.209	10012	10012	(8+9)-III-1	(8+9)-III-4	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$ Comb: (8+9)-I-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	1605	--	60298	40627	40627	0	10012	80.0	10.05	25
Des							10012			

Trave di fondazione: 9008 [36,11], Pilastrate [--,--] Sez. R: By=60.0 cm Bz=50.0 cm L=529.1 cm

Ln=529.1 cm Terreno=Terreno1 Criterio : CLS_TraviFondazione_Rett - Verifica a flessione: **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	614	218	--	79	6.03	6.03	10012	10012	(8+9)-III-1	(8+9)-III-4	16
52.9	444	420	66	--	6.03	6.03	10012	10012	(8+9)-III-1	(8+9)-III-4	20
CAMP	345	425	--	--	6.03	6.03	10012	10012	(8+9)-I-1	(8+9)-III-3	24
476.2	378	2	1	48	6.03	6.03	10012	10012	2	(8+9)-I-4	26
FLN	381	32	--	12	6.03	6.03	10012	10012	2	(8+9)-I-4	26

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	9.6	45.9	0.210	9.6	45.9	0.209	10012	10012	(8+9)-III-1	(8+9)-III-4	Parz.	Parz.
52.9	9.6	45.9	0.209	9.6	45.9	0.209	10012	10012	(8+9)-III-1	(8+9)-III-4	Parz.	Parz.
CAMP	9.6	45.9	0.209	9.6	45.9	0.209	10012	10012	(8+9)-I-1	(8+9)-III-3	Parz.	Parz.
476.2	9.6	45.9	0.209	9.6	45.9	0.209	10012	10012	2	(8+9)-I-4	Parz.	Parz.
FLN	9.6	45.9	0.209	9.6	45.9	0.209	10012	10012	2	(8+9)-I-4	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500 Comb: Sin=3 Cen=3 Des=(8+9)-VII-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	877	--	60298	40627	40627	0	10012	50.0	10.05	46
Cen	777	--	60298	36933	36933	--	--	--	9.14	48
Des	306	--	60298	40627	40627	0	10012	50.0	10.05	>100

Trave di fondazione: 9009 [13,34], Pilastrate [--,--] Sez. R: By=60.0 cm Bz=50.0 cm L=603.0 cm
Ln=603.0 cm Terreno=Terreno1 Criterio : CLS_TraviFondazione_Rett - Verifica a flessione: **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	1271	917	--	--	6.03	6.03	10012	10012	(8+9)-IV-3	(8+9)-IV-2	7.9
60.3	795	448	163	161	6.03	6.03	10012	10012	(8+9)-IV-3	(8+9)-IV-2	10
CAMP	501	413	--	--	6.03	6.03	10012	10012	(8+9)-VI-2	(8+9)-VI-3	20
542.7	454	385	7	64	6.03	6.03	10012	10012	(8+9)-VI-3	(8+9)-VI-2	22
FLN	474	571	--	--	6.03	6.03	10012	10012	(8+9)-VI-3	(8+9)-VI-2	18

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	9.6	45.9	0.210	9.6	45.9	0.210	10012	10012	(8+9)-IV-3	(8+9)-IV-2	Parz.	Parz.
60.3	9.6	45.9	0.210	9.6	45.9	0.210	10012	10012	(8+9)-IV-3	(8+9)-IV-2	Parz.	Parz.
CAMP	9.6	45.9	0.209	9.6	45.9	0.209	10012	10012	(8+9)-VI-2	(8+9)-VI-3	Parz.	Parz.
542.7	9.6	45.9	0.209	9.6	45.9	0.209	10012	10012	(8+9)-VI-3	(8+9)-VI-2	Parz.	Parz.
FLN	9.6	45.9	0.209	9.6	45.9	0.210	10012	10012	(8+9)-VI-3	(8+9)-VI-2	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500 Comb: Sin=(8+9)-VIII-2 Cen=(8+9)-IV-3 Des=(8+9)-VI-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	870	--	60298	40627	40627	0	10012	50.0	10.05	47
Cen	1477	--	60298	37219	37219	--	--	--	9.21	25
Des	347	--	60298	40627	40627	0	10012	50.0	10.05	>100

Trave di fondazione: 9010 [112,213], Pilastrate [--,--] Sez. R: By=60.0 cm Bz=50.0 cm L=456.6 cm
Ln=456.6 cm Terreno=Terreno1 Criterio : CLS_TraviFondazione - Verifica a flessione: **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
ILN	12	75	14	--	6.03	7.60	10019	12520	(8+9)-V-1	(8+9)-V-4	>100
45.7	56	-45	--	114	6.03	7.60	10019	12520	(8+9)-VI-2	(8+9)-VI-4	>100
CAMP	110	132	105	--	6.03	7.60	10019	12520	(8+9)-IV-3	(8+9)-VIII-2	47
410.9	342	21	67	71	6.03	7.60	10019	12520	(8+9)-IV-3	(8+9)-IV-2	25
FLN	490	178	--	--	6.03	7.60	10019	12520	(8+9)-IV-3	(8+9)-IV-2	20

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	9.4	45.9	0.206	10.6	45.9	0.232	10019	12520	(8+9)-V-1	(8+9)-V-4	Parz.	Parz.
45.7	9.4	45.9	0.206	10.6	45.9	0.232	10019	12520	(8+9)-VI-2	(8+9)-VI-4	Parz.	Parz.
CAMP	9.4	45.9	0.206	10.7	45.9	0.232	10019	12520	(8+9)-IV-3	(8+9)-VIII-2	Parz.	Parz.
410.9	9.4	45.9	0.206	10.7	45.9	0.232	10019	12520	(8+9)-IV-3	(8+9)-IV-2	Parz.	Parz.
FLN	9.4	45.9	0.206	10.7	45.9	0.232	10019	12520	(8+9)-IV-3	(8+9)-IV-2	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Des=2.500 Comb: Sin=(8+9)-VIII-4 Des=(8+9)-III-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	479	--	60298	37000	37000	0	12520	228.3	9.16	77
Des	618	--	60298	40627	40627	0	10019	228.3	10.05	66

Trave di fondazione: 9010 [114,112], Pilastrate [--,--] Sez. R: By=60.0 cm Bz=50.0 cm L=459.1 cm
Ln=459.1 cm Terreno=Terreno1 Criterio : CLS_TraviFondazione - Verifica a flessione: **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	119	83	--	--	6.03	7.60	10019	12520	(8+9)-I-1	(8+9)-I-4	84
45.9	81	-58	17	131	6.03	7.60	10019	12520	(8+9)-III-2	(8+9)-II-4	>100
CAMP	39	83	59	--	6.03	7.60	10019	12520	(8+9)-III-2	(8+9)-III-2	>100
413.1	27	14	--	71	6.03	7.60	10019	12520	(8+9)-III-4	(8+9)-V-2	>100
FLN	--	180	--	--	6.03	7.60	10019	12520			70

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	9.4	45.9	0.206	10.6	45.9	0.232	10019	12520	(8+9)-I-1	(8+9)-I-4	Parz.	Parz.
45.9	9.4	45.9	0.206	10.6	45.9	0.232	10019	12520	(8+9)-III-2	(8+9)-II-4	Parz.	Parz.
CAMP	9.4	45.9	0.206	10.6	45.9	0.232	10019	12520	(8+9)-III-2	(8+9)-III-2	Parz.	Parz.
413.1	9.4	45.9	0.206	10.7	45.9	0.232	10019	12520	(8+9)-III-4	(8+9)-V-2	Parz.	Parz.
FLN	--	--	--	10.7	45.9	0.232	10019	12520	1	2	--	Parz.

Verifica a taglio: $\cot(\theta)$ =2.500 Comb: 3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	602	--	60298	37000	37000	0	12520	459.1	9.16	61
Des							10019			

Trave di fondazione: 9010 [106,114], Pilastrate [--,--] Sez. R: By=60.0 cm Bz=50.0 cm L=615.3 cm
Ln=615.3 cm Terreno=Terreno1 Criterio : CLS_TraviFondazione - Verifica a flessione: **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	255	70	3	13	6.03	7.60	10019	12520	2	(8+9)-V-2	39
61.5	286	107	--	58	6.03	7.60	10019	12520	(8+9)-VII-4	(8+9)-VII-1	35
CAMP	179	281	81	--	6.03	7.60	10019	12520	2	(8+9)-VII-1	38
553.7	55	49	11	65	6.03	7.60	10019	12520	(8+9)-IV-2	(8+9)-VIII-1	>100
FLN	--	282	--	--	6.03	7.60	10019	12520	1	2	44

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	9.4	45.9	0.206	10.6	45.9	0.232	10019	12520	2	(8+9)-V-2	Parz.	Parz.
61.5	9.4	45.9	0.206	10.7	45.9	0.232	10019	12520	(8+9)-VII-4	(8+9)-VII-1	Parz.	Parz.
CAMP	9.4	45.9	0.206	10.7	45.9	0.232	10019	12520	2	(8+9)-VII-1	Parz.	Parz.
553.7	9.4	45.9	0.206	10.7	45.9	0.232	10019	12520	(8+9)-IV-2	(8+9)-VIII-1	Parz.	Parz.
FLN	--	--	--	10.7	45.9	0.232	10019	12520	1	2	--	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Des=2.500 Comb: Sin=3 Des=3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	640	--	60298	40627	40627	0	12520	307.6	10.05	63
Des	727	--	60298	37000	37000	0	10019	307.6	9.16	51

Trave di fondazione: 9011 [213,113], Pilastrate [--,--] Sez. R: By=60.0 cm Bz=50.0 cm L=134.6 cm
Ln=134.6 cm Terreno=Terreno1 Criterio : CLS_TraviFondazione - Verifica a flessione: **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	569	-4	--	22	6.03	7.60	10019	12520	(8+9)-IV-3	(8+9)-IV-2	18
13.5	488	6	81	19	6.03	7.60	10019	12520	(8+9)-IV-3	(8+9)-IV-2	18
CAMP	400	35	131	47	6.03	7.60	10019	12520	(8+9)-IV-3	(8+9)-VIII-2	19
121.2	82	61	40	40	6.03	7.60	10019	12520	(8+9)-IV-3	(8+9)-VIII-2	82
FLN	44	101	55	--	6.03	7.60	10019	12520	(8+9)-IV-3	(8+9)-VIII-2	>100

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	9.4	45.9	0.206	10.6	45.9	0.232	10019	12520	(8+9)-IV-3	(8+9)-IV-2	Parz.	Parz.
13.5	9.4	45.9	0.206	10.6	45.9	0.232	10019	12520	(8+9)-IV-3	(8+9)-IV-2	Parz.	Parz.
CAMP	9.4	45.9	0.206	10.6	45.9	0.232	10019	12520	(8+9)-IV-3	(8+9)-VIII-2	Parz.	Parz.
121.2	9.4	45.9	0.206	10.7	45.9	0.232	10019	12520	(8+9)-IV-3	(8+9)-VIII-2	Parz.	Parz.
FLN	9.4	45.9	0.206	10.7	45.9	0.232	10019	12520	(8+9)-IV-3	(8+9)-VIII-2	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Des=2.500 Comb: Sin=(8+9)-IV-3 Des=(8+9)-III-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	844	--	60298	40627	40627	0	12520	67.3	10.05	48
Des	605	--	60298	37100	37100	0	10019	67.3	9.18	61

Trave di fondazione: 9011 [113,134], Pilastrate [--,--] Sez. R: By=60.0 cm Bz=50.0 cm L=604.1 cm
Ln=604.0 cm Terreno=Terreno1 Criterio : CLS_TraviFondazione - Verifica a flessione: **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	--	134	--	--	6.03	7.60	10019	12520	1	2	93
60.4	68	-68	--	203	6.03	7.60	10019	12520	2	2	93
CAMP	46	153	39	--	6.03	7.60	10019	12520	(8+9)-VI-2	2	82
543.6	161	116	--	50	6.03	7.60	10019	12520	(8+9)-VI-2	(8+9)-V-3	62
FLN	5	267	52	--	6.03	7.60	10019	12520	(8+9)-V-2	(8+9)-I-3	47

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	--	--	--	10.7	45.9	0.232	10019	12520	1	2	--	Parz.
60.4	9.4	45.9	0.206	10.7	45.9	0.232	10019	12520	2	2	Parz.	Parz.
CAMP	9.4	45.9	0.206	10.7	45.9	0.232	10019	12520	(8+9)-VI-2	2	Parz.	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
543.6	9.4	45.9	0.206	10.7	45.9	0.232	10019	12520	(8+9)-VI-2	(8+9)-V-3	Parz.	Parz.
FLN	9.4	45.9	0.206	10.7	45.9	0.232	10019	12520	(8+9)-V-2	(8+9)-I-3	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Des=2.500 Comb: Sin=3 Des=3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	610	--	60298	37100	37100	0	12520	302.0	9.18	61
Des	605	--	60298	40627	40627	0	10019	302.0	10.05	67

Trave di fondazione: 9012 [13,213], Pilastrate [--,--] Sez. R: By=60.0 cm Bz=50.0 cm L=206.2 cm
Ln=206.1 cm Terreno=Terreno1 Criterio : CLS_TraviFondazione - Verifica a flessione: **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	1572	1239	--	--	6.03	7.60	10019	12520	(8+9)-IV-3	(8+9)-IV-2	6.4
20.6	946	839	626	400	6.03	7.60	10019	12520	(8+9)-IV-3	(8+9)-IV-2	6.4
CAMP	597	1148	350	--	6.03	7.60	10019	12520	(8+9)-IV-3	(8+9)-IV-3	11
185.5	11	938	30	210	6.03	7.60	10019	12520	(8+9)-IV-2	(8+9)-IV-3	11
FLN	-32	913	43	25	6.03	7.60	10019	12520	(8+9)-IV-2	(8+9)-IV-3	13

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	9.5	45.9	0.207	10.7	45.9	0.233	10019	12520	(8+9)-IV-3	(8+9)-IV-2	Parz.	Parz.
20.6	9.5	45.9	0.207	10.7	45.9	0.233	10019	12520	(8+9)-IV-3	(8+9)-IV-2	Parz.	Parz.
CAMP	9.5	45.9	0.206	10.7	45.9	0.233	10019	12520	(8+9)-IV-3	(8+9)-IV-3	Parz.	Parz.
185.5	9.4	45.9	0.206	10.7	45.9	0.233	10019	12520	(8+9)-IV-2	(8+9)-IV-3	Parz.	Parz.
FLN	9.4	45.9	0.206	10.7	45.9	0.233	10019	12520	(8+9)-IV-2	(8+9)-IV-3	Parz.	Parz.

Verifica a taglio: $\cot(\theta)$ Sin=2.500, $\cot(\theta)$ Cen=2.500, $\cot(\theta)$ Des=2.500 Comb: Sin=(8+9)-IV-3 Cen=(8+9)-IV-3 Des=(8+9)-IV-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	3052	--	60298	40627	40627	0	12520	50.0	10.05	13
Cen	2916	--	60298	36933	36933	--	--	--	9.14	13
Des	799	--	60298	40627	40627	0	10019	50.0	10.05	51

Verifica dei Muri in calcestruzzo

Scenario di calcolo: **Set_NT_SLV_SLD_A2_STR/GEO_2018**

Simbologia:

Muro	Indice del muro in verifica
Nodi	[n1-n2-n3-n4...] Indici dei nodi di attacco del muro
Pann.X	Numero di pannelli in direzione locale X del muro(per muri a pannelli)
Pann.Y	Numero di pannelli in direzione locale Y del muro(per muri a pannelli)
Pann	Numero totale di pannelli (per muri a mesh)
Spess [cm]	Spessore del muro
Criterio	Criterio di verifica adottato per la verifica
Pannello	Indice del pannello
Nx [kg]	Sforzo in direzione x locale per metro lineare ($N_x = s_{xx} \cdot \text{spessore}$)
Ny [kg]	Sforzo in direzione y locale per metro lineare ($N_y = s_{yy} \cdot \text{spessore}$)
Nxy [kg]	Sforzo tagliante locale per metro lineare ($N_{xy} = s_{xy} \cdot \text{spessore}$)
Mx [kg*m]	Momento in direzione x locale per metro lineare
My [kg*m]	Momento in direzione y locale per metro lineare

Mxy [kg*m]	Momento torcente locale per metro lineare
Ax [mq]	Armatura totale pannello in direzione x locale ⁽¹⁾
Ay [mq]	Armatura totale pannello in direzione y locale ⁽¹⁾
ε_c	Deformazione nel cls ⁽²⁾
ε_f	Deformazione nell'acciaio ⁽²⁾
Massimi	Armature massime riscontrate nel muro
Massimo	massima sigma ideale riscontrata nel muro
$\sigma_{id+}, \sigma_{id-}$ [kg/cmq]	$(\sigma_x^2 + \sigma_y^2 - \sigma_x \sigma_y + 3 \tau_{xy}^2)^{1/2}$ Tensioni ideali ai lembi della lastra (Acciaio)
$\sigma_{id+}, \sigma_{id-}$ [kg/cmq]	$(\sigma_x^2 + \sigma_y^2 - \sigma_x \sigma_y + 3 \tau_{xy}^2)^{1/2}$ Tensioni ideali ai lembi della lastra (Legno)
Fatt.Ampl.Sisma	Fattore moltiplicativo di gruppo per le azioni sismiche (solo se diverso da 1.0)
Cs	Coefficiente di sicurezza definito dal rapporto $ M_r(N) / M_d $ ($M_r(N)$ =Momento resistente corrispondente allo sforzo normale N, M_d =momento agente), quando richiesto dal criterio di verifica
ζ_E	Livello di sicurezza sismico definito come rapporto tra l'accelerazione sopportabile e l'accelerazione di progetto, quando richiesto dal criterio di verifica

Note Verifica muri:

⁽¹⁾: Le armature Ax ed Ay vanno intese come a metro lineare di pannello.

⁽²⁾: Le deformazioni sono stampate a meno del fattore 10^{-3} ; esse si riferiscono alla verifica considerando quali sollecitazioni di progetto $M_{x,d} = M_x \pm |M_{xy}|$, $M_{y,d} = M_y \pm |M_{xy}|$ scegliendo il segno in modo tale da rendere massimo in valore assoluto il relativo momento flettente, le sollecitazioni stampate si riferiscono alle sollecitazioni in una data combinazione riferite al sistema locale del pannello

Muro [Platea]: 1 - Nodi: [15-7-5-6-21-25-24-23-22-18-17-16]Pann=439Spess.=25 cm, Terreno=Terreno1,
 ,Criterio=CLS_Platee, Materiale=C30/37: **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	496	-6345	-1565	-115	-168	295	13.40	16.08	2	12
2	-123	-8452	-2092	-224	-53	386	13.40	16.08	2	8.4
3	-1347	-9295	-2816	-247	78	420	13.40	16.08	2	7.8
4	-2357	-8987	-3322	-253	178	405	13.40	16.08	2	8.1
5	-2809	-8170	-3210	-253	267	341	13.40	16.08	2	9.0
6	-2354	-7684	-2865	-266	339	244	13.40	16.08	2	10
7	-4112	-1281	2225	-488	-12	-42	13.40	16.08	(8+9)-VI-3	10
8	-4537	-2646	2929	-587	49	-137	13.40	16.08	(8+9)-VI-3	7.6
9	-4341	-4673	3083	-560	68	-195	13.40	16.08	(8+9)-VI-3	7.3
10	-3369	-7316	-3051	-747	202	-90	13.40	16.08	2	6.5
11	-3533	-6834	-3006	-764	172	-139	13.40	16.08	2	6.0
12	-3459	-6241	-2954	-742	150	-186	13.40	16.08	2	5.8
13	-3533	-5356	-2949	-696	124	-233	13.40	16.08	2	5.8
14	-3452	-4280	-2891	-659	80	-286	13.40	16.08	2	5.7
15	-3186	-2973	-2806	-596	18	-336	13.40	16.08	2	5.8
16	-3014	-1265	-2672	-485	-58	-377	13.40	16.08	2	6.2
17	-2926	856	-2325	-322	-153	-406	13.40	16.08	2	7.4
18	-2902	3177	-1485	-107	-271	-411	13.40	16.08	2	8.4
19	-3121	4976	129	143	-421	-377	13.40	16.08	2	7.0
20	-5923	8175	1555	238	-636	-180	13.40	16.08	2	6.5
21	-2631	3124	3052	96	-1013	-229	13.40	16.08	2	4.6
22	-1176	545	4134	-106	-1503	-192	13.40	16.08	2	3.5
23	640	-1415	4302	-279	-1935	-167	13.40	16.08	2	2.9
24	2172	-2867	3888	-415	-2303	-139	13.40	16.08	2	2.6
25	3101	-3913	3205	-499	-2620	-110	13.40	16.08	2	2.4
26	3463	-4641	2533	-543	-2906	-78	13.40	16.08	2	2.2
27	3462	-5050	1995	-574	-3131	-58	13.40	16.08	2	2.0
28	3381	-5299	1575	-590	-3266	-51	13.40	16.08	2	2.0
29	3243	-5508	1170	-597	-3367	-46	13.40	16.08	2	1.9
30	2969	-5633	790	-593	-3486	-31	13.40	16.08	2	1.9
31	2590	-5635	556	-595	-3653	-18	13.40	16.08	2	1.8
32	2258	-5639	503	-598	-3767	-17	13.40	16.08	2	1.7
33	2151	-5655	497	-589	-3825	-26	13.40	16.08	2	1.7
34	2179	-5630	453	-600	-3871	-1	13.40	16.08	2	1.7
35	2134	-5618	372	-619	-3903	-5	13.40	16.08	2	1.7
36	2026	-5654	351	-592	-3844	-1	13.40	16.08	2	1.7
37	2022	-5692	379	-572	-3748	-6	13.40	16.08	2	1.8
38	2309	-5751	384	-593	-3762	-8	13.40	16.08	2	1.7
39	2765	-5760	227	-634	-3823	-4	13.40	16.08	2	1.7
40	3067	-5769	-80	-656	-3867	2	13.40	16.08	2	1.7
41	3094	-5766	-397	-652	-3881	9	13.40	16.08	2	1.7
42	3039	-5752	-624	-644	-3854	13	13.40	16.08	2	1.7
43	3118	-5694	-843	-634	-3761	13	13.40	16.08	2	1.7
44	3249	-5584	-1198	-630	-3636	24	13.40	16.08	2	1.8
45	3183	-5381	-1695	-620	-3534	35	13.40	16.08	2	1.8
46	2778	-5014	-2183	-580	-3419	49	13.40	16.08	2	1.9
47	2180	-4557	-2453	-523	-3266	61	13.40	16.08	2	1.9
48	1668	-3906	-2659	-478	-3095	72	13.40	16.08	2	2.0
49	1161	-2993	-2832	-425	-2886	88	13.40	16.08	2	2.1
50	434	-1730	-2906	-345	-2600	115	13.40	16.08	2	2.3
51	-642	138	-2598	-229	-2236	142	13.40	16.08	2	2.5
52	-1764	2635	-1440	-98	-1805	140	13.40	16.08	2	3.0
53	-2826	6759	462	19	-1344	85	13.40	16.08	2	3.8
54	-2654	10188	3056	18	-969	218	13.40	16.08	2	4.3
55	-1823	5341	3798	-128	-857	372	13.40	16.08	2	4.5
56	-1538	1363	4466	-375	-677	489	13.40	16.08	2	5.1
57	-1835	-2281	4473	-572	-525	546	13.40	16.08	2	4.7
58	-1750	-4301	4826	-734	-450	519	13.40	16.08	2	4.2

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
59	-1118	-6739	5096	-810	-293	448	13.40	16.08	2	4.1
60	-1229	-9866	4177	-724	-12	399	13.40	16.08	2	4.6
61	-1544	-11259	2678	-607	143	368	13.40	16.08	2	5.4
62	-1916	-8237	6180	-735	-554	211	13.40	16.08	(8+9)-V-2	5.6
63	906	4297	9021	-778	-490	-158	13.40	16.08	(8+9)-II-2	5.3
64	-2125	-10387	1319	-576	220	245	13.40	16.08	2	6.4
65	-1947	-10063	1230	-533	259	186	13.40	16.08	2	7.3
66	-1690	-9668	1204	-454	302	111	13.40	16.08	2	9.3
67	-4716	407	-2698	-321	-56	70	13.40	16.08	(8+9)-VI-1	14
68	-2101	-7766	5850	161	528	-77	13.40	16.08	(8+9)-V-2	11
69	-2459	-9173	5592	221	642	-145	13.40	16.08	(8+9)-V-2	8.8
70	-965	-10467	1444	-321	319	-288	13.40	16.08	2	8.5
71	243	-9627	319	-341	165	-318	13.40	16.08	2	7.7
72	1536	-7818	-708	-261	-46	-276	13.40	16.08	2	9.2
73	1862	-5657	-511	-187	-155	-197	13.40	16.08	2	13
74	2170	-6822	359	-190	-395	-121	13.40	16.08	2	13
75	2653	-7441	8	-268	-618	-128	13.40	16.08	2	9.0
76	9716	-4093	2176	-605	-471	-102	13.40	16.08	(8+9)-VII-4	5.8
77	10404	-3913	-1988	-654	-449	29	13.40	16.08	(8+9)-VII-4	6.0
78	7779	-3289	-3464	-469	-442	64	13.40	16.08	(8+9)-VII-4	8.1
79	-10280	-965	3186	492	47	-89	13.40	16.08	(8+9)-VII-1	10
80	-9835	-3867	541	446	-198	-71	13.40	16.08	2	12
81	-10385	-3568	2611	477	-175	-88	13.40	16.08	2	11
82	-9734	-3673	4727	445	-208	-103	13.40	16.08	2	11
83	2563	-3640	6135	-163	-467	-127	13.40	16.08	(8+9)-V-2	11
84	5614	-4775	6066	-346	-649	-113	13.40	16.08	(8+9)-V-2	8.5
85	9419	-5409	5045	-623	-858	-117	13.40	16.08	(8+9)-V-2	5.6
86	12072	-5918	2964	-804	-939	-23	13.40	16.08	(8+9)-V-2	4.7
87	11224	-5652	-872	-739	-684	58	13.40	16.08	(8+9)-VII-1	5.0
88	9481	-8823	2672	-663	-1001	-40	13.40	16.08	2	5.9
89	8854	-8727	-229	-650	-896	5	13.40	16.08	2	6.5
90	8558	-4389	2751	-509	-489	-139	13.40	16.08	(8+9)-VII-4	6.6
91	12173	-5275	-75	-721	-724	-70	13.40	16.08	(8+9)-VII-4	4.9
92	11760	-5432	-3945	-679	-734	19	13.40	16.08	(8+9)-VII-4	5.6
93	6779	-3974	-6674	-434	-501	75	13.40	16.08	(8+9)-VII-4	8.7
94	2451	-2608	-6866	-183	-353	76	13.40	16.08	(8+9)-VIII-4	15
95	-8675	-3500	-4805	385	-210	67	13.40	16.08	2	13
96	-9893	-3052	-2828	458	-146	55	13.40	16.08	2	12
97	-9941	-3037	-758	463	-136	40	13.40	16.08	2	12
98	-10701	-440	-2913	536	222	-65	13.40	16.08	(8+9)-V-3	10
99	7925	-3011	3259	-453	-510	74	13.40	16.08	(8+9)-V-2	8.2
100	12019	-3850	2268	-689	-491	79	13.40	16.08	(8+9)-V-2	5.1
101	13948	-3997	-1417	-839	-579	138	13.40	16.08	(8+9)-V-2	3.8
102	12434	-3907	-4420	-733	-532	178	13.40	16.08	(8+9)-V-2	4.2
103	8840	-3470	-6545	-499	-411	185	13.40	16.08	(8+9)-V-2	6.2
104	1885	-6938	-2314	-210	-628	161	13.40	16.08	2	8.5
105	667	-6524	-2398	-81	-366	198	13.40	16.08	2	12
106	-1987	557	2167	-56	-560	510	13.40	16.08	2	5.6
107	-1995	2840	1414	1	-840	464	13.40	16.08	2	4.4
108	-1771	4392	569	7	-1132	338	13.40	16.08	2	3.8
109	-1256	1802	-1004	-20	-1291	378	13.40	16.08	2	3.5
110	-459	-446	-1900	-103	-1491	350	13.40	16.08	2	3.3
111	-1036	-1930	-562	174	-238	443	13.40	16.08	2	8.4
112	-559	-1189	-1340	35	-802	447	13.40	16.08	2	4.9
113	-1664	-618	550	131	-405	498	13.40	16.08	2	6.8
114	-1367	620	-331	70	-802	493	13.40	16.08	2	4.6
115	2205	-4757	-1829	-412	-2224	134	13.40	16.08	2	2.8
116	1795	-4380	-2104	-353	-2118	163	13.40	16.08	2	2.8
117	327	-1969	-2301	-207	-1754	281	13.40	16.08	2	3.1
118	893	-2955	-2411	-290	-1968	225	13.40	16.08	2	2.9
119	1362	-3756	-2281	-319	-2054	199	13.40	16.08	2	2.8
120	-285	-3176	-1059	127	-36	340	13.40	16.08	2	11
121	679	-2987	-2066	-171	-1289	308	13.40	16.08	2	4.0
122	374	-3152	-1721	-34	-675	349	13.40	16.08	2	6.2

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
123	196	-2397	-1852	-53	-1017	389	13.40	16.08	2	4.5
124	917	-3738	-1868	-127	-1071	248	13.40	16.08	2	4.9
125	1676	-4518	-1555	-254	-1241	187	13.40	16.08	2	4.5
126	1276	-4175	-1732	-156	-1053	251	13.40	16.08	2	4.9
127	1043	-4398	-1364	-59	-374	248	13.40	16.08	2	10
128	153	-4085	-981	89	322	221	13.40	16.08	2	12
129	324	-4552	-723	77	654	128	13.40	16.08	2	8.3
130	1525	-4805	-1001	-176	-467	132	13.40	16.08	2	11
131	1024	-4749	-942	-46	97	149	13.40	16.08	2	26
132	1366	-4713	-1189	-115	-384	188	13.40	16.08	2	11
133	1399	-4938	-814	-104	-114	81	13.40	16.08	2	27
134	1197	-4994	-585	-61	180	71	13.40	16.08	2	26
135	1185	-5096	-308	-53	293	36	13.40	16.08	2	20
136	647	-4863	-220	32	766	37	13.40	16.08	2	8.1
137	578	-4758	-513	35	711	81	13.40	16.08	2	8.2
138	182	-4690	-242	85	961	37	13.40	16.08	2	6.5
139	2668	-5583	-401	-492	-2682	29	13.40	16.08	2	2.4
140	2556	-5582	-192	-484	-2575	12	13.40	16.08	2	2.5
141	2115	-5423	-280	-320	-1441	27	13.40	16.08	2	4.5
142	1679	-5267	-326	-171	-459	32	13.40	16.08	2	13
143	1775	-5218	-538	-196	-630	62	13.40	16.08	2	9.4
144	2251	-5412	-481	-334	-1585	50	13.40	16.08	2	4.0
145	1881	-4878	-1369	-285	-1245	138	13.40	16.08	2	4.7
146	2499	-5093	-1511	-448	-2280	100	13.40	16.08	2	2.7
147	2021	-5046	-1069	-297	-1222	106	13.40	16.08	2	4.9
148	2598	-5328	-1153	-450	-2310	72	13.40	16.08	2	2.7
149	2712	-5499	-869	-456	-2560	69	13.40	16.08	2	2.5
150	2409	-5425	-710	-362	-1866	74	13.40	16.08	2	3.4
151	2734	-5564	-621	-509	-2808	41	13.40	16.08	2	2.3
152	1950	-5197	-794	-258	-974	80	13.40	16.08	2	6.2
153	-713	-4485	159	51	991	-15	13.40	16.08	2	6.4
154	-993	-4578	206	113	951	-57	13.40	16.08	2	6.4
155	-1360	-4900	445	209	882	-60	13.40	16.08	2	6.9
156	-1069	-4612	53	197	909	3	13.40	16.08	2	7.1
157	-491	-4447	-320	159	902	68	13.40	16.08	2	6.7
158	-613	-4466	-8	94	1004	6	13.40	16.08	2	6.4
159	-414	-4512	-210	113	986	29	13.40	16.08	2	6.4
160	-819	-4505	-49	132	964	-5	13.40	16.08	2	6.7
161	-208	-4491	331	-84	934	-32	13.40	16.08	2	6.7
162	6867	-3608	648	-581	-384	-102	13.40	16.08	(8+9)-VI-2	6.5
163	3891	-2961	-661	-433	-168	176	13.40	16.08	(8+9)-VII-1	7.7
164	2948	-2626	957	-440	15	109	13.40	16.08	(8+9)-VII-1	8.8
165	4149	-6307	307	-381	323	33	13.40	16.08	2	11
166	1227	-5190	913	-218	735	-84	13.40	16.08	2	8.0
167	-1506	-5287	893	229	858	-124	13.40	16.08	2	6.7
168	-937	-4885	652	88	926	-125	13.40	16.08	2	6.2
169	129	-5403	1575	-38	705	-195	13.40	16.08	2	7.3
170	-808	-5201	1151	71	824	-203	13.40	16.08	2	6.4
171	-1041	-5452	1936	108	678	-238	13.40	16.08	2	7.2
172	-1957	-5694	1985	252	692	-216	13.40	16.08	2	7.2
173	-1647	-5586	1374	237	802	-185	13.40	16.08	2	6.7
174	-2478	-5808	1779	352	743	-159	13.40	16.08	2	7.3
175	-3287	-5933	2333	398	581	-161	13.40	16.08	2	8.9
176	-2515	-5792	2684	292	526	-227	13.40	16.08	2	8.7
177	-5418	-5069	5155	359	4	-194	13.40	16.08	2	10
178	-3693	-5558	3753	333	291	-222	13.40	16.08	2	9.8
179	-6810	-4895	3892	457	90	-148	13.40	16.08	2	9.5
180	-4720	-5613	3065	435	359	-164	13.40	16.08	2	9.2
181	4186	-2625	1780	-412	-61	-111	13.40	16.08	(8+9)-VI-2	8.9
182	7096	-4019	2165	-634	-363	-66	13.40	16.08	(8+9)-V-2	6.3
183	4714	-3866	4343	-313	-405	-210	13.40	16.08	(8+9)-V-2	8.9
184	6406	-4231	3341	-491	-418	-185	13.40	16.08	(8+9)-V-2	6.6
185	4139	-3308	4053	-329	-201	-222	13.40	16.08	(8+9)-V-2	8.5
186	-1211	-5777	3037	105	439	-266	13.40	16.08	2	9.3

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
187	-2312	-4857	1370	336	622	59	13.40	16.08	2	9.5
188	-1861	-4007	633	334	557	167	13.40	16.08	2	8.9
189	-1170	-3425	-198	278	413	281	13.40	16.08	2	9.2
190	-1494	-4233	196	317	714	124	13.40	16.08	2	7.7
191	-1021	-4322	-132	253	828	102	13.40	16.08	2	6.9
192	-829	-3971	-404	231	641	187	13.40	16.08	2	7.8
193	-1477	-4639	356	274	834	23	13.40	16.08	2	7.6
194	-1912	-4750	816	336	741	38	13.40	16.08	2	8.3
195	-2048	-1817	3017	-147	-346	478	13.40	16.08	2	7.6
196	-1675	-2708	454	263	144	357	13.40	16.08	2	8.5
197	-2017	-2097	1562	135	-117	418	13.40	16.08	2	9.5
198	-1969	-4102	3610	-256	-204	384	13.40	16.08	2	8.2
199	-2137	-3859	1338	265	335	223	13.40	16.08	2	11
200	-2234	-3820	2348	79	72	291	13.40	16.08	2	14
201	-2054	-7383	3228	-300	195	225	13.40	16.08	2	10
202	-2270	-5779	2824	-30	214	189	13.40	16.08	2	16
203	-1908	-6018	3705	-366	-53	297	13.40	16.08	2	7.9
204	-2430	-5284	2060	194	433	109	13.40	16.08	2	12
205	-7682	-2810	2618	489	127	-118	13.40	16.08	(8+9)-VII-1	9.6
206	-5763	-3230	2268	461	85	-126	13.40	16.08	(8+9)-VII-1	9.6
207	-3664	-2584	3955	284	-13	-241	13.40	16.08	(8+9)-V-2	10
208	-5204	-5613	2422	470	386	-103	13.40	16.08	2	9.7
209	-7339	-4876	2588	493	130	-98	13.40	16.08	2	9.8
210	-6945	-2448	3365	417	-5	-131	13.40	16.08	(8+9)-VII-1	10
211	-2198	-5410	1388	346	760	-27	13.40	16.08	2	8.3
212	-1787	-5105	830	295	820	-42	13.40	16.08	2	7.6
213	-1964	-5634	1277	324	812	-86	13.40	16.08	2	7.3
214	-2401	-5929	1741	367	785	-55	13.40	16.08	2	7.9
215	-2514	-6025	1748	372	762	-89	13.40	16.08	2	7.8
216	-3365	-2832	-1721	272	405	213	13.40	16.08	(8+9)-VI-3	10
217	-3108	-6164	1963	417	684	-62	13.40	16.08	2	8.9
218	-3895	-5896	2133	442	588	-93	13.40	16.08	2	9.7
219	-3443	-6172	1892	409	665	-43	13.40	16.08	2	9.4
220	-1935	-8567	-526	105	531	174	13.40	16.08	(8+9)-VI-1	9.7
221	-2840	-5516	-610	254	466	115	13.40	16.08	(8+9)-II-1	11
222	-2502	-5808	1902	328	685	-14	13.40	16.08	2	9.4
223	-2435	-6051	-2536	166	551	354	13.40	16.08	(8+9)-II-3	7.3
224	-1993	-7827	-3197	126	652	348	13.40	16.08	(8+9)-II-3	6.8
225	933	2498	5999	-527	-326	-288	13.40	16.08	(8+9)-II-2	6.1
226	2117	-4	3370	-372	-46	-240	13.40	16.08	(8+9)-II-4	8.0
227	1496	-1049	6357	-482	-136	-290	13.40	16.08	(8+9)-II-2	6.4
228	1894	-2666	6099	-365	77	-264	13.40	16.08	(8+9)-II-2	7.8
229	2403	-1429	3336	-348	101	-232	13.40	16.08	(8+9)-II-4	8.4
230	1829	-7452	5783	-4	371	-194	13.40	16.08	(8+9)-VI-2	12
231	1721	-6740	5014	-107	523	-251	13.40	16.08	(8+9)-VI-2	8.6
232	1828	-5519	5931	-172	221	-245	13.40	16.08	(8+9)-VI-2	12
233	1365	-2686	4615	-187	339	-296	13.40	16.08	(8+9)-VI-2	9.9
234	-8004	-1610	1776	559	117	-92	13.40	16.08	(8+9)-VII-1	9.0
235	-5732	-3457	1846	507	96	-94	13.40	16.08	(8+9)-VII-1	9.4
236	6187	-3016	-1044	-537	-79	-127	13.40	16.08	(8+9)-VII-4	6.8
237	3852	-1027	1327	-374	70	-158	13.40	16.08	(8+9)-VIII-4	8.9
238	324	-7300	316	-143	75	-247	13.40	16.08	2	13
239	1379	-6879	161	-171	-159	-223	13.40	16.08	2	13
240	4123	-1298	-343	-354	30	-176	13.40	16.08	(8+9)-VII-4	8.8
241	6154	-3230	1476	-487	-112	-157	13.40	16.08	(8+9)-VII-4	7.0
242	4908	-3394	2097	-304	-85	-191	13.40	16.08	(8+9)-VII-4	9.3
243	3901	-1492	1488	-236	86	-229	13.40	16.08	(8+9)-VII-4	10
244	-3591	-5406	-994	385	468	192	13.40	16.08	(8+9)-II-1	9.4
245	-3400	-5808	-783	322	524	187	13.40	16.08	(8+9)-II-1	9.3
246	-2607	-6313	2080	338	785	-50	13.40	16.08	2	7.9
247	-2530	-6582	2124	298	728	-44	13.40	16.08	2	8.6
248	-2485	-7017	2087	245	766	-63	13.40	16.08	2	8.1
249	-1683	-8515	1304	-26	660	-123	13.40	16.08	2	8.7
250	-1310	-9036	1091	-149	531	-186	13.40	16.08	2	9.6

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
251	-1988	-8217	1705	64	700	-83	13.40	16.08	2	8.7
252	-1276	-8132	830	-58	502	-187	13.40	16.08	2	9.9
253	1379	-2391	891	163	62	-252	13.40	16.08	(8+9)-V-3	12
254	3557	-1728	1855	-256	80	-194	13.40	16.08	(8+9)-VIII-4	11
255	-1859	-7635	1211	63	658	-136	13.40	16.08	2	8.5
256	-2285	-7240	1690	181	757	-89	13.40	16.08	2	7.9
257	-2904	-6325	1904	320	727	-24	13.40	16.08	2	8.8
258	-2388	-6545	1583	186	696	-71	13.40	16.08	2	8.7
259	-1667	-6934	1109	67	564	-141	13.40	16.08	2	9.5
260	567	-4968	31	47	844	4	13.40	16.08	2	7.7
261	1007	-5175	152	23	577	-46	13.40	16.08	2	10
262	1183	-5122	-93	-56	316	3	13.40	16.08	2	20
263	1932	-5618	307	-363	-2121	-22	13.40	16.08	2	3.1
264	1630	-5479	235	-149	-571	-44	13.40	16.08	2	11
265	1635	-5336	-119	-175	-445	1	13.40	16.08	2	15
266	1821	-5446	19	-208	-950	-49	13.40	16.08	2	6.6
267	1996	-5440	-125	-316	-1371	-4	13.40	16.08	2	4.8
268	2365	-5599	-14	-462	-2453	-2	13.40	16.08	2	2.7
269	2126	-5656	155	-396	-2245	-10	13.40	16.08	2	2.9
270	798	-5014	744	36	545	-102	13.40	16.08	2	10
271	2204	-5559	614	-482	-2875	-48	13.40	16.08	2	2.2
272	2042	-5511	650	-345	-1941	-58	13.40	16.08	2	3.3
273	2096	-5620	522	-392	-2556	-16	13.40	16.08	2	2.6
274	2296	-5563	765	-394	-2432	-98	13.40	16.08	2	2.6
275	1638	-5359	759	-157	-598	-91	13.40	16.08	2	9.5
276	795	-5170	412	49	700	-33	13.40	16.08	2	8.9
277	2029	-5573	413	-494	-2923	-7	13.40	16.08	2	2.2
278	1887	-5526	435	-338	-1927	-53	13.40	16.08	2	3.3
279	1972	-5636	379	-377	-2425	31	13.40	16.08	2	2.7
280	2012	-5616	511	-393	-2586	-62	13.40	16.08	2	2.5
281	1555	-5433	475	-147	-529	-51	13.40	16.08	2	11
282	2406	-5451	944	-403	-2118	-87	13.40	16.08	2	3.0
283	2635	-5251	1300	-429	-2094	-114	13.40	16.08	2	3.0
284	557	-4652	990	50	488	-179	13.40	16.08	2	9.7
285	2005	-4955	1373	-266	-1080	-151	13.40	16.08	2	5.3
286	1875	-5200	1067	-190	-831	-83	13.40	16.08	2	7.1
287	1350	-4801	1247	-88	-201	-184	13.40	16.08	2	17
288	1984	-4646	1650	-249	-1076	-213	13.40	16.08	2	5.0
289	2730	-4973	1642	-427	-2106	-137	13.40	16.08	2	2.9
290	2003	-3594	2653	-326	-1519	-279	13.40	16.08	2	3.6
291	2767	-4685	1982	-433	-2130	-158	13.40	16.08	2	2.8
292	2066	-4380	1982	-257	-1236	-258	13.40	16.08	2	4.3
293	2564	-4297	2332	-360	-1833	-225	13.40	16.08	2	3.1
294	-496	-3513	1114	171	436	-363	13.40	16.08	2	8.0
295	116	-4139	1139	118	486	-276	13.40	16.08	2	8.5
296	1105	-4366	1506	-54	-148	-277	13.40	16.08	2	15
297	1113	-3315	2191	-153	-692	-382	13.40	16.08	2	5.9
298	1193	-3931	1855	-106	-428	-309	13.40	16.08	2	8.7
299	325	-3324	1705	26	-27	-414	13.40	16.08	2	12
300	-2730	-1261	-1341	-161	26	-439	13.40	16.08	2	8.9
301	-1088	-2818	922	196	319	-458	13.40	16.08	2	7.9
302	-1750	-2056	470	170	214	-500	13.40	16.08	2	7.8
303	-2293	-1593	-328	51	115	-489	13.40	16.08	2	9.8
304	-2478	163	-812	-76	-94	-492	13.40	16.08	2	9.4
305	-2002	-564	221	64	-32	-548	13.40	16.08	2	8.6
306	-1759	980	1466	69	-468	-536	13.40	16.08	2	5.9
307	-2503	2625	726	93	-464	-498	13.40	16.08	2	6.0
308	-2077	1984	2327	49	-709	-453	13.40	16.08	2	5.0
309	-2231	1622	21	29	-252	-516	13.40	16.08	2	7.7
310	-1703	289	833	74	-237	-568	13.40	16.08	2	7.5
311	307	-1439	3089	-153	-1165	-401	13.40	16.08	2	4.0
312	1290	-2620	2983	-254	-1348	-346	13.40	16.08	2	3.7
313	-842	-14	2848	-41	-951	-433	13.40	16.08	2	4.4
314	-315	-2550	1567	79	-26	-507	13.40	16.08	2	8.7

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
315	507	-2510	2280	-85	-612	-464	13.40	16.08	2	5.8
316	-189	-1538	2207	-24	-576	-517	13.40	16.08	2	5.7
317	-920	-393	1981	30	-533	-539	13.40	16.08	2	5.7
318	-1137	-718	1370	78	-242	-574	13.40	16.08	2	7.5
319	-712	-1772	1468	89	-145	-546	13.40	16.08	2	8.1
320	-1326	-1315	1007	118	-0	-561	13.40	16.08	2	7.7
321	-2476	-5118	-1311	258	776	68	13.40	16.08	2	7.7
322	3799	-1273	-2743	-301	-35	316	13.40	16.08	(8+9)-V-2	7.7
323	3223	-980	-2374	-318	4	293	13.40	16.08	(8+9)-V-2	7.8
324	4091	-1071	-2286	-381	-16	294	13.40	16.08	(8+9)-V-2	6.9
325	4781	-2877	-4596	-277	-103	294	13.40	16.08	(8+9)-V-2	8.1
326	6984	-2851	-4024	-487	-221	296	13.40	16.08	(8+9)-V-2	5.6
327	5379	-1306	-2735	-444	-89	311	13.40	16.08	(8+9)-V-2	6.0
328	4513	-1439	-3346	-296	-73	321	13.40	16.08	(8+9)-V-2	7.5
329	-2470	-7811	-2819	-207	444	222	13.40	16.08	2	10
330	-2600	-7594	-2987	-285	403	169	13.40	16.08	2	12
331	-2610	-7398	-2742	-145	483	178	13.40	16.08	2	10
332	179	-6355	-2059	-50	-83	281	13.40	16.08	2	15
333	1421	-2179	-4098	96	47	252	13.40	16.08	(8+9)-VII-1	14
334	3539	-1535	-3744	-162	-43	224	13.40	16.08	(8+9)-V-2	12
335	3262	-1486	-3095	-198	-21	291	13.40	16.08	(8+9)-V-2	9.8
336	-1678	-7892	-2256	-80	289	324	13.40	16.08	2	11
337	-1698	-6890	-1886	47	389	269	13.40	16.08	2	10
338	-1050	-7207	-1980	-46	180	315	13.40	16.08	2	14
339	-2129	-5931	-1551	175	629	177	13.40	16.08	2	8.2
340	-2526	-5655	-1553	241	717	119	13.40	16.08	2	7.9
341	-2154	-6693	-1821	101	554	218	13.40	16.08	2	8.6
342	-2484	-6408	-1891	152	641	163	13.40	16.08	2	8.3
343	-2360	-7983	-2628	-132	415	282	13.40	16.08	2	9.7
344	-2195	-7434	-2204	-3	495	252	13.40	16.08	2	9.0
345	-2067	-8126	-2560	-105	363	317	13.40	16.08	2	10
346	-2493	-7180	-2431	-27	546	182	13.40	16.08	2	9.2
347	-2416	-7095	-2205	29	562	204	13.40	16.08	2	8.8
348	-2434	-7587	-2648	-105	484	232	13.40	16.08	2	9.4
349	1636	-793	-3583	-170	11	245	13.40	16.08	(8+9)-V-2	12
350	-3133	-7065	-2835	-361	337	21	13.40	16.08	2	14
351	-2872	-7426	-2905	-326	371	95	13.40	16.08	2	13
352	-2837	-6991	-2673	-119	470	122	13.40	16.08	2	11
353	-3911	-3526	1035	497	486	-177	13.40	16.08	(8+9)-V-3	8.1
354	-2764	-6639	-2343	36	556	134	13.40	16.08	2	9.7
355	-3991	-3957	1378	335	403	-187	13.40	16.08	(8+9)-V-3	10
356	-2756	-6041	-1941	178	629	107	13.40	16.08	2	9.0
357	-4004	-3645	1174	489	481	-183	13.40	16.08	(8+9)-V-3	8.1
358	-1863	-3205	242	270	505	-357	13.40	16.08	2	7.4
359	-1460	-3846	329	330	700	-257	13.40	16.08	2	6.7
360	-2273	-3758	-272	322	643	-219	13.40	16.08	2	7.4
361	-3700	-3774	1298	477	438	-201	13.40	16.08	(8+9)-V-3	8.0
362	-2586	-4302	-800	336	662	-119	13.40	16.08	2	8.3
363	-2487	-4478	-802	375	758	-65	13.40	16.08	2	7.9
364	-3841	-4014	1441	384	400	-222	13.40	16.08	(8+9)-V-3	9.0
365	-3528	-4138	1614	360	368	-251	13.40	16.08	(8+9)-V-3	8.9
366	-3497	-6138	-2655	-401	268	-107	13.40	16.08	2	11
367	-3409	-5286	1848	6	291	-284	13.40	16.08	(8+9)-V-3	11
368	-3685	-4678	1776	161	326	-263	13.40	16.08	(8+9)-V-3	11
369	-3327	-6616	-2762	-382	303	-47	13.40	16.08	2	13
370	-3956	-4425	1702	173	334	-235	13.40	16.08	(8+9)-V-3	11
371	-2978	-2507	-1658	-217	118	-377	13.40	16.08	2	9.0
372	-3078	-4965	1724	76	277	-288	13.40	16.08	(8+9)-V-3	12
373	-3282	-3546	-1869	-216	208	-306	13.40	16.08	2	10
374	-3096	-4213	1778	318	329	-271	13.40	16.08	(8+9)-V-3	9.1
375	-2635	-2478	-770	29	215	-414	13.40	16.08	2	10.0
376	-2331	-2783	-237	194	360	-401	13.40	16.08	2	8.3
377	-2740	-3211	-907	82	331	-331	13.40	16.08	2	9.6
378	-487	-4963	250	163	940	-9	13.40	16.08	2	6.9

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
379	73	-4960	383	119	957	-28	13.40	16.08	2	6.6
380	-236	-4856	257	132	995	9	13.40	16.08	2	6.5
381	-866	-5059	14	191	897	25	13.40	16.08	2	7.1
382	-659	-4907	159	143	936	48	13.40	16.08	2	6.6
383	-594	-4722	198	97	971	53	13.40	16.08	2	6.3
384	-625	-4458	203	53	999	34	13.40	16.08	2	6.3
385	-385	-4592	66	83	1018	21	13.40	16.08	2	6.2
386	-230	-4730	190	98	1015	20	13.40	16.08	2	6.3
387	65	-4751	10	83	1003	20	13.40	16.08	2	6.3
388	-633	-4854	90	81	948	102	13.40	16.08	2	6.2
389	-372	-4667	104	8	978	69	13.40	16.08	2	6.2
390	-160	-4913	-169	-21	854	148	13.40	16.08	2	6.5
391	7232	-3187	-1637	-613	-278	35	13.40	16.08	(8+9)-VII-4	6.8
392	4411	-2767	-3178	-416	-140	133	13.40	16.08	(8+9)-VII-4	8.5
393	231	-5377	-1458	-62	563	215	13.40	16.08	2	8.4
394	3880	-2017	-280	-429	176	-125	13.40	16.08	(8+9)-VII-4	8.5
395	-909	-5042	-31	162	902	100	13.40	16.08	2	6.5
396	-1259	-5268	-279	235	856	61	13.40	16.08	2	7.1
397	-1847	-5480	-736	301	778	94	13.40	16.08	2	7.5
398	-1212	-5269	-579	194	817	158	13.40	16.08	2	6.7
399	-1769	-5501	-1544	235	592	199	13.40	16.08	2	8.3
400	-5942	-4625	-3631	398	63	130	13.40	16.08	2	11
401	-3413	-5142	-2835	334	305	180	13.40	16.08	2	11
402	-3660	-5099	-4126	271	62	178	13.40	16.08	2	12
403	-2770	-5497	-1292	369	624	112	13.40	16.08	2	8.9
404	-4525	-5078	-1950	428	391	107	13.40	16.08	2	10
405	-6846	-4285	-2482	466	130	87	13.40	16.08	2	10
406	-5422	-2710	567	435	387	-158	13.40	16.08	(8+9)-IV-3	9.4
407	-4840	-5114	-1295	453	413	40	13.40	16.08	2	11
408	-5632	-2281	603	399	366	-91	13.40	16.08	(8+9)-VIII-3	11
409	-3301	-5419	-1107	403	604	27	13.40	16.08	2	10
410	-7627	-2472	1357	501	254	-163	13.40	16.08	(8+9)-IV-3	8.7
411	-7111	-2169	1493	435	250	-132	13.40	16.08	(8+9)-IV-3	10
412	-6946	-4337	-1159	478	168	33	13.40	16.08	2	11
413	-6265	-2871	729	570	415	-163	13.40	16.08	(8+9)-V-3	7.7
414	4063	-883	-1878	-427	21	224	13.40	16.08	(8+9)-V-2	7.2
415	6028	-1241	-2069	-553	-85	244	13.40	16.08	(8+9)-V-2	5.6
416	8727	-2860	-2805	-667	-288	246	13.40	16.08	(8+9)-V-2	4.6
417	9462	-2812	-1548	-744	-336	152	13.40	16.08	(8+9)-V-2	4.6
418	6374	-2366	-1395	-576	-100	134	13.40	16.08	(8+9)-V-2	6.3
419	8171	-2654	783	-613	-270	78	13.40	16.08	(8+9)-V-2	6.2
420	-1883	-4745	-564	296	841	-51	13.40	16.08	2	7.3
421	-2127	-4393	-505	311	799	-71	13.40	16.08	2	7.4
422	-1637	-4516	-215	298	829	-87	13.40	16.08	2	7.1
423	-304	-4492	631	174	834	-149	13.40	16.08	2	6.6
424	-1124	-4465	257	276	874	-127	13.40	16.08	2	6.5
425	-906	-4137	515	235	771	-207	13.40	16.08	2	6.6
426	-1533	-4928	-407	265	853	-38	13.40	16.08	2	7.3
427	-1188	-5040	-179	232	870	-8	13.40	16.08	2	7.4
428	-31	-4832	511	146	902	-82	13.40	16.08	2	6.6
429	-1152	-4781	-21	243	877	-58	13.40	16.08	2	6.9
430	-764	-4692	228	206	901	-71	13.40	16.08	2	6.7
431	-817	-4883	82	209	911	-33	13.40	16.08	2	6.9
432	-2459	-5278	-970	319	768	-47	13.40	16.08	2	8.0
433	-2300	-5457	-849	343	759	14	13.40	16.08	2	8.5
434	-1911	-5116	-739	290	834	-32	13.40	16.08	2	7.5
435	-1617	-5260	-537	277	836	8	13.40	16.08	2	7.7
436	-2145	-4884	-865	293	838	-42	13.40	16.08	2	7.4
437	-2375	-4767	-981	313	822	-23	13.40	16.08	2	7.7
438	-4623	-3310	828	512	498	-181	13.40	16.08	(8+9)-V-3	8.0
439	-2414	-5028	-1040	268	796	-49	13.40	16.08	2	7.7
Massimi/minimi										
1							13.40			
1								16.08		

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
35										1.7

Muro [Platea]: 2 - Nodi: [21-6-14-19-20-8-31-30-29-28-27-26]Pann=449Spess.=25 cm, Terreno=Terreno1,
 ,Criterio=CLS_Platee, Materiale=C30/37: **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-2421	1405	758	310	-11	379	13.40	16.08	2	7.7
2	-2016	-839	1161	144	127	359	13.40	16.08	2	11
3	-1804	-2722	1143	-22	209	307	13.40	16.08	2	12
4	-1749	-4120	904	-166	257	242	13.40	16.08	2	13
5	-1758	-5051	543	-276	279	173	13.40	16.08	2	12
6	-1751	-5600	112	-354	282	104	13.40	16.08	2	11
7	-1726	-5780	-352	-407	268	37	13.40	16.08	2	12
8	-1695	-5614	-799	-438	238	-28	13.40	16.08	2	11
9	-1634	-5081	-1205	-439	198	-89	13.40	16.08	2	9.9
10	-1458	-4105	-1543	-395	148	-144	13.40	16.08	2	9.7
11	-1461	-2578	-1675	-308	82	-194	13.40	16.08	2	10
12	632	1029	-3260	-397	-100	-76	13.40	16.08	(8+9)-I-4	11
13	1087	4143	-2754	-360	-315	-87	13.40	16.08	(8+9)-III-3	11
14	-2580	4234	1547	40	-442	-206	13.40	16.08	2	8.7
15	-140	240	2092	-104	-719	-273	13.40	16.08	2	6.1
16	1040	-1091	2243	-214	-944	-304	13.40	16.08	2	4.9
17	2025	-1887	1828	-304	-1126	-311	13.40	16.08	2	4.3
18	2590	-2077	1253	-365	-1263	-308	13.40	16.08	2	4.0
19	3203	-2204	569	-404	-1370	-323	13.40	16.08	2	3.7
20	3615	-1940	-222	-473	-1523	-321	13.40	16.08	2	3.4
21	3910	-1607	-1253	-534	-1669	-325	13.40	16.08	2	3.1
22	3287	-835	-2503	-563	-1782	-316	13.40	16.08	2	2.9
23	1162	324	-3261	-460	-1800	-298	13.40	16.08	2	2.9
24	-2139	487	-2573	-190	-1620	-296	13.40	16.08	2	3.1
25	-3186	87	-732	-14	-1389	-295	13.40	16.08	2	3.6
26	-2814	-413	622	-42	-1345	-350	13.40	16.08	2	3.6
27	-775	-1153	1598	-201	-1494	-388	13.40	16.08	2	3.3
28	2022	-1385	1032	-410	-1676	-355	13.40	16.08	2	3.0
29	2916	-1212	-250	-481	-1790	-317	13.40	16.08	2	2.9
30	2461	-785	-1209	-457	-1785	-306	13.40	16.08	2	2.9
31	1554	-388	-1613	-387	-1689	-292	13.40	16.08	2	3.1
32	684	99	-1566	-316	-1566	-269	13.40	16.08	2	3.3
33	58	539	-1269	-251	-1442	-246	13.40	16.08	2	3.6
34	-291	1120	-768	-190	-1303	-216	13.40	16.08	2	3.9
35	-341	2013	-42	-128	-1133	-175	13.40	16.08	2	4.5
36	58	3491	1080	-54	-915	-116	13.40	16.08	2	5.5
37	1994	10698	4748	-190	-723	-105	13.40	16.08	(8+9)-VI-1	6.1
38	1424	9097	6690	-329	-780	-29	13.40	16.08	(8+9)-II-1	6.4
39	1692	3812	7886	-543	-616	-8	13.40	16.08	(8+9)-VI-1	8.9
40	1941	807	7321	-471	-271	64	13.40	16.08	(8+9)-VI-1	9.2
41	1268	-2733	4127	-412	-232	92	13.40	16.08	(8+9)-VI-3	9.9
42	570	-5536	1406	-225	0	263	13.40	16.08	2	10
43	-32	-5940	596	-273	48	260	13.40	16.08	2	9.5
44	-336	-5871	211	-337	41	250	13.40	16.08	2	8.7
45	-355	-5725	229	-393	35	231	13.40	16.08	2	8.2
46	-249	-6072	380	-401	70	216	13.40	16.08	2	8.3
47	-147	-6947	-161	-373	160	192	13.40	16.08	2	9.0
48	-390	-7561	-1087	-296	269	170	13.40	16.08	2	11
49	-898	-7318	-2065	-243	350	137	13.40	16.08	2	14
50	-1491	-6466	-2780	-207	399	96	13.40	16.08	2	13
51	-2008	-5135	-3356	-185	414	49	13.40	16.08	2	14
52	-2328	-3731	-3676	-201	389	6	13.40	16.08	2	16

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
53	-2527	-2452	-3859	-206	363	-48	13.40	16.08	2	15
54	-2511	-1806	-3867	-193	363	-85	13.40	16.08	2	14
55	-2618	-860	-3922	-141	375	-135	13.40	16.08	2	12
56	-2947	938	-3855	-44	373	-203	13.40	16.08	2	10
57	-3075	3292	-3634	54	323	-284	13.40	16.08	2	9.5
58	-3272	5992	-2973	149	230	-362	13.40	16.08	2	9.3
59	-3193	8635	-1875	232	71	-428	13.40	16.08	2	8.2
60	-4149	12384	1331	-157	-622	-146	13.40	16.08	(8+9)-VI-2	6.3
61	-2206	13869	3689	-198	-670	-209	13.40	16.08	(8+9)-V-2	5.4
62	-3176	15419	3741	191	-785	-238	13.40	16.08	2	4.5
63	-1260	10414	2682	-10	-1172	-148	13.40	16.08	2	3.8
64	-342	7362	2427	-74	-1395	-167	13.40	16.08	2	3.4
65	919	4484	2619	-244	-1856	-95	13.40	16.08	2	2.9
66	1768	2487	2529	-341	-2197	-63	13.40	16.08	2	2.6
67	2291	1030	2462	-401	-2425	-52	13.40	16.08	2	2.4
68	2726	-103	2388	-443	-2539	-65	13.40	16.08	2	2.3
69	3248	-873	2197	-475	-2691	-89	13.40	16.08	2	2.2
70	3648	-1413	1961	-549	-2974	-62	13.40	16.08	2	2.0
71	3726	-1784	1614	-572	-3161	-44	13.40	16.08	2	1.9
72	3565	-2041	1344	-574	-3279	-32	13.40	16.08	2	1.9
73	3457	-2198	1152	-579	-3367	-28	13.40	16.08	2	1.8
74	3506	-2264	924	-595	-3433	-23	13.40	16.08	2	1.8
75	3486	-2268	590	-604	-3474	-12	13.40	16.08	2	1.8
76	3203	-2206	251	-590	-3484	-1	13.40	16.08	2	1.8
77	2760	-2109	62	-560	-3472	4	13.40	16.08	2	1.8
78	2463	-2027	42	-539	-3450	4	13.40	16.08	2	1.8
79	2441	-1999	34	-538	-3421	6	13.40	16.08	2	1.8
80	2536	-1981	-93	-544	-3390	12	13.40	16.08	2	1.8
81	2573	-1941	-272	-542	-3361	20	13.40	16.08	2	1.8
82	2557	-1932	-389	-532	-3330	24	13.40	16.08	2	1.9
83	2683	-1958	-484	-533	-3292	25	13.40	16.08	2	1.9
84	3022	-1979	-657	-547	-3240	28	13.40	16.08	2	1.9
85	3403	-2008	-966	-561	-3161	34	13.40	16.08	2	2.0
86	3631	-2036	-1387	-561	-3058	42	13.40	16.08	2	2.0
87	3724	-2035	-1838	-549	-2940	46	13.40	16.08	2	2.1
88	3755	-2002	-2313	-534	-2789	51	13.40	16.08	2	2.2
89	3693	-1914	-2906	-502	-2558	63	13.40	16.08	2	2.4
90	3222	-1538	-3593	-464	-2287	82	13.40	16.08	2	2.6
91	2237	-1021	-4236	-388	-2022	94	13.40	16.08	2	2.9
92	672	-244	-4563	-259	-1711	100	13.40	16.08	2	3.4
93	-1179	1027	-4314	-96	-1357	102	13.40	16.08	2	4.1
94	-2808	2838	-3334	85	-992	102	13.40	16.08	2	5.3
95	-6203	7332	-1915	352	-565	151	13.40	16.08	2	7.5
96	-3099	3536	-311	427	-225	345	13.40	16.08	2	7.0
97	1289	-1425	825	-172	-294	-222	13.40	16.08	2	12
98	369	-1177	855	-72	120	-244	13.40	16.08	2	16
99	1061	-1422	1291	-193	-386	-301	13.40	16.08	2	9.0
100	-714	230	1029	-91	-238	-330	13.40	16.08	2	11
101	338	-878	1416	-135	-302	-330	13.40	16.08	2	9.7
102	-459	-1013	702	-37	134	-285	13.40	16.08	2	15
103	-965	-780	140	-81	36	-294	13.40	16.08	2	14
104	-1764	-1471	-252	159	637	51	13.40	16.08	2	9.0
105	-1261	-771	-150	177	769	47	13.40	16.08	2	7.5
106	-631	-909	380	62	510	-110	13.40	16.08	2	9.9
107	-1560	-1941	-50	23	380	-133	13.40	16.08	2	12
108	-1217	-1267	217	96	460	-128	13.40	16.08	2	10
109	-1076	-1527	291	-9	312	-209	13.40	16.08	2	12
110	-1566	-1763	-146	78	497	-67	13.40	16.08	2	11
111	-1917	-3975	-601	-188	337	-18	13.40	16.08	2	18
112	-1990	-3984	-422	-136	384	63	13.40	16.08	2	14
113	-2004	-2555	-401	53	505	68	13.40	16.08	2	11
114	-1909	-2632	-348	-9	436	-32	13.40	16.08	2	13
115	-1332	-1859	-412	-105	196	-218	13.40	16.08	2	15
116	-1830	-3733	-746	-224	281	-84	13.40	16.08	2	17

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
117	-1649	-2956	-720	-178	254	-147	13.40	16.08	2	16
118	-1742	-2566	-364	-65	342	-111	13.40	16.08	2	14
119	-1791	-2776	-106	14	366	329	13.40	16.08	2	9.1
120	-1573	-1851	-845	105	466	382	13.40	16.08	2	7.3
121	-1852	-2179	-659	100	537	291	13.40	16.08	2	7.6
122	-1971	-2410	-531	92	547	185	13.40	16.08	2	8.6
123	-1999	-3793	-266	-87	410	154	13.40	16.08	2	11
124	-1934	-3403	-154	-40	406	244	13.40	16.08	2	9.8
125	-695	-760	-1249	148	780	283	13.40	16.08	2	5.8
126	-1194	-745	-698	195	847	183	13.40	16.08	2	5.9
127	-1704	-1350	-683	189	709	197	13.40	16.08	2	6.8
128	-1430	-1395	-1045	158	654	308	13.40	16.08	2	6.4
129	-962	-1046	-1296	149	653	342	13.40	16.08	2	6.2
130	-1244	-1292	-1246	128	540	389	13.40	16.08	2	6.6
131	-1674	-1830	-183	79	287	401	13.40	16.08	2	9.1
132	-1288	-1323	-1096	104	335	450	13.40	16.08	2	7.9
133	-1627	-641	-458	138	149	445	13.40	16.08	2	9.0
134	-1114	-624	-1480	88	127	476	13.40	16.08	2	9.2
135	-2472	2261	-2011	148	-428	338	13.40	16.08	2	7.6
136	-1666	692	-1041	172	-75	436	13.40	16.08	2	8.6
137	-1011	568	-2936	-14	-675	324	13.40	16.08	2	6.0
138	-903	31	-2071	51	-199	441	13.40	16.08	2	9.4
139	129	-824	-1722	33	462	319	13.40	16.08	2	7.9
140	2955	-1611	-2261	-411	-1854	144	13.40	16.08	2	3.1
141	2626	-1512	-2651	-333	-1492	204	13.40	16.08	2	3.7
142	2077	-1337	-2244	-268	-988	226	13.40	16.08	2	5.1
143	1100	-1004	-2108	-127	-188	294	13.40	16.08	2	12
144	179	-304	-3298	-148	-900	306	13.40	16.08	2	5.0
145	1914	-1152	-2978	-297	-1158	244	13.40	16.08	2	4.4
146	1150	-770	-3265	-240	-1044	285	13.40	16.08	2	4.6
147	-270	-826	-1840	40	366	389	13.40	16.08	2	8.1
148	-782	-1050	-1634	70	336	442	13.40	16.08	2	7.9
149	-171	-453	-2542	-49	-343	412	13.40	16.08	2	8.1
150	-362	-738	-2110	20	39	453	13.40	16.08	2	11
151	341	-828	-2514	-88	-303	376	13.40	16.08	2	9.0
152	739	-888	-2378	-117	-233	354	13.40	16.08	2	10
153	1609	-1435	-310	-70	-10	77	13.40	16.08	2	34
154	1082	-1141	-321	42	657	90	13.40	16.08	2	8.2
155	923	-989	-682	39	664	133	13.40	16.08	2	7.7
156	1223	-1135	-576	10	483	95	13.40	16.08	2	11
157	1331	-1170	-780	-45	246	126	13.40	16.08	2	17
158	1742	-1387	-768	-135	-321	108	13.40	16.08	2	14
159	1678	-1419	-547	-98	-156	90	13.40	16.08	2	25
160	2147	-1610	-720	-250	-1125	91	13.40	16.08	2	5.1
161	2482	-1808	-629	-384	-2133	60	13.40	16.08	2	2.8
162	2310	-1820	-280	-369	-2063	48	13.40	16.08	2	2.9
163	2362	-1812	-439	-370	-2088	56	13.40	16.08	2	2.9
164	2002	-1656	-298	-210	-940	65	13.40	16.08	2	6.2
165	2059	-1641	-503	-225	-1022	80	13.40	16.08	2	5.6
166	2946	-1705	-1874	-404	-1879	125	13.40	16.08	2	3.1
167	455	-829	-1488	23	513	254	13.40	16.08	2	8.0
168	1292	-1107	-1747	-109	-98	242	13.40	16.08	2	14
169	2119	-1396	-1875	-254	-909	194	13.40	16.08	2	5.6
170	757	-898	-1219	11	519	202	13.40	16.08	2	8.5
171	1449	-1180	-1408	-108	-87	195	13.40	16.08	2	16
172	1785	-1351	-959	-162	-420	128	13.40	16.08	2	11
173	1683	-1272	-1156	-123	-255	175	13.40	16.08	2	14
174	1355	-1173	-990	-57	138	153	13.40	16.08	2	21
175	885	-943	-940	16	581	166	13.40	16.08	2	8.2
176	2643	-1786	-867	-400	-2112	70	13.40	16.08	2	2.9
177	2225	-1570	-949	-271	-1151	104	13.40	16.08	2	4.9
178	2163	-1450	-1517	-254	-932	162	13.40	16.08	2	5.7
179	2889	-1738	-1490	-408	-1927	108	13.40	16.08	2	3.1
180	2790	-1764	-1155	-409	-2017	87	13.40	16.08	2	3.0

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
181	2224	-1530	-1218	-264	-1046	128	13.40	16.08	2	5.3
182	507	-820	-268	113	990	97	13.40	16.08	2	5.6
183	53	-579	-144	153	1042	100	13.40	16.08	2	5.4
184	-635	-503	-627	175	964	160	13.40	16.08	2	5.4
185	-233	-630	-1106	123	850	227	13.40	16.08	2	5.7
186	191	-690	-957	103	860	190	13.40	16.08	2	5.8
187	-169	-488	-637	144	1005	154	13.40	16.08	2	5.3
188	347	-691	-774	99	897	153	13.40	16.08	2	5.8
189	411	-743	-535	107	955	126	13.40	16.08	2	5.7
190	-114	-510	-367	150	1040	121	13.40	16.08	2	5.3
191	-707	-457	-123	162	890	76	13.40	16.08	2	6.3
192	-339	-380	-71	140	925	94	13.40	16.08	2	6.0
193	-166	-474	-31	146	885	100	13.40	16.08	2	6.2
194	2	-692	-164	130	375	87	13.40	16.08	2	13
195	-67	-526	-2	107	614	87	13.40	16.08	2	8.7
196	188	-584	-74	19	247	63	13.40	16.08	2	20
197	-336	-607	-692	8	-582	-48	13.40	16.08	2	9.7
198	-553	-902	-405	93	-421	-42	13.40	16.08	2	13
199	-1162	-383	-955	-11	-878	-168	13.40	16.08	2	5.8
200	-151	-797	-410	50	-201	-24	13.40	16.08	2	27
201	-65	261	-553	-156	-96	49	13.40	16.08	(8+9)-I-1	25
202	-823	-241	-1269	-126	-1166	-154	13.40	16.08	2	4.6
203	132	-460	-953	-98	-740	-67	13.40	16.08	2	7.6
204	525	-322	-1538	-262	-1126	-139	13.40	16.08	2	4.8
205	-176	-553	267	26	578	-26	13.40	16.08	2	10
206	-79	-459	106	66	659	56	13.40	16.08	2	8.5
207	1985	-1070	-224	-312	-611	-183	13.40	16.08	2	7.8
208	804	-777	151	-127	89	-102	13.40	16.08	2	22
209	1662	-1359	372	-224	-329	-223	13.40	16.08	2	11
210	462	-561	-8	-76	192	8	13.40	16.08	2	31
211	1593	-453	-1403	-370	-1017	-146	13.40	16.08	2	5.2
212	941	-516	-502	-205	-383	-50	13.40	16.08	2	14
213	2076	-837	-795	-355	-785	-176	13.40	16.08	2	6.4
214	-234	3420	-766	-21	-347	106	13.40	16.08	(8+9)-V-3	13
215	-255	4480	-769	98	-442	96	13.40	16.08	(8+9)-V-3	10
216	789	3524	3401	-41	-663	-70	13.40	16.08	(8+9)-VI-1	7.8
217	754	5849	4624	-115	-638	-66	13.40	16.08	(8+9)-II-1	7.8
218	-7	1657	891	86	-496	96	13.40	16.08	2	10.0
219	-219	270	-268	143	-227	140	13.40	16.08	2	16
220	-212	507	220	151	-259	149	13.40	16.08	2	15
221	-27	1073	19	85	-509	86	13.40	16.08	2	10.0
222	48	1496	-97	-9	-797	-15	13.40	16.08	2	7.3
223	55	788	-644	-55	-881	-47	13.40	16.08	2	6.4
224	4	544	-469	56	-523	69	13.40	16.08	2	10
225	-692	-2719	-1585	186	143	145	13.40	16.08	(8+9)-VI-2	16
226	-635	-3201	-1944	231	140	130	13.40	16.08	(8+9)-VI-2	14
227	-698	-2494	-3522	252	93	174	13.40	16.08	(8+9)-II-4	12
228	-390	-2084	-2732	136	79	201	13.40	16.08	(8+9)-II-4	15
229	-567	-145	-48	209	38	172	13.40	16.08	2	14
230	-906	-696	149	259	258	156	13.40	16.08	2	12
231	-762	-1069	561	207	143	177	13.40	16.08	2	13
232	-480	-223	404	192	-32	180	13.40	16.08	2	14
233	260	284	-949	-106	-941	-70	13.40	16.08	2	6.0
234	630	-52	-1037	-168	-982	-87	13.40	16.08	2	5.7
235	297	-69	-687	-34	-474	36	13.40	16.08	2	12
236	128	158	-684	13	-523	51	13.40	16.08	2	11
237	-838	-416	-115	235	319	147	13.40	16.08	2	13
238	-479	-130	-327	182	76	154	13.40	16.08	2	15
239	-1560	553	1044	164	-54	-97	13.40	16.08	(8+9)-II-1	20
240	-150	65	-479	107	-204	123	13.40	16.08	2	19
241	-719	-229	-288	179	365	122	13.40	16.08	2	12
242	1262	118	-788	-87	-8	168	13.40	16.08	(8+9)-I-4	20
243	1574	-509	-709	-336	-1235	-172	13.40	16.08	2	4.3
244	1142	-323	-1010	-242	-1119	-124	13.40	16.08	2	4.9

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
245	822	-303	-641	-191	-768	-65	13.40	16.08	2	7.3
246	2059	37	-1057	-166	-165	146	13.40	16.08	(8+9)-I-4	16
247	-232	-645	-326	130	453	36	13.40	16.08	2	12
248	-449	-400	-424	127	454	50	13.40	16.08	2	12
249	-517	-743	-383	18	-347	-160	13.40	16.08	2	12
250	-681	-892	-493	47	-364	-147	13.40	16.08	2	12
251	-1478	-212	138	129	-33	-27	13.40	16.08	(8+9)-II-1	34
252	-960	-779	-83	3	-737	-213	13.40	16.08	2	6.4
253	-2008	-317	-160	169	47	-47	13.40	16.08	(8+9)-I-1	24
254	-349	-533	-370	-57	-384	-147	13.40	16.08	2	11
255	-616	-707	83	-139	-902	-278	13.40	16.08	2	5.2
256	559	-724	17	-285	-1003	-246	13.40	16.08	2	4.9
257	1428	-638	-288	-346	-1131	-195	13.40	16.08	2	4.6
258	-5	-402	-387	-143	-474	-123	13.40	16.08	2	10
259	471	-301	-434	-196	-610	-85	13.40	16.08	2	8.7
260	-606	-240	-370	133	424	82	13.40	16.08	2	12
261	1325	60	-528	-121	30	125	13.40	16.08	(8+9)-I-4	20
262	1660	-14	36	-175	-26	77	13.40	16.08	(8+9)-I-4	20
263	2034	-2	-672	-195	-110	118	13.40	16.08	(8+9)-I-4	16
264	-558	-411	-155	183	701	77	13.40	16.08	2	7.8
265	-471	-525	116	198	860	59	13.40	16.08	2	6.6
266	-174	-537	-41	166	889	79	13.40	16.08	2	6.3
267	-276	-514	-119	164	761	87	13.40	16.08	2	7.2
268	-251	-546	31	180	903	70	13.40	16.08	2	6.3
269	69	-628	23	160	1033	76	13.40	16.08	2	5.5
270	530	-884	13	127	1019	67	13.40	16.08	2	5.6
271	-200	-717	346	196	982	27	13.40	16.08	2	6.1
272	11	-690	196	172	1014	52	13.40	16.08	2	5.7
273	481	-941	278	139	1026	37	13.40	16.08	2	5.8
274	506	-1009	495	142	1002	7	13.40	16.08	2	6.1
275	143	-904	533	173	1025	-3	13.40	16.08	2	6.0
276	515	-1088	707	139	978	-28	13.40	16.08	2	6.1
277	-1139	-1070	340	275	661	34	13.40	16.08	2	8.9
278	-1241	-1604	401	253	595	26	13.40	16.08	2	10.0
279	-1219	-1342	471	274	721	-23	13.40	16.08	2	8.3
280	-1119	-697	98	267	485	106	13.40	16.08	2	10
281	-1263	-1137	228	272	499	82	13.40	16.08	2	11
282	-1181	-862	227	275	598	70	13.40	16.08	2	9.2
283	-698	-857	492	243	874	-6	13.40	16.08	2	7.0
284	-458	-734	447	219	930	10	13.40	16.08	2	6.5
285	-953	-1015	516	261	807	-16	13.40	16.08	2	7.5
286	-948	-440	-67	237	554	99	13.40	16.08	2	9.3
287	-791	-365	-116	209	642	84	13.40	16.08	2	8.4
288	-844	-705	301	247	796	30	13.40	16.08	2	7.4
289	-688	-582	223	225	831	42	13.40	16.08	2	7.0
290	-831	-535	124	230	733	62	13.40	16.08	2	7.7
291	-1024	-839	330	266	731	28	13.40	16.08	2	8.1
292	-1035	-654	163	259	659	67	13.40	16.08	2	8.4
293	-168	-1430	944	199	920	-166	13.40	16.08	2	5.7
294	-438	-1634	776	201	881	-190	13.40	16.08	2	5.8
295	-1009	-1543	603	259	795	-63	13.40	16.08	2	7.2
296	-1120	-1721	507	238	784	-80	13.40	16.08	2	7.2
297	-811	-1453	689	245	876	-98	13.40	16.08	2	6.4
298	-527	-1478	807	225	908	-133	13.40	16.08	2	5.9
299	-844	-1838	569	220	846	-138	13.40	16.08	2	6.3
300	-142	-912	646	200	995	-25	13.40	16.08	2	6.0
301	307	-1113	833	162	987	-57	13.40	16.08	2	5.9
302	-736	-1179	687	249	886	-61	13.40	16.08	2	6.5
303	-419	-1018	705	225	949	-47	13.40	16.08	2	6.2
304	30	-1181	894	193	979	-87	13.40	16.08	2	5.8
305	-329	-1394	888	220	937	-123	13.40	16.08	2	5.8
306	-236	-1220	909	217	964	-109	13.40	16.08	2	5.7
307	-2	-1361	991	192	944	-136	13.40	16.08	2	5.7
308	-466	-1315	784	226	925	-97	13.40	16.08	2	6.0

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
309	-1193	-2400	180	195	754	-118	13.40	16.08	2	7.2
310	-927	-1850	-0	163	763	-221	13.40	16.08	2	6.3
311	-686	-1732	422	193	835	-211	13.40	16.08	2	5.9
312	-1019	-2279	22	171	768	-167	13.40	16.08	2	6.7
313	-1515	-4866	-1497	-37	509	16	13.40	16.08	2	12
314	-1714	-4011	-1858	-16	534	-37	13.40	16.08	2	11
315	-1440	-3514	-502	98	622	-60	13.40	16.08	2	9.4
316	-1417	-3011	-769	107	658	-115	13.40	16.08	2	8.2
317	-1210	-1923	-616	135	700	-213	13.40	16.08	2	6.8
318	-1386	-2604	-1037	94	642	-156	13.40	16.08	2	7.9
319	-1499	-1964	-1333	80	617	-197	13.40	16.08	2	7.7
320	-1969	-1909	-2393	-3	509	-166	13.40	16.08	2	9.2
321	-2170	-2499	-3014	-92	429	-98	13.40	16.08	2	12
322	-2233	-1641	-3132	-75	442	-139	13.40	16.08	2	11
323	-1789	-2991	-1913	9	538	-98	13.40	16.08	2	10.0
324	-2010	-3113	-2810	-63	469	-77	13.40	16.08	2	12
325	-1791	-2130	-2104	23	544	-151	13.40	16.08	2	9.0
326	-1287	-2389	274	212	679	-58	13.40	16.08	2	8.5
327	-914	-6073	-764	-175	353	97	13.40	16.08	2	15
328	-1167	-5691	-1249	-101	446	62	13.40	16.08	2	13
329	-1197	-4831	-543	-28	450	32	13.40	16.08	2	13
330	-1390	-3560	-229	107	558	-23	13.40	16.08	2	11
331	-1278	-3377	35	125	476	10	13.40	16.08	2	13
332	-1288	-2314	269	239	565	-4	13.40	16.08	2	11
333	-1135	-2906	287	172	415	63	13.40	16.08	2	13
334	-901	-1856	584	196	243	156	13.40	16.08	2	15
335	-1082	-2334	450	200	353	110	13.40	16.08	2	14
336	-1125	-1541	342	258	370	115	13.40	16.08	2	13
337	-1034	-4545	-98	-17	354	57	13.40	16.08	2	16
338	1037	-3390	2713	-267	152	-36	13.40	16.08	(8+9)-VI-3	16
339	-833	-568	-1849	190	141	121	13.40	16.08	(8+9)-VI-2	17
340	-941	-2639	-1549	181	9	129	13.40	16.08	(8+9)-VI-2	17
341	-697	-337	-865	-211	-26	92	13.40	16.08	(8+9)-V-3	17
342	-768	-3435	664	80	230	152	13.40	16.08	2	17
343	-808	-4053	280	32	276	104	13.40	16.08	2	17
344	-385	-5708	66	-236	146	160	13.40	16.08	2	13
345	533	-445	2598	-228	-26	74	13.40	16.08	(8+9)-V-3	17
346	2564	-1991	304	-396	-2202	8	13.40	16.08	2	2.8
347	2389	-1952	157	-375	-2173	13	13.40	16.08	2	2.9
348	2264	-1838	434	-249	-1122	2	13.40	16.08	2	5.5
349	2168	-1810	257	-236	-1097	17	13.40	16.08	2	5.6
350	2002	-1694	-108	-205	-924	48	13.40	16.08	2	6.4
351	2299	-1858	-124	-368	-2069	31	13.40	16.08	2	3.0
352	2313	-1914	20	-367	-2118	21	13.40	16.08	2	2.9
353	2076	-1779	70	-216	-1010	30	13.40	16.08	2	6.0
354	1895	-1667	502	-118	-266	-4	13.40	16.08	2	23
355	1023	-1256	524	79	803	2	13.40	16.08	2	7.7
356	1491	-1483	524	-6	388	-5	13.40	16.08	2	16
357	1095	-1197	-5	54	717	58	13.40	16.08	2	7.9
358	1605	-1492	-51	-57	50	53	13.40	16.08	2	45
359	1857	-1638	327	-121	-297	19	13.40	16.08	2	20
360	1755	-1572	162	-70	-99	60	13.40	16.08	2	38
361	1504	-1467	308	-11	313	24	13.40	16.08	2	18
362	1050	-1224	282	63	770	32	13.40	16.08	2	7.7
363	3097	-2009	1182	-418	-2148	-70	13.40	16.08	2	2.8
364	2630	-1822	1221	-269	-1110	-103	13.40	16.08	2	5.1
365	3048	-2065	941	-428	-2186	-54	13.40	16.08	2	2.8
366	2582	-1876	1007	-273	-1134	-75	13.40	16.08	2	5.1
367	2381	-1863	615	-263	-1131	-18	13.40	16.08	2	5.4
368	2781	-2032	488	-420	-2212	-9	13.40	16.08	2	2.8
369	2955	-2061	703	-432	-2205	-30	13.40	16.08	2	2.8
370	2493	-1880	806	-272	-1139	-47	13.40	16.08	2	5.3
371	2118	-1651	1236	-136	-290	-122	13.40	16.08	2	15
372	2038	-1703	877	-134	-286	-58	13.40	16.08	2	18

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
373	1962	-1688	692	-125	-263	-30	13.40	16.08	2	21
374	2097	-1700	1059	-138	-299	-90	13.40	16.08	2	16
375	1582	-1505	1220	-21	308	-133	13.40	16.08	2	14
376	1053	-1388	1166	70	691	-133	13.40	16.08	2	7.5
377	529	-1297	1056	144	911	-117	13.40	16.08	2	6.0
378	1007	-1299	753	81	798	-34	13.40	16.08	2	7.4
379	1510	-1496	735	-10	384	-33	13.40	16.08	2	15
380	1565	-1524	912	-19	341	-63	13.40	16.08	2	15
381	1602	-1539	1077	-26	306	-97	13.40	16.08	2	15
382	1139	-1401	1061	57	671	-98	13.40	16.08	2	8.0
383	1089	-1346	914	74	736	-58	13.40	16.08	2	7.8
384	750	-1277	963	120	885	-83	13.40	16.08	2	6.4
385	276	-1366	1109	157	866	-192	13.40	16.08	2	5.8
386	381	-1317	1098	154	896	-152	13.40	16.08	2	5.9
387	946	-1360	1237	81	696	-170	13.40	16.08	2	7.1
388	826	-1338	1249	90	690	-211	13.40	16.08	2	6.9
389	482	-975	1060	95	650	-295	13.40	16.08	2	6.5
390	-173	-1333	742	162	805	-259	13.40	16.08	2	5.8
391	672	-1219	1208	98	674	-251	13.40	16.08	2	6.7
392	105	-1387	1003	161	842	-228	13.40	16.08	2	5.8
393	1202	-777	1353	-32	211	-320	13.40	16.08	2	12
394	1859	-1070	1535	-106	-128	-253	13.40	16.08	2	14
395	1227	-1171	1343	17	367	-263	13.40	16.08	2	9.8
396	2994	-1241	1802	-400	-1827	-150	13.40	16.08	2	3.1
397	2376	-1100	1664	-232	-826	-217	13.40	16.08	2	5.9
398	2604	-833	1862	-264	-1274	-240	13.40	16.08	2	4.0
399	3133	-1856	1424	-412	-2067	-88	13.40	16.08	2	2.9
400	3125	-1598	1631	-405	-1951	-111	13.40	16.08	2	3.0
401	2527	-1436	1584	-244	-929	-170	13.40	16.08	2	5.6
402	2619	-1685	1425	-262	-1048	-131	13.40	16.08	2	5.3
403	1394	-1331	1381	-3	349	-216	13.40	16.08	2	11
404	1515	-1436	1332	-13	324	-172	13.40	16.08	2	12
405	2092	-1547	1396	-128	-254	-160	13.40	16.08	2	15
406	2017	-1377	1510	-121	-214	-202	13.40	16.08	2	15
407	76	-763	603	107	644	-328	13.40	16.08	2	6.3
408	-533	-1308	270	153	755	-279	13.40	16.08	2	6.0
409	-579	-493	-158	110	630	-336	13.40	16.08	2	6.3
410	-1008	-1225	-376	130	696	-276	13.40	16.08	2	6.3
411	-2191	-625	-2779	-10	478	-211	13.40	16.08	2	8.9
412	-1391	-1214	-1161	87	621	-253	13.40	16.08	2	7.0
413	-1701	-915	-1818	42	546	-240	13.40	16.08	2	7.8
414	-1390	-278	-1120	88	591	-308	13.40	16.08	2	6.8
415	870	236	1038	-12	139	-361	13.40	16.08	2	12
416	1135	-352	1297	-44	95	-311	13.40	16.08	2	14
417	455	-182	904	56	428	-368	13.40	16.08	2	7.6
418	1985	224	1855	-190	-863	-254	13.40	16.08	2	5.4
419	2118	-386	1748	-229	-995	-212	13.40	16.08	2	5.0
420	2297	160	2028	-297	-1477	-217	13.40	16.08	2	3.6
421	1775	-73	1625	-119	-459	-319	13.40	16.08	2	7.8
422	1588	1025	1719	-152	-738	-300	13.40	16.08	2	5.7
423	1975	1085	2109	-272	-1522	-203	13.40	16.08	2	3.4
424	1102	696	1328	-71	-207	-343	13.40	16.08	2	11
425	-276	351	224	82	503	-379	13.40	16.08	2	6.8
426	-2041	2642	-2028	89	381	-344	13.40	16.08	2	8.0
427	-2211	841	-2385	38	464	-278	13.40	16.08	2	8.0
428	-779	931	-443	89	470	-379	13.40	16.08	2	7.0
429	-1349	615	-1151	83	521	-340	13.40	16.08	2	7.0
430	-1186	1826	-994	83	413	-382	13.40	16.08	2	7.4
431	1485	2417	2067	-225	-1339	-221	13.40	16.08	2	3.7
432	992	2243	1520	-117	-632	-322	13.40	16.08	2	6.1
433	-350	1660	156	61	307	-405	13.40	16.08	2	8.3
434	300	899	653	35	266	-393	13.40	16.08	2	9.1
435	511	2256	1040	-34	-186	-377	13.40	16.08	2	10
436	598	1450	963	-28	-31	-371	13.40	16.08	2	13

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
437	160	2064	587	27	104	-402	13.40	16.08	2	12
438	-1936	4553	-1460	127	244	-397	13.40	16.08	2	8.8
439	-368	2928	225	47	118	-415	13.40	16.08	2	11
440	-863	2463	-442	81	298	-408	13.40	16.08	2	8.2
441	-997	3518	-427	87	203	-423	13.40	16.08	2	9.1
442	-552	5394	819	18	-366	-382	13.40	16.08	2	7.4
443	-2902	9207	1038	2	-530	-229	13.40	16.08	(8+9)-VI-2	6.8
444	-188	6266	1367	-54	-735	-308	13.40	16.08	2	5.2
445	-1620	6347	-630	149	34	-426	13.40	16.08	2	9.1
446	-667	4648	187	63	-41	-420	13.40	16.08	2	11
447	-24	3379	723	5	-139	-400	13.40	16.08	2	11
448	323	3732	1250	-62	-518	-347	13.40	16.08	2	6.6
449	823	4080	1866	-156	-1088	-255	13.40	16.08	2	4.2
Massimi/minimi										
1							13.40			
1								16.08		
76										1.8

Muro [Platea]: 3 - Nodi: [8-20-19-14-12-35-36-11-10-9]Pann=206Spess.=25 cm, Terreno=Terreno1,
 ,Criterio=CLS_Platee, Materiale=C30/37: **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-888	658	-1394	-69	-1328	77	13.40	16.08	2	4.3
2	-2473	819	-308	57	-1198	22	13.40	16.08	2	4.9
3	-2215	691	1138	45	-1202	-44	13.40	16.08	2	4.8
4	-123	241	2173	-110	-1332	-99	13.40	16.08	2	4.2
5	2812	104	2201	-363	-1544	-58	13.40	16.08	2	3.8
6	4494	-466	1069	-463	-1697	-5	13.40	16.08	2	3.6
7	4555	-534	-229	-450	-1710	16	13.40	16.08	2	3.5
8	3880	-413	-1081	-388	-1611	23	13.40	16.08	2	3.7
9	3104	-132	-1595	-327	-1464	30	13.40	16.08	2	4.1
10	2316	291	-1922	-267	-1283	41	13.40	16.08	2	4.5
11	1326	933	-2137	-187	-1061	63	13.40	16.08	2	5.3
12	112	1978	-2005	-70	-781	94	13.40	16.08	2	6.7
13	-1084	3388	-2006	-6	-650	56	13.40	16.08	2	8.1
14	-3168	6618	-2012	201	-405	127	13.40	16.08	2	10
15	-3835	-807	-2481	370	38	185	13.40	16.08	(8+9)-III-2	9.8
16	-3038	-341	-2229	342	62	194	13.40	16.08	(8+9)-III-2	10
17	-2586	-253	-1037	310	75	183	13.40	16.08	(8+9)-III-2	11
18	-2429	-414	-674	256	96	155	13.40	16.08	(8+9)-III-2	13
19	160	-700	1160	-273	18	-50	13.40	16.08	(8+9)-III-3	16
20	103	200	887	-304	-22	-67	13.40	16.08	(8+9)-III-3	14
21	-16	625	707	-319	-72	-79	13.40	16.08	(8+9)-III-3	13
22	-162	1212	628	-302	-123	-87	13.40	16.08	(8+9)-III-3	13
23	-414	1597	-719	-243	-148	-98	13.40	16.08	(8+9)-III-3	15
24	-473	1783	-704	-153	-146	-96	13.40	16.08	(8+9)-III-3	21
25	-247	1831	-344	-46	-150	-59	13.40	16.08	(8+9)-III-3	28
26	-895	244	963	12	-280	-88	13.40	16.08	2	16
27	-446	212	906	-34	-389	-73	13.40	16.08	2	13
28	-408	214	618	-42	-456	-37	13.40	16.08	2	12
29	-904	228	573	-1	-511	-18	13.40	16.08	2	11
30	-846	268	891	-7	-585	-27	13.40	16.08	2	9.9
31	41	241	1129	-82	-680	-22	13.40	16.08	2	8.6
32	848	70	903	-140	-744	-11	13.40	16.08	2	8.0
33	1323	-48	446	-170	-776	-1	13.40	16.08	2	7.8
34	1404	-92	-38	-172	-784	8	13.40	16.08	2	7.6
35	1210	-83	-425	-155	-780	17	13.40	16.08	2	7.6
36	999	-63	-669	-140	-773	21	13.40	16.08	2	7.6

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
37	915	-70	-915	-138	-762	27	13.40	16.08	2	7.7
38	793	-121	-1317	-132	-735	38	13.40	16.08	2	7.8
39	436	-17	-1723	-118	-702	56	13.40	16.08	2	8.0
40	-127	-39	-2132	-79	-638	70	13.40	16.08	2	8.6
41	-847	24	-2333	-21	-531	87	13.40	16.08	2	9.8
42	-1419	-83	-2317	30	-380	107	13.40	16.08	2	12
43	-275	560	-2187	61	-325	99	13.40	16.08	(8+9)-VI-1	14
44	-1586	2585	683	-22	-242	90	13.40	16.08	(8+9)-VI-1	17
45	-1134	285	112	-0	-239	96	13.40	16.08	(8+9)-II-3	18
46	-2270	994	-3697	-125	-51	174	13.40	16.08	(8+9)-III-2	18
47	-2995	3353	-3108	-280	-201	164	13.40	16.08	(8+9)-VII-2	12
48	-3056	5243	-2265	-430	-337	94	13.40	16.08	(8+9)-V-2	10
49	-219	4347	1056	-435	-249	-69	13.40	16.08	(8+9)-VI-2	10
50	-130	2781	1164	-321	-113	-74	13.40	16.08	(8+9)-VI-2	13
51	27	3012	1067	-256	-108	-84	13.40	16.08	(8+9)-VI-2	15
52	137	4328	1229	-235	-197	-94	13.40	16.08	(8+9)-VI-2	15
53	-81	5779	903	-216	-293	-93	13.40	16.08	(8+9)-VIII-2	14
54	-1576	7564	-802	50	-341	-181	13.40	16.08	2	10
55	-1543	9953	641	40	-572	-108	13.40	16.08	2	7.5
56	-380	5991	647	-37	-779	-84	13.40	16.08	2	6.3
57	-145	4051	922	-82	-959	-79	13.40	16.08	2	5.5
58	230	2791	1131	-128	-1144	-70	13.40	16.08	2	4.8
59	782	1918	1245	-181	-1318	-60	13.40	16.08	2	4.3
60	1496	1277	1200	-241	-1470	-50	13.40	16.08	2	3.9
61	2300	795	905	-306	-1594	-41	13.40	16.08	2	3.7
62	2946	508	245	-366	-1673	-30	13.40	16.08	2	3.5
63	2904	409	-755	-373	-1646	-7	13.40	16.08	2	3.6
64	1482	757	-1576	-288	-1508	41	13.40	16.08	2	3.9
65	835	189	-10	-99	-298	-2	13.40	16.08	2	20
66	-1328	-15	-429	67	131	-32	13.40	16.08	(8+9)-III-2	37
67	195	495	-112	54	487	-24	13.40	16.08	2	12
68	-62	172	184	87	-215	-51	13.40	16.08	2	23
69	257	357	-148	102	438	-35	13.40	16.08	2	13
70	143	511	-169	96	647	-26	13.40	16.08	2	8.9
71	-676	353	477	114	258	-68	13.40	16.08	2	18
72	-1005	642	782	95	-124	-92	13.40	16.08	(8+9)-III-3	28
73	-1060	1435	-112	17	-134	-132	13.40	16.08	(8+9)-IV-3	22
74	-697	1137	176	42	-120	-126	13.40	16.08	(8+9)-IV-3	24
75	-902	187	535	107	179	-95	13.40	16.08	2	22
76	-684	1417	36	-16	-112	-105	13.40	16.08	(8+9)-IV-3	27
77	-287	462	155	122	460	-51	13.40	16.08	2	12
78	-397	363	370	95	225	-66	13.40	16.08	2	21
79	-208	377	243	65	206	-62	13.40	16.08	2	22
80	119	483	-9	53	404	-36	13.40	16.08	2	14
81	-24	480	-42	85	516	-48	13.40	16.08	2	11
82	-22	408	125	45	275	-54	13.40	16.08	2	18
83	-325	364	857	72	-154	-79	13.40	16.08	(8+9)-III-3	26
84	-273	-187	377	11	121	26	13.40	16.08	(8+9)-II-2	41
85	717	225	273	-98	-313	-23	13.40	16.08	2	18
86	-48	247	626	-33	-344	-55	13.40	16.08	2	15
87	320	151	629	-24	-120	-65	13.40	16.08	(8+9)-III-3	33
88	114	209	966	-13	-224	-73	13.40	16.08	(8+9)-III-3	20
89	204	58	15	21	-89	-54	13.40	16.08	(8+9)-IV-3	42
90	403	237	522	-73	-332	-43	13.40	16.08	2	16
91	340	510	-275	39	460	-36	13.40	16.08	2	12
92	54	548	-198	94	643	-32	13.40	16.08	2	8.9
93	-337	553	16	116	554	-8	13.40	16.08	2	11
94	-37	596	-177	96	617	-1	13.40	16.08	2	9.7
95	-138	595	-147	103	573	44	13.40	16.08	2	9.7
96	286	637	-276	31	460	77	13.40	16.08	2	11
97	359	629	-285	19	477	15	13.40	16.08	2	12
98	1587	352	494	-243	-679	-62	13.40	16.08	2	8.1
99	469	-542	-570	-164	-32	-28	13.40	16.08	(8+9)-III-2	26
100	485	387	332	-45	-393	-112	13.40	16.08	2	12

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
101	931	583	-353	-73	158	97	13.40	16.08	2	24
102	456	-236	-425	-162	23	52	13.40	16.08	(8+9)-I-1	24
103	1769	396	-433	-182	-306	103	13.40	16.08	2	15
104	2815	41	-647	-291	-916	81	13.40	16.08	2	6.1
105	3118	87	-108	-347	-1009	47	13.40	16.08	2	5.7
106	1840	376	-72	-221	-424	44	13.40	16.08	2	13
107	2707	123	328	-320	-851	-10	13.40	16.08	2	7.0
108	-1414	-1770	403	125	219	-43	13.40	16.08	(8+9)-VI-2	24
109	-991	-516	486	9	251	33	13.40	16.08	2	22
110	-907	-390	536	10	285	106	13.40	16.08	2	16
111	-669	427	234	147	445	-12	13.40	16.08	2	13
112	-932	128	390	125	307	-26	13.40	16.08	2	18
113	-862	89	277	106	373	56	13.40	16.08	2	14
114	-702	139	181	84	383	135	13.40	16.08	2	12
115	-446	407	-19	104	453	127	13.40	16.08	2	10
116	-571	395	92	127	479	63	13.40	16.08	2	11
117	-287	545	-86	115	522	88	13.40	16.08	2	9.8
118	2305	182	-1092	-234	-789	109	13.40	16.08	2	6.7
119	124	614	-279	50	428	132	13.40	16.08	2	11
120	709	578	-466	-37	186	155	13.40	16.08	2	18
121	1463	435	-715	-135	-226	149	13.40	16.08	2	16
122	-101	497	-220	62	387	178	13.40	16.08	2	11
123	-426	369	1	60	340	204	13.40	16.08	2	11
124	-774	50	545	34	278	179	13.40	16.08	2	13
125	1675	462	-1334	-178	-639	138	13.40	16.08	2	7.7
126	378	580	-480	-3	204	204	13.40	16.08	2	15
127	1008	563	-842	-87	-139	190	13.40	16.08	2	18
128	-1945	-784	-1688	144	34	181	13.40	16.08	(8+9)-III-2	16
129	45	1554	-1045	-46	-281	199	13.40	16.08	2	12
130	-2426	-591	-1847	218	46	189	13.40	16.08	(8+9)-III-2	13
131	457	815	-766	-40	-61	223	13.40	16.08	2	19
132	980	892	-1367	-117	-482	167	13.40	16.08	2	9.2
133	-1939	-456	-758	211	80	179	13.40	16.08	(8+9)-III-2	14
134	-350	929	-63	49	176	249	13.40	16.08	2	14
135	-2150	-484	-995	240	84	194	13.40	16.08	(8+9)-III-2	12
136	-5	659	-333	26	210	239	13.40	16.08	2	13
137	-1854	-313	747	148	-93	-74	13.40	16.08	(8+9)-I-1	24
138	136	406	119	125	432	-1	13.40	16.08	2	14
139	88	551	-77	111	646	-1	13.40	16.08	2	9.3
140	789	157	-304	-84	-294	18	13.40	16.08	2	19
141	180	526	-189	63	495	7	13.40	16.08	2	12
142	53	-136	330	48	140	26	13.40	16.08	(8+9)-VI-2	37
143	15	581	-307	79	475	37	13.40	16.08	2	12
144	-300	639	-585	95	396	77	13.40	16.08	2	13
145	255	191	-1118	-34	-238	77	13.40	16.08	2	19
146	661	135	565	38	108	64	13.40	16.08	(8+9)-VI-4	35
147	550	186	-845	-74	-330	43	13.40	16.08	2	16
148	656	154	-592	-72	-303	29	13.40	16.08	2	18
149	311	371	-496	5	135	38	13.40	16.08	2	35
150	-2009	728	-1989	70	152	163	13.40	16.08	(8+9)-I-2	19
151	-1510	-105	-1913	97	99	207	13.40	16.08	2	17
152	-731	584	-983	136	302	122	13.40	16.08	2	14
153	-1197	360	-1489	150	185	176	13.40	16.08	2	16
154	-1215	-29	-1999	79	-147	177	13.40	16.08	2	19
155	-1017	161	-1692	93	-12	184	13.40	16.08	2	19
156	-842	125	-1959	27	-269	147	13.40	16.08	2	15
157	-420	157	-1771	-17	-312	121	13.40	16.08	2	14
158	-506	321	-1416	50	-15	143	13.40	16.08	2	27
159	-79	206	-1391	-19	-230	91	13.40	16.08	2	19
160	-104	692	-53	127	635	20	13.40	16.08	2	9.1
161	-382	864	-178	153	600	29	13.40	16.08	2	9.5
162	-3	688	206	101	453	16	13.40	16.08	2	13
163	-163	1011	123	113	482	-17	13.40	16.08	2	12
164	-139	661	56	13	-390	82	13.40	16.08	2	13

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
165	1964	-141	-432	-199	28	28	13.40	16.08	(8+9)-I-4	22
166	611	863	-166	-157	-664	41	13.40	16.08	2	8.5
167	1795	1003	82	-264	-1020	-64	13.40	16.08	2	5.5
168	1438	890	-154	-228	-833	-4	13.40	16.08	2	7.1
169	808	1139	43	-135	-452	-63	13.40	16.08	2	12
170	2174	-46	-389	-210	62	-88	13.40	16.08	(8+9)-I-4	16
171	-1072	1548	-561	154	305	-123	13.40	16.08	2	14
172	-1398	698	-1196	180	313	107	13.40	16.08	2	14
173	-1478	-1273	-1039	131	312	65	13.40	16.08	(8+9)-VI-3	16
174	-970	1156	-508	204	456	-14	13.40	16.08	2	13
175	-705	1036	-333	197	547	13	13.40	16.08	2	11
176	-924	872	-710	190	452	73	13.40	16.08	2	11
177	-693	1444	-219	163	375	-106	13.40	16.08	2	12
178	-387	1288	4	134	433	-65	13.40	16.08	2	12
179	-1509	-2357	-1445	74	289	109	13.40	16.08	(8+9)-VI-3	16
180	1037	1767	1387	-96	-13	-187	13.40	16.08	(8+9)-II-4	18
181	980	2082	1882	-153	-41	-171	13.40	16.08	(8+9)-II-4	15
182	-1654	-1998	-1419	103	298	80	13.40	16.08	(8+9)-VI-3	16
183	-1650	-3261	-1643	71	353	105	13.40	16.08	(8+9)-VI-3	14
184	773	2463	1496	-168	-112	-164	13.40	16.08	(8+9)-II-4	15
185	1549	1099	444	-209	-960	-102	13.40	16.08	2	5.6
186	683	1899	818	-104	-797	-149	13.40	16.08	2	6.2
187	1137	1410	713	-153	-885	-129	13.40	16.08	2	5.8
188	790	1309	244	-95	-372	-124	13.40	16.08	2	12
189	618	1533	396	-57	-366	-165	13.40	16.08	2	11
190	356	1902	479	-28	-353	-196	13.40	16.08	2	11
191	2146	-276	-445	-174	81	-143	13.40	16.08	(8+9)-I-4	15
192	1804	-674	1370	-110	-49	-219	13.40	16.08	(8+9)-II-4	15
193	2155	-564	1012	-147	53	-175	13.40	16.08	(8+9)-I-4	15
194	-336	1697	41	101	199	-175	13.40	16.08	2	16
195	1186	2037	2166	-116	-39	-166	13.40	16.08	(8+9)-II-4	18
196	-792	1969	-238	104	191	-197	13.40	16.08	2	15
197	1249	1762	1718	-90	-19	-200	13.40	16.08	(8+9)-II-4	17
198	6	2509	442	-3	-296	-220	13.40	16.08	2	11
199	1547	1435	1642	-84	-52	-224	13.40	16.08	(8+9)-II-4	16
200	251	2653	787	-63	-680	-167	13.40	16.08	2	6.8
201	1364	1879	1991	-68	-67	-209	13.40	16.08	(8+9)-II-4	18
202	271	3608	1304	-100	-157	-130	13.40	16.08	(8+9)-VI-2	20
203	-454	3349	183	8	-225	-232	13.40	16.08	2	13
204	-201	3760	610	-31	-546	-181	13.40	16.08	2	7.8
205	-1042	4467	-442	4	-181	-219	13.40	16.08	2	14
206	-904	5530	192	-4	-428	-183	13.40	16.08	2	9.0
Massimi/minimi										
1							13.40			
1								16.08		
62										3.5

Muro [Platea]: 4 - Nodi: [11-36-35-12-13-34-33-32]Pann=130Spess.=25 cm, Terreno=Terreno1,
 ,Criterio=CLS_Platee, Materiale=C30/37: **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-1324	-840	80	14	-410	21	13.40	16.08	2	14
2	-796	-1050	502	-37	-552	11	13.40	16.08	2	11
3	-79	-1267	626	-88	-682	15	13.40	16.08	2	8.9
4	465	-1310	528	-139	-794	20	13.40	16.08	2	7.6
5	700	-1380	344	-154	-835	21	13.40	16.08	2	7.2
6	723	-1427	187	-151	-820	19	13.40	16.08	2	7.4
7	779	-1449	65	-149	-813	12	13.40	16.08	2	7.5

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
8	972	-1457	-82	-162	-828	4	13.40	16.08	2	7.4
9	1167	-1428	-356	-185	-865	6	13.40	16.08	2	7.1
10	1131	-1332	-719	-187	-893	12	13.40	16.08	2	6.8
11	696	-1208	-1056	-152	-844	20	13.40	16.08	2	7.1
12	-26	-1070	-1078	-63	-687	52	13.40	16.08	2	8.3
13	-952	-862	-866	-21	-607	35	13.40	16.08	2	9.6
14	-1032	-681	-439	-14	-560	10	13.40	16.08	2	11
15	-547	-403	-315	-45	-470	26	13.40	16.08	2	12
16	-570	-104	-420	-30	-325	54	13.40	16.08	2	16
17	-899	354	-571	-3	-251	30	13.40	16.08	2	21
18	-2459	600	-673	158	-60	34	13.40	16.08	(8+9)-IV-1	28
19	-1764	979	552	212	34	118	13.40	16.08	(8+9)-IV-3	16
20	-1810	-534	870	198	116	112	13.40	16.08	(8+9)-IV-3	17
21	-1937	-1514	1245	210	165	96	13.40	16.08	(8+9)-IV-3	17
22	-427	470	-564	-297	-73	-82	13.40	16.08	(8+9)-IV-2	14
23	-84	865	-708	-342	-120	-110	13.40	16.08	(8+9)-IV-2	11
24	690	1683	-721	-328	-185	-122	13.40	16.08	(8+9)-IV-2	11
25	2705	2457	-191	-254	-239	-105	13.40	16.08	(8+9)-IV-2	13
26	1574	926	-672	-120	-247	-93	13.40	16.08	(8+9)-IV-2	18
27	396	272	-961	-53	-266	-80	13.40	16.08	(8+9)-VIII-2	17
28	-409	-55	-1151	-4	-293	-62	13.40	16.08	(8+9)-VIII-2	17
29	-1008	-277	-1052	45	-269	-48	13.40	16.08	(8+9)-IV-2	19
30	-1790	-382	-813	70	-240	-36	13.40	16.08	(8+9)-VIII-2	22
31	-2139	-465	-596	75	-232	-34	13.40	16.08	(8+9)-IV-2	23
32	-2276	-611	-406	76	-234	-31	13.40	16.08	(8+9)-IV-2	23
33	-2327	-672	277	76	-244	-29	13.40	16.08	(8+9)-II-2	22
34	-2295	-686	513	72	-275	-17	13.40	16.08	(8+9)-VI-2	21
35	-2004	-724	1264	57	-301	-35	13.40	16.08	(8+9)-II-2	18
36	-1529	-726	1732	31	-374	-42	13.40	16.08	(8+9)-VI-2	15
37	-544	-715	2206	-27	-452	-55	13.40	16.08	(8+9)-VI-2	12
38	613	-122	2771	-100	-532	-73	13.40	16.08	(8+9)-VI-2	10
39	-3353	-4652	-3563	194	640	126	13.40	16.08	(8+9)-VI-3	8.5
40	2607	7220	4703	-218	-602	-48	13.40	16.08	(8+9)-VI-2	8.3
41	-3044	-3897	-6734	76	303	172	13.40	16.08	(8+9)-VI-3	14
42	2251	-6116	4737	51	343	-110	13.40	16.08	(8+9)-VI-2	15
43	1500	-9567	1283	215	646	-29	13.40	16.08	(8+9)-VI-2	10
44	-1156	4475	1323	-282	-293	-146	13.40	16.08	(8+9)-VI-3	12
45	65	-3463	755	-14	159	-78	13.40	16.08	(8+9)-III-4	27
46	12	-2902	1164	97	159	-61	13.40	16.08	(8+9)-III-3	29
47	-1751	3444	-1581	-31	-247	43	13.40	16.08	(8+9)-I-1	20
48	-1274	748	-1730	68	-310	47	13.40	16.08	(8+9)-III-2	17
49	-2018	-3060	1117	221	246	19	13.40	16.08	(8+9)-IV-3	22
50	-2346	-3457	991	221	277	-1	13.40	16.08	(8+9)-IV-3	23
51	-1945	-2809	815	174	261	-1	13.40	16.08	(8+9)-IV-3	24
52	-1010	-1039	61	119	269	63	13.40	16.08	2	19
53	-1426	-2405	938	189	209	45	13.40	16.08	(8+9)-IV-3	22
54	-932	-298	-195	19	17	121	13.40	16.08	2	37
55	-1130	-709	43	55	158	118	13.40	16.08	2	22
56	-717	-639	-436	21	-123	90	13.40	16.08	2	29
57	-1107	240	-241	66	58	100	13.40	16.08	(8+9)-VIII-2	31
58	-729	-730	-562	18	-264	64	13.40	16.08	2	19
59	-859	-828	-210	84	177	110	13.40	16.08	2	21
60	-1106	138	-83	75	64	101	13.40	16.08	(8+9)-IV-2	30
61	-791	-15	46	86	65	92	13.40	16.08	(8+9)-IV-2	29
62	-579	-991	-316	87	148	102	13.40	16.08	2	25
63	-456	-987	-505	24	-226	80	13.40	16.08	2	20
64	-471	-1936	890	96	261	-25	13.40	16.08	(8+9)-III-3	22
65	-1504	-2310	640	114	255	-30	13.40	16.08	(8+9)-VII-3	22
66	-946	-1108	130	127	330	14	13.40	16.08	2	18
67	-2109	-2205	1106	109	259	-19	13.40	16.08	(8+9)-VIII-3	23
68	-779	-1031	-88	109	301	65	13.40	16.08	2	17
69	-1325	-2073	1198	57	234	-16	13.40	16.08	(8+9)-VIII-3	25
70	-602	-1847	1042	12	227	-6	13.40	16.08	(8+9)-VIII-3	27
71	-457	-1871	901	75	255	-24	13.40	16.08	(8+9)-III-3	22

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
72	713	-1476	-93	-59	178	23	13.40	16.08	(8+9)-VI-3	31
73	-592	-1199	-94	49	281	-2	13.40	16.08	2	22
74	337	-1493	638	-41	201	11	13.40	16.08	(8+9)-IV-3	29
75	-135	-1574	955	-7	223	-17	13.40	16.08	(8+9)-III-3	26
76	-552	-1118	-131	57	408	5	13.40	16.08	2	15
77	-626	-1089	-44	73	384	15	13.40	16.08	2	15
78	-751	-1115	32	101	363	19	13.40	16.08	2	16
79	-1291	-727	279	70	91	50	13.40	16.08	(8+9)-III-2	43
80	431	-1274	-174	-74	-232	-8	13.40	16.08	2	26
81	541	-1213	-390	-114	-373	17	13.40	16.08	2	16
82	-316	-1080	-156	23	336	7	13.40	16.08	2	18
83	-424	-1049	-164	50	348	36	13.40	16.08	2	16
84	-559	-1044	-157	79	320	61	13.40	16.08	2	16
85	-143	-995	-447	-24	-124	81	13.40	16.08	2	30
86	-1344	-208	54	111	58	91	13.40	16.08	(8+9)-III-2	26
87	-193	-1025	-663	-54	-334	61	13.40	16.08	2	16
88	-1224	-330	166	109	119	71	13.40	16.08	(8+9)-III-2	29
89	340	-1143	-699	-109	-496	49	13.40	16.08	2	11
90	137	-1091	-475	-57	-206	56	13.40	16.08	2	23
91	525	-1176	-542	-112	-450	28	13.40	16.08	2	13
92	-967	-520	187	76	128	53	13.40	16.08	(8+9)-IV-2	34
93	365	-1315	-56	-62	-222	2	13.40	16.08	2	28
94	-931	-1306	190	38	127	-20	13.40	16.08	(8+9)-VI-2	42
95	325	-1295	130	-85	-350	-11	13.40	16.08	2	17
96	181	-1274	313	-97	-495	-21	13.40	16.08	2	12
97	-85	-1262	172	-39	-206	-53	13.40	16.08	2	24
98	272	-1334	226	-87	-416	-6	13.40	16.08	2	15
99	-126	-1306	240	-37	-337	-57	13.40	16.08	2	16
100	-1052	-1589	250	6	195	4	13.40	16.08	(8+9)-VI-2	31
101	-242	-2697	312	14	286	23	13.40	16.08	(8+9)-VI-2	20
102	-297	-4328	183	99	410	61	13.40	16.08	(8+9)-VI-2	14
103	-964	-1099	-41	34	-211	-52	13.40	16.08	2	23
104	-578	-1228	103	2	-261	-61	13.40	16.08	2	19
105	-610	822	-304	41	-116	-148	13.40	16.08	(8+9)-II-3	23
106	-83	896	407	-50	-44	-167	13.40	16.08	(8+9)-V-3	24
107	-1110	614	-1567	86	-172	40	13.40	16.08	(8+9)-III-2	28
108	-355	-1570	378	-17	270	-132	13.40	16.08	(8+9)-VI-2	15
109	-388	-1885	345	-10	400	-78	13.40	16.08	(8+9)-VI-2	13
110	362	-2111	1627	-36	304	-152	13.40	16.08	(8+9)-VI-2	14
111	-297	-4085	1068	23	524	-48	13.40	16.08	(8+9)-VI-2	11
112	-2181	-3331	-2579	154	324	206	13.40	16.08	(8+9)-VI-3	12
113	-923	-1117	-1684	74	336	137	13.40	16.08	(8+9)-VI-3	13
114	-1848	-1168	-1656	122	339	173	13.40	16.08	(8+9)-VI-3	12
115	-1293	-1150	-940	117	259	166	13.40	16.08	(8+9)-VI-3	14
116	-475	-1378	-219	79	344	-47	13.40	16.08	2	16
117	-608	-1460	-302	96	376	-14	13.40	16.08	2	16
118	-609	-1271	-197	64	374	-2	13.40	16.08	2	16
119	-517	-1258	-215	65	421	-9	13.40	16.08	2	14
120	-603	-1280	-223	74	388	-5	13.40	16.08	2	16
121	-598	-1138	-172	64	406	-7	13.40	16.08	2	15
122	-334	-1186	-160	33	334	-19	13.40	16.08	2	17
123	744	-1444	-235	-57	188	37	13.40	16.08	(8+9)-VI-3	28
124	-568	-1208	-181	47	287	2	13.40	16.08	2	21
125	202	-1099	-351	-19	240	64	13.40	16.08	(8+9)-VI-3	20
126	613	-1417	-461	-42	207	54	13.40	16.08	(8+9)-VI-3	24
127	-635	-1138	-610	59	246	125	13.40	16.08	(8+9)-VI-3	17
128	-42	-1102	-472	13	246	89	13.40	16.08	(8+9)-VI-3	18
129	267	-1467	-708	-14	238	76	13.40	16.08	(8+9)-VI-3	20
130	-246	-1106	-963	20	283	106	13.40	16.08	(8+9)-VI-3	16
Massimi/minimi										
1							13.40			
1								16.08		
10										6.8

Muro [Platea]: 5 - Nodi: [6-106-114-112-213-13-12-14]Pann=104Spess.=25 cm, Terreno=Terreno1,
 ,Criterio=CLS_Platea, Materiale=C30/37: **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	805	-692	-1070	-480	-8	75	13.40	16.08	(8+9)-IV-2	9.0
2	1071	-308	78	-630	-40	-59	13.40	16.08	(8+9)-II-2	7.2
3	-745	-160	-204	-759	-89	-59	13.40	16.08	(8+9)-III-2	6.3
4	129	-165	97	-700	-96	-40	13.40	16.08	(8+9)-III-2	6.9
5	529	-83	471	-716	-79	-51	13.40	16.08	(8+9)-IV-2	6.6
6	278	273	959	-673	-76	-81	13.40	16.08	(8+9)-III-2	6.7
7	1743	-83	1319	-564	-63	-95	13.40	16.08	(8+9)-III-2	7.5
8	110	-712	-424	-508	-32	27	13.40	16.08	(8+9)-IV-3	9.5
9	413	-551	461	-570	-58	5	13.40	16.08	(8+9)-IV-3	8.8
10	3588	-1185	1443	-379	33	-94	13.40	16.08	(8+9)-IV-3	10
11	2657	-2120	805	-92	124	-186	13.40	16.08	(8+9)-IV-3	17
12	2546	-2998	397	-39	154	-184	13.40	16.08	(8+9)-IV-3	19
13	2815	-4098	-359	115	207	-225	13.40	16.08	(8+9)-IV-3	14
14	1912	-4651	-658	285	263	-151	13.40	16.08	(8+9)-IV-3	11
15	-763	-5279	-1501	348	250	-91	13.40	16.08	(8+9)-IV-3	12
16	494	-5484	-771	511	305	5	13.40	16.08	(8+9)-IV-3	9.8
17	1334	-4524	-909	603	288	15	13.40	16.08	(8+9)-IV-3	8.0
18	1530	-3578	-1415	649	235	45	13.40	16.08	(8+9)-IV-3	7.1
19	1374	-2661	-1921	627	191	72	13.40	16.08	(8+9)-IV-3	7.1
20	797	-1788	-2334	589	152	87	13.40	16.08	(8+9)-IV-3	7.4
21	634	-744	-1628	567	95	64	13.40	16.08	(8+9)-IV-1	8.0
22	1238	-619	615	601	104	-6	13.40	16.08	(8+9)-III-1	8.2
23	946	-396	731	667	98	-10	13.40	16.08	(8+9)-III-1	7.4
24	986	-1029	1262	707	132	-26	13.40	16.08	(8+9)-III-1	6.8
25	1911	-1840	2117	686	174	-40	13.40	16.08	(8+9)-III-2	6.8
26	827	-2122	1716	667	195	-38	13.40	16.08	(8+9)-III-2	7.1
27	1058	-2494	-262	695	216	-11	13.40	16.08	(8+9)-III-2	7.1
28	2117	-2825	-262	689	221	19	13.40	16.08	(8+9)-IV-2	6.9
29	1985	-1644	-829	683	179	32	13.40	16.08	(8+9)-IV-2	6.9
30	1649	-974	-1305	687	136	44	13.40	16.08	(8+9)-IV-2	6.7
31	263	555	-207	756	77	63	13.40	16.08	(8+9)-III-2	6.2
32	-156	911	-182	814	53	67	13.40	16.08	(8+9)-III-2	5.8
33	-1093	400	-24	925	54	71	13.40	16.08	(8+9)-III-2	5.2
34	-1600	369	712	1094	79	73	13.40	16.08	(8+9)-III-2	4.5
35	-2467	-1692	324	1335	253	60	13.40	16.08	(8+9)-I-1	3.8
36	-1440	-3074	2528	1389	332	-47	13.40	16.08	(8+9)-III-2	3.6
37	-160	-3141	962	1239	304	-55	13.40	16.08	(8+9)-III-2	3.9
38	1464	-2635	511	1048	231	-25	13.40	16.08	(8+9)-III-2	4.6
39	654	-2070	-745	809	168	9	13.40	16.08	(8+9)-III-2	6.1
40	935	-614	-881	697	168	33	13.40	16.08	(8+9)-III-2	6.8
41	1072	-773	-1171	596	90	41	13.40	16.08	(8+9)-III-2	7.8
42	1135	-784	-1474	519	90	54	13.40	16.08	(8+9)-III-2	8.7
43	1791	-5592	-629	434	320	74	13.40	16.08	2	9.7
44	1449	-5652	-2033	420	323	116	13.40	16.08	2	9.2
45	902	-5561	-3399	403	307	148	13.40	16.08	2	9.1
46	-201	468	-124	553	139	52	13.40	16.08	(8+9)-IV-1	8.4
47	-387	-1993	-331	592	131	66	13.40	16.08	(8+9)-IV-1	7.8
48	-978	-1752	361	652	132	68	13.40	16.08	(8+9)-VIII-1	7.2
49	-2302	-1646	429	655	134	65	13.40	16.08	(8+9)-VIII-1	7.4
50	-3743	-3496	510	652	231	62	13.40	16.08	(8+9)-VIII-1	7.6
51	-9152	-2176	700	596	162	118	13.40	16.08	(8+9)-VIII-1	8.3
52	-5075	1768	-4146	261	-148	140	13.40	16.08	2	14
53	-4824	129	-3754	354	22	216	13.40	16.08	2	9.7
54	-1228	1088	840	-391	-69	-39	13.40	16.08	(8+9)-VIII-1	12

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
55	84	-597	142	-411	-74	-62	13.40	16.08	(8+9)-VIII-1	11
56	936	-3296	-278	260	222	-81	13.40	16.08	(8+9)-VI-3	15
57	1304	-3324	-289	154	175	-156	13.40	16.08	(8+9)-IV-3	16
58	1166	-324	1187	-6	46	-115	13.40	16.08	(8+9)-IV-2	38
59	735	-1331	1382	390	131	-93	13.40	16.08	(8+9)-III-2	10
60	1721	-1074	1864	506	123	-81	13.40	16.08	(8+9)-III-2	8.4
61	621	-1900	-1152	157	97	92	13.40	16.08	(8+9)-IV-3	20
62	630	-1408	-768	-119	29	62	13.40	16.08	(8+9)-IV-3	28
63	330	-1130	-1279	78	54	124	13.40	16.08	(8+9)-IV-3	25
64	853	-1897	-316	146	83	28	13.40	16.08	(8+9)-IV-3	29
65	1302	-3090	-226	306	175	-33	13.40	16.08	(8+9)-IV-3	15
66	575	-1296	-1901	365	105	119	13.40	16.08	(8+9)-IV-3	10
67	881	-2219	-1411	388	143	93	13.40	16.08	(8+9)-IV-3	10
68	1046	-2916	-916	403	171	48	13.40	16.08	(8+9)-IV-3	11
69	1776	-128	1603	23	22	-137	13.40	16.08	(8+9)-IV-2	31
70	1731	-495	1678	366	89	-92	13.40	16.08	(8+9)-III-2	11
71	511	-359	-1381	418	55	78	13.40	16.08	(8+9)-IV-1	10
72	1672	-2071	-344	522	192	27	13.40	16.08	(8+9)-IV-2	9.0
73	1795	-1437	-420	330	146	32	13.40	16.08	(8+9)-IV-2	14
74	1632	-1187	-590	486	151	45	13.40	16.08	(8+9)-IV-2	9.3
75	895	-1696	833	474	165	-39	13.40	16.08	(8+9)-III-2	9.8
76	1738	71	-923	-20	59	83	13.40	16.08	(8+9)-I-4	43
77	1324	-1454	1603	406	107	-108	13.40	16.08	(8+9)-II-2	9.6
78	-1918	1181	1785	235	-72	-152	13.40	16.08		2
79	-73	-2210	785	955	236	23	13.40	16.08	(8+9)-III-2	5.2
80	-1639	-1702	1384	889	267	-14	13.40	16.08	(8+9)-III-2	5.8
81	1229	-180	-1306	569	61	79	13.40	16.08	(8+9)-IV-2	7.7
82	1261	-255	-1045	393	48	83	13.40	16.08	(8+9)-IV-2	10
83	869	376	-1158	533	17	73	13.40	16.08	(8+9)-IV-2	8.3
84	1524	-588	-966	494	80	64	13.40	16.08	(8+9)-IV-2	8.9
85	-494	-36	-1243	102	38	115	13.40	16.08		2
86	-1738	1611	-491	185	-75	69	13.40	16.08		2
87	-1928	-949	116	950	170	-14	13.40	16.08	(8+9)-I-1	5.5
88	429	1397	-890	606	-63	81	13.40	16.08	(8+9)-IV-2	7.3
89	752	-622	-1278	206	43	117	13.40	16.08	(8+9)-III-2	16
90	1601	-922	1265	-47	55	-142	13.40	16.08	(8+9)-III-3	26
91	10	-3263	-842	211	192	64	13.40	16.08		2
92	698	-448	-756	225	34	106	13.40	16.08	(8+9)-III-2	15
93	721	-1644	-648	370	117	71	13.40	16.08	(8+9)-III-2	11
94	878	-4415	-908	339	271	80	13.40	16.08		2
95	945	-676	-1361	359	66	98	13.40	16.08	(8+9)-III-2	11
96	858	-656	-1035	421	67	85	13.40	16.08	(8+9)-III-2	9.9
97	585	-4426	-2250	339	276	141	13.40	16.08		2
98	39	-4279	-3699	330	255	205	13.40	16.08		2
99	-4345	635	-4300	268	-1	277	13.40	16.08		2
100	-2210	-2327	-5086	246	162	299	13.40	16.08		2
101	-3663	-588	-4675	245	82	311	13.40	16.08		2
102	-1412	-2927	-4015	243	178	262	13.40	16.08		2
103	-1534	-2042	-3463	92	115	249	13.40	16.08		2
104	-310	-3187	-2431	228	194	156	13.40	16.08		2
Massimi/minimi										
1							13.40			
1								16.08		
36										3.6

Muro [Platea]: 6 - Nodi: [13-213-113-134-34]Pann=59Spess.=25 cm, Terreno=Terreno1,
 ,Criterio=CLS_Platee, Materiale=C30/37: **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	1458	-935	1320	-379	-342	-317	13.40	16.08	(8+9)-IV-3	7.1
2	534	-35	716	-336	-361	-286	13.40	16.08	(8+9)-IV-3	8.1
3	1858	1127	1344	-338	-282	-242	13.40	16.08	1	8.5
4	1733	1391	1238	-403	-349	-290	13.40	16.08	1	7.1
5	2375	-2054	-955	-392	-194	-204	13.40	16.08	(8+9)-V-3	8.2
6	2177	-3162	-1545	-183	-121	-95	13.40	16.08	(8+9)-V-3	18
7	386	-6446	-3110	296	157	99	13.40	16.08	(8+9)-VI-3	13
8	-5162	-7891	-4479	530	362	256	13.40	16.08	(8+9)-VI-3	7.1
9	-2174	-5324	-1147	521	465	285	13.40	16.08	(8+9)-VI-3	6.6
10	72	-3326	-356	440	403	290	13.40	16.08	(8+9)-VI-3	7.0
11	600	-2254	-360	353	343	276	13.40	16.08	(8+9)-VI-3	8.0
12	1749	-1291	-429	284	284	256	13.40	16.08	(8+9)-VI-3	9.1
13	1914	-408	-538	243	235	237	13.40	16.08	(8+9)-VI-3	10
14	1890	166	-642	225	195	221	13.40	16.08	(8+9)-II-3	11
15	1160	1157	-448	218	151	220	13.40	16.08	(8+9)-II-3	11
16	1038	1777	-158	222	157	216	13.40	16.08	(8+9)-IV-3	11
17	272	1930	-128	231	163	215	13.40	16.08	(8+9)-IV-3	11
18	-142	2236	68	271	210	215	13.40	16.08	(8+9)-IV-3	10
19	-644	2246	535	323	240	229	13.40	16.08	(8+9)-IV-3	9.3
20	-1256	2077	1206	366	291	238	13.40	16.08	(8+9)-IV-3	8.6
21	-1962	1432	1901	429	384	231	13.40	16.08	(8+9)-IV-3	8.0
22	-2403	138	2761	471	476	208	13.40	16.08	(8+9)-IV-3	7.8
23	-2949	-1271	3350	455	513	151	13.40	16.08	(8+9)-IV-3	8.8
24	-4062	-626	3030	282	581	85	13.40	16.08	(8+9)-IV-3	9.2
25	-1025	-598	4036	125	621	48	13.40	16.08	(8+9)-IV-3	9.1
26	1259	-862	4153	-12	608	13	13.40	16.08	(8+9)-IV-3	9.9
27	3216	-1230	3662	-153	503	-46	13.40	16.08	(8+9)-IV-3	11
28	4398	-1699	3109	-211	374	-103	13.40	16.08	(8+9)-IV-3	13
29	4678	-2333	2904	-223	127	-146	13.40	16.08	(8+9)-IV-3	13
30	4123	-1641	2515	-352	-72	-251	13.40	16.08	(8+9)-IV-3	7.8
31	2911	-1138	2112	-384	-229	-294	13.40	16.08	(8+9)-IV-3	7.1
32	698	-809	2738	-51	328	-48	13.40	16.08	(8+9)-IV-3	16
33	2202	-940	2601	-229	153	-133	13.40	16.08	(8+9)-IV-3	13
34	738	-557	1702	-168	24	-124	13.40	16.08	(8+9)-IV-3	17
35	1458	2925	2164	56	-195	-75	13.40	16.08	(8+9)-II-2	21
36	-514	-3406	-1714	268	249	136	13.40	16.08	(8+9)-VI-3	13
37	-289	-2220	-643	183	257	154	13.40	16.08	(8+9)-VI-3	15
38	1233	324	401	-57	-44	33	13.40	16.08	(8+9)-VI-3	56
39	1283	2209	1923	111	-130	-71	13.40	16.08	(8+9)-VI-2	27
40	1417	-58	-10	-174	-28	-85	13.40	16.08	(8+9)-V-3	19
41	1500	2047	2225	23	-86	-69	13.40	16.08	(8+9)-VI-2	38
42	1415	2212	1792	71	-186	-78	13.40	16.08	(8+9)-II-2	22
43	494	-1869	-292	103	218	144	13.40	16.08	(8+9)-VI-3	17
44	684	-642	-191	100	197	149	13.40	16.08	(8+9)-VI-3	18
45	1126	1365	-3	116	75	155	13.40	16.08	(8+9)-VI-3	18
46	936	-125	-93	107	164	154	13.40	16.08	(8+9)-VI-3	19
47	1053	62	-526	124	151	159	13.40	16.08	(8+9)-VI-3	18
48	-5	1787	394	181	55	126	13.40	16.08	(8+9)-IV-3	17
49	2544	573	1777	-123	51	-61	13.40	16.08	(8+9)-IV-2	26
50	198	1450	789	156	19	98	13.40	16.08	(8+9)-IV-3	20
51	632	1698	268	70	-42	68	13.40	16.08	(8+9)-VIII-3	36
52	1071	1383	534	-48	-11	79	13.40	16.08	(8+9)-VI-3	39
53	-834	-474	2528	90	390	14	13.40	16.08	(8+9)-VIII-3	15
54	-1987	-902	2711	268	448	64	13.40	16.08	(8+9)-IV-3	12
55	2703	497	153	-132	32	35	13.40	16.08	(8+9)-IV-2	29
56	-1141	-585	2251	277	321	90	13.40	16.08	(8+9)-IV-3	14
57	-952	282	1673	280	195	106	13.40	16.08	(8+9)-IV-3	13
58	2853	346	862	-157	132	19	13.40	16.08	(8+9)-IV-2	27
59	-549	1354	977	196	46	86	13.40	16.08	(8+9)-IV-3	18
Massimi/minimi										
1							13.40			
1								16.08		
9										6.6

Muro : 7 - Nodi: [106-114-214-206], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri, Materiale=C30/37: **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-173	-2211	-9770	162	1304	53	13.40	16.08	(8+9)-VIII-1	6.1
2	320	-1832	-10500	98	797	58	13.40	16.08	(8+9)-VIII-1	9.6
3	-650	-6935	-9632	59	449	46	13.40	16.08	(8+9)-VIII-1	18
4	97	348	942	-18	-111	-57	13.40	16.08	2	47
5	-432	-1637	-6181	78	625	-24	13.40	16.08	(8+9)-VII-1	13
6	-460	501	-6704	42	366	1	13.40	16.08	(8+9)-VII-1	22
7	-602	-1403	-6829	23	199	-19	13.40	16.08	(8+9)-VII-1	38
8	-206	-1396	-1693	-10	-94	26	13.40	16.08	2	68
9	-267	-2170	-1583	82	657	-29	13.40	16.08	(8+9)-IV-2	12
10	-178	-1625	-1712	42	305	2	13.40	16.08	(8+9)-IV-2	27
11	-170	-1924	-3347	-13	-107	7	13.40	16.08	2	73
12	-301	-2206	-3104	-2	-50	-16	13.40	16.08	2	>100
13	-289	-2339	-2051	91	697	2	13.40	16.08	(8+9)-IV-2	12
14	-194	-1835	-2132	14	114	-10	13.40	16.08	(8+9)-IV-2	67
15	-201	-1345	-3460	-11	-59	10	13.40	16.08	2	>100
16	-177	-1388	-3385	-7	-54	11	13.40	16.08	2	>100
Massimi/minimi										
1							13.40			
1								16.08		
1										6.1

Muro : 8 - Nodi: [114-112-212-214], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri, Materiale=C30/37: **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-189	-2274	-1569	81	658	-11	13.40	16.08	(8+9)-IV-2	12
2	-190	-1311	-2673	35	-107	66	13.40	16.08	2	47
3	-200	-1002	-2676	53	-134	-19	13.40	16.08	2	53
4	-157	-833	-2685	43	-78	-83	13.40	16.08	2	50
5	-265	-2219	-3779	83	645	2	13.40	16.08	(8+9)-IV-2	13
6	-210	-1547	-2179	-92	-289	53	13.40	16.08	2	24
7	-156	-1205	-2189	-92	-354	15	13.40	16.08	2	22
8	-138	-864	-2177	-27	-132	-38	13.40	16.08	2	48
9	-205	-2329	-3548	73	606	3	13.40	16.08	(8+9)-IV-2	14
10	-136	-1661	-1875	-116	-287	-11	13.40	16.08	2	28
11	-139	-1276	-1880	-141	-320	47	13.40	16.08	2	22
12	-113	-936	-1847	-76	-90	82	13.40	16.08	2	43
13	-339	-2215	-3417	56	470	2	13.40	16.08	(8+9)-IV-2	18
14	-220	-1588	-1936	50	-97	-67	13.40	16.08	1	50
15	-124	-1183	-1552	52	-83	66	13.40	16.08	2	55
16	-58	-860	-1510	13	-21	74	13.40	16.08	2	78
Massimi/minimi										
1							13.40			
1								16.08		
1										12

Muro : 9 - Nodi: [112-213-313-212], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri, Materiale=C30/37: **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-134	-1876	-2361	70	379	56	13.40	16.08	(8+9)-IV-4	19
2	-187	-1535	-1269	92	-109	88	13.40	16.08	2	38
3	-151	-1023	-1258	107	-94	-55	13.40	16.08	2	42
4	-104	-475	-1253	46	-39	-103	13.40	16.08	2	46
5	-253	-2020	-1295	26	457	61	13.40	16.08	1	16
6	-193	-1602	-1042	-144	-305	45	13.40	16.08	2	23
7	-120	-1072	-1072	-163	-350	-23	13.40	16.08	2	22
8	-75	-534	-1077	-66	-113	-82	13.40	16.08	2	41
9	-86	-2205	938	46	479	-42	13.40	16.08	(8+9)-IV-3	16
10	-120	-1663	-957	-143	-304	-44	13.40	16.08	2	24
11	-112	-1103	-957	-161	-349	24	13.40	16.08	2	22
12	-55	-585	-929	-65	-113	82	13.40	16.08	2	41
13	774	-2724	-122	68	398	-29	13.40	16.08	(8+9)-IV-3	20
14	-378	-1231	-840	91	-111	-91	13.40	16.08	2	38
15	-161	-940	-763	105	-100	54	13.40	16.08	2	43
16	-77	-522	-739	46	-38	103	13.40	16.08	2	46
Massimi/minimi										
1							13.40			
1								16.08		
9										16

Muro : 10 - Nodi: [213-113-213-313], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri, Materiale=C30/37: **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	1837	916	3057	17	324	-18	13.40	16.08	(8+9)-IV-3	23
2	-1217	-956	1051	-5	-68	43	13.40	16.08	(8+9)-IV-3	73
3	-21	-988	-493	63	3	-17	13.40	16.08	2	85
4	-213	-354	1022	19	4	-19	13.40	16.08	(8+9)-VI-3	>100
5	1499	-2750	1885	66	390	-16	13.40	16.08	(8+9)-IV-3	21
6	-575	-1013	1610	-19	-85	29	13.40	16.08	(8+9)-IV-3	71
7	-99	-1038	-422	-66	-23	-9	13.40	16.08	2	91
8	-118	-475	-532	-24	0	-13	13.40	16.08	1	>100
9	462	-3145	1153	80	433	0	13.40	16.08	(8+9)-IV-3	19
10	62	-1693	1415	-13	-95	-19	13.40	16.08	(8+9)-IV-3	72
11	-66	-1061	-342	-65	-20	8	13.40	16.08	2	93
12	-57	-515	-460	-23	1	15	13.40	16.08	1	>100
13	198	-2907	866	34	437	-8	13.40	16.08	(8+9)-IV-3	19
14	144	-1927	1080	-6	-96	-51	13.40	16.08	(8+9)-IV-3	56
15	-44	-1111	-314	66	20	20	13.40	16.08	2	80
16	-11	-549	-351	23	-4	23	13.40	16.08	2	>100
Massimi/minimi										
1							13.40			
1								16.08		
13										19

Muro : 11 - Nodi: [113-134-234-213], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri, Materiale=C30/37: **Verificato**

Armatura a maglia doppia

Pannello	Nx	Ny	Nxy	Mx	My	Mxy	Ax	Ay	C	Cs
	kg	kg	kg	kg*m	kg*m	kg*m	cmq	cmq		
1	-264	-2211	581	73	476	35	13.40	16.08	(8+9)-IV-3	16
2	-201	-1681	-288	46	-134	94	13.40	16.08	2	36
3	-132	-1102	-267	56	-132	-43	13.40	16.08	2	47
4	-65	-565	-268	25	-57	-90	13.40	16.08	2	55
5	-263	-2126	-88	52	581	37	13.40	16.08	1	13
6	-202	-1620	-80	-102	-307	33	13.40	16.08	2	24
7	-162	-1062	-71	-125	-416	-14	13.40	16.08	2	19
8	-84	-541	-65	-52	-155	-62	13.40	16.08	2	37
9	-317	-1988	56	54	605	-50	13.40	16.08	1	13
10	-284	-1566	143	-102	-299	-28	13.40	16.08	2	25
11	-202	-1045	173	-122	-418	19	13.40	16.08	2	19
12	-91	-540	177	-51	-158	59	13.40	16.08	2	37
13	-833	-2865	2726	133	912	-76	13.40	16.08	(8+9)-V-3	8.5
14	-149	-2142	398	37	-150	-110	13.40	16.08	1	32
15	-85	-1401	244	55	-130	38	13.40	16.08	2	49
16	-44	-684	193	24	-64	130	13.40	16.08	2	42
Massimi/minimi										
1							13.40			
1								16.08		
13										8.5

Verifica delle Pareti XLAM SLV

Scenario di calcolo: **Set_NT_SLV_SLD_A2_STR/GEO_2018**

Parete Xlam 12 - Nodi: [5-6-104-105] - **Crit.Prog.** Criterio di verifica XLAM 0 - **Verificato:**
[Cs=3.771,Comb=(8+9)-IV-3]

Geometria setti

Setto	Crit.	X	L	S	X90	L90	S90
		mm	cm	cm	mm	cm	cm
1	Criterio di verifica XLAM 0	0	387.0	12.1	0	570.8	12.1
		2854	387.0	12.1	1935	570.8	12.1
		5708	387.0	12.1	3870	570.8	12.1

Setto 1: origine (366.0,1315.0,193.5), direzione (-0.610709,0.791855,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	1	-1104	36	865	-0.39	0.49	0.48	79.20	115.20	115.20	>100
0	2	-2189	69	1768	-0.78	0.92	0.98	118.80	172.80	172.80	91
0	3	-2189	69	1768	-0.78	0.92	0.98	118.80	172.80	172.80	91
0	4	-1104	36	865	-0.39	0.49	0.48	105.60	153.60	153.60	>100
0	5	-1104	36	865	-0.39	0.49	0.48	105.60	153.60	153.60	>100
0	6	-1104	36	865	-0.39	0.49	0.48	105.60	153.60	153.60	>100
0	7	-1104	36	865	-0.39	0.49	0.48	105.60	153.60	153.60	>100
0	(8+9)-VIII-4	-375	-68	-9756	-0.13	-0.90	-5.38	132.00	192.00	192.00	31
0	(8+9)-IV-1	-1132	115	11033	-0.40	1.53	6.09	132.00	192.00	192.00	25
0	(8+9)-V-1	-666	113	-6208	-0.24	1.51	-3.43	132.00	192.00	192.00	39
0	(8+9)-I-2	-374	57	-13221	-0.13	0.76	-7.30	132.00	192.00	192.00	24
0	(8+9)-V-2	-445	69	-13538	-0.16	0.92	-7.47	132.00	192.00	192.00	23
0	(8+9)-I-4	-933	-50	7073	-0.33	-0.66	3.90	132.00	192.00	192.00	42
0	(8+9)-V-3	-1083	-18	14720	-0.39	-0.24	8.12	132.00	192.00	192.00	23
0	(8+9)-II-2	-311	-32	-14669	-0.11	-0.42	-8.09	132.00	192.00	192.00	23
0	(8+9)-V-4	-862	-62	7391	-0.31	-0.83	4.08	132.00	192.00	192.00	39
0	(8+9)-II-4	-479	-63	-8581	-0.17	-0.85	-4.73	132.00	192.00	192.00	34
0	(8+9)-VI-1	-1070	118	9668	-0.38	1.58	5.33	132.00	192.00	192.00	28
0	(8+9)-III-2	-349	56	-13602	-0.12	0.75	-7.51	132.00	192.00	192.00	23

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-VI-2	-333	-28	-14764	-0.12	-0.37	-8.15	132.00	192.00	192.00	23
0	(8+9)-III-4	-908	-50	6692	-0.32	-0.66	3.69	132.00	192.00	192.00	44
0	(8+9)-VI-3	-1195	79	15946	-0.43	1.05	8.80	132.00	192.00	192.00	19
0	(8+9)-IV-2	-228	-32	-15939	-0.08	-0.43	-8.80	132.00	192.00	192.00	21
0	(8+9)-VI-4	-458	-67	-8486	-0.16	-0.90	-4.68	132.00	192.00	192.00	34
0	(8+9)-IV-4	-396	-64	-9851	-0.14	-0.85	-5.44	132.00	192.00	192.00	31
0	(8+9)-VII-1	-691	113	-5827	-0.25	1.51	-3.22	132.00	192.00	192.00	41
0	(8+9)-II-1	-1049	114	9763	-0.37	1.53	5.39	132.00	192.00	192.00	28
0	(8+9)-VII-2	-420	69	-13919	-0.15	0.92	-7.68	132.00	192.00	192.00	22
0	(8+9)-III-1	-620	100	-5510	-0.22	1.34	-3.04	132.00	192.00	192.00	44
0	(8+9)-VII-3	-1108	-18	15101	-0.39	-0.24	8.33	132.00	192.00	192.00	22
0	(8+9)-I-1	-595	100	-5891	-0.21	1.34	-3.25	132.00	192.00	192.00	42
0	(8+9)-VII-4	-837	-62	7010	-0.30	-0.83	3.87	132.00	192.00	192.00	41
0	(8+9)-III-3	-1179	-6	14784	-0.42	-0.08	8.16	132.00	192.00	192.00	23
0	(8+9)-IV-3	-1299	83	17121	-0.46	1.11	9.45	132.00	192.00	192.00	18
0	(8+9)-II-3	-1216	82	15851	-0.43	1.10	8.75	132.00	192.00	192.00	19
0	(8+9)-VIII-1	-1153	118	10938	-0.41	1.58	6.04	132.00	192.00	192.00	25
0	(8+9)-VIII-2	-250	-28	-16034	-0.09	-0.38	-8.85	132.00	192.00	192.00	21
0	(8+9)-VIII-3	-1278	79	17216	-0.45	1.06	9.50	132.00	192.00	192.00	18
0	(8+9)-I-3	-1154	-6	14403	-0.41	-0.08	7.95	132.00	192.00	192.00	24
Verifiche nella direzione secondaria											
0	1	-6648	-18	-271	-2.41	-0.38	-0.10	79.20	115.20	115.20	>100
0	2	-12998	-22	295	-4.70	-0.45	0.11	118.80	172.80	172.80	>100
0	3	-12998	-22	295	-4.70	-0.45	0.11	118.80	172.80	172.80	>100
0	4	-6648	-18	-271	-2.41	-0.38	-0.10	105.60	153.60	153.60	>100
0	5	-6648	-18	-271	-2.41	-0.38	-0.10	105.60	153.60	153.60	>100
0	6	-6648	-18	-271	-2.41	-0.38	-0.10	105.60	153.60	153.60	>100
0	7	-6648	-18	-271	-2.41	-0.38	-0.10	105.60	153.60	153.60	>100
0	(8+9)-VIII-4	-6438	83	15381	-2.33	1.72	5.85	132.00	192.00	192.00	25
0	(8+9)-IV-2	-1445	-21	15995	-0.52	-0.43	6.09	132.00	192.00	192.00	29
0	(8+9)-V-1	4344	-289	-3042	1.57	-5.99	-1.16	132.00	192.00	192.00	20
0	(8+9)-I-2	3007	-84	4594	1.09	-1.73	1.75	132.00	192.00	192.00	38
0	(8+9)-V-2	5441	-244	6121	1.97	-5.05	2.33	132.00	192.00	192.00	19
0	(8+9)-I-4	-11202	101	4073	-4.05	2.10	1.55	132.00	192.00	192.00	51
0	(8+9)-V-3	-14733	216	-6618	-5.33	4.47	-2.52	132.00	192.00	192.00	27
0	(8+9)-II-2	-686	34	15103	-0.25	0.70	5.75	132.00	192.00	192.00	30
0	(8+9)-V-4	-13636	261	2546	-4.94	5.41	0.97	132.00	192.00	192.00	30
0	(8+9)-II-4	-4949	89	14946	-1.79	1.85	5.69	132.00	192.00	192.00	25
0	(8+9)-VI-1	-3613	-165	-14985	-1.31	-3.42	-5.70	132.00	192.00	192.00	21
0	(8+9)-III-2	2780	-100	4862	1.01	-2.07	1.85	132.00	192.00	192.00	36
0	(8+9)-VI-2	44	-14	15561	0.02	-0.29	5.92	132.00	192.00	192.00	31
0	(8+9)-III-4	-11430	85	4341	-4.14	1.76	1.65	132.00	192.00	192.00	55
0	(8+9)-VI-3	-9336	-14	-16057	-3.38	-0.28	-6.11	132.00	192.00	192.00	30
0	(8+9)-I-1	1910	-129	-4570	0.69	-2.67	-1.74	132.00	192.00	192.00	35
0	(8+9)-VI-4	-5679	137	14488	-2.06	2.84	5.51	132.00	192.00	192.00	23
0	(8+9)-IV-4	-5708	35	15839	-2.07	0.72	6.03	132.00	192.00	192.00	28
0	(8+9)-VII-1	4571	-273	-3310	1.65	-5.65	-1.26	132.00	192.00	192.00	21
0	(8+9)-II-1	-4343	-117	-15443	-1.57	-2.42	-5.88	132.00	192.00	192.00	23
0	(8+9)-VII-2	5213	-260	6389	1.89	-5.39	2.43	132.00	192.00	192.00	18
0	(8+9)-III-1	2138	-113	-4838	0.77	-2.33	-1.84	132.00	192.00	192.00	36
0	(8+9)-VII-3	-14505	232	-6886	-5.25	4.81	-2.62	132.00	192.00	192.00	25
0	(8+9)-IV-1	-3585	-63	-16336	-1.30	-1.30	-6.22	132.00	192.00	192.00	26
0	(8+9)-VII-4	-13863	245	2814	-5.02	5.07	1.07	132.00	192.00	192.00	31
0	(8+9)-III-3	-12072	72	-5358	-4.37	1.50	-2.04	132.00	192.00	192.00	53
0	(8+9)-IV-3	-7847	-7	-16492	-2.84	-0.15	-6.27	132.00	192.00	192.00	30
0	(8+9)-II-3	-8606	-62	-15599	-3.12	-1.28	-5.94	132.00	192.00	192.00	26
0	(8+9)-VIII-1	-2854	-111	-15877	-1.03	-2.29	-6.04	132.00	192.00	192.00	23
0	(8+9)-VIII-2	-715	-69	16453	-0.26	-1.42	6.26	132.00	192.00	192.00	25
0	(8+9)-VIII-3	-8577	41	-16950	-3.10	0.85	-6.45	132.00	192.00	192.00	26
0	(8+9)-I-3	-12299	56	-5090	-4.45	1.16	-1.94	132.00	192.00	192.00	60

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
0	1	-15	0.00	3.84	Si	>100
0	4	-15	0.00	5.12	Si	>100
0	5	-15	0.00	5.12	Si	>100
0	6	-15	0.00	5.12	Si	>100
0	7	-15	0.00	5.12	Si	>100
0	(8+9)-II-4	-46	0.01	6.40	Si	>100
0	(8+9)-IV-2	-20	0.01	6.40	Si	>100
5708	2	24	0.01	5.76	Si	>100
5708	3	24	0.01	5.76	Si	>100
5708	(8+9)-VIII-4	-421	0.11	6.40	Si	59
5708	(8+9)-IV-1	48	0.01	6.40	Si	>100
5708	(8+9)-V-2	1404	0.36	6.40	Si	18
5708	(8+9)-I-4	-41	0.01	6.40	Si	>100
5708	(8+9)-V-3	-1384	0.36	6.40	Si	18
5708	(8+9)-II-2	85	0.02	6.40	Si	>100
5708	(8+9)-V-4	-1351	0.35	6.40	Si	18
5708	(8+9)-I-3	-73	0.02	6.40	Si	>100
5708	(8+9)-VI-1	368	0.10	6.40	Si	67
5708	(8+9)-III-2	71	0.02	6.40	Si	>100
5708	(8+9)-VI-2	478	0.12	6.40	Si	52
5708	(8+9)-III-4	-62	0.02	6.40	Si	>100
5708	(8+9)-VI-3	-458	0.12	6.40	Si	54
5708	(8+9)-I-1	60	0.02	6.40	Si	>100
5708	(8+9)-VI-4	-349	0.09	6.40	Si	71
5708	(8+9)-IV-4	-28	0.01	6.40	Si	>100
5708	(8+9)-VII-1	1393	0.36	6.40	Si	18
5708	(8+9)-II-1	-25	0.01	6.40	Si	>100
5708	(8+9)-VII-2	1382	0.36	6.40	Si	18
5708	(8+9)-III-1	82	0.02	6.40	Si	>100
5708	(8+9)-VII-3	-1362	0.35	6.40	Si	18
5708	(8+9)-I-2	93	0.02	6.40	Si	>100
5708	(8+9)-VII-4	-1373	0.36	6.40	Si	18
5708	(8+9)-III-3	-52	0.01	6.40	Si	>100
5708	(8+9)-IV-3	8	0.00	6.40	Si	>100
5708	(8+9)-II-3	-65	0.02	6.40	Si	>100
5708	(8+9)-VIII-1	441	0.11	6.40	Si	56
5708	(8+9)-VIII-2	405	0.10	6.40	Si	61
5708	(8+9)-VIII-3	-385	0.10	6.40	Si	64
5708	(8+9)-V-1	1371	0.35	6.40	Si	18
Verifiche nella direzione secondaria						
0	1	23	0.01	3.84	Si	>100
0	2	23	0.01	5.76	Si	>100
0	3	23	0.01	5.76	Si	>100
0	4	23	0.01	5.12	Si	>100
0	5	23	0.01	5.12	Si	>100
0	6	23	0.01	5.12	Si	>100
0	7	23	0.01	5.12	Si	>100
0	(8+9)-III-4	-81	0.03	6.40	Si	>100
0	(8+9)-I-4	-66	0.02	6.40	Si	>100
0	(8+9)-II-3	-81	0.03	6.40	Si	>100
0	(8+9)-I-2	142	0.05	6.40	Si	>100
0	(8+9)-I-1	101	0.03	6.40	Si	>100
0	(8+9)-II-2	116	0.04	6.40	Si	>100
0	(8+9)-I-3	-106	0.04	6.40	Si	>100
0	(8+9)-VI-2	113	0.04	6.40	Si	>100
0	(8+9)-III-1	116	0.04	6.40	Si	>100
0	(8+9)-III-2	127	0.04	6.40	Si	>100
0	(8+9)-III-3	-92	0.03	6.40	Si	>100
1935	(8+9)-VIII-4	-248	0.08	6.40	Si	77
1935	(8+9)-IV-2	-118	0.04	6.40	Si	>100
1935	(8+9)-VI-3	-84	0.03	6.40	Si	>100
1935	(8+9)-IV-1	89	0.03	6.40	Si	>100
1935	(8+9)-VI-4	-206	0.07	6.40	Si	93

X	Comb.	Ty	τ_d	fvd	RS	Cs
1935	(8+9)-IV-3	110	0.04	6.40	Si	>100
1935	(8+9)-VII-1	495	0.17	6.40	Si	39
1935	(8+9)-V-1	482	0.16	6.40	Si	40
1935	(8+9)-VII-2	433	0.14	6.40	Si	44
1935	(8+9)-V-3	-454	0.15	6.40	Si	42
1935	(8+9)-VII-3	-441	0.15	6.40	Si	43
1935	(8+9)-VI-1	197	0.07	6.40	Si	97
1935	(8+9)-VII-4	-503	0.17	6.40	Si	38
1935	(8+9)-V-2	445	0.15	6.40	Si	43
1935	(8+9)-V-4	-490	0.16	6.40	Si	39
1935	(8+9)-II-1	47	0.02	6.40	Si	>100
1935	(8+9)-IV-4	-98	0.03	6.40	Si	>100
1935	(8+9)-VIII-1	240	0.08	6.40	Si	80
1935	(8+9)-II-4	-55	0.02	6.40	Si	>100
3870	(8+9)-VIII-2	85	0.03	6.40	Si	>100
3870	(8+9)-VIII-3	-92	0.03	6.40	Si	>100

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	2	1643	0.88	28.80	33	0.21	18.00	85	V	33
0	3	1643	0.88	28.80	33	0.21	18.00	85	V	33
0	(8+9)-V-1	-5355	-2.86	32.00	11	-0.69	20.00	29	V	11
0	(8+9)-V-4	6369	3.40	32.00	9.4	0.82	20.00	24	V	9.4
0	(8+9)-VII-4	5759	3.07	32.00	10	0.74	20.00	27	V	10
0	(8+9)-VII-1	-4746	-2.53	32.00	13	-0.61	20.00	33	V	13
0	(8+9)-I-1	-4374	-2.34	32.00	14	-0.57	20.00	35	V	14
2854	1	751	0.40	19.20	48	0.10	12.00	>100	V	48
2854	4	751	0.40	25.60	64	0.10	16.00	>100	V	64
2854	5	751	0.40	25.60	64	0.10	16.00	>100	V	64
2854	6	751	0.40	25.60	64	0.10	16.00	>100	V	64
2854	7	751	0.40	25.60	64	0.10	16.00	>100	V	64
2854	(8+9)-VII-3	11709	6.25	32.00	5.1	1.51	20.00	13	V	5.1
2854	(8+9)-III-3	11438	6.11	32.00	5.2	1.48	20.00	14	V	5.2
2854	(8+9)-II-1	7670	4.10	32.00	7.8	0.99	20.00	20	V	7.8
2854	(8+9)-II-3	12291	6.56	32.00	4.9	1.59	20.00	13	V	4.9
2854	(8+9)-V-2	-10284	-5.49	32.00	5.8	-1.33	20.00	15	V	5.8
2854	(8+9)-III-1	-3964	-2.12	32.00	15	-0.51	20.00	39	V	15
2854	(8+9)-V-3	11334	6.05	32.00	5.3	1.46	20.00	14	V	5.3
2854	(8+9)-II-2	-11241	-6.00	32.00	5.3	-1.45	20.00	14	V	5.3
2854	(8+9)-I-4	5390	2.88	32.00	11	0.70	20.00	29	V	11
2854	(8+9)-VI-1	7589	4.05	32.00	7.9	0.98	20.00	20	V	7.9
2854	(8+9)-IV-3	13542	7.23	32.00	4.4	1.75	20.00	11	V	4.4
2854	(8+9)-VI-2	-11322	-6.04	32.00	5.3	-1.46	20.00	14	V	5.3
2854	(8+9)-II-4	-6620	-3.53	32.00	9.1	-0.86	20.00	23	V	9.1
2854	(8+9)-VI-3	12372	6.61	32.00	4.8	1.60	20.00	13	V	4.8
2854	(8+9)-III-4	5015	2.68	32.00	12	0.65	20.00	31	V	12
2854	(8+9)-VIII-2	-12573	-6.71	32.00	4.8	-1.62	20.00	12	V	4.8
2854	(8+9)-III-2	-10388	-5.55	32.00	5.8	-1.34	20.00	15	V	5.8
2854	(8+9)-VIII-3	13623	7.27	32.00	4.4	1.76	20.00	11	V	4.4
2854	(8+9)-I-3	11063	5.91	32.00	5.4	1.43	20.00	14	V	5.4
2854	(8+9)-I-2	-10013	-5.35	32.00	6.0	-1.29	20.00	15	V	6.0
2854	(8+9)-VII-2	-10659	-5.69	32.00	5.6	-1.38	20.00	15	V	5.6
5708	(8+9)-VIII-4	-12235	-6.53	32.00	4.9	-1.58	20.00	13	V	4.9
5708	(8+9)-VI-4	-8170	-4.36	32.00	7.3	-1.06	20.00	19	V	7.3
5708	(8+9)-VIII-1	11638	6.21	32.00	5.2	1.50	20.00	13	V	5.2
5708	(8+9)-IV-4	-10614	-5.67	32.00	5.6	-1.37	20.00	15	V	5.6
5708	(8+9)-IV-2	-13675	-7.30	32.00	4.4	-1.77	20.00	11	V	4.4
5708	(8+9)-IV-1	10016	5.35	32.00	6.0	1.29	20.00	15	V	6.0
Verifiche nella direzione secondaria										
0	1	-714	-0.26	19.20	74	-0.06	12.00	>100	V	74
0	2	-1404	-0.51	28.80	57	-0.12	18.00	>100	V	57
0	3	-1404	-0.51	28.80	57	-0.12	18.00	>100	V	57

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
0	4	-714	-0.26	25.60	99	-0.06	16.00	>100	V	99
0	5	-714	-0.26	25.60	99	-0.06	16.00	>100	V	99
0	6	-714	-0.26	25.60	99	-0.06	16.00	>100	V	99
0	7	-714	-0.26	25.60	99	-0.06	16.00	>100	V	99
1935	(8+9)-VIII-4	14874	5.38	32.00	5.9	1.30	20.00	15	V	5.9
1935	(8+9)-IV-2	22664	8.20	32.00	3.9	1.99	20.00	10	V	3.9
1935	(8+9)-V-1	7096	2.57	32.00	12	0.62	20.00	32	V	12
1935	(8+9)-I-2	18087	6.55	32.00	4.9	1.58	20.00	13	V	4.9
1935	(8+9)-V-2	17172	6.22	32.00	5.1	1.50	20.00	13	V	5.1
1935	(8+9)-I-4	-8793	-3.18	32.00	10	-0.77	20.00	26	V	10
1935	(8+9)-V-3	-17954	-6.50	32.00	4.9	-1.57	20.00	13	V	4.9
1935	(8+9)-II-2	20434	7.40	32.00	4.3	1.79	20.00	11	V	4.3
1935	(8+9)-V-4	-7878	-2.85	32.00	11	-0.69	20.00	29	V	11
1935	(8+9)-II-4	12370	4.48	32.00	7.1	1.08	20.00	18	V	7.1
1935	(8+9)-VI-1	-13427	-4.86	32.00	6.6	-1.18	20.00	17	V	6.6
1935	(8+9)-III-2	18756	6.79	32.00	4.7	1.64	20.00	12	V	4.7
1935	(8+9)-VI-2	20159	7.30	32.00	4.4	1.77	20.00	11	V	4.4
1935	(8+9)-III-4	-8124	-2.94	32.00	11	-0.71	20.00	28	V	11
1935	(8+9)-VI-3	-20942	-7.58	32.00	4.2	-1.83	20.00	11	V	4.2
1935	(8+9)-I-1	8011	2.90	32.00	11	0.70	20.00	29	V	11
1935	(8+9)-VI-4	12644	4.58	32.00	7.0	1.11	20.00	18	V	7.0
1935	(8+9)-IV-4	14600	5.28	32.00	6.1	1.28	20.00	16	V	6.1
1935	(8+9)-VII-1	6427	2.33	32.00	14	0.56	20.00	36	V	14
1935	(8+9)-II-1	-13152	-4.76	32.00	6.7	-1.15	20.00	17	V	6.7
1935	(8+9)-VII-2	17841	6.46	32.00	5.0	1.56	20.00	13	V	5.0
1935	(8+9)-III-1	7342	2.66	32.00	12	0.64	20.00	31	V	12
1935	(8+9)-VII-3	-18623	-6.74	32.00	4.7	-1.63	20.00	12	V	4.7
1935	(8+9)-IV-1	-15382	-5.57	32.00	5.7	-1.35	20.00	15	V	5.7
1935	(8+9)-VII-4	-7209	-2.61	32.00	12	-0.63	20.00	32	V	12
1935	(8+9)-III-3	-19538	-7.07	32.00	4.5	-1.71	20.00	12	V	4.5
1935	(8+9)-IV-3	-23446	-8.49	32.00	3.8	-2.05	20.00	9.7	V	3.8
1935	(8+9)-II-3	-21216	-7.68	32.00	4.2	-1.86	20.00	11	V	4.2
1935	(8+9)-VIII-1	-15657	-5.67	32.00	5.6	-1.37	20.00	15	V	5.6
1935	(8+9)-VIII-2	22389	8.10	32.00	3.9	1.96	20.00	10	V	3.9
1935	(8+9)-VIII-3	-23172	-8.39	32.00	3.8	-2.03	20.00	9.9	V	3.8
1935	(8+9)-I-3	-18869	-6.83	32.00	4.7	-1.65	20.00	12	V	4.7

Verifiche a instabilità

Setto(X)	Comb.	krit _c	krit _m	$\lambda_{rel,c}$	$\lambda_{rel,m}$	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
(cm)						kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	
1(0.0)	(8+9)-IV-3	0.22	--	2.07	--	-0.46	1.11	9.45	132.00	192.00	192.00	15

Parete Xlam 12 - Nodi: [5-6-104-105] - **Crit.Prog.** Criterio di verifica XLAM 0 - **Verificato:**
[Cs=3.771,Comb=(8+9)-IV-3]

Geometria setti

Setto	Crit.	X	L	S	X90	L90	S90
		mm	cm	cm	mm	cm	cm
1	Criterio di verifica XLAM 0	0	387.0	12.1	0	570.8	12.1
		2854	387.0	12.1	1935	570.8	12.1
		5708	387.0	12.1	3870	570.8	12.1

Setto 1: origine (366.0,1315.0,193.5), direzione (-0.610709,0.791855,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	
0	1	-1104	36	865	-0.39	0.49	0.48	79.20	115.20	115.20	>100
0	2	-2189	69	1768	-0.78	0.92	0.98	118.80	172.80	172.80	91
0	3	-2189	69	1768	-0.78	0.92	0.98	118.80	172.80	172.80	91
0	4	-1104	36	865	-0.39	0.49	0.48	105.60	153.60	153.60	>100

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	5	-1104	36	865	-0.39	0.49	0.48	105.60	153.60	153.60	>100
0	6	-1104	36	865	-0.39	0.49	0.48	105.60	153.60	153.60	>100
0	7	-1104	36	865	-0.39	0.49	0.48	105.60	153.60	153.60	>100
0	(8+9)-VIII-4	-375	-68	-9756	-0.13	-0.90	-5.38	132.00	192.00	192.00	31
0	(8+9)-IV-1	-1132	115	11033	-0.40	1.53	6.09	132.00	192.00	192.00	25
0	(8+9)-V-1	-666	113	-6208	-0.24	1.51	-3.43	132.00	192.00	192.00	39
0	(8+9)-I-2	-374	57	-13221	-0.13	0.76	-7.30	132.00	192.00	192.00	24
0	(8+9)-V-2	-445	69	-13538	-0.16	0.92	-7.47	132.00	192.00	192.00	23
0	(8+9)-I-4	-933	-50	7073	-0.33	-0.66	3.90	132.00	192.00	192.00	42
0	(8+9)-V-3	-1083	-18	14720	-0.39	-0.24	8.12	132.00	192.00	192.00	23
0	(8+9)-II-2	-311	-32	-14669	-0.11	-0.42	-8.09	132.00	192.00	192.00	23
0	(8+9)-V-4	-862	-62	7391	-0.31	-0.83	4.08	132.00	192.00	192.00	39
0	(8+9)-II-4	-479	-63	-8581	-0.17	-0.85	-4.73	132.00	192.00	192.00	34
0	(8+9)-VI-1	-1070	118	9668	-0.38	1.58	5.33	132.00	192.00	192.00	28
0	(8+9)-III-2	-349	56	-13602	-0.12	0.75	-7.51	132.00	192.00	192.00	23
0	(8+9)-VI-2	-333	-28	-14764	-0.12	-0.37	-8.15	132.00	192.00	192.00	23
0	(8+9)-III-4	-908	-50	6692	-0.32	-0.66	3.69	132.00	192.00	192.00	44
0	(8+9)-VI-3	-1195	79	15946	-0.43	1.05	8.80	132.00	192.00	192.00	19
0	(8+9)-IV-2	-228	-32	-15939	-0.08	-0.43	-8.80	132.00	192.00	192.00	21
0	(8+9)-VI-4	-458	-67	-8486	-0.16	-0.90	-4.68	132.00	192.00	192.00	34
0	(8+9)-IV-4	-396	-64	-9851	-0.14	-0.85	-5.44	132.00	192.00	192.00	31
0	(8+9)-VII-1	-691	113	-5827	-0.25	1.51	-3.22	132.00	192.00	192.00	41
0	(8+9)-II-1	-1049	114	9763	-0.37	1.53	5.39	132.00	192.00	192.00	28
0	(8+9)-VII-2	-420	69	-13919	-0.15	0.92	-7.68	132.00	192.00	192.00	22
0	(8+9)-III-1	-620	100	-5510	-0.22	1.34	-3.04	132.00	192.00	192.00	44
0	(8+9)-VII-3	-1108	-18	15101	-0.39	-0.24	8.33	132.00	192.00	192.00	22
0	(8+9)-I-1	-595	100	-5891	-0.21	1.34	-3.25	132.00	192.00	192.00	42
0	(8+9)-VII-4	-837	-62	7010	-0.30	-0.83	3.87	132.00	192.00	192.00	41
0	(8+9)-III-3	-1179	-6	14784	-0.42	-0.08	8.16	132.00	192.00	192.00	23
0	(8+9)-IV-3	-1299	83	17121	-0.46	1.11	9.45	132.00	192.00	192.00	18
0	(8+9)-II-3	-1216	82	15851	-0.43	1.10	8.75	132.00	192.00	192.00	19
0	(8+9)-VIII-1	-1153	118	10938	-0.41	1.58	6.04	132.00	192.00	192.00	25
0	(8+9)-VIII-2	-250	-28	-16034	-0.09	-0.38	-8.85	132.00	192.00	192.00	21
0	(8+9)-VIII-3	-1278	79	17216	-0.45	1.06	9.50	132.00	192.00	192.00	18
0	(8+9)-I-3	-1154	-6	14403	-0.41	-0.08	7.95	132.00	192.00	192.00	24
Verifiche nella direzione secondaria											
0	1	-6648	-18	-271	-2.41	-0.38	-0.10	79.20	115.20	115.20	>100
0	2	-12998	-22	295	-4.70	-0.45	0.11	118.80	172.80	172.80	>100
0	3	-12998	-22	295	-4.70	-0.45	0.11	118.80	172.80	172.80	>100
0	4	-6648	-18	-271	-2.41	-0.38	-0.10	105.60	153.60	153.60	>100
0	5	-6648	-18	-271	-2.41	-0.38	-0.10	105.60	153.60	153.60	>100
0	6	-6648	-18	-271	-2.41	-0.38	-0.10	105.60	153.60	153.60	>100
0	7	-6648	-18	-271	-2.41	-0.38	-0.10	105.60	153.60	153.60	>100
0	(8+9)-VIII-4	-6438	83	15381	-2.33	1.72	5.85	132.00	192.00	192.00	25
0	(8+9)-IV-2	-1445	-21	15995	-0.52	-0.43	6.09	132.00	192.00	192.00	29
0	(8+9)-V-1	4344	-289	-3042	1.57	-5.99	-1.16	132.00	192.00	192.00	20
0	(8+9)-I-2	3007	-84	4594	1.09	-1.73	1.75	132.00	192.00	192.00	38
0	(8+9)-V-2	5441	-244	6121	1.97	-5.05	2.33	132.00	192.00	192.00	19
0	(8+9)-I-4	-11202	101	4073	-4.05	2.10	1.55	132.00	192.00	192.00	51
0	(8+9)-V-3	-14733	216	-6618	-5.33	4.47	-2.52	132.00	192.00	192.00	27
0	(8+9)-II-2	-686	34	15103	-0.25	0.70	5.75	132.00	192.00	192.00	30
0	(8+9)-V-4	-13636	261	2546	-4.94	5.41	0.97	132.00	192.00	192.00	30
0	(8+9)-II-4	-4949	89	14946	-1.79	1.85	5.69	132.00	192.00	192.00	25
0	(8+9)-VI-1	-3613	-165	-14985	-1.31	-3.42	-5.70	132.00	192.00	192.00	21
0	(8+9)-III-2	2780	-100	4862	1.01	-2.07	1.85	132.00	192.00	192.00	36
0	(8+9)-VI-2	44	-14	15561	0.02	-0.29	5.92	132.00	192.00	192.00	31
0	(8+9)-III-4	-11430	85	4341	-4.14	1.76	1.65	132.00	192.00	192.00	55
0	(8+9)-VI-3	-9336	-14	-16057	-3.38	-0.28	-6.11	132.00	192.00	192.00	30
0	(8+9)-I-1	1910	-129	-4570	0.69	-2.67	-1.74	132.00	192.00	192.00	35
0	(8+9)-VI-4	-5679	137	14488	-2.06	2.84	5.51	132.00	192.00	192.00	23
0	(8+9)-IV-4	-5708	35	15839	-2.07	0.72	6.03	132.00	192.00	192.00	28
0	(8+9)-VII-1	4571	-273	-3310	1.65	-5.65	-1.26	132.00	192.00	192.00	21
0	(8+9)-II-1	-4343	-117	-15443	-1.57	-2.42	-5.88	132.00	192.00	192.00	23
0	(8+9)-VII-2	5213	-260	6389	1.89	-5.39	2.43	132.00	192.00	192.00	18

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-III-1	2138	-113	-4838	0.77	-2.33	-1.84	132.00	192.00	192.00	36
0	(8+9)-VII-3	-14505	232	-6886	-5.25	4.81	-2.62	132.00	192.00	192.00	25
0	(8+9)-IV-1	-3585	-63	-16336	-1.30	-1.30	-6.22	132.00	192.00	192.00	26
0	(8+9)-VII-4	-13863	245	2814	-5.02	5.07	1.07	132.00	192.00	192.00	31
0	(8+9)-III-3	-12072	72	-5358	-4.37	1.50	-2.04	132.00	192.00	192.00	53
0	(8+9)-IV-3	-7847	-7	-16492	-2.84	-0.15	-6.27	132.00	192.00	192.00	30
0	(8+9)-II-3	-8606	-62	-15599	-3.12	-1.28	-5.94	132.00	192.00	192.00	26
0	(8+9)-VIII-1	-2854	-111	-15877	-1.03	-2.29	-6.04	132.00	192.00	192.00	23
0	(8+9)-VIII-2	-715	-69	16453	-0.26	-1.42	6.26	132.00	192.00	192.00	25
0	(8+9)-VIII-3	-8577	41	-16950	-3.10	0.85	-6.45	132.00	192.00	192.00	26
0	(8+9)-I-3	-12299	56	-5090	-4.45	1.16	-1.94	132.00	192.00	192.00	60

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Ty kg	τ_d kg/cmq	fvd kg/cmq	RS	Cs
0	1	-15	0.00	3.84	Si	>100
0	4	-15	0.00	5.12	Si	>100
0	5	-15	0.00	5.12	Si	>100
0	6	-15	0.00	5.12	Si	>100
0	7	-15	0.00	5.12	Si	>100
0	(8+9)-II-4	-46	0.01	6.40	Si	>100
0	(8+9)-IV-2	-20	0.01	6.40	Si	>100
5708	2	24	0.01	5.76	Si	>100
5708	3	24	0.01	5.76	Si	>100
5708	(8+9)-VIII-4	-421	0.11	6.40	Si	59
5708	(8+9)-IV-1	48	0.01	6.40	Si	>100
5708	(8+9)-V-2	1404	0.36	6.40	Si	18
5708	(8+9)-I-4	-41	0.01	6.40	Si	>100
5708	(8+9)-V-3	-1384	0.36	6.40	Si	18
5708	(8+9)-II-2	85	0.02	6.40	Si	>100
5708	(8+9)-V-4	-1351	0.35	6.40	Si	18
5708	(8+9)-I-3	-73	0.02	6.40	Si	>100
5708	(8+9)-VI-1	368	0.10	6.40	Si	67
5708	(8+9)-III-2	71	0.02	6.40	Si	>100
5708	(8+9)-VI-2	478	0.12	6.40	Si	52
5708	(8+9)-III-4	-62	0.02	6.40	Si	>100
5708	(8+9)-VI-3	-458	0.12	6.40	Si	54
5708	(8+9)-I-1	60	0.02	6.40	Si	>100
5708	(8+9)-VI-4	-349	0.09	6.40	Si	71
5708	(8+9)-IV-4	-28	0.01	6.40	Si	>100
5708	(8+9)-VII-1	1393	0.36	6.40	Si	18
5708	(8+9)-II-1	-25	0.01	6.40	Si	>100
5708	(8+9)-VII-2	1382	0.36	6.40	Si	18
5708	(8+9)-III-1	82	0.02	6.40	Si	>100
5708	(8+9)-VII-3	-1362	0.35	6.40	Si	18
5708	(8+9)-I-2	93	0.02	6.40	Si	>100
5708	(8+9)-VII-4	-1373	0.36	6.40	Si	18
5708	(8+9)-III-3	-52	0.01	6.40	Si	>100
5708	(8+9)-IV-3	8	0.00	6.40	Si	>100
5708	(8+9)-II-3	-65	0.02	6.40	Si	>100
5708	(8+9)-VIII-1	441	0.11	6.40	Si	56
5708	(8+9)-VIII-2	405	0.10	6.40	Si	61
5708	(8+9)-VIII-3	-385	0.10	6.40	Si	64
5708	(8+9)-V-1	1371	0.35	6.40	Si	18
Verifiche nella direzione secondaria						
0	1	23	0.01	3.84	Si	>100
0	2	23	0.01	5.76	Si	>100
0	3	23	0.01	5.76	Si	>100
0	4	23	0.01	5.12	Si	>100
0	5	23	0.01	5.12	Si	>100
0	6	23	0.01	5.12	Si	>100
0	7	23	0.01	5.12	Si	>100
0	(8+9)-III-4	-81	0.03	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
0	(8+9)-I-4	-66	0.02	6.40	Si	>100
0	(8+9)-II-3	-81	0.03	6.40	Si	>100
0	(8+9)-I-2	142	0.05	6.40	Si	>100
0	(8+9)-I-1	101	0.03	6.40	Si	>100
0	(8+9)-II-2	116	0.04	6.40	Si	>100
0	(8+9)-I-3	-106	0.04	6.40	Si	>100
0	(8+9)-VI-2	113	0.04	6.40	Si	>100
0	(8+9)-III-1	116	0.04	6.40	Si	>100
0	(8+9)-III-2	127	0.04	6.40	Si	>100
0	(8+9)-III-3	-92	0.03	6.40	Si	>100
1935	(8+9)-VIII-4	-248	0.08	6.40	Si	77
1935	(8+9)-IV-2	-118	0.04	6.40	Si	>100
1935	(8+9)-VI-3	-84	0.03	6.40	Si	>100
1935	(8+9)-IV-1	89	0.03	6.40	Si	>100
1935	(8+9)-VI-4	-206	0.07	6.40	Si	93
1935	(8+9)-IV-3	110	0.04	6.40	Si	>100
1935	(8+9)-VII-1	495	0.17	6.40	Si	39
1935	(8+9)-V-1	482	0.16	6.40	Si	40
1935	(8+9)-VII-2	433	0.14	6.40	Si	44
1935	(8+9)-V-3	-454	0.15	6.40	Si	42
1935	(8+9)-VII-3	-441	0.15	6.40	Si	43
1935	(8+9)-VI-1	197	0.07	6.40	Si	97
1935	(8+9)-VII-4	-503	0.17	6.40	Si	38
1935	(8+9)-V-2	445	0.15	6.40	Si	43
1935	(8+9)-V-4	-490	0.16	6.40	Si	39
1935	(8+9)-II-1	47	0.02	6.40	Si	>100
1935	(8+9)-IV-4	-98	0.03	6.40	Si	>100
1935	(8+9)-VIII-1	240	0.08	6.40	Si	80
1935	(8+9)-II-4	-55	0.02	6.40	Si	>100
3870	(8+9)-VIII-2	85	0.03	6.40	Si	>100
3870	(8+9)-VIII-3	-92	0.03	6.40	Si	>100

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	2	1643	0.88	28.80	33	0.21	18.00	85	V	33
0	3	1643	0.88	28.80	33	0.21	18.00	85	V	33
0	(8+9)-V-1	-5355	-2.86	32.00	11	-0.69	20.00	29	V	11
0	(8+9)-V-4	6369	3.40	32.00	9.4	0.82	20.00	24	V	9.4
0	(8+9)-VII-4	5759	3.07	32.00	10	0.74	20.00	27	V	10
0	(8+9)-VII-1	-4746	-2.53	32.00	13	-0.61	20.00	33	V	13
0	(8+9)-I-1	-4374	-2.34	32.00	14	-0.57	20.00	35	V	14
2854	1	751	0.40	19.20	48	0.10	12.00	>100	V	48
2854	4	751	0.40	25.60	64	0.10	16.00	>100	V	64
2854	5	751	0.40	25.60	64	0.10	16.00	>100	V	64
2854	6	751	0.40	25.60	64	0.10	16.00	>100	V	64
2854	7	751	0.40	25.60	64	0.10	16.00	>100	V	64
2854	(8+9)-VII-3	11709	6.25	32.00	5.1	1.51	20.00	13	V	5.1
2854	(8+9)-III-3	11438	6.11	32.00	5.2	1.48	20.00	14	V	5.2
2854	(8+9)-II-1	7670	4.10	32.00	7.8	0.99	20.00	20	V	7.8
2854	(8+9)-II-3	12291	6.56	32.00	4.9	1.59	20.00	13	V	4.9
2854	(8+9)-V-2	-10284	-5.49	32.00	5.8	-1.33	20.00	15	V	5.8
2854	(8+9)-III-1	-3964	-2.12	32.00	15	-0.51	20.00	39	V	15
2854	(8+9)-V-3	11334	6.05	32.00	5.3	1.46	20.00	14	V	5.3
2854	(8+9)-II-2	-11241	-6.00	32.00	5.3	-1.45	20.00	14	V	5.3
2854	(8+9)-I-4	5390	2.88	32.00	11	0.70	20.00	29	V	11
2854	(8+9)-VI-1	7589	4.05	32.00	7.9	0.98	20.00	20	V	7.9
2854	(8+9)-IV-3	13542	7.23	32.00	4.4	1.75	20.00	11	V	4.4
2854	(8+9)-VI-2	-11322	-6.04	32.00	5.3	-1.46	20.00	14	V	5.3
2854	(8+9)-II-4	-6620	-3.53	32.00	9.1	-0.86	20.00	23	V	9.1
2854	(8+9)-VI-3	12372	6.61	32.00	4.8	1.60	20.00	13	V	4.8
2854	(8+9)-III-4	5015	2.68	32.00	12	0.65	20.00	31	V	12
2854	(8+9)-VIII-2	-12573	-6.71	32.00	4.8	-1.62	20.00	12	V	4.8

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
2854	(8+9)-III-2	-10388	-5.55	32.00	5.8	-1.34	20.00	15	V	5.8
2854	(8+9)-VIII-3	13623	7.27	32.00	4.4	1.76	20.00	11	V	4.4
2854	(8+9)-I-3	11063	5.91	32.00	5.4	1.43	20.00	14	V	5.4
2854	(8+9)-I-2	-10013	-5.35	32.00	6.0	-1.29	20.00	15	V	6.0
2854	(8+9)-VII-2	-10659	-5.69	32.00	5.6	-1.38	20.00	15	V	5.6
5708	(8+9)-VIII-4	-12235	-6.53	32.00	4.9	-1.58	20.00	13	V	4.9
5708	(8+9)-VI-4	-8170	-4.36	32.00	7.3	-1.06	20.00	19	V	7.3
5708	(8+9)-VIII-1	11638	6.21	32.00	5.2	1.50	20.00	13	V	5.2
5708	(8+9)-IV-4	-10614	-5.67	32.00	5.6	-1.37	20.00	15	V	5.6
5708	(8+9)-IV-2	-13675	-7.30	32.00	4.4	-1.77	20.00	11	V	4.4
5708	(8+9)-IV-1	10016	5.35	32.00	6.0	1.29	20.00	15	V	6.0
Verifiche nella direzione secondaria										
0	1	-714	-0.26	19.20	74	-0.06	12.00	>100	V	74
0	2	-1404	-0.51	28.80	57	-0.12	18.00	>100	V	57
0	3	-1404	-0.51	28.80	57	-0.12	18.00	>100	V	57
0	4	-714	-0.26	25.60	99	-0.06	16.00	>100	V	99
0	5	-714	-0.26	25.60	99	-0.06	16.00	>100	V	99
0	6	-714	-0.26	25.60	99	-0.06	16.00	>100	V	99
0	7	-714	-0.26	25.60	99	-0.06	16.00	>100	V	99
1935	(8+9)-VIII-4	14874	5.38	32.00	5.9	1.30	20.00	15	V	5.9
1935	(8+9)-IV-2	22664	8.20	32.00	3.9	1.99	20.00	10	V	3.9
1935	(8+9)-V-1	7096	2.57	32.00	12	0.62	20.00	32	V	12
1935	(8+9)-I-2	18087	6.55	32.00	4.9	1.58	20.00	13	V	4.9
1935	(8+9)-V-2	17172	6.22	32.00	5.1	1.50	20.00	13	V	5.1
1935	(8+9)-I-4	-8793	-3.18	32.00	10	-0.77	20.00	26	V	10
1935	(8+9)-V-3	-17954	-6.50	32.00	4.9	-1.57	20.00	13	V	4.9
1935	(8+9)-II-2	20434	7.40	32.00	4.3	1.79	20.00	11	V	4.3
1935	(8+9)-V-4	-7878	-2.85	32.00	11	-0.69	20.00	29	V	11
1935	(8+9)-II-4	12370	4.48	32.00	7.1	1.08	20.00	18	V	7.1
1935	(8+9)-VI-1	-13427	-4.86	32.00	6.6	-1.18	20.00	17	V	6.6
1935	(8+9)-III-2	18756	6.79	32.00	4.7	1.64	20.00	12	V	4.7
1935	(8+9)-VI-2	20159	7.30	32.00	4.4	1.77	20.00	11	V	4.4
1935	(8+9)-III-4	-8124	-2.94	32.00	11	-0.71	20.00	28	V	11
1935	(8+9)-VI-3	-20942	-7.58	32.00	4.2	-1.83	20.00	11	V	4.2
1935	(8+9)-I-1	8011	2.90	32.00	11	0.70	20.00	29	V	11
1935	(8+9)-VI-4	12644	4.58	32.00	7.0	1.11	20.00	18	V	7.0
1935	(8+9)-IV-4	14600	5.28	32.00	6.1	1.28	20.00	16	V	6.1
1935	(8+9)-VII-1	6427	2.33	32.00	14	0.56	20.00	36	V	14
1935	(8+9)-II-1	-13152	-4.76	32.00	6.7	-1.15	20.00	17	V	6.7
1935	(8+9)-VII-2	17841	6.46	32.00	5.0	1.56	20.00	13	V	5.0
1935	(8+9)-III-1	7342	2.66	32.00	12	0.64	20.00	31	V	12
1935	(8+9)-VII-3	-18623	-6.74	32.00	4.7	-1.63	20.00	12	V	4.7
1935	(8+9)-IV-1	-15382	-5.57	32.00	5.7	-1.35	20.00	15	V	5.7
1935	(8+9)-VII-4	-7209	-2.61	32.00	12	-0.63	20.00	32	V	12
1935	(8+9)-III-3	-19538	-7.07	32.00	4.5	-1.71	20.00	12	V	4.5
1935	(8+9)-IV-3	-23446	-8.49	32.00	3.8	-2.05	20.00	9.7	V	3.8
1935	(8+9)-II-3	-21216	-7.68	32.00	4.2	-1.86	20.00	11	V	4.2
1935	(8+9)-VIII-1	-15657	-5.67	32.00	5.6	-1.37	20.00	15	V	5.6
1935	(8+9)-VIII-2	22389	8.10	32.00	3.9	1.96	20.00	10	V	3.9
1935	(8+9)-VIII-3	-23172	-8.39	32.00	3.8	-2.03	20.00	9.9	V	3.8
1935	(8+9)-I-3	-18869	-6.83	32.00	4.7	-1.65	20.00	12	V	4.7

Verifiche a instabilità

Setto(X)	Comb.	k _{critc}	k _{critm}	λ_{relc}	λ_{relm}	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
(cm)						kg/cm q	kg/cm q	kg/cm q	kg/cm q	kg/cm q	kg/cm q	
1(0.0)	(8+9)-IV-3	0.22	--	2.07	--	-0.46	1.11	9.45	132.00	192.00	192.00	15

Parete Xlam 14 - Nodi: [7-5-105-106] - **Crit.Prog.** Criterio di verifica XLAM 0 - **Verificato:**
[Cs=2.226,Comb=(8+9)-IV-2]

Geometria setti

Setto	Crit.	X	L	S	X90	L90	S90
		mm	cm	cm	mm	cm	cm
2	Criterio di verifica XLAM 0	0	387.0	12.1	0	60.0	12.1
		300	387.0	12.1	1935	60.0	12.1
		600	387.0	12.1	3870	60.0	12.1
3	Criterio di verifica XLAM 0	0	387.0	12.1	0	57.9	12.1
		289	387.0	12.1	1935	57.9	12.1
		579	387.0	12.1	3870	57.9	12.1
4	Criterio di verifica XLAM 0	0	90.0	12.1	0	130.0	12.1
		650	90.0	12.1	450	130.0	12.1
		1300	90.0	12.1	900	130.0	12.1
5	Criterio di verifica XLAM 0	0	117.0	12.1	0	130.0	12.1
		650	117.0	12.1	585	130.0	12.1
		1300	117.0	12.1	1170	130.0	12.1

Setto 2: origine (40.6,1953.5,193.5), direzione (0.123439,0.992352,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	1	239	-5	-79	0.08	-0.07	-0.04	79.20	115.20	115.20	>100
0	2	442	-11	-184	0.16	-0.14	-0.10	118.80	172.80	172.80	>100
0	3	442	-11	-184	0.16	-0.14	-0.10	118.80	172.80	172.80	>100
0	4	239	-5	-79	0.08	-0.07	-0.04	105.60	153.60	153.60	>100
0	5	239	-5	-79	0.08	-0.07	-0.04	105.60	153.60	153.60	>100
0	6	239	-5	-79	0.08	-0.07	-0.04	105.60	153.60	153.60	>100
0	7	239	-5	-79	0.08	-0.07	-0.04	105.60	153.60	153.60	>100
0	(8+9)-VIII-4	1064	13	-3084	0.38	0.18	-1.70	132.00	192.00	192.00	79
0	(8+9)-IV-1	-173	-19	2543	-0.06	-0.25	1.40	132.00	192.00	192.00	>100
0	(8+9)-V-1	-266	6	2888	-0.09	0.08	1.59	132.00	192.00	192.00	>100
0	(8+9)-VI-1	-584	-16	2012	-0.21	-0.22	1.11	132.00	192.00	192.00	>100
0	(8+9)-VII-1	-310	5	3178	-0.11	0.07	1.75	132.00	192.00	192.00	>100
0	(8+9)-V-2	143	17	2108	0.05	0.22	1.16	132.00	192.00	192.00	>100
0	(8+9)-IV-2	1480	24	-1989	0.53	0.32	-1.10	132.00	192.00	192.00	88
0	(8+9)-VIII-3	-589	-29	1448	-0.21	-0.39	0.80	132.00	192.00	192.00	>100
0	(8+9)-IV-3	-1144	-31	1884	-0.41	-0.41	1.04	132.00	192.00	192.00	>100
0	(8+9)-II-4	366	8	-1681	0.13	0.10	-0.93	132.00	192.00	192.00	>100
0	(8+9)-IV-4	510	12	-2648	0.18	0.16	-1.46	132.00	192.00	192.00	>100
0	(8+9)-VII-4	646	-12	-3283	0.23	-0.16	-1.81	132.00	192.00	192.00	83
0	(8+9)-VI-4	920	9	-2117	0.33	0.12	-1.17	132.00	192.00	192.00	>100
0	(8+9)-VIII-2	926	22	-1553	0.33	0.30	-0.86	132.00	192.00	192.00	>100
0	(8+9)-VIII-1	-727	-20	2979	-0.26	-0.27	1.64	132.00	192.00	192.00	>100
0	(8+9)-VII-3	150	-25	-1924	0.05	-0.33	-1.06	132.00	192.00	192.00	>100
0	(8+9)-II-1	-29	-15	1576	-0.01	-0.20	0.87	132.00	192.00	192.00	>100
0	(8+9)-VII-2	186	18	1818	0.07	0.24	1.00	132.00	192.00	192.00	>100
0	(8+9)-V-3	193	-23	-2214	0.07	-0.31	-1.22	132.00	192.00	192.00	>100
0	(8+9)-V-4	603	-13	-2993	0.21	-0.18	-1.65	132.00	192.00	192.00	90
300	(8+9)-I-2	1294	56	1421	0.46	0.75	0.78	132.00	192.00	192.00	87
300	(8+9)-I-4	-976	-53	-2167	-0.35	-0.71	-1.20	132.00	192.00	192.00	>100
300	(8+9)-III-3	-1216	-66	-1282	-0.43	-0.89	-0.71	132.00	192.00	192.00	>100
300	(8+9)-III-2	1317	58	1118	0.47	0.77	0.62	132.00	192.00	192.00	93
300	(8+9)-I-3	-1194	-65	-1585	-0.42	-0.87	-0.87	132.00	192.00	192.00	>100
300	(8+9)-III-4	-954	-51	-2471	-0.34	-0.68	-1.36	132.00	192.00	192.00	94
300	(8+9)-III-1	1054	43	2307	0.38	0.57	1.27	132.00	192.00	192.00	80
300	(8+9)-I-1	1077	44	2003	0.38	0.59	1.11	132.00	192.00	192.00	85
600	(8+9)-VI-3	-762	-70	659	-0.27	-0.94	0.36	132.00	192.00	192.00	>100
600	(8+9)-II-3	-770	-76	693	-0.27	-1.01	0.38	132.00	192.00	192.00	>100
600	(8+9)-II-2	871	66	-519	0.31	0.88	-0.29	132.00	192.00	192.00	>100
600	(8+9)-VI-2	863	60	-486	0.31	0.81	-0.27	132.00	192.00	192.00	>100
Verifiche nella direzione secondaria											
0	1	-1271	4	165	-4.38	0.70	5.69	79.20	115.20	115.20	18
0	2	-2498	9	309	-8.60	1.85	10.65	118.80	172.80	172.80	13
0	3	-2498	9	309	-8.60	1.85	10.65	118.80	172.80	172.80	13
0	4	-1271	4	165	-4.38	0.70	5.69	105.60	153.60	153.60	24
0	5	-1271	4	165	-4.38	0.70	5.69	105.60	153.60	153.60	24

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	6	-1271	4	165	-4.38	0.70	5.69	105.60	153.60	153.60	24
0	7	-1271	4	165	-4.38	0.70	5.69	105.60	153.60	153.60	24
0	(8+9)-VIII-4	-3749	38	1609	-12.91	7.56	55.39	132.00	192.00	192.00	3.0
0	(8+9)-IV-2	-1340	7	1458	-4.61	1.46	50.20	132.00	192.00	192.00	3.7
0	(8+9)-V-1	4000	-51	-539	13.77	-10.05	-18.57	132.00	192.00	192.00	3.9
0	(8+9)-I-2	2258	-47	270	7.77	-9.34	9.30	132.00	192.00	192.00	6.4
0	(8+9)-V-2	3582	-52	77	12.33	-10.29	2.64	132.00	192.00	192.00	6.2
0	(8+9)-I-4	-4449	51	579	-15.32	10.02	19.93	132.00	192.00	192.00	6.2
0	(8+9)-V-3	-5355	57	156	-18.44	11.21	5.37	132.00	192.00	192.00	10
0	(8+9)-II-2	-577	-14	1097	-1.99	-2.85	37.76	132.00	192.00	192.00	4.7
0	(8+9)-V-4	-5773	56	772	-19.88	10.97	26.58	132.00	192.00	192.00	4.8
0	(8+9)-II-4	-2590	15	1189	-8.92	2.96	40.95	132.00	192.00	192.00	4.3
0	(8+9)-VI-1	1213	-12	-1015	4.18	-2.33	-34.94	132.00	192.00	192.00	4.4
0	(8+9)-III-2	2029	-41	378	6.99	-8.05	13.03	132.00	192.00	192.00	6.1
0	(8+9)-VI-2	-180	-16	1039	-0.62	-3.13	35.77	132.00	192.00	192.00	4.9
0	(8+9)-III-4	-4678	57	687	-16.11	11.31	23.66	132.00	192.00	192.00	5.3
0	(8+9)-VI-3	-1593	21	-806	-5.49	4.05	-27.75	132.00	192.00	192.00	6.0
0	(8+9)-I-1	2676	-46	-346	9.21	-9.10	-11.91	132.00	192.00	192.00	5.6
0	(8+9)-VI-4	-2987	16	1247	-10.29	3.24	42.95	132.00	192.00	192.00	4.1
0	(8+9)-IV-4	-3352	37	1551	-11.54	7.27	53.39	132.00	192.00	192.00	3.1
0	(8+9)-VII-1	4229	-58	-648	14.56	-11.35	-22.30	132.00	192.00	192.00	3.5
0	(8+9)-II-1	816	-10	-957	2.81	-2.04	-32.94	132.00	192.00	192.00	4.9
0	(8+9)-VII-2	3353	-46	185	11.55	-9.00	6.37	132.00	192.00	192.00	6.0
0	(8+9)-III-1	2905	-53	-454	10.00	-10.40	-15.64	132.00	192.00	192.00	4.7
0	(8+9)-VII-3	-5127	50	48	-17.65	9.92	1.64	132.00	192.00	192.00	15
0	(8+9)-IV-1	1579	-32	-1318	5.44	-6.36	-45.38	132.00	192.00	192.00	3.2
0	(8+9)-VII-4	-6002	62	880	-20.67	12.26	30.32	132.00	192.00	192.00	4.3
0	(8+9)-III-3	-3802	46	-146	-13.09	8.97	-5.02	132.00	192.00	192.00	13
0	(8+9)-IV-3	-433	-3	-1225	-1.49	-0.55	-42.19	132.00	192.00	192.00	4.5
0	(8+9)-II-3	-1196	19	-864	-4.12	3.76	-29.75	132.00	192.00	192.00	5.7
0	(8+9)-VIII-1	1976	-34	-1376	6.80	-6.64	-47.38	132.00	192.00	192.00	3.0
0	(8+9)-VIII-2	-943	6	1400	-3.25	1.18	48.21	132.00	192.00	192.00	3.9
0	(8+9)-VIII-3	-831	-1	-1167	-2.86	-0.26	-40.19	132.00	192.00	192.00	4.7
0	(8+9)-I-3	-4031	52	-37	-13.88	10.26	-1.29	132.00	192.00	192.00	15

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
0	1	-5	0.00	3.84	Si	>100
0	2	-12	0.00	5.76	Si	>100
0	3	-12	0.00	5.76	Si	>100
0	4	-5	0.00	5.12	Si	>100
0	5	-5	0.00	5.12	Si	>100
0	6	-5	0.00	5.12	Si	>100
0	7	-5	0.00	5.12	Si	>100
0	(8+9)-VIII-4	25	0.01	6.40	Si	>100
0	(8+9)-VIII-1	-31	0.01	6.40	Si	>100
0	(8+9)-VIII-3	-33	0.01	6.40	Si	>100
0	(8+9)-VIII-2	27	0.01	6.40	Si	>100
300	(8+9)-IV-1	35	0.01	6.40	Si	>100
300	(8+9)-V-1	25	0.01	6.40	Si	>100
300	(8+9)-I-2	177	0.05	6.40	Si	>100
300	(8+9)-V-4	-29	0.01	6.40	Si	>100
300	(8+9)-I-4	-177	0.05	6.40	Si	>100
300	(8+9)-IV-2	68	0.02	6.40	Si	>100
300	(8+9)-III-3	-184	0.05	6.40	Si	>100
300	(8+9)-III-4	-174	0.05	6.40	Si	>100
300	(8+9)-I-1	173	0.04	6.40	Si	>100
300	(8+9)-III-2	180	0.05	6.40	Si	>100
300	(8+9)-IV-3	-72	0.02	6.40	Si	>100
300	(8+9)-IV-4	-39	0.01	6.40	Si	>100
300	(8+9)-I-3	-182	0.05	6.40	Si	>100
300	(8+9)-III-1	170	0.04	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
600	(8+9)-II-3	-154	0.04	6.40	Si	>100
600	(8+9)-VI-1	-113	0.03	6.40	Si	>100
600	(8+9)-VII-2	39	0.01	6.40	Si	>100
600	(8+9)-II-4	90	0.02	6.40	Si	>100
600	(8+9)-VII-3	-43	0.01	6.40	Si	>100
600	(8+9)-VI-2	131	0.03	6.40	Si	>100
600	(8+9)-VII-4	-35	0.01	6.40	Si	>100
600	(8+9)-V-3	-76	0.02	6.40	Si	>100
600	(8+9)-VI-3	-136	0.04	6.40	Si	>100
600	(8+9)-VII-1	31	0.01	6.40	Si	>100
600	(8+9)-II-1	-95	0.02	6.40	Si	>100
600	(8+9)-V-2	72	0.02	6.40	Si	>100
600	(8+9)-II-2	150	0.04	6.40	Si	>100
600	(8+9)-VI-4	109	0.03	6.40	Si	>100
Verifiche nella direzione secondaria						
0	(8+9)-VIII-4	-51	0.16	6.40	Si	39
0	(8+9)-V-4	-69	0.22	6.40	Si	29
0	(8+9)-II-4	-39	0.12	6.40	Si	51
0	(8+9)-III-1	35	0.11	6.40	Si	58
0	(8+9)-VIII-1	42	0.13	6.40	Si	48
0	(8+9)-VI-1	38	0.12	6.40	Si	53
0	(8+9)-VII-3	-53	0.17	6.40	Si	38
0	(8+9)-III-3	-26	0.08	6.40	Si	77
0	(8+9)-I-1	34	0.11	6.40	Si	60
0	(8+9)-III-4	-44	0.14	6.40	Si	46
0	(8+9)-I-3	-27	0.09	6.40	Si	74
0	(8+9)-IV-1	34	0.11	6.40	Si	59
0	(8+9)-II-1	30	0.10	6.40	Si	66
0	(8+9)-V-3	-54	0.17	6.40	Si	37
0	(8+9)-VI-4	-47	0.15	6.40	Si	43
0	(8+9)-II-3	12	0.04	6.40	Si	>100
0	(8+9)-VII-4	-70	0.22	6.40	Si	29
0	(8+9)-IV-3	16	0.05	6.40	Si	>100
0	(8+9)-VII-1	62	0.20	6.40	Si	33
0	(8+9)-V-2	45	0.14	6.40	Si	45
0	(8+9)-VII-2	44	0.14	6.40	Si	46
0	(8+9)-I-4	-43	0.14	6.40	Si	47
0	(8+9)-IV-4	-43	0.14	6.40	Si	47
0	(8+9)-V-1	60	0.19	6.40	Si	33
1935	(8+9)-VIII-3	-12	0.04	6.40	Si	>100
3870	1	-16	0.05	3.84	Si	75
3870	2	-34	0.11	5.76	Si	53
3870	3	-34	0.11	5.76	Si	53
3870	4	-16	0.05	5.12	Si	99
3870	5	-16	0.05	5.12	Si	99
3870	6	-16	0.05	5.12	Si	99
3870	7	-16	0.05	5.12	Si	99
3870	(8+9)-IV-2	-32	0.10	6.40	Si	63
3870	(8+9)-I-2	-25	0.08	6.40	Si	81
3870	(8+9)-II-2	-32	0.10	6.40	Si	63
3870	(8+9)-VI-3	10	0.03	6.40	Si	>100
3870	(8+9)-VIII-2	-32	0.10	6.40	Si	63
3870	(8+9)-VI-2	-32	0.10	6.40	Si	63
3870	(8+9)-III-2	-25	0.08	6.40	Si	82

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	(8+9)-I-2	1433	0.77	32.00	42	0.19	20.00	>100	V	42
0	(8+9)-III-2	951	0.51	32.00	63	0.12	20.00	>100	V	63
300	1	-920	-0.49	19.20	39	-0.12	12.00	>100	V	39
300	2	-1791	-0.96	28.80	30	-0.23	18.00	78	V	30
300	3	-1791	-0.96	28.80	30	-0.23	18.00	78	V	30

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
300	4	-920	-0.49	25.60	52	-0.12	16.00	>100	V	52
300	5	-920	-0.49	25.60	52	-0.12	16.00	>100	V	52
300	6	-920	-0.49	25.60	52	-0.12	16.00	>100	V	52
300	7	-920	-0.49	25.60	52	-0.12	16.00	>100	V	52
300	(8+9)-V-4	-7352	-3.93	32.00	8.2	-0.95	20.00	21	V	8.2
300	(8+9)-II-2	-5113	-2.73	32.00	12	-0.66	20.00	30	V	12
300	(8+9)-III-3	-1685	-0.90	32.00	36	-0.22	20.00	92	V	36
300	(8+9)-I-4	-5081	-2.71	32.00	12	-0.66	20.00	30	V	12
300	(8+9)-VI-4	-7499	-4.00	32.00	8.0	-0.97	20.00	21	V	8.0
300	(8+9)-VII-3	-3956	-2.11	32.00	15	-0.51	20.00	39	V	15
300	(8+9)-II-4	-6818	-3.64	32.00	8.8	-0.88	20.00	23	V	8.8
300	(8+9)-VI-3	3146	1.68	32.00	19	0.41	20.00	49	V	19
300	(8+9)-I-1	3797	2.03	32.00	16	0.49	20.00	41	V	16
300	(8+9)-II-3	3828	2.04	32.00	16	0.49	20.00	40	V	16
300	(8+9)-VII-2	2671	1.43	32.00	22	0.35	20.00	58	V	22
300	(8+9)-II-1	5533	2.95	32.00	11	0.71	20.00	28	V	11
300	(8+9)-VI-2	-4431	-2.37	32.00	14	-0.57	20.00	35	V	14
300	(8+9)-VI-1	6214	3.32	32.00	9.6	0.80	20.00	25	V	9.6
300	(8+9)-V-1	6068	3.24	32.00	9.9	0.78	20.00	26	V	9.9
600	(8+9)-VIII-4	-11056	-5.90	32.00	5.4	-1.43	20.00	14	V	5.4
600	(8+9)-IV-1	9360	5.00	32.00	6.4	1.21	20.00	17	V	6.4
600	(8+9)-III-1	5170	2.76	32.00	12	0.67	20.00	30	V	12
600	(8+9)-V-3	-4358	-2.33	32.00	14	-0.56	20.00	36	V	14
600	(8+9)-I-3	-2403	-1.28	32.00	25	-0.31	20.00	64	V	25
600	(8+9)-IV-4	-10469	-5.59	32.00	5.7	-1.35	20.00	15	V	5.7
600	(8+9)-VII-4	-8234	-4.40	32.00	7.3	-1.06	20.00	19	V	7.3
600	(8+9)-VII-1	7125	3.80	32.00	8.4	0.92	20.00	22	V	8.4
600	(8+9)-V-2	3249	1.73	32.00	18	0.42	20.00	48	V	18
600	(8+9)-IV-3	7547	4.03	32.00	7.9	0.98	20.00	21	V	7.9
600	(8+9)-III-4	-6279	-3.35	32.00	9.5	-0.81	20.00	25	V	9.5
600	(8+9)-VIII-1	9947	5.31	32.00	6.0	1.29	20.00	16	V	6.0
600	(8+9)-VIII-2	-8070	-4.31	32.00	7.4	-1.04	20.00	19	V	7.4
600	(8+9)-VIII-3	6961	3.72	32.00	8.6	0.90	20.00	22	V	8.6
600	(8+9)-IV-2	-8656	-4.62	32.00	6.9	-1.12	20.00	18	V	6.9
Verifiche nella direzione secondaria										
0	1	263	0.90	19.20	21	0.22	12.00	55	V	21
0	2	516	1.78	28.80	16	0.43	18.00	42	V	16
0	3	516	1.78	28.80	16	0.43	18.00	42	V	16
0	4	263	0.90	25.60	28	0.22	16.00	73	V	28
0	5	263	0.90	25.60	28	0.22	16.00	73	V	28
0	6	263	0.90	25.60	28	0.22	16.00	73	V	28
0	7	263	0.90	25.60	28	0.22	16.00	73	V	28
1935	(8+9)-VIII-4	2245	7.73	32.00	4.1	1.87	20.00	11	V	4.1
1935	(8+9)-IV-2	1504	5.18	32.00	6.2	1.25	20.00	16	V	6.2
1935	(8+9)-V-1	-1626	-5.60	32.00	5.7	-1.36	20.00	15	V	5.7
1935	(8+9)-I-2	-588	-2.03	32.00	16	-0.49	20.00	41	V	16
1935	(8+9)-V-2	-916	-3.15	32.00	10	-0.76	20.00	26	V	10
1935	(8+9)-I-4	1554	5.35	32.00	6.0	1.29	20.00	15	V	6.0
1935	(8+9)-V-3	1171	4.03	32.00	7.9	0.98	20.00	20	V	7.9
1935	(8+9)-II-2	990	3.41	32.00	9.4	0.82	20.00	24	V	9.4
1935	(8+9)-V-4	1881	6.48	32.00	4.9	1.57	20.00	13	V	4.9
1935	(8+9)-II-4	1632	5.62	32.00	5.7	1.36	20.00	15	V	5.7
1935	(8+9)-VI-1	-1475	-5.08	32.00	6.3	-1.23	20.00	16	V	6.3
1935	(8+9)-III-2	-434	-1.50	32.00	21	-0.36	20.00	55	V	21
1935	(8+9)-VI-2	891	3.07	32.00	10	0.74	20.00	27	V	10
1935	(8+9)-III-4	1708	5.88	32.00	5.4	1.42	20.00	14	V	5.4
1935	(8+9)-VI-3	-636	-2.19	32.00	15	-0.53	20.00	38	V	15
1935	(8+9)-I-1	-1299	-4.47	32.00	7.2	-1.08	20.00	18	V	7.2
1935	(8+9)-VI-4	1731	5.96	32.00	5.4	1.44	20.00	14	V	5.4
1935	(8+9)-IV-4	2146	7.39	32.00	4.3	1.79	20.00	11	V	4.3
1935	(8+9)-VII-1	-1780	-6.13	32.00	5.2	-1.48	20.00	13	V	5.2
1935	(8+9)-II-1	-1377	-4.74	32.00	6.7	-1.15	20.00	17	V	6.7
1935	(8+9)-VII-2	-762	-2.62	32.00	12	-0.63	20.00	32	V	12
1935	(8+9)-III-1	-1453	-5.00	32.00	6.4	-1.21	20.00	17	V	6.4

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
1935	(8+9)-VII-3	1017	3.50	32.00	9.1	0.85	20.00	24	V	9.1
1935	(8+9)-IV-1	-1891	-6.51	32.00	4.9	-1.58	20.00	13	V	4.9
1935	(8+9)-VII-4	2035	7.01	32.00	4.6	1.70	20.00	12	V	4.6
1935	(8+9)-III-3	689	2.37	32.00	13	0.57	20.00	35	V	13
1935	(8+9)-IV-3	-1249	-4.30	32.00	7.4	-1.04	20.00	19	V	7.4
1935	(8+9)-II-3	-735	-2.53	32.00	13	-0.61	20.00	33	V	13
1935	(8+9)-VIII-1	-1989	-6.85	32.00	4.7	-1.66	20.00	12	V	4.7
1935	(8+9)-VIII-2	1405	4.84	32.00	6.6	1.17	20.00	17	V	6.6
1935	(8+9)-VIII-3	-1150	-3.96	32.00	8.1	-0.96	20.00	21	V	8.1
1935	(8+9)-I-3	844	2.90	32.00	11	0.70	20.00	28	V	11

Setto 3: origine (17.4,1767.0,193.5), direzione (0.123439,0.992352,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	(8+9)-VII-4	-574	-80	-583	-0.20	-1.08	-0.32	132.00	192.00	192.00	>100
0	(8+9)-VII-1	741	92	801	0.26	1.23	0.44	132.00	192.00	192.00	93
0	(8+9)-V-1	706	88	779	0.25	1.18	0.43	132.00	192.00	192.00	97
0	(8+9)-V-4	-540	-76	-561	-0.19	-1.02	-0.31	132.00	192.00	192.00	>100
0	(8+9)-V-2	748	90	747	0.27	1.20	0.41	132.00	192.00	192.00	96
0	(8+9)-VII-2	714	85	724	0.25	1.14	0.40	132.00	192.00	192.00	>100
0	(8+9)-VII-3	-547	-74	-507	-0.19	-0.99	-0.28	132.00	192.00	192.00	>100
0	(8+9)-V-3	-582	-78	-529	-0.21	-1.04	-0.29	132.00	192.00	192.00	>100
289	(8+9)-II-3	-178	0	-2065	-0.06	0.01	-1.14	132.00	192.00	192.00	>100
289	(8+9)-III-3	-992	-49	-2085	-0.35	-0.65	-1.15	132.00	192.00	192.00	>100
289	(8+9)-I-3	-1014	-50	-2024	-0.36	-0.67	-1.12	132.00	192.00	192.00	>100
289	(8+9)-III-4	-1080	-60	-905	-0.38	-0.80	-0.50	132.00	192.00	192.00	>100
289	(8+9)-I-2	1180	56	2441	0.42	0.75	1.35	132.00	192.00	192.00	71
289	(8+9)-I-1	1225	65	1384	0.44	0.87	0.76	132.00	192.00	192.00	85
289	(8+9)-II-2	344	5	2482	0.12	0.07	1.37	132.00	192.00	192.00	>100
289	(8+9)-III-1	1246	66	1322	0.44	0.88	0.73	132.00	192.00	192.00	85
289	(8+9)-III-2	1158	55	2503	0.41	0.73	1.38	132.00	192.00	192.00	71
289	(8+9)-I-4	-1058	-59	-966	-0.38	-0.79	-0.53	132.00	192.00	192.00	>100
579	1	247	2	329	0.09	0.02	0.18	79.20	115.20	115.20	>100
579	2	459	3	616	0.16	0.04	0.34	118.80	172.80	172.80	>100
579	3	459	3	616	0.16	0.04	0.34	118.80	172.80	172.80	>100
579	4	247	2	329	0.09	0.02	0.18	105.60	153.60	153.60	>100
579	5	247	2	329	0.09	0.02	0.18	105.60	153.60	153.60	>100
579	6	247	2	329	0.09	0.02	0.18	105.60	153.60	153.60	>100
579	7	247	2	329	0.09	0.02	0.18	105.60	153.60	153.60	>100
579	(8+9)-VIII-4	-263	-22	2884	-0.09	-0.29	1.59	132.00	192.00	192.00	>100
579	(8+9)-IV-1	1013	21	-2040	0.36	0.29	-1.13	132.00	192.00	192.00	99
579	(8+9)-IV-2	292	-16	2585	0.10	-0.21	1.43	132.00	192.00	192.00	>100
579	(8+9)-IV-4	-665	-19	2503	-0.24	-0.26	1.38	132.00	192.00	192.00	>100
579	(8+9)-II-4	-506	-18	1921	-0.18	-0.24	1.06	132.00	192.00	192.00	>100
579	(8+9)-VI-2	49	-12	1622	0.02	-0.16	0.90	132.00	192.00	192.00	>100
579	(8+9)-II-1	854	20	-1458	0.30	0.27	-0.80	132.00	192.00	192.00	>100
579	(8+9)-VI-1	452	23	-1839	0.16	0.30	-1.01	132.00	192.00	192.00	>100
579	(8+9)-VI-3	299	14	-1159	0.11	0.19	-0.64	132.00	192.00	192.00	>100
579	(8+9)-IV-3	56	18	-2122	0.02	0.24	-1.17	132.00	192.00	192.00	>100
579	(8+9)-VIII-1	611	24	-2421	0.22	0.32	-1.34	132.00	192.00	192.00	97
579	(8+9)-VIII-2	-110	-13	2204	-0.04	-0.18	1.22	132.00	192.00	192.00	>100
579	(8+9)-VIII-3	458	16	-1741	0.16	0.21	-0.96	132.00	192.00	192.00	>100
579	(8+9)-VI-4	-104	-20	2302	-0.04	-0.27	1.27	132.00	192.00	192.00	>100
Verifiche nella direzione secondaria											
0	1	-572	-8	-62	-2.04	-1.67	-2.29	79.20	115.20	115.20	29
0	2	-1095	-14	-102	-3.91	-2.84	-3.79	118.80	172.80	172.80	26
0	3	-1095	-14	-102	-3.91	-2.84	-3.79	118.80	172.80	172.80	26
0	4	-572	-8	-62	-2.04	-1.67	-2.29	105.60	153.60	153.60	39
0	5	-572	-8	-62	-2.04	-1.67	-2.29	105.60	153.60	153.60	39
0	6	-572	-8	-62	-2.04	-1.67	-2.29	105.60	153.60	153.60	39
0	7	-572	-8	-62	-2.04	-1.67	-2.29	105.60	153.60	153.60	39
0	(8+9)-VIII-4	4641	-40	1212	16.56	-8.17	44.83	132.00	192.00	192.00	2.5

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-IV-2	5989	-76	1070	21.37	-15.58	39.58	132.00	192.00	192.00	2.2
0	(8+9)-V-1	-1018	-37	-1182	-3.63	-7.47	-43.72	132.00	192.00	192.00	3.7
0	(8+9)-I-2	4709	-96	620	16.80	-19.61	22.93	132.00	192.00	192.00	2.9
0	(8+9)-V-2	1697	-80	-785	6.06	-16.44	-29.04	132.00	192.00	192.00	3.5
0	(8+9)-I-4	-2798	40	-312	-9.98	8.26	-11.55	132.00	192.00	192.00	9.4
0	(8+9)-V-3	-2501	69	696	-8.93	14.05	25.74	132.00	192.00	192.00	4.8
0	(8+9)-II-2	5249	-100	757	18.73	-20.32	27.99	132.00	192.00	192.00	2.5
0	(8+9)-V-4	214	25	1093	0.76	5.08	40.42	132.00	192.00	192.00	4.1
0	(8+9)-II-4	2997	-59	477	10.70	-11.95	17.65	132.00	192.00	192.00	4.3
0	(8+9)-VI-1	-4705	52	-988	-16.79	10.52	-36.54	132.00	192.00	192.00	4.0
0	(8+9)-III-2	4931	-89	714	17.60	-18.19	26.41	132.00	192.00	192.00	2.7
0	(8+9)-VI-2	4345	-95	335	15.51	-19.36	12.40	132.00	192.00	192.00	3.5
0	(8+9)-III-4	-2576	47	-218	-9.19	9.68	-8.08	132.00	192.00	192.00	11
0	(8+9)-VI-3	-5150	83	-425	-18.38	16.97	-15.70	132.00	192.00	192.00	5.6
0	(8+9)-I-1	1994	-52	223	7.11	-10.65	8.25	132.00	192.00	192.00	6.6
0	(8+9)-VI-4	3901	-63	899	13.92	-12.91	33.24	132.00	192.00	192.00	2.9
0	(8+9)-IV-4	3737	-35	791	13.34	-7.22	29.24	132.00	192.00	192.00	3.4
0	(8+9)-VII-1	-1240	-44	-1276	-4.43	-8.89	-47.20	132.00	192.00	192.00	3.4
0	(8+9)-II-1	-3801	47	-566	-13.57	9.56	-20.95	132.00	192.00	192.00	6.1
0	(8+9)-VII-2	1919	-74	-691	6.85	-15.01	-25.56	132.00	192.00	192.00	3.8
0	(8+9)-III-1	1772	-59	129	6.32	-12.07	4.77	132.00	192.00	192.00	7.4
0	(8+9)-VII-3	-2723	62	602	-9.72	12.63	22.26	132.00	192.00	192.00	5.4
0	(8+9)-IV-1	-4541	24	-880	-16.21	4.83	-32.54	132.00	192.00	192.00	5.0
0	(8+9)-VII-4	436	32	1187	1.56	6.50	43.90	132.00	192.00	192.00	3.6
0	(8+9)-III-3	-5735	77	-803	-20.47	15.80	-29.71	132.00	192.00	192.00	4.0
0	(8+9)-IV-3	-6793	65	-1160	-24.24	13.19	-42.89	132.00	192.00	192.00	3.2
0	(8+9)-II-3	-6053	88	-846	-21.60	17.93	-31.30	132.00	192.00	192.00	3.7
0	(8+9)-VIII-1	-5445	28	-1301	-19.43	5.78	-48.13	132.00	192.00	192.00	3.4
0	(8+9)-VIII-2	5085	-72	649	18.15	-14.63	23.99	132.00	192.00	192.00	3.0
0	(8+9)-VIII-3	-5890	60	-738	-21.02	12.24	-27.30	132.00	192.00	192.00	4.6
0	(8+9)-I-3	-5513	84	-709	-19.67	17.23	-26.24	132.00	192.00	192.00	4.2

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
0	(8+9)-V-1	-69	0.02	6.40	Si	>100
0	(8+9)-VII-4	50	0.01	6.40	Si	>100
0	(8+9)-VII-1	-70	0.02	6.40	Si	>100
0	(8+9)-VIII-3	32	0.01	6.40	Si	>100
0	(8+9)-VII-3	63	0.02	6.40	Si	>100
0	(8+9)-VIII-2	-51	0.01	6.40	Si	>100
0	(8+9)-VI-2	-55	0.01	6.40	Si	>100
0	(8+9)-V-2	-84	0.02	6.40	Si	>100
0	(8+9)-V-4	49	0.01	6.40	Si	>100
0	(8+9)-VI-3	36	0.01	6.40	Si	>100
0	(8+9)-V-3	64	0.02	6.40	Si	>100
0	(8+9)-VII-2	-83	0.02	6.40	Si	>100
289	1	-14	0.00	3.84	Si	>100
289	2	-25	0.01	5.76	Si	>100
289	3	-25	0.01	5.76	Si	>100
289	4	-14	0.00	5.12	Si	>100
289	5	-14	0.00	5.12	Si	>100
289	6	-14	0.00	5.12	Si	>100
289	7	-14	0.00	5.12	Si	>100
289	(8+9)-VIII-4	-28	0.01	6.40	Si	>100
289	(8+9)-IV-1	-72	0.02	6.40	Si	>100
289	(8+9)-II-3	87	0.02	6.40	Si	>100
289	(8+9)-IV-2	-103	0.03	6.40	Si	>100
289	(8+9)-VI-4	-32	0.01	6.40	Si	>100
289	(8+9)-IV-4	53	0.01	6.40	Si	>100
289	(8+9)-II-2	-106	0.03	6.40	Si	>100
289	(8+9)-III-3	254	0.07	6.40	Si	97
289	(8+9)-II-1	-69	0.02	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
289	(8+9)-III-1	-264	0.07	6.40	Si	94
289	(8+9)-I-4	243	0.06	6.40	Si	>100
289	(8+9)-II-4	49	0.01	6.40	Si	>100
289	(8+9)-I-3	255	0.07	6.40	Si	97
289	(8+9)-VI-1	12	0.00	6.40	Si	>100
289	(8+9)-IV-3	83	0.02	6.40	Si	>100
289	(8+9)-III-2	-273	0.07	6.40	Si	90
289	(8+9)-III-4	245	0.06	6.40	Si	>100
289	(8+9)-I-2	-275	0.07	6.40	Si	90
289	(8+9)-I-1	-263	0.07	6.40	Si	94
579	(8+9)-VIII-1	-13	0.00	6.40	Si	>100
Verifiche nella direzione secondaria						
0	1	18	0.06	3.84	Si	63
0	2	32	0.11	5.76	Si	54
0	3	32	0.11	5.76	Si	54
0	4	18	0.06	5.12	Si	84
0	5	18	0.06	5.12	Si	84
0	6	18	0.06	5.12	Si	84
0	7	18	0.06	5.12	Si	84
0	(8+9)-VIII-4	123	0.41	6.40	Si	16
0	(8+9)-IV-2	189	0.62	6.40	Si	10
0	(8+9)-I-2	245	0.81	6.40	Si	7.9
0	(8+9)-V-2	57	0.19	6.40	Si	34
0	(8+9)-I-4	-161	0.53	6.40	Si	12
0	(8+9)-V-3	-31	0.10	6.40	Si	63
0	(8+9)-II-2	170	0.56	6.40	Si	11
0	(8+9)-VIII-1	-97	0.32	6.40	Si	20
0	(8+9)-II-3	-144	0.47	6.40	Si	13
0	(8+9)-II-4	49	0.16	6.40	Si	40
0	(8+9)-III-2	251	0.83	6.40	Si	7.8
0	(8+9)-VI-1	-79	0.26	6.40	Si	25
0	(8+9)-III-4	-155	0.51	6.40	Si	13
0	(8+9)-VI-2	114	0.38	6.40	Si	17
0	(8+9)-I-1	187	0.62	6.40	Si	10
0	(8+9)-VI-3	-88	0.29	6.40	Si	22
0	(8+9)-IV-4	67	0.22	6.40	Si	29
0	(8+9)-VIII-2	132	0.44	6.40	Si	15
0	(8+9)-I-3	-219	0.72	6.40	Si	8.9
0	(8+9)-VI-4	105	0.35	6.40	Si	19
0	(8+9)-III-3	-224	0.74	6.40	Si	8.7
0	(8+9)-IV-3	-162	0.54	6.40	Si	12
0	(8+9)-III-1	182	0.60	6.40	Si	11
0	(8+9)-IV-1	-41	0.13	6.40	Si	48
0	(8+9)-VIII-3	-106	0.35	6.40	Si	18
0	(8+9)-VII-2	63	0.21	6.40	Si	31
0	(8+9)-VII-3	-37	0.12	6.40	Si	53
1935	(8+9)-II-1	33	0.11	6.40	Si	58
3870	(8+9)-V-1	-35	0.12	6.40	Si	55
3870	(8+9)-VII-4	44	0.14	6.40	Si	44
3870	(8+9)-VII-1	-38	0.13	6.40	Si	51
3870	(8+9)-V-4	41	0.13	6.40	Si	48

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	1	-502	-0.27	19.20	72	-0.06	12.00	>100	V	72
0	2	-950	-0.51	28.80	57	-0.12	18.00	>100	V	57
0	3	-950	-0.51	28.80	57	-0.12	18.00	>100	V	57
0	4	-502	-0.27	25.60	96	-0.06	16.00	>100	V	96
0	5	-502	-0.27	25.60	96	-0.06	16.00	>100	V	96
0	6	-502	-0.27	25.60	96	-0.06	16.00	>100	V	96
0	7	-502	-0.27	25.60	96	-0.06	16.00	>100	V	96
0	(8+9)-III-4	1456	0.78	32.00	41	0.19	20.00	>100	V	41

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
0	(8+9)-I-3	5152	2.75	32.00	12	0.67	20.00	30	V	12
0	(8+9)-VI-2	-5138	-2.74	32.00	12	-0.66	20.00	30	V	12
0	(8+9)-I-4	1983	1.06	32.00	30	0.26	20.00	78	V	30
0	(8+9)-VI-3	4435	2.37	32.00	14	0.57	20.00	35	V	14
0	(8+9)-II-2	-6810	-3.64	32.00	8.8	-0.88	20.00	23	V	8.8
0	(8+9)-I-1	-2686	-1.43	32.00	22	-0.35	20.00	58	V	22
0	(8+9)-I-2	-5855	-3.13	32.00	10	-0.76	20.00	26	V	10
0	(8+9)-III-1	-2160	-1.15	32.00	28	-0.28	20.00	72	V	28
0	(8+9)-III-2	-6382	-3.41	32.00	9.4	-0.82	20.00	24	V	9.4
289	(8+9)-IV-2	-9750	-5.21	32.00	6.1	-1.26	20.00	16	V	6.1
289	(8+9)-II-1	4022	2.15	32.00	15	0.52	20.00	38	V	15
289	(8+9)-III-3	5826	3.11	32.00	10	0.75	20.00	27	V	10
289	(8+9)-VI-4	-7106	-3.79	32.00	8.4	-0.92	20.00	22	V	8.4
289	(8+9)-II-4	-4560	-2.43	32.00	13	-0.59	20.00	34	V	13
289	(8+9)-IV-3	9212	4.92	32.00	6.5	1.19	20.00	17	V	6.5
289	(8+9)-VIII-1	9615	5.13	32.00	6.2	1.24	20.00	16	V	6.2
289	(8+9)-VIII-3	6666	3.56	32.00	9.0	0.86	20.00	23	V	9.0
289	(8+9)-VIII-2	-7204	-3.85	32.00	8.3	-0.93	20.00	21	V	8.3
289	(8+9)-VIII-4	-10153	-5.42	32.00	5.9	-1.31	20.00	15	V	5.9
289	(8+9)-VI-1	6568	3.51	32.00	9.1	0.85	20.00	24	V	9.1
289	(8+9)-II-3	6165	3.29	32.00	9.7	0.80	20.00	25	V	9.7
289	(8+9)-IV-1	7069	3.77	32.00	8.5	0.91	20.00	22	V	8.5
289	(8+9)-IV-4	-7607	-4.06	32.00	7.9	-0.98	20.00	20	V	7.9
579	(8+9)-VII-1	7865	4.20	32.00	7.6	1.02	20.00	20	V	7.6
579	(8+9)-V-3	-5845	-3.12	32.00	10	-0.76	20.00	26	V	10
579	(8+9)-VII-2	4454	2.38	32.00	13	0.58	20.00	35	V	13
579	(8+9)-VII-4	-8473	-4.52	32.00	7.1	-1.09	20.00	18	V	7.1
579	(8+9)-V-4	-7689	-4.11	32.00	7.8	-0.99	20.00	20	V	7.8
579	(8+9)-VII-3	-5062	-2.70	32.00	12	-0.65	20.00	31	V	12
579	(8+9)-V-2	5237	2.80	32.00	11	0.68	20.00	30	V	11
579	(8+9)-V-1	7082	3.78	32.00	8.5	0.91	20.00	22	V	8.5
Verifiche nella direzione secondaria										
0	(8+9)-III-4	-456	-1.63	32.00	20	-0.39	20.00	51	V	20
1935	(8+9)-VIII-4	2181	7.78	32.00	4.1	1.88	20.00	11	V	4.1
1935	(8+9)-VII-2	-618	-2.21	32.00	15	-0.53	20.00	37	V	15
1935	(8+9)-III-3	-1493	-5.33	32.00	6.0	-1.29	20.00	16	V	6.0
1935	(8+9)-IV-2	2131	7.60	32.00	4.2	1.84	20.00	11	V	4.2
1935	(8+9)-VII-3	774	2.76	32.00	12	0.67	20.00	30	V	12
1935	(8+9)-VIII-2	1451	5.18	32.00	6.2	1.25	20.00	16	V	6.2
1935	(8+9)-IV-1	-1345	-4.80	32.00	6.7	-1.16	20.00	17	V	6.7
1935	(8+9)-VII-4	1817	6.48	32.00	4.9	1.57	20.00	13	V	4.9
1935	(8+9)-I-2	1511	5.39	32.00	5.9	1.30	20.00	15	V	5.9
1935	(8+9)-IV-3	-1975	-7.05	32.00	4.5	-1.71	20.00	12	V	4.5
1935	(8+9)-I-4	-588	-2.10	32.00	15	-0.51	20.00	39	V	15
1935	(8+9)-IV-4	1501	5.36	32.00	6.0	1.30	20.00	15	V	6.0
1935	(8+9)-II-2	1670	5.96	32.00	5.4	1.44	20.00	14	V	5.4
1935	(8+9)-V-1	-1522	-5.43	32.00	5.9	-1.31	20.00	15	V	5.9
1935	(8+9)-II-4	1040	3.71	32.00	8.6	0.90	20.00	22	V	8.6
1935	(8+9)-V-2	-756	-2.70	32.00	12	-0.65	20.00	31	V	12
1935	(8+9)-III-2	1649	5.88	32.00	5.4	1.42	20.00	14	V	5.4
1935	(8+9)-V-3	912	3.26	32.00	9.8	0.79	20.00	25	V	9.8
1935	(8+9)-VIII-1	-2025	-7.23	32.00	4.4	-1.75	20.00	11	V	4.4
1935	(8+9)-V-4	1678	5.99	32.00	5.3	1.45	20.00	14	V	5.3
1935	(8+9)-I-3	-1354	-4.83	32.00	6.6	-1.17	20.00	17	V	6.6
1935	(8+9)-VI-1	-1564	-5.58	32.00	5.7	-1.35	20.00	15	V	5.7
1935	(8+9)-II-3	-1514	-5.40	32.00	5.9	-1.31	20.00	15	V	5.9
1935	(8+9)-VI-2	990	3.53	32.00	9.1	0.85	20.00	23	V	9.1
1935	(8+9)-VIII-3	-1295	-4.62	32.00	6.9	-1.12	20.00	18	V	6.9
1935	(8+9)-II-1	-884	-3.15	32.00	10	-0.76	20.00	26	V	10
1935	(8+9)-III-1	606	2.16	32.00	15	0.52	20.00	38	V	15
1935	(8+9)-I-1	744	2.66	32.00	12	0.64	20.00	31	V	12
1935	(8+9)-VI-3	-834	-2.98	32.00	11	-0.72	20.00	28	V	11
1935	(8+9)-VI-4	1720	6.14	32.00	5.2	1.49	20.00	13	V	5.2
1935	(8+9)-VII-1	-1661	-5.93	32.00	5.4	-1.43	20.00	14	V	5.4

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
3870	1	167	0.60	19.20	32	0.14	12.00	83	V	32
3870	2	328	1.17	28.80	25	0.28	18.00	64	V	25
3870	3	328	1.17	28.80	25	0.28	18.00	64	V	25
3870	4	167	0.60	25.60	43	0.14	16.00	>100	V	43
3870	5	167	0.60	25.60	43	0.14	16.00	>100	V	43
3870	6	167	0.60	25.60	43	0.14	16.00	>100	V	43
3870	7	167	0.60	25.60	43	0.14	16.00	>100	V	43

Setto 4: origine (24.5,1824.5,45.0), direzione (0.123439,0.992352,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	
0	1	268	2	-45	0.41	0.12	-0.46	79.20	115.20	115.20	98
0	2	506	4	-89	0.77	0.24	-0.91	118.80	172.80	172.80	76
0	3	506	4	-89	0.77	0.24	-0.91	118.80	172.80	172.80	76
0	4	268	2	-45	0.41	0.12	-0.46	105.60	153.60	153.60	>100
0	5	268	2	-45	0.41	0.12	-0.46	105.60	153.60	153.60	>100
0	6	268	2	-45	0.41	0.12	-0.46	105.60	153.60	153.60	>100
0	7	268	2	-45	0.41	0.12	-0.46	105.60	153.60	153.60	>100
0	(8+9)-V-3	433	6	-375	0.66	0.32	-3.83	132.00	192.00	192.00	38
0	(8+9)-VII-4	1079	8	-746	1.65	0.49	-7.61	132.00	192.00	192.00	18
0	(8+9)-VI-4	1290	6	-701	1.97	0.36	-7.15	132.00	192.00	192.00	18
0	(8+9)-I-2	1340	7	-511	2.05	0.41	-5.22	132.00	192.00	192.00	22
0	(8+9)-III-2	1420	8	-570	2.17	0.46	-5.81	132.00	192.00	192.00	20
0	(8+9)-VIII-2	1242	6	-596	1.90	0.37	-6.08	132.00	192.00	192.00	21
0	(8+9)-III-3	-1042	-5	508	-1.60	-0.29	5.18	132.00	192.00	192.00	35
0	(8+9)-II-2	1392	6	-648	2.13	0.35	-6.61	132.00	192.00	192.00	19
0	(8+9)-VI-2	974	3	-401	1.49	0.19	-4.09	132.00	192.00	192.00	30
0	(8+9)-VIII-4	1558	9	-896	2.38	0.54	-9.14	132.00	192.00	192.00	15
0	(8+9)-II-3	-1015	-3	586	-1.55	-0.18	5.98	132.00	192.00	192.00	31
0	(8+9)-I-3	-962	-4	449	-1.47	-0.23	4.58	132.00	192.00	192.00	40
0	(8+9)-V-4	998	8	-687	1.53	0.43	-7.01	132.00	192.00	192.00	20
0	(8+9)-IV-2	1660	9	-843	2.54	0.53	-8.60	132.00	192.00	192.00	15
0	(8+9)-IV-3	-1283	-6	781	-1.96	-0.36	7.97	132.00	192.00	192.00	23
1300	(8+9)-VII-1	1481	6	-736	2.27	0.35	-7.51	132.00	192.00	192.00	17
1300	(8+9)-I-1	1341	2	-511	2.05	0.14	-5.21	132.00	192.00	192.00	23
1300	(8+9)-II-4	-972	-8	679	-1.49	-0.45	6.93	132.00	192.00	192.00	26
1300	(8+9)-V-1	1371	6	-672	2.10	0.33	-6.86	132.00	192.00	192.00	19
1300	(8+9)-VII-2	864	2	-301	1.32	0.12	-3.07	132.00	192.00	192.00	38
1300	(8+9)-IV-4	-1338	-9	892	-2.05	-0.51	9.10	132.00	192.00	192.00	20
1300	(8+9)-VII-3	-812	-5	393	-1.24	-0.30	4.01	132.00	192.00	192.00	44
1300	(8+9)-VI-1	1033	6	-635	1.58	0.32	-6.48	132.00	192.00	192.00	21
1300	(8+9)-II-1	1024	5	-587	1.57	0.27	-5.99	132.00	192.00	192.00	22
1300	(8+9)-V-2	973	2	-365	1.49	0.14	-3.72	132.00	192.00	192.00	32
1300	(8+9)-IV-1	1389	6	-800	2.13	0.33	-8.16	132.00	192.00	192.00	17
1300	(8+9)-III-4	-1399	-6	667	-2.14	-0.34	6.80	132.00	192.00	192.00	27
1300	(8+9)-III-1	1451	3	-575	2.22	0.16	-5.87	132.00	192.00	192.00	21
1300	(8+9)-VIII-1	1398	7	-848	2.14	0.39	-8.65	132.00	192.00	192.00	16
1300	(8+9)-I-4	-1290	-5	603	-1.97	-0.32	6.15	132.00	192.00	192.00	30
1300	(8+9)-VIII-3	710	3	-509	1.09	0.20	-5.20	132.00	192.00	192.00	28
1300	(8+9)-VI-3	345	2	-296	0.53	0.13	-3.02	132.00	192.00	192.00	49
Verifiche nella direzione secondaria											
0	(8+9)-VII-2	-147	-66	948	-0.23	-5.99	6.95	132.00	192.00	192.00	15
0	(8+9)-I-4	-3819	83	-728	-6.07	7.54	-5.34	132.00	192.00	192.00	15
0	(8+9)-III-1	2543	-91	597	4.04	-8.29	4.38	132.00	192.00	192.00	10
0	(8+9)-VII-3	-1151	62	-1236	-1.83	5.65	-9.06	132.00	192.00	192.00	13
0	(8+9)-V-3	-1173	67	-1392	-1.86	6.07	-10.21	132.00	192.00	192.00	12
0	(8+9)-III-4	-3841	87	-885	-6.11	7.95	-6.49	132.00	192.00	192.00	13
0	(8+9)-V-2	-125	-70	1105	-0.20	-6.40	8.10	132.00	192.00	192.00	13
0	(8+9)-I-1	2521	-87	440	4.01	-7.88	3.23	132.00	192.00	192.00	11
0	(8+9)-I-2	2670	-102	-495	4.24	-9.30	-3.63	132.00	192.00	192.00	10
450	(8+9)-II-2	1459	-26	-2018	2.32	-2.33	-14.80	132.00	192.00	192.00	9.4
450	(8+9)-V-1	-952	-42	2428	-1.51	-3.86	17.81	132.00	192.00	192.00	8.9

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
450	(8+9)-VIII-3	-1454	26	1854	-2.31	2.36	13.60	132.00	192.00	192.00	12
450	(8+9)-III-3	-3845	40	1187	-6.11	3.66	8.71	132.00	192.00	192.00	15
450	(8+9)-VI-2	452	-28	-1286	0.72	-2.58	-9.43	132.00	192.00	192.00	15
450	(8+9)-VII-1	-1006	-43	2633	-1.60	-3.90	19.32	132.00	192.00	192.00	8.3
450	(8+9)-II-3	-2281	25	1902	-3.63	2.24	13.95	132.00	192.00	192.00	12
450	(8+9)-VI-3	-1274	27	1170	-2.02	2.49	8.58	132.00	192.00	192.00	17
450	(8+9)-I-3	-3791	41	982	-6.03	3.70	7.20	132.00	192.00	192.00	17
450	(8+9)-V-4	130	42	-2544	0.21	3.77	-18.66	132.00	192.00	192.00	8.4
450	(8+9)-III-2	3023	-41	-1303	4.80	-3.75	-9.56	132.00	192.00	192.00	9.5
450	(8+9)-IV-2	1639	-24	-2702	2.60	-2.20	-19.82	132.00	192.00	192.00	7.4
450	(8+9)-IV-3	-2461	23	2585	-3.91	2.11	18.97	132.00	192.00	192.00	9.1
450	(8+9)-VIII-2	632	-27	-1970	1.00	-2.45	-14.45	132.00	192.00	192.00	10
900	1	-446	0	-267	-0.71	0.04	-1.96	79.20	115.20	115.20	58
900	2	-871	1	-527	-1.38	0.09	-3.87	118.80	172.80	172.80	44
900	3	-871	1	-527	-1.38	0.09	-3.87	118.80	172.80	172.80	44
900	4	-446	0	-267	-0.71	0.04	-1.96	105.60	153.60	153.60	77
900	5	-446	0	-267	-0.71	0.04	-1.96	105.60	153.60	153.60	77
900	6	-446	0	-267	-0.71	0.04	-1.96	105.60	153.60	153.60	77
900	7	-446	0	-267	-0.71	0.04	-1.96	105.60	153.60	153.60	77
900	(8+9)-VIII-4	-547	8	-3715	-0.87	0.70	-27.25	132.00	192.00	192.00	6.9
900	(8+9)-VI-4	-417	-5	-2905	-0.66	-0.44	-21.31	132.00	192.00	192.00	8.8
900	(8+9)-II-1	536	3	1903	0.85	0.30	13.96	132.00	192.00	192.00	12
900	(8+9)-VI-1	-206	5	2533	-0.33	0.50	18.58	132.00	192.00	192.00	10
900	(8+9)-VII-4	-751	10	-3220	-1.19	0.87	-23.62	132.00	192.00	192.00	7.8
900	(8+9)-VIII-1	-76	-7	3344	-0.12	-0.65	24.53	132.00	192.00	192.00	7.6
900	(8+9)-II-4	-1159	-3	-2274	-1.84	-0.24	-16.68	132.00	192.00	192.00	11
900	(8+9)-IV-1	666	-9	2714	1.06	-0.85	19.91	132.00	192.00	192.00	8.6
900	(8+9)-IV-4	-1289	10	-3085	-2.05	0.90	-22.63	132.00	192.00	192.00	8.2

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Ty kg	τ_d kg/cmq	fvd kg/cmq	RS	Cs
0	1	-6	0.01	3.84	Si	>100
0	2	-11	0.01	5.76	Si	>100
0	3	-11	0.01	5.76	Si	>100
0	4	-6	0.01	5.12	Si	>100
0	5	-6	0.01	5.12	Si	>100
0	6	-6	0.01	5.12	Si	>100
0	7	-6	0.01	5.12	Si	>100
0	(8+9)-VIII-4	-35	0.04	6.40	Si	>100
0	(8+9)-IV-1	-28	0.03	6.40	Si	>100
0	(8+9)-I-2	-191	0.21	6.40	Si	30
0	(8+9)-VIII-1	25	0.03	6.40	Si	>100
0	(8+9)-IV-3	79	0.09	6.40	Si	73
0	(8+9)-I-4	165	0.18	6.40	Si	35
0	(8+9)-II-2	-87	0.10	6.40	Si	66
0	(8+9)-I-3	182	0.20	6.40	Si	32
0	(8+9)-II-4	20	0.02	6.40	Si	>100
0	(8+9)-VI-4	-33	0.04	6.40	Si	>100
0	(8+9)-III-1	-174	0.19	6.40	Si	33
0	(8+9)-III-2	-192	0.21	6.40	Si	30
0	(8+9)-III-4	164	0.18	6.40	Si	35
0	(8+9)-VIII-3	26	0.03	6.40	Si	>100
0	(8+9)-IV-2	-88	0.10	6.40	Si	65
0	(8+9)-VIII-2	-35	0.04	6.40	Si	>100
0	(8+9)-II-3	78	0.09	6.40	Si	74
0	(8+9)-I-1	-174	0.19	6.40	Si	33
0	(8+9)-II-1	-29	0.03	6.40	Si	>100
0	(8+9)-III-3	182	0.20	6.40	Si	32
0	(8+9)-VI-1	24	0.03	6.40	Si	>100
0	(8+9)-VI-2	-34	0.04	6.40	Si	>100
0	(8+9)-VI-3	25	0.03	6.40	Si	>100
650	(8+9)-IV-4	20	0.02	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
1300	(8+9)-V-1	22	0.02	6.40	Si	>100
1300	(8+9)-VII-2	21	0.02	6.40	Si	>100
1300	(8+9)-VII-3	-25	0.03	6.40	Si	>100
1300	(8+9)-VII-4	-27	0.03	6.40	Si	>100
1300	(8+9)-VII-1	24	0.03	6.40	Si	>100
1300	(8+9)-V-4	-26	0.03	6.40	Si	>100
1300	(8+9)-V-3	-26	0.03	6.40	Si	>100
1300	(8+9)-V-2	22	0.02	6.40	Si	>100
Verifiche nella direzione secondaria						
0	1	5	0.01	3.84	Si	>100
0	4	5	0.01	5.12	Si	>100
0	5	5	0.01	5.12	Si	>100
0	6	5	0.01	5.12	Si	>100
0	7	5	0.01	5.12	Si	>100
0	(8+9)-VIII-4	18	0.03	6.40	Si	>100
0	(8+9)-IV-2	88	0.13	6.40	Si	49
0	(8+9)-VI-4	14	0.02	6.40	Si	>100
0	(8+9)-VIII-1	-10	0.01	6.40	Si	>100
450	2	7	0.01	5.76	Si	>100
450	3	7	0.01	5.76	Si	>100
450	(8+9)-V-1	68	0.10	6.40	Si	64
450	(8+9)-V-2	81	0.12	6.40	Si	54
450	(8+9)-VII-1	67	0.10	6.40	Si	65
450	(8+9)-V-3	-74	0.11	6.40	Si	59
450	(8+9)-VI-3	-40	0.06	6.40	Si	>100
450	(8+9)-VII-3	-75	0.11	6.40	Si	58
450	(8+9)-VII-2	82	0.12	6.40	Si	53
450	(8+9)-VIII-3	-44	0.06	6.40	Si	100
450	(8+9)-VII-4	-59	0.09	6.40	Si	74
450	(8+9)-VI-2	48	0.07	6.40	Si	91
450	(8+9)-V-4	-60	0.09	6.40	Si	72
450	(8+9)-VIII-2	51	0.08	6.40	Si	85
900	(8+9)-I-1	248	0.36	6.40	Si	18
900	(8+9)-II-2	90	0.13	6.40	Si	48
900	(8+9)-III-4	-247	0.36	6.40	Si	18
900	(8+9)-I-4	-247	0.36	6.40	Si	18
900	(8+9)-III-3	-254	0.37	6.40	Si	17
900	(8+9)-IV-3	-86	0.13	6.40	Si	51
900	(8+9)-III-2	256	0.38	6.40	Si	17
900	(8+9)-II-1	63	0.09	6.40	Si	70
900	(8+9)-III-1	249	0.37	6.40	Si	18
900	(8+9)-VI-1	-8	0.01	6.40	Si	>100
900	(8+9)-IV-1	65	0.10	6.40	Si	67
900	(8+9)-IV-4	-63	0.09	6.40	Si	69
900	(8+9)-I-2	257	0.38	6.40	Si	17
900	(8+9)-II-4	-61	0.09	6.40	Si	72
900	(8+9)-II-3	-88	0.13	6.40	Si	49
900	(8+9)-I-3	-255	0.37	6.40	Si	17

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	(8+9)-V-1	2314	5.31	32.00	6.0	1.29	20.00	16	V	6.0
0	(8+9)-II-2	-2269	-5.21	32.00	6.1	-1.26	20.00	16	V	6.1
0	(8+9)-III-2	-2255	-5.18	32.00	6.2	-1.25	20.00	16	V	6.2
0	(8+9)-I-3	2105	4.83	32.00	6.6	1.17	20.00	17	V	6.6
0	(8+9)-II-3	2319	5.32	32.00	6.0	1.29	20.00	16	V	6.0
0	(8+9)-VIII-1	3049	7.00	32.00	4.6	1.69	20.00	12	V	4.6
0	(8+9)-IV-3	2986	6.86	32.00	4.7	1.66	20.00	12	V	4.7
0	(8+9)-VII-2	1012	2.32	32.00	14	0.56	20.00	36	V	14
0	(8+9)-VI-1	2382	5.47	32.00	5.9	1.32	20.00	15	V	5.9
0	(8+9)-III-3	2305	5.29	32.00	6.0	1.28	20.00	16	V	6.0
0	(8+9)-IV-2	-2936	-6.74	32.00	4.7	-1.63	20.00	12	V	4.7

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
0	(8+9)-VIII-3	2006	4.60	32.00	6.9	1.11	20.00	18	V	6.9
0	(8+9)-V-2	1212	2.78	32.00	11	0.67	20.00	30	V	11
0	(8+9)-I-2	-2055	-4.72	32.00	6.8	-1.14	20.00	18	V	6.8
0	(8+9)-VII-1	2514	5.77	32.00	5.5	1.40	20.00	14	V	5.5
0	(8+9)-VI-3	1339	3.07	32.00	10	0.74	20.00	27	V	10
1300	1	-422	-0.97	19.20	20	-0.23	12.00	51	V	20
1300	2	-833	-1.91	28.80	15	-0.46	18.00	39	V	15
1300	3	-833	-1.91	28.80	15	-0.46	18.00	39	V	15
1300	4	-422	-0.97	25.60	26	-0.23	16.00	68	V	26
1300	5	-422	-0.97	25.60	26	-0.23	16.00	68	V	26
1300	6	-422	-0.97	25.60	26	-0.23	16.00	68	V	26
1300	7	-422	-0.97	25.60	26	-0.23	16.00	68	V	26
1300	(8+9)-VIII-4	-3071	-7.05	32.00	4.5	-1.71	20.00	12	V	4.5
1300	(8+9)-IV-1	2360	5.42	32.00	5.9	1.31	20.00	15	V	5.9
1300	(8+9)-II-4	-2265	-5.20	32.00	6.2	-1.26	20.00	16	V	6.2
1300	(8+9)-IV-4	-2947	-6.77	32.00	4.7	-1.64	20.00	12	V	4.7
1300	(8+9)-II-1	1677	3.85	32.00	8.3	0.93	20.00	21	V	8.3
1300	(8+9)-V-4	-2570	-5.90	32.00	5.4	-1.43	20.00	14	V	5.4
1300	(8+9)-VII-3	-1434	-3.29	32.00	9.7	-0.80	20.00	25	V	9.7
1300	(8+9)-VI-2	-1302	-2.99	32.00	11	-0.72	20.00	28	V	11
1300	(8+9)-VII-4	-2775	-6.37	32.00	5.0	-1.54	20.00	13	V	5.0
1300	(8+9)-III-4	-2362	-5.42	32.00	5.9	-1.31	20.00	15	V	5.9
1300	(8+9)-III-1	1775	4.07	32.00	7.9	0.99	20.00	20	V	7.9
1300	(8+9)-V-3	-1639	-3.76	32.00	8.5	-0.91	20.00	22	V	8.5
1300	(8+9)-I-4	-2158	-4.95	32.00	6.5	-1.20	20.00	17	V	6.5
1300	(8+9)-VIII-2	-1985	-4.56	32.00	7.0	-1.10	20.00	18	V	7.0
1300	(8+9)-I-1	1570	3.60	32.00	8.9	0.87	20.00	23	V	8.9
1300	(8+9)-VI-4	-2389	-5.48	32.00	5.8	-1.33	20.00	15	V	5.8
Verifiche nella direzione secondaria										
450	1	268	0.43	19.20	45	0.10	12.00	>100	V	45
450	2	522	0.83	28.80	35	0.20	18.00	90	V	35
450	3	522	0.83	28.80	35	0.20	18.00	90	V	35
450	4	268	0.43	25.60	60	0.10	16.00	>100	V	60
450	5	268	0.43	25.60	60	0.10	16.00	>100	V	60
450	6	268	0.43	25.60	60	0.10	16.00	>100	V	60
450	7	268	0.43	25.60	60	0.10	16.00	>100	V	60
450	(8+9)-VIII-4	3404	5.41	32.00	5.9	1.31	20.00	15	V	5.9
450	(8+9)-IV-2	3137	4.99	32.00	6.4	1.21	20.00	17	V	6.4
450	(8+9)-I-2	1375	2.19	32.00	15	0.53	20.00	38	V	15
450	(8+9)-VI-1	-2362	-3.75	32.00	8.5	-0.91	20.00	22	V	8.5
450	(8+9)-IV-1	-2432	-3.86	32.00	8.3	-0.94	20.00	21	V	8.3
450	(8+9)-VI-4	2735	4.35	32.00	7.4	1.05	20.00	19	V	7.4
450	(8+9)-II-2	2469	3.92	32.00	8.2	0.95	20.00	21	V	8.2
450	(8+9)-IV-3	-2764	-4.39	32.00	7.3	-1.06	20.00	19	V	7.3
450	(8+9)-II-4	2137	3.40	32.00	9.4	0.82	20.00	24	V	9.4
450	(8+9)-IV-4	2805	4.46	32.00	7.2	1.08	20.00	19	V	7.2
450	(8+9)-III-2	1575	2.50	32.00	13	0.61	20.00	33	V	13
450	(8+9)-I-3	-1002	-1.59	32.00	20	-0.39	20.00	52	V	20
450	(8+9)-VIII-2	2539	4.03	32.00	7.9	0.98	20.00	20	V	7.9
450	(8+9)-II-3	-2095	-3.33	32.00	9.6	-0.81	20.00	25	V	9.6
450	(8+9)-VIII-3	-2165	-3.44	32.00	9.3	-0.83	20.00	24	V	9.3
450	(8+9)-III-3	-1202	-1.91	32.00	17	-0.46	20.00	43	V	17
450	(8+9)-II-1	-1763	-2.80	32.00	11	-0.68	20.00	29	V	11
450	(8+9)-VI-2	1870	2.97	32.00	11	0.72	20.00	28	V	11
450	(8+9)-VI-3	-1497	-2.38	32.00	13	-0.58	20.00	35	V	13
900	(8+9)-V-2	-1232	-1.96	32.00	16	-0.47	20.00	42	V	16
900	(8+9)-V-1	-2349	-3.73	32.00	8.6	-0.90	20.00	22	V	8.6
900	(8+9)-I-4	432	0.69	32.00	47	0.17	20.00	>100	V	47
900	(8+9)-VII-3	1313	2.09	32.00	15	0.51	20.00	40	V	15
900	(8+9)-V-4	2660	4.23	32.00	7.6	1.02	20.00	20	V	7.6
900	(8+9)-VII-4	2889	4.59	32.00	7.0	1.11	20.00	18	V	7.0
900	(8+9)-VII-2	-1003	-1.59	32.00	20	-0.39	20.00	52	V	20
900	(8+9)-V-3	1542	2.45	32.00	13	0.59	20.00	34	V	13
900	(8+9)-VII-1	-2578	-4.10	32.00	7.8	-0.99	20.00	20	V	7.8

X	Comb.	Tx	τvd	fvd	Csv	τM	fTd	Csm	Mecc.	Cs
900	(8+9)-VIII-1	-3054	-4.85	32.00	6.6	-1.17	20.00	17	V	6.6
900	(8+9)-III-4	661	1.05	32.00	30	0.25	20.00	79	V	30
900	(8+9)-III-1	-351	-0.56	32.00	57	-0.13	20.00	>100	V	57
900	(8+9)-I-1	-122	-0.19	32.00	>100	-0.05	20.00	>100	V	>100

Setto 5: origine (24.5,1824.5,328.5), direzione (0.123439,0.992352,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σn	σmx	σmy	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	(8+9)-III-2	-433	-12	-659	-0.51	-0.53	-3.98	132.00	192.00	192.00	43
0	(8+9)-I-2	-303	-10	-593	-0.36	-0.45	-3.58	132.00	192.00	192.00	48
0	(8+9)-IV-1	1550	24	737	1.82	1.07	4.45	132.00	192.00	192.00	24
0	(8+9)-I-3	273	9	518	0.32	0.42	3.13	132.00	192.00	192.00	48
0	(8+9)-VIII-1	1844	31	1042	2.17	1.37	6.29	132.00	192.00	192.00	18
0	(8+9)-V-1	1346	24	821	1.58	1.08	4.95	132.00	192.00	192.00	23
0	(8+9)-VII-1	1477	26	887	1.74	1.16	5.35	132.00	192.00	192.00	21
0	(8+9)-II-1	1115	18	517	1.31	0.79	3.12	132.00	192.00	192.00	33
0	(8+9)-VI-1	1409	25	822	1.66	1.09	4.96	132.00	192.00	192.00	23
0	(8+9)-IV-3	1522	26	951	1.79	1.17	5.74	132.00	192.00	192.00	20
0	(8+9)-VI-3	793	13	426	0.93	0.59	2.57	132.00	192.00	192.00	42
0	(8+9)-V-2	677	13	424	0.80	0.56	2.56	132.00	192.00	192.00	45
0	(8+9)-VII-2	546	11	358	0.64	0.48	2.16	132.00	192.00	192.00	54
0	(8+9)-II-3	1087	20	731	1.28	0.90	4.41	132.00	192.00	192.00	27
0	(8+9)-VIII-3	1228	20	646	1.45	0.87	3.90	132.00	192.00	192.00	28
0	(8+9)-III-3	404	11	584	0.48	0.50	3.52	132.00	192.00	192.00	41
1300	1	204	-3	80	0.24	-0.12	0.48	79.20	115.20	115.20	>100
1300	2	398	-6	155	0.47	-0.27	0.94	118.80	172.80	172.80	91
1300	3	398	-6	155	0.47	-0.27	0.94	118.80	172.80	172.80	91
1300	4	204	-3	80	0.24	-0.12	0.48	105.60	153.60	153.60	>100
1300	5	204	-3	80	0.24	-0.12	0.48	105.60	153.60	153.60	>100
1300	6	204	-3	80	0.24	-0.12	0.48	105.60	153.60	153.60	>100
1300	7	204	-3	80	0.24	-0.12	0.48	105.60	153.60	153.60	>100
1300	(8+9)-VIII-4	2381	25	1096	2.80	1.08	6.61	132.00	192.00	192.00	16
1300	(8+9)-VI-2	1055	26	470	1.24	1.15	2.84	132.00	192.00	192.00	33
1300	(8+9)-III-1	-1208	6	-555	-1.42	0.27	-3.35	132.00	192.00	192.00	53
1300	(8+9)-IV-2	1735	32	801	2.04	1.42	4.84	132.00	192.00	192.00	21
1300	(8+9)-V-3	1100	-18	501	1.30	-0.81	3.03	132.00	192.00	192.00	34
1300	(8+9)-VII-3	946	-20	427	1.11	-0.86	2.58	132.00	192.00	192.00	38
1300	(8+9)-I-1	-1053	7	-480	-1.24	0.32	-2.90	132.00	192.00	192.00	60
1300	(8+9)-VII-4	2045	-2	938	2.41	-0.09	5.66	132.00	192.00	192.00	21
1300	(8+9)-II-2	1221	28	552	1.44	1.26	3.33	132.00	192.00	192.00	29
1300	(8+9)-V-4	1891	-3	863	2.23	-0.14	5.21	132.00	192.00	192.00	22
1300	(8+9)-I-4	1339	-11	591	1.58	-0.48	3.57	132.00	192.00	192.00	30
1300	(8+9)-VI-4	1867	21	846	2.20	0.92	5.11	132.00	192.00	192.00	21
1300	(8+9)-II-4	1701	18	765	2.00	0.81	4.62	132.00	192.00	192.00	23
1300	(8+9)-VIII-2	1570	30	720	1.85	1.32	4.35	132.00	192.00	192.00	23
1300	(8+9)-III-4	1493	-10	666	1.76	-0.43	4.02	132.00	192.00	192.00	27
1300	(8+9)-IV-4	2216	22	1014	2.61	0.98	6.12	132.00	192.00	192.00	18
Verifiche nella direzione secondaria											
0	1	-651	-2	366	-1.03	-0.18	2.69	79.20	115.20	115.20	40
0	2	-1315	-4	737	-2.09	-0.38	5.41	118.80	172.80	172.80	30
0	3	-1315	-4	737	-2.09	-0.38	5.41	118.80	172.80	172.80	30
0	4	-651	-2	366	-1.03	-0.18	2.69	105.60	153.60	153.60	53
0	5	-651	-2	366	-1.03	-0.18	2.69	105.60	153.60	153.60	53
0	6	-651	-2	366	-1.03	-0.18	2.69	105.60	153.60	153.60	53
0	7	-651	-2	366	-1.03	-0.18	2.69	105.60	153.60	153.60	53
0	(8+9)-VIII-4	-165	-7	3883	-0.26	-0.67	28.48	132.00	192.00	192.00	6.6
0	(8+9)-IV-2	485	10	3040	0.77	0.88	22.30	132.00	192.00	192.00	7.9
0	(8+9)-V-1	-477	12	-2645	-0.76	1.12	-19.41	132.00	192.00	192.00	9.4
0	(8+9)-I-2	1742	42	345	2.77	3.80	2.53	132.00	192.00	192.00	19
0	(8+9)-V-2	-317	13	-1366	-0.50	1.19	-10.02	132.00	192.00	192.00	17
0	(8+9)-I-4	-2485	-44	1443	-3.95	-3.96	10.59	132.00	192.00	192.00	13
0	(8+9)-V-3	-586	-16	1874	-0.93	-1.44	13.75	132.00	192.00	192.00	13

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-II-2	449	13	2222	0.71	1.17	16.30	132.00	192.00	192.00	10
0	(8+9)-V-4	-426	-15	3154	-0.68	-1.36	23.13	132.00	192.00	192.00	7.8
0	(8+9)-II-4	-818	-13	2552	-1.30	-1.16	18.72	132.00	192.00	192.00	9.7
0	(8+9)-VI-1	-702	1	-2557	-1.12	0.13	-18.75	132.00	192.00	192.00	10
0	(8+9)-III-2	1753	41	590	2.79	3.71	4.33	132.00	192.00	192.00	16
0	(8+9)-VI-2	-168	4	1709	-0.27	0.39	12.54	132.00	192.00	192.00	15
0	(8+9)-III-4	-2474	-45	1688	-3.93	-4.05	12.39	132.00	192.00	192.00	12
0	(8+9)-VI-3	-735	-7	-1201	-1.17	-0.64	-8.81	132.00	192.00	192.00	20
0	(8+9)-I-1	1582	41	-935	2.51	3.72	-6.86	132.00	192.00	192.00	13
0	(8+9)-VI-4	-201	-4	3065	-0.32	-0.38	22.48	132.00	192.00	192.00	8.4
0	(8+9)-IV-4	-783	-16	3370	-1.24	-1.45	24.72	132.00	192.00	192.00	7.3
0	(8+9)-VII-1	-488	13	-2891	-0.78	1.20	-21.20	132.00	192.00	192.00	8.6
0	(8+9)-II-1	-84	10	-2044	-0.13	0.91	-14.99	132.00	192.00	192.00	12
0	(8+9)-VII-2	-306	12	-1120	-0.49	1.11	-8.22	132.00	192.00	192.00	21
0	(8+9)-III-1	1571	42	-1180	2.50	3.81	-8.66	132.00	192.00	192.00	12
0	(8+9)-VII-3	-597	-15	1629	-0.95	-1.35	11.95	132.00	192.00	192.00	14
0	(8+9)-IV-1	-120	13	-2861	-0.19	1.20	-20.99	132.00	192.00	192.00	8.7
0	(8+9)-VII-4	-415	-16	3399	-0.66	-1.45	24.93	132.00	192.00	192.00	7.3
0	(8+9)-VIII-3	-770	-4	-2019	-1.22	-0.34	-14.81	132.00	192.00	192.00	13
0	(8+9)-IV-3	-1388	-12	-2532	-2.21	-1.12	-18.57	132.00	192.00	192.00	9.7
0	(8+9)-II-3	-1352	-16	-1714	-2.15	-1.42	-12.57	132.00	192.00	192.00	14
0	(8+9)-VIII-1	-738	5	-3374	-1.17	0.42	-24.75	132.00	192.00	192.00	7.6
0	(8+9)-VIII-2	-132	1	2527	-0.21	0.10	18.54	132.00	192.00	192.00	10
585	(8+9)-III-3	-2060	-43	219	-3.27	-3.88	1.60	132.00	192.00	192.00	35
585	(8+9)-I-3	-2080	-43	321	-3.31	-3.91	2.35	132.00	192.00	192.00	30

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
0	(8+9)-III-4	-159	0.14	6.40	Si	47
0	(8+9)-I-3	-181	0.15	6.40	Si	41
0	(8+9)-II-2	81	0.07	6.40	Si	92
0	(8+9)-I-1	161	0.14	6.40	Si	46
0	(8+9)-I-4	-162	0.14	6.40	Si	46
0	(8+9)-I-2	179	0.15	6.40	Si	42
0	(8+9)-IV-2	91	0.08	6.40	Si	83
0	(8+9)-III-3	-183	0.16	6.40	Si	41
0	(8+9)-IV-3	-92	0.08	6.40	Si	81
0	(8+9)-III-1	158	0.14	6.40	Si	47
0	(8+9)-III-2	182	0.16	6.40	Si	41
0	(8+9)-II-3	-83	0.07	6.40	Si	90
650	(8+9)-IV-1	-36	0.03	6.40	Si	>100
650	(8+9)-II-1	-28	0.02	6.40	Si	>100
650	(8+9)-II-4	25	0.02	6.40	Si	>100
650	(8+9)-VII-3	13	0.01	6.40	Si	>100
650	(8+9)-IV-4	34	0.03	6.40	Si	>100
650	(8+9)-V-2	-18	0.02	6.40	Si	>100
650	(8+9)-V-3	16	0.01	6.40	Si	>100
1300	1	-2	0.00	3.84	Si	>100
1300	2	-5	0.00	5.76	Si	>100
1300	3	-5	0.00	5.76	Si	>100
1300	4	-2	0.00	5.12	Si	>100
1300	5	-2	0.00	5.12	Si	>100
1300	6	-2	0.00	5.12	Si	>100
1300	7	-2	0.00	5.12	Si	>100
1300	(8+9)-VIII-4	49	0.04	6.40	Si	>100
1300	(8+9)-VI-3	-30	0.03	6.40	Si	>100
1300	(8+9)-V-1	-40	0.03	6.40	Si	>100
1300	(8+9)-VI-1	-46	0.04	6.40	Si	>100
1300	(8+9)-VII-4	39	0.03	6.40	Si	>100
1300	(8+9)-VII-1	-42	0.04	6.40	Si	>100
1300	(8+9)-VII-2	-16	0.01	6.40	Si	>100
1300	(8+9)-VI-2	27	0.02	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
1300	(8+9)-VI-4	43	0.04	6.40	Si	>100
1300	(8+9)-VIII-1	-52	0.04	6.40	Si	>100
1300	(8+9)-VIII-2	33	0.03	6.40	Si	>100
1300	(8+9)-VIII-3	-36	0.03	6.40	Si	>100
1300	(8+9)-V-4	37	0.03	6.40	Si	>100
Verifiche nella direzione secondaria						
0	1	4	0.01	3.84	Si	>100
0	2	8	0.01	5.76	Si	>100
0	3	8	0.01	5.76	Si	>100
0	4	4	0.01	5.12	Si	>100
0	5	4	0.01	5.12	Si	>100
0	6	4	0.01	5.12	Si	>100
0	7	4	0.01	5.12	Si	>100
0	(8+9)-IV-2	36	0.05	6.40	Si	>100
0	(8+9)-VI-2	2	0.00	6.40	Si	>100
0	(8+9)-III-1	107	0.16	6.40	Si	41
0	(8+9)-I-2	107	0.16	6.40	Si	41
0	(8+9)-III-2	108	0.16	6.40	Si	40
0	(8+9)-I-4	-103	0.15	6.40	Si	43
0	(8+9)-III-3	-103	0.15	6.40	Si	42
0	(8+9)-II-2	33	0.05	6.40	Si	>100
0	(8+9)-III-4	-102	0.15	6.40	Si	43
0	(8+9)-II-1	35	0.05	6.40	Si	>100
0	(8+9)-II-3	-28	0.04	6.40	Si	>100
0	(8+9)-I-3	-102	0.15	6.40	Si	43
0	(8+9)-IV-1	32	0.05	6.40	Si	>100
0	(8+9)-I-1	107	0.16	6.40	Si	41
0	(8+9)-IV-3	-31	0.05	6.40	Si	>100
0	(8+9)-II-4	-30	0.04	6.40	Si	>100
585	(8+9)-VIII-4	11	0.02	6.40	Si	>100
585	(8+9)-VI-3	5	0.01	6.40	Si	>100
585	(8+9)-VIII-3	-4	0.01	6.40	Si	>100
585	(8+9)-VIII-2	8	0.01	6.40	Si	>100
1170	(8+9)-V-1	-9	0.01	6.40	Si	>100
1170	(8+9)-VII-1	-11	0.02	6.40	Si	>100
1170	(8+9)-V-2	-8	0.01	6.40	Si	>100
1170	(8+9)-VII-4	13	0.02	6.40	Si	>100
1170	(8+9)-VI-1	-4	0.01	6.40	Si	>100
1170	(8+9)-VII-2	-6	0.01	6.40	Si	>100
1170	(8+9)-VII-3	9	0.01	6.40	Si	>100
1170	(8+9)-VI-4	6	0.01	6.40	Si	>100
1170	(8+9)-VIII-1	-9	0.01	6.40	Si	>100
1170	(8+9)-V-4	11	0.02	6.40	Si	>100
1170	(8+9)-V-3	10	0.02	6.40	Si	>100
1170	(8+9)-IV-4	31	0.05	6.40	Si	>100

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Tx kg	τ_{vd} kg/cm ²	fvd kg/cm ²	Csv	τ_M kg/cm ²	fTd kg/cm ²	Csm	Mecc.	Cs
0	1	-473	-0.83	19.20	23	-0.20	12.00	59	V	23
0	2	-938	-1.66	28.80	17	-0.40	18.00	45	V	17
0	3	-938	-1.66	28.80	17	-0.40	18.00	45	V	17
0	4	-473	-0.83	25.60	31	-0.20	16.00	79	V	31
0	5	-473	-0.83	25.60	31	-0.20	16.00	79	V	31
0	6	-473	-0.83	25.60	31	-0.20	16.00	79	V	31
0	7	-473	-0.83	25.60	31	-0.20	16.00	79	V	31
0	(8+9)-V-4	-2779	-4.91	32.00	6.5	-1.19	20.00	17	V	6.5
0	(8+9)-IV-2	-2836	-5.01	32.00	6.4	-1.21	20.00	17	V	6.4
0	(8+9)-II-4	-2566	-4.53	32.00	7.1	-1.10	20.00	18	V	7.1
0	(8+9)-VI-4	-2871	-5.07	32.00	6.3	-1.23	20.00	16	V	6.3
0	(8+9)-VIII-2	-2531	-4.47	32.00	7.2	-1.08	20.00	18	V	7.2
0	(8+9)-II-2	-2063	-3.64	32.00	8.8	-0.88	20.00	23	V	8.8
0	(8+9)-VII-3	-1356	-2.39	32.00	13	-0.58	20.00	35	V	13

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
0	(8+9)-VIII-4	-3644	-6.44	32.00	5.0	-1.56	20.00	13	V	5.0
0	(8+9)-VII-4	-3012	-5.32	32.00	6.0	-1.29	20.00	16	V	6.0
0	(8+9)-VI-2	-1758	-3.10	32.00	10	-0.75	20.00	27	V	10
0	(8+9)-V-3	-1588	-2.80	32.00	11	-0.68	20.00	29	V	11
0	(8+9)-IV-4	-3340	-5.90	32.00	5.4	-1.43	20.00	14	V	5.4
650	(8+9)-I-2	604	1.07	32.00	30	0.26	20.00	78	V	30
650	(8+9)-I-4	-1934	-3.41	32.00	9.4	-0.83	20.00	24	V	9.4
650	(8+9)-I-3	-905	-1.60	32.00	20	-0.39	20.00	52	V	20
650	(8+9)-III-4	-2141	-3.78	32.00	8.5	-0.91	20.00	22	V	8.5
650	(8+9)-I-1	1632	2.88	32.00	11	0.70	20.00	29	V	11
650	(8+9)-III-1	1839	3.25	32.00	9.9	0.79	20.00	25	V	9.9
650	(8+9)-III-3	-698	-1.23	32.00	26	-0.30	20.00	67	V	26
1300	(8+9)-IV-1	2858	5.05	32.00	6.3	1.22	20.00	16	V	6.3
1300	(8+9)-IV-3	2662	4.70	32.00	6.8	1.14	20.00	18	V	6.8
1300	(8+9)-II-3	1877	3.31	32.00	9.7	0.80	20.00	25	V	9.7
1300	(8+9)-VI-1	2572	4.54	32.00	7.0	1.10	20.00	18	V	7.0
1300	(8+9)-II-1	2073	3.66	32.00	8.7	0.89	20.00	23	V	8.7
1300	(8+9)-VII-1	2848	5.03	32.00	6.4	1.22	20.00	16	V	6.4
1300	(8+9)-VII-2	1216	2.15	32.00	15	0.52	20.00	38	V	15
1300	(8+9)-III-2	-447	-0.79	32.00	41	-0.19	20.00	>100	V	41
1300	(8+9)-V-2	1451	2.56	32.00	12	0.62	20.00	32	V	12
1300	(8+9)-VIII-1	3357	5.93	32.00	5.4	1.43	20.00	14	V	5.4
1300	(8+9)-V-1	2612	4.61	32.00	6.9	1.12	20.00	18	V	6.9
1300	(8+9)-VIII-3	2163	3.82	32.00	8.4	0.92	20.00	22	V	8.4
1300	(8+9)-VI-3	1378	2.43	32.00	13	0.59	20.00	34	V	13
Verifiche nella direzione secondaria										
0	(8+9)-V-1	-2912	-4.63	32.00	6.9	-1.12	20.00	18	V	6.9
0	(8+9)-VIII-1	-3796	-6.03	32.00	5.3	-1.46	20.00	14	V	5.3
0	(8+9)-VI-3	-1433	-2.28	32.00	14	-0.55	20.00	36	V	14
0	(8+9)-VI-2	1786	2.84	32.00	11	0.69	20.00	29	V	11
0	(8+9)-VII-3	1591	2.53	32.00	13	0.61	20.00	33	V	13
0	(8+9)-VI-1	-2868	-4.56	32.00	7.0	-1.10	20.00	18	V	7.0
0	(8+9)-VII-1	-3191	-5.07	32.00	6.3	-1.23	20.00	16	V	6.3
0	(8+9)-VII-4	3545	5.63	32.00	5.7	1.36	20.00	15	V	5.7
0	(8+9)-VII-2	-1238	-1.97	32.00	16	-0.48	20.00	42	V	16
0	(8+9)-VI-4	3221	5.12	32.00	6.3	1.24	20.00	16	V	6.3
0	(8+9)-V-4	3266	5.19	32.00	6.2	1.26	20.00	16	V	6.2
0	(8+9)-V-3	1870	2.97	32.00	11	0.72	20.00	28	V	11
0	(8+9)-V-2	-1516	-2.41	32.00	13	-0.58	20.00	34	V	13
585	1	275	0.44	19.20	44	0.11	12.00	>100	V	44
585	2	543	0.86	28.80	33	0.21	18.00	86	V	33
585	3	543	0.86	28.80	33	0.21	18.00	86	V	33
585	4	275	0.44	25.60	59	0.11	16.00	>100	V	59
585	5	275	0.44	25.60	59	0.11	16.00	>100	V	59
585	6	275	0.44	25.60	59	0.11	16.00	>100	V	59
585	7	275	0.44	25.60	59	0.11	16.00	>100	V	59
585	(8+9)-II-3	-2234	-3.55	32.00	9.0	-0.86	20.00	23	V	9.0
585	(8+9)-VIII-4	4157	6.61	32.00	4.8	1.60	20.00	13	V	4.8
585	(8+9)-IV-3	-3221	-5.12	32.00	6.3	-1.24	20.00	16	V	6.3
585	(8+9)-I-3	-994	-1.58	32.00	20	-0.38	20.00	52	V	20
585	(8+9)-VIII-2	2747	4.37	32.00	7.3	1.06	20.00	19	V	7.3
585	(8+9)-III-3	-1290	-2.05	32.00	16	-0.50	20.00	40	V	16
585	(8+9)-IV-2	3603	5.73	32.00	5.6	1.39	20.00	14	V	5.6
585	(8+9)-II-2	2616	4.16	32.00	7.7	1.01	20.00	20	V	7.7
585	(8+9)-I-2	1376	2.19	32.00	15	0.53	20.00	38	V	15
585	(8+9)-III-2	1672	2.66	32.00	12	0.64	20.00	31	V	12
585	(8+9)-VIII-3	-2365	-3.76	32.00	8.5	-0.91	20.00	22	V	8.5
1170	(8+9)-I-4	1250	1.99	32.00	16	0.48	20.00	42	V	16
1170	(8+9)-I-1	-902	-1.43	32.00	22	-0.35	20.00	58	V	22
1170	(8+9)-II-1	-2244	-3.57	32.00	9.0	-0.86	20.00	23	V	9.0
1170	(8+9)-IV-4	3491	5.55	32.00	5.8	1.34	20.00	15	V	5.8
1170	(8+9)-IV-1	-3144	-5.00	32.00	6.4	-1.21	20.00	17	V	6.4
1170	(8+9)-III-4	1520	2.42	32.00	13	0.58	20.00	34	V	13
1170	(8+9)-III-1	-1172	-1.86	32.00	17	-0.45	20.00	44	V	17

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
1170	(8+9)-II-4	2591	4.12	32.00	7.8	1.00	20.00	20	V	7.8

Verifiche a instabilità

Setto(X)	Comb.	kcrit _c	kcrit _m	λ_{relc}	λ_{relm}	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
(cm)						kg/cm ^q	kg/cm ^q	kg/cm ^q	kg/cm ^q	kg/cm ^q	kg/cm ^q	
2(0.0)	(8+9)-VIII-4	--	--	--	--	0.38	0.18	-1.70	132.00	192.00	192.00	79
3(28.9)	(8+9)-III-2	--	--	--	--	0.41	0.73	1.38	132.00	192.00	192.00	71
4(0.0)	(8+9)-VIII-4	--	--	--	--	2.38	0.54	-9.14	132.00	192.00	192.00	15
5(130.0)	(8+9)-VIII-4	--	--	--	--	2.80	1.08	6.61	132.00	192.00	192.00	16

Parete Xlam 14 - Nodi: [7-5-105-106] - **Crit.Prog.** Criterio di verifica XLAM 0 - **Verificato:**

[Cs=2.226,Comb=(8+9)-IV-2]

Geometria setti

Setto	Crit.	X	L	S	X90	L90	S90
		mm	cm	cm	mm	cm	cm
2	Criterio di verifica XLAM 0	0	387.0	12.1	0	60.0	12.1
		300	387.0	12.1	1935	60.0	12.1
		600	387.0	12.1	3870	60.0	12.1
3	Criterio di verifica XLAM 0	0	387.0	12.1	0	57.9	12.1
		289	387.0	12.1	1935	57.9	12.1
		579	387.0	12.1	3870	57.9	12.1
4	Criterio di verifica XLAM 0	0	90.0	12.1	0	130.0	12.1
		650	90.0	12.1	450	130.0	12.1
		1300	90.0	12.1	900	130.0	12.1
5	Criterio di verifica XLAM 0	0	117.0	12.1	0	130.0	12.1
		650	117.0	12.1	585	130.0	12.1
		1300	117.0	12.1	1170	130.0	12.1

Setto 2: origine (40.6,1953.5,193.5), direzione (0.123439,0.992352,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cm ^q	kg/cm ^q	kg/cm ^q	kg/cm ^q	kg/cm ^q	kg/cm ^q	
0	1	239	-5	-79	0.08	-0.07	-0.04	79.20	115.20	115.20	>100
0	2	442	-11	-184	0.16	-0.14	-0.10	118.80	172.80	172.80	>100
0	3	442	-11	-184	0.16	-0.14	-0.10	118.80	172.80	172.80	>100
0	4	239	-5	-79	0.08	-0.07	-0.04	105.60	153.60	153.60	>100
0	5	239	-5	-79	0.08	-0.07	-0.04	105.60	153.60	153.60	>100
0	6	239	-5	-79	0.08	-0.07	-0.04	105.60	153.60	153.60	>100
0	7	239	-5	-79	0.08	-0.07	-0.04	105.60	153.60	153.60	>100
0	(8+9)-VIII-4	1064	13	-3084	0.38	0.18	-1.70	132.00	192.00	192.00	79
0	(8+9)-IV-1	-173	-19	2543	-0.06	-0.25	1.40	132.00	192.00	192.00	>100
0	(8+9)-V-1	-266	6	2888	-0.09	0.08	1.59	132.00	192.00	192.00	>100
0	(8+9)-VI-1	-584	-16	2012	-0.21	-0.22	1.11	132.00	192.00	192.00	>100
0	(8+9)-VII-1	-310	5	3178	-0.11	0.07	1.75	132.00	192.00	192.00	>100
0	(8+9)-V-2	143	17	2108	0.05	0.22	1.16	132.00	192.00	192.00	>100
0	(8+9)-IV-2	1480	24	-1989	0.53	0.32	-1.10	132.00	192.00	192.00	88
0	(8+9)-VIII-3	-589	-29	1448	-0.21	-0.39	0.80	132.00	192.00	192.00	>100
0	(8+9)-IV-3	-1144	-31	1884	-0.41	-0.41	1.04	132.00	192.00	192.00	>100
0	(8+9)-II-4	366	8	-1681	0.13	0.10	-0.93	132.00	192.00	192.00	>100
0	(8+9)-IV-4	510	12	-2648	0.18	0.16	-1.46	132.00	192.00	192.00	>100
0	(8+9)-VII-4	646	-12	-3283	0.23	-0.16	-1.81	132.00	192.00	192.00	83
0	(8+9)-VI-4	920	9	-2117	0.33	0.12	-1.17	132.00	192.00	192.00	>100
0	(8+9)-VIII-2	926	22	-1553	0.33	0.30	-0.86	132.00	192.00	192.00	>100
0	(8+9)-VIII-1	-727	-20	2979	-0.26	-0.27	1.64	132.00	192.00	192.00	>100
0	(8+9)-VII-3	150	-25	-1924	0.05	-0.33	-1.06	132.00	192.00	192.00	>100
0	(8+9)-II-1	-29	-15	1576	-0.01	-0.20	0.87	132.00	192.00	192.00	>100
0	(8+9)-VII-2	186	18	1818	0.07	0.24	1.00	132.00	192.00	192.00	>100

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-V-3	193	-23	-2214	0.07	-0.31	-1.22	132.00	192.00	192.00	>100
0	(8+9)-V-4	603	-13	-2993	0.21	-0.18	-1.65	132.00	192.00	192.00	90
300	(8+9)-I-2	1294	56	1421	0.46	0.75	0.78	132.00	192.00	192.00	87
300	(8+9)-I-4	-976	-53	-2167	-0.35	-0.71	-1.20	132.00	192.00	192.00	>100
300	(8+9)-III-3	-1216	-66	-1282	-0.43	-0.89	-0.71	132.00	192.00	192.00	>100
300	(8+9)-III-2	1317	58	1118	0.47	0.77	0.62	132.00	192.00	192.00	93
300	(8+9)-I-3	-1194	-65	-1585	-0.42	-0.87	-0.87	132.00	192.00	192.00	>100
300	(8+9)-III-4	-954	-51	-2471	-0.34	-0.68	-1.36	132.00	192.00	192.00	94
300	(8+9)-III-1	1054	43	2307	0.38	0.57	1.27	132.00	192.00	192.00	80
300	(8+9)-I-1	1077	44	2003	0.38	0.59	1.11	132.00	192.00	192.00	85
600	(8+9)-VI-3	-762	-70	659	-0.27	-0.94	0.36	132.00	192.00	192.00	>100
600	(8+9)-II-3	-770	-76	693	-0.27	-1.01	0.38	132.00	192.00	192.00	>100
600	(8+9)-II-2	871	66	-519	0.31	0.88	-0.29	132.00	192.00	192.00	>100
600	(8+9)-VI-2	863	60	-486	0.31	0.81	-0.27	132.00	192.00	192.00	>100
Verifiche nella direzione secondaria											
0	1	-1271	4	165	-4.38	0.70	5.69	79.20	115.20	115.20	18
0	2	-2498	9	309	-8.60	1.85	10.65	118.80	172.80	172.80	13
0	3	-2498	9	309	-8.60	1.85	10.65	118.80	172.80	172.80	13
0	4	-1271	4	165	-4.38	0.70	5.69	105.60	153.60	153.60	24
0	5	-1271	4	165	-4.38	0.70	5.69	105.60	153.60	153.60	24
0	6	-1271	4	165	-4.38	0.70	5.69	105.60	153.60	153.60	24
0	7	-1271	4	165	-4.38	0.70	5.69	105.60	153.60	153.60	24
0	(8+9)-VIII-4	-3749	38	1609	-12.91	7.56	55.39	132.00	192.00	192.00	3.0
0	(8+9)-IV-2	-1340	7	1458	-4.61	1.46	50.20	132.00	192.00	192.00	3.7
0	(8+9)-V-1	4000	-51	-539	13.77	-10.05	-18.57	132.00	192.00	192.00	3.9
0	(8+9)-I-2	2258	-47	270	7.77	-9.34	9.30	132.00	192.00	192.00	6.4
0	(8+9)-V-2	3582	-52	77	12.33	-10.29	2.64	132.00	192.00	192.00	6.2
0	(8+9)-I-4	-4449	51	579	-15.32	10.02	19.93	132.00	192.00	192.00	6.2
0	(8+9)-V-3	-5355	57	156	-18.44	11.21	5.37	132.00	192.00	192.00	10
0	(8+9)-II-2	-577	-14	1097	-1.99	-2.85	37.76	132.00	192.00	192.00	4.7
0	(8+9)-V-4	-5773	56	772	-19.88	10.97	26.58	132.00	192.00	192.00	4.8
0	(8+9)-II-4	-2590	15	1189	-8.92	2.96	40.95	132.00	192.00	192.00	4.3
0	(8+9)-VI-1	1213	-12	-1015	4.18	-2.33	-34.94	132.00	192.00	192.00	4.4
0	(8+9)-III-2	2029	-41	378	6.99	-8.05	13.03	132.00	192.00	192.00	6.1
0	(8+9)-VI-2	-180	-16	1039	-0.62	-3.13	35.77	132.00	192.00	192.00	4.9
0	(8+9)-III-4	-4678	57	687	-16.11	11.31	23.66	132.00	192.00	192.00	5.3
0	(8+9)-VI-3	-1593	21	-806	-5.49	4.05	-27.75	132.00	192.00	192.00	6.0
0	(8+9)-I-1	2676	-46	-346	9.21	-9.10	-11.91	132.00	192.00	192.00	5.6
0	(8+9)-VI-4	-2987	16	1247	-10.29	3.24	42.95	132.00	192.00	192.00	4.1
0	(8+9)-IV-4	-3352	37	1551	-11.54	7.27	53.39	132.00	192.00	192.00	3.1
0	(8+9)-VII-1	4229	-58	-648	14.56	-11.35	-22.30	132.00	192.00	192.00	3.5
0	(8+9)-II-1	816	-10	-957	2.81	-2.04	-32.94	132.00	192.00	192.00	4.9
0	(8+9)-VII-2	3353	-46	185	11.55	-9.00	6.37	132.00	192.00	192.00	6.0
0	(8+9)-III-1	2905	-53	-454	10.00	-10.40	-15.64	132.00	192.00	192.00	4.7
0	(8+9)-VII-3	-5127	50	48	-17.65	9.92	1.64	132.00	192.00	192.00	15
0	(8+9)-IV-1	1579	-32	-1318	5.44	-6.36	-45.38	132.00	192.00	192.00	3.2
0	(8+9)-VII-4	-6002	62	880	-20.67	12.26	30.32	132.00	192.00	192.00	4.3
0	(8+9)-III-3	-3802	46	-146	-13.09	8.97	-5.02	132.00	192.00	192.00	13
0	(8+9)-IV-3	-433	-3	-1225	-1.49	-0.55	-42.19	132.00	192.00	192.00	4.5
0	(8+9)-II-3	-1196	19	-864	-4.12	3.76	-29.75	132.00	192.00	192.00	5.7
0	(8+9)-VIII-1	1976	-34	-1376	6.80	-6.64	-47.38	132.00	192.00	192.00	3.0
0	(8+9)-VIII-2	-943	6	1400	-3.25	1.18	48.21	132.00	192.00	192.00	3.9
0	(8+9)-VIII-3	-831	-1	-1167	-2.86	-0.26	-40.19	132.00	192.00	192.00	4.7
0	(8+9)-I-3	-4031	52	-37	-13.88	10.26	-1.29	132.00	192.00	192.00	15

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Ty kg	τ_d kg/cmq	fvd kg/cmq	RS	Cs
0	1	-5	0.00	3.84	Si	>100
0	2	-12	0.00	5.76	Si	>100
0	3	-12	0.00	5.76	Si	>100
0	4	-5	0.00	5.12	Si	>100
0	5	-5	0.00	5.12	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
0	6	-5	0.00	5.12	Si	>100
0	7	-5	0.00	5.12	Si	>100
0	(8+9)-VIII-4	25	0.01	6.40	Si	>100
0	(8+9)-VIII-1	-31	0.01	6.40	Si	>100
0	(8+9)-VIII-3	-33	0.01	6.40	Si	>100
0	(8+9)-VIII-2	27	0.01	6.40	Si	>100
300	(8+9)-IV-1	35	0.01	6.40	Si	>100
300	(8+9)-V-1	25	0.01	6.40	Si	>100
300	(8+9)-I-2	177	0.05	6.40	Si	>100
300	(8+9)-V-4	-29	0.01	6.40	Si	>100
300	(8+9)-I-4	-177	0.05	6.40	Si	>100
300	(8+9)-IV-2	68	0.02	6.40	Si	>100
300	(8+9)-III-3	-184	0.05	6.40	Si	>100
300	(8+9)-III-4	-174	0.05	6.40	Si	>100
300	(8+9)-I-1	173	0.04	6.40	Si	>100
300	(8+9)-III-2	180	0.05	6.40	Si	>100
300	(8+9)-IV-3	-72	0.02	6.40	Si	>100
300	(8+9)-IV-4	-39	0.01	6.40	Si	>100
300	(8+9)-I-3	-182	0.05	6.40	Si	>100
300	(8+9)-III-1	170	0.04	6.40	Si	>100
600	(8+9)-II-3	-154	0.04	6.40	Si	>100
600	(8+9)-VI-1	-113	0.03	6.40	Si	>100
600	(8+9)-VII-2	39	0.01	6.40	Si	>100
600	(8+9)-II-4	90	0.02	6.40	Si	>100
600	(8+9)-VII-3	-43	0.01	6.40	Si	>100
600	(8+9)-VI-2	131	0.03	6.40	Si	>100
600	(8+9)-VII-4	-35	0.01	6.40	Si	>100
600	(8+9)-V-3	-76	0.02	6.40	Si	>100
600	(8+9)-VI-3	-136	0.04	6.40	Si	>100
600	(8+9)-VII-1	31	0.01	6.40	Si	>100
600	(8+9)-II-1	-95	0.02	6.40	Si	>100
600	(8+9)-V-2	72	0.02	6.40	Si	>100
600	(8+9)-II-2	150	0.04	6.40	Si	>100
600	(8+9)-VI-4	109	0.03	6.40	Si	>100
Verifiche nella direzione secondaria						
0	(8+9)-VIII-4	-51	0.16	6.40	Si	39
0	(8+9)-V-4	-69	0.22	6.40	Si	29
0	(8+9)-II-4	-39	0.12	6.40	Si	51
0	(8+9)-III-1	35	0.11	6.40	Si	58
0	(8+9)-VIII-1	42	0.13	6.40	Si	48
0	(8+9)-VI-1	38	0.12	6.40	Si	53
0	(8+9)-VII-3	-53	0.17	6.40	Si	38
0	(8+9)-III-3	-26	0.08	6.40	Si	77
0	(8+9)-I-1	34	0.11	6.40	Si	60
0	(8+9)-III-4	-44	0.14	6.40	Si	46
0	(8+9)-I-3	-27	0.09	6.40	Si	74
0	(8+9)-IV-1	34	0.11	6.40	Si	59
0	(8+9)-II-1	30	0.10	6.40	Si	66
0	(8+9)-V-3	-54	0.17	6.40	Si	37
0	(8+9)-VI-4	-47	0.15	6.40	Si	43
0	(8+9)-II-3	12	0.04	6.40	Si	>100
0	(8+9)-VII-4	-70	0.22	6.40	Si	29
0	(8+9)-IV-3	16	0.05	6.40	Si	>100
0	(8+9)-VII-1	62	0.20	6.40	Si	33
0	(8+9)-V-2	45	0.14	6.40	Si	45
0	(8+9)-VII-2	44	0.14	6.40	Si	46
0	(8+9)-I-4	-43	0.14	6.40	Si	47
0	(8+9)-IV-4	-43	0.14	6.40	Si	47
0	(8+9)-V-1	60	0.19	6.40	Si	33
1935	(8+9)-VIII-3	-12	0.04	6.40	Si	>100
3870	1	-16	0.05	3.84	Si	75
3870	2	-34	0.11	5.76	Si	53
3870	3	-34	0.11	5.76	Si	53
3870	4	-16	0.05	5.12	Si	99

X	Comb.	Ty	τ_d	fvd	RS	Cs
3870	5	-16	0.05	5.12	Si	99
3870	6	-16	0.05	5.12	Si	99
3870	7	-16	0.05	5.12	Si	99
3870	(8+9)-IV-2	-32	0.10	6.40	Si	63
3870	(8+9)-I-2	-25	0.08	6.40	Si	81
3870	(8+9)-II-2	-32	0.10	6.40	Si	63
3870	(8+9)-VI-3	10	0.03	6.40	Si	>100
3870	(8+9)-VIII-2	-32	0.10	6.40	Si	63
3870	(8+9)-VI-2	-32	0.10	6.40	Si	63
3870	(8+9)-III-2	-25	0.08	6.40	Si	82

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	(8+9)-I-2	1433	0.77	32.00	42	0.19	20.00	>100	V	42
0	(8+9)-III-2	951	0.51	32.00	63	0.12	20.00	>100	V	63
300	1	-920	-0.49	19.20	39	-0.12	12.00	>100	V	39
300	2	-1791	-0.96	28.80	30	-0.23	18.00	78	V	30
300	3	-1791	-0.96	28.80	30	-0.23	18.00	78	V	30
300	4	-920	-0.49	25.60	52	-0.12	16.00	>100	V	52
300	5	-920	-0.49	25.60	52	-0.12	16.00	>100	V	52
300	6	-920	-0.49	25.60	52	-0.12	16.00	>100	V	52
300	7	-920	-0.49	25.60	52	-0.12	16.00	>100	V	52
300	(8+9)-V-4	-7352	-3.93	32.00	8.2	-0.95	20.00	21	V	8.2
300	(8+9)-II-2	-5113	-2.73	32.00	12	-0.66	20.00	30	V	12
300	(8+9)-III-3	-1685	-0.90	32.00	36	-0.22	20.00	92	V	36
300	(8+9)-I-4	-5081	-2.71	32.00	12	-0.66	20.00	30	V	12
300	(8+9)-VI-4	-7499	-4.00	32.00	8.0	-0.97	20.00	21	V	8.0
300	(8+9)-VII-3	-3956	-2.11	32.00	15	-0.51	20.00	39	V	15
300	(8+9)-II-4	-6818	-3.64	32.00	8.8	-0.88	20.00	23	V	8.8
300	(8+9)-VI-3	3146	1.68	32.00	19	0.41	20.00	49	V	19
300	(8+9)-I-1	3797	2.03	32.00	16	0.49	20.00	41	V	16
300	(8+9)-II-3	3828	2.04	32.00	16	0.49	20.00	40	V	16
300	(8+9)-VII-2	2671	1.43	32.00	22	0.35	20.00	58	V	22
300	(8+9)-II-1	5533	2.95	32.00	11	0.71	20.00	28	V	11
300	(8+9)-VI-2	-4431	-2.37	32.00	14	-0.57	20.00	35	V	14
300	(8+9)-VI-1	6214	3.32	32.00	9.6	0.80	20.00	25	V	9.6
300	(8+9)-V-1	6068	3.24	32.00	9.9	0.78	20.00	26	V	9.9
600	(8+9)-VIII-4	-11056	-5.90	32.00	5.4	-1.43	20.00	14	V	5.4
600	(8+9)-IV-1	9360	5.00	32.00	6.4	1.21	20.00	17	V	6.4
600	(8+9)-III-1	5170	2.76	32.00	12	0.67	20.00	30	V	12
600	(8+9)-V-3	-4358	-2.33	32.00	14	-0.56	20.00	36	V	14
600	(8+9)-I-3	-2403	-1.28	32.00	25	-0.31	20.00	64	V	25
600	(8+9)-IV-4	-10469	-5.59	32.00	5.7	-1.35	20.00	15	V	5.7
600	(8+9)-VII-4	-8234	-4.40	32.00	7.3	-1.06	20.00	19	V	7.3
600	(8+9)-VII-1	7125	3.80	32.00	8.4	0.92	20.00	22	V	8.4
600	(8+9)-V-2	3249	1.73	32.00	18	0.42	20.00	48	V	18
600	(8+9)-IV-3	7547	4.03	32.00	7.9	0.98	20.00	21	V	7.9
600	(8+9)-III-4	-6279	-3.35	32.00	9.5	-0.81	20.00	25	V	9.5
600	(8+9)-VIII-1	9947	5.31	32.00	6.0	1.29	20.00	16	V	6.0
600	(8+9)-VIII-2	-8070	-4.31	32.00	7.4	-1.04	20.00	19	V	7.4
600	(8+9)-VIII-3	6961	3.72	32.00	8.6	0.90	20.00	22	V	8.6
600	(8+9)-IV-2	-8656	-4.62	32.00	6.9	-1.12	20.00	18	V	6.9
Verifiche nella direzione secondaria										
0	1	263	0.90	19.20	21	0.22	12.00	55	V	21
0	2	516	1.78	28.80	16	0.43	18.00	42	V	16
0	3	516	1.78	28.80	16	0.43	18.00	42	V	16
0	4	263	0.90	25.60	28	0.22	16.00	73	V	28
0	5	263	0.90	25.60	28	0.22	16.00	73	V	28
0	6	263	0.90	25.60	28	0.22	16.00	73	V	28
0	7	263	0.90	25.60	28	0.22	16.00	73	V	28
1935	(8+9)-VIII-4	2245	7.73	32.00	4.1	1.87	20.00	11	V	4.1
1935	(8+9)-IV-2	1504	5.18	32.00	6.2	1.25	20.00	16	V	6.2

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
1935	(8+9)-V-1	-1626	-5.60	32.00	5.7	-1.36	20.00	15	V	5.7
1935	(8+9)-I-2	-588	-2.03	32.00	16	-0.49	20.00	41	V	16
1935	(8+9)-V-2	-916	-3.15	32.00	10	-0.76	20.00	26	V	10
1935	(8+9)-I-4	1554	5.35	32.00	6.0	1.29	20.00	15	V	6.0
1935	(8+9)-V-3	1171	4.03	32.00	7.9	0.98	20.00	20	V	7.9
1935	(8+9)-II-2	990	3.41	32.00	9.4	0.82	20.00	24	V	9.4
1935	(8+9)-V-4	1881	6.48	32.00	4.9	1.57	20.00	13	V	4.9
1935	(8+9)-II-4	1632	5.62	32.00	5.7	1.36	20.00	15	V	5.7
1935	(8+9)-VI-1	-1475	-5.08	32.00	6.3	-1.23	20.00	16	V	6.3
1935	(8+9)-III-2	-434	-1.50	32.00	21	-0.36	20.00	55	V	21
1935	(8+9)-VI-2	891	3.07	32.00	10	0.74	20.00	27	V	10
1935	(8+9)-III-4	1708	5.88	32.00	5.4	1.42	20.00	14	V	5.4
1935	(8+9)-VI-3	-636	-2.19	32.00	15	-0.53	20.00	38	V	15
1935	(8+9)-I-1	-1299	-4.47	32.00	7.2	-1.08	20.00	18	V	7.2
1935	(8+9)-VI-4	1731	5.96	32.00	5.4	1.44	20.00	14	V	5.4
1935	(8+9)-IV-4	2146	7.39	32.00	4.3	1.79	20.00	11	V	4.3
1935	(8+9)-VII-1	-1780	-6.13	32.00	5.2	-1.48	20.00	13	V	5.2
1935	(8+9)-II-1	-1377	-4.74	32.00	6.7	-1.15	20.00	17	V	6.7
1935	(8+9)-VII-2	-762	-2.62	32.00	12	-0.63	20.00	32	V	12
1935	(8+9)-III-1	-1453	-5.00	32.00	6.4	-1.21	20.00	17	V	6.4
1935	(8+9)-VII-3	1017	3.50	32.00	9.1	0.85	20.00	24	V	9.1
1935	(8+9)-IV-1	-1891	-6.51	32.00	4.9	-1.58	20.00	13	V	4.9
1935	(8+9)-VII-4	2035	7.01	32.00	4.6	1.70	20.00	12	V	4.6
1935	(8+9)-III-3	689	2.37	32.00	13	0.57	20.00	35	V	13
1935	(8+9)-IV-3	-1249	-4.30	32.00	7.4	-1.04	20.00	19	V	7.4
1935	(8+9)-II-3	-735	-2.53	32.00	13	-0.61	20.00	33	V	13
1935	(8+9)-VIII-1	-1989	-6.85	32.00	4.7	-1.66	20.00	12	V	4.7
1935	(8+9)-VIII-2	1405	4.84	32.00	6.6	1.17	20.00	17	V	6.6
1935	(8+9)-VIII-3	-1150	-3.96	32.00	8.1	-0.96	20.00	21	V	8.1
1935	(8+9)-I-3	844	2.90	32.00	11	0.70	20.00	28	V	11

Setto 3: origine (17.4,1767.0,193.5), direzione (0.123439,0.992352,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_N	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	(8+9)-VII-4	-574	-80	-583	-0.20	-1.08	-0.32	132.00	192.00	192.00	>100
0	(8+9)-VII-1	741	92	801	0.26	1.23	0.44	132.00	192.00	192.00	93
0	(8+9)-V-1	706	88	779	0.25	1.18	0.43	132.00	192.00	192.00	97
0	(8+9)-V-4	-540	-76	-561	-0.19	-1.02	-0.31	132.00	192.00	192.00	>100
0	(8+9)-V-2	748	90	747	0.27	1.20	0.41	132.00	192.00	192.00	96
0	(8+9)-VII-2	714	85	724	0.25	1.14	0.40	132.00	192.00	192.00	>100
0	(8+9)-VII-3	-547	-74	-507	-0.19	-0.99	-0.28	132.00	192.00	192.00	>100
0	(8+9)-V-3	-582	-78	-529	-0.21	-1.04	-0.29	132.00	192.00	192.00	>100
289	(8+9)-II-3	-178	0	-2065	-0.06	0.01	-1.14	132.00	192.00	192.00	>100
289	(8+9)-III-3	-992	-49	-2085	-0.35	-0.65	-1.15	132.00	192.00	192.00	>100
289	(8+9)-I-3	-1014	-50	-2024	-0.36	-0.67	-1.12	132.00	192.00	192.00	>100
289	(8+9)-III-4	-1080	-60	-905	-0.38	-0.80	-0.50	132.00	192.00	192.00	>100
289	(8+9)-I-2	1180	56	2441	0.42	0.75	1.35	132.00	192.00	192.00	71
289	(8+9)-I-1	1225	65	1384	0.44	0.87	0.76	132.00	192.00	192.00	85
289	(8+9)-II-2	344	5	2482	0.12	0.07	1.37	132.00	192.00	192.00	>100
289	(8+9)-III-1	1246	66	1322	0.44	0.88	0.73	132.00	192.00	192.00	85
289	(8+9)-III-2	1158	55	2503	0.41	0.73	1.38	132.00	192.00	192.00	71
289	(8+9)-I-4	-1058	-59	-966	-0.38	-0.79	-0.53	132.00	192.00	192.00	>100
579	1	247	2	329	0.09	0.02	0.18	79.20	115.20	115.20	>100
579	2	459	3	616	0.16	0.04	0.34	118.80	172.80	172.80	>100
579	3	459	3	616	0.16	0.04	0.34	118.80	172.80	172.80	>100
579	4	247	2	329	0.09	0.02	0.18	105.60	153.60	153.60	>100
579	5	247	2	329	0.09	0.02	0.18	105.60	153.60	153.60	>100
579	6	247	2	329	0.09	0.02	0.18	105.60	153.60	153.60	>100
579	7	247	2	329	0.09	0.02	0.18	105.60	153.60	153.60	>100
579	(8+9)-VIII-4	-263	-22	2884	-0.09	-0.29	1.59	132.00	192.00	192.00	>100
579	(8+9)-IV-1	1013	21	-2040	0.36	0.29	-1.13	132.00	192.00	192.00	99
579	(8+9)-IV-2	292	-16	2585	0.10	-0.21	1.43	132.00	192.00	192.00	>100

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
579	(8+9)-IV-4	-665	-19	2503	-0.24	-0.26	1.38	132.00	192.00	192.00	>100
579	(8+9)-II-4	-506	-18	1921	-0.18	-0.24	1.06	132.00	192.00	192.00	>100
579	(8+9)-VI-2	49	-12	1622	0.02	-0.16	0.90	132.00	192.00	192.00	>100
579	(8+9)-II-1	854	20	-1458	0.30	0.27	-0.80	132.00	192.00	192.00	>100
579	(8+9)-VI-1	452	23	-1839	0.16	0.30	-1.01	132.00	192.00	192.00	>100
579	(8+9)-VI-3	299	14	-1159	0.11	0.19	-0.64	132.00	192.00	192.00	>100
579	(8+9)-IV-3	56	18	-2122	0.02	0.24	-1.17	132.00	192.00	192.00	>100
579	(8+9)-VIII-1	611	24	-2421	0.22	0.32	-1.34	132.00	192.00	192.00	97
579	(8+9)-VIII-2	-110	-13	2204	-0.04	-0.18	1.22	132.00	192.00	192.00	>100
579	(8+9)-VIII-3	458	16	-1741	0.16	0.21	-0.96	132.00	192.00	192.00	>100
579	(8+9)-VI-4	-104	-20	2302	-0.04	-0.27	1.27	132.00	192.00	192.00	>100
Verifiche nella direzione secondaria											
0	1	-572	-8	-62	-2.04	-1.67	-2.29	79.20	115.20	115.20	29
0	2	-1095	-14	-102	-3.91	-2.84	-3.79	118.80	172.80	172.80	26
0	3	-1095	-14	-102	-3.91	-2.84	-3.79	118.80	172.80	172.80	26
0	4	-572	-8	-62	-2.04	-1.67	-2.29	105.60	153.60	153.60	39
0	5	-572	-8	-62	-2.04	-1.67	-2.29	105.60	153.60	153.60	39
0	6	-572	-8	-62	-2.04	-1.67	-2.29	105.60	153.60	153.60	39
0	7	-572	-8	-62	-2.04	-1.67	-2.29	105.60	153.60	153.60	39
0	(8+9)-VIII-4	4641	-40	1212	16.56	-8.17	44.83	132.00	192.00	192.00	2.5
0	(8+9)-IV-2	5989	-76	1070	21.37	-15.58	39.58	132.00	192.00	192.00	2.2
0	(8+9)-V-1	-1018	-37	-1182	-3.63	-7.47	-43.72	132.00	192.00	192.00	3.7
0	(8+9)-I-2	4709	-96	620	16.80	-19.61	22.93	132.00	192.00	192.00	2.9
0	(8+9)-V-2	1697	-80	-785	6.06	-16.44	-29.04	132.00	192.00	192.00	3.5
0	(8+9)-I-4	-2798	40	-312	-9.98	8.26	-11.55	132.00	192.00	192.00	9.4
0	(8+9)-V-3	-2501	69	696	-8.93	14.05	25.74	132.00	192.00	192.00	4.8
0	(8+9)-II-2	5249	-100	757	18.73	-20.32	27.99	132.00	192.00	192.00	2.5
0	(8+9)-V-4	214	25	1093	0.76	5.08	40.42	132.00	192.00	192.00	4.1
0	(8+9)-II-4	2997	-59	477	10.70	-11.95	17.65	132.00	192.00	192.00	4.3
0	(8+9)-VI-1	-4705	52	-988	-16.79	10.52	-36.54	132.00	192.00	192.00	4.0
0	(8+9)-III-2	4931	-89	714	17.60	-18.19	26.41	132.00	192.00	192.00	2.7
0	(8+9)-VI-2	4345	-95	335	15.51	-19.36	12.40	132.00	192.00	192.00	3.5
0	(8+9)-III-4	-2576	47	-218	-9.19	9.68	-8.08	132.00	192.00	192.00	11
0	(8+9)-VI-3	-5150	83	-425	-18.38	16.97	-15.70	132.00	192.00	192.00	5.6
0	(8+9)-I-1	1994	-52	223	7.11	-10.65	8.25	132.00	192.00	192.00	6.6
0	(8+9)-VI-4	3901	-63	899	13.92	-12.91	33.24	132.00	192.00	192.00	2.9
0	(8+9)-IV-4	3737	-35	791	13.34	-7.22	29.24	132.00	192.00	192.00	3.4
0	(8+9)-VII-1	-1240	-44	-1276	-4.43	-8.89	-47.20	132.00	192.00	192.00	3.4
0	(8+9)-II-1	-3801	47	-566	-13.57	9.56	-20.95	132.00	192.00	192.00	6.1
0	(8+9)-VII-2	1919	-74	-691	6.85	-15.01	-25.56	132.00	192.00	192.00	3.8
0	(8+9)-III-1	1772	-59	129	6.32	-12.07	4.77	132.00	192.00	192.00	7.4
0	(8+9)-VII-3	-2723	62	602	-9.72	12.63	22.26	132.00	192.00	192.00	5.4
0	(8+9)-IV-1	-4541	24	-880	-16.21	4.83	-32.54	132.00	192.00	192.00	5.0
0	(8+9)-VII-4	436	32	1187	1.56	6.50	43.90	132.00	192.00	192.00	3.6
0	(8+9)-III-3	-5735	77	-803	-20.47	15.80	-29.71	132.00	192.00	192.00	4.0
0	(8+9)-IV-3	-6793	65	-1160	-24.24	13.19	-42.89	132.00	192.00	192.00	3.2
0	(8+9)-II-3	-6053	88	-846	-21.60	17.93	-31.30	132.00	192.00	192.00	3.7
0	(8+9)-VIII-1	-5445	28	-1301	-19.43	5.78	-48.13	132.00	192.00	192.00	3.4
0	(8+9)-VIII-2	5085	-72	649	18.15	-14.63	23.99	132.00	192.00	192.00	3.0
0	(8+9)-VIII-3	-5890	60	-738	-21.02	12.24	-27.30	132.00	192.00	192.00	4.6
0	(8+9)-I-3	-5513	84	-709	-19.67	17.23	-26.24	132.00	192.00	192.00	4.2

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
0	(8+9)-V-1	-69	0.02	6.40	Si	>100
0	(8+9)-VII-4	50	0.01	6.40	Si	>100
0	(8+9)-VII-1	-70	0.02	6.40	Si	>100
0	(8+9)-VIII-3	32	0.01	6.40	Si	>100
0	(8+9)-VII-3	63	0.02	6.40	Si	>100
0	(8+9)-VIII-2	-51	0.01	6.40	Si	>100
0	(8+9)-VI-2	-55	0.01	6.40	Si	>100
0	(8+9)-V-2	-84	0.02	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
0	(8+9)-V-4	49	0.01	6.40	Si	>100
0	(8+9)-VI-3	36	0.01	6.40	Si	>100
0	(8+9)-V-3	64	0.02	6.40	Si	>100
0	(8+9)-VII-2	-83	0.02	6.40	Si	>100
289	1	-14	0.00	3.84	Si	>100
289	2	-25	0.01	5.76	Si	>100
289	3	-25	0.01	5.76	Si	>100
289	4	-14	0.00	5.12	Si	>100
289	5	-14	0.00	5.12	Si	>100
289	6	-14	0.00	5.12	Si	>100
289	7	-14	0.00	5.12	Si	>100
289	(8+9)-VIII-4	-28	0.01	6.40	Si	>100
289	(8+9)-IV-1	-72	0.02	6.40	Si	>100
289	(8+9)-II-3	87	0.02	6.40	Si	>100
289	(8+9)-IV-2	-103	0.03	6.40	Si	>100
289	(8+9)-VI-4	-32	0.01	6.40	Si	>100
289	(8+9)-IV-4	53	0.01	6.40	Si	>100
289	(8+9)-II-2	-106	0.03	6.40	Si	>100
289	(8+9)-III-3	254	0.07	6.40	Si	97
289	(8+9)-II-1	-69	0.02	6.40	Si	>100
289	(8+9)-III-1	-264	0.07	6.40	Si	94
289	(8+9)-I-4	243	0.06	6.40	Si	>100
289	(8+9)-II-4	49	0.01	6.40	Si	>100
289	(8+9)-I-3	255	0.07	6.40	Si	97
289	(8+9)-VI-1	12	0.00	6.40	Si	>100
289	(8+9)-IV-3	83	0.02	6.40	Si	>100
289	(8+9)-III-2	-273	0.07	6.40	Si	90
289	(8+9)-III-4	245	0.06	6.40	Si	>100
289	(8+9)-I-2	-275	0.07	6.40	Si	90
289	(8+9)-I-1	-263	0.07	6.40	Si	94
579	(8+9)-VIII-1	-13	0.00	6.40	Si	>100
Verifiche nella direzione secondaria						
0	1	18	0.06	3.84	Si	63
0	2	32	0.11	5.76	Si	54
0	3	32	0.11	5.76	Si	54
0	4	18	0.06	5.12	Si	84
0	5	18	0.06	5.12	Si	84
0	6	18	0.06	5.12	Si	84
0	7	18	0.06	5.12	Si	84
0	(8+9)-VIII-4	123	0.41	6.40	Si	16
0	(8+9)-IV-2	189	0.62	6.40	Si	10
0	(8+9)-I-2	245	0.81	6.40	Si	7.9
0	(8+9)-V-2	57	0.19	6.40	Si	34
0	(8+9)-I-4	-161	0.53	6.40	Si	12
0	(8+9)-V-3	-31	0.10	6.40	Si	63
0	(8+9)-II-2	170	0.56	6.40	Si	11
0	(8+9)-VIII-1	-97	0.32	6.40	Si	20
0	(8+9)-II-3	-144	0.47	6.40	Si	13
0	(8+9)-II-4	49	0.16	6.40	Si	40
0	(8+9)-III-2	251	0.83	6.40	Si	7.8
0	(8+9)-VI-1	-79	0.26	6.40	Si	25
0	(8+9)-III-4	-155	0.51	6.40	Si	13
0	(8+9)-VI-2	114	0.38	6.40	Si	17
0	(8+9)-I-1	187	0.62	6.40	Si	10
0	(8+9)-VI-3	-88	0.29	6.40	Si	22
0	(8+9)-IV-4	67	0.22	6.40	Si	29
0	(8+9)-VIII-2	132	0.44	6.40	Si	15
0	(8+9)-I-3	-219	0.72	6.40	Si	8.9
0	(8+9)-VI-4	105	0.35	6.40	Si	19
0	(8+9)-III-3	-224	0.74	6.40	Si	8.7
0	(8+9)-IV-3	-162	0.54	6.40	Si	12
0	(8+9)-III-1	182	0.60	6.40	Si	11
0	(8+9)-IV-1	-41	0.13	6.40	Si	48
0	(8+9)-VIII-3	-106	0.35	6.40	Si	18

X	Comb.	Ty	τ_d	fvd	RS	Cs
0	(8+9)-VII-2	63	0.21	6.40	Si	31
0	(8+9)-VII-3	-37	0.12	6.40	Si	53
1935	(8+9)-II-1	33	0.11	6.40	Si	58
3870	(8+9)-V-1	-35	0.12	6.40	Si	55
3870	(8+9)-VII-4	44	0.14	6.40	Si	44
3870	(8+9)-VII-1	-38	0.13	6.40	Si	51
3870	(8+9)-V-4	41	0.13	6.40	Si	48

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	1	-502	-0.27	19.20	72	-0.06	12.00	>100	V	72
0	2	-950	-0.51	28.80	57	-0.12	18.00	>100	V	57
0	3	-950	-0.51	28.80	57	-0.12	18.00	>100	V	57
0	4	-502	-0.27	25.60	96	-0.06	16.00	>100	V	96
0	5	-502	-0.27	25.60	96	-0.06	16.00	>100	V	96
0	6	-502	-0.27	25.60	96	-0.06	16.00	>100	V	96
0	7	-502	-0.27	25.60	96	-0.06	16.00	>100	V	96
0	(8+9)-III-4	1456	0.78	32.00	41	0.19	20.00	>100	V	41
0	(8+9)-I-3	5152	2.75	32.00	12	0.67	20.00	30	V	12
0	(8+9)-VI-2	-5138	-2.74	32.00	12	-0.66	20.00	30	V	12
0	(8+9)-I-4	1983	1.06	32.00	30	0.26	20.00	78	V	30
0	(8+9)-VI-3	4435	2.37	32.00	14	0.57	20.00	35	V	14
0	(8+9)-II-2	-6810	-3.64	32.00	8.8	-0.88	20.00	23	V	8.8
0	(8+9)-I-1	-2686	-1.43	32.00	22	-0.35	20.00	58	V	22
0	(8+9)-I-2	-5855	-3.13	32.00	10	-0.76	20.00	26	V	10
0	(8+9)-III-1	-2160	-1.15	32.00	28	-0.28	20.00	72	V	28
0	(8+9)-III-2	-6382	-3.41	32.00	9.4	-0.82	20.00	24	V	9.4
289	(8+9)-IV-2	-9750	-5.21	32.00	6.1	-1.26	20.00	16	V	6.1
289	(8+9)-II-1	4022	2.15	32.00	15	0.52	20.00	38	V	15
289	(8+9)-III-3	5826	3.11	32.00	10	0.75	20.00	27	V	10
289	(8+9)-VI-4	-7106	-3.79	32.00	8.4	-0.92	20.00	22	V	8.4
289	(8+9)-II-4	-4560	-2.43	32.00	13	-0.59	20.00	34	V	13
289	(8+9)-IV-3	9212	4.92	32.00	6.5	1.19	20.00	17	V	6.5
289	(8+9)-VIII-1	9615	5.13	32.00	6.2	1.24	20.00	16	V	6.2
289	(8+9)-VIII-3	6666	3.56	32.00	9.0	0.86	20.00	23	V	9.0
289	(8+9)-VIII-2	-7204	-3.85	32.00	8.3	-0.93	20.00	21	V	8.3
289	(8+9)-VIII-4	-10153	-5.42	32.00	5.9	-1.31	20.00	15	V	5.9
289	(8+9)-VI-1	6568	3.51	32.00	9.1	0.85	20.00	24	V	9.1
289	(8+9)-II-3	6165	3.29	32.00	9.7	0.80	20.00	25	V	9.7
289	(8+9)-IV-1	7069	3.77	32.00	8.5	0.91	20.00	22	V	8.5
289	(8+9)-IV-4	-7607	-4.06	32.00	7.9	-0.98	20.00	20	V	7.9
579	(8+9)-VII-1	7865	4.20	32.00	7.6	1.02	20.00	20	V	7.6
579	(8+9)-V-3	-5845	-3.12	32.00	10	-0.76	20.00	26	V	10
579	(8+9)-VII-2	4454	2.38	32.00	13	0.58	20.00	35	V	13
579	(8+9)-VII-4	-8473	-4.52	32.00	7.1	-1.09	20.00	18	V	7.1
579	(8+9)-V-4	-7689	-4.11	32.00	7.8	-0.99	20.00	20	V	7.8
579	(8+9)-VII-3	-5062	-2.70	32.00	12	-0.65	20.00	31	V	12
579	(8+9)-V-2	5237	2.80	32.00	11	0.68	20.00	30	V	11
579	(8+9)-V-1	7082	3.78	32.00	8.5	0.91	20.00	22	V	8.5
Verifiche nella direzione secondaria										
0	(8+9)-III-4	-456	-1.63	32.00	20	-0.39	20.00	51	V	20
1935	(8+9)-VIII-4	2181	7.78	32.00	4.1	1.88	20.00	11	V	4.1
1935	(8+9)-VII-2	-618	-2.21	32.00	15	-0.53	20.00	37	V	15
1935	(8+9)-III-3	-1493	-5.33	32.00	6.0	-1.29	20.00	16	V	6.0
1935	(8+9)-IV-2	2131	7.60	32.00	4.2	1.84	20.00	11	V	4.2
1935	(8+9)-VII-3	774	2.76	32.00	12	0.67	20.00	30	V	12
1935	(8+9)-VIII-2	1451	5.18	32.00	6.2	1.25	20.00	16	V	6.2
1935	(8+9)-IV-1	-1345	-4.80	32.00	6.7	-1.16	20.00	17	V	6.7
1935	(8+9)-VII-4	1817	6.48	32.00	4.9	1.57	20.00	13	V	4.9
1935	(8+9)-I-2	1511	5.39	32.00	5.9	1.30	20.00	15	V	5.9
1935	(8+9)-IV-3	-1975	-7.05	32.00	4.5	-1.71	20.00	12	V	4.5
1935	(8+9)-I-4	-588	-2.10	32.00	15	-0.51	20.00	39	V	15

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
1935	(8+9)-IV-4	1501	5.36	32.00	6.0	1.30	20.00	15	V	6.0
1935	(8+9)-II-2	1670	5.96	32.00	5.4	1.44	20.00	14	V	5.4
1935	(8+9)-V-1	-1522	-5.43	32.00	5.9	-1.31	20.00	15	V	5.9
1935	(8+9)-II-4	1040	3.71	32.00	8.6	0.90	20.00	22	V	8.6
1935	(8+9)-V-2	-756	-2.70	32.00	12	-0.65	20.00	31	V	12
1935	(8+9)-III-2	1649	5.88	32.00	5.4	1.42	20.00	14	V	5.4
1935	(8+9)-V-3	912	3.26	32.00	9.8	0.79	20.00	25	V	9.8
1935	(8+9)-VIII-1	-2025	-7.23	32.00	4.4	-1.75	20.00	11	V	4.4
1935	(8+9)-V-4	1678	5.99	32.00	5.3	1.45	20.00	14	V	5.3
1935	(8+9)-I-3	-1354	-4.83	32.00	6.6	-1.17	20.00	17	V	6.6
1935	(8+9)-VI-1	-1564	-5.58	32.00	5.7	-1.35	20.00	15	V	5.7
1935	(8+9)-II-3	-1514	-5.40	32.00	5.9	-1.31	20.00	15	V	5.9
1935	(8+9)-VI-2	990	3.53	32.00	9.1	0.85	20.00	23	V	9.1
1935	(8+9)-VIII-3	-1295	-4.62	32.00	6.9	-1.12	20.00	18	V	6.9
1935	(8+9)-II-1	-884	-3.15	32.00	10	-0.76	20.00	26	V	10
1935	(8+9)-III-1	606	2.16	32.00	15	0.52	20.00	38	V	15
1935	(8+9)-I-1	744	2.66	32.00	12	0.64	20.00	31	V	12
1935	(8+9)-VI-3	-834	-2.98	32.00	11	-0.72	20.00	28	V	11
1935	(8+9)-VI-4	1720	6.14	32.00	5.2	1.49	20.00	13	V	5.2
1935	(8+9)-VII-1	-1661	-5.93	32.00	5.4	-1.43	20.00	14	V	5.4
3870	1	167	0.60	19.20	32	0.14	12.00	83	V	32
3870	2	328	1.17	28.80	25	0.28	18.00	64	V	25
3870	3	328	1.17	28.80	25	0.28	18.00	64	V	25
3870	4	167	0.60	25.60	43	0.14	16.00	>100	V	43
3870	5	167	0.60	25.60	43	0.14	16.00	>100	V	43
3870	6	167	0.60	25.60	43	0.14	16.00	>100	V	43
3870	7	167	0.60	25.60	43	0.14	16.00	>100	V	43

Setto 4: origine (24.5,1824.5,45.0), direzione (0.123439,0.992352,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	1	268	2	-45	0.41	0.12	-0.46	79.20	115.20	115.20	98
0	2	506	4	-89	0.77	0.24	-0.91	118.80	172.80	172.80	76
0	3	506	4	-89	0.77	0.24	-0.91	118.80	172.80	172.80	76
0	4	268	2	-45	0.41	0.12	-0.46	105.60	153.60	153.60	>100
0	5	268	2	-45	0.41	0.12	-0.46	105.60	153.60	153.60	>100
0	6	268	2	-45	0.41	0.12	-0.46	105.60	153.60	153.60	>100
0	7	268	2	-45	0.41	0.12	-0.46	105.60	153.60	153.60	>100
0	(8+9)-V-3	433	6	-375	0.66	0.32	-3.83	132.00	192.00	192.00	38
0	(8+9)-VII-4	1079	8	-746	1.65	0.49	-7.61	132.00	192.00	192.00	18
0	(8+9)-VI-4	1290	6	-701	1.97	0.36	-7.15	132.00	192.00	192.00	18
0	(8+9)-I-2	1340	7	-511	2.05	0.41	-5.22	132.00	192.00	192.00	22
0	(8+9)-III-2	1420	8	-570	2.17	0.46	-5.81	132.00	192.00	192.00	20
0	(8+9)-VIII-2	1242	6	-596	1.90	0.37	-6.08	132.00	192.00	192.00	21
0	(8+9)-III-3	-1042	-5	508	-1.60	-0.29	5.18	132.00	192.00	192.00	35
0	(8+9)-II-2	1392	6	-648	2.13	0.35	-6.61	132.00	192.00	192.00	19
0	(8+9)-VI-2	974	3	-401	1.49	0.19	-4.09	132.00	192.00	192.00	30
0	(8+9)-VIII-4	1558	9	-896	2.38	0.54	-9.14	132.00	192.00	192.00	15
0	(8+9)-II-3	-1015	-3	586	-1.55	-0.18	5.98	132.00	192.00	192.00	31
0	(8+9)-I-3	-962	-4	449	-1.47	-0.23	4.58	132.00	192.00	192.00	40
0	(8+9)-V-4	998	8	-687	1.53	0.43	-7.01	132.00	192.00	192.00	20
0	(8+9)-IV-2	1660	9	-843	2.54	0.53	-8.60	132.00	192.00	192.00	15
0	(8+9)-IV-3	-1283	-6	781	-1.96	-0.36	7.97	132.00	192.00	192.00	23
1300	(8+9)-VII-1	1481	6	-736	2.27	0.35	-7.51	132.00	192.00	192.00	17
1300	(8+9)-I-1	1341	2	-511	2.05	0.14	-5.21	132.00	192.00	192.00	23
1300	(8+9)-II-4	-972	-8	679	-1.49	-0.45	6.93	132.00	192.00	192.00	26
1300	(8+9)-V-1	1371	6	-672	2.10	0.33	-6.86	132.00	192.00	192.00	19
1300	(8+9)-VII-2	864	2	-301	1.32	0.12	-3.07	132.00	192.00	192.00	38
1300	(8+9)-IV-4	-1338	-9	892	-2.05	-0.51	9.10	132.00	192.00	192.00	20
1300	(8+9)-VII-3	-812	-5	393	-1.24	-0.30	4.01	132.00	192.00	192.00	44
1300	(8+9)-VI-1	1033	6	-635	1.58	0.32	-6.48	132.00	192.00	192.00	21
1300	(8+9)-II-1	1024	5	-587	1.57	0.27	-5.99	132.00	192.00	192.00	22

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
1300	(8+9)-V-2	973	2	-365	1.49	0.14	-3.72	132.00	192.00	192.00	32
1300	(8+9)-IV-1	1389	6	-800	2.13	0.33	-8.16	132.00	192.00	192.00	17
1300	(8+9)-III-4	-1399	-6	667	-2.14	-0.34	6.80	132.00	192.00	192.00	27
1300	(8+9)-III-1	1451	3	-575	2.22	0.16	-5.87	132.00	192.00	192.00	21
1300	(8+9)-VIII-1	1398	7	-848	2.14	0.39	-8.65	132.00	192.00	192.00	16
1300	(8+9)-I-4	-1290	-5	603	-1.97	-0.32	6.15	132.00	192.00	192.00	30
1300	(8+9)-VIII-3	710	3	-509	1.09	0.20	-5.20	132.00	192.00	192.00	28
1300	(8+9)-VI-3	345	2	-296	0.53	0.13	-3.02	132.00	192.00	192.00	49
Verifiche nella direzione secondaria											
0	(8+9)-VII-2	-147	-66	948	-0.23	-5.99	6.95	132.00	192.00	192.00	15
0	(8+9)-I-4	-3819	83	-728	-6.07	7.54	-5.34	132.00	192.00	192.00	15
0	(8+9)-III-1	2543	-91	597	4.04	-8.29	4.38	132.00	192.00	192.00	10
0	(8+9)-VII-3	-1151	62	-1236	-1.83	5.65	-9.06	132.00	192.00	192.00	13
0	(8+9)-V-3	-1173	67	-1392	-1.86	6.07	-10.21	132.00	192.00	192.00	12
0	(8+9)-III-4	-3841	87	-885	-6.11	7.95	-6.49	132.00	192.00	192.00	13
0	(8+9)-V-2	-125	-70	1105	-0.20	-6.40	8.10	132.00	192.00	192.00	13
0	(8+9)-I-1	2521	-87	440	4.01	-7.88	3.23	132.00	192.00	192.00	11
0	(8+9)-I-2	2670	-102	-495	4.24	-9.30	-3.63	132.00	192.00	192.00	10
450	(8+9)-II-2	1459	-26	-2018	2.32	-2.33	-14.80	132.00	192.00	192.00	9.4
450	(8+9)-V-1	-952	-42	2428	-1.51	-3.86	17.81	132.00	192.00	192.00	8.9
450	(8+9)-VIII-3	-1454	26	1854	-2.31	2.36	13.60	132.00	192.00	192.00	12
450	(8+9)-III-3	-3845	40	1187	-6.11	3.66	8.71	132.00	192.00	192.00	15
450	(8+9)-VI-2	452	-28	-1286	0.72	-2.58	-9.43	132.00	192.00	192.00	15
450	(8+9)-VII-1	-1006	-43	2633	-1.60	-3.90	19.32	132.00	192.00	192.00	8.3
450	(8+9)-II-3	-2281	25	1902	-3.63	2.24	13.95	132.00	192.00	192.00	12
450	(8+9)-VI-3	-1274	27	1170	-2.02	2.49	8.58	132.00	192.00	192.00	17
450	(8+9)-I-3	-3791	41	982	-6.03	3.70	7.20	132.00	192.00	192.00	17
450	(8+9)-V-4	130	42	-2544	0.21	3.77	-18.66	132.00	192.00	192.00	8.4
450	(8+9)-III-2	3023	-41	-1303	4.80	-3.75	-9.56	132.00	192.00	192.00	9.5
450	(8+9)-IV-2	1639	-24	-2702	2.60	-2.20	-19.82	132.00	192.00	192.00	7.4
450	(8+9)-IV-3	-2461	23	2585	-3.91	2.11	18.97	132.00	192.00	192.00	9.1
450	(8+9)-VIII-2	632	-27	-1970	1.00	-2.45	-14.45	132.00	192.00	192.00	10
900	1	-446	0	-267	-0.71	0.04	-1.96	79.20	115.20	115.20	58
900	2	-871	1	-527	-1.38	0.09	-3.87	118.80	172.80	172.80	44
900	3	-871	1	-527	-1.38	0.09	-3.87	118.80	172.80	172.80	44
900	4	-446	0	-267	-0.71	0.04	-1.96	105.60	153.60	153.60	77
900	5	-446	0	-267	-0.71	0.04	-1.96	105.60	153.60	153.60	77
900	6	-446	0	-267	-0.71	0.04	-1.96	105.60	153.60	153.60	77
900	7	-446	0	-267	-0.71	0.04	-1.96	105.60	153.60	153.60	77
900	(8+9)-VIII-4	-547	8	-3715	-0.87	0.70	-27.25	132.00	192.00	192.00	6.9
900	(8+9)-VI-4	-417	-5	-2905	-0.66	-0.44	-21.31	132.00	192.00	192.00	8.8
900	(8+9)-II-1	536	3	1903	0.85	0.30	13.96	132.00	192.00	192.00	12
900	(8+9)-VI-1	-206	5	2533	-0.33	0.50	18.58	132.00	192.00	192.00	10
900	(8+9)-VII-4	-751	10	-3220	-1.19	0.87	-23.62	132.00	192.00	192.00	7.8
900	(8+9)-VIII-1	-76	-7	3344	-0.12	-0.65	24.53	132.00	192.00	192.00	7.6
900	(8+9)-II-4	-1159	-3	-2274	-1.84	-0.24	-16.68	132.00	192.00	192.00	11
900	(8+9)-IV-1	666	-9	2714	1.06	-0.85	19.91	132.00	192.00	192.00	8.6
900	(8+9)-IV-4	-1289	10	-3085	-2.05	0.90	-22.63	132.00	192.00	192.00	8.2

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
0	1	-6	0.01	3.84	Si	>100
0	2	-11	0.01	5.76	Si	>100
0	3	-11	0.01	5.76	Si	>100
0	4	-6	0.01	5.12	Si	>100
0	5	-6	0.01	5.12	Si	>100
0	6	-6	0.01	5.12	Si	>100
0	7	-6	0.01	5.12	Si	>100
0	(8+9)-VIII-4	-35	0.04	6.40	Si	>100
0	(8+9)-IV-1	-28	0.03	6.40	Si	>100
0	(8+9)-I-2	-191	0.21	6.40	Si	30
0	(8+9)-VIII-1	25	0.03	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
0	(8+9)-IV-3	79	0.09	6.40	Si	73
0	(8+9)-I-4	165	0.18	6.40	Si	35
0	(8+9)-II-2	-87	0.10	6.40	Si	66
0	(8+9)-I-3	182	0.20	6.40	Si	32
0	(8+9)-II-4	20	0.02	6.40	Si	>100
0	(8+9)-VI-4	-33	0.04	6.40	Si	>100
0	(8+9)-III-1	-174	0.19	6.40	Si	33
0	(8+9)-III-2	-192	0.21	6.40	Si	30
0	(8+9)-III-4	164	0.18	6.40	Si	35
0	(8+9)-VIII-3	26	0.03	6.40	Si	>100
0	(8+9)-IV-2	-88	0.10	6.40	Si	65
0	(8+9)-VIII-2	-35	0.04	6.40	Si	>100
0	(8+9)-II-3	78	0.09	6.40	Si	74
0	(8+9)-I-1	-174	0.19	6.40	Si	33
0	(8+9)-II-1	-29	0.03	6.40	Si	>100
0	(8+9)-III-3	182	0.20	6.40	Si	32
0	(8+9)-VI-1	24	0.03	6.40	Si	>100
0	(8+9)-VI-2	-34	0.04	6.40	Si	>100
0	(8+9)-VI-3	25	0.03	6.40	Si	>100
650	(8+9)-IV-4	20	0.02	6.40	Si	>100
1300	(8+9)-V-1	22	0.02	6.40	Si	>100
1300	(8+9)-VII-2	21	0.02	6.40	Si	>100
1300	(8+9)-VII-3	-25	0.03	6.40	Si	>100
1300	(8+9)-VII-4	-27	0.03	6.40	Si	>100
1300	(8+9)-VII-1	24	0.03	6.40	Si	>100
1300	(8+9)-V-4	-26	0.03	6.40	Si	>100
1300	(8+9)-V-3	-26	0.03	6.40	Si	>100
1300	(8+9)-V-2	22	0.02	6.40	Si	>100
Verifiche nella direzione secondaria						
0	1	5	0.01	3.84	Si	>100
0	4	5	0.01	5.12	Si	>100
0	5	5	0.01	5.12	Si	>100
0	6	5	0.01	5.12	Si	>100
0	7	5	0.01	5.12	Si	>100
0	(8+9)-VIII-4	18	0.03	6.40	Si	>100
0	(8+9)-IV-2	88	0.13	6.40	Si	49
0	(8+9)-VI-4	14	0.02	6.40	Si	>100
0	(8+9)-VIII-1	-10	0.01	6.40	Si	>100
450	2	7	0.01	5.76	Si	>100
450	3	7	0.01	5.76	Si	>100
450	(8+9)-V-1	68	0.10	6.40	Si	64
450	(8+9)-V-2	81	0.12	6.40	Si	54
450	(8+9)-VII-1	67	0.10	6.40	Si	65
450	(8+9)-V-3	-74	0.11	6.40	Si	59
450	(8+9)-VI-3	-40	0.06	6.40	Si	>100
450	(8+9)-VII-3	-75	0.11	6.40	Si	58
450	(8+9)-VII-2	82	0.12	6.40	Si	53
450	(8+9)-VIII-3	-44	0.06	6.40	Si	100
450	(8+9)-VII-4	-59	0.09	6.40	Si	74
450	(8+9)-VI-2	48	0.07	6.40	Si	91
450	(8+9)-V-4	-60	0.09	6.40	Si	72
450	(8+9)-VIII-2	51	0.08	6.40	Si	85
900	(8+9)-I-1	248	0.36	6.40	Si	18
900	(8+9)-II-2	90	0.13	6.40	Si	48
900	(8+9)-III-4	-247	0.36	6.40	Si	18
900	(8+9)-I-4	-247	0.36	6.40	Si	18
900	(8+9)-III-3	-254	0.37	6.40	Si	17
900	(8+9)-IV-3	-86	0.13	6.40	Si	51
900	(8+9)-III-2	256	0.38	6.40	Si	17
900	(8+9)-II-1	63	0.09	6.40	Si	70
900	(8+9)-III-1	249	0.37	6.40	Si	18
900	(8+9)-VI-1	-8	0.01	6.40	Si	>100
900	(8+9)-IV-1	65	0.10	6.40	Si	67
900	(8+9)-IV-4	-63	0.09	6.40	Si	69

X	Comb.	Ty	τ_d	fvd	RS	Cs
900	(8+9)-I-2	257	0.38	6.40	Si	17
900	(8+9)-II-4	-61	0.09	6.40	Si	72
900	(8+9)-II-3	-88	0.13	6.40	Si	49
900	(8+9)-I-3	-255	0.37	6.40	Si	17

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	(8+9)-V-1	2314	5.31	32.00	6.0	1.29	20.00	16	V	6.0
0	(8+9)-II-2	-2269	-5.21	32.00	6.1	-1.26	20.00	16	V	6.1
0	(8+9)-III-2	-2255	-5.18	32.00	6.2	-1.25	20.00	16	V	6.2
0	(8+9)-I-3	2105	4.83	32.00	6.6	1.17	20.00	17	V	6.6
0	(8+9)-II-3	2319	5.32	32.00	6.0	1.29	20.00	16	V	6.0
0	(8+9)-VIII-1	3049	7.00	32.00	4.6	1.69	20.00	12	V	4.6
0	(8+9)-IV-3	2986	6.86	32.00	4.7	1.66	20.00	12	V	4.7
0	(8+9)-VII-2	1012	2.32	32.00	14	0.56	20.00	36	V	14
0	(8+9)-VI-1	2382	5.47	32.00	5.9	1.32	20.00	15	V	5.9
0	(8+9)-III-3	2305	5.29	32.00	6.0	1.28	20.00	16	V	6.0
0	(8+9)-IV-2	-2936	-6.74	32.00	4.7	-1.63	20.00	12	V	4.7
0	(8+9)-VIII-3	2006	4.60	32.00	6.9	1.11	20.00	18	V	6.9
0	(8+9)-V-2	1212	2.78	32.00	11	0.67	20.00	30	V	11
0	(8+9)-I-2	-2055	-4.72	32.00	6.8	-1.14	20.00	18	V	6.8
0	(8+9)-VII-1	2514	5.77	32.00	5.5	1.40	20.00	14	V	5.5
0	(8+9)-VI-3	1339	3.07	32.00	10	0.74	20.00	27	V	10
1300	1	-422	-0.97	19.20	20	-0.23	12.00	51	V	20
1300	2	-833	-1.91	28.80	15	-0.46	18.00	39	V	15
1300	3	-833	-1.91	28.80	15	-0.46	18.00	39	V	15
1300	4	-422	-0.97	25.60	26	-0.23	16.00	68	V	26
1300	5	-422	-0.97	25.60	26	-0.23	16.00	68	V	26
1300	6	-422	-0.97	25.60	26	-0.23	16.00	68	V	26
1300	7	-422	-0.97	25.60	26	-0.23	16.00	68	V	26
1300	(8+9)-VIII-4	-3071	-7.05	32.00	4.5	-1.71	20.00	12	V	4.5
1300	(8+9)-IV-1	2360	5.42	32.00	5.9	1.31	20.00	15	V	5.9
1300	(8+9)-II-4	-2265	-5.20	32.00	6.2	-1.26	20.00	16	V	6.2
1300	(8+9)-IV-4	-2947	-6.77	32.00	4.7	-1.64	20.00	12	V	4.7
1300	(8+9)-II-1	1677	3.85	32.00	8.3	0.93	20.00	21	V	8.3
1300	(8+9)-V-4	-2570	-5.90	32.00	5.4	-1.43	20.00	14	V	5.4
1300	(8+9)-VII-3	-1434	-3.29	32.00	9.7	-0.80	20.00	25	V	9.7
1300	(8+9)-VI-2	-1302	-2.99	32.00	11	-0.72	20.00	28	V	11
1300	(8+9)-VII-4	-2775	-6.37	32.00	5.0	-1.54	20.00	13	V	5.0
1300	(8+9)-III-4	-2362	-5.42	32.00	5.9	-1.31	20.00	15	V	5.9
1300	(8+9)-III-1	1775	4.07	32.00	7.9	0.99	20.00	20	V	7.9
1300	(8+9)-V-3	-1639	-3.76	32.00	8.5	-0.91	20.00	22	V	8.5
1300	(8+9)-I-4	-2158	-4.95	32.00	6.5	-1.20	20.00	17	V	6.5
1300	(8+9)-VIII-2	-1985	-4.56	32.00	7.0	-1.10	20.00	18	V	7.0
1300	(8+9)-I-1	1570	3.60	32.00	8.9	0.87	20.00	23	V	8.9
1300	(8+9)-VI-4	-2389	-5.48	32.00	5.8	-1.33	20.00	15	V	5.8
Verifiche nella direzione secondaria										
450	1	268	0.43	19.20	45	0.10	12.00	>100	V	45
450	2	522	0.83	28.80	35	0.20	18.00	90	V	35
450	3	522	0.83	28.80	35	0.20	18.00	90	V	35
450	4	268	0.43	25.60	60	0.10	16.00	>100	V	60
450	5	268	0.43	25.60	60	0.10	16.00	>100	V	60
450	6	268	0.43	25.60	60	0.10	16.00	>100	V	60
450	7	268	0.43	25.60	60	0.10	16.00	>100	V	60
450	(8+9)-VIII-4	3404	5.41	32.00	5.9	1.31	20.00	15	V	5.9
450	(8+9)-IV-2	3137	4.99	32.00	6.4	1.21	20.00	17	V	6.4
450	(8+9)-I-2	1375	2.19	32.00	15	0.53	20.00	38	V	15
450	(8+9)-VI-1	-2362	-3.75	32.00	8.5	-0.91	20.00	22	V	8.5
450	(8+9)-IV-1	-2432	-3.86	32.00	8.3	-0.94	20.00	21	V	8.3
450	(8+9)-VI-4	2735	4.35	32.00	7.4	1.05	20.00	19	V	7.4
450	(8+9)-II-2	2469	3.92	32.00	8.2	0.95	20.00	21	V	8.2
450	(8+9)-IV-3	-2764	-4.39	32.00	7.3	-1.06	20.00	19	V	7.3

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
450	(8+9)-II-4	2137	3.40	32.00	9.4	0.82	20.00	24	V	9.4
450	(8+9)-IV-4	2805	4.46	32.00	7.2	1.08	20.00	19	V	7.2
450	(8+9)-III-2	1575	2.50	32.00	13	0.61	20.00	33	V	13
450	(8+9)-I-3	-1002	-1.59	32.00	20	-0.39	20.00	52	V	20
450	(8+9)-VIII-2	2539	4.03	32.00	7.9	0.98	20.00	20	V	7.9
450	(8+9)-II-3	-2095	-3.33	32.00	9.6	-0.81	20.00	25	V	9.6
450	(8+9)-VIII-3	-2165	-3.44	32.00	9.3	-0.83	20.00	24	V	9.3
450	(8+9)-III-3	-1202	-1.91	32.00	17	-0.46	20.00	43	V	17
450	(8+9)-II-1	-1763	-2.80	32.00	11	-0.68	20.00	29	V	11
450	(8+9)-VI-2	1870	2.97	32.00	11	0.72	20.00	28	V	11
450	(8+9)-VI-3	-1497	-2.38	32.00	13	-0.58	20.00	35	V	13
900	(8+9)-V-2	-1232	-1.96	32.00	16	-0.47	20.00	42	V	16
900	(8+9)-V-1	-2349	-3.73	32.00	8.6	-0.90	20.00	22	V	8.6
900	(8+9)-I-4	432	0.69	32.00	47	0.17	20.00	>100	V	47
900	(8+9)-VII-3	1313	2.09	32.00	15	0.51	20.00	40	V	15
900	(8+9)-V-4	2660	4.23	32.00	7.6	1.02	20.00	20	V	7.6
900	(8+9)-VII-4	2889	4.59	32.00	7.0	1.11	20.00	18	V	7.0
900	(8+9)-VII-2	-1003	-1.59	32.00	20	-0.39	20.00	52	V	20
900	(8+9)-V-3	1542	2.45	32.00	13	0.59	20.00	34	V	13
900	(8+9)-VII-1	-2578	-4.10	32.00	7.8	-0.99	20.00	20	V	7.8
900	(8+9)-VIII-1	-3054	-4.85	32.00	6.6	-1.17	20.00	17	V	6.6
900	(8+9)-III-4	661	1.05	32.00	30	0.25	20.00	79	V	30
900	(8+9)-III-1	-351	-0.56	32.00	57	-0.13	20.00	>100	V	57
900	(8+9)-I-1	-122	-0.19	32.00	>100	-0.05	20.00	>100	V	>100

Setto 5: origine (24.5,1824.5,328.5), direzione (0.123439,0.992352,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X mm	Comb.	N kg	Mx kg*m	My kg*m	σ_n kg/cmq	σ_{mx} kg/cmq	σ_{my} kg/cmq	ftd kg/cmq	fcd kg/cmq	fmd kg/cmq	Cs
0	(8+9)-III-2	-433	-12	-659	-0.51	-0.53	-3.98	132.00	192.00	192.00	43
0	(8+9)-I-2	-303	-10	-593	-0.36	-0.45	-3.58	132.00	192.00	192.00	48
0	(8+9)-IV-1	1550	24	737	1.82	1.07	4.45	132.00	192.00	192.00	24
0	(8+9)-I-3	273	9	518	0.32	0.42	3.13	132.00	192.00	192.00	48
0	(8+9)-VIII-1	1844	31	1042	2.17	1.37	6.29	132.00	192.00	192.00	18
0	(8+9)-V-1	1346	24	821	1.58	1.08	4.95	132.00	192.00	192.00	23
0	(8+9)-VII-1	1477	26	887	1.74	1.16	5.35	132.00	192.00	192.00	21
0	(8+9)-II-1	1115	18	517	1.31	0.79	3.12	132.00	192.00	192.00	33
0	(8+9)-VI-1	1409	25	822	1.66	1.09	4.96	132.00	192.00	192.00	23
0	(8+9)-IV-3	1522	26	951	1.79	1.17	5.74	132.00	192.00	192.00	20
0	(8+9)-VI-3	793	13	426	0.93	0.59	2.57	132.00	192.00	192.00	42
0	(8+9)-V-2	677	13	424	0.80	0.56	2.56	132.00	192.00	192.00	45
0	(8+9)-VII-2	546	11	358	0.64	0.48	2.16	132.00	192.00	192.00	54
0	(8+9)-II-3	1087	20	731	1.28	0.90	4.41	132.00	192.00	192.00	27
0	(8+9)-VIII-3	1228	20	646	1.45	0.87	3.90	132.00	192.00	192.00	28
0	(8+9)-III-3	404	11	584	0.48	0.50	3.52	132.00	192.00	192.00	41
1300	1	204	-3	80	0.24	-0.12	0.48	79.20	115.20	115.20	>100
1300	2	398	-6	155	0.47	-0.27	0.94	118.80	172.80	172.80	91
1300	3	398	-6	155	0.47	-0.27	0.94	118.80	172.80	172.80	91
1300	4	204	-3	80	0.24	-0.12	0.48	105.60	153.60	153.60	>100
1300	5	204	-3	80	0.24	-0.12	0.48	105.60	153.60	153.60	>100
1300	6	204	-3	80	0.24	-0.12	0.48	105.60	153.60	153.60	>100
1300	7	204	-3	80	0.24	-0.12	0.48	105.60	153.60	153.60	>100
1300	(8+9)-VIII-4	2381	25	1096	2.80	1.08	6.61	132.00	192.00	192.00	16
1300	(8+9)-VI-2	1055	26	470	1.24	1.15	2.84	132.00	192.00	192.00	33
1300	(8+9)-III-1	-1208	6	-555	-1.42	0.27	-3.35	132.00	192.00	192.00	53
1300	(8+9)-IV-2	1735	32	801	2.04	1.42	4.84	132.00	192.00	192.00	21
1300	(8+9)-V-3	1100	-18	501	1.30	-0.81	3.03	132.00	192.00	192.00	34
1300	(8+9)-VII-3	946	-20	427	1.11	-0.86	2.58	132.00	192.00	192.00	38
1300	(8+9)-I-1	-1053	7	-480	-1.24	0.32	-2.90	132.00	192.00	192.00	60
1300	(8+9)-VII-4	2045	-2	938	2.41	-0.09	5.66	132.00	192.00	192.00	21
1300	(8+9)-II-2	1221	28	552	1.44	1.26	3.33	132.00	192.00	192.00	29
1300	(8+9)-V-4	1891	-3	863	2.23	-0.14	5.21	132.00	192.00	192.00	22
1300	(8+9)-I-4	1339	-11	591	1.58	-0.48	3.57	132.00	192.00	192.00	30

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
1300	(8+9)-VI-4	1867	21	846	2.20	0.92	5.11	132.00	192.00	192.00	21
1300	(8+9)-II-4	1701	18	765	2.00	0.81	4.62	132.00	192.00	192.00	23
1300	(8+9)-VIII-2	1570	30	720	1.85	1.32	4.35	132.00	192.00	192.00	23
1300	(8+9)-III-4	1493	-10	666	1.76	-0.43	4.02	132.00	192.00	192.00	27
1300	(8+9)-IV-4	2216	22	1014	2.61	0.98	6.12	132.00	192.00	192.00	18
Verifiche nella direzione secondaria											
0	1	-651	-2	366	-1.03	-0.18	2.69	79.20	115.20	115.20	40
0	2	-1315	-4	737	-2.09	-0.38	5.41	118.80	172.80	172.80	30
0	3	-1315	-4	737	-2.09	-0.38	5.41	118.80	172.80	172.80	30
0	4	-651	-2	366	-1.03	-0.18	2.69	105.60	153.60	153.60	53
0	5	-651	-2	366	-1.03	-0.18	2.69	105.60	153.60	153.60	53
0	6	-651	-2	366	-1.03	-0.18	2.69	105.60	153.60	153.60	53
0	7	-651	-2	366	-1.03	-0.18	2.69	105.60	153.60	153.60	53
0	(8+9)-VIII-4	-165	-7	3883	-0.26	-0.67	28.48	132.00	192.00	192.00	6.6
0	(8+9)-IV-2	485	10	3040	0.77	0.88	22.30	132.00	192.00	192.00	7.9
0	(8+9)-V-1	-477	12	-2645	-0.76	1.12	-19.41	132.00	192.00	192.00	9.4
0	(8+9)-I-2	1742	42	345	2.77	3.80	2.53	132.00	192.00	192.00	19
0	(8+9)-V-2	-317	13	-1366	-0.50	1.19	-10.02	132.00	192.00	192.00	17
0	(8+9)-I-4	-2485	-44	1443	-3.95	-3.96	10.59	132.00	192.00	192.00	13
0	(8+9)-V-3	-586	-16	1874	-0.93	-1.44	13.75	132.00	192.00	192.00	13
0	(8+9)-II-2	449	13	2222	0.71	1.17	16.30	132.00	192.00	192.00	10
0	(8+9)-V-4	-426	-15	3154	-0.68	-1.36	23.13	132.00	192.00	192.00	7.8
0	(8+9)-II-4	-818	-13	2552	-1.30	-1.16	18.72	132.00	192.00	192.00	9.7
0	(8+9)-VI-1	-702	1	-2557	-1.12	0.13	-18.75	132.00	192.00	192.00	10
0	(8+9)-III-2	1753	41	590	2.79	3.71	4.33	132.00	192.00	192.00	16
0	(8+9)-VI-2	-168	4	1709	-0.27	0.39	12.54	132.00	192.00	192.00	15
0	(8+9)-III-4	-2474	-45	1688	-3.93	-4.05	12.39	132.00	192.00	192.00	12
0	(8+9)-VI-3	-735	-7	-1201	-1.17	-0.64	-8.81	132.00	192.00	192.00	20
0	(8+9)-I-1	1582	41	-935	2.51	3.72	-6.86	132.00	192.00	192.00	13
0	(8+9)-VI-4	-201	-4	3065	-0.32	-0.38	22.48	132.00	192.00	192.00	8.4
0	(8+9)-IV-4	-783	-16	3370	-1.24	-1.45	24.72	132.00	192.00	192.00	7.3
0	(8+9)-VII-1	-488	13	-2891	-0.78	1.20	-21.20	132.00	192.00	192.00	8.6
0	(8+9)-II-1	-84	10	-2044	-0.13	0.91	-14.99	132.00	192.00	192.00	12
0	(8+9)-VII-2	-306	12	-1120	-0.49	1.11	-8.22	132.00	192.00	192.00	21
0	(8+9)-III-1	1571	42	-1180	2.50	3.81	-8.66	132.00	192.00	192.00	12
0	(8+9)-VII-3	-597	-15	1629	-0.95	-1.35	11.95	132.00	192.00	192.00	14
0	(8+9)-IV-1	-120	13	-2861	-0.19	1.20	-20.99	132.00	192.00	192.00	8.7
0	(8+9)-VII-4	-415	-16	3399	-0.66	-1.45	24.93	132.00	192.00	192.00	7.3
0	(8+9)-VIII-3	-770	-4	-2019	-1.22	-0.34	-14.81	132.00	192.00	192.00	13
0	(8+9)-IV-3	-1388	-12	-2532	-2.21	-1.12	-18.57	132.00	192.00	192.00	9.7
0	(8+9)-II-3	-1352	-16	-1714	-2.15	-1.42	-12.57	132.00	192.00	192.00	14
0	(8+9)-VIII-1	-738	5	-3374	-1.17	0.42	-24.75	132.00	192.00	192.00	7.6
0	(8+9)-VIII-2	-132	1	2527	-0.21	0.10	18.54	132.00	192.00	192.00	10
585	(8+9)-III-3	-2060	-43	219	-3.27	-3.88	1.60	132.00	192.00	192.00	35
585	(8+9)-I-3	-2080	-43	321	-3.31	-3.91	2.35	132.00	192.00	192.00	30

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Ty kg	τ_d kg/cm ²	fvd kg/cm ²	RS	Cs
0	(8+9)-III-4	-159	0.14	6.40	Si	47
0	(8+9)-I-3	-181	0.15	6.40	Si	41
0	(8+9)-II-2	81	0.07	6.40	Si	92
0	(8+9)-I-1	161	0.14	6.40	Si	46
0	(8+9)-I-4	-162	0.14	6.40	Si	46
0	(8+9)-I-2	179	0.15	6.40	Si	42
0	(8+9)-IV-2	91	0.08	6.40	Si	83
0	(8+9)-III-3	-183	0.16	6.40	Si	41
0	(8+9)-IV-3	-92	0.08	6.40	Si	81
0	(8+9)-III-1	158	0.14	6.40	Si	47
0	(8+9)-III-2	182	0.16	6.40	Si	41
0	(8+9)-II-3	-83	0.07	6.40	Si	90
650	(8+9)-IV-1	-36	0.03	6.40	Si	>100
650	(8+9)-II-1	-28	0.02	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
650	(8+9)-II-4	25	0.02	6.40	Si	>100
650	(8+9)-VII-3	13	0.01	6.40	Si	>100
650	(8+9)-IV-4	34	0.03	6.40	Si	>100
650	(8+9)-V-2	-18	0.02	6.40	Si	>100
650	(8+9)-V-3	16	0.01	6.40	Si	>100
1300	1	-2	0.00	3.84	Si	>100
1300	2	-5	0.00	5.76	Si	>100
1300	3	-5	0.00	5.76	Si	>100
1300	4	-2	0.00	5.12	Si	>100
1300	5	-2	0.00	5.12	Si	>100
1300	6	-2	0.00	5.12	Si	>100
1300	7	-2	0.00	5.12	Si	>100
1300	(8+9)-VIII-4	49	0.04	6.40	Si	>100
1300	(8+9)-VI-3	-30	0.03	6.40	Si	>100
1300	(8+9)-V-1	-40	0.03	6.40	Si	>100
1300	(8+9)-VI-1	-46	0.04	6.40	Si	>100
1300	(8+9)-VII-4	39	0.03	6.40	Si	>100
1300	(8+9)-VII-1	-42	0.04	6.40	Si	>100
1300	(8+9)-VII-2	-16	0.01	6.40	Si	>100
1300	(8+9)-VI-2	27	0.02	6.40	Si	>100
1300	(8+9)-VI-4	43	0.04	6.40	Si	>100
1300	(8+9)-VIII-1	-52	0.04	6.40	Si	>100
1300	(8+9)-VIII-2	33	0.03	6.40	Si	>100
1300	(8+9)-VIII-3	-36	0.03	6.40	Si	>100
1300	(8+9)-V-4	37	0.03	6.40	Si	>100
Verifiche nella direzione secondaria						
0	1	4	0.01	3.84	Si	>100
0	2	8	0.01	5.76	Si	>100
0	3	8	0.01	5.76	Si	>100
0	4	4	0.01	5.12	Si	>100
0	5	4	0.01	5.12	Si	>100
0	6	4	0.01	5.12	Si	>100
0	7	4	0.01	5.12	Si	>100
0	(8+9)-IV-2	36	0.05	6.40	Si	>100
0	(8+9)-VI-2	2	0.00	6.40	Si	>100
0	(8+9)-III-1	107	0.16	6.40	Si	41
0	(8+9)-I-2	107	0.16	6.40	Si	41
0	(8+9)-III-2	108	0.16	6.40	Si	40
0	(8+9)-I-4	-103	0.15	6.40	Si	43
0	(8+9)-III-3	-103	0.15	6.40	Si	42
0	(8+9)-II-2	33	0.05	6.40	Si	>100
0	(8+9)-III-4	-102	0.15	6.40	Si	43
0	(8+9)-II-1	35	0.05	6.40	Si	>100
0	(8+9)-II-3	-28	0.04	6.40	Si	>100
0	(8+9)-I-3	-102	0.15	6.40	Si	43
0	(8+9)-IV-1	32	0.05	6.40	Si	>100
0	(8+9)-I-1	107	0.16	6.40	Si	41
0	(8+9)-IV-3	-31	0.05	6.40	Si	>100
0	(8+9)-II-4	-30	0.04	6.40	Si	>100
585	(8+9)-VIII-4	11	0.02	6.40	Si	>100
585	(8+9)-VI-3	5	0.01	6.40	Si	>100
585	(8+9)-VIII-3	-4	0.01	6.40	Si	>100
585	(8+9)-VIII-2	8	0.01	6.40	Si	>100
1170	(8+9)-V-1	-9	0.01	6.40	Si	>100
1170	(8+9)-VII-1	-11	0.02	6.40	Si	>100
1170	(8+9)-V-2	-8	0.01	6.40	Si	>100
1170	(8+9)-VII-4	13	0.02	6.40	Si	>100
1170	(8+9)-VI-1	-4	0.01	6.40	Si	>100
1170	(8+9)-VII-2	-6	0.01	6.40	Si	>100
1170	(8+9)-VII-3	9	0.01	6.40	Si	>100
1170	(8+9)-VI-4	6	0.01	6.40	Si	>100
1170	(8+9)-VIII-1	-9	0.01	6.40	Si	>100
1170	(8+9)-V-4	11	0.02	6.40	Si	>100
1170	(8+9)-V-3	10	0.02	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
1170	(8+9)-IV-4	31	0.05	6.40	Si	>100

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	1	-473	-0.83	19.20	23	-0.20	12.00	59	V	23
0	2	-938	-1.66	28.80	17	-0.40	18.00	45	V	17
0	3	-938	-1.66	28.80	17	-0.40	18.00	45	V	17
0	4	-473	-0.83	25.60	31	-0.20	16.00	79	V	31
0	5	-473	-0.83	25.60	31	-0.20	16.00	79	V	31
0	6	-473	-0.83	25.60	31	-0.20	16.00	79	V	31
0	7	-473	-0.83	25.60	31	-0.20	16.00	79	V	31
0	(8+9)-V-4	-2779	-4.91	32.00	6.5	-1.19	20.00	17	V	6.5
0	(8+9)-IV-2	-2836	-5.01	32.00	6.4	-1.21	20.00	17	V	6.4
0	(8+9)-II-4	-2566	-4.53	32.00	7.1	-1.10	20.00	18	V	7.1
0	(8+9)-VI-4	-2871	-5.07	32.00	6.3	-1.23	20.00	16	V	6.3
0	(8+9)-VIII-2	-2531	-4.47	32.00	7.2	-1.08	20.00	18	V	7.2
0	(8+9)-II-2	-2063	-3.64	32.00	8.8	-0.88	20.00	23	V	8.8
0	(8+9)-VII-3	-1356	-2.39	32.00	13	-0.58	20.00	35	V	13
0	(8+9)-VIII-4	-3644	-6.44	32.00	5.0	-1.56	20.00	13	V	5.0
0	(8+9)-VII-4	-3012	-5.32	32.00	6.0	-1.29	20.00	16	V	6.0
0	(8+9)-VI-2	-1758	-3.10	32.00	10	-0.75	20.00	27	V	10
0	(8+9)-V-3	-1588	-2.80	32.00	11	-0.68	20.00	29	V	11
0	(8+9)-IV-4	-3340	-5.90	32.00	5.4	-1.43	20.00	14	V	5.4
650	(8+9)-I-2	604	1.07	32.00	30	0.26	20.00	78	V	30
650	(8+9)-I-4	-1934	-3.41	32.00	9.4	-0.83	20.00	24	V	9.4
650	(8+9)-I-3	-905	-1.60	32.00	20	-0.39	20.00	52	V	20
650	(8+9)-III-4	-2141	-3.78	32.00	8.5	-0.91	20.00	22	V	8.5
650	(8+9)-I-1	1632	2.88	32.00	11	0.70	20.00	29	V	11
650	(8+9)-III-1	1839	3.25	32.00	9.9	0.79	20.00	25	V	9.9
650	(8+9)-III-3	-698	-1.23	32.00	26	-0.30	20.00	67	V	26
1300	(8+9)-IV-1	2858	5.05	32.00	6.3	1.22	20.00	16	V	6.3
1300	(8+9)-IV-3	2662	4.70	32.00	6.8	1.14	20.00	18	V	6.8
1300	(8+9)-II-3	1877	3.31	32.00	9.7	0.80	20.00	25	V	9.7
1300	(8+9)-VI-1	2572	4.54	32.00	7.0	1.10	20.00	18	V	7.0
1300	(8+9)-II-1	2073	3.66	32.00	8.7	0.89	20.00	23	V	8.7
1300	(8+9)-VII-1	2848	5.03	32.00	6.4	1.22	20.00	16	V	6.4
1300	(8+9)-VII-2	1216	2.15	32.00	15	0.52	20.00	38	V	15
1300	(8+9)-III-2	-447	-0.79	32.00	41	-0.19	20.00	>100	V	41
1300	(8+9)-V-2	1451	2.56	32.00	12	0.62	20.00	32	V	12
1300	(8+9)-VIII-1	3357	5.93	32.00	5.4	1.43	20.00	14	V	5.4
1300	(8+9)-V-1	2612	4.61	32.00	6.9	1.12	20.00	18	V	6.9
1300	(8+9)-VIII-3	2163	3.82	32.00	8.4	0.92	20.00	22	V	8.4
1300	(8+9)-VI-3	1378	2.43	32.00	13	0.59	20.00	34	V	13
Verifiche nella direzione secondaria										
0	(8+9)-V-1	-2912	-4.63	32.00	6.9	-1.12	20.00	18	V	6.9
0	(8+9)-VIII-1	-3796	-6.03	32.00	5.3	-1.46	20.00	14	V	5.3
0	(8+9)-VI-3	-1433	-2.28	32.00	14	-0.55	20.00	36	V	14
0	(8+9)-VI-2	1786	2.84	32.00	11	0.69	20.00	29	V	11
0	(8+9)-VII-3	1591	2.53	32.00	13	0.61	20.00	33	V	13
0	(8+9)-VI-1	-2868	-4.56	32.00	7.0	-1.10	20.00	18	V	7.0
0	(8+9)-VII-1	-3191	-5.07	32.00	6.3	-1.23	20.00	16	V	6.3
0	(8+9)-VII-4	3545	5.63	32.00	5.7	1.36	20.00	15	V	5.7
0	(8+9)-VII-2	-1238	-1.97	32.00	16	-0.48	20.00	42	V	16
0	(8+9)-VI-4	3221	5.12	32.00	6.3	1.24	20.00	16	V	6.3
0	(8+9)-V-4	3266	5.19	32.00	6.2	1.26	20.00	16	V	6.2
0	(8+9)-V-3	1870	2.97	32.00	11	0.72	20.00	28	V	11
0	(8+9)-V-2	-1516	-2.41	32.00	13	-0.58	20.00	34	V	13
585	1	275	0.44	19.20	44	0.11	12.00	>100	V	44
585	2	543	0.86	28.80	33	0.21	18.00	86	V	33
585	3	543	0.86	28.80	33	0.21	18.00	86	V	33
585	4	275	0.44	25.60	59	0.11	16.00	>100	V	59
585	5	275	0.44	25.60	59	0.11	16.00	>100	V	59

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
585	6	275	0.44	25.60	59	0.11	16.00	>100	V	59
585	7	275	0.44	25.60	59	0.11	16.00	>100	V	59
585	(8+9)-II-3	-2234	-3.55	32.00	9.0	-0.86	20.00	23	V	9.0
585	(8+9)-VIII-4	4157	6.61	32.00	4.8	1.60	20.00	13	V	4.8
585	(8+9)-IV-3	-3221	-5.12	32.00	6.3	-1.24	20.00	16	V	6.3
585	(8+9)-I-3	-994	-1.58	32.00	20	-0.38	20.00	52	V	20
585	(8+9)-VIII-2	2747	4.37	32.00	7.3	1.06	20.00	19	V	7.3
585	(8+9)-III-3	-1290	-2.05	32.00	16	-0.50	20.00	40	V	16
585	(8+9)-IV-2	3603	5.73	32.00	5.6	1.39	20.00	14	V	5.6
585	(8+9)-II-2	2616	4.16	32.00	7.7	1.01	20.00	20	V	7.7
585	(8+9)-I-2	1376	2.19	32.00	15	0.53	20.00	38	V	15
585	(8+9)-III-2	1672	2.66	32.00	12	0.64	20.00	31	V	12
585	(8+9)-VIII-3	-2365	-3.76	32.00	8.5	-0.91	20.00	22	V	8.5
1170	(8+9)-I-4	1250	1.99	32.00	16	0.48	20.00	42	V	16
1170	(8+9)-I-1	-902	-1.43	32.00	22	-0.35	20.00	58	V	22
1170	(8+9)-II-1	-2244	-3.57	32.00	9.0	-0.86	20.00	23	V	9.0
1170	(8+9)-IV-4	3491	5.55	32.00	5.8	1.34	20.00	15	V	5.8
1170	(8+9)-IV-1	-3144	-5.00	32.00	6.4	-1.21	20.00	17	V	6.4
1170	(8+9)-III-4	1520	2.42	32.00	13	0.58	20.00	34	V	13
1170	(8+9)-III-1	-1172	-1.86	32.00	17	-0.45	20.00	44	V	17
1170	(8+9)-II-4	2591	4.12	32.00	7.8	1.00	20.00	20	V	7.8

Verifiche a instabilità

Setto(X)	Comb.	kcrit _c	kcrit _m	λ_{relc}	λ_{relm}	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
(cm)						kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	
2(0.0)	(8+9)-VIII-4	--	--	--	--	0.38	0.18	-1.70	132.00	192.00	192.00	79
3(28.9)	(8+9)-III-2	--	--	--	--	0.41	0.73	1.38	132.00	192.00	192.00	71
4(0.0)	(8+9)-VIII-4	--	--	--	--	2.38	0.54	-9.14	132.00	192.00	192.00	15
5(130.0)	(8+9)-VIII-4	--	--	--	--	2.80	1.08	6.61	132.00	192.00	192.00	16

Parete Xlam 10 - Nodi: [8-9-2-3-10-11-111-110] - **Crit.Prog.** Criterio di verifica XLAM 0 - **Verificato**:
[Cs=1.656,Comb=(8+9)-VI-2]

Geometria setti

Setto	Crit.	X mm	L cm	S cm	X90 mm	L90 cm	S90 cm
6	Criterio di verifica XLAM 0	0	375.2	12.1	0	60.0	12.1
		300	381.1	12.1	1935	60.0	12.1
		600	387.0	12.1	--	--	--
7	Criterio di verifica XLAM 0	0	330.0	12.1	0	80.0	12.1
		400	337.8	12.1	1728	80.0	12.1
		800	345.7	12.1	--	--	--
8	Criterio di verifica XLAM 0	0	299.0	12.1	0	37.2	12.1
		186	302.7	12.1	1532	37.2	12.1
		372	306.3	12.1	--	--	--
9	Criterio di verifica XLAM 0	0	120.0	12.1	0	150.0	12.1
		750	120.0	12.1	600	150.0	12.1
		1500	120.0	12.1	1200	150.0	12.1
10	Criterio di verifica XLAM 0	0	75.7	12.1	0	150.0	12.1
		750	90.4	12.1	526	150.0	12.1
		1500	105.2	12.1	--	--	--
11	Criterio di verifica XLAM 0	0	86.3	12.1	0	120.0	12.1
		600	98.1	12.1	550	120.0	12.1
		1200	109.9	12.1	--	--	--

Setto 6: origine (1651.1,1123.2,187.6), direzione (-0.201275,0.979535,0)
Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
600	1	-2103	53	3211	-0.75	0.71	1.77	79.20	115.20	115.20	46
600	2	-4263	113	6709	-1.52	1.51	3.70	118.80	172.80	172.80	33
600	3	-4263	113	6709	-1.52	1.51	3.70	118.80	172.80	172.80	33
600	4	-2103	53	3211	-0.75	0.71	1.77	105.60	153.60	153.60	62
600	5	-2103	53	3211	-0.75	0.71	1.77	105.60	153.60	153.60	62
600	6	-2103	53	3211	-0.75	0.71	1.77	105.60	153.60	153.60	62
600	7	-2103	53	3211	-0.75	0.71	1.77	105.60	153.60	153.60	62
600	(8+9)-VIII-4	-9194	1200	9807	-3.27	16.05	5.41	132.00	192.00	192.00	8.9
600	(8+9)-IV-1	7201	-1157	-6269	2.56	-15.47	-3.46	132.00	192.00	192.00	8.5
600	(8+9)-V-1	-7180	-1213	8152	-2.56	-16.22	4.50	132.00	192.00	192.00	9.3
600	(8+9)-I-2	-11417	-1226	12292	-4.06	-16.40	6.78	132.00	192.00	192.00	8.3
600	(8+9)-V-2	-14395	-1128	15151	-5.12	-15.09	8.36	132.00	192.00	192.00	8.1
600	(8+9)-I-4	1315	1383	-898	0.47	18.49	-0.50	132.00	192.00	192.00	9.8
600	(8+9)-V-3	11508	1201	-10756	4.10	16.06	-5.94	132.00	192.00	192.00	6.9
600	(8+9)-II-2	-15379	-214	15842	-5.47	-2.87	8.74	132.00	192.00	192.00	16
600	(8+9)-V-4	4293	1285	-3757	1.53	17.19	-2.07	132.00	192.00	192.00	8.9
600	(8+9)-II-4	-11559	568	11885	-4.11	7.60	6.56	132.00	192.00	192.00	13
600	(8+9)-VI-1	7779	-466	-6632	2.77	-6.24	-3.66	132.00	192.00	192.00	14
600	(8+9)-III-2	-10976	-1028	11926	-3.91	-13.74	6.58	132.00	192.00	192.00	9.4
600	(8+9)-VI-2	-16272	-185	16700	-5.79	-2.48	9.22	132.00	192.00	192.00	16
600	(8+9)-III-4	1756	1582	-1264	0.63	21.15	-0.70	132.00	192.00	192.00	8.4
600	(8+9)-VI-3	13385	258	-12305	4.76	3.44	-6.79	132.00	192.00	192.00	11
600	(8+9)-IV-2	-13907	447	14622	-4.95	5.97	8.07	132.00	192.00	192.00	14
600	(8+9)-VI-4	-10666	539	11027	-3.80	7.21	6.09	132.00	192.00	192.00	14
600	(8+9)-IV-4	-10088	1229	10665	-3.59	16.44	5.89	132.00	192.00	192.00	8.6
600	(8+9)-VII-1	-7621	-1411	8518	-2.71	-18.87	4.70	132.00	192.00	192.00	8.1
600	(8+9)-II-1	8672	-496	-7490	3.09	-6.63	-4.13	132.00	192.00	192.00	13
600	(8+9)-VII-2	-13954	-930	14785	-4.97	-12.44	8.16	132.00	192.00	192.00	9.3
600	(8+9)-III-1	-4643	-1509	5659	-1.65	-20.18	3.12	132.00	192.00	192.00	8.2
600	(8+9)-VII-3	11067	1003	-10390	3.94	13.41	-5.73	132.00	192.00	192.00	7.7
600	(8+9)-I-1	-4202	-1311	5293	-1.50	-17.52	2.92	132.00	192.00	192.00	9.4
600	(8+9)-VII-4	4734	1484	-4123	1.69	19.84	-2.28	132.00	192.00	192.00	7.8
600	(8+9)-III-3	8089	1100	-7531	2.88	14.71	-4.16	132.00	192.00	192.00	8.3
600	(8+9)-IV-3	11021	-374	-10226	3.92	-5.00	-5.64	132.00	192.00	192.00	12
600	(8+9)-II-3	12492	287	-11447	4.45	3.84	-6.32	132.00	192.00	192.00	12
600	(8+9)-VIII-1	6308	-1128	-5412	2.25	-15.08	-2.99	132.00	192.00	192.00	9.0
600	(8+9)-VIII-2	-14801	476	15479	-5.27	6.36	8.54	132.00	192.00	192.00	13
600	(8+9)-VIII-3	11914	-403	-11084	4.24	-5.39	-6.12	132.00	192.00	192.00	11
600	(8+9)-I-3	8530	1299	-7897	3.04	17.37	-4.36	132.00	192.00	192.00	7.3
Verifiche nella direzione secondaria											
0	(8+9)-VIII-4	-3975	-11	947	-13.69	-2.24	32.60	132.00	192.00	192.00	5.4
0	(8+9)-VII-2	-6791	-58	1566	-23.38	-11.42	53.93	132.00	192.00	192.00	2.8
0	(8+9)-III-3	4549	40	-1180	15.66	7.90	-40.63	132.00	192.00	192.00	2.7
0	(8+9)-IV-2	-6547	-37	1538	-22.55	-7.30	52.96	132.00	192.00	192.00	3.1
0	(8+9)-III-4	1782	28	-405	6.14	5.47	-13.94	132.00	192.00	192.00	6.8
0	(8+9)-VIII-2	-6765	-39	1650	-23.29	-7.78	56.81	132.00	192.00	192.00	2.8
0	(8+9)-IV-1	2676	4	-1045	9.22	0.79	-36.00	132.00	192.00	192.00	3.8
0	(8+9)-VII-4	2507	36	-778	8.63	7.06	-26.79	132.00	192.00	192.00	4.1
0	(8+9)-I-1	-3644	-40	207	-12.55	-7.93	7.12	132.00	192.00	192.00	12
0	(8+9)-IV-3	5031	27	-1525	17.32	5.38	-52.51	132.00	192.00	192.00	2.3
0	(8+9)-I-3	4203	37	-1391	14.47	7.36	-47.90	132.00	192.00	192.00	2.5
0	(8+9)-IV-4	-4193	-14	1059	-14.44	-2.72	36.45	132.00	192.00	192.00	4.8
0	(8+9)-II-1	1524	-5	-1749	5.25	-1.01	-60.23	132.00	192.00	192.00	2.8
0	(8+9)-V-1	-4369	-48	580	-15.05	-9.53	19.97	132.00	192.00	192.00	6.3
0	(8+9)-II-3	3879	18	-2229	13.36	3.58	-76.74	132.00	192.00	192.00	1.9
0	(8+9)-V-2	-6445	-55	1777	-22.19	-10.88	61.20	132.00	192.00	192.00	2.6
0	(8+9)-III-1	-3298	-38	418	-11.36	-7.39	14.39	132.00	192.00	192.00	8.5
0	(8+9)-V-3	4929	45	-1764	16.97	8.95	-60.75	132.00	192.00	192.00	2.0
0	(8+9)-VIII-3	5248	30	-1637	18.07	5.86	-56.36	132.00	192.00	192.00	2.2
0	(8+9)-V-4	2853	39	-567	9.82	7.60	-19.52	132.00	192.00	192.00	4.6
0	(8+9)-VII-3	5274	48	-1553	18.16	9.49	-53.48	132.00	192.00	192.00	2.1
0	(8+9)-VI-1	1307	-8	-1637	4.50	-1.49	-56.38	132.00	192.00	192.00	3.0
0	(8+9)-I-4	2128	31	-194	7.33	6.01	-6.67	132.00	192.00	192.00	8.2

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-VI-2	-5613	-30	2354	-19.33	-5.98	81.05	132.00	192.00	192.00	2.2
0	(8+9)-II-4	-3041	-5	1762	-10.47	-0.92	60.68	132.00	192.00	192.00	3.1
0	(8+9)-VIII-1	2459	2	-933	8.47	0.31	-32.14	132.00	192.00	192.00	4.3
0	(8+9)-I-2	-5720	-47	1404	-19.70	-9.28	48.35	132.00	192.00	192.00	3.2
0	(8+9)-II-2	-5395	-28	2242	-18.58	-5.50	77.19	132.00	192.00	192.00	2.3
0	(8+9)-III-2	-6065	-50	1193	-20.89	-9.82	41.08	132.00	192.00	192.00	3.6
0	(8+9)-VI-3	4096	21	-2340	14.11	4.06	-80.59	132.00	192.00	192.00	1.8
0	(8+9)-VI-4	-2823	-2	1650	-9.72	-0.44	56.83	132.00	192.00	192.00	3.3
0	(8+9)-VII-1	-4024	-46	791	-13.86	-8.99	27.24	132.00	192.00	192.00	5.2
1935	1	-918	4	-75	-3.16	0.77	-2.59	79.20	115.20	115.20	33
1935	2	-1504	9	-188	-5.18	1.69	-6.47	118.80	172.80	172.80	21
1935	3	-1504	9	-188	-5.18	1.69	-6.47	118.80	172.80	172.80	21
1935	4	-918	4	-75	-3.16	0.77	-2.59	105.60	153.60	153.60	45
1935	5	-918	4	-75	-3.16	0.77	-2.59	105.60	153.60	153.60	45
1935	6	-918	4	-75	-3.16	0.77	-2.59	105.60	153.60	153.60	45
1935	7	-918	4	-75	-3.16	0.77	-2.59	105.60	153.60	153.60	45

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Ty kg	τ_d kg/cmq	fvd kg/cmq	RS	Cs
0	1	36	0.01	3.84	Si	>100
0	2	77	0.02	5.76	Si	>100
0	3	77	0.02	5.76	Si	>100
0	4	36	0.01	5.12	Si	>100
0	5	36	0.01	5.12	Si	>100
0	6	36	0.01	5.12	Si	>100
0	7	36	0.01	5.12	Si	>100
0	(8+9)-VIII-4	583	0.16	6.40	Si	41
0	(8+9)-IV-1	-445	0.12	6.40	Si	54
0	(8+9)-V-1	-734	0.20	6.40	Si	33
0	(8+9)-V-2	-614	0.16	6.40	Si	39
0	(8+9)-I-4	487	0.13	6.40	Si	49
0	(8+9)-V-3	663	0.18	6.40	Si	36
0	(8+9)-II-2	105	0.03	6.40	Si	>100
0	(8+9)-V-4	783	0.21	6.40	Si	31
0	(8+9)-II-4	346	0.09	6.40	Si	69
0	(8+9)-VII-2	-569	0.15	6.40	Si	42
0	(8+9)-II-1	-297	0.08	6.40	Si	81
0	(8+9)-VI-1	-386	0.10	6.40	Si	62
0	(8+9)-II-3	-56	0.01	6.40	Si	>100
0	(8+9)-III-4	531	0.14	6.40	Si	45
0	(8+9)-VII-4	828	0.22	6.40	Si	29
0	(8+9)-IV-2	253	0.07	6.40	Si	95
0	(8+9)-IV-4	494	0.13	6.40	Si	49
0	(8+9)-VII-3	618	0.17	6.40	Si	39
0	(8+9)-VII-1	-779	0.21	6.40	Si	31
0	(8+9)-VI-4	435	0.12	6.40	Si	55
0	(8+9)-VIII-1	-534	0.14	6.40	Si	45
0	(8+9)-VI-3	33	0.01	6.40	Si	>100
300	(8+9)-VIII-3	-227	0.06	6.40	Si	>100
300	(8+9)-IV-3	-231	0.06	6.40	Si	>100
300	(8+9)-VIII-2	204	0.05	6.40	Si	>100
600	(8+9)-I-2	-450	0.12	6.40	Si	55
600	(8+9)-VI-2	-26	0.01	6.40	Si	>100
600	(8+9)-III-1	-536	0.14	6.40	Si	46
600	(8+9)-I-3	427	0.11	6.40	Si	58
600	(8+9)-I-1	-515	0.13	6.40	Si	48
600	(8+9)-III-3	406	0.11	6.40	Si	61
600	(8+9)-III-2	-430	0.11	6.40	Si	58
Verifiche nella direzione secondaria						
0	1	12	0.04	3.84	Si	>100
0	2	27	0.09	5.76	Si	66
0	3	27	0.09	5.76	Si	66

X	Comb.	Ty	τ_d	fvd	RS	Cs
0	4	12	0.04	5.12	Si	>100
0	5	12	0.04	5.12	Si	>100
0	6	12	0.04	5.12	Si	>100
0	7	12	0.04	5.12	Si	>100
0	(8+9)-IV-2	59	0.19	6.40	Si	34
0	(8+9)-V-1	53	0.17	6.40	Si	38
0	(8+9)-I-2	56	0.18	6.40	Si	36
0	(8+9)-V-2	63	0.20	6.40	Si	32
0	(8+9)-I-4	-29	0.09	6.40	Si	70
0	(8+9)-VII-1	47	0.15	6.40	Si	43
0	(8+9)-IV-3	-43	0.14	6.40	Si	47
0	(8+9)-V-3	-47	0.15	6.40	Si	43
0	(8+9)-IV-4	34	0.11	6.40	Si	60
0	(8+9)-VIII-2	61	0.19	6.40	Si	33
0	(8+9)-I-3	-40	0.13	6.40	Si	51
0	(8+9)-III-2	62	0.20	6.40	Si	33
0	(8+9)-VII-3	-53	0.17	6.40	Si	38
0	(8+9)-III-4	-23	0.07	6.40	Si	88
0	(8+9)-I-1	45	0.14	6.40	Si	45
0	(8+9)-III-1	39	0.12	6.40	Si	52
0	(8+9)-III-3	-46	0.15	6.40	Si	44
0	(8+9)-VII-4	-31	0.10	6.40	Si	66
0	(8+9)-VIII-3	-45	0.14	6.40	Si	45
0	(8+9)-V-4	-37	0.12	6.40	Si	55
0	(8+9)-VII-2	70	0.22	6.40	Si	29
0	(8+9)-VI-2	41	0.13	6.40	Si	49
1935	(8+9)-VIII-4	32	0.10	6.40	Si	63
1935	(8+9)-II-2	39	0.12	6.40	Si	51
1935	(8+9)-IV-1	-21	0.07	6.40	Si	94
1935	(8+9)-VI-1	-18	0.06	6.40	Si	>100
1935	(8+9)-II-1	-17	0.05	6.40	Si	>100
1935	(8+9)-VI-3	-29	0.09	6.40	Si	70
1935	(8+9)-VIII-1	-22	0.07	6.40	Si	90
1935	(8+9)-II-4	26	0.08	6.40	Si	76
1935	(8+9)-II-3	-30	0.09	6.40	Si	68
1935	(8+9)-VI-4	28	0.09	6.40	Si	73

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Tx kg	τ_{vd} kg/cmq	fvd kg/cmq	Csv	τ_M kg/cmq	fTd kg/cmq	Csm	Mecc.	Cs
0	(8+9)-VII-4	6217	3.42	32.00	9.3	0.83	20.00	24	V	9.3
0	(8+9)-I-4	1723	0.95	32.00	34	0.23	20.00	87	V	34
0	(8+9)-III-4	2582	1.42	32.00	23	0.34	20.00	58	V	23
0	(8+9)-V-4	5358	2.95	32.00	11	0.71	20.00	28	V	11
300	1	-1618	-0.88	19.20	22	-0.21	12.00	57	V	22
300	2	-3527	-1.91	28.80	15	-0.46	18.00	39	V	15
300	3	-3527	-1.91	28.80	15	-0.46	18.00	39	V	15
300	4	-1618	-0.88	25.60	29	-0.21	16.00	75	V	29
300	5	-1618	-0.88	25.60	29	-0.21	16.00	75	V	29
300	6	-1618	-0.88	25.60	29	-0.21	16.00	75	V	29
300	7	-1618	-0.88	25.60	29	-0.21	16.00	75	V	29
300	(8+9)-V-3	12803	6.94	32.00	4.6	1.68	20.00	12	V	4.6
300	(8+9)-VII-3	11884	6.44	32.00	5.0	1.56	20.00	13	V	5.0
300	(8+9)-VIII-2	-13996	-7.59	32.00	4.2	-1.84	20.00	11	V	4.2
300	(8+9)-VII-1	-8250	-4.47	32.00	7.2	-1.08	20.00	18	V	7.2
300	(8+9)-VII-2	-14154	-7.67	32.00	4.2	-1.86	20.00	11	V	4.2
300	(8+9)-VI-2	-17059	-9.25	32.00	3.5	-2.24	20.00	8.9	V	3.5
300	(8+9)-III-2	-10154	-5.50	32.00	5.8	-1.33	20.00	15	V	5.8
300	(8+9)-I-2	-11073	-6.00	32.00	5.3	-1.45	20.00	14	V	5.3
300	(8+9)-I-3	8802	4.77	32.00	6.7	1.15	20.00	17	V	6.7
300	(8+9)-III-1	-4249	-2.30	32.00	14	-0.56	20.00	36	V	14
300	(8+9)-III-3	7883	4.27	32.00	7.5	1.03	20.00	19	V	7.5
300	(8+9)-I-1	-3331	-1.81	32.00	18	-0.44	20.00	46	V	18

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
300	(8+9)-V-1	-7331	-3.97	32.00	8.1	-0.96	20.00	21	V	8.1
300	(8+9)-V-2	-15073	-8.17	32.00	3.9	-1.98	20.00	10	V	3.9
600	(8+9)-VIII-4	-10226	-5.46	32.00	5.9	-1.32	20.00	15	V	5.9
600	(8+9)-IV-1	8569	4.57	32.00	7.0	1.11	20.00	18	V	7.0
600	(8+9)-II-4	-13846	-7.39	32.00	4.3	-1.79	20.00	11	V	4.3
600	(8+9)-IV-4	-10672	-5.70	32.00	5.6	-1.38	20.00	15	V	5.6
600	(8+9)-II-3	14765	7.88	32.00	4.1	1.91	20.00	10	V	4.1
600	(8+9)-IV-3	11592	6.19	32.00	5.2	1.50	20.00	13	V	5.2
600	(8+9)-II-2	-16868	-9.01	32.00	3.6	-2.18	20.00	9.2	V	3.6
600	(8+9)-VI-1	11296	6.03	32.00	5.3	1.46	20.00	14	V	5.3
600	(8+9)-VI-3	15211	8.12	32.00	3.9	1.97	20.00	10	V	3.9
600	(8+9)-IV-2	-13695	-7.31	32.00	4.4	-1.77	20.00	11	V	4.4
600	(8+9)-VIII-1	8123	4.34	32.00	7.4	1.05	20.00	19	V	7.4
600	(8+9)-II-1	11742	6.27	32.00	5.1	1.52	20.00	13	V	5.1
600	(8+9)-VIII-3	12038	6.43	32.00	5.0	1.56	20.00	13	V	5.0
600	(8+9)-VI-4	-13399	-7.15	32.00	4.5	-1.73	20.00	12	V	4.5
Verifiche nella direzione secondaria										
1935	1	84	0.29	19.20	67	0.07	12.00	>100	V	67
1935	2	175	0.60	28.80	48	0.15	18.00	>100	V	48
1935	3	175	0.60	28.80	48	0.15	18.00	>100	V	48
1935	4	84	0.29	25.60	89	0.07	16.00	>100	V	89
1935	5	84	0.29	25.60	89	0.07	16.00	>100	V	89
1935	6	84	0.29	25.60	89	0.07	16.00	>100	V	89
1935	7	84	0.29	25.60	89	0.07	16.00	>100	V	89
1935	(8+9)-VIII-4	2362	8.13	32.00	3.9	1.97	20.00	10	V	3.9
1935	(8+9)-IV-2	3895	13.41	32.00	2.4	3.25	20.00	6.2	V	2.4
1935	(8+9)-V-1	1911	6.58	32.00	4.9	1.59	20.00	13	V	4.9
1935	(8+9)-I-2	3323	11.44	32.00	2.8	2.77	20.00	7.2	V	2.8
1935	(8+9)-V-2	4177	14.38	32.00	2.2	3.48	20.00	5.7	V	2.2
1935	(8+9)-I-4	-933	-3.21	32.00	10.0	-0.78	20.00	26	V	10.0
1935	(8+9)-V-3	-4052	-13.95	32.00	2.3	-3.38	20.00	5.9	V	2.3
1935	(8+9)-II-2	4476	15.41	32.00	2.1	3.73	20.00	5.4	V	2.1
1935	(8+9)-V-4	-1787	-6.15	32.00	5.2	-1.49	20.00	13	V	5.2
1935	(8+9)-II-4	3199	11.02	32.00	2.9	2.67	20.00	7.5	V	2.9
1935	(8+9)-VI-1	-2819	-9.71	32.00	3.3	-2.35	20.00	8.5	V	3.3
1935	(8+9)-III-2	3149	10.84	32.00	3.0	2.62	20.00	7.6	V	3.0
1935	(8+9)-VI-2	4732	16.30	32.00	2.0	3.94	20.00	5.1	V	2.0
1935	(8+9)-III-4	-1108	-3.81	32.00	8.4	-0.92	20.00	22	V	8.4
1935	(8+9)-VI-3	-4608	-15.87	32.00	2.0	-3.84	20.00	5.2	V	2.0
1935	(8+9)-I-1	1058	3.64	32.00	8.8	0.88	20.00	23	V	8.8
1935	(8+9)-VI-4	2943	10.14	32.00	3.2	2.45	20.00	8.2	V	3.2
1935	(8+9)-IV-4	2618	9.01	32.00	3.5	2.18	20.00	9.2	V	3.5
1935	(8+9)-VII-1	2086	7.18	32.00	4.5	1.74	20.00	12	V	4.5
1935	(8+9)-II-1	-3075	-10.59	32.00	3.0	-2.56	20.00	7.8	V	3.0
1935	(8+9)-VII-2	4002	13.78	32.00	2.3	3.34	20.00	6.0	V	2.3
1935	(8+9)-III-1	1232	4.24	32.00	7.5	1.03	20.00	19	V	7.5
1935	(8+9)-VII-3	-3877	-13.35	32.00	2.4	-3.23	20.00	6.2	V	2.4
1935	(8+9)-IV-1	-2493	-8.59	32.00	3.7	-2.08	20.00	9.6	V	3.7
1935	(8+9)-VII-4	-1961	-6.75	32.00	4.7	-1.63	20.00	12	V	4.7
1935	(8+9)-III-3	-3024	-10.41	32.00	3.1	-2.52	20.00	7.9	V	3.1
1935	(8+9)-IV-3	-3770	-12.98	32.00	2.5	-3.14	20.00	6.4	V	2.5
1935	(8+9)-II-3	-4352	-14.98	32.00	2.1	-3.63	20.00	5.5	V	2.1
1935	(8+9)-VIII-1	-2237	-7.70	32.00	4.2	-1.86	20.00	11	V	4.2
1935	(8+9)-VIII-2	4151	14.29	32.00	2.2	3.46	20.00	5.8	V	2.2
1935	(8+9)-VIII-3	-4026	-13.86	32.00	2.3	-3.36	20.00	6.0	V	2.3
1935	(8+9)-I-3	-3198	-11.01	32.00	2.9	-2.67	20.00	7.5	V	2.9

Setto 7: origine (1697.4,897.9,165.0), direzione (-0.201275,0.979535,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	(8+9)-II-3	5162	-393	-7533	2.16	-6.16	-5.72	132.00	192.00	192.00	13
0	(8+9)-VI-3	5531	-365	-8047	2.31	-5.72	-6.11	132.00	192.00	192.00	13

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-VI-2	-5397	365	7818	-2.25	5.72	5.93	132.00	192.00	192.00	16
0	(8+9)-II-2	-5028	393	7304	-2.10	6.16	5.54	132.00	192.00	192.00	16
400	(8+9)-VII-2	-6438	560	9256	-2.62	8.58	6.70	132.00	192.00	192.00	13
400	(8+9)-III-2	-4827	659	6986	-1.97	10.09	5.06	132.00	192.00	192.00	13
400	(8+9)-IV-3	6451	251	-9532	2.63	3.84	-6.90	132.00	192.00	192.00	13
400	(8+9)-IV-1	4481	732	-6629	1.83	11.22	-4.80	132.00	192.00	192.00	10
400	(8+9)-VII-3	6584	-554	-9680	2.68	-8.49	-7.01	132.00	192.00	192.00	9.9
400	(8+9)-IV-2	-6304	-245	9108	-2.57	-3.75	6.60	132.00	192.00	192.00	18
400	(8+9)-I-2	-5055	737	7326	-2.06	11.28	5.31	132.00	192.00	192.00	12
400	(8+9)-I-4	1510	-869	-2349	0.62	-13.31	-1.70	132.00	192.00	192.00	12
400	(8+9)-IV-4	-4335	-727	6205	-1.77	-11.13	4.49	132.00	192.00	192.00	12
400	(8+9)-VII-4	3349	-847	-4959	1.37	-12.98	-3.59	132.00	192.00	192.00	10
400	(8+9)-V-1	-2974	776	4195	-1.21	11.88	3.04	132.00	192.00	192.00	13
400	(8+9)-II-4	-5094	-468	7339	-2.08	-7.17	5.31	132.00	192.00	192.00	15
400	(8+9)-V-2	-6665	637	9596	-2.72	9.76	6.95	132.00	192.00	192.00	11
400	(8+9)-VIII-2	-6787	-275	9789	-2.77	-4.21	7.09	132.00	192.00	192.00	17
400	(8+9)-V-3	6812	-632	-10020	2.78	-9.68	-7.26	132.00	192.00	192.00	9.2
400	(8+9)-III-4	1738	-946	-2689	0.71	-14.50	-1.95	132.00	192.00	192.00	11
400	(8+9)-V-4	3121	-770	-4618	1.27	-11.79	-3.34	132.00	192.00	192.00	11
400	(8+9)-I-3	5201	-731	-7750	2.12	-11.19	-5.61	132.00	192.00	192.00	9.7
400	(8+9)-VI-1	4757	444	-7082	1.94	6.80	-5.13	132.00	192.00	192.00	13
400	(8+9)-VIII-1	3998	703	-5948	1.63	10.76	-4.31	132.00	192.00	192.00	11
400	(8+9)-VIII-3	6934	281	-10213	2.83	4.30	-7.40	132.00	192.00	192.00	12
400	(8+9)-III-3	4974	-653	-7410	2.03	-10.01	-5.37	132.00	192.00	192.00	10
400	(8+9)-II-1	5240	474	-7763	2.14	7.26	-5.62	132.00	192.00	192.00	12
400	(8+9)-III-1	-1591	952	2265	-0.65	14.59	1.64	132.00	192.00	192.00	12
400	(8+9)-I-1	-1364	875	1925	-0.56	13.40	1.39	132.00	192.00	192.00	13
400	(8+9)-VIII-4	-3851	-697	5524	-1.57	-10.68	4.00	132.00	192.00	192.00	13
400	(8+9)-VI-4	-4610	-438	6658	-1.88	-6.72	4.82	132.00	192.00	192.00	17
400	(8+9)-VII-1	-3202	853	4535	-1.31	13.07	3.28	132.00	192.00	192.00	12
800	1	169	7	-402	0.07	0.11	-0.28	79.20	115.20	115.20	>100
800	2	252	15	-713	0.10	0.23	-0.49	118.80	172.80	172.80	>100
800	3	252	15	-713	0.10	0.23	-0.49	118.80	172.80	172.80	>100
800	4	169	7	-402	0.07	0.11	-0.28	105.60	153.60	153.60	>100
800	5	169	7	-402	0.07	0.11	-0.28	105.60	153.60	153.60	>100
800	6	169	7	-402	0.07	0.11	-0.28	105.60	153.60	153.60	>100
800	7	169	7	-402	0.07	0.11	-0.28	105.60	153.60	153.60	>100
Verifiche nella direzione secondaria											
0	2	-3258	-12	12	-8.42	-1.73	0.24	118.80	172.80	172.80	73
0	3	-3258	-12	12	-8.42	-1.73	0.24	118.80	172.80	172.80	73
0	(8+9)-VIII-4	-3315	1	1639	-8.56	0.14	31.74	132.00	192.00	192.00	6.0
0	(8+9)-VI-4	-3642	1	2055	-9.41	0.17	39.81	132.00	192.00	192.00	4.7
0	(8+9)-III-3	1254	6	-2196	3.24	0.95	-42.53	132.00	192.00	192.00	4.0
0	(8+9)-IV-3	1850	-0	-2725	4.78	-0.05	-52.78	132.00	192.00	192.00	3.2
0	(8+9)-VII-1	-3120	-19	1437	-8.06	-2.75	27.84	132.00	192.00	192.00	6.2
0	(8+9)-VIII-2	-4837	-8	2909	-12.49	-1.21	56.35	132.00	192.00	192.00	3.3
0	(8+9)-IV-1	748	-6	-1815	1.93	-0.92	-35.17	132.00	192.00	192.00	4.9
0	(8+9)-VII-4	343	12	-1434	0.89	1.73	-27.77	132.00	192.00	192.00	6.2
0	(8+9)-IV-2	-4627	-7	2729	-11.95	-0.97	52.86	132.00	192.00	192.00	3.5
0	(8+9)-I-3	1352	6	-2321	3.49	0.94	-44.95	132.00	192.00	192.00	3.8
0	(8+9)-II-1	1075	-6	-2232	2.78	-0.95	-43.23	132.00	192.00	192.00	4.0
0	(8+9)-IV-4	-3525	-1	1819	-9.10	-0.10	35.24	132.00	192.00	192.00	5.4
0	(8+9)-II-3	2177	-1	-3141	5.62	-0.08	-60.85	132.00	192.00	192.00	2.8
0	(8+9)-V-1	-3022	-19	1312	-7.80	-2.76	25.42	132.00	192.00	192.00	6.7
0	(8+9)-VII-2	-4733	-19	2801	-12.22	-2.77	54.25	132.00	192.00	192.00	3.3
0	(8+9)-V-2	-4831	-19	2925	-12.48	-2.76	56.67	132.00	192.00	192.00	3.2
0	(8+9)-VIII-3	2060	1	-2905	5.32	0.19	-56.28	132.00	192.00	192.00	3.0
0	(8+9)-V-3	2054	12	-2922	5.30	1.74	-56.59	132.00	192.00	192.00	2.9
0	(8+9)-I-2	-4129	-13	2324	-10.66	-1.96	45.02	132.00	192.00	192.00	4.0
0	(8+9)-V-4	245	12	-1309	0.63	1.74	-25.35	132.00	192.00	192.00	6.9
0	(8+9)-II-2	-4954	-6	3145	-12.79	-0.94	60.92	132.00	192.00	192.00	3.1
0	(8+9)-III-2	-4031	-13	2200	-10.41	-1.97	42.60	132.00	192.00	192.00	4.3
0	(8+9)-VIII-1	538	-8	-1635	1.39	-1.16	-31.67	132.00	192.00	192.00	5.5
0	(8+9)-VII-3	1956	12	-2797	5.05	1.75	-54.18	132.00	192.00	192.00	3.0

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-II-4	-3852	-0	2235	-9.95	-0.07	43.30	132.00	192.00	192.00	4.4
0	(8+9)-VI-1	865	-8	-2051	2.23	-1.19	-39.74	132.00	192.00	192.00	4.3
0	(8+9)-VI-2	-5164	-8	3325	-13.34	-1.18	64.41	132.00	192.00	192.00	2.9
0	(8+9)-VI-3	2388	1	-3322	6.17	0.16	-64.34	132.00	192.00	192.00	2.6
1728	1	-1951	1	-38	-5.04	0.17	-0.73	79.20	115.20	115.20	>100
1728	4	-1951	1	-38	-5.04	0.17	-0.73	105.60	153.60	153.60	>100
1728	5	-1951	1	-38	-5.04	0.17	-0.73	105.60	153.60	153.60	>100
1728	6	-1951	1	-38	-5.04	0.17	-0.73	105.60	153.60	153.60	>100
1728	7	-1951	1	-38	-5.04	0.17	-0.73	105.60	153.60	153.60	>100
1728	(8+9)-III-4	-1790	161	-18	-4.62	23.80	-0.34	132.00	192.00	192.00	7.9
1728	(8+9)-III-1	-892	-159	-34	-2.30	-23.56	-0.65	132.00	192.00	192.00	7.9
1728	(8+9)-I-4	-1686	132	-12	-4.35	19.46	-0.23	132.00	192.00	192.00	9.7
1728	(8+9)-I-1	-996	-130	-40	-2.57	-19.22	-0.77	132.00	192.00	192.00	9.6

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
0	(8+9)-IV-2	91	0.03	6.40	Si	>100
0	(8+9)-VIII-3	-99	0.03	6.40	Si	>100
0	(8+9)-VIII-2	111	0.03	6.40	Si	>100
0	(8+9)-II-3	85	0.03	6.40	Si	>100
0	(8+9)-II-2	-73	0.02	6.40	Si	>100
0	(8+9)-IV-3	-79	0.02	6.40	Si	>100
0	(8+9)-VI-2	-53	0.02	6.40	Si	>100
0	(8+9)-VI-3	65	0.02	6.40	Si	>100
800	1	15	0.00	3.84	Si	>100
800	2	32	0.01	5.76	Si	>100
800	3	32	0.01	5.76	Si	>100
800	4	15	0.00	5.12	Si	>100
800	5	15	0.00	5.12	Si	>100
800	6	15	0.00	5.12	Si	>100
800	7	15	0.00	5.12	Si	>100
800	(8+9)-VIII-4	156	0.05	6.40	Si	>100
800	(8+9)-IV-1	-136	0.04	6.40	Si	>100
800	(8+9)-VI-1	-128	0.04	6.40	Si	>100
800	(8+9)-III-2	-227	0.07	6.40	Si	97
800	(8+9)-I-4	287	0.08	6.40	Si	77
800	(8+9)-III-4	289	0.08	6.40	Si	76
800	(8+9)-I-3	250	0.07	6.40	Si	88
800	(8+9)-II-4	150	0.04	6.40	Si	>100
800	(8+9)-VI-4	148	0.04	6.40	Si	>100
800	(8+9)-IV-4	157	0.05	6.40	Si	>100
800	(8+9)-VII-1	-265	0.08	6.40	Si	83
800	(8+9)-V-2	-226	0.07	6.40	Si	98
800	(8+9)-VII-2	-224	0.06	6.40	Si	99
800	(8+9)-V-4	284	0.08	6.40	Si	78
800	(8+9)-VII-3	244	0.07	6.40	Si	90
800	(8+9)-III-1	-269	0.08	6.40	Si	82
800	(8+9)-VII-4	286	0.08	6.40	Si	77
800	(8+9)-III-3	248	0.07	6.40	Si	89
800	(8+9)-II-1	-129	0.04	6.40	Si	>100
800	(8+9)-V-3	247	0.07	6.40	Si	90
800	(8+9)-VIII-1	-135	0.04	6.40	Si	>100
800	(8+9)-I-2	-229	0.07	6.40	Si	96
800	(8+9)-I-1	-266	0.08	6.40	Si	83
800	(8+9)-V-1	-263	0.08	6.40	Si	84
Verifiche nella direzione secondaria						
0	1	4	0.01	3.84	Si	>100
0	2	10	0.02	5.76	Si	>100
0	3	10	0.02	5.76	Si	>100
0	4	4	0.01	5.12	Si	>100
0	5	4	0.01	5.12	Si	>100
0	6	4	0.01	5.12	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
0	7	4	0.01	5.12	Si	>100
0	(8+9)-VIII-4	25	0.06	6.40	Si	>100
0	(8+9)-VI-1	-25	0.06	6.40	Si	>100
0	(8+9)-III-4	21	0.05	6.40	Si	>100
0	(8+9)-V-1	-56	0.13	6.40	Si	48
0	(8+9)-IV-1	-7	0.02	6.40	Si	>100
0	(8+9)-I-4	23	0.06	6.40	Si	>100
0	(8+9)-VI-4	31	0.07	6.40	Si	87
0	(8+9)-VIII-2	-9	0.02	6.40	Si	>100
0	(8+9)-VI-3	8	0.02	6.40	Si	>100
0	(8+9)-II-4	19	0.05	6.40	Si	>100
0	(8+9)-IV-4	13	0.03	6.40	Si	>100
0	(8+9)-VII-2	-51	0.12	6.40	Si	53
0	(8+9)-VIII-3	15	0.03	6.40	Si	>100
0	(8+9)-VII-4	60	0.14	6.40	Si	45
0	(8+9)-VII-3	57	0.14	6.40	Si	47
0	(8+9)-VII-1	-54	0.13	6.40	Si	50
0	(8+9)-II-1	-13	0.03	6.40	Si	>100
0	(8+9)-V-2	-49	0.12	6.40	Si	55
0	(8+9)-V-3	55	0.13	6.40	Si	49
0	(8+9)-V-4	62	0.15	6.40	Si	44
1728	(8+9)-IV-2	21	0.05	6.40	Si	>100
1728	(8+9)-I-2	25	0.06	6.40	Si	>100
1728	(8+9)-III-1	18	0.04	6.40	Si	>100
1728	(8+9)-VI-2	7	0.02	6.40	Si	>100
1728	(8+9)-II-3	-16	0.04	6.40	Si	>100
1728	(8+9)-III-2	26	0.06	6.40	Si	>100
1728	(8+9)-IV-3	-17	0.04	6.40	Si	>100
1728	(8+9)-III-3	-22	0.05	6.40	Si	>100
1728	(8+9)-VIII-1	-19	0.05	6.40	Si	>100
1728	(8+9)-II-2	20	0.05	6.40	Si	>100
1728	(8+9)-I-3	-21	0.05	6.40	Si	>100
1728	(8+9)-I-1	18	0.04	6.40	Si	>100

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
400	1	-353	-0.22	19.20	89	-0.05	12.00	>100	V	89
400	4	-353	-0.22	25.60	>100	-0.05	16.00	>100	V	>100
400	5	-353	-0.22	25.60	>100	-0.05	16.00	>100	V	>100
400	6	-353	-0.22	25.60	>100	-0.05	16.00	>100	V	>100
400	7	-353	-0.22	25.60	>100	-0.05	16.00	>100	V	>100
400	(8+9)-VIII-4	-6024	-3.68	32.00	8.7	-0.89	20.00	22	V	8.7
400	(8+9)-IV-1	6034	3.69	32.00	8.7	0.89	20.00	22	V	8.7
400	(8+9)-IV-4	-6540	-4.00	32.00	8.0	-0.97	20.00	21	V	8.0
400	(8+9)-V-1	-4443	-2.72	32.00	12	-0.66	20.00	30	V	12
400	(8+9)-I-2	-8238	-5.04	32.00	6.4	-1.22	20.00	16	V	6.4
400	(8+9)-V-2	-9957	-6.09	32.00	5.3	-1.47	20.00	14	V	5.3
400	(8+9)-I-4	2217	1.36	32.00	24	0.33	20.00	61	V	24
400	(8+9)-V-3	9451	5.78	32.00	5.5	1.40	20.00	14	V	5.5
400	(8+9)-II-2	-11012	-6.74	32.00	4.8	-1.63	20.00	12	V	4.8
400	(8+9)-V-4	3937	2.41	32.00	13	0.58	20.00	34	V	13
400	(8+9)-II-4	-7876	-4.82	32.00	6.6	-1.17	20.00	17	V	6.6
400	(8+9)-VI-1	6854	4.19	32.00	7.6	1.01	20.00	20	V	7.6
400	(8+9)-III-2	-7837	-4.79	32.00	6.7	-1.16	20.00	17	V	6.7
400	(8+9)-VI-2	-11528	-7.05	32.00	4.5	-1.71	20.00	12	V	4.5
400	(8+9)-III-4	2617	1.60	32.00	20	0.39	20.00	52	V	20
400	(8+9)-VI-3	11022	6.74	32.00	4.7	1.63	20.00	12	V	4.7
400	(8+9)-IV-2	-9677	-5.92	32.00	5.4	-1.43	20.00	14	V	5.4
400	(8+9)-VI-4	-7360	-4.50	32.00	7.1	-1.09	20.00	18	V	7.1
400	(8+9)-I-1	-2723	-1.67	32.00	19	-0.40	20.00	50	V	19
400	(8+9)-VII-1	-4844	-2.96	32.00	11	-0.72	20.00	28	V	11
400	(8+9)-II-1	7369	4.51	32.00	7.1	1.09	20.00	18	V	7.1

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
400	(8+9)-VII-2	-9557	-5.85	32.00	5.5	-1.41	20.00	14	V	5.5
400	(8+9)-III-1	-3124	-1.91	32.00	17	-0.46	20.00	43	V	17
400	(8+9)-VIII-3	9686	5.92	32.00	5.4	1.43	20.00	14	V	5.4
400	(8+9)-VII-3	9050	5.54	32.00	5.8	1.34	20.00	15	V	5.8
400	(8+9)-I-3	7731	4.73	32.00	6.8	1.14	20.00	17	V	6.8
400	(8+9)-II-3	10506	6.43	32.00	5.0	1.56	20.00	13	V	5.0
400	(8+9)-III-3	7331	4.48	32.00	7.1	1.09	20.00	18	V	7.1
400	(8+9)-IV-3	9170	5.61	32.00	5.7	1.36	20.00	15	V	5.7
400	(8+9)-VII-4	4337	2.65	32.00	12	0.64	20.00	31	V	12
400	(8+9)-VIII-1	5518	3.38	32.00	9.5	0.82	20.00	24	V	9.5
400	(8+9)-VIII-2	-10193	-6.23	32.00	5.1	-1.51	20.00	13	V	5.1
800	2	-598	-0.36	28.80	81	-0.09	18.00	>100	V	81
800	3	-598	-0.36	28.80	81	-0.09	18.00	>100	V	81
Verifiche nella direzione secondaria										
0	1	79	0.20	19.20	94	0.05	12.00	>100	V	94
0	2	162	0.42	28.80	69	0.10	18.00	>100	V	69
0	3	162	0.42	28.80	69	0.10	18.00	>100	V	69
0	4	79	0.20	25.60	>100	0.05	16.00	>100	V	>100
0	5	79	0.20	25.60	>100	0.05	16.00	>100	V	>100
0	6	79	0.20	25.60	>100	0.05	16.00	>100	V	>100
0	7	79	0.20	25.60	>100	0.05	16.00	>100	V	>100
1728	(8+9)-VIII-4	2482	6.41	32.00	5.0	1.55	20.00	13	V	5.0
1728	(8+9)-IV-2	4124	10.65	32.00	3.0	2.58	20.00	7.8	V	3.0
1728	(8+9)-V-1	1949	5.03	32.00	6.4	1.22	20.00	16	V	6.4
1728	(8+9)-I-2	3518	9.09	32.00	3.5	2.20	20.00	9.1	V	3.5
1728	(8+9)-V-2	4384	11.32	32.00	2.8	2.74	20.00	7.3	V	2.8
1728	(8+9)-I-4	-1088	-2.81	32.00	11	-0.68	20.00	29	V	11
1728	(8+9)-V-3	-4389	-11.34	32.00	2.8	-2.74	20.00	7.3	V	2.8
1728	(8+9)-II-2	4747	12.26	32.00	2.6	2.97	20.00	6.7	V	2.6
1728	(8+9)-V-4	-1954	-5.05	32.00	6.3	-1.22	20.00	16	V	6.3
1728	(8+9)-II-4	3365	8.69	32.00	3.7	2.10	20.00	9.5	V	3.7
1728	(8+9)-VI-1	-3111	-8.03	32.00	4.0	-1.94	20.00	10	V	4.0
1728	(8+9)-III-2	3331	8.60	32.00	3.7	2.08	20.00	9.6	V	3.7
1728	(8+9)-VI-2	5006	12.93	32.00	2.5	3.13	20.00	6.4	V	2.5
1728	(8+9)-III-4	-1275	-3.29	32.00	9.7	-0.80	20.00	25	V	9.7
1728	(8+9)-VI-3	-5012	-12.94	32.00	2.5	-3.13	20.00	6.4	V	2.5
1728	(8+9)-I-1	1083	2.80	32.00	11	0.68	20.00	30	V	11
1728	(8+9)-VI-4	3105	8.02	32.00	4.0	1.94	20.00	10	V	4.0
1728	(8+9)-IV-4	2742	7.08	32.00	4.5	1.71	20.00	12	V	4.5
1728	(8+9)-VII-1	2135	5.52	32.00	5.8	1.33	20.00	15	V	5.8
1728	(8+9)-II-1	-3370	-8.70	32.00	3.7	-2.11	20.00	9.5	V	3.7
1728	(8+9)-VII-2	4197	10.84	32.00	3.0	2.62	20.00	7.6	V	3.0
1728	(8+9)-III-1	1270	3.28	32.00	9.8	0.79	20.00	25	V	9.8
1728	(8+9)-VII-3	-4202	-10.85	32.00	2.9	-2.63	20.00	7.6	V	2.9
1728	(8+9)-IV-1	-2748	-7.10	32.00	4.5	-1.72	20.00	12	V	4.5
1728	(8+9)-VII-4	-2141	-5.53	32.00	5.8	-1.34	20.00	15	V	5.8
1728	(8+9)-III-3	-3337	-8.62	32.00	3.7	-2.09	20.00	9.6	V	3.7
1728	(8+9)-IV-3	-4130	-10.67	32.00	3.0	-2.58	20.00	7.7	V	3.0
1728	(8+9)-II-3	-4752	-12.27	32.00	2.6	-2.97	20.00	6.7	V	2.6
1728	(8+9)-VIII-1	-2488	-6.43	32.00	5.0	-1.55	20.00	13	V	5.0
1728	(8+9)-VIII-2	4384	11.32	32.00	2.8	2.74	20.00	7.3	V	2.8
1728	(8+9)-VIII-3	-4389	-11.34	32.00	2.8	-2.74	20.00	7.3	V	2.8
1728	(8+9)-I-3	-3523	-9.10	32.00	3.5	-2.20	20.00	9.1	V	3.5

Setto 8: origine (1729.0,744.0,149.5), direzione (-0.201275,0.979535,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	1	44	-14	-264	0.02	-0.24	-0.24	79.20	115.20	115.20	>100
0	2	36	-28	-389	0.02	-0.48	-0.36	118.80	172.80	172.80	>100
0	3	36	-28	-389	0.02	-0.48	-0.36	118.80	172.80	172.80	>100
0	4	44	-14	-264	0.02	-0.24	-0.24	105.60	153.60	153.60	>100
0	5	44	-14	-264	0.02	-0.24	-0.24	105.60	153.60	153.60	>100

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	6	44	-14	-264	0.02	-0.24	-0.24	105.60	153.60	153.60	>100
0	7	44	-14	-264	0.02	-0.24	-0.24	105.60	153.60	153.60	>100
0	(8+9)-III-4	1400	567	-1412	0.64	9.81	-1.31	132.00	192.00	192.00	16
0	(8+9)-VIII-1	3066	-435	-2701	1.41	-7.53	-2.50	132.00	192.00	192.00	16
0	(8+9)-V-4	2361	437	-2165	1.09	7.55	-2.00	132.00	192.00	192.00	17
0	(8+9)-I-4	1183	491	-1230	0.54	8.50	-1.14	132.00	192.00	192.00	18
0	(8+9)-VII-1	-2497	-531	1961	-1.15	-9.19	1.81	132.00	192.00	192.00	17
0	(8+9)-VII-4	2577	512	-2348	1.19	8.86	-2.17	132.00	192.00	192.00	15
0	(8+9)-V-1	-2280	-456	1778	-1.05	-7.89	1.64	132.00	192.00	192.00	20
0	(8+9)-I-1	-1103	-510	843	-0.51	-8.83	0.78	132.00	192.00	192.00	20
0	(8+9)-III-1	-1320	-586	1025	-0.61	-10.14	0.95	132.00	192.00	192.00	17
186	(8+9)-VIII-4	-2981	380	3238	-1.36	6.50	2.92	132.00	192.00	192.00	20
186	(8+9)-IV-1	3410	-417	-3888	1.55	-7.12	-3.51	132.00	192.00	192.00	15
186	(8+9)-III-3	3933	350	-4520	1.79	5.98	-4.08	132.00	192.00	192.00	15
186	(8+9)-III-2	-3853	-368	4250	-1.75	-6.29	3.83	132.00	192.00	192.00	19
186	(8+9)-I-2	-4071	-443	4503	-1.85	-7.57	4.06	132.00	192.00	192.00	16
186	(8+9)-I-3	4151	425	-4773	1.89	7.27	-4.31	132.00	192.00	192.00	13
186	(8+9)-IV-4	-3330	399	3618	-1.52	6.82	3.26	132.00	192.00	192.00	19
372	(8+9)-VI-2	-5973	-79	8407	-2.69	-1.33	7.41	132.00	192.00	192.00	22
372	(8+9)-VI-3	6053	62	-8578	2.72	1.06	-7.56	132.00	192.00	192.00	15
372	(8+9)-II-4	-4067	123	5692	-1.83	2.08	5.01	132.00	192.00	192.00	27
372	(8+9)-VII-2	-4990	-268	7000	-2.24	-4.52	6.17	132.00	192.00	192.00	18
372	(8+9)-V-3	5287	305	-7482	2.38	5.15	-6.59	132.00	192.00	192.00	13
372	(8+9)-VII-3	5071	251	-7171	2.28	4.25	-6.32	132.00	192.00	192.00	14
372	(8+9)-VI-1	3783	-130	-5380	1.70	-2.20	-4.74	132.00	192.00	192.00	20
372	(8+9)-IV-3	4968	-106	-7058	2.23	-1.80	-6.22	132.00	192.00	192.00	17
372	(8+9)-II-1	4147	-139	-5863	1.86	-2.36	-5.16	132.00	192.00	192.00	19
372	(8+9)-II-2	-5610	-88	7925	-2.52	-1.49	6.98	132.00	192.00	192.00	23
372	(8+9)-V-2	-5207	-321	7311	-2.34	-5.43	6.44	132.00	192.00	192.00	16
372	(8+9)-VI-4	-3703	114	5210	-1.67	1.92	4.59	132.00	192.00	192.00	29
372	(8+9)-IV-2	-4888	90	6888	-2.20	1.52	6.07	132.00	192.00	192.00	25
372	(8+9)-VIII-2	-5251	99	7370	-2.36	1.68	6.49	132.00	192.00	192.00	23
372	(8+9)-VIII-3	5331	-116	-7541	2.40	-1.96	-6.64	132.00	192.00	192.00	16
372	(8+9)-II-3	5690	72	-8095	2.56	1.21	-7.13	132.00	192.00	192.00	16
Verifiche nella direzione secondaria											
0	(8+9)-VIII-4	3052	-2	341	16.95	-0.76	30.58	132.00	192.00	192.00	3.4
0	(8+9)-VII-2	4947	-11	581	27.47	-3.55	52.03	132.00	192.00	192.00	2.0
0	(8+9)-III-3	-4823	1	-431	-26.79	0.28	-38.63	132.00	192.00	192.00	4.5
0	(8+9)-IV-2	5163	-5	560	28.67	-1.61	50.16	132.00	192.00	192.00	2.1
0	(8+9)-III-4	-2088	-2	-148	-11.59	-0.71	-13.24	132.00	192.00	192.00	13
0	(8+9)-VIII-2	5399	-8	604	29.99	-2.58	54.15	132.00	192.00	192.00	1.9
0	(8+9)-IV-1	-3954	5	-385	-21.96	1.69	-34.50	132.00	192.00	192.00	5.0
0	(8+9)-VII-4	-2877	8	-296	-15.98	2.52	-26.55	132.00	192.00	192.00	6.3
0	(8+9)-I-1	1172	3	122	6.51	0.90	10.89	132.00	192.00	192.00	9.0
0	(8+9)-IV-3	-5828	5	-559	-32.37	1.57	-50.08	132.00	192.00	192.00	3.4
0	(8+9)-I-3	-5073	2	-458	-28.18	0.50	-41.06	132.00	192.00	192.00	4.2
0	(8+9)-IV-4	3289	-5	386	18.27	-1.73	34.57	132.00	192.00	192.00	3.1
0	(8+9)-II-1	-4789	8	-475	-26.60	2.44	-42.58	132.00	192.00	192.00	3.9
0	(8+9)-V-1	1961	-7	270	10.89	-2.33	24.21	132.00	192.00	192.00	4.5
0	(8+9)-II-3	-6663	7	-649	-37.01	2.32	-58.16	132.00	192.00	192.00	2.8
0	(8+9)-V-2	5197	-12	608	28.87	-3.77	54.45	132.00	192.00	192.00	1.9
0	(8+9)-III-1	1423	2	149	7.90	0.68	13.31	132.00	192.00	192.00	7.5
0	(8+9)-V-3	-5862	12	-607	-32.56	3.73	-54.37	132.00	192.00	192.00	3.0
0	(8+9)-VIII-3	-6064	8	-604	-33.68	2.54	-54.07	132.00	192.00	192.00	3.1
0	(8+9)-V-4	-2626	7	-269	-14.58	2.30	-24.13	132.00	192.00	192.00	7.0
0	(8+9)-VII-3	-5612	11	-580	-31.17	3.51	-51.95	132.00	192.00	192.00	3.2
0	(8+9)-VI-1	-4553	5	-431	-25.29	1.47	-38.58	132.00	192.00	192.00	4.4
0	(8+9)-I-4	-1837	-3	-121	-10.20	-0.94	-10.81	132.00	192.00	192.00	16
0	(8+9)-VI-2	6235	-10	695	34.63	-3.32	62.23	132.00	192.00	192.00	1.7
0	(8+9)-II-4	4125	-8	476	22.91	-2.47	42.65	132.00	192.00	192.00	2.4
0	(8+9)-VIII-1	-3717	2	-340	-20.65	0.72	-30.50	132.00	192.00	192.00	5.7
0	(8+9)-I-2	4408	-2	459	24.48	-0.54	41.13	132.00	192.00	192.00	2.5
0	(8+9)-II-2	5998	-7	650	33.31	-2.36	58.24	132.00	192.00	192.00	1.8
0	(8+9)-III-2	4158	-1	432	23.09	-0.31	38.71	132.00	192.00	192.00	2.6

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-VI-3	-6900	10	-694	-38.32	3.29	-62.16	132.00	192.00	192.00	2.6
0	(8+9)-VI-4	3888	-5	432	21.59	-1.50	38.66	132.00	192.00	192.00	2.7
0	(8+9)-VII-1	2212	-8	297	12.28	-2.56	26.63	132.00	192.00	192.00	4.1
1532	1	-597	0	-16	-3.32	0.03	-1.44	79.20	115.20	115.20	74
1532	2	-991	0	-27	-5.51	0.01	-2.42	118.80	172.80	172.80	66
1532	3	-991	0	-27	-5.51	0.01	-2.42	118.80	172.80	172.80	66
1532	4	-597	0	-16	-3.32	0.03	-1.44	105.60	153.60	153.60	100
1532	5	-597	0	-16	-3.32	0.03	-1.44	105.60	153.60	153.60	100
1532	6	-597	0	-16	-3.32	0.03	-1.44	105.60	153.60	153.60	100
1532	7	-597	0	-16	-3.32	0.03	-1.44	105.60	153.60	153.60	100

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Ty kg	τ_d kg/cmq	fvd kg/cmq	RS	Cs
0	1	5	0.00	3.84	Si	>100
0	2	11	0.00	5.76	Si	>100
0	3	11	0.00	5.76	Si	>100
0	4	5	0.00	5.12	Si	>100
0	5	5	0.00	5.12	Si	>100
0	6	5	0.00	5.12	Si	>100
0	7	5	0.00	5.12	Si	>100
0	(8+9)-VIII-1	209	0.07	6.40	Si	91
0	(8+9)-IV-4	-176	0.06	6.40	Si	>100
0	(8+9)-VII-1	329	0.11	6.40	Si	58
0	(8+9)-V-3	-262	0.09	6.40	Si	73
0	(8+9)-VI-2	11	0.00	6.40	Si	>100
0	(8+9)-V-2	270	0.09	6.40	Si	71
0	(8+9)-IV-1	183	0.06	6.40	Si	>100
0	(8+9)-VII-4	-322	0.11	6.40	Si	59
0	(8+9)-VIII-4	-202	0.07	6.40	Si	95
186	(8+9)-VIII-3	38	0.01	6.40	Si	>100
186	(8+9)-II-2	-21	0.01	6.40	Si	>100
186	(8+9)-VIII-2	-30	0.01	6.40	Si	>100
186	(8+9)-II-3	29	0.01	6.40	Si	>100
186	(8+9)-IV-2	-60	0.02	6.40	Si	>100
186	(8+9)-IV-3	67	0.02	6.40	Si	>100
372	(8+9)-I-2	250	0.08	6.40	Si	78
372	(8+9)-VII-2	280	0.09	6.40	Si	70
372	(8+9)-V-1	334	0.11	6.40	Si	59
372	(8+9)-VII-3	-273	0.09	6.40	Si	72
372	(8+9)-III-3	-249	0.08	6.40	Si	79
372	(8+9)-II-4	-178	0.06	6.40	Si	>100
372	(8+9)-VI-1	193	0.06	6.40	Si	>100
372	(8+9)-I-1	310	0.10	6.40	Si	63
372	(8+9)-VI-3	12	0.00	6.40	Si	>100
372	(8+9)-II-1	185	0.06	6.40	Si	>100
372	(8+9)-III-1	304	0.10	6.40	Si	64
372	(8+9)-I-4	-302	0.10	6.40	Si	65
372	(8+9)-V-4	-326	0.11	6.40	Si	60
372	(8+9)-VI-4	-185	0.06	6.40	Si	>100
372	(8+9)-III-4	-296	0.10	6.40	Si	66
372	(8+9)-III-2	256	0.08	6.40	Si	76
372	(8+9)-I-3	-243	0.08	6.40	Si	81
Verifiche nella direzione secondaria						
0	2	2	0.01	5.76	Si	>100
0	3	2	0.01	5.76	Si	>100
0	(8+9)-VII-1	26	0.14	6.40	Si	47
0	(8+9)-III-3	-25	0.13	6.40	Si	50
0	(8+9)-VIII-3	-21	0.11	6.40	Si	60
0	(8+9)-III-4	-18	0.09	6.40	Si	70
0	(8+9)-VII-4	-26	0.13	6.40	Si	48
0	(8+9)-IV-1	-6	0.03	6.40	Si	>100
0	(8+9)-I-1	17	0.09	6.40	Si	74

X	Comb.	Ty	τ_d	fvd	RS	Cs
0	(8+9)-IV-2	19	0.10	6.40	Si	66
0	(8+9)-I-3	-27	0.14	6.40	Si	47
0	(8+9)-IV-3	-19	0.10	6.40	Si	67
0	(8+9)-II-1	-10	0.05	6.40	Si	>100
0	(8+9)-IV-4	6	0.03	6.40	Si	>100
0	(8+9)-II-3	-23	0.12	6.40	Si	53
0	(8+9)-V-1	25	0.13	6.40	Si	50
0	(8+9)-III-1	18	0.09	6.40	Si	68
0	(8+9)-V-2	35	0.18	6.40	Si	35
0	(8+9)-VIII-2	21	0.11	6.40	Si	58
0	(8+9)-V-3	-35	0.18	6.40	Si	36
0	(8+9)-I-2	27	0.14	6.40	Si	46
0	(8+9)-V-4	-24	0.13	6.40	Si	51
0	(8+9)-II-2	24	0.12	6.40	Si	52
0	(8+9)-III-2	26	0.13	6.40	Si	49
0	(8+9)-VII-3	-33	0.17	6.40	Si	38
0	(8+9)-I-4	-16	0.08	6.40	Si	76
0	(8+9)-II-4	11	0.06	6.40	Si	>100
0	(8+9)-VII-2	34	0.17	6.40	Si	37
0	(8+9)-VI-2	26	0.14	6.40	Si	47
0	(8+9)-VI-3	-26	0.13	6.40	Si	48
1532	1	-1	0.01	3.84	Si	>100
1532	4	-1	0.01	5.12	Si	>100
1532	5	-1	0.01	5.12	Si	>100
1532	6	-1	0.01	5.12	Si	>100
1532	7	-1	0.01	5.12	Si	>100
1532	(8+9)-VI-4	11	0.06	6.40	Si	>100
1532	(8+9)-VI-1	-12	0.06	6.40	Si	>100
1532	(8+9)-VIII-1	-9	0.04	6.40	Si	>100
1532	(8+9)-VIII-4	7	0.04	6.40	Si	>100

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	1	-441	-0.30	19.20	63	-0.07	12.00	>100	V	63
0	2	-713	-0.49	28.80	58	-0.12	18.00	>100	V	58
0	3	-713	-0.49	28.80	58	-0.12	18.00	>100	V	58
0	4	-441	-0.30	25.60	84	-0.07	16.00	>100	V	84
0	5	-441	-0.30	25.60	84	-0.07	16.00	>100	V	84
0	6	-441	-0.30	25.60	84	-0.07	16.00	>100	V	84
0	7	-441	-0.30	25.60	84	-0.07	16.00	>100	V	84
0	(8+9)-VIII-4	-5238	-3.62	32.00	8.8	-0.88	20.00	23	V	8.8
0	(8+9)-V-1	-4355	-3.01	32.00	11	-0.73	20.00	27	V	11
0	(8+9)-I-2	-7829	-5.41	32.00	5.9	-1.31	20.00	15	V	5.9
0	(8+9)-V-2	-9226	-6.38	32.00	5.0	-1.54	20.00	13	V	5.0
0	(8+9)-I-4	2337	1.61	32.00	20	0.39	20.00	51	V	20
0	(8+9)-V-3	8606	5.95	32.00	5.4	1.44	20.00	14	V	5.4
0	(8+9)-II-2	-9954	-6.88	32.00	4.7	-1.66	20.00	12	V	4.7
0	(8+9)-V-4	3735	2.58	32.00	12	0.62	20.00	32	V	12
0	(8+9)-II-4	-6904	-4.77	32.00	6.7	-1.15	20.00	17	V	6.7
0	(8+9)-VIII-2	-9126	-6.31	32.00	5.1	-1.53	20.00	13	V	5.1
0	(8+9)-III-1	-3331	-2.30	32.00	14	-0.56	20.00	36	V	14
0	(8+9)-III-2	-7454	-5.15	32.00	6.2	-1.25	20.00	16	V	6.2
0	(8+9)-III-4	2711	1.87	32.00	17	0.45	20.00	44	V	17
0	(8+9)-VI-2	-10373	-7.17	32.00	4.5	-1.73	20.00	12	V	4.5
0	(8+9)-IV-2	-8707	-6.02	32.00	5.3	-1.46	20.00	14	V	5.3
0	(8+9)-VI-3	9753	6.74	32.00	4.7	1.63	20.00	12	V	4.7
0	(8+9)-IV-4	-5657	-3.91	32.00	8.2	-0.95	20.00	21	V	8.2
0	(8+9)-VI-4	-6485	-4.48	32.00	7.1	-1.08	20.00	18	V	7.1
0	(8+9)-VIII-3	8506	5.88	32.00	5.4	1.42	20.00	14	V	5.4
0	(8+9)-VII-1	-4729	-3.27	32.00	9.8	-0.79	20.00	25	V	9.8
0	(8+9)-III-3	6834	4.72	32.00	6.8	1.14	20.00	18	V	6.8
0	(8+9)-IV-3	8086	5.59	32.00	5.7	1.35	20.00	15	V	5.7

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
0	(8+9)-I-3	7208	4.98	32.00	6.4	1.21	20.00	17	V	6.4
0	(8+9)-II-3	9334	6.45	32.00	5.0	1.56	20.00	13	V	5.0
0	(8+9)-I-1	-2957	-2.04	32.00	16	-0.49	20.00	40	V	16
0	(8+9)-VII-2	-8852	-6.12	32.00	5.2	-1.48	20.00	14	V	5.2
0	(8+9)-VII-3	8232	5.69	32.00	5.6	1.38	20.00	15	V	5.6
0	(8+9)-VII-4	4109	2.84	32.00	11	0.69	20.00	29	V	11
186	(8+9)-IV-1	5152	3.52	32.00	9.1	0.85	20.00	23	V	9.1
186	(8+9)-VIII-1	4682	3.20	32.00	10	0.77	20.00	26	V	10
186	(8+9)-II-1	6413	4.38	32.00	7.3	1.06	20.00	19	V	7.3
186	(8+9)-VI-1	5943	4.06	32.00	7.9	0.98	20.00	20	V	7.9
Verifiche nella direzione secondaria										
1532	1	38	0.21	19.20	91	0.05	12.00	>100	V	91
1532	2	64	0.35	28.80	81	0.09	18.00	>100	V	81
1532	3	64	0.35	28.80	81	0.09	18.00	>100	V	81
1532	4	38	0.21	25.60	>100	0.05	16.00	>100	V	>100
1532	5	38	0.21	25.60	>100	0.05	16.00	>100	V	>100
1532	6	38	0.21	25.60	>100	0.05	16.00	>100	V	>100
1532	7	38	0.21	25.60	>100	0.05	16.00	>100	V	>100
1532	(8+9)-VIII-4	804	4.47	32.00	7.2	1.08	20.00	18	V	7.2
1532	(8+9)-IV-2	1323	7.35	32.00	4.4	1.78	20.00	11	V	4.4
1532	(8+9)-V-1	646	3.59	32.00	8.9	0.87	20.00	23	V	8.9
1532	(8+9)-I-2	1134	6.30	32.00	5.1	1.52	20.00	13	V	5.1
1532	(8+9)-V-2	1412	7.84	32.00	4.1	1.90	20.00	11	V	4.1
1532	(8+9)-I-4	-315	-1.75	32.00	18	-0.42	20.00	47	V	18
1532	(8+9)-V-3	-1359	-7.55	32.00	4.2	-1.83	20.00	11	V	4.2
1532	(8+9)-II-2	1520	8.44	32.00	3.8	2.04	20.00	9.8	V	3.8
1532	(8+9)-V-4	-593	-3.29	32.00	9.7	-0.80	20.00	25	V	9.7
1532	(8+9)-II-4	1086	6.03	32.00	5.3	1.46	20.00	14	V	5.3
1532	(8+9)-VI-1	-950	-5.27	32.00	6.1	-1.28	20.00	16	V	6.1
1532	(8+9)-III-2	1074	5.97	32.00	5.4	1.44	20.00	14	V	5.4
1532	(8+9)-VI-2	1604	8.91	32.00	3.6	2.16	20.00	9.3	V	3.6
1532	(8+9)-III-4	-374	-2.08	32.00	15	-0.50	20.00	40	V	15
1532	(8+9)-VI-3	-1551	-8.62	32.00	3.7	-2.08	20.00	9.6	V	3.7
1532	(8+9)-I-1	368	2.04	32.00	16	0.49	20.00	40	V	16
1532	(8+9)-VI-4	1002	5.57	32.00	5.7	1.35	20.00	15	V	5.7
1532	(8+9)-IV-4	888	4.93	32.00	6.5	1.19	20.00	17	V	6.5
1532	(8+9)-VII-1	705	3.92	32.00	8.2	0.95	20.00	21	V	8.2
1532	(8+9)-II-1	-1033	-5.74	32.00	5.6	-1.39	20.00	14	V	5.6
1532	(8+9)-VII-2	1352	7.51	32.00	4.3	1.82	20.00	11	V	4.3
1532	(8+9)-III-1	427	2.37	32.00	13	0.57	20.00	35	V	13
1532	(8+9)-VII-3	-1300	-7.22	32.00	4.4	-1.75	20.00	11	V	4.4
1532	(8+9)-IV-1	-835	-4.64	32.00	6.9	-1.12	20.00	18	V	6.9
1532	(8+9)-VII-4	-653	-3.62	32.00	8.8	-0.88	20.00	23	V	8.8
1532	(8+9)-III-3	-1022	-5.68	32.00	5.6	-1.37	20.00	15	V	5.6
1532	(8+9)-IV-3	-1270	-7.05	32.00	4.5	-1.71	20.00	12	V	4.5
1532	(8+9)-II-3	-1468	-8.15	32.00	3.9	-1.97	20.00	10	V	3.9
1532	(8+9)-VIII-1	-752	-4.18	32.00	7.7	-1.01	20.00	20	V	7.7
1532	(8+9)-VIII-2	1406	7.81	32.00	4.1	1.89	20.00	11	V	4.1
1532	(8+9)-VIII-3	-1353	-7.52	32.00	4.3	-1.82	20.00	11	V	4.3
1532	(8+9)-I-3	-1081	-6.00	32.00	5.3	-1.45	20.00	14	V	5.3

Setto 9: origine (1681.3,976.3,60.0), direzione (-0.201275,0.979535,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	(8+9)-III-1	354	43	-583	0.41	1.86	-3.35	132.00	192.00	192.00	33
0	(8+9)-I-1	295	39	-496	0.34	1.68	-2.85	132.00	192.00	192.00	38
1500	1	-292	9	26	-0.33	0.40	0.15	79.20	115.20	115.20	>100
1500	2	-582	20	41	-0.67	0.86	0.24	118.80	172.80	172.80	>100
1500	3	-582	20	41	-0.67	0.86	0.24	118.80	172.80	172.80	>100
1500	4	-292	9	26	-0.33	0.40	0.15	105.60	153.60	153.60	>100
1500	5	-292	9	26	-0.33	0.40	0.15	105.60	153.60	153.60	>100
1500	6	-292	9	26	-0.33	0.40	0.15	105.60	153.60	153.60	>100

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
1500	7	-292	9	26	-0.33	0.40	0.15	105.60	153.60	153.60	>100
1500	(8+9)-IV-3	3838	14	-2555	4.41	0.62	-14.66	132.00	192.00	192.00	8.9
1500	(8+9)-V-4	1753	-4	-1221	2.01	-0.19	-7.01	132.00	192.00	192.00	19
1500	(8+9)-I-4	859	-9	-635	0.99	-0.40	-3.64	132.00	192.00	192.00	35
1500	(8+9)-VI-1	2812	23	-1926	3.23	0.98	-11.05	132.00	192.00	192.00	11
1500	(8+9)-II-2	-4848	-5	2995	-5.57	-0.20	17.19	132.00	192.00	192.00	11
1500	(8+9)-VI-2	-5116	-6	3171	-5.87	-0.26	18.20	132.00	192.00	192.00	10
1500	(8+9)-II-4	-3495	-11	2143	-4.01	-0.49	12.30	132.00	192.00	192.00	15
1500	(8+9)-VI-3	4702	19	-3129	5.40	0.81	-17.96	132.00	192.00	192.00	7.2
1500	(8+9)-III-2	-3474	14	2086	-3.99	0.62	11.97	132.00	192.00	192.00	15
1500	(8+9)-VI-4	-3227	-10	1968	-3.70	-0.43	11.29	132.00	192.00	192.00	16
1500	(8+9)-III-4	1037	-8	-755	1.19	-0.36	-4.33	132.00	192.00	192.00	30
1500	(8+9)-VII-1	-2346	16	1382	-2.69	0.70	7.93	132.00	192.00	192.00	22
1500	(8+9)-IV-2	-4253	-2	2596	-4.88	-0.07	14.90	132.00	192.00	192.00	13
1500	(8+9)-VII-2	-4368	9	2672	-5.01	0.41	15.33	132.00	192.00	192.00	12
1500	(8+9)-IV-4	-2900	-8	1744	-3.33	-0.36	10.01	132.00	192.00	192.00	18
1500	(8+9)-VII-3	3953	3	-2630	4.54	0.14	-15.09	132.00	192.00	192.00	8.8
1500	(8+9)-V-2	-4546	9	2792	-5.22	0.37	16.02	132.00	192.00	192.00	12
1500	(8+9)-VII-4	1931	-4	-1340	2.22	-0.15	-7.69	132.00	192.00	192.00	17
1500	(8+9)-II-1	3080	24	-2101	3.54	1.04	-12.06	132.00	192.00	192.00	11
1500	(8+9)-VIII-1	2217	20	-1527	2.54	0.85	-8.76	132.00	192.00	192.00	14
1500	(8+9)-I-3	3237	-1	-2164	3.72	-0.03	-12.42	132.00	192.00	192.00	11
1500	(8+9)-VIII-2	-4521	-3	2772	-5.19	-0.13	15.91	132.00	192.00	192.00	12
1500	(8+9)-IV-1	2485	21	-1702	2.85	0.91	-9.77	132.00	192.00	192.00	13
1500	(8+9)-VIII-3	4106	16	-2730	4.71	0.68	-15.67	132.00	192.00	192.00	8.3
1500	(8+9)-V-1	-2168	17	1263	-2.49	0.74	7.25	132.00	192.00	192.00	24
1500	(8+9)-II-3	4434	17	-2954	5.09	0.75	-16.95	132.00	192.00	192.00	7.6
1500	(8+9)-III-3	3059	-2	-2044	3.51	-0.07	-11.73	132.00	192.00	192.00	11
1500	(8+9)-I-2	-3652	13	2206	-4.19	0.58	12.66	132.00	192.00	192.00	14
1500	(8+9)-V-3	4131	4	-2750	4.74	0.18	-15.78	132.00	192.00	192.00	8.4
1500	(8+9)-VIII-4	-2631	-7	1569	-3.02	-0.30	9.00	132.00	192.00	192.00	21
Verifiche nella direzione secondaria											
600	(8+9)-II-1	-327	-16	3876	-0.45	-1.28	21.35	132.00	192.00	192.00	8.5
600	(8+9)-VI-1	-367	-23	3590	-0.51	-1.78	19.78	132.00	192.00	192.00	8.9
1200	1	-1668	-2	-562	-2.30	-0.12	-3.10	79.20	115.20	115.20	35
1200	2	-2764	-4	-990	-3.81	-0.31	-5.46	118.80	172.80	172.80	30
1200	3	-2764	-4	-990	-3.81	-0.31	-5.46	118.80	172.80	172.80	30
1200	4	-1668	-2	-562	-2.30	-0.12	-3.10	105.60	153.60	153.60	47
1200	5	-1668	-2	-562	-2.30	-0.12	-3.10	105.60	153.60	153.60	47
1200	6	-1668	-2	-562	-2.30	-0.12	-3.10	105.60	153.60	153.60	47
1200	7	-1668	-2	-562	-2.30	-0.12	-3.10	105.60	153.60	153.60	47
1200	(8+9)-VIII-4	-1062	31	-3683	-1.46	2.43	-20.29	132.00	192.00	192.00	8.4
1200	(8+9)-IV-3	-398	-4	6228	-0.55	-0.34	34.32	132.00	192.00	192.00	5.5
1200	(8+9)-V-2	-2359	-54	-8229	-3.25	-4.23	-45.34	132.00	192.00	192.00	3.9
1200	(8+9)-I-4	451	42	2912	0.62	3.28	16.04	132.00	192.00	192.00	9.5
1200	(8+9)-V-3	56	52	7433	0.08	4.07	40.95	132.00	192.00	192.00	4.3
1200	(8+9)-II-2	-943	-18	-7219	-1.30	-1.42	-39.77	132.00	192.00	192.00	4.7
1200	(8+9)-V-4	435	49	4225	0.60	3.89	23.28	132.00	192.00	192.00	6.8
1200	(8+9)-II-4	-95	8	-4270	-0.13	0.65	-23.53	132.00	192.00	192.00	7.9
1200	(8+9)-I-1	-2755	-44	-3708	-3.79	-3.44	-20.43	132.00	192.00	192.00	8.0
1200	(8+9)-III-2	-2664	-40	-6858	-3.67	-3.14	-37.79	132.00	192.00	192.00	4.7
1200	(8+9)-VI-2	-938	-20	-7613	-1.29	-1.60	-41.94	132.00	192.00	192.00	4.4
1200	(8+9)-III-4	163	48	2970	0.22	3.75	16.36	132.00	192.00	192.00	9.4
1200	(8+9)-VI-3	-1365	18	6816	-1.88	1.44	37.55	132.00	192.00	192.00	4.9
1200	(8+9)-IV-2	-1905	2	-7025	-2.62	0.18	-38.70	132.00	192.00	192.00	4.9
1200	(8+9)-VI-4	-100	11	-3876	-0.14	0.83	-21.36	132.00	192.00	192.00	8.7
1200	(8+9)-IV-4	-1057	29	-4076	-1.46	2.25	-22.46	132.00	192.00	192.00	7.8
1200	(8+9)-VII-1	-2450	-58	-5080	-3.38	-4.53	-27.99	132.00	192.00	192.00	5.9
1200	(8+9)-I-3	72	44	6120	0.10	3.46	33.72	132.00	192.00	192.00	5.1
1200	(8+9)-VII-2	-2648	-48	-8171	-3.65	-3.75	-45.02	132.00	192.00	192.00	3.9
1200	(8+9)-III-1	-2466	-50	-3767	-3.40	-3.92	-20.75	132.00	192.00	192.00	7.8
1200	(8+9)-VII-3	345	46	7375	0.47	3.59	40.63	132.00	192.00	192.00	4.3
1200	(8+9)-IV-1	-1246	-31	3280	-1.72	-2.41	18.07	132.00	192.00	192.00	9.4
1200	(8+9)-VII-4	147	55	4283	0.20	4.36	23.60	132.00	192.00	192.00	6.8

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
1200	(8+9)-III-3	361	38	6061	0.50	2.98	33.40	132.00	192.00	192.00	5.2
1200	(8+9)-I-2	-2375	-46	-6916	-3.27	-3.62	-38.11	132.00	192.00	192.00	4.6
1200	(8+9)-II-3	-1360	16	6422	-1.87	1.25	35.38	132.00	192.00	192.00	5.2
1200	(8+9)-VIII-1	-1241	-33	2886	-1.71	-2.60	15.90	132.00	192.00	192.00	10
1200	(8+9)-VIII-2	-1900	-0	-7419	-2.62	-0.01	-40.88	132.00	192.00	192.00	4.7
1200	(8+9)-VIII-3	-403	-2	6622	-0.56	-0.16	36.49	132.00	192.00	192.00	5.2
1200	(8+9)-V-1	-2739	-51	-5022	-3.77	-4.05	-27.67	132.00	192.00	192.00	6.0

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
0	(8+9)-V-2	-24	0.02	6.40	Si	>100
0	(8+9)-IV-3	7	0.01	6.40	Si	>100
0	(8+9)-III-1	-12	0.01	6.40	Si	>100
0	(8+9)-I-2	-12	0.01	6.40	Si	>100
0	(8+9)-VIII-1	-4	0.00	6.40	Si	>100
0	(8+9)-I-3	14	0.01	6.40	Si	>100
0	(8+9)-VI-1	-7	0.01	6.40	Si	>100
0	(8+9)-I-4	14	0.01	6.40	Si	>100
0	(8+9)-V-1	-24	0.02	6.40	Si	>100
0	(8+9)-VII-2	-25	0.02	6.40	Si	>100
0	(8+9)-I-1	-12	0.01	6.40	Si	>100
0	(8+9)-III-3	14	0.01	6.40	Si	>100
0	(8+9)-VI-2	-7	0.01	6.40	Si	>100
0	(8+9)-VII-1	-23	0.02	6.40	Si	>100
750	(8+9)-VI-3	11	0.01	6.40	Si	>100
750	(8+9)-II-3	7	0.01	6.40	Si	>100
750	(8+9)-V-4	28	0.02	6.40	Si	>100
750	(8+9)-VI-4	11	0.01	6.40	Si	>100
750	(8+9)-III-4	14	0.01	6.40	Si	>100
750	(8+9)-VII-3	28	0.02	6.40	Si	>100
750	(8+9)-VIII-3	11	0.01	6.40	Si	>100
750	(8+9)-II-4	7	0.01	6.40	Si	>100
750	(8+9)-V-3	28	0.02	6.40	Si	>100
750	(8+9)-VII-4	28	0.02	6.40	Si	>100
1500	1	11	0.01	3.84	Si	>100
1500	2	25	0.02	5.76	Si	>100
1500	3	25	0.02	5.76	Si	>100
1500	4	11	0.01	5.12	Si	>100
1500	5	11	0.01	5.12	Si	>100
1500	6	11	0.01	5.12	Si	>100
1500	7	11	0.01	5.12	Si	>100
1500	(8+9)-IV-4	13	0.01	6.40	Si	>100
1500	(8+9)-IV-2	15	0.01	6.40	Si	>100
1500	(8+9)-II-1	9	0.01	6.40	Si	>100
1500	(8+9)-III-2	14	0.01	6.40	Si	>100
1500	(8+9)-IV-1	2	0.00	6.40	Si	>100
1500	(8+9)-VIII-2	13	0.01	6.40	Si	>100
1500	(8+9)-II-2	9	0.01	6.40	Si	>100
1500	(8+9)-VIII-4	15	0.01	6.40	Si	>100
Verifiche nella direzione secondaria						
0	(8+9)-II-1	9	0.01	6.40	Si	>100
0	(8+9)-VI-1	11	0.01	6.40	Si	>100
600	(8+9)-VIII-4	17	0.02	6.40	Si	>100
1200	1	15	0.02	3.84	Si	>100
1200	2	35	0.04	5.76	Si	>100
1200	3	35	0.04	5.76	Si	>100
1200	4	15	0.02	5.12	Si	>100
1200	5	15	0.02	5.12	Si	>100
1200	6	15	0.02	5.12	Si	>100
1200	7	15	0.02	5.12	Si	>100
1200	(8+9)-IV-3	-42	0.05	6.40	Si	>100
1200	(8+9)-V-1	91	0.12	6.40	Si	55

X	Comb.	Ty	τ_d	fvd	RS	Cs
1200	(8+9)-I-1	75	0.10	6.40	Si	67
1200	(8+9)-V-3	-88	0.11	6.40	Si	57
1200	(8+9)-II-2	62	0.08	6.40	Si	82
1200	(8+9)-V-4	-70	0.09	6.40	Si	72
1200	(8+9)-II-4	18	0.02	6.40	Si	>100
1200	(8+9)-I-2	93	0.12	6.40	Si	54
1200	(8+9)-III-2	93	0.12	6.40	Si	54
1200	(8+9)-VI-2	66	0.08	6.40	Si	76
1200	(8+9)-III-4	-54	0.07	6.40	Si	94
1200	(8+9)-VI-3	-46	0.06	6.40	Si	>100
1200	(8+9)-IV-2	63	0.08	6.40	Si	80
1200	(8+9)-VI-4	13	0.02	6.40	Si	>100
1200	(8+9)-IV-4	19	0.02	6.40	Si	>100
1200	(8+9)-VII-1	91	0.12	6.40	Si	56
1200	(8+9)-V-2	108	0.14	6.40	Si	46
1200	(8+9)-VII-2	109	0.14	6.40	Si	46
1200	(8+9)-III-1	75	0.09	6.40	Si	67
1200	(8+9)-VII-3	-88	0.11	6.40	Si	57
1200	(8+9)-IV-1	2	0.00	6.40	Si	>100
1200	(8+9)-VII-4	-70	0.09	6.40	Si	72
1200	(8+9)-III-3	-72	0.09	6.40	Si	70
1200	(8+9)-I-4	-54	0.07	6.40	Si	93
1200	(8+9)-II-3	-41	0.05	6.40	Si	>100
1200	(8+9)-VIII-1	7	0.01	6.40	Si	>100
1200	(8+9)-VIII-2	68	0.09	6.40	Si	74
1200	(8+9)-VIII-3	-47	0.06	6.40	Si	>100
1200	(8+9)-I-3	-72	0.09	6.40	Si	70

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
1500	1	-287	-0.49	19.20	39	-0.12	12.00	>100	V	39
1500	2	-441	-0.76	28.80	38	-0.18	18.00	98	V	38
1500	3	-441	-0.76	28.80	38	-0.18	18.00	98	V	38
1500	4	-287	-0.49	25.60	52	-0.12	16.00	>100	V	52
1500	5	-287	-0.49	25.60	52	-0.12	16.00	>100	V	52
1500	6	-287	-0.49	25.60	52	-0.12	16.00	>100	V	52
1500	7	-287	-0.49	25.60	52	-0.12	16.00	>100	V	52
1500	(8+9)-VIII-4	-4400	-7.58	32.00	4.2	-1.83	20.00	11	V	4.2
1500	(8+9)-IV-1	4454	7.67	32.00	4.2	1.86	20.00	11	V	4.2
1500	(8+9)-V-1	-3592	-6.18	32.00	5.2	-1.50	20.00	13	V	5.2
1500	(8+9)-I-2	-6107	-10.52	32.00	3.0	-2.54	20.00	7.9	V	3.0
1500	(8+9)-V-2	-7662	-13.19	32.00	2.4	-3.19	20.00	6.3	V	2.4
1500	(8+9)-I-4	1625	2.80	32.00	11	0.68	20.00	30	V	11
1500	(8+9)-V-3	7249	12.48	32.00	2.6	3.02	20.00	6.6	V	2.6
1500	(8+9)-II-2	-8149	-14.03	32.00	2.3	-3.40	20.00	5.9	V	2.3
1500	(8+9)-V-4	3180	5.47	32.00	5.8	1.32	20.00	15	V	5.8
1500	(8+9)-II-4	-5829	-10.04	32.00	3.2	-2.43	20.00	8.2	V	3.2
1500	(8+9)-VI-1	4950	8.52	32.00	3.8	2.06	20.00	9.7	V	3.8
1500	(8+9)-III-2	-5818	-10.02	32.00	3.2	-2.42	20.00	8.2	V	3.2
1500	(8+9)-VI-2	-8615	-14.83	32.00	2.2	-3.59	20.00	5.6	V	2.2
1500	(8+9)-III-4	1914	3.30	32.00	9.7	0.80	20.00	25	V	9.7
1500	(8+9)-VI-3	8203	14.12	32.00	2.3	3.42	20.00	5.9	V	2.3
1500	(8+9)-IV-2	-7186	-12.37	32.00	2.6	-2.99	20.00	6.7	V	2.6
1500	(8+9)-VI-4	-5363	-9.23	32.00	3.5	-2.23	20.00	9.0	V	3.5
1500	(8+9)-IV-4	-4866	-8.38	32.00	3.8	-2.03	20.00	9.9	V	3.8
1500	(8+9)-VII-1	-3881	-6.68	32.00	4.8	-1.62	20.00	12	V	4.8
1500	(8+9)-II-1	5417	9.33	32.00	3.4	2.26	20.00	8.9	V	3.4
1500	(8+9)-VII-2	-7373	-12.69	32.00	2.5	-3.07	20.00	6.5	V	2.5
1500	(8+9)-III-1	-2326	-4.01	32.00	8.0	-0.97	20.00	21	V	8.0
1500	(8+9)-VII-3	6961	11.98	32.00	2.7	2.90	20.00	6.9	V	2.7
1500	(8+9)-I-1	-2038	-3.51	32.00	9.1	-0.85	20.00	24	V	9.1
1500	(8+9)-VII-4	3469	5.97	32.00	5.4	1.45	20.00	14	V	5.4

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
1500	(8+9)-III-3	5406	9.31	32.00	3.4	2.25	20.00	8.9	V	3.4
1500	(8+9)-IV-3	6774	11.66	32.00	2.7	2.82	20.00	7.1	V	2.7
1500	(8+9)-II-3	7737	13.32	32.00	2.4	3.22	20.00	6.2	V	2.4
1500	(8+9)-VIII-1	3988	6.87	32.00	4.7	1.66	20.00	12	V	4.7
1500	(8+9)-VIII-2	-7652	-13.18	32.00	2.4	-3.19	20.00	6.3	V	2.4
1500	(8+9)-VIII-3	7240	12.47	32.00	2.6	3.02	20.00	6.6	V	2.6
1500	(8+9)-I-3	5695	9.81	32.00	3.3	2.37	20.00	8.4	V	3.3
Verifiche nella direzione secondaria										
0	1	177	0.24	19.20	79	0.06	12.00	>100	V	79
0	2	342	0.47	28.80	61	0.11	18.00	>100	V	61
0	3	342	0.47	28.80	61	0.11	18.00	>100	V	61
0	4	177	0.24	25.60	>100	0.06	16.00	>100	V	>100
0	5	177	0.24	25.60	>100	0.06	16.00	>100	V	>100
0	6	177	0.24	25.60	>100	0.06	16.00	>100	V	>100
0	7	177	0.24	25.60	>100	0.06	16.00	>100	V	>100
600	(8+9)-VIII-4	4629	6.38	32.00	5.0	1.54	20.00	13	V	5.0
600	(8+9)-IV-2	7640	10.52	32.00	3.0	2.55	20.00	7.9	V	3.0
600	(8+9)-V-1	3711	5.11	32.00	6.3	1.24	20.00	16	V	6.3
600	(8+9)-I-2	6520	8.98	32.00	3.6	2.17	20.00	9.2	V	3.6
600	(8+9)-V-2	8167	11.25	32.00	2.8	2.72	20.00	7.3	V	2.8
600	(8+9)-I-4	-1869	-2.57	32.00	12	-0.62	20.00	32	V	12
600	(8+9)-V-3	-7972	-10.98	32.00	2.9	-2.66	20.00	7.5	V	2.9
600	(8+9)-II-2	8783	12.10	32.00	2.6	2.93	20.00	6.8	V	2.6
600	(8+9)-V-4	-3516	-4.84	32.00	6.6	-1.17	20.00	17	V	6.6
600	(8+9)-II-4	6266	8.63	32.00	3.7	2.09	20.00	9.6	V	3.7
600	(8+9)-VI-1	-5577	-7.68	32.00	4.2	-1.86	20.00	11	V	4.2
600	(8+9)-III-2	6177	8.51	32.00	3.8	2.06	20.00	9.7	V	3.8
600	(8+9)-VI-2	9277	12.78	32.00	2.5	3.09	20.00	6.5	V	2.5
600	(8+9)-III-4	-2212	-3.05	32.00	11	-0.74	20.00	27	V	11
600	(8+9)-VI-3	-9082	-12.51	32.00	2.6	-3.03	20.00	6.6	V	2.6
600	(8+9)-I-1	2064	2.84	32.00	11	0.69	20.00	29	V	11
600	(8+9)-VI-4	5772	7.95	32.00	4.0	1.92	20.00	10	V	4.0
600	(8+9)-IV-4	5123	7.06	32.00	4.5	1.71	20.00	12	V	4.5
600	(8+9)-VII-1	4053	5.58	32.00	5.7	1.35	20.00	15	V	5.7
600	(8+9)-II-1	-6071	-8.36	32.00	3.8	-2.02	20.00	9.9	V	3.8
600	(8+9)-VII-2	7824	10.78	32.00	3.0	2.61	20.00	7.7	V	3.0
600	(8+9)-III-1	2407	3.31	32.00	9.7	0.80	20.00	25	V	9.7
600	(8+9)-VII-3	-7629	-10.51	32.00	3.0	-2.54	20.00	7.9	V	3.0
600	(8+9)-VII-4	-3859	-5.32	32.00	6.0	-1.29	20.00	16	V	6.0
600	(8+9)-I-3	-6325	-8.71	32.00	3.7	-2.11	20.00	9.5	V	3.7
600	(8+9)-III-3	-5983	-8.24	32.00	3.9	-1.99	20.00	10	V	3.9
600	(8+9)-IV-3	-7445	-10.26	32.00	3.1	-2.48	20.00	8.1	V	3.1
600	(8+9)-II-3	-8588	-11.83	32.00	2.7	-2.86	20.00	7.0	V	2.7
600	(8+9)-VIII-3	-7939	-10.94	32.00	2.9	-2.65	20.00	7.6	V	2.9
600	(8+9)-VIII-2	8134	11.20	32.00	2.9	2.71	20.00	7.4	V	2.9
1200	(8+9)-VIII-1	-4480	-6.17	32.00	5.2	-1.49	20.00	13	V	5.2
1200	(8+9)-IV-1	-4950	-6.82	32.00	4.7	-1.65	20.00	12	V	4.7

Setto 10: origine (1681.3,976.3,307.8), direzione (-0.201275,0.979535,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	(8+9)-VIII-4	-5127	-608	-445	-9.33	-41.54	-6.42	132.00	192.00	192.00	4.0
0	(8+9)-IV-1	6262	648	483	11.39	44.30	6.96	132.00	192.00	192.00	2.8
0	(8+9)-VI-4	-6224	-379	-566	-11.32	-25.92	-8.16	132.00	192.00	192.00	5.5
0	(8+9)-III-2	-6527	604	-604	-11.88	41.31	-8.72	132.00	192.00	192.00	3.8
0	(8+9)-IV-2	-8507	-201	-747	-15.48	-13.74	-10.77	132.00	192.00	192.00	7.5
0	(8+9)-III-3	7015	-593	588	12.77	-40.53	8.47	132.00	192.00	192.00	2.8
0	(8+9)-VIII-2	-9154	-230	-801	-16.66	-15.72	-11.56	132.00	192.00	192.00	6.7
0	(8+9)-III-4	2585	-848	219	4.70	-57.94	3.15	132.00	192.00	192.00	2.8
0	(8+9)-VII-4	4740	-751	401	8.62	-51.35	5.79	132.00	192.00	192.00	2.8
0	(8+9)-VII-2	-8682	508	-787	-15.80	34.73	-11.35	132.00	192.00	192.00	4.1
0	(8+9)-I-2	-6856	673	-641	-12.48	46.00	-9.24	132.00	192.00	192.00	3.4

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-I-4	2256	-779	182	4.10	-53.26	2.63	132.00	192.00	192.00	3.1
0	(8+9)-IV-3	8996	212	730	16.37	14.52	10.53	132.00	192.00	192.00	3.9
0	(8+9)-VII-3	9171	-497	770	16.69	-33.94	11.11	132.00	192.00	192.00	2.8
0	(8+9)-IV-4	-5774	-637	-500	-10.51	-43.52	-7.21	132.00	192.00	192.00	3.7
0	(8+9)-II-4	-6870	-408	-621	-12.50	-27.90	-8.95	132.00	192.00	192.00	5.1
0	(8+9)-V-1	-3923	694	-382	-7.14	47.45	-5.51	132.00	192.00	192.00	3.6
0	(8+9)-VIII-3	9642	241	785	17.55	16.50	11.32	132.00	192.00	192.00	3.6
0	(8+9)-V-2	-9011	577	-823	-16.40	39.41	-11.87	132.00	192.00	192.00	3.6
0	(8+9)-I-1	-1767	791	-199	-3.22	54.04	-2.87	132.00	192.00	192.00	3.4
0	(8+9)-V-3	9500	-565	806	17.29	-38.63	11.63	132.00	192.00	192.00	2.5
0	(8+9)-II-1	7358	420	604	13.39	28.68	8.71	132.00	192.00	192.00	3.4
0	(8+9)-V-4	4411	-683	365	8.03	-46.67	5.27	132.00	192.00	192.00	3.0
0	(8+9)-III-1	-2096	859	-236	-3.81	58.73	-3.40	132.00	192.00	192.00	3.1
0	(8+9)-I-3	7344	-661	624	13.36	-45.21	9.00	132.00	192.00	192.00	2.6
0	(8+9)-II-3	10092	-16	851	18.36	-1.09	12.27	132.00	192.00	192.00	4.8
0	(8+9)-VIII-1	5616	619	428	10.22	42.32	6.17	132.00	192.00	192.00	3.0
0	(8+9)-VI-1	6712	391	549	12.21	26.71	7.92	132.00	192.00	192.00	3.7
0	(8+9)-VII-1	-4251	763	-418	-7.74	52.14	-6.03	132.00	192.00	192.00	3.3
0	(8+9)-VI-3	10739	13	905	19.54	0.88	13.06	132.00	192.00	192.00	4.5
750	1	325	21	158	0.50	1.20	1.59	79.20	115.20	115.20	33
750	2	506	44	276	0.77	2.54	2.79	118.80	172.80	172.80	27
750	3	506	44	276	0.77	2.54	2.79	118.80	172.80	172.80	27
750	4	325	21	158	0.50	1.20	1.59	105.60	153.60	153.60	44
750	5	325	21	158	0.50	1.20	1.59	105.60	153.60	153.60	44
750	6	325	21	158	0.50	1.20	1.59	105.60	153.60	153.60	44
750	7	325	21	158	0.50	1.20	1.59	105.60	153.60	153.60	44
1500	(8+9)-VI-2	-8011	-267	923	-10.49	-13.16	6.89	132.00	192.00	192.00	9.3
1500	(8+9)-II-2	-7176	-292	1062	-9.40	-14.36	7.93	132.00	192.00	192.00	8.4
Verifiche nella direzione secondaria											
0	(8+9)-VIII-4	-1385	25	2608	-1.91	1.98	14.37	132.00	192.00	192.00	12
0	(8+9)-IV-4	-1290	10	2948	-1.78	0.79	16.24	132.00	192.00	192.00	11
0	(8+9)-II-2	-1904	11	4420	-2.62	0.87	24.35	132.00	192.00	192.00	7.6
0	(8+9)-IV-2	-1950	16	3843	-2.69	1.25	21.17	132.00	192.00	192.00	8.6
0	(8+9)-II-3	406	-5	-3482	0.56	-0.41	-19.18	132.00	192.00	192.00	9.4
0	(8+9)-VIII-2	-1855	1	4183	-2.56	0.05	23.05	132.00	192.00	192.00	8.3
0	(8+9)-II-4	-1243	5	3525	-1.71	0.41	19.42	132.00	192.00	192.00	9.7
0	(8+9)-VII-4	-227	47	-1278	-0.31	3.68	-7.04	132.00	192.00	192.00	18
0	(8+9)-VI-1	-159	-15	-2247	-0.22	-1.15	-12.38	132.00	192.00	192.00	14
0	(8+9)-VII-2	-1793	-35	3972	-2.47	-2.75	21.89	132.00	192.00	192.00	7.8
0	(8+9)-V-4	-213	45	-1105	-0.29	3.57	-6.09	132.00	192.00	192.00	20
0	(8+9)-VI-3	310	10	-3822	0.43	0.78	-21.06	132.00	192.00	192.00	8.5
0	(8+9)-V-3	281	42	-3207	0.39	3.32	-17.67	132.00	192.00	192.00	8.9
0	(8+9)-II-1	-255	1	-2587	-0.35	0.05	-14.25	132.00	192.00	192.00	13
0	(8+9)-V-2	-1779	-36	4146	-2.45	-2.87	22.84	132.00	192.00	192.00	7.5
0	(8+9)-VI-4	-1339	20	3185	-1.84	1.61	17.55	132.00	192.00	192.00	10
0	(8+9)-VI-2	-1808	-4	4760	-2.49	-0.32	26.23	132.00	192.00	192.00	7.2
0	(8+9)-VIII-3	357	5	-3244	0.49	0.41	-17.87	132.00	192.00	192.00	10
0	(8+9)-VII-3	295	41	-3034	0.41	3.21	-16.71	132.00	192.00	192.00	9.4
0	(8+9)-IV-1	-208	-4	-2009	-0.29	-0.33	-11.07	132.00	192.00	192.00	17
0	(8+9)-VIII-1	-113	-19	-1669	-0.16	-1.52	-9.20	132.00	192.00	192.00	18
0	(8+9)-IV-3	453	-10	-2904	0.62	-0.79	-16.00	132.00	192.00	192.00	11
526	1	-664	9	760	-0.92	0.74	4.19	79.20	115.20	115.20	23
526	2	-800	20	1539	-1.10	1.57	8.48	118.80	172.80	172.80	17
526	3	-800	20	1539	-1.10	1.57	8.48	118.80	172.80	172.80	17
526	4	-664	9	760	-0.92	0.74	4.19	105.60	153.60	153.60	31
526	5	-664	9	760	-0.92	0.74	4.19	105.60	153.60	153.60	31
526	6	-664	9	760	-0.92	0.74	4.19	105.60	153.60	153.60	31
526	7	-664	9	760	-0.92	0.74	4.19	105.60	153.60	153.60	31
526	(8+9)-VII-1	-856	117	1187	-1.18	9.23	6.54	132.00	192.00	192.00	12
526	(8+9)-V-1	-849	115	1132	-1.17	9.04	6.23	132.00	192.00	192.00	13
526	(8+9)-III-1	-667	235	893	-0.92	18.49	4.92	132.00	192.00	192.00	8.2
526	(8+9)-I-1	-660	232	837	-0.91	18.30	4.61	132.00	192.00	192.00	8.4
526	(8+9)-I-4	-237	-219	212	-0.33	-17.27	1.17	132.00	192.00	192.00	10
526	(8+9)-I-3	171	-213	-545	0.24	-16.76	-3.00	132.00	192.00	192.00	9.5

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
526	(8+9)-III-2	-1062	223	1539	-1.46	17.59	8.48	132.00	192.00	192.00	7.4
526	(8+9)-III-3	165	-210	-490	0.23	-16.57	-2.70	132.00	192.00	192.00	9.8
526	(8+9)-III-4	-230	-222	157	-0.32	-17.47	0.86	132.00	192.00	192.00	10
526	(8+9)-I-2	-1068	226	1595	-1.47	17.79	8.79	132.00	192.00	192.00	7.2

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
0	(8+9)-VI-2	-6	0.01	6.40	Si	>100
0	(8+9)-VIII-3	31	0.04	6.40	Si	>100
750	(8+9)-III-3	777	0.86	6.40	Si	7.4
750	(8+9)-I-3	779	0.86	6.40	Si	7.4
750	(8+9)-IV-3	118	0.13	6.40	Si	49
750	(8+9)-II-1	-359	0.40	6.40	Si	16
750	(8+9)-II-2	-97	0.11	6.40	Si	59
750	(8+9)-III-4	860	0.95	6.40	Si	6.7
750	(8+9)-II-3	124	0.14	6.40	Si	46
750	(8+9)-I-2	-752	0.83	6.40	Si	7.7
750	(8+9)-I-4	858	0.95	6.40	Si	6.7
750	(8+9)-IV-1	-365	0.40	6.40	Si	16
750	(8+9)-I-1	-831	0.92	6.40	Si	7.0
750	(8+9)-IV-4	392	0.43	6.40	Si	15
750	(8+9)-II-4	386	0.43	6.40	Si	15
750	(8+9)-III-1	-833	0.92	6.40	Si	6.9
750	(8+9)-III-2	-750	0.83	6.40	Si	7.7
1500	1	25	0.02	3.84	Si	>100
1500	2	53	0.05	5.76	Si	>100
1500	3	53	0.05	5.76	Si	>100
1500	4	25	0.02	5.12	Si	>100
1500	5	25	0.02	5.12	Si	>100
1500	6	25	0.02	5.12	Si	>100
1500	7	25	0.02	5.12	Si	>100
1500	(8+9)-VI-4	411	0.39	6.40	Si	16
1500	(8+9)-VII-4	776	0.74	6.40	Si	8.7
1500	(8+9)-V-3	651	0.62	6.40	Si	10
1500	(8+9)-VIII-1	-418	0.40	6.40	Si	16
1500	(8+9)-VI-1	-377	0.36	6.40	Si	18
1500	(8+9)-VIII-2	37	0.04	6.40	Si	>100
1500	(8+9)-VI-3	37	0.04	6.40	Si	>100
1500	(8+9)-IV-2	125	0.12	6.40	Si	54
1500	(8+9)-VII-1	-742	0.71	6.40	Si	9.1
1500	(8+9)-VIII-4	452	0.43	6.40	Si	15
1500	(8+9)-VII-3	639	0.61	6.40	Si	11
1500	(8+9)-V-2	-617	0.59	6.40	Si	11
1500	(8+9)-V-1	-729	0.69	6.40	Si	9.2
1500	(8+9)-VII-2	-605	0.58	6.40	Si	11
1500	(8+9)-V-4	764	0.73	6.40	Si	8.8
Verifiche nella direzione secondaria						
0	(8+9)-VI-2	39	0.05	6.40	Si	>100
0	(8+9)-VIII-2	12	0.02	6.40	Si	>100
0	(8+9)-VI-3	-34	0.04	6.40	Si	>100
526	1	14	0.02	3.84	Si	>100
526	2	30	0.04	5.76	Si	>100
526	3	30	0.04	5.76	Si	>100
526	4	14	0.02	5.12	Si	>100
526	5	14	0.02	5.12	Si	>100
526	6	14	0.02	5.12	Si	>100
526	7	14	0.02	5.12	Si	>100
526	(8+9)-VIII-4	-120	0.15	6.40	Si	42
526	(8+9)-IV-3	-414	0.53	6.40	Si	12
526	(8+9)-V-3	-185	0.24	6.40	Si	27
526	(8+9)-II-1	554	0.70	6.40	Si	9.1
526	(8+9)-V-4	-217	0.28	6.40	Si	23

X	Comb.	Ty	τ_d	fvd	RS	Cs
526	(8+9)-II-3	-428	0.54	6.40	Si	12
526	(8+9)-VI-1	126	0.16	6.40	Si	40
526	(8+9)-III-1	1666	2.12	6.40	Si	3.0
526	(8+9)-I-3	-1611	2.05	6.40	Si	3.1
526	(8+9)-III-3	-1606	2.04	6.40	Si	3.1
526	(8+9)-I-2	1631	2.07	6.40	Si	3.1
526	(8+9)-IV-1	568	0.72	6.40	Si	8.9
526	(8+9)-VI-4	-106	0.13	6.40	Si	47
526	(8+9)-I-4	-1642	2.09	6.40	Si	3.1
526	(8+9)-VII-1	241	0.31	6.40	Si	21
526	(8+9)-V-1	237	0.30	6.40	Si	21
526	(8+9)-VII-2	201	0.26	6.40	Si	25
526	(8+9)-II-2	448	0.57	6.40	Si	11
526	(8+9)-VII-3	-181	0.23	6.40	Si	28
526	(8+9)-III-2	1626	2.07	6.40	Si	3.1
526	(8+9)-VII-4	-221	0.28	6.40	Si	23
526	(8+9)-V-2	205	0.26	6.40	Si	25
526	(8+9)-II-4	-534	0.68	6.40	Si	9.4
526	(8+9)-III-4	-1646	2.09	6.40	Si	3.1
526	(8+9)-IV-4	-548	0.70	6.40	Si	9.2
526	(8+9)-VIII-1	140	0.18	6.40	Si	36
526	(8+9)-I-1	1662	2.11	6.40	Si	3.0
526	(8+9)-VIII-3	14	0.02	6.40	Si	>100
526	(8+9)-IV-2	434	0.55	6.40	Si	12

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	2	-765	-2.09	28.80	14	-0.51	18.00	36	V	14
0	3	-765	-2.09	28.80	14	-0.51	18.00	36	V	14
0	(8+9)-V-2	-2904	-7.93	32.00	4.0	-1.92	20.00	10	V	4.0
0	(8+9)-II-2	-3062	-8.36	32.00	3.8	-2.02	20.00	9.9	V	3.8
0	(8+9)-VIII-4	-1792	-4.89	32.00	6.5	-1.18	20.00	17	V	6.5
0	(8+9)-II-4	-2251	-6.14	32.00	5.2	-1.49	20.00	13	V	5.2
0	(8+9)-VIII-2	-2920	-7.97	32.00	4.0	-1.93	20.00	10	V	4.0
0	(8+9)-III-1	-1065	-2.91	32.00	11	-0.70	20.00	28	V	11
0	(8+9)-VII-1	-1594	-4.35	32.00	7.4	-1.05	20.00	19	V	7.4
0	(8+9)-III-2	-2285	-6.24	32.00	5.1	-1.51	20.00	13	V	5.1
0	(8+9)-I-2	-2375	-6.48	32.00	4.9	-1.57	20.00	13	V	4.9
0	(8+9)-VI-2	-3221	-8.79	32.00	3.6	-2.13	20.00	9.4	V	3.6
0	(8+9)-VI-3	2575	7.03	32.00	4.6	1.70	20.00	12	V	4.6
0	(8+9)-VI-1	1446	3.95	32.00	8.1	0.96	20.00	21	V	8.1
0	(8+9)-VIII-3	2274	6.21	32.00	5.2	1.50	20.00	13	V	5.2
0	(8+9)-VII-2	-2814	-7.68	32.00	4.2	-1.86	20.00	11	V	4.2
0	(8+9)-IV-2	-2762	-7.54	32.00	4.2	-1.82	20.00	11	V	4.2
0	(8+9)-VI-4	-2093	-5.71	32.00	5.6	-1.38	20.00	14	V	5.6
0	(8+9)-II-3	2416	6.59	32.00	4.9	1.60	20.00	13	V	4.9
0	(8+9)-I-1	-975	-2.66	32.00	12	-0.64	20.00	31	V	12
0	(8+9)-II-1	1605	4.38	32.00	7.3	1.06	20.00	19	V	7.3
0	(8+9)-IV-3	2116	5.77	32.00	5.5	1.40	20.00	14	V	5.5
0	(8+9)-IV-4	-1951	-5.32	32.00	6.0	-1.29	20.00	16	V	6.0
0	(8+9)-V-1	-1504	-4.10	32.00	7.8	-0.99	20.00	20	V	7.8
1500	1	671	1.32	19.20	15	0.32	12.00	38	V	15
1500	4	671	1.32	25.60	19	0.32	16.00	50	V	19
1500	5	671	1.32	25.60	19	0.32	16.00	50	V	19
1500	6	671	1.32	25.60	19	0.32	16.00	50	V	19
1500	7	671	1.32	25.60	19	0.32	16.00	50	V	19
1500	(8+9)-IV-1	1840	3.61	32.00	8.9	0.87	20.00	23	V	8.9
1500	(8+9)-V-3	3557	6.99	32.00	4.6	1.69	20.00	12	V	4.6
1500	(8+9)-VII-4	2297	4.51	32.00	7.1	1.09	20.00	18	V	7.1
1500	(8+9)-III-3	2848	5.59	32.00	5.7	1.35	20.00	15	V	5.7
1500	(8+9)-VII-3	3453	6.78	32.00	4.7	1.64	20.00	12	V	4.7
1500	(8+9)-I-4	1588	3.12	32.00	10	0.75	20.00	26	V	10

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
1500	(8+9)-VIII-1	1659	3.26	32.00	9.8	0.79	20.00	25	V	9.8
1500	(8+9)-III-4	1692	3.32	32.00	9.6	0.80	20.00	25	V	9.6
1500	(8+9)-V-4	2193	4.31	32.00	7.4	1.04	20.00	19	V	7.4
1500	(8+9)-I-3	2952	5.80	32.00	5.5	1.40	20.00	14	V	5.5
Verifiche nella direzione secondaria										
0	(8+9)-VIII-4	2123	2.92	32.00	11	0.71	20.00	28	V	11
0	(8+9)-IV-3	-3723	-5.13	32.00	6.2	-1.24	20.00	16	V	6.2
0	(8+9)-I-4	-1882	-2.59	32.00	12	-0.63	20.00	32	V	12
0	(8+9)-IV-2	3769	5.19	32.00	6.2	1.26	20.00	16	V	6.2
0	(8+9)-V-2	3604	4.96	32.00	6.4	1.20	20.00	17	V	6.4
0	(8+9)-VII-2	3466	4.77	32.00	6.7	1.16	20.00	17	V	6.7
0	(8+9)-II-2	4231	5.83	32.00	5.5	1.41	20.00	14	V	5.5
0	(8+9)-VI-4	2585	3.56	32.00	9.0	0.86	20.00	23	V	9.0
0	(8+9)-II-3	-4185	-5.76	32.00	5.6	-1.39	20.00	14	V	5.6
0	(8+9)-I-1	1928	2.66	32.00	12	0.64	20.00	31	V	12
0	(8+9)-V-1	1603	2.21	32.00	14	0.53	20.00	37	V	14
0	(8+9)-I-3	-3883	-5.35	32.00	6.0	-1.29	20.00	15	V	6.0
0	(8+9)-III-1	2066	2.85	32.00	11	0.69	20.00	29	V	11
0	(8+9)-I-2	3929	5.41	32.00	5.9	1.31	20.00	15	V	5.9
0	(8+9)-VIII-2	3672	5.06	32.00	6.3	1.22	20.00	16	V	6.3
0	(8+9)-VI-2	4133	5.69	32.00	5.6	1.38	20.00	15	V	5.6
0	(8+9)-III-2	3791	5.22	32.00	6.1	1.26	20.00	16	V	6.1
0	(8+9)-III-3	-3745	-5.16	32.00	6.2	-1.25	20.00	16	V	6.2
0	(8+9)-III-4	-2020	-2.78	32.00	11	-0.67	20.00	30	V	11
0	(8+9)-VII-1	1741	2.40	32.00	13	0.58	20.00	34	V	13
526	1	-172	-0.24	19.20	81	-0.06	12.00	>100	V	81
526	2	-293	-0.40	28.80	71	-0.10	18.00	>100	V	71
526	3	-293	-0.40	28.80	71	-0.10	18.00	>100	V	71
526	4	-172	-0.24	25.60	>100	-0.06	16.00	>100	V	>100
526	5	-172	-0.24	25.60	>100	-0.06	16.00	>100	V	>100
526	6	-172	-0.24	25.60	>100	-0.06	16.00	>100	V	>100
526	7	-172	-0.24	25.60	>100	-0.06	16.00	>100	V	>100
526	(8+9)-IV-1	-2281	-3.14	32.00	10	-0.76	20.00	26	V	10
526	(8+9)-II-4	2509	3.46	32.00	9.3	0.84	20.00	24	V	9.3
526	(8+9)-V-4	-1804	-2.48	32.00	13	-0.60	20.00	33	V	13
526	(8+9)-VII-4	-1941	-2.67	32.00	12	-0.65	20.00	31	V	12
526	(8+9)-II-1	-2739	-3.77	32.00	8.5	-0.91	20.00	22	V	8.5
526	(8+9)-VI-1	-2614	-3.60	32.00	8.9	-0.87	20.00	23	V	8.9
526	(8+9)-VII-3	-3648	-5.02	32.00	6.4	-1.22	20.00	16	V	6.4
526	(8+9)-V-3	-3785	-5.21	32.00	6.1	-1.26	20.00	16	V	6.1
526	(8+9)-VIII-1	-2156	-2.97	32.00	11	-0.72	20.00	28	V	11
526	(8+9)-IV-4	2051	2.83	32.00	11	0.68	20.00	29	V	11
526	(8+9)-VIII-3	-3764	-5.18	32.00	6.2	-1.25	20.00	16	V	6.2
526	(8+9)-VI-3	-4221	-5.81	32.00	5.5	-1.41	20.00	14	V	5.5

Setto 11: origine (1721.5,780.4,263.2), direzione (-0.201275,0.979535,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	1	195	-11	-129	0.31	-0.69	-1.43	79.20	115.20	115.20	45
0	2	284	-23	-201	0.45	-1.40	-2.23	118.80	172.80	172.80	40
0	3	284	-23	-201	0.45	-1.40	-2.23	118.80	172.80	172.80	40
0	4	195	-11	-129	0.31	-0.69	-1.43	105.60	153.60	153.60	60
0	5	195	-11	-129	0.31	-0.69	-1.43	105.60	153.60	153.60	60
0	6	195	-11	-129	0.31	-0.69	-1.43	105.60	153.60	153.60	60
0	7	195	-11	-129	0.31	-0.69	-1.43	105.60	153.60	153.60	60
1200	(8+9)-VIII-4	-2456	-622	1974	-3.08	-29.30	13.50	132.00	192.00	192.00	4.5
1200	(8+9)-IV-1	2946	653	-2199	3.69	30.72	-15.04	132.00	192.00	192.00	3.8
1200	(8+9)-V-1	-1873	560	1514	-2.35	26.36	10.36	132.00	192.00	192.00	5.2
1200	(8+9)-I-2	-3048	769	2694	-3.82	36.19	18.43	132.00	192.00	192.00	3.5
1200	(8+9)-V-2	-4196	668	3417	-5.26	31.43	23.38	132.00	192.00	192.00	3.5
1200	(8+9)-I-4	871	-661	-799	1.09	-31.13	-5.47	132.00	192.00	192.00	5.0
1200	(8+9)-V-3	4342	-668	-3425	5.44	-31.43	-23.43	132.00	192.00	192.00	3.1

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
1200	(8+9)-II-2	-4387	394	3692	-5.50	18.54	25.26	132.00	192.00	192.00	4.4
1200	(8+9)-V-4	2019	-560	-1522	2.53	-26.37	-10.41	132.00	192.00	192.00	4.7
1200	(8+9)-II-4	-3211	-35	2644	-4.02	-1.66	18.09	132.00	192.00	192.00	9.7
1200	(8+9)-VI-1	3012	5	-2435	3.78	0.22	-16.66	132.00	192.00	192.00	8.6
1200	(8+9)-III-2	-2925	584	2558	-3.67	27.47	17.50	132.00	192.00	192.00	4.3
1200	(8+9)-VI-2	-4731	363	3909	-5.93	17.11	26.74	132.00	192.00	192.00	4.4
1200	(8+9)-III-4	994	-847	-935	1.25	-39.85	-6.40	132.00	192.00	192.00	4.0
1200	(8+9)-VI-3	4877	-364	-3917	6.11	-17.12	-26.79	132.00	192.00	192.00	3.6
1200	(8+9)-IV-2	-3976	-224	3239	-4.98	-10.53	22.16	132.00	192.00	192.00	5.9
1200	(8+9)-VI-4	-2867	-5	2427	-3.59	-0.23	16.60	132.00	192.00	192.00	11
1200	(8+9)-IV-4	-2800	-653	2191	-3.51	-30.72	14.99	132.00	192.00	192.00	4.2
1200	(8+9)-VII-1	-1997	745	1650	-2.50	35.08	11.29	132.00	192.00	192.00	4.1
1200	(8+9)-II-1	3357	35	-2652	4.21	1.65	-18.14	132.00	192.00	192.00	7.4
1200	(8+9)-VII-2	-4073	482	3281	-5.10	22.71	22.45	132.00	192.00	192.00	4.2
1200	(8+9)-III-1	-849	846	927	-1.06	39.84	6.34	132.00	192.00	192.00	4.2
1200	(8+9)-VII-3	4219	-482	-3289	5.29	-22.71	-22.50	132.00	192.00	192.00	3.6
1200	(8+9)-I-1	-725	661	791	-0.91	31.12	5.41	132.00	192.00	192.00	5.3
1200	(8+9)-VII-4	2142	-745	-1658	2.68	-35.09	-11.34	132.00	192.00	192.00	3.8
1200	(8+9)-III-3	3070	-584	-2567	3.85	-27.48	-17.56	132.00	192.00	192.00	3.8
1200	(8+9)-IV-3	4121	224	-3247	5.16	10.52	-22.21	132.00	192.00	192.00	4.8
1200	(8+9)-II-3	4533	-394	-3700	5.68	-18.54	-25.31	132.00	192.00	192.00	3.7
1200	(8+9)-VIII-1	2601	622	-1982	3.26	29.29	-13.56	132.00	192.00	192.00	4.0
1200	(8+9)-VIII-2	-4320	-254	3455	-5.41	-11.96	23.64	132.00	192.00	192.00	5.4
1200	(8+9)-VIII-3	4466	254	-3464	5.60	11.95	-23.69	132.00	192.00	192.00	4.4
1200	(8+9)-I-3	3194	-769	-2703	4.00	-36.20	-18.49	132.00	192.00	192.00	3.2
Verifiche nella direzione secondaria											
0	(8+9)-VIII-4	-1082	50	3218	-1.86	4.97	27.70	132.00	192.00	192.00	5.9
0	(8+9)-VII-2	-1504	-85	5711	-2.59	-8.36	49.16	132.00	192.00	192.00	3.3
0	(8+9)-III-3	-642	113	-4619	-1.11	11.18	-39.77	132.00	192.00	192.00	3.8
0	(8+9)-IV-2	-1296	-13	5488	-2.23	-1.28	47.25	132.00	192.00	192.00	4.0
0	(8+9)-III-4	-790	127	-1857	-1.36	12.49	-15.99	132.00	192.00	192.00	6.7
0	(8+9)-VIII-2	-1357	-5	5856	-2.34	-0.47	50.41	132.00	192.00	192.00	3.8
0	(8+9)-IV-1	-803	-57	-3720	-1.38	-5.66	-32.02	132.00	192.00	192.00	5.1
0	(8+9)-VII-4	-590	99	-3082	-1.01	9.80	-26.53	132.00	192.00	192.00	5.3
0	(8+9)-I-1	-1163	-122	1467	-2.00	-12.07	12.63	132.00	192.00	192.00	7.8
0	(8+9)-IV-3	-649	14	-5622	-1.12	1.41	-48.40	132.00	192.00	192.00	3.9
0	(8+9)-I-3	-650	117	-4875	-1.12	11.48	-41.97	132.00	192.00	192.00	3.6
0	(8+9)-IV-4	-1143	59	3586	-1.97	5.78	30.87	132.00	192.00	192.00	5.2
0	(8+9)-II-1	-827	-47	-4571	-1.42	-4.65	-39.36	132.00	192.00	192.00	4.4
0	(8+9)-V-1	-1363	-95	2693	-2.35	-9.37	23.18	132.00	192.00	192.00	5.9
0	(8+9)-II-3	-673	25	-6474	-1.16	2.41	-55.74	132.00	192.00	192.00	3.3
0	(8+9)-V-2	-1497	-88	5966	-2.58	-8.66	51.36	132.00	192.00	192.00	3.2
0	(8+9)-III-1	-1155	-126	1723	-1.99	-12.37	14.83	132.00	192.00	192.00	7.1
0	(8+9)-V-3	-449	89	-6100	-0.77	8.79	-52.51	132.00	192.00	192.00	3.1
0	(8+9)-VIII-3	-589	6	-5990	-1.01	0.60	-51.57	132.00	192.00	192.00	3.7
0	(8+9)-V-4	-582	96	-2827	-1.00	9.49	-24.33	132.00	192.00	192.00	5.7
0	(8+9)-VII-3	-442	86	-5844	-0.76	8.48	-50.31	132.00	192.00	192.00	3.3
0	(8+9)-VI-1	-887	-39	-4204	-1.53	-3.84	-36.19	132.00	192.00	192.00	4.8
0	(8+9)-I-4	-783	124	-1601	-1.35	12.19	-13.79	132.00	192.00	192.00	7.4
0	(8+9)-VI-2	-1333	-15	6708	-2.29	-1.48	57.75	132.00	192.00	192.00	3.2
0	(8+9)-II-4	-1119	48	4438	-1.93	4.77	38.20	132.00	192.00	192.00	4.5
0	(8+9)-VIII-1	-864	-49	-3352	-1.49	-4.85	-28.86	132.00	192.00	192.00	5.7
0	(8+9)-I-2	-1296	-115	4741	-2.23	-11.36	40.81	132.00	192.00	192.00	3.7
0	(8+9)-II-2	-1273	-23	6340	-2.19	-2.29	54.58	132.00	192.00	192.00	3.4
0	(8+9)-III-2	-1303	-112	4485	-2.24	-11.06	38.61	132.00	192.00	192.00	3.9
0	(8+9)-VI-3	-613	16	-6842	-1.06	1.61	-58.90	132.00	192.00	192.00	3.2
0	(8+9)-VI-4	-1058	40	4070	-1.82	3.96	35.04	132.00	192.00	192.00	4.9
0	(8+9)-VII-1	-1356	-98	2948	-2.34	-9.67	25.38	132.00	192.00	192.00	5.5
550	1	-1249	0	129	-2.15	0.03	1.11	79.20	115.20	115.20	98
550	2	-2123	1	218	-3.66	0.12	1.87	118.80	172.80	172.80	84
550	3	-2123	1	218	-3.66	0.12	1.87	118.80	172.80	172.80	84
550	4	-1249	0	129	-2.15	0.03	1.11	105.60	153.60	153.60	>100
550	5	-1249	0	129	-2.15	0.03	1.11	105.60	153.60	153.60	>100
550	6	-1249	0	129	-2.15	0.03	1.11	105.60	153.60	153.60	>100

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
550	7	-1249	0	129	-2.15	0.03	1.11	105.60	153.60	153.60	>100

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Ty kg	τ_d kg/cmq	fvd kg/cmq	RS	Cs
0	1	8	0.01	3.84	Si	>100
0	2	16	0.02	5.76	Si	>100
0	3	16	0.02	5.76	Si	>100
0	4	8	0.01	5.12	Si	>100
0	5	8	0.01	5.12	Si	>100
0	6	8	0.01	5.12	Si	>100
0	7	8	0.01	5.12	Si	>100
0	(8+9)-V-1	442	0.51	6.40	Si	12
0	(8+9)-VI-1	218	0.25	6.40	Si	25
0	(8+9)-I-2	316	0.37	6.40	Si	17
0	(8+9)-I-3	-305	0.35	6.40	Si	18
0	(8+9)-VII-2	398	0.46	6.40	Si	14
0	(8+9)-I-4	-359	0.42	6.40	Si	15
0	(8+9)-VII-1	432	0.50	6.40	Si	13
0	(8+9)-VII-4	-421	0.49	6.40	Si	13
0	(8+9)-VI-4	-207	0.24	6.40	Si	27
0	(8+9)-II-4	-186	0.22	6.40	Si	30
0	(8+9)-III-2	326	0.38	6.40	Si	17
0	(8+9)-I-1	370	0.43	6.40	Si	15
0	(8+9)-III-4	-349	0.40	6.40	Si	16
0	(8+9)-VII-3	-387	0.45	6.40	Si	14
0	(8+9)-III-1	360	0.42	6.40	Si	15
0	(8+9)-III-3	-315	0.37	6.40	Si	18
0	(8+9)-II-1	197	0.23	6.40	Si	28
0	(8+9)-V-2	388	0.45	6.40	Si	14
0	(8+9)-V-3	-377	0.44	6.40	Si	15
0	(8+9)-V-4	-431	0.50	6.40	Si	13
600	(8+9)-VI-2	82	0.08	6.40	Si	77
600	(8+9)-IV-4	-223	0.23	6.40	Si	28
600	(8+9)-VI-3	-71	0.07	6.40	Si	89
600	(8+9)-VIII-4	-255	0.26	6.40	Si	25
600	(8+9)-VIII-1	266	0.27	6.40	Si	24
600	(8+9)-IV-1	234	0.24	6.40	Si	27
1200	(8+9)-VIII-3	-89	0.08	6.40	Si	79
1200	(8+9)-II-2	-74	0.07	6.40	Si	95
1200	(8+9)-II-3	85	0.08	6.40	Si	83
1200	(8+9)-VIII-2	101	0.09	6.40	Si	70
1200	(8+9)-IV-2	80	0.07	6.40	Si	88
1200	(8+9)-IV-3	-68	0.06	6.40	Si	>100
Verifiche nella direzione secondaria						
0	(8+9)-I-4	25	0.04	6.40	Si	>100
0	(8+9)-VII-4	78	0.12	6.40	Si	52
0	(8+9)-VII-1	-79	0.12	6.40	Si	51
0	(8+9)-V-3	71	0.11	6.40	Si	56
0	(8+9)-V-2	-72	0.11	6.40	Si	56
0	(8+9)-III-3	18	0.03	6.40	Si	>100
0	(8+9)-III-2	-19	0.03	6.40	Si	>100
550	1	-7	0.01	3.84	Si	>100
550	2	-12	0.02	5.76	Si	>100
550	3	-12	0.02	5.76	Si	>100
550	4	-7	0.01	5.12	Si	>100
550	5	-7	0.01	5.12	Si	>100
550	6	-7	0.01	5.12	Si	>100
550	7	-7	0.01	5.12	Si	>100
550	(8+9)-VIII-4	155	0.25	6.40	Si	26
550	(8+9)-V-1	95	0.15	6.40	Si	42
550	(8+9)-I-2	-78	0.12	6.40	Si	52
550	(8+9)-VI-1	95	0.15	6.40	Si	43

X	Comb.	Ty	τ_d	fvd	RS	Cs
550	(8+9)-III-1	-109	0.17	6.40	Si	37
550	(8+9)-VI-2	-58	0.09	6.40	Si	69
550	(8+9)-III-4	99	0.16	6.40	Si	41
550	(8+9)-VI-3	48	0.08	6.40	Si	84
550	(8+9)-IV-2	163	0.26	6.40	Si	25
550	(8+9)-VI-4	-105	0.17	6.40	Si	38
550	(8+9)-IV-4	193	0.31	6.40	Si	21
550	(8+9)-I-1	-32	0.05	6.40	Si	>100
550	(8+9)-II-2	-96	0.15	6.40	Si	42
550	(8+9)-VII-2	127	0.20	6.40	Si	32
550	(8+9)-V-4	-105	0.17	6.40	Si	38
550	(8+9)-VII-3	-137	0.22	6.40	Si	29
550	(8+9)-IV-1	-203	0.32	6.40	Si	20
550	(8+9)-I-3	67	0.11	6.40	Si	60
550	(8+9)-II-4	-67	0.11	6.40	Si	60
550	(8+9)-IV-3	-173	0.28	6.40	Si	23
550	(8+9)-II-1	57	0.09	6.40	Si	71
550	(8+9)-VIII-1	-165	0.26	6.40	Si	24
550	(8+9)-VIII-2	201	0.32	6.40	Si	20
550	(8+9)-VIII-3	-211	0.34	6.40	Si	19
550	(8+9)-II-3	86	0.14	6.40	Si	47

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	(8+9)-V-1	-1766	-4.23	32.00	7.6	-1.02	20.00	20	V	7.6
0	(8+9)-II-2	-4039	-9.66	32.00	3.3	-2.34	20.00	8.6	V	3.3
0	(8+9)-III-2	-2845	-6.81	32.00	4.7	-1.65	20.00	12	V	4.7
0	(8+9)-VIII-4	-2232	-5.34	32.00	6.0	-1.29	20.00	15	V	6.0
0	(8+9)-VII-1	-1920	-4.60	32.00	7.0	-1.11	20.00	18	V	7.0
0	(8+9)-VIII-2	-3743	-8.96	32.00	3.6	-2.17	20.00	9.2	V	3.6
0	(8+9)-V-2	-3730	-8.93	32.00	3.6	-2.16	20.00	9.3	V	3.6
0	(8+9)-VII-2	-3575	-8.56	32.00	3.7	-2.07	20.00	9.7	V	3.7
0	(8+9)-VI-2	-4258	-10.19	32.00	3.1	-2.47	20.00	8.1	V	3.1
0	(8+9)-VI-4	-2747	-6.57	32.00	4.9	-1.59	20.00	13	V	4.9
0	(8+9)-IV-2	-3524	-8.43	32.00	3.8	-2.04	20.00	9.8	V	3.8
0	(8+9)-I-1	-1036	-2.48	32.00	13	-0.60	20.00	33	V	13
0	(8+9)-IV-4	-2451	-5.87	32.00	5.5	-1.42	20.00	14	V	5.5
0	(8+9)-I-2	-2999	-7.18	32.00	4.5	-1.74	20.00	12	V	4.5
0	(8+9)-II-4	-2966	-7.10	32.00	4.5	-1.72	20.00	12	V	4.5
0	(8+9)-III-1	-1190	-2.85	32.00	11	-0.69	20.00	29	V	11
1200	1	548	1.03	19.20	19	0.25	12.00	48	V	19
1200	2	912	1.71	28.80	17	0.41	18.00	43	V	17
1200	3	912	1.71	28.80	17	0.41	18.00	43	V	17
1200	4	548	1.03	25.60	25	0.25	16.00	64	V	25
1200	5	548	1.03	25.60	25	0.25	16.00	64	V	25
1200	6	548	1.03	25.60	25	0.25	16.00	64	V	25
1200	7	548	1.03	25.60	25	0.25	16.00	64	V	25
1200	(8+9)-VI-1	3509	6.60	32.00	4.9	1.60	20.00	13	V	4.9
1200	(8+9)-I-3	3875	7.28	32.00	4.4	1.76	20.00	11	V	4.4
1200	(8+9)-II-3	5136	9.66	32.00	3.3	2.34	20.00	8.6	V	3.3
1200	(8+9)-IV-3	4493	8.44	32.00	3.8	2.04	20.00	9.8	V	3.8
1200	(8+9)-II-1	3770	7.09	32.00	4.5	1.71	20.00	12	V	4.5
1200	(8+9)-V-4	2297	4.32	32.00	7.4	1.05	20.00	19	V	7.4
1200	(8+9)-VII-3	4552	8.56	32.00	3.7	2.07	20.00	9.7	V	3.7
1200	(8+9)-III-4	1620	3.05	32.00	11	0.74	20.00	27	V	11
1200	(8+9)-VII-4	2490	4.68	32.00	6.8	1.13	20.00	18	V	6.8
1200	(8+9)-IV-1	3126	5.88	32.00	5.4	1.42	20.00	14	V	5.4
1200	(8+9)-VI-3	5397	10.15	32.00	3.2	2.46	20.00	8.1	V	3.2
1200	(8+9)-V-3	4745	8.92	32.00	3.6	2.16	20.00	9.3	V	3.6
1200	(8+9)-VIII-1	2865	5.39	32.00	5.9	1.30	20.00	15	V	5.9
1200	(8+9)-I-4	1427	2.68	32.00	12	0.65	20.00	31	V	12
1200	(8+9)-VIII-3	4754	8.94	32.00	3.6	2.16	20.00	9.2	V	3.6

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
1200	(8+9)-III-3	3682	6.92	32.00	4.6	1.67	20.00	12	V	4.6
Verifiche nella direzione secondaria										
0	(8+9)-III-1	1621	2.79	32.00	11	0.68	20.00	30	V	11
0	(8+9)-I-2	4287	7.38	32.00	4.3	1.79	20.00	11	V	4.3
0	(8+9)-VII-4	-2544	-4.38	32.00	7.3	-1.06	20.00	19	V	7.3
0	(8+9)-I-3	-4216	-7.26	32.00	4.4	-1.76	20.00	11	V	4.4
0	(8+9)-V-4	-2321	-4.00	32.00	8.0	-0.97	20.00	21	V	8.0
0	(8+9)-I-4	-1326	-2.28	32.00	14	-0.55	20.00	36	V	14
0	(8+9)-IV-3	-4879	-8.40	32.00	3.8	-2.03	20.00	9.8	V	3.8
0	(8+9)-I-1	1398	2.41	32.00	13	0.58	20.00	34	V	13
0	(8+9)-VII-3	-4988	-8.59	32.00	3.7	-2.08	20.00	9.6	V	3.7
0	(8+9)-V-3	-5211	-8.97	32.00	3.6	-2.17	20.00	9.2	V	3.6
0	(8+9)-III-4	-1549	-2.67	32.00	12	-0.65	20.00	31	V	12
0	(8+9)-III-3	-3993	-6.88	32.00	4.7	-1.66	20.00	12	V	4.7
0	(8+9)-III-2	4064	7.00	32.00	4.6	1.69	20.00	12	V	4.6
0	(8+9)-II-3	-5622	-9.68	32.00	3.3	-2.34	20.00	8.5	V	3.3
550	1	123	0.21	19.20	91	0.05	12.00	>100	V	91
550	2	219	0.38	28.80	76	0.09	18.00	>100	V	76
550	3	219	0.38	28.80	76	0.09	18.00	>100	V	76
550	4	123	0.21	25.60	>100	0.05	16.00	>100	V	>100
550	5	123	0.21	25.60	>100	0.05	16.00	>100	V	>100
550	6	123	0.21	25.60	>100	0.05	16.00	>100	V	>100
550	7	123	0.21	25.60	>100	0.05	16.00	>100	V	>100
550	(8+9)-VIII-4	3120	5.37	32.00	6.0	1.30	20.00	15	V	6.0
550	(8+9)-VI-1	-3666	-6.31	32.00	5.1	-1.53	20.00	13	V	5.1
550	(8+9)-II-4	4186	7.21	32.00	4.4	1.74	20.00	11	V	4.4
550	(8+9)-VII-1	2630	4.53	32.00	7.1	1.10	20.00	18	V	7.1
550	(8+9)-V-1	2414	4.16	32.00	7.7	1.01	20.00	20	V	7.7
550	(8+9)-VII-2	5133	8.84	32.00	3.6	2.14	20.00	9.4	V	3.6
550	(8+9)-IV-4	3464	5.96	32.00	5.4	1.44	20.00	14	V	5.4
550	(8+9)-II-1	-4010	-6.90	32.00	4.6	-1.67	20.00	12	V	4.6
550	(8+9)-IV-1	-3289	-5.66	32.00	5.7	-1.37	20.00	15	V	5.7
550	(8+9)-II-2	5774	9.94	32.00	3.2	2.41	20.00	8.3	V	3.2
550	(8+9)-V-2	5349	9.21	32.00	3.5	2.23	20.00	9.0	V	3.5
550	(8+9)-IV-2	5052	8.70	32.00	3.7	2.11	20.00	9.5	V	3.7
550	(8+9)-VI-2	6118	10.53	32.00	3.0	2.55	20.00	7.8	V	3.0
550	(8+9)-VI-4	3841	6.61	32.00	4.8	1.60	20.00	12	V	4.8
550	(8+9)-VIII-1	-2945	-5.07	32.00	6.3	-1.23	20.00	16	V	6.3
550	(8+9)-VIII-2	5397	9.29	32.00	3.4	2.25	20.00	8.9	V	3.4
550	(8+9)-VIII-3	-5221	-8.99	32.00	3.6	-2.18	20.00	9.2	V	3.6
550	(8+9)-VI-3	-5942	-10.23	32.00	3.1	-2.48	20.00	8.1	V	3.1

Verifiche a instabilità

Setto(X)	Comb.	k _{critc}	k _{critm}	λ_{relc}	λ_{relm}	σ_n	σ_{mx}	σ_{my}	f _{td}	f _{cd}	f _{md}	Cs
(cm)						kg/cm ² q	kg/cm ² q	kg/cm ² q	kg/cm ² q	kg/cm ² q	kg/cm ² q	
6(60.0)	(8+9)-V-2	1.00	--	0.22	--	-5.12	-15.09	8.36	132.00	192.00	192.00	6.7
7(40.0)	(8+9)-V-3	--	--	--	--	2.78	-9.68	-7.26	132.00	192.00	192.00	9.2
8(37.2)	(8+9)-V-3	--	--	--	--	2.38	5.15	-6.59	132.00	192.00	192.00	13
9(150.0)	(8+9)-VI-3	--	--	--	--	5.40	0.81	-17.96	132.00	192.00	192.00	7.2
10(0.0)	(8+9)-V-3	--	--	--	--	17.29	-38.63	11.63	132.00	192.00	192.00	2.5
11(120.0)	(8+9)-V-3	--	--	--	--	5.44	-31.43	-23.43	132.00	192.00	192.00	3.1

Parete Xlam 10 - Nodi: [8-9-2-3-10-11-111-110] - **Crit.Prog.** Criterio di verifica XLAM 0 - **Verificato:**
[Cs=1.656,Comb=(8+9)-VI-2]

Geometria setti

Setto	Crit.	X	L	S	X90	L90	S90
		mm	cm	cm	mm	cm	cm
6	Criterio di verifica XLAM 0	0	375.2	12.1	0	60.0	12.1
		300	381.1	12.1	1935	60.0	12.1
		600	387.0	12.1	--	--	--
7	Criterio di verifica XLAM 0	0	330.0	12.1	0	80.0	12.1
		400	337.8	12.1	1728	80.0	12.1
		800	345.7	12.1	--	--	--
8	Criterio di verifica XLAM 0	0	299.0	12.1	0	37.2	12.1
		186	302.7	12.1	1532	37.2	12.1
		372	306.3	12.1	--	--	--
9	Criterio di verifica XLAM 0	0	120.0	12.1	0	150.0	12.1
		750	120.0	12.1	600	150.0	12.1
		1500	120.0	12.1	1200	150.0	12.1
10	Criterio di verifica XLAM 0	0	75.7	12.1	0	150.0	12.1
		750	90.4	12.1	526	150.0	12.1
		1500	105.2	12.1	--	--	--
11	Criterio di verifica XLAM 0	0	86.3	12.1	0	120.0	12.1
		600	98.1	12.1	550	120.0	12.1
		1200	109.9	12.1	--	--	--

Setto 6: origine (1651.1,1123.2,187.6), direzione (-0.201275,0.979535,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
600	1	-2103	53	3211	-0.75	0.71	1.77	79.20	115.20	115.20	46
600	2	-4263	113	6709	-1.52	1.51	3.70	118.80	172.80	172.80	33
600	3	-4263	113	6709	-1.52	1.51	3.70	118.80	172.80	172.80	33
600	4	-2103	53	3211	-0.75	0.71	1.77	105.60	153.60	153.60	62
600	5	-2103	53	3211	-0.75	0.71	1.77	105.60	153.60	153.60	62
600	6	-2103	53	3211	-0.75	0.71	1.77	105.60	153.60	153.60	62
600	7	-2103	53	3211	-0.75	0.71	1.77	105.60	153.60	153.60	62
600	(8+9)-VIII-4	-9194	1200	9807	-3.27	16.05	5.41	132.00	192.00	192.00	8.9
600	(8+9)-IV-1	7201	-1157	-6269	2.56	-15.47	-3.46	132.00	192.00	192.00	8.5
600	(8+9)-V-1	-7180	-1213	8152	-2.56	-16.22	4.50	132.00	192.00	192.00	9.3
600	(8+9)-I-2	-11417	-1226	12292	-4.06	-16.40	6.78	132.00	192.00	192.00	8.3
600	(8+9)-V-2	-14395	-1128	15151	-5.12	-15.09	8.36	132.00	192.00	192.00	8.1
600	(8+9)-I-4	1315	1383	-898	0.47	18.49	-0.50	132.00	192.00	192.00	9.8
600	(8+9)-V-3	11508	1201	-10756	4.10	16.06	-5.94	132.00	192.00	192.00	6.9
600	(8+9)-II-2	-15379	-214	15842	-5.47	-2.87	8.74	132.00	192.00	192.00	16
600	(8+9)-V-4	4293	1285	-3757	1.53	17.19	-2.07	132.00	192.00	192.00	8.9
600	(8+9)-II-4	-11559	568	11885	-4.11	7.60	6.56	132.00	192.00	192.00	13
600	(8+9)-VI-1	7779	-466	-6632	2.77	-6.24	-3.66	132.00	192.00	192.00	14
600	(8+9)-III-2	-10976	-1028	11926	-3.91	-13.74	6.58	132.00	192.00	192.00	9.4
600	(8+9)-VI-2	-16272	-185	16700	-5.79	-2.48	9.22	132.00	192.00	192.00	16
600	(8+9)-III-4	1756	1582	-1264	0.63	21.15	-0.70	132.00	192.00	192.00	8.4
600	(8+9)-VI-3	13385	258	-12305	4.76	3.44	-6.79	132.00	192.00	192.00	11
600	(8+9)-IV-2	-13907	447	14622	-4.95	5.97	8.07	132.00	192.00	192.00	14
600	(8+9)-VI-4	-10666	539	11027	-3.80	7.21	6.09	132.00	192.00	192.00	14
600	(8+9)-IV-4	-10088	1229	10665	-3.59	16.44	5.89	132.00	192.00	192.00	8.6
600	(8+9)-VII-1	-7621	-1411	8518	-2.71	-18.87	4.70	132.00	192.00	192.00	8.1
600	(8+9)-II-1	8672	-496	-7490	3.09	-6.63	-4.13	132.00	192.00	192.00	13
600	(8+9)-VII-2	-13954	-930	14785	-4.97	-12.44	8.16	132.00	192.00	192.00	9.3
600	(8+9)-III-1	-4643	-1509	5659	-1.65	-20.18	3.12	132.00	192.00	192.00	8.2
600	(8+9)-VII-3	11067	1003	-10390	3.94	13.41	-5.73	132.00	192.00	192.00	7.7
600	(8+9)-I-1	-4202	-1311	5293	-1.50	-17.52	2.92	132.00	192.00	192.00	9.4
600	(8+9)-VII-4	4734	1484	-4123	1.69	19.84	-2.28	132.00	192.00	192.00	7.8
600	(8+9)-III-3	8089	1100	-7531	2.88	14.71	-4.16	132.00	192.00	192.00	8.3
600	(8+9)-IV-3	11021	-374	-10226	3.92	-5.00	-5.64	132.00	192.00	192.00	12
600	(8+9)-II-3	12492	287	-11447	4.45	3.84	-6.32	132.00	192.00	192.00	12
600	(8+9)-VIII-1	6308	-1128	-5412	2.25	-15.08	-2.99	132.00	192.00	192.00	9.0
600	(8+9)-VIII-2	-14801	476	15479	-5.27	6.36	8.54	132.00	192.00	192.00	13
600	(8+9)-VIII-3	11914	-403	-11084	4.24	-5.39	-6.12	132.00	192.00	192.00	11

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
600	(8+9)-I-3	8530	1299	-7897	3.04	17.37	-4.36	132.00	192.00	192.00	7.3
Verifiche nella direzione secondaria											
0	(8+9)-VIII-4	-3975	-11	947	-13.69	-2.24	32.60	132.00	192.00	192.00	5.4
0	(8+9)-VII-2	-6791	-58	1566	-23.38	-11.42	53.93	132.00	192.00	192.00	2.8
0	(8+9)-III-3	4549	40	-1180	15.66	7.90	-40.63	132.00	192.00	192.00	2.7
0	(8+9)-IV-2	-6547	-37	1538	-22.55	-7.30	52.96	132.00	192.00	192.00	3.1
0	(8+9)-III-4	1782	28	-405	6.14	5.47	-13.94	132.00	192.00	192.00	6.8
0	(8+9)-VIII-2	-6765	-39	1650	-23.29	-7.78	56.81	132.00	192.00	192.00	2.8
0	(8+9)-IV-1	2676	4	-1045	9.22	0.79	-36.00	132.00	192.00	192.00	3.8
0	(8+9)-VII-4	2507	36	-778	8.63	7.06	-26.79	132.00	192.00	192.00	4.1
0	(8+9)-I-1	-3644	-40	207	-12.55	-7.93	7.12	132.00	192.00	192.00	12
0	(8+9)-IV-3	5031	27	-1525	17.32	5.38	-52.51	132.00	192.00	192.00	2.3
0	(8+9)-I-3	4203	37	-1391	14.47	7.36	-47.90	132.00	192.00	192.00	2.5
0	(8+9)-IV-4	-4193	-14	1059	-14.44	-2.72	36.45	132.00	192.00	192.00	4.8
0	(8+9)-II-1	1524	-5	-1749	5.25	-1.01	-60.23	132.00	192.00	192.00	2.8
0	(8+9)-V-1	-4369	-48	580	-15.05	-9.53	19.97	132.00	192.00	192.00	6.3
0	(8+9)-II-3	3879	18	-2229	13.36	3.58	-76.74	132.00	192.00	192.00	1.9
0	(8+9)-V-2	-6445	-55	1777	-22.19	-10.88	61.20	132.00	192.00	192.00	2.6
0	(8+9)-III-1	-3298	-38	418	-11.36	-7.39	14.39	132.00	192.00	192.00	8.5
0	(8+9)-V-3	4929	45	-1764	16.97	8.95	-60.75	132.00	192.00	192.00	2.0
0	(8+9)-VIII-3	5248	30	-1637	18.07	5.86	-56.36	132.00	192.00	192.00	2.2
0	(8+9)-V-4	2853	39	-567	9.82	7.60	-19.52	132.00	192.00	192.00	4.6
0	(8+9)-VII-3	5274	48	-1553	18.16	9.49	-53.48	132.00	192.00	192.00	2.1
0	(8+9)-VI-1	1307	-8	-1637	4.50	-1.49	-56.38	132.00	192.00	192.00	3.0
0	(8+9)-I-4	2128	31	-194	7.33	6.01	-6.67	132.00	192.00	192.00	8.2
0	(8+9)-VI-2	-5613	-30	2354	-19.33	-5.98	81.05	132.00	192.00	192.00	2.2
0	(8+9)-II-4	-3041	-5	1762	-10.47	-0.92	60.68	132.00	192.00	192.00	3.1
0	(8+9)-VIII-1	2459	2	-933	8.47	0.31	-32.14	132.00	192.00	192.00	4.3
0	(8+9)-I-2	-5720	-47	1404	-19.70	-9.28	48.35	132.00	192.00	192.00	3.2
0	(8+9)-II-2	-5395	-28	2242	-18.58	-5.50	77.19	132.00	192.00	192.00	2.3
0	(8+9)-III-2	-6065	-50	1193	-20.89	-9.82	41.08	132.00	192.00	192.00	3.6
0	(8+9)-VI-3	4096	21	-2340	14.11	4.06	-80.59	132.00	192.00	192.00	1.8
0	(8+9)-VI-4	-2823	-2	1650	-9.72	-0.44	56.83	132.00	192.00	192.00	3.3
0	(8+9)-VII-1	-4024	-46	791	-13.86	-8.99	27.24	132.00	192.00	192.00	5.2
1935	1	-918	4	-75	-3.16	0.77	-2.59	79.20	115.20	115.20	33
1935	2	-1504	9	-188	-5.18	1.69	-6.47	118.80	172.80	172.80	21
1935	3	-1504	9	-188	-5.18	1.69	-6.47	118.80	172.80	172.80	21
1935	4	-918	4	-75	-3.16	0.77	-2.59	105.60	153.60	153.60	45
1935	5	-918	4	-75	-3.16	0.77	-2.59	105.60	153.60	153.60	45
1935	6	-918	4	-75	-3.16	0.77	-2.59	105.60	153.60	153.60	45
1935	7	-918	4	-75	-3.16	0.77	-2.59	105.60	153.60	153.60	45

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
0	1	36	0.01	3.84	Si	>100
0	2	77	0.02	5.76	Si	>100
0	3	77	0.02	5.76	Si	>100
0	4	36	0.01	5.12	Si	>100
0	5	36	0.01	5.12	Si	>100
0	6	36	0.01	5.12	Si	>100
0	7	36	0.01	5.12	Si	>100
0	(8+9)-VIII-4	583	0.16	6.40	Si	41
0	(8+9)-IV-1	-445	0.12	6.40	Si	54
0	(8+9)-V-1	-734	0.20	6.40	Si	33
0	(8+9)-V-2	-614	0.16	6.40	Si	39
0	(8+9)-I-4	487	0.13	6.40	Si	49
0	(8+9)-V-3	663	0.18	6.40	Si	36
0	(8+9)-II-2	105	0.03	6.40	Si	>100
0	(8+9)-V-4	783	0.21	6.40	Si	31
0	(8+9)-II-4	346	0.09	6.40	Si	69
0	(8+9)-VII-2	-569	0.15	6.40	Si	42
0	(8+9)-II-1	-297	0.08	6.40	Si	81

X	Comb.	Ty	τ_d	fvd	RS	Cs
0	(8+9)-VI-1	-386	0.10	6.40	Si	62
0	(8+9)-II-3	-56	0.01	6.40	Si	>100
0	(8+9)-III-4	531	0.14	6.40	Si	45
0	(8+9)-VII-4	828	0.22	6.40	Si	29
0	(8+9)-IV-2	253	0.07	6.40	Si	95
0	(8+9)-IV-4	494	0.13	6.40	Si	49
0	(8+9)-VII-3	618	0.17	6.40	Si	39
0	(8+9)-VII-1	-779	0.21	6.40	Si	31
0	(8+9)-VI-4	435	0.12	6.40	Si	55
0	(8+9)-VIII-1	-534	0.14	6.40	Si	45
0	(8+9)-VI-3	33	0.01	6.40	Si	>100
300	(8+9)-VIII-3	-227	0.06	6.40	Si	>100
300	(8+9)-IV-3	-231	0.06	6.40	Si	>100
300	(8+9)-VIII-2	204	0.05	6.40	Si	>100
600	(8+9)-I-2	-450	0.12	6.40	Si	55
600	(8+9)-VI-2	-26	0.01	6.40	Si	>100
600	(8+9)-III-1	-536	0.14	6.40	Si	46
600	(8+9)-I-3	427	0.11	6.40	Si	58
600	(8+9)-I-1	-515	0.13	6.40	Si	48
600	(8+9)-III-3	406	0.11	6.40	Si	61
600	(8+9)-III-2	-430	0.11	6.40	Si	58
Verifiche nella direzione secondaria						
0	1	12	0.04	3.84	Si	>100
0	2	27	0.09	5.76	Si	66
0	3	27	0.09	5.76	Si	66
0	4	12	0.04	5.12	Si	>100
0	5	12	0.04	5.12	Si	>100
0	6	12	0.04	5.12	Si	>100
0	7	12	0.04	5.12	Si	>100
0	(8+9)-IV-2	59	0.19	6.40	Si	34
0	(8+9)-V-1	53	0.17	6.40	Si	38
0	(8+9)-I-2	56	0.18	6.40	Si	36
0	(8+9)-V-2	63	0.20	6.40	Si	32
0	(8+9)-I-4	-29	0.09	6.40	Si	70
0	(8+9)-VII-1	47	0.15	6.40	Si	43
0	(8+9)-IV-3	-43	0.14	6.40	Si	47
0	(8+9)-V-3	-47	0.15	6.40	Si	43
0	(8+9)-IV-4	34	0.11	6.40	Si	60
0	(8+9)-VIII-2	61	0.19	6.40	Si	33
0	(8+9)-I-3	-40	0.13	6.40	Si	51
0	(8+9)-III-2	62	0.20	6.40	Si	33
0	(8+9)-VII-3	-53	0.17	6.40	Si	38
0	(8+9)-III-4	-23	0.07	6.40	Si	88
0	(8+9)-I-1	45	0.14	6.40	Si	45
0	(8+9)-III-1	39	0.12	6.40	Si	52
0	(8+9)-III-3	-46	0.15	6.40	Si	44
0	(8+9)-VII-4	-31	0.10	6.40	Si	66
0	(8+9)-VIII-3	-45	0.14	6.40	Si	45
0	(8+9)-V-4	-37	0.12	6.40	Si	55
0	(8+9)-VII-2	70	0.22	6.40	Si	29
0	(8+9)-VI-2	41	0.13	6.40	Si	49
1935	(8+9)-VIII-4	32	0.10	6.40	Si	63
1935	(8+9)-II-2	39	0.12	6.40	Si	51
1935	(8+9)-IV-1	-21	0.07	6.40	Si	94
1935	(8+9)-VI-1	-18	0.06	6.40	Si	>100
1935	(8+9)-II-1	-17	0.05	6.40	Si	>100
1935	(8+9)-VI-3	-29	0.09	6.40	Si	70
1935	(8+9)-VIII-1	-22	0.07	6.40	Si	90
1935	(8+9)-II-4	26	0.08	6.40	Si	76
1935	(8+9)-II-3	-30	0.09	6.40	Si	68
1935	(8+9)-VI-4	28	0.09	6.40	Si	73

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	(8+9)-VII-4	6217	3.42	32.00	9.3	0.83	20.00	24	V	9.3
0	(8+9)-I-4	1723	0.95	32.00	34	0.23	20.00	87	V	34
0	(8+9)-III-4	2582	1.42	32.00	23	0.34	20.00	58	V	23
0	(8+9)-V-4	5358	2.95	32.00	11	0.71	20.00	28	V	11
300	1	-1618	-0.88	19.20	22	-0.21	12.00	57	V	22
300	2	-3527	-1.91	28.80	15	-0.46	18.00	39	V	15
300	3	-3527	-1.91	28.80	15	-0.46	18.00	39	V	15
300	4	-1618	-0.88	25.60	29	-0.21	16.00	75	V	29
300	5	-1618	-0.88	25.60	29	-0.21	16.00	75	V	29
300	6	-1618	-0.88	25.60	29	-0.21	16.00	75	V	29
300	7	-1618	-0.88	25.60	29	-0.21	16.00	75	V	29
300	(8+9)-V-3	12803	6.94	32.00	4.6	1.68	20.00	12	V	4.6
300	(8+9)-VII-3	11884	6.44	32.00	5.0	1.56	20.00	13	V	5.0
300	(8+9)-VIII-2	-13996	-7.59	32.00	4.2	-1.84	20.00	11	V	4.2
300	(8+9)-VII-1	-8250	-4.47	32.00	7.2	-1.08	20.00	18	V	7.2
300	(8+9)-VII-2	-14154	-7.67	32.00	4.2	-1.86	20.00	11	V	4.2
300	(8+9)-VI-2	-17059	-9.25	32.00	3.5	-2.24	20.00	8.9	V	3.5
300	(8+9)-III-2	-10154	-5.50	32.00	5.8	-1.33	20.00	15	V	5.8
300	(8+9)-I-2	-11073	-6.00	32.00	5.3	-1.45	20.00	14	V	5.3
300	(8+9)-I-3	8802	4.77	32.00	6.7	1.15	20.00	17	V	6.7
300	(8+9)-III-1	-4249	-2.30	32.00	14	-0.56	20.00	36	V	14
300	(8+9)-III-3	7883	4.27	32.00	7.5	1.03	20.00	19	V	7.5
300	(8+9)-I-1	-3331	-1.81	32.00	18	-0.44	20.00	46	V	18
300	(8+9)-V-1	-7331	-3.97	32.00	8.1	-0.96	20.00	21	V	8.1
300	(8+9)-V-2	-15073	-8.17	32.00	3.9	-1.98	20.00	10	V	3.9
600	(8+9)-VIII-4	-10226	-5.46	32.00	5.9	-1.32	20.00	15	V	5.9
600	(8+9)-IV-1	8569	4.57	32.00	7.0	1.11	20.00	18	V	7.0
600	(8+9)-II-4	-13846	-7.39	32.00	4.3	-1.79	20.00	11	V	4.3
600	(8+9)-IV-4	-10672	-5.70	32.00	5.6	-1.38	20.00	15	V	5.6
600	(8+9)-II-3	14765	7.88	32.00	4.1	1.91	20.00	10	V	4.1
600	(8+9)-IV-3	11592	6.19	32.00	5.2	1.50	20.00	13	V	5.2
600	(8+9)-II-2	-16868	-9.01	32.00	3.6	-2.18	20.00	9.2	V	3.6
600	(8+9)-VI-1	11296	6.03	32.00	5.3	1.46	20.00	14	V	5.3
600	(8+9)-VI-3	15211	8.12	32.00	3.9	1.97	20.00	10	V	3.9
600	(8+9)-IV-2	-13695	-7.31	32.00	4.4	-1.77	20.00	11	V	4.4
600	(8+9)-VIII-1	8123	4.34	32.00	7.4	1.05	20.00	19	V	7.4
600	(8+9)-II-1	11742	6.27	32.00	5.1	1.52	20.00	13	V	5.1
600	(8+9)-VIII-3	12038	6.43	32.00	5.0	1.56	20.00	13	V	5.0
600	(8+9)-VI-4	-13399	-7.15	32.00	4.5	-1.73	20.00	12	V	4.5
Verifiche nella direzione secondaria										
1935	1	84	0.29	19.20	67	0.07	12.00	>100	V	67
1935	2	175	0.60	28.80	48	0.15	18.00	>100	V	48
1935	3	175	0.60	28.80	48	0.15	18.00	>100	V	48
1935	4	84	0.29	25.60	89	0.07	16.00	>100	V	89
1935	5	84	0.29	25.60	89	0.07	16.00	>100	V	89
1935	6	84	0.29	25.60	89	0.07	16.00	>100	V	89
1935	7	84	0.29	25.60	89	0.07	16.00	>100	V	89
1935	(8+9)-VIII-4	2362	8.13	32.00	3.9	1.97	20.00	10	V	3.9
1935	(8+9)-IV-2	3895	13.41	32.00	2.4	3.25	20.00	6.2	V	2.4
1935	(8+9)-V-1	1911	6.58	32.00	4.9	1.59	20.00	13	V	4.9
1935	(8+9)-I-2	3323	11.44	32.00	2.8	2.77	20.00	7.2	V	2.8
1935	(8+9)-V-2	4177	14.38	32.00	2.2	3.48	20.00	5.7	V	2.2
1935	(8+9)-I-4	-933	-3.21	32.00	10.0	-0.78	20.00	26	V	10.0
1935	(8+9)-V-3	-4052	-13.95	32.00	2.3	-3.38	20.00	5.9	V	2.3
1935	(8+9)-II-2	4476	15.41	32.00	2.1	3.73	20.00	5.4	V	2.1
1935	(8+9)-V-4	-1787	-6.15	32.00	5.2	-1.49	20.00	13	V	5.2
1935	(8+9)-II-4	3199	11.02	32.00	2.9	2.67	20.00	7.5	V	2.9
1935	(8+9)-VI-1	-2819	-9.71	32.00	3.3	-2.35	20.00	8.5	V	3.3
1935	(8+9)-III-2	3149	10.84	32.00	3.0	2.62	20.00	7.6	V	3.0
1935	(8+9)-VI-2	4732	16.30	32.00	2.0	3.94	20.00	5.1	V	2.0
1935	(8+9)-III-4	-1108	-3.81	32.00	8.4	-0.92	20.00	22	V	8.4
1935	(8+9)-VI-3	-4608	-15.87	32.00	2.0	-3.84	20.00	5.2	V	2.0
1935	(8+9)-I-1	1058	3.64	32.00	8.8	0.88	20.00	23	V	8.8

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
1935	(8+9)-VI-4	2943	10.14	32.00	3.2	2.45	20.00	8.2	V	3.2
1935	(8+9)-IV-4	2618	9.01	32.00	3.5	2.18	20.00	9.2	V	3.5
1935	(8+9)-VII-1	2086	7.18	32.00	4.5	1.74	20.00	12	V	4.5
1935	(8+9)-II-1	-3075	-10.59	32.00	3.0	-2.56	20.00	7.8	V	3.0
1935	(8+9)-VII-2	4002	13.78	32.00	2.3	3.34	20.00	6.0	V	2.3
1935	(8+9)-III-1	1232	4.24	32.00	7.5	1.03	20.00	19	V	7.5
1935	(8+9)-VII-3	-3877	-13.35	32.00	2.4	-3.23	20.00	6.2	V	2.4
1935	(8+9)-IV-1	-2493	-8.59	32.00	3.7	-2.08	20.00	9.6	V	3.7
1935	(8+9)-VII-4	-1961	-6.75	32.00	4.7	-1.63	20.00	12	V	4.7
1935	(8+9)-III-3	-3024	-10.41	32.00	3.1	-2.52	20.00	7.9	V	3.1
1935	(8+9)-IV-3	-3770	-12.98	32.00	2.5	-3.14	20.00	6.4	V	2.5
1935	(8+9)-II-3	-4352	-14.98	32.00	2.1	-3.63	20.00	5.5	V	2.1
1935	(8+9)-VIII-1	-2237	-7.70	32.00	4.2	-1.86	20.00	11	V	4.2
1935	(8+9)-VIII-2	4151	14.29	32.00	2.2	3.46	20.00	5.8	V	2.2
1935	(8+9)-VIII-3	-4026	-13.86	32.00	2.3	-3.36	20.00	6.0	V	2.3
1935	(8+9)-I-3	-3198	-11.01	32.00	2.9	-2.67	20.00	7.5	V	2.9

Setto 7: origine (1697.4,897.9,165.0), direzione (-0.201275,0.979535,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	(8+9)-II-3	5162	-393	-7533	2.16	-6.16	-5.72	132.00	192.00	192.00	13
0	(8+9)-VI-3	5531	-365	-8047	2.31	-5.72	-6.11	132.00	192.00	192.00	13
0	(8+9)-VI-2	-5397	365	7818	-2.25	5.72	5.93	132.00	192.00	192.00	16
0	(8+9)-II-2	-5028	393	7304	-2.10	6.16	5.54	132.00	192.00	192.00	16
400	(8+9)-VII-2	-6438	560	9256	-2.62	8.58	6.70	132.00	192.00	192.00	13
400	(8+9)-III-2	-4827	659	6986	-1.97	10.09	5.06	132.00	192.00	192.00	13
400	(8+9)-IV-3	6451	251	-9532	2.63	3.84	-6.90	132.00	192.00	192.00	13
400	(8+9)-IV-1	4481	732	-6629	1.83	11.22	-4.80	132.00	192.00	192.00	10
400	(8+9)-VII-3	6584	-554	-9680	2.68	-8.49	-7.01	132.00	192.00	192.00	9.9
400	(8+9)-IV-2	-6304	-245	9108	-2.57	-3.75	6.60	132.00	192.00	192.00	18
400	(8+9)-I-2	-5055	737	7326	-2.06	11.28	5.31	132.00	192.00	192.00	12
400	(8+9)-I-4	1510	-869	-2349	0.62	-13.31	-1.70	132.00	192.00	192.00	12
400	(8+9)-IV-4	-4335	-727	6205	-1.77	-11.13	4.49	132.00	192.00	192.00	12
400	(8+9)-VII-4	3349	-847	-4959	1.37	-12.98	-3.59	132.00	192.00	192.00	10
400	(8+9)-V-1	-2974	776	4195	-1.21	11.88	3.04	132.00	192.00	192.00	13
400	(8+9)-II-4	-5094	-468	7339	-2.08	-7.17	5.31	132.00	192.00	192.00	15
400	(8+9)-V-2	-6665	637	9596	-2.72	9.76	6.95	132.00	192.00	192.00	11
400	(8+9)-VIII-2	-6787	-275	9789	-2.77	-4.21	7.09	132.00	192.00	192.00	17
400	(8+9)-V-3	6812	-632	-10020	2.78	-9.68	-7.26	132.00	192.00	192.00	9.2
400	(8+9)-III-4	1738	-946	-2689	0.71	-14.50	-1.95	132.00	192.00	192.00	11
400	(8+9)-V-4	3121	-770	-4618	1.27	-11.79	-3.34	132.00	192.00	192.00	11
400	(8+9)-I-3	5201	-731	-7750	2.12	-11.19	-5.61	132.00	192.00	192.00	9.7
400	(8+9)-VI-1	4757	444	-7082	1.94	6.80	-5.13	132.00	192.00	192.00	13
400	(8+9)-VIII-1	3998	703	-5948	1.63	10.76	-4.31	132.00	192.00	192.00	11
400	(8+9)-VIII-3	6934	281	-10213	2.83	4.30	-7.40	132.00	192.00	192.00	12
400	(8+9)-III-3	4974	-653	-7410	2.03	-10.01	-5.37	132.00	192.00	192.00	10
400	(8+9)-II-1	5240	474	-7763	2.14	7.26	-5.62	132.00	192.00	192.00	12
400	(8+9)-III-1	-1591	952	2265	-0.65	14.59	1.64	132.00	192.00	192.00	12
400	(8+9)-I-1	-1364	875	1925	-0.56	13.40	1.39	132.00	192.00	192.00	13
400	(8+9)-VIII-4	-3851	-697	5524	-1.57	-10.68	4.00	132.00	192.00	192.00	13
400	(8+9)-VI-4	-4610	-438	6658	-1.88	-6.72	4.82	132.00	192.00	192.00	17
400	(8+9)-VII-1	-3202	853	4535	-1.31	13.07	3.28	132.00	192.00	192.00	12
800	1	169	7	-402	0.07	0.11	-0.28	79.20	115.20	115.20	>100
800	2	252	15	-713	0.10	0.23	-0.49	118.80	172.80	172.80	>100
800	3	252	15	-713	0.10	0.23	-0.49	118.80	172.80	172.80	>100
800	4	169	7	-402	0.07	0.11	-0.28	105.60	153.60	153.60	>100
800	5	169	7	-402	0.07	0.11	-0.28	105.60	153.60	153.60	>100
800	6	169	7	-402	0.07	0.11	-0.28	105.60	153.60	153.60	>100
800	7	169	7	-402	0.07	0.11	-0.28	105.60	153.60	153.60	>100
Verifiche nella direzione secondaria											
0	2	-3258	-12	12	-8.42	-1.73	0.24	118.80	172.80	172.80	73
0	3	-3258	-12	12	-8.42	-1.73	0.24	118.80	172.80	172.80	73

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-VIII-4	-3315	1	1639	-8.56	0.14	31.74	132.00	192.00	192.00	6.0
0	(8+9)-VI-4	-3642	1	2055	-9.41	0.17	39.81	132.00	192.00	192.00	4.7
0	(8+9)-III-3	1254	6	-2196	3.24	0.95	-42.53	132.00	192.00	192.00	4.0
0	(8+9)-IV-3	1850	-0	-2725	4.78	-0.05	-52.78	132.00	192.00	192.00	3.2
0	(8+9)-VII-1	-3120	-19	1437	-8.06	-2.75	27.84	132.00	192.00	192.00	6.2
0	(8+9)-VIII-2	-4837	-8	2909	-12.49	-1.21	56.35	132.00	192.00	192.00	3.3
0	(8+9)-IV-1	748	-6	-1815	1.93	-0.92	-35.17	132.00	192.00	192.00	4.9
0	(8+9)-VII-4	343	12	-1434	0.89	1.73	-27.77	132.00	192.00	192.00	6.2
0	(8+9)-IV-2	-4627	-7	2729	-11.95	-0.97	52.86	132.00	192.00	192.00	3.5
0	(8+9)-I-3	1352	6	-2321	3.49	0.94	-44.95	132.00	192.00	192.00	3.8
0	(8+9)-II-1	1075	-6	-2232	2.78	-0.95	-43.23	132.00	192.00	192.00	4.0
0	(8+9)-IV-4	-3525	-1	1819	-9.10	-0.10	35.24	132.00	192.00	192.00	5.4
0	(8+9)-II-3	2177	-1	-3141	5.62	-0.08	-60.85	132.00	192.00	192.00	2.8
0	(8+9)-V-1	-3022	-19	1312	-7.80	-2.76	25.42	132.00	192.00	192.00	6.7
0	(8+9)-VII-2	-4733	-19	2801	-12.22	-2.77	54.25	132.00	192.00	192.00	3.3
0	(8+9)-V-2	-4831	-19	2925	-12.48	-2.76	56.67	132.00	192.00	192.00	3.2
0	(8+9)-VIII-3	2060	1	-2905	5.32	0.19	-56.28	132.00	192.00	192.00	3.0
0	(8+9)-V-3	2054	12	-2922	5.30	1.74	-56.59	132.00	192.00	192.00	2.9
0	(8+9)-I-2	-4129	-13	2324	-10.66	-1.96	45.02	132.00	192.00	192.00	4.0
0	(8+9)-V-4	245	12	-1309	0.63	1.74	-25.35	132.00	192.00	192.00	6.9
0	(8+9)-II-2	-4954	-6	3145	-12.79	-0.94	60.92	132.00	192.00	192.00	3.1
0	(8+9)-III-2	-4031	-13	2200	-10.41	-1.97	42.60	132.00	192.00	192.00	4.3
0	(8+9)-VIII-1	538	-8	-1635	1.39	-1.16	-31.67	132.00	192.00	192.00	5.5
0	(8+9)-VII-3	1956	12	-2797	5.05	1.75	-54.18	132.00	192.00	192.00	3.0
0	(8+9)-II-4	-3852	-0	2235	-9.95	-0.07	43.30	132.00	192.00	192.00	4.4
0	(8+9)-VI-1	865	-8	-2051	2.23	-1.19	-39.74	132.00	192.00	192.00	4.3
0	(8+9)-VI-2	-5164	-8	3325	-13.34	-1.18	64.41	132.00	192.00	192.00	2.9
0	(8+9)-VI-3	2388	1	-3322	6.17	0.16	-64.34	132.00	192.00	192.00	2.6
1728	1	-1951	1	-38	-5.04	0.17	-0.73	79.20	115.20	115.20	>100
1728	4	-1951	1	-38	-5.04	0.17	-0.73	105.60	153.60	153.60	>100
1728	5	-1951	1	-38	-5.04	0.17	-0.73	105.60	153.60	153.60	>100
1728	6	-1951	1	-38	-5.04	0.17	-0.73	105.60	153.60	153.60	>100
1728	7	-1951	1	-38	-5.04	0.17	-0.73	105.60	153.60	153.60	>100
1728	(8+9)-III-4	-1790	161	-18	-4.62	23.80	-0.34	132.00	192.00	192.00	7.9
1728	(8+9)-III-1	-892	-159	-34	-2.30	-23.56	-0.65	132.00	192.00	192.00	7.9
1728	(8+9)-I-4	-1686	132	-12	-4.35	19.46	-0.23	132.00	192.00	192.00	9.7
1728	(8+9)-I-1	-996	-130	-40	-2.57	-19.22	-0.77	132.00	192.00	192.00	9.6

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Ty kg	τ_d kg/cmq	fvd kg/cmq	RS	Cs
0	(8+9)-IV-2	91	0.03	6.40	Si	>100
0	(8+9)-VIII-3	-99	0.03	6.40	Si	>100
0	(8+9)-VIII-2	111	0.03	6.40	Si	>100
0	(8+9)-II-3	85	0.03	6.40	Si	>100
0	(8+9)-II-2	-73	0.02	6.40	Si	>100
0	(8+9)-IV-3	-79	0.02	6.40	Si	>100
0	(8+9)-VI-2	-53	0.02	6.40	Si	>100
0	(8+9)-VI-3	65	0.02	6.40	Si	>100
800	1	15	0.00	3.84	Si	>100
800	2	32	0.01	5.76	Si	>100
800	3	32	0.01	5.76	Si	>100
800	4	15	0.00	5.12	Si	>100
800	5	15	0.00	5.12	Si	>100
800	6	15	0.00	5.12	Si	>100
800	7	15	0.00	5.12	Si	>100
800	(8+9)-VIII-4	156	0.05	6.40	Si	>100
800	(8+9)-IV-1	-136	0.04	6.40	Si	>100
800	(8+9)-VI-1	-128	0.04	6.40	Si	>100
800	(8+9)-III-2	-227	0.07	6.40	Si	97
800	(8+9)-I-4	287	0.08	6.40	Si	77
800	(8+9)-III-4	289	0.08	6.40	Si	76
800	(8+9)-I-3	250	0.07	6.40	Si	88

X	Comb.	Ty	τ_d	fvd	RS	Cs
800	(8+9)-II-4	150	0.04	6.40	Si	>100
800	(8+9)-VI-4	148	0.04	6.40	Si	>100
800	(8+9)-IV-4	157	0.05	6.40	Si	>100
800	(8+9)-VII-1	-265	0.08	6.40	Si	83
800	(8+9)-V-2	-226	0.07	6.40	Si	98
800	(8+9)-VII-2	-224	0.06	6.40	Si	99
800	(8+9)-V-4	284	0.08	6.40	Si	78
800	(8+9)-VII-3	244	0.07	6.40	Si	90
800	(8+9)-III-1	-269	0.08	6.40	Si	82
800	(8+9)-VII-4	286	0.08	6.40	Si	77
800	(8+9)-III-3	248	0.07	6.40	Si	89
800	(8+9)-II-1	-129	0.04	6.40	Si	>100
800	(8+9)-V-3	247	0.07	6.40	Si	90
800	(8+9)-VIII-1	-135	0.04	6.40	Si	>100
800	(8+9)-I-2	-229	0.07	6.40	Si	96
800	(8+9)-I-1	-266	0.08	6.40	Si	83
800	(8+9)-V-1	-263	0.08	6.40	Si	84
Verifiche nella direzione secondaria						
0	1	4	0.01	3.84	Si	>100
0	2	10	0.02	5.76	Si	>100
0	3	10	0.02	5.76	Si	>100
0	4	4	0.01	5.12	Si	>100
0	5	4	0.01	5.12	Si	>100
0	6	4	0.01	5.12	Si	>100
0	7	4	0.01	5.12	Si	>100
0	(8+9)-VIII-4	25	0.06	6.40	Si	>100
0	(8+9)-VI-1	-25	0.06	6.40	Si	>100
0	(8+9)-III-4	21	0.05	6.40	Si	>100
0	(8+9)-V-1	-56	0.13	6.40	Si	48
0	(8+9)-IV-1	-7	0.02	6.40	Si	>100
0	(8+9)-I-4	23	0.06	6.40	Si	>100
0	(8+9)-VI-4	31	0.07	6.40	Si	87
0	(8+9)-VIII-2	-9	0.02	6.40	Si	>100
0	(8+9)-VI-3	8	0.02	6.40	Si	>100
0	(8+9)-II-4	19	0.05	6.40	Si	>100
0	(8+9)-IV-4	13	0.03	6.40	Si	>100
0	(8+9)-VII-2	-51	0.12	6.40	Si	53
0	(8+9)-VIII-3	15	0.03	6.40	Si	>100
0	(8+9)-VII-4	60	0.14	6.40	Si	45
0	(8+9)-VII-3	57	0.14	6.40	Si	47
0	(8+9)-VII-1	-54	0.13	6.40	Si	50
0	(8+9)-II-1	-13	0.03	6.40	Si	>100
0	(8+9)-V-2	-49	0.12	6.40	Si	55
0	(8+9)-V-3	55	0.13	6.40	Si	49
0	(8+9)-V-4	62	0.15	6.40	Si	44
1728	(8+9)-IV-2	21	0.05	6.40	Si	>100
1728	(8+9)-I-2	25	0.06	6.40	Si	>100
1728	(8+9)-III-1	18	0.04	6.40	Si	>100
1728	(8+9)-VI-2	7	0.02	6.40	Si	>100
1728	(8+9)-II-3	-16	0.04	6.40	Si	>100
1728	(8+9)-III-2	26	0.06	6.40	Si	>100
1728	(8+9)-IV-3	-17	0.04	6.40	Si	>100
1728	(8+9)-III-3	-22	0.05	6.40	Si	>100
1728	(8+9)-VIII-1	-19	0.05	6.40	Si	>100
1728	(8+9)-II-2	20	0.05	6.40	Si	>100
1728	(8+9)-I-3	-21	0.05	6.40	Si	>100
1728	(8+9)-I-1	18	0.04	6.40	Si	>100

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
400	1	-353	-0.22	19.20	89	-0.05	12.00	>100	V	89
400	4	-353	-0.22	25.60	>100	-0.05	16.00	>100	V	>100

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
400	5	-353	-0.22	25.60	>100	-0.05	16.00	>100	V	>100
400	6	-353	-0.22	25.60	>100	-0.05	16.00	>100	V	>100
400	7	-353	-0.22	25.60	>100	-0.05	16.00	>100	V	>100
400	(8+9)-VIII-4	-6024	-3.68	32.00	8.7	-0.89	20.00	22	V	8.7
400	(8+9)-IV-1	6034	3.69	32.00	8.7	0.89	20.00	22	V	8.7
400	(8+9)-IV-4	-6540	-4.00	32.00	8.0	-0.97	20.00	21	V	8.0
400	(8+9)-V-1	-4443	-2.72	32.00	12	-0.66	20.00	30	V	12
400	(8+9)-I-2	-8238	-5.04	32.00	6.4	-1.22	20.00	16	V	6.4
400	(8+9)-V-2	-9957	-6.09	32.00	5.3	-1.47	20.00	14	V	5.3
400	(8+9)-I-4	2217	1.36	32.00	24	0.33	20.00	61	V	24
400	(8+9)-V-3	9451	5.78	32.00	5.5	1.40	20.00	14	V	5.5
400	(8+9)-II-2	-11012	-6.74	32.00	4.8	-1.63	20.00	12	V	4.8
400	(8+9)-V-4	3937	2.41	32.00	13	0.58	20.00	34	V	13
400	(8+9)-II-4	-7876	-4.82	32.00	6.6	-1.17	20.00	17	V	6.6
400	(8+9)-VI-1	6854	4.19	32.00	7.6	1.01	20.00	20	V	7.6
400	(8+9)-III-2	-7837	-4.79	32.00	6.7	-1.16	20.00	17	V	6.7
400	(8+9)-VI-2	-11528	-7.05	32.00	4.5	-1.71	20.00	12	V	4.5
400	(8+9)-III-4	2617	1.60	32.00	20	0.39	20.00	52	V	20
400	(8+9)-VI-3	11022	6.74	32.00	4.7	1.63	20.00	12	V	4.7
400	(8+9)-IV-2	-9677	-5.92	32.00	5.4	-1.43	20.00	14	V	5.4
400	(8+9)-VI-4	-7360	-4.50	32.00	7.1	-1.09	20.00	18	V	7.1
400	(8+9)-I-1	-2723	-1.67	32.00	19	-0.40	20.00	50	V	19
400	(8+9)-VII-1	-4844	-2.96	32.00	11	-0.72	20.00	28	V	11
400	(8+9)-II-1	7369	4.51	32.00	7.1	1.09	20.00	18	V	7.1
400	(8+9)-VII-2	-9557	-5.85	32.00	5.5	-1.41	20.00	14	V	5.5
400	(8+9)-III-1	-3124	-1.91	32.00	17	-0.46	20.00	43	V	17
400	(8+9)-VIII-3	9686	5.92	32.00	5.4	1.43	20.00	14	V	5.4
400	(8+9)-VII-3	9050	5.54	32.00	5.8	1.34	20.00	15	V	5.8
400	(8+9)-I-3	7731	4.73	32.00	6.8	1.14	20.00	17	V	6.8
400	(8+9)-II-3	10506	6.43	32.00	5.0	1.56	20.00	13	V	5.0
400	(8+9)-III-3	7331	4.48	32.00	7.1	1.09	20.00	18	V	7.1
400	(8+9)-IV-3	9170	5.61	32.00	5.7	1.36	20.00	15	V	5.7
400	(8+9)-VII-4	4337	2.65	32.00	12	0.64	20.00	31	V	12
400	(8+9)-VIII-1	5518	3.38	32.00	9.5	0.82	20.00	24	V	9.5
400	(8+9)-VIII-2	-10193	-6.23	32.00	5.1	-1.51	20.00	13	V	5.1
800	2	-598	-0.36	28.80	81	-0.09	18.00	>100	V	81
800	3	-598	-0.36	28.80	81	-0.09	18.00	>100	V	81
Verifiche nella direzione secondaria										
0	1	79	0.20	19.20	94	0.05	12.00	>100	V	94
0	2	162	0.42	28.80	69	0.10	18.00	>100	V	69
0	3	162	0.42	28.80	69	0.10	18.00	>100	V	69
0	4	79	0.20	25.60	>100	0.05	16.00	>100	V	>100
0	5	79	0.20	25.60	>100	0.05	16.00	>100	V	>100
0	6	79	0.20	25.60	>100	0.05	16.00	>100	V	>100
0	7	79	0.20	25.60	>100	0.05	16.00	>100	V	>100
1728	(8+9)-VIII-4	2482	6.41	32.00	5.0	1.55	20.00	13	V	5.0
1728	(8+9)-IV-2	4124	10.65	32.00	3.0	2.58	20.00	7.8	V	3.0
1728	(8+9)-V-1	1949	5.03	32.00	6.4	1.22	20.00	16	V	6.4
1728	(8+9)-I-2	3518	9.09	32.00	3.5	2.20	20.00	9.1	V	3.5
1728	(8+9)-V-2	4384	11.32	32.00	2.8	2.74	20.00	7.3	V	2.8
1728	(8+9)-I-4	-1088	-2.81	32.00	11	-0.68	20.00	29	V	11
1728	(8+9)-V-3	-4389	-11.34	32.00	2.8	-2.74	20.00	7.3	V	2.8
1728	(8+9)-II-2	4747	12.26	32.00	2.6	2.97	20.00	6.7	V	2.6
1728	(8+9)-V-4	-1954	-5.05	32.00	6.3	-1.22	20.00	16	V	6.3
1728	(8+9)-II-4	3365	8.69	32.00	3.7	2.10	20.00	9.5	V	3.7
1728	(8+9)-VI-1	-3111	-8.03	32.00	4.0	-1.94	20.00	10	V	4.0
1728	(8+9)-III-2	3331	8.60	32.00	3.7	2.08	20.00	9.6	V	3.7
1728	(8+9)-VI-2	5006	12.93	32.00	2.5	3.13	20.00	6.4	V	2.5
1728	(8+9)-III-4	-1275	-3.29	32.00	9.7	-0.80	20.00	25	V	9.7
1728	(8+9)-VI-3	-5012	-12.94	32.00	2.5	-3.13	20.00	6.4	V	2.5
1728	(8+9)-I-1	1083	2.80	32.00	11	0.68	20.00	30	V	11
1728	(8+9)-VI-4	3105	8.02	32.00	4.0	1.94	20.00	10	V	4.0
1728	(8+9)-IV-4	2742	7.08	32.00	4.5	1.71	20.00	12	V	4.5
1728	(8+9)-VII-1	2135	5.52	32.00	5.8	1.33	20.00	15	V	5.8

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
1728	(8+9)-II-1	-3370	-8.70	32.00	3.7	-2.11	20.00	9.5	V	3.7
1728	(8+9)-VII-2	4197	10.84	32.00	3.0	2.62	20.00	7.6	V	3.0
1728	(8+9)-III-1	1270	3.28	32.00	9.8	0.79	20.00	25	V	9.8
1728	(8+9)-VII-3	-4202	-10.85	32.00	2.9	-2.63	20.00	7.6	V	2.9
1728	(8+9)-IV-1	-2748	-7.10	32.00	4.5	-1.72	20.00	12	V	4.5
1728	(8+9)-VII-4	-2141	-5.53	32.00	5.8	-1.34	20.00	15	V	5.8
1728	(8+9)-III-3	-3337	-8.62	32.00	3.7	-2.09	20.00	9.6	V	3.7
1728	(8+9)-IV-3	-4130	-10.67	32.00	3.0	-2.58	20.00	7.7	V	3.0
1728	(8+9)-II-3	-4752	-12.27	32.00	2.6	-2.97	20.00	6.7	V	2.6
1728	(8+9)-VIII-1	-2488	-6.43	32.00	5.0	-1.55	20.00	13	V	5.0
1728	(8+9)-VIII-2	4384	11.32	32.00	2.8	2.74	20.00	7.3	V	2.8
1728	(8+9)-VIII-3	-4389	-11.34	32.00	2.8	-2.74	20.00	7.3	V	2.8
1728	(8+9)-I-3	-3523	-9.10	32.00	3.5	-2.20	20.00	9.1	V	3.5

Setto 8: origine (1729.0,744.0,149.5), direzione (-0.201275,0.979535,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	1	44	-14	-264	0.02	-0.24	-0.24	79.20	115.20	115.20	>100
0	2	36	-28	-389	0.02	-0.48	-0.36	118.80	172.80	172.80	>100
0	3	36	-28	-389	0.02	-0.48	-0.36	118.80	172.80	172.80	>100
0	4	44	-14	-264	0.02	-0.24	-0.24	105.60	153.60	153.60	>100
0	5	44	-14	-264	0.02	-0.24	-0.24	105.60	153.60	153.60	>100
0	6	44	-14	-264	0.02	-0.24	-0.24	105.60	153.60	153.60	>100
0	7	44	-14	-264	0.02	-0.24	-0.24	105.60	153.60	153.60	>100
0	(8+9)-III-4	1400	567	-1412	0.64	9.81	-1.31	132.00	192.00	192.00	16
0	(8+9)-VIII-1	3066	-435	-2701	1.41	-7.53	-2.50	132.00	192.00	192.00	16
0	(8+9)-V-4	2361	437	-2165	1.09	7.55	-2.00	132.00	192.00	192.00	17
0	(8+9)-I-4	1183	491	-1230	0.54	8.50	-1.14	132.00	192.00	192.00	18
0	(8+9)-VII-1	-2497	-531	1961	-1.15	-9.19	1.81	132.00	192.00	192.00	17
0	(8+9)-VII-4	2577	512	-2348	1.19	8.86	-2.17	132.00	192.00	192.00	15
0	(8+9)-V-1	-2280	-456	1778	-1.05	-7.89	1.64	132.00	192.00	192.00	20
0	(8+9)-I-1	-1103	-510	843	-0.51	-8.83	0.78	132.00	192.00	192.00	20
0	(8+9)-III-1	-1320	-586	1025	-0.61	-10.14	0.95	132.00	192.00	192.00	17
186	(8+9)-VIII-4	-2981	380	3238	-1.36	6.50	2.92	132.00	192.00	192.00	20
186	(8+9)-IV-1	3410	-417	-3888	1.55	-7.12	-3.51	132.00	192.00	192.00	15
186	(8+9)-III-3	3933	350	-4520	1.79	5.98	-4.08	132.00	192.00	192.00	15
186	(8+9)-III-2	-3853	-368	4250	-1.75	-6.29	3.83	132.00	192.00	192.00	19
186	(8+9)-I-2	-4071	-443	4503	-1.85	-7.57	4.06	132.00	192.00	192.00	16
186	(8+9)-I-3	4151	425	-4773	1.89	7.27	-4.31	132.00	192.00	192.00	13
186	(8+9)-IV-4	-3330	399	3618	-1.52	6.82	3.26	132.00	192.00	192.00	19
372	(8+9)-VI-2	-5973	-79	8407	-2.69	-1.33	7.41	132.00	192.00	192.00	22
372	(8+9)-VI-3	6053	62	-8578	2.72	1.06	-7.56	132.00	192.00	192.00	15
372	(8+9)-II-4	-4067	123	5692	-1.83	2.08	5.01	132.00	192.00	192.00	27
372	(8+9)-VII-2	-4990	-268	7000	-2.24	-4.52	6.17	132.00	192.00	192.00	18
372	(8+9)-V-3	5287	305	-7482	2.38	5.15	-6.59	132.00	192.00	192.00	13
372	(8+9)-VII-3	5071	251	-7171	2.28	4.25	-6.32	132.00	192.00	192.00	14
372	(8+9)-VI-1	3783	-130	-5380	1.70	-2.20	-4.74	132.00	192.00	192.00	20
372	(8+9)-IV-3	4968	-106	-7058	2.23	-1.80	-6.22	132.00	192.00	192.00	17
372	(8+9)-II-1	4147	-139	-5863	1.86	-2.36	-5.16	132.00	192.00	192.00	19
372	(8+9)-II-2	-5610	-88	7925	-2.52	-1.49	6.98	132.00	192.00	192.00	23
372	(8+9)-V-2	-5207	-321	7311	-2.34	-5.43	6.44	132.00	192.00	192.00	16
372	(8+9)-VI-4	-3703	114	5210	-1.67	1.92	4.59	132.00	192.00	192.00	29
372	(8+9)-IV-2	-4888	90	6888	-2.20	1.52	6.07	132.00	192.00	192.00	25
372	(8+9)-VIII-2	-5251	99	7370	-2.36	1.68	6.49	132.00	192.00	192.00	23
372	(8+9)-VIII-3	5331	-116	-7541	2.40	-1.96	-6.64	132.00	192.00	192.00	16
372	(8+9)-II-3	5690	72	-8095	2.56	1.21	-7.13	132.00	192.00	192.00	16
Verifiche nella direzione secondaria											
0	(8+9)-VIII-4	3052	-2	341	16.95	-0.76	30.58	132.00	192.00	192.00	3.4
0	(8+9)-VII-2	4947	-11	581	27.47	-3.55	52.03	132.00	192.00	192.00	2.0
0	(8+9)-III-3	-4823	1	-431	-26.79	0.28	-38.63	132.00	192.00	192.00	4.5
0	(8+9)-IV-2	5163	-5	560	28.67	-1.61	50.16	132.00	192.00	192.00	2.1
0	(8+9)-III-4	-2088	-2	-148	-11.59	-0.71	-13.24	132.00	192.00	192.00	13

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-VIII-2	5399	-8	604	29.99	-2.58	54.15	132.00	192.00	192.00	1.9
0	(8+9)-IV-1	-3954	5	-385	-21.96	1.69	-34.50	132.00	192.00	192.00	5.0
0	(8+9)-VII-4	-2877	8	-296	-15.98	2.52	-26.55	132.00	192.00	192.00	6.3
0	(8+9)-I-1	1172	3	122	6.51	0.90	10.89	132.00	192.00	192.00	9.0
0	(8+9)-IV-3	-5828	5	-559	-32.37	1.57	-50.08	132.00	192.00	192.00	3.4
0	(8+9)-I-3	-5073	2	-458	-28.18	0.50	-41.06	132.00	192.00	192.00	4.2
0	(8+9)-IV-4	3289	-5	386	18.27	-1.73	34.57	132.00	192.00	192.00	3.1
0	(8+9)-II-1	-4789	8	-475	-26.60	2.44	-42.58	132.00	192.00	192.00	3.9
0	(8+9)-V-1	1961	-7	270	10.89	-2.33	24.21	132.00	192.00	192.00	4.5
0	(8+9)-II-3	-6663	7	-649	-37.01	2.32	-58.16	132.00	192.00	192.00	2.8
0	(8+9)-V-2	5197	-12	608	28.87	-3.77	54.45	132.00	192.00	192.00	1.9
0	(8+9)-III-1	1423	2	149	7.90	0.68	13.31	132.00	192.00	192.00	7.5
0	(8+9)-V-3	-5862	12	-607	-32.56	3.73	-54.37	132.00	192.00	192.00	3.0
0	(8+9)-VIII-3	-6064	8	-604	-33.68	2.54	-54.07	132.00	192.00	192.00	3.1
0	(8+9)-V-4	-2626	7	-269	-14.58	2.30	-24.13	132.00	192.00	192.00	7.0
0	(8+9)-VII-3	-5612	11	-580	-31.17	3.51	-51.95	132.00	192.00	192.00	3.2
0	(8+9)-VI-1	-4553	5	-431	-25.29	1.47	-38.58	132.00	192.00	192.00	4.4
0	(8+9)-I-4	-1837	-3	-121	-10.20	-0.94	-10.81	132.00	192.00	192.00	16
0	(8+9)-VI-2	6235	-10	695	34.63	-3.32	62.23	132.00	192.00	192.00	1.7
0	(8+9)-II-4	4125	-8	476	22.91	-2.47	42.65	132.00	192.00	192.00	2.4
0	(8+9)-VIII-1	-3717	2	-340	-20.65	0.72	-30.50	132.00	192.00	192.00	5.7
0	(8+9)-I-2	4408	-2	459	24.48	-0.54	41.13	132.00	192.00	192.00	2.5
0	(8+9)-II-2	5998	-7	650	33.31	-2.36	58.24	132.00	192.00	192.00	1.8
0	(8+9)-III-2	4158	-1	432	23.09	-0.31	38.71	132.00	192.00	192.00	2.6
0	(8+9)-VI-3	-6900	10	-694	-38.32	3.29	-62.16	132.00	192.00	192.00	2.6
0	(8+9)-VI-4	3888	-5	432	21.59	-1.50	38.66	132.00	192.00	192.00	2.7
0	(8+9)-VII-1	2212	-8	297	12.28	-2.56	26.63	132.00	192.00	192.00	4.1
1532	1	-597	0	-16	-3.32	0.03	-1.44	79.20	115.20	115.20	74
1532	2	-991	0	-27	-5.51	0.01	-2.42	118.80	172.80	172.80	66
1532	3	-991	0	-27	-5.51	0.01	-2.42	118.80	172.80	172.80	66
1532	4	-597	0	-16	-3.32	0.03	-1.44	105.60	153.60	153.60	100
1532	5	-597	0	-16	-3.32	0.03	-1.44	105.60	153.60	153.60	100
1532	6	-597	0	-16	-3.32	0.03	-1.44	105.60	153.60	153.60	100
1532	7	-597	0	-16	-3.32	0.03	-1.44	105.60	153.60	153.60	100

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
0	1	5	0.00	3.84	Si	>100
0	2	11	0.00	5.76	Si	>100
0	3	11	0.00	5.76	Si	>100
0	4	5	0.00	5.12	Si	>100
0	5	5	0.00	5.12	Si	>100
0	6	5	0.00	5.12	Si	>100
0	7	5	0.00	5.12	Si	>100
0	(8+9)-VIII-1	209	0.07	6.40	Si	91
0	(8+9)-IV-4	-176	0.06	6.40	Si	>100
0	(8+9)-VII-1	329	0.11	6.40	Si	58
0	(8+9)-V-3	-262	0.09	6.40	Si	73
0	(8+9)-VI-2	11	0.00	6.40	Si	>100
0	(8+9)-V-2	270	0.09	6.40	Si	71
0	(8+9)-IV-1	183	0.06	6.40	Si	>100
0	(8+9)-VII-4	-322	0.11	6.40	Si	59
0	(8+9)-VIII-4	-202	0.07	6.40	Si	95
186	(8+9)-VIII-3	38	0.01	6.40	Si	>100
186	(8+9)-II-2	-21	0.01	6.40	Si	>100
186	(8+9)-VIII-2	-30	0.01	6.40	Si	>100
186	(8+9)-II-3	29	0.01	6.40	Si	>100
186	(8+9)-IV-2	-60	0.02	6.40	Si	>100
186	(8+9)-IV-3	67	0.02	6.40	Si	>100
372	(8+9)-I-2	250	0.08	6.40	Si	78
372	(8+9)-VII-2	280	0.09	6.40	Si	70
372	(8+9)-V-1	334	0.11	6.40	Si	59

X	Comb.	Ty	τ_d	fvd	RS	Cs
372	(8+9)-VII-3	-273	0.09	6.40	Si	72
372	(8+9)-III-3	-249	0.08	6.40	Si	79
372	(8+9)-II-4	-178	0.06	6.40	Si	>100
372	(8+9)-VI-1	193	0.06	6.40	Si	>100
372	(8+9)-I-1	310	0.10	6.40	Si	63
372	(8+9)-VI-3	12	0.00	6.40	Si	>100
372	(8+9)-II-1	185	0.06	6.40	Si	>100
372	(8+9)-III-1	304	0.10	6.40	Si	64
372	(8+9)-I-4	-302	0.10	6.40	Si	65
372	(8+9)-V-4	-326	0.11	6.40	Si	60
372	(8+9)-VI-4	-185	0.06	6.40	Si	>100
372	(8+9)-III-4	-296	0.10	6.40	Si	66
372	(8+9)-III-2	256	0.08	6.40	Si	76
372	(8+9)-I-3	-243	0.08	6.40	Si	81
Verifiche nella direzione secondaria						
0	2	2	0.01	5.76	Si	>100
0	3	2	0.01	5.76	Si	>100
0	(8+9)-VII-1	26	0.14	6.40	Si	47
0	(8+9)-III-3	-25	0.13	6.40	Si	50
0	(8+9)-VIII-3	-21	0.11	6.40	Si	60
0	(8+9)-III-4	-18	0.09	6.40	Si	70
0	(8+9)-VII-4	-26	0.13	6.40	Si	48
0	(8+9)-IV-1	-6	0.03	6.40	Si	>100
0	(8+9)-I-1	17	0.09	6.40	Si	74
0	(8+9)-IV-2	19	0.10	6.40	Si	66
0	(8+9)-I-3	-27	0.14	6.40	Si	47
0	(8+9)-IV-3	-19	0.10	6.40	Si	67
0	(8+9)-II-1	-10	0.05	6.40	Si	>100
0	(8+9)-IV-4	6	0.03	6.40	Si	>100
0	(8+9)-II-3	-23	0.12	6.40	Si	53
0	(8+9)-V-1	25	0.13	6.40	Si	50
0	(8+9)-III-1	18	0.09	6.40	Si	68
0	(8+9)-V-2	35	0.18	6.40	Si	35
0	(8+9)-VIII-2	21	0.11	6.40	Si	58
0	(8+9)-V-3	-35	0.18	6.40	Si	36
0	(8+9)-I-2	27	0.14	6.40	Si	46
0	(8+9)-V-4	-24	0.13	6.40	Si	51
0	(8+9)-II-2	24	0.12	6.40	Si	52
0	(8+9)-III-2	26	0.13	6.40	Si	49
0	(8+9)-VII-3	-33	0.17	6.40	Si	38
0	(8+9)-I-4	-16	0.08	6.40	Si	76
0	(8+9)-II-4	11	0.06	6.40	Si	>100
0	(8+9)-VII-2	34	0.17	6.40	Si	37
0	(8+9)-VI-2	26	0.14	6.40	Si	47
0	(8+9)-VI-3	-26	0.13	6.40	Si	48
1532	1	-1	0.01	3.84	Si	>100
1532	4	-1	0.01	5.12	Si	>100
1532	5	-1	0.01	5.12	Si	>100
1532	6	-1	0.01	5.12	Si	>100
1532	7	-1	0.01	5.12	Si	>100
1532	(8+9)-VI-4	11	0.06	6.40	Si	>100
1532	(8+9)-VI-1	-12	0.06	6.40	Si	>100
1532	(8+9)-VIII-1	-9	0.04	6.40	Si	>100
1532	(8+9)-VIII-4	7	0.04	6.40	Si	>100

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Tx kg	τ_{vd} kg/cmq	fvd kg/cmq	Csv	τ_M kg/cmq	fTd kg/cmq	Csm	Mecc.	Cs
0	1	-441	-0.30	19.20	63	-0.07	12.00	>100	V	63
0	2	-713	-0.49	28.80	58	-0.12	18.00	>100	V	58
0	3	-713	-0.49	28.80	58	-0.12	18.00	>100	V	58
0	4	-441	-0.30	25.60	84	-0.07	16.00	>100	V	84
0	5	-441	-0.30	25.60	84	-0.07	16.00	>100	V	84

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
0	6	-441	-0.30	25.60	84	-0.07	16.00	>100	V	84
0	7	-441	-0.30	25.60	84	-0.07	16.00	>100	V	84
0	(8+9)-VIII-4	-5238	-3.62	32.00	8.8	-0.88	20.00	23	V	8.8
0	(8+9)-V-1	-4355	-3.01	32.00	11	-0.73	20.00	27	V	11
0	(8+9)-I-2	-7829	-5.41	32.00	5.9	-1.31	20.00	15	V	5.9
0	(8+9)-V-2	-9226	-6.38	32.00	5.0	-1.54	20.00	13	V	5.0
0	(8+9)-I-4	2337	1.61	32.00	20	0.39	20.00	51	V	20
0	(8+9)-V-3	8606	5.95	32.00	5.4	1.44	20.00	14	V	5.4
0	(8+9)-II-2	-9954	-6.88	32.00	4.7	-1.66	20.00	12	V	4.7
0	(8+9)-V-4	3735	2.58	32.00	12	0.62	20.00	32	V	12
0	(8+9)-II-4	-6904	-4.77	32.00	6.7	-1.15	20.00	17	V	6.7
0	(8+9)-VIII-2	-9126	-6.31	32.00	5.1	-1.53	20.00	13	V	5.1
0	(8+9)-III-1	-3331	-2.30	32.00	14	-0.56	20.00	36	V	14
0	(8+9)-III-2	-7454	-5.15	32.00	6.2	-1.25	20.00	16	V	6.2
0	(8+9)-III-4	2711	1.87	32.00	17	0.45	20.00	44	V	17
0	(8+9)-VI-2	-10373	-7.17	32.00	4.5	-1.73	20.00	12	V	4.5
0	(8+9)-IV-2	-8707	-6.02	32.00	5.3	-1.46	20.00	14	V	5.3
0	(8+9)-VI-3	9753	6.74	32.00	4.7	1.63	20.00	12	V	4.7
0	(8+9)-IV-4	-5657	-3.91	32.00	8.2	-0.95	20.00	21	V	8.2
0	(8+9)-VI-4	-6485	-4.48	32.00	7.1	-1.08	20.00	18	V	7.1
0	(8+9)-VIII-3	8506	5.88	32.00	5.4	1.42	20.00	14	V	5.4
0	(8+9)-VII-1	-4729	-3.27	32.00	9.8	-0.79	20.00	25	V	9.8
0	(8+9)-III-3	6834	4.72	32.00	6.8	1.14	20.00	18	V	6.8
0	(8+9)-IV-3	8086	5.59	32.00	5.7	1.35	20.00	15	V	5.7
0	(8+9)-I-3	7208	4.98	32.00	6.4	1.21	20.00	17	V	6.4
0	(8+9)-II-3	9334	6.45	32.00	5.0	1.56	20.00	13	V	5.0
0	(8+9)-I-1	-2957	-2.04	32.00	16	-0.49	20.00	40	V	16
0	(8+9)-VII-2	-8852	-6.12	32.00	5.2	-1.48	20.00	14	V	5.2
0	(8+9)-VII-3	8232	5.69	32.00	5.6	1.38	20.00	15	V	5.6
0	(8+9)-VII-4	4109	2.84	32.00	11	0.69	20.00	29	V	11
186	(8+9)-IV-1	5152	3.52	32.00	9.1	0.85	20.00	23	V	9.1
186	(8+9)-VIII-1	4682	3.20	32.00	10	0.77	20.00	26	V	10
186	(8+9)-II-1	6413	4.38	32.00	7.3	1.06	20.00	19	V	7.3
186	(8+9)-VI-1	5943	4.06	32.00	7.9	0.98	20.00	20	V	7.9
Verifiche nella direzione secondaria										
1532	1	38	0.21	19.20	91	0.05	12.00	>100	V	91
1532	2	64	0.35	28.80	81	0.09	18.00	>100	V	81
1532	3	64	0.35	28.80	81	0.09	18.00	>100	V	81
1532	4	38	0.21	25.60	>100	0.05	16.00	>100	V	>100
1532	5	38	0.21	25.60	>100	0.05	16.00	>100	V	>100
1532	6	38	0.21	25.60	>100	0.05	16.00	>100	V	>100
1532	7	38	0.21	25.60	>100	0.05	16.00	>100	V	>100
1532	(8+9)-VIII-4	804	4.47	32.00	7.2	1.08	20.00	18	V	7.2
1532	(8+9)-IV-2	1323	7.35	32.00	4.4	1.78	20.00	11	V	4.4
1532	(8+9)-V-1	646	3.59	32.00	8.9	0.87	20.00	23	V	8.9
1532	(8+9)-I-2	1134	6.30	32.00	5.1	1.52	20.00	13	V	5.1
1532	(8+9)-V-2	1412	7.84	32.00	4.1	1.90	20.00	11	V	4.1
1532	(8+9)-I-4	-315	-1.75	32.00	18	-0.42	20.00	47	V	18
1532	(8+9)-V-3	-1359	-7.55	32.00	4.2	-1.83	20.00	11	V	4.2
1532	(8+9)-II-2	1520	8.44	32.00	3.8	2.04	20.00	9.8	V	3.8
1532	(8+9)-V-4	-593	-3.29	32.00	9.7	-0.80	20.00	25	V	9.7
1532	(8+9)-II-4	1086	6.03	32.00	5.3	1.46	20.00	14	V	5.3
1532	(8+9)-VI-1	-950	-5.27	32.00	6.1	-1.28	20.00	16	V	6.1
1532	(8+9)-III-2	1074	5.97	32.00	5.4	1.44	20.00	14	V	5.4
1532	(8+9)-VI-2	1604	8.91	32.00	3.6	2.16	20.00	9.3	V	3.6
1532	(8+9)-III-4	-374	-2.08	32.00	15	-0.50	20.00	40	V	15
1532	(8+9)-VI-3	-1551	-8.62	32.00	3.7	-2.08	20.00	9.6	V	3.7
1532	(8+9)-I-1	368	2.04	32.00	16	0.49	20.00	40	V	16
1532	(8+9)-VI-4	1002	5.57	32.00	5.7	1.35	20.00	15	V	5.7
1532	(8+9)-IV-4	888	4.93	32.00	6.5	1.19	20.00	17	V	6.5
1532	(8+9)-VII-1	705	3.92	32.00	8.2	0.95	20.00	21	V	8.2
1532	(8+9)-II-1	-1033	-5.74	32.00	5.6	-1.39	20.00	14	V	5.6
1532	(8+9)-VII-2	1352	7.51	32.00	4.3	1.82	20.00	11	V	4.3
1532	(8+9)-III-1	427	2.37	32.00	13	0.57	20.00	35	V	13

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
1532	(8+9)-VII-3	-1300	-7.22	32.00	4.4	-1.75	20.00	11	V	4.4
1532	(8+9)-IV-1	-835	-4.64	32.00	6.9	-1.12	20.00	18	V	6.9
1532	(8+9)-VII-4	-653	-3.62	32.00	8.8	-0.88	20.00	23	V	8.8
1532	(8+9)-III-3	-1022	-5.68	32.00	5.6	-1.37	20.00	15	V	5.6
1532	(8+9)-IV-3	-1270	-7.05	32.00	4.5	-1.71	20.00	12	V	4.5
1532	(8+9)-II-3	-1468	-8.15	32.00	3.9	-1.97	20.00	10	V	3.9
1532	(8+9)-VIII-1	-752	-4.18	32.00	7.7	-1.01	20.00	20	V	7.7
1532	(8+9)-VIII-2	1406	7.81	32.00	4.1	1.89	20.00	11	V	4.1
1532	(8+9)-VIII-3	-1353	-7.52	32.00	4.3	-1.82	20.00	11	V	4.3
1532	(8+9)-I-3	-1081	-6.00	32.00	5.3	-1.45	20.00	14	V	5.3

Setto 9: origine (1681.3,976.3,60.0), direzione (-0.201275,0.979535,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	(8+9)-III-1	354	43	-583	0.41	1.86	-3.35	132.00	192.00	192.00	33
0	(8+9)-I-1	295	39	-496	0.34	1.68	-2.85	132.00	192.00	192.00	38
1500	1	-292	9	26	-0.33	0.40	0.15	79.20	115.20	115.20	>100
1500	2	-582	20	41	-0.67	0.86	0.24	118.80	172.80	172.80	>100
1500	3	-582	20	41	-0.67	0.86	0.24	118.80	172.80	172.80	>100
1500	4	-292	9	26	-0.33	0.40	0.15	105.60	153.60	153.60	>100
1500	5	-292	9	26	-0.33	0.40	0.15	105.60	153.60	153.60	>100
1500	6	-292	9	26	-0.33	0.40	0.15	105.60	153.60	153.60	>100
1500	7	-292	9	26	-0.33	0.40	0.15	105.60	153.60	153.60	>100
1500	(8+9)-IV-3	3838	14	-2555	4.41	0.62	-14.66	132.00	192.00	192.00	8.9
1500	(8+9)-V-4	1753	-4	-1221	2.01	-0.19	-7.01	132.00	192.00	192.00	19
1500	(8+9)-I-4	859	-9	-635	0.99	-0.40	-3.64	132.00	192.00	192.00	35
1500	(8+9)-VI-1	2812	23	-1926	3.23	0.98	-11.05	132.00	192.00	192.00	11
1500	(8+9)-II-2	-4848	-5	2995	-5.57	-0.20	17.19	132.00	192.00	192.00	11
1500	(8+9)-VI-2	-5116	-6	3171	-5.87	-0.26	18.20	132.00	192.00	192.00	10
1500	(8+9)-II-4	-3495	-11	2143	-4.01	-0.49	12.30	132.00	192.00	192.00	15
1500	(8+9)-VI-3	4702	19	-3129	5.40	0.81	-17.96	132.00	192.00	192.00	7.2
1500	(8+9)-III-2	-3474	14	2086	-3.99	0.62	11.97	132.00	192.00	192.00	15
1500	(8+9)-VI-4	-3227	-10	1968	-3.70	-0.43	11.29	132.00	192.00	192.00	16
1500	(8+9)-III-4	1037	-8	-755	1.19	-0.36	-4.33	132.00	192.00	192.00	30
1500	(8+9)-VII-1	-2346	16	1382	-2.69	0.70	7.93	132.00	192.00	192.00	22
1500	(8+9)-IV-2	-4253	-2	2596	-4.88	-0.07	14.90	132.00	192.00	192.00	13
1500	(8+9)-VII-2	-4368	9	2672	-5.01	0.41	15.33	132.00	192.00	192.00	12
1500	(8+9)-IV-4	-2900	-8	1744	-3.33	-0.36	10.01	132.00	192.00	192.00	18
1500	(8+9)-VII-3	3953	3	-2630	4.54	0.14	-15.09	132.00	192.00	192.00	8.8
1500	(8+9)-V-2	-4546	9	2792	-5.22	0.37	16.02	132.00	192.00	192.00	12
1500	(8+9)-VII-4	1931	-4	-1340	2.22	-0.15	-7.69	132.00	192.00	192.00	17
1500	(8+9)-II-1	3080	24	-2101	3.54	1.04	-12.06	132.00	192.00	192.00	11
1500	(8+9)-VIII-1	2217	20	-1527	2.54	0.85	-8.76	132.00	192.00	192.00	14
1500	(8+9)-I-3	3237	-1	-2164	3.72	-0.03	-12.42	132.00	192.00	192.00	11
1500	(8+9)-VIII-2	-4521	-3	2772	-5.19	-0.13	15.91	132.00	192.00	192.00	12
1500	(8+9)-IV-1	2485	21	-1702	2.85	0.91	-9.77	132.00	192.00	192.00	13
1500	(8+9)-VIII-3	4106	16	-2730	4.71	0.68	-15.67	132.00	192.00	192.00	8.3
1500	(8+9)-V-1	-2168	17	1263	-2.49	0.74	7.25	132.00	192.00	192.00	24
1500	(8+9)-II-3	4434	17	-2954	5.09	0.75	-16.95	132.00	192.00	192.00	7.6
1500	(8+9)-III-3	3059	-2	-2044	3.51	-0.07	-11.73	132.00	192.00	192.00	11
1500	(8+9)-I-2	-3652	13	2206	-4.19	0.58	12.66	132.00	192.00	192.00	14
1500	(8+9)-V-3	4131	4	-2750	4.74	0.18	-15.78	132.00	192.00	192.00	8.4
1500	(8+9)-VIII-4	-2631	-7	1569	-3.02	-0.30	9.00	132.00	192.00	192.00	21
Verifiche nella direzione secondaria											
600	(8+9)-II-1	-327	-16	3876	-0.45	-1.28	21.35	132.00	192.00	192.00	8.5
600	(8+9)-VI-1	-367	-23	3590	-0.51	-1.78	19.78	132.00	192.00	192.00	8.9
1200	1	-1668	-2	-562	-2.30	-0.12	-3.10	79.20	115.20	115.20	35
1200	2	-2764	-4	-990	-3.81	-0.31	-5.46	118.80	172.80	172.80	30
1200	3	-2764	-4	-990	-3.81	-0.31	-5.46	118.80	172.80	172.80	30
1200	4	-1668	-2	-562	-2.30	-0.12	-3.10	105.60	153.60	153.60	47
1200	5	-1668	-2	-562	-2.30	-0.12	-3.10	105.60	153.60	153.60	47
1200	6	-1668	-2	-562	-2.30	-0.12	-3.10	105.60	153.60	153.60	47

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
1200	7	-1668	-2	-562	-2.30	-0.12	-3.10	105.60	153.60	153.60	47
1200	(8+9)-VIII-4	-1062	31	-3683	-1.46	2.43	-20.29	132.00	192.00	192.00	8.4
1200	(8+9)-IV-3	-398	-4	6228	-0.55	-0.34	34.32	132.00	192.00	192.00	5.5
1200	(8+9)-V-2	-2359	-54	-8229	-3.25	-4.23	-45.34	132.00	192.00	192.00	3.9
1200	(8+9)-I-4	451	42	2912	0.62	3.28	16.04	132.00	192.00	192.00	9.5
1200	(8+9)-V-3	56	52	7433	0.08	4.07	40.95	132.00	192.00	192.00	4.3
1200	(8+9)-II-2	-943	-18	-7219	-1.30	-1.42	-39.77	132.00	192.00	192.00	4.7
1200	(8+9)-V-4	435	49	4225	0.60	3.89	23.28	132.00	192.00	192.00	6.8
1200	(8+9)-II-4	-95	8	-4270	-0.13	0.65	-23.53	132.00	192.00	192.00	7.9
1200	(8+9)-I-1	-2755	-44	-3708	-3.79	-3.44	-20.43	132.00	192.00	192.00	8.0
1200	(8+9)-III-2	-2664	-40	-6858	-3.67	-3.14	-37.79	132.00	192.00	192.00	4.7
1200	(8+9)-VI-2	-938	-20	-7613	-1.29	-1.60	-41.94	132.00	192.00	192.00	4.4
1200	(8+9)-III-4	163	48	2970	0.22	3.75	16.36	132.00	192.00	192.00	9.4
1200	(8+9)-VI-3	-1365	18	6816	-1.88	1.44	37.55	132.00	192.00	192.00	4.9
1200	(8+9)-IV-2	-1905	2	-7025	-2.62	0.18	-38.70	132.00	192.00	192.00	4.9
1200	(8+9)-VI-4	-100	11	-3876	-0.14	0.83	-21.36	132.00	192.00	192.00	8.7
1200	(8+9)-IV-4	-1057	29	-4076	-1.46	2.25	-22.46	132.00	192.00	192.00	7.8
1200	(8+9)-VII-1	-2450	-58	-5080	-3.38	-4.53	-27.99	132.00	192.00	192.00	5.9
1200	(8+9)-I-3	72	44	6120	0.10	3.46	33.72	132.00	192.00	192.00	5.1
1200	(8+9)-VII-2	-2648	-48	-8171	-3.65	-3.75	-45.02	132.00	192.00	192.00	3.9
1200	(8+9)-III-1	-2466	-50	-3767	-3.40	-3.92	-20.75	132.00	192.00	192.00	7.8
1200	(8+9)-VII-3	345	46	7375	0.47	3.59	40.63	132.00	192.00	192.00	4.3
1200	(8+9)-IV-1	-1246	-31	3280	-1.72	-2.41	18.07	132.00	192.00	192.00	9.4
1200	(8+9)-VII-4	147	55	4283	0.20	4.36	23.60	132.00	192.00	192.00	6.8
1200	(8+9)-III-3	361	38	6061	0.50	2.98	33.40	132.00	192.00	192.00	5.2
1200	(8+9)-I-2	-2375	-46	-6916	-3.27	-3.62	-38.11	132.00	192.00	192.00	4.6
1200	(8+9)-II-3	-1360	16	6422	-1.87	1.25	35.38	132.00	192.00	192.00	5.2
1200	(8+9)-VIII-1	-1241	-33	2886	-1.71	-2.60	15.90	132.00	192.00	192.00	10
1200	(8+9)-VIII-2	-1900	-0	-7419	-2.62	-0.01	-40.88	132.00	192.00	192.00	4.7
1200	(8+9)-VIII-3	-403	-2	6622	-0.56	-0.16	36.49	132.00	192.00	192.00	5.2
1200	(8+9)-V-1	-2739	-51	-5022	-3.77	-4.05	-27.67	132.00	192.00	192.00	6.0

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
0	(8+9)-V-2	-24	0.02	6.40	Si	>100
0	(8+9)-IV-3	7	0.01	6.40	Si	>100
0	(8+9)-III-1	-12	0.01	6.40	Si	>100
0	(8+9)-I-2	-12	0.01	6.40	Si	>100
0	(8+9)-VIII-1	-4	0.00	6.40	Si	>100
0	(8+9)-I-3	14	0.01	6.40	Si	>100
0	(8+9)-VI-1	-7	0.01	6.40	Si	>100
0	(8+9)-I-4	14	0.01	6.40	Si	>100
0	(8+9)-V-1	-24	0.02	6.40	Si	>100
0	(8+9)-VII-2	-25	0.02	6.40	Si	>100
0	(8+9)-I-1	-12	0.01	6.40	Si	>100
0	(8+9)-III-3	14	0.01	6.40	Si	>100
0	(8+9)-VI-2	-7	0.01	6.40	Si	>100
0	(8+9)-VII-1	-23	0.02	6.40	Si	>100
750	(8+9)-VI-3	11	0.01	6.40	Si	>100
750	(8+9)-II-3	7	0.01	6.40	Si	>100
750	(8+9)-V-4	28	0.02	6.40	Si	>100
750	(8+9)-VI-4	11	0.01	6.40	Si	>100
750	(8+9)-III-4	14	0.01	6.40	Si	>100
750	(8+9)-VII-3	28	0.02	6.40	Si	>100
750	(8+9)-VIII-3	11	0.01	6.40	Si	>100
750	(8+9)-II-4	7	0.01	6.40	Si	>100
750	(8+9)-V-3	28	0.02	6.40	Si	>100
750	(8+9)-VII-4	28	0.02	6.40	Si	>100
1500	1	11	0.01	3.84	Si	>100
1500	2	25	0.02	5.76	Si	>100
1500	3	25	0.02	5.76	Si	>100
1500	4	11	0.01	5.12	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
1500	5	11	0.01	5.12	Si	>100
1500	6	11	0.01	5.12	Si	>100
1500	7	11	0.01	5.12	Si	>100
1500	(8+9)-IV-4	13	0.01	6.40	Si	>100
1500	(8+9)-IV-2	15	0.01	6.40	Si	>100
1500	(8+9)-II-1	9	0.01	6.40	Si	>100
1500	(8+9)-III-2	14	0.01	6.40	Si	>100
1500	(8+9)-IV-1	2	0.00	6.40	Si	>100
1500	(8+9)-VIII-2	13	0.01	6.40	Si	>100
1500	(8+9)-II-2	9	0.01	6.40	Si	>100
1500	(8+9)-VIII-4	15	0.01	6.40	Si	>100
Verifiche nella direzione secondaria						
0	(8+9)-II-1	9	0.01	6.40	Si	>100
0	(8+9)-VI-1	11	0.01	6.40	Si	>100
600	(8+9)-VIII-4	17	0.02	6.40	Si	>100
1200	1	15	0.02	3.84	Si	>100
1200	2	35	0.04	5.76	Si	>100
1200	3	35	0.04	5.76	Si	>100
1200	4	15	0.02	5.12	Si	>100
1200	5	15	0.02	5.12	Si	>100
1200	6	15	0.02	5.12	Si	>100
1200	7	15	0.02	5.12	Si	>100
1200	(8+9)-IV-3	-42	0.05	6.40	Si	>100
1200	(8+9)-V-1	91	0.12	6.40	Si	55
1200	(8+9)-I-1	75	0.10	6.40	Si	67
1200	(8+9)-V-3	-88	0.11	6.40	Si	57
1200	(8+9)-II-2	62	0.08	6.40	Si	82
1200	(8+9)-V-4	-70	0.09	6.40	Si	72
1200	(8+9)-II-4	18	0.02	6.40	Si	>100
1200	(8+9)-I-2	93	0.12	6.40	Si	54
1200	(8+9)-III-2	93	0.12	6.40	Si	54
1200	(8+9)-VI-2	66	0.08	6.40	Si	76
1200	(8+9)-III-4	-54	0.07	6.40	Si	94
1200	(8+9)-VI-3	-46	0.06	6.40	Si	>100
1200	(8+9)-IV-2	63	0.08	6.40	Si	80
1200	(8+9)-VI-4	13	0.02	6.40	Si	>100
1200	(8+9)-IV-4	19	0.02	6.40	Si	>100
1200	(8+9)-VII-1	91	0.12	6.40	Si	56
1200	(8+9)-V-2	108	0.14	6.40	Si	46
1200	(8+9)-VII-2	109	0.14	6.40	Si	46
1200	(8+9)-III-1	75	0.09	6.40	Si	67
1200	(8+9)-VII-3	-88	0.11	6.40	Si	57
1200	(8+9)-IV-1	2	0.00	6.40	Si	>100
1200	(8+9)-VII-4	-70	0.09	6.40	Si	72
1200	(8+9)-III-3	-72	0.09	6.40	Si	70
1200	(8+9)-I-4	-54	0.07	6.40	Si	93
1200	(8+9)-II-3	-41	0.05	6.40	Si	>100
1200	(8+9)-VIII-1	7	0.01	6.40	Si	>100
1200	(8+9)-VIII-2	68	0.09	6.40	Si	74
1200	(8+9)-VIII-3	-47	0.06	6.40	Si	>100
1200	(8+9)-I-3	-72	0.09	6.40	Si	70

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
1500	1	-287	-0.49	19.20	39	-0.12	12.00	>100	V	39
1500	2	-441	-0.76	28.80	38	-0.18	18.00	98	V	38
1500	3	-441	-0.76	28.80	38	-0.18	18.00	98	V	38
1500	4	-287	-0.49	25.60	52	-0.12	16.00	>100	V	52
1500	5	-287	-0.49	25.60	52	-0.12	16.00	>100	V	52
1500	6	-287	-0.49	25.60	52	-0.12	16.00	>100	V	52
1500	7	-287	-0.49	25.60	52	-0.12	16.00	>100	V	52
1500	(8+9)-VIII-4	-4400	-7.58	32.00	4.2	-1.83	20.00	11	V	4.2

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
1500	(8+9)-IV-1	4454	7.67	32.00	4.2	1.86	20.00	11	V	4.2
1500	(8+9)-V-1	-3592	-6.18	32.00	5.2	-1.50	20.00	13	V	5.2
1500	(8+9)-I-2	-6107	-10.52	32.00	3.0	-2.54	20.00	7.9	V	3.0
1500	(8+9)-V-2	-7662	-13.19	32.00	2.4	-3.19	20.00	6.3	V	2.4
1500	(8+9)-I-4	1625	2.80	32.00	11	0.68	20.00	30	V	11
1500	(8+9)-V-3	7249	12.48	32.00	2.6	3.02	20.00	6.6	V	2.6
1500	(8+9)-II-2	-8149	-14.03	32.00	2.3	-3.40	20.00	5.9	V	2.3
1500	(8+9)-V-4	3180	5.47	32.00	5.8	1.32	20.00	15	V	5.8
1500	(8+9)-II-4	-5829	-10.04	32.00	3.2	-2.43	20.00	8.2	V	3.2
1500	(8+9)-VI-1	4950	8.52	32.00	3.8	2.06	20.00	9.7	V	3.8
1500	(8+9)-III-2	-5818	-10.02	32.00	3.2	-2.42	20.00	8.2	V	3.2
1500	(8+9)-VI-2	-8615	-14.83	32.00	2.2	-3.59	20.00	5.6	V	2.2
1500	(8+9)-III-4	1914	3.30	32.00	9.7	0.80	20.00	25	V	9.7
1500	(8+9)-VI-3	8203	14.12	32.00	2.3	3.42	20.00	5.9	V	2.3
1500	(8+9)-IV-2	-7186	-12.37	32.00	2.6	-2.99	20.00	6.7	V	2.6
1500	(8+9)-VI-4	-5363	-9.23	32.00	3.5	-2.23	20.00	9.0	V	3.5
1500	(8+9)-IV-4	-4866	-8.38	32.00	3.8	-2.03	20.00	9.9	V	3.8
1500	(8+9)-VII-1	-3881	-6.68	32.00	4.8	-1.62	20.00	12	V	4.8
1500	(8+9)-II-1	5417	9.33	32.00	3.4	2.26	20.00	8.9	V	3.4
1500	(8+9)-VII-2	-7373	-12.69	32.00	2.5	-3.07	20.00	6.5	V	2.5
1500	(8+9)-III-1	-2326	-4.01	32.00	8.0	-0.97	20.00	21	V	8.0
1500	(8+9)-VII-3	6961	11.98	32.00	2.7	2.90	20.00	6.9	V	2.7
1500	(8+9)-I-1	-2038	-3.51	32.00	9.1	-0.85	20.00	24	V	9.1
1500	(8+9)-VII-4	3469	5.97	32.00	5.4	1.45	20.00	14	V	5.4
1500	(8+9)-III-3	5406	9.31	32.00	3.4	2.25	20.00	8.9	V	3.4
1500	(8+9)-IV-3	6774	11.66	32.00	2.7	2.82	20.00	7.1	V	2.7
1500	(8+9)-II-3	7737	13.32	32.00	2.4	3.22	20.00	6.2	V	2.4
1500	(8+9)-VIII-1	3988	6.87	32.00	4.7	1.66	20.00	12	V	4.7
1500	(8+9)-VIII-2	-7652	-13.18	32.00	2.4	-3.19	20.00	6.3	V	2.4
1500	(8+9)-VIII-3	7240	12.47	32.00	2.6	3.02	20.00	6.6	V	2.6
1500	(8+9)-I-3	5695	9.81	32.00	3.3	2.37	20.00	8.4	V	3.3
Verifiche nella direzione secondaria										
0	1	177	0.24	19.20	79	0.06	12.00	>100	V	79
0	2	342	0.47	28.80	61	0.11	18.00	>100	V	61
0	3	342	0.47	28.80	61	0.11	18.00	>100	V	61
0	4	177	0.24	25.60	>100	0.06	16.00	>100	V	>100
0	5	177	0.24	25.60	>100	0.06	16.00	>100	V	>100
0	6	177	0.24	25.60	>100	0.06	16.00	>100	V	>100
0	7	177	0.24	25.60	>100	0.06	16.00	>100	V	>100
600	(8+9)-VIII-4	4629	6.38	32.00	5.0	1.54	20.00	13	V	5.0
600	(8+9)-IV-2	7640	10.52	32.00	3.0	2.55	20.00	7.9	V	3.0
600	(8+9)-V-1	3711	5.11	32.00	6.3	1.24	20.00	16	V	6.3
600	(8+9)-I-2	6520	8.98	32.00	3.6	2.17	20.00	9.2	V	3.6
600	(8+9)-V-2	8167	11.25	32.00	2.8	2.72	20.00	7.3	V	2.8
600	(8+9)-I-4	-1869	-2.57	32.00	12	-0.62	20.00	32	V	12
600	(8+9)-V-3	-7972	-10.98	32.00	2.9	-2.66	20.00	7.5	V	2.9
600	(8+9)-II-2	8783	12.10	32.00	2.6	2.93	20.00	6.8	V	2.6
600	(8+9)-V-4	-3516	-4.84	32.00	6.6	-1.17	20.00	17	V	6.6
600	(8+9)-II-4	6266	8.63	32.00	3.7	2.09	20.00	9.6	V	3.7
600	(8+9)-VI-1	-5577	-7.68	32.00	4.2	-1.86	20.00	11	V	4.2
600	(8+9)-III-2	6177	8.51	32.00	3.8	2.06	20.00	9.7	V	3.8
600	(8+9)-VI-2	9277	12.78	32.00	2.5	3.09	20.00	6.5	V	2.5
600	(8+9)-III-4	-2212	-3.05	32.00	11	-0.74	20.00	27	V	11
600	(8+9)-VI-3	-9082	-12.51	32.00	2.6	-3.03	20.00	6.6	V	2.6
600	(8+9)-I-1	2064	2.84	32.00	11	0.69	20.00	29	V	11
600	(8+9)-VI-4	5772	7.95	32.00	4.0	1.92	20.00	10	V	4.0
600	(8+9)-IV-4	5123	7.06	32.00	4.5	1.71	20.00	12	V	4.5
600	(8+9)-VII-1	4053	5.58	32.00	5.7	1.35	20.00	15	V	5.7
600	(8+9)-II-1	-6071	-8.36	32.00	3.8	-2.02	20.00	9.9	V	3.8
600	(8+9)-VII-2	7824	10.78	32.00	3.0	2.61	20.00	7.7	V	3.0
600	(8+9)-III-1	2407	3.31	32.00	9.7	0.80	20.00	25	V	9.7
600	(8+9)-VII-3	-7629	-10.51	32.00	3.0	-2.54	20.00	7.9	V	3.0
600	(8+9)-VII-4	-3859	-5.32	32.00	6.0	-1.29	20.00	16	V	6.0
600	(8+9)-I-3	-6325	-8.71	32.00	3.7	-2.11	20.00	9.5	V	3.7

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
600	(8+9)-III-3	-5983	-8.24	32.00	3.9	-1.99	20.00	10	V	3.9
600	(8+9)-IV-3	-7445	-10.26	32.00	3.1	-2.48	20.00	8.1	V	3.1
600	(8+9)-II-3	-8588	-11.83	32.00	2.7	-2.86	20.00	7.0	V	2.7
600	(8+9)-VIII-3	-7939	-10.94	32.00	2.9	-2.65	20.00	7.6	V	2.9
600	(8+9)-VIII-2	8134	11.20	32.00	2.9	2.71	20.00	7.4	V	2.9
1200	(8+9)-VIII-1	-4480	-6.17	32.00	5.2	-1.49	20.00	13	V	5.2
1200	(8+9)-IV-1	-4950	-6.82	32.00	4.7	-1.65	20.00	12	V	4.7

Setto 10: origine (1681.3,976.3,307.8), direzione (-0.201275,0.979535,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	
0	(8+9)-VIII-4	-5127	-608	-445	-9.33	-41.54	-6.42	132.00	192.00	192.00	4.0
0	(8+9)-IV-1	6262	648	483	11.39	44.30	6.96	132.00	192.00	192.00	2.8
0	(8+9)-VI-4	-6224	-379	-566	-11.32	-25.92	-8.16	132.00	192.00	192.00	5.5
0	(8+9)-III-2	-6527	604	-604	-11.88	41.31	-8.72	132.00	192.00	192.00	3.8
0	(8+9)-IV-2	-8507	-201	-747	-15.48	-13.74	-10.77	132.00	192.00	192.00	7.5
0	(8+9)-III-3	7015	-593	588	12.77	-40.53	8.47	132.00	192.00	192.00	2.8
0	(8+9)-VIII-2	-9154	-230	-801	-16.66	-15.72	-11.56	132.00	192.00	192.00	6.7
0	(8+9)-III-4	2585	-848	219	4.70	-57.94	3.15	132.00	192.00	192.00	2.8
0	(8+9)-VII-4	4740	-751	401	8.62	-51.35	5.79	132.00	192.00	192.00	2.8
0	(8+9)-VII-2	-8682	508	-787	-15.80	34.73	-11.35	132.00	192.00	192.00	4.1
0	(8+9)-I-2	-6856	673	-641	-12.48	46.00	-9.24	132.00	192.00	192.00	3.4
0	(8+9)-I-4	2256	-779	182	4.10	-53.26	2.63	132.00	192.00	192.00	3.1
0	(8+9)-IV-3	8996	212	730	16.37	14.52	10.53	132.00	192.00	192.00	3.9
0	(8+9)-VII-3	9171	-497	770	16.69	-33.94	11.11	132.00	192.00	192.00	2.8
0	(8+9)-IV-4	-5774	-637	-500	-10.51	-43.52	-7.21	132.00	192.00	192.00	3.7
0	(8+9)-II-4	-6870	-408	-621	-12.50	-27.90	-8.95	132.00	192.00	192.00	5.1
0	(8+9)-V-1	-3923	694	-382	-7.14	47.45	-5.51	132.00	192.00	192.00	3.6
0	(8+9)-VIII-3	9642	241	785	17.55	16.50	11.32	132.00	192.00	192.00	3.6
0	(8+9)-V-2	-9011	577	-823	-16.40	39.41	-11.87	132.00	192.00	192.00	3.6
0	(8+9)-I-1	-1767	791	-199	-3.22	54.04	-2.87	132.00	192.00	192.00	3.4
0	(8+9)-V-3	9500	-565	806	17.29	-38.63	11.63	132.00	192.00	192.00	2.5
0	(8+9)-II-1	7358	420	604	13.39	28.68	8.71	132.00	192.00	192.00	3.4
0	(8+9)-V-4	4411	-683	365	8.03	-46.67	5.27	132.00	192.00	192.00	3.0
0	(8+9)-III-1	-2096	859	-236	-3.81	58.73	-3.40	132.00	192.00	192.00	3.1
0	(8+9)-I-3	7344	-661	624	13.36	-45.21	9.00	132.00	192.00	192.00	2.6
0	(8+9)-II-3	10092	-16	851	18.36	-1.09	12.27	132.00	192.00	192.00	4.8
0	(8+9)-VIII-1	5616	619	428	10.22	42.32	6.17	132.00	192.00	192.00	3.0
0	(8+9)-VI-1	6712	391	549	12.21	26.71	7.92	132.00	192.00	192.00	3.7
0	(8+9)-VII-1	-4251	763	-418	-7.74	52.14	-6.03	132.00	192.00	192.00	3.3
0	(8+9)-VI-3	10739	13	905	19.54	0.88	13.06	132.00	192.00	192.00	4.5
750	1	325	21	158	0.50	1.20	1.59	79.20	115.20	115.20	33
750	2	506	44	276	0.77	2.54	2.79	118.80	172.80	172.80	27
750	3	506	44	276	0.77	2.54	2.79	118.80	172.80	172.80	27
750	4	325	21	158	0.50	1.20	1.59	105.60	153.60	153.60	44
750	5	325	21	158	0.50	1.20	1.59	105.60	153.60	153.60	44
750	6	325	21	158	0.50	1.20	1.59	105.60	153.60	153.60	44
750	7	325	21	158	0.50	1.20	1.59	105.60	153.60	153.60	44
1500	(8+9)-VI-2	-8011	-267	923	-10.49	-13.16	6.89	132.00	192.00	192.00	9.3
1500	(8+9)-II-2	-7176	-292	1062	-9.40	-14.36	7.93	132.00	192.00	192.00	8.4
Verifiche nella direzione secondaria											
0	(8+9)-VIII-4	-1385	25	2608	-1.91	1.98	14.37	132.00	192.00	192.00	12
0	(8+9)-IV-4	-1290	10	2948	-1.78	0.79	16.24	132.00	192.00	192.00	11
0	(8+9)-II-2	-1904	11	4420	-2.62	0.87	24.35	132.00	192.00	192.00	7.6
0	(8+9)-IV-2	-1950	16	3843	-2.69	1.25	21.17	132.00	192.00	192.00	8.6
0	(8+9)-II-3	406	-5	-3482	0.56	-0.41	-19.18	132.00	192.00	192.00	9.4
0	(8+9)-VIII-2	-1855	1	4183	-2.56	0.05	23.05	132.00	192.00	192.00	8.3
0	(8+9)-II-4	-1243	5	3525	-1.71	0.41	19.42	132.00	192.00	192.00	9.7
0	(8+9)-VII-4	-227	47	-1278	-0.31	3.68	-7.04	132.00	192.00	192.00	18
0	(8+9)-VI-1	-159	-15	-2247	-0.22	-1.15	-12.38	132.00	192.00	192.00	14
0	(8+9)-VII-2	-1793	-35	3972	-2.47	-2.75	21.89	132.00	192.00	192.00	7.8
0	(8+9)-V-4	-213	45	-1105	-0.29	3.57	-6.09	132.00	192.00	192.00	20

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-VI-3	310	10	-3822	0.43	0.78	-21.06	132.00	192.00	192.00	8.5
0	(8+9)-V-3	281	42	-3207	0.39	3.32	-17.67	132.00	192.00	192.00	8.9
0	(8+9)-II-1	-255	1	-2587	-0.35	0.05	-14.25	132.00	192.00	192.00	13
0	(8+9)-V-2	-1779	-36	4146	-2.45	-2.87	22.84	132.00	192.00	192.00	7.5
0	(8+9)-VI-4	-1339	20	3185	-1.84	1.61	17.55	132.00	192.00	192.00	10
0	(8+9)-VI-2	-1808	-4	4760	-2.49	-0.32	26.23	132.00	192.00	192.00	7.2
0	(8+9)-VIII-3	357	5	-3244	0.49	0.41	-17.87	132.00	192.00	192.00	10
0	(8+9)-VII-3	295	41	-3034	0.41	3.21	-16.71	132.00	192.00	192.00	9.4
0	(8+9)-IV-1	-208	-4	-2009	-0.29	-0.33	-11.07	132.00	192.00	192.00	17
0	(8+9)-VIII-1	-113	-19	-1669	-0.16	-1.52	-9.20	132.00	192.00	192.00	18
0	(8+9)-IV-3	453	-10	-2904	0.62	-0.79	-16.00	132.00	192.00	192.00	11
526	1	-664	9	760	-0.92	0.74	4.19	79.20	115.20	115.20	23
526	2	-800	20	1539	-1.10	1.57	8.48	118.80	172.80	172.80	17
526	3	-800	20	1539	-1.10	1.57	8.48	118.80	172.80	172.80	17
526	4	-664	9	760	-0.92	0.74	4.19	105.60	153.60	153.60	31
526	5	-664	9	760	-0.92	0.74	4.19	105.60	153.60	153.60	31
526	6	-664	9	760	-0.92	0.74	4.19	105.60	153.60	153.60	31
526	7	-664	9	760	-0.92	0.74	4.19	105.60	153.60	153.60	31
526	(8+9)-VII-1	-856	117	1187	-1.18	9.23	6.54	132.00	192.00	192.00	12
526	(8+9)-V-1	-849	115	1132	-1.17	9.04	6.23	132.00	192.00	192.00	13
526	(8+9)-III-1	-667	235	893	-0.92	18.49	4.92	132.00	192.00	192.00	8.2
526	(8+9)-I-1	-660	232	837	-0.91	18.30	4.61	132.00	192.00	192.00	8.4
526	(8+9)-I-4	-237	-219	212	-0.33	-17.27	1.17	132.00	192.00	192.00	10
526	(8+9)-I-3	171	-213	-545	0.24	-16.76	-3.00	132.00	192.00	192.00	9.5
526	(8+9)-III-2	-1062	223	1539	-1.46	17.59	8.48	132.00	192.00	192.00	7.4
526	(8+9)-III-3	165	-210	-490	0.23	-16.57	-2.70	132.00	192.00	192.00	9.8
526	(8+9)-III-4	-230	-222	157	-0.32	-17.47	0.86	132.00	192.00	192.00	10
526	(8+9)-I-2	-1068	226	1595	-1.47	17.79	8.79	132.00	192.00	192.00	7.2

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Ty kg	τ_d kg/cmq	fvd kg/cmq	RS	Cs
0	(8+9)-VI-2	-6	0.01	6.40	Si	>100
0	(8+9)-VIII-3	31	0.04	6.40	Si	>100
750	(8+9)-III-3	777	0.86	6.40	Si	7.4
750	(8+9)-I-3	779	0.86	6.40	Si	7.4
750	(8+9)-IV-3	118	0.13	6.40	Si	49
750	(8+9)-II-1	-359	0.40	6.40	Si	16
750	(8+9)-II-2	-97	0.11	6.40	Si	59
750	(8+9)-III-4	860	0.95	6.40	Si	6.7
750	(8+9)-II-3	124	0.14	6.40	Si	46
750	(8+9)-I-2	-752	0.83	6.40	Si	7.7
750	(8+9)-I-4	858	0.95	6.40	Si	6.7
750	(8+9)-IV-1	-365	0.40	6.40	Si	16
750	(8+9)-I-1	-831	0.92	6.40	Si	7.0
750	(8+9)-IV-4	392	0.43	6.40	Si	15
750	(8+9)-II-4	386	0.43	6.40	Si	15
750	(8+9)-III-1	-833	0.92	6.40	Si	6.9
750	(8+9)-III-2	-750	0.83	6.40	Si	7.7
1500	1	25	0.02	3.84	Si	>100
1500	2	53	0.05	5.76	Si	>100
1500	3	53	0.05	5.76	Si	>100
1500	4	25	0.02	5.12	Si	>100
1500	5	25	0.02	5.12	Si	>100
1500	6	25	0.02	5.12	Si	>100
1500	7	25	0.02	5.12	Si	>100
1500	(8+9)-VI-4	411	0.39	6.40	Si	16
1500	(8+9)-VII-4	776	0.74	6.40	Si	8.7
1500	(8+9)-V-3	651	0.62	6.40	Si	10
1500	(8+9)-VIII-1	-418	0.40	6.40	Si	16
1500	(8+9)-VI-1	-377	0.36	6.40	Si	18
1500	(8+9)-VII-2	37	0.04	6.40	Si	>100
1500	(8+9)-VI-3	37	0.04	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
1500	(8+9)-IV-2	125	0.12	6.40	Si	54
1500	(8+9)-VII-1	-742	0.71	6.40	Si	9.1
1500	(8+9)-VIII-4	452	0.43	6.40	Si	15
1500	(8+9)-VII-3	639	0.61	6.40	Si	11
1500	(8+9)-V-2	-617	0.59	6.40	Si	11
1500	(8+9)-V-1	-729	0.69	6.40	Si	9.2
1500	(8+9)-VII-2	-605	0.58	6.40	Si	11
1500	(8+9)-V-4	764	0.73	6.40	Si	8.8
Verifiche nella direzione secondaria						
0	(8+9)-VI-2	39	0.05	6.40	Si	>100
0	(8+9)-VIII-2	12	0.02	6.40	Si	>100
0	(8+9)-VI-3	-34	0.04	6.40	Si	>100
526	1	14	0.02	3.84	Si	>100
526	2	30	0.04	5.76	Si	>100
526	3	30	0.04	5.76	Si	>100
526	4	14	0.02	5.12	Si	>100
526	5	14	0.02	5.12	Si	>100
526	6	14	0.02	5.12	Si	>100
526	7	14	0.02	5.12	Si	>100
526	(8+9)-VIII-4	-120	0.15	6.40	Si	42
526	(8+9)-IV-3	-414	0.53	6.40	Si	12
526	(8+9)-V-3	-185	0.24	6.40	Si	27
526	(8+9)-II-1	554	0.70	6.40	Si	9.1
526	(8+9)-V-4	-217	0.28	6.40	Si	23
526	(8+9)-II-3	-428	0.54	6.40	Si	12
526	(8+9)-VI-1	126	0.16	6.40	Si	40
526	(8+9)-III-1	1666	2.12	6.40	Si	3.0
526	(8+9)-I-3	-1611	2.05	6.40	Si	3.1
526	(8+9)-III-3	-1606	2.04	6.40	Si	3.1
526	(8+9)-I-2	1631	2.07	6.40	Si	3.1
526	(8+9)-IV-1	568	0.72	6.40	Si	8.9
526	(8+9)-VI-4	-106	0.13	6.40	Si	47
526	(8+9)-I-4	-1642	2.09	6.40	Si	3.1
526	(8+9)-VII-1	241	0.31	6.40	Si	21
526	(8+9)-V-1	237	0.30	6.40	Si	21
526	(8+9)-VII-2	201	0.26	6.40	Si	25
526	(8+9)-II-2	448	0.57	6.40	Si	11
526	(8+9)-VII-3	-181	0.23	6.40	Si	28
526	(8+9)-III-2	1626	2.07	6.40	Si	3.1
526	(8+9)-VII-4	-221	0.28	6.40	Si	23
526	(8+9)-V-2	205	0.26	6.40	Si	25
526	(8+9)-II-4	-534	0.68	6.40	Si	9.4
526	(8+9)-III-4	-1646	2.09	6.40	Si	3.1
526	(8+9)-IV-4	-548	0.70	6.40	Si	9.2
526	(8+9)-VIII-1	140	0.18	6.40	Si	36
526	(8+9)-I-1	1662	2.11	6.40	Si	3.0
526	(8+9)-VIII-3	14	0.02	6.40	Si	>100
526	(8+9)-IV-2	434	0.55	6.40	Si	12

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	2	-765	-2.09	28.80	14	-0.51	18.00	36	V	14
0	3	-765	-2.09	28.80	14	-0.51	18.00	36	V	14
0	(8+9)-V-2	-2904	-7.93	32.00	4.0	-1.92	20.00	10	V	4.0
0	(8+9)-II-2	-3062	-8.36	32.00	3.8	-2.02	20.00	9.9	V	3.8
0	(8+9)-VIII-4	-1792	-4.89	32.00	6.5	-1.18	20.00	17	V	6.5
0	(8+9)-II-4	-2251	-6.14	32.00	5.2	-1.49	20.00	13	V	5.2
0	(8+9)-VIII-2	-2920	-7.97	32.00	4.0	-1.93	20.00	10	V	4.0
0	(8+9)-III-1	-1065	-2.91	32.00	11	-0.70	20.00	28	V	11
0	(8+9)-VII-1	-1594	-4.35	32.00	7.4	-1.05	20.00	19	V	7.4
0	(8+9)-III-2	-2285	-6.24	32.00	5.1	-1.51	20.00	13	V	5.1
0	(8+9)-I-2	-2375	-6.48	32.00	4.9	-1.57	20.00	13	V	4.9

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
0	(8+9)-VI-2	-3221	-8.79	32.00	3.6	-2.13	20.00	9.4	V	3.6
0	(8+9)-VI-3	2575	7.03	32.00	4.6	1.70	20.00	12	V	4.6
0	(8+9)-VI-1	1446	3.95	32.00	8.1	0.96	20.00	21	V	8.1
0	(8+9)-VIII-3	2274	6.21	32.00	5.2	1.50	20.00	13	V	5.2
0	(8+9)-VII-2	-2814	-7.68	32.00	4.2	-1.86	20.00	11	V	4.2
0	(8+9)-IV-2	-2762	-7.54	32.00	4.2	-1.82	20.00	11	V	4.2
0	(8+9)-VI-4	-2093	-5.71	32.00	5.6	-1.38	20.00	14	V	5.6
0	(8+9)-II-3	2416	6.59	32.00	4.9	1.60	20.00	13	V	4.9
0	(8+9)-I-1	-975	-2.66	32.00	12	-0.64	20.00	31	V	12
0	(8+9)-II-1	1605	4.38	32.00	7.3	1.06	20.00	19	V	7.3
0	(8+9)-IV-3	2116	5.77	32.00	5.5	1.40	20.00	14	V	5.5
0	(8+9)-IV-4	-1951	-5.32	32.00	6.0	-1.29	20.00	16	V	6.0
0	(8+9)-V-1	-1504	-4.10	32.00	7.8	-0.99	20.00	20	V	7.8
1500	1	671	1.32	19.20	15	0.32	12.00	38	V	15
1500	4	671	1.32	25.60	19	0.32	16.00	50	V	19
1500	5	671	1.32	25.60	19	0.32	16.00	50	V	19
1500	6	671	1.32	25.60	19	0.32	16.00	50	V	19
1500	7	671	1.32	25.60	19	0.32	16.00	50	V	19
1500	(8+9)-IV-1	1840	3.61	32.00	8.9	0.87	20.00	23	V	8.9
1500	(8+9)-V-3	3557	6.99	32.00	4.6	1.69	20.00	12	V	4.6
1500	(8+9)-VII-4	2297	4.51	32.00	7.1	1.09	20.00	18	V	7.1
1500	(8+9)-III-3	2848	5.59	32.00	5.7	1.35	20.00	15	V	5.7
1500	(8+9)-VII-3	3453	6.78	32.00	4.7	1.64	20.00	12	V	4.7
1500	(8+9)-I-4	1588	3.12	32.00	10	0.75	20.00	26	V	10
1500	(8+9)-VIII-1	1659	3.26	32.00	9.8	0.79	20.00	25	V	9.8
1500	(8+9)-III-4	1692	3.32	32.00	9.6	0.80	20.00	25	V	9.6
1500	(8+9)-V-4	2193	4.31	32.00	7.4	1.04	20.00	19	V	7.4
1500	(8+9)-I-3	2952	5.80	32.00	5.5	1.40	20.00	14	V	5.5
Verifiche nella direzione secondaria										
0	(8+9)-VIII-4	2123	2.92	32.00	11	0.71	20.00	28	V	11
0	(8+9)-IV-3	-3723	-5.13	32.00	6.2	-1.24	20.00	16	V	6.2
0	(8+9)-I-4	-1882	-2.59	32.00	12	-0.63	20.00	32	V	12
0	(8+9)-IV-2	3769	5.19	32.00	6.2	1.26	20.00	16	V	6.2
0	(8+9)-V-2	3604	4.96	32.00	6.4	1.20	20.00	17	V	6.4
0	(8+9)-VII-2	3466	4.77	32.00	6.7	1.16	20.00	17	V	6.7
0	(8+9)-II-2	4231	5.83	32.00	5.5	1.41	20.00	14	V	5.5
0	(8+9)-VI-4	2585	3.56	32.00	9.0	0.86	20.00	23	V	9.0
0	(8+9)-II-3	-4185	-5.76	32.00	5.6	-1.39	20.00	14	V	5.6
0	(8+9)-I-1	1928	2.66	32.00	12	0.64	20.00	31	V	12
0	(8+9)-V-1	1603	2.21	32.00	14	0.53	20.00	37	V	14
0	(8+9)-I-3	-3883	-5.35	32.00	6.0	-1.29	20.00	15	V	6.0
0	(8+9)-III-1	2066	2.85	32.00	11	0.69	20.00	29	V	11
0	(8+9)-I-2	3929	5.41	32.00	5.9	1.31	20.00	15	V	5.9
0	(8+9)-VIII-2	3672	5.06	32.00	6.3	1.22	20.00	16	V	6.3
0	(8+9)-VI-2	4133	5.69	32.00	5.6	1.38	20.00	15	V	5.6
0	(8+9)-III-2	3791	5.22	32.00	6.1	1.26	20.00	16	V	6.1
0	(8+9)-III-3	-3745	-5.16	32.00	6.2	-1.25	20.00	16	V	6.2
0	(8+9)-III-4	-2020	-2.78	32.00	11	-0.67	20.00	30	V	11
0	(8+9)-VII-1	1741	2.40	32.00	13	0.58	20.00	34	V	13
526	1	-172	-0.24	19.20	81	-0.06	12.00	>100	V	81
526	2	-293	-0.40	28.80	71	-0.10	18.00	>100	V	71
526	3	-293	-0.40	28.80	71	-0.10	18.00	>100	V	71
526	4	-172	-0.24	25.60	>100	-0.06	16.00	>100	V	>100
526	5	-172	-0.24	25.60	>100	-0.06	16.00	>100	V	>100
526	6	-172	-0.24	25.60	>100	-0.06	16.00	>100	V	>100
526	7	-172	-0.24	25.60	>100	-0.06	16.00	>100	V	>100
526	(8+9)-IV-1	-2281	-3.14	32.00	10	-0.76	20.00	26	V	10
526	(8+9)-II-4	2509	3.46	32.00	9.3	0.84	20.00	24	V	9.3
526	(8+9)-V-4	-1804	-2.48	32.00	13	-0.60	20.00	33	V	13
526	(8+9)-VII-4	-1941	-2.67	32.00	12	-0.65	20.00	31	V	12
526	(8+9)-II-1	-2739	-3.77	32.00	8.5	-0.91	20.00	22	V	8.5
526	(8+9)-VI-1	-2614	-3.60	32.00	8.9	-0.87	20.00	23	V	8.9
526	(8+9)-VII-3	-3648	-5.02	32.00	6.4	-1.22	20.00	16	V	6.4
526	(8+9)-V-3	-3785	-5.21	32.00	6.1	-1.26	20.00	16	V	6.1

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
526	(8+9)-VIII-1	-2156	-2.97	32.00	11	-0.72	20.00	28	V	11
526	(8+9)-IV-4	2051	2.83	32.00	11	0.68	20.00	29	V	11
526	(8+9)-VIII-3	-3764	-5.18	32.00	6.2	-1.25	20.00	16	V	6.2
526	(8+9)-VI-3	-4221	-5.81	32.00	5.5	-1.41	20.00	14	V	5.5

Setto 11: origine (1721.5,780.4,263.2), direzione (-0.201275,0.979535,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	1	195	-11	-129	0.31	-0.69	-1.43	79.20	115.20	115.20	45
0	2	284	-23	-201	0.45	-1.40	-2.23	118.80	172.80	172.80	40
0	3	284	-23	-201	0.45	-1.40	-2.23	118.80	172.80	172.80	40
0	4	195	-11	-129	0.31	-0.69	-1.43	105.60	153.60	153.60	60
0	5	195	-11	-129	0.31	-0.69	-1.43	105.60	153.60	153.60	60
0	6	195	-11	-129	0.31	-0.69	-1.43	105.60	153.60	153.60	60
0	7	195	-11	-129	0.31	-0.69	-1.43	105.60	153.60	153.60	60
1200	(8+9)-VIII-4	-2456	-622	1974	-3.08	-29.30	13.50	132.00	192.00	192.00	4.5
1200	(8+9)-IV-1	2946	653	-2199	3.69	30.72	-15.04	132.00	192.00	192.00	3.8
1200	(8+9)-V-1	-1873	560	1514	-2.35	26.36	10.36	132.00	192.00	192.00	5.2
1200	(8+9)-I-2	-3048	769	2694	-3.82	36.19	18.43	132.00	192.00	192.00	3.5
1200	(8+9)-V-2	-4196	668	3417	-5.26	31.43	23.38	132.00	192.00	192.00	3.5
1200	(8+9)-I-4	871	-661	-799	1.09	-31.13	-5.47	132.00	192.00	192.00	5.0
1200	(8+9)-V-3	4342	-668	-3425	5.44	-31.43	-23.43	132.00	192.00	192.00	3.1
1200	(8+9)-II-2	-4387	394	3692	-5.50	18.54	25.26	132.00	192.00	192.00	4.4
1200	(8+9)-V-4	2019	-560	-1522	2.53	-26.37	-10.41	132.00	192.00	192.00	4.7
1200	(8+9)-II-4	-3211	-35	2644	-4.02	-1.66	18.09	132.00	192.00	192.00	9.7
1200	(8+9)-VI-1	3012	5	-2435	3.78	0.22	-16.66	132.00	192.00	192.00	8.6
1200	(8+9)-III-2	-2925	584	2558	-3.67	27.47	17.50	132.00	192.00	192.00	4.3
1200	(8+9)-VI-2	-4731	363	3909	-5.93	17.11	26.74	132.00	192.00	192.00	4.4
1200	(8+9)-III-4	994	-847	-935	1.25	-39.85	-6.40	132.00	192.00	192.00	4.0
1200	(8+9)-VI-3	4877	-364	-3917	6.11	-17.12	-26.79	132.00	192.00	192.00	3.6
1200	(8+9)-IV-2	-3976	-224	3239	-4.98	-10.53	22.16	132.00	192.00	192.00	5.9
1200	(8+9)-VI-4	-2867	-5	2427	-3.59	-0.23	16.60	132.00	192.00	192.00	11
1200	(8+9)-IV-4	-2800	-653	2191	-3.51	-30.72	14.99	132.00	192.00	192.00	4.2
1200	(8+9)-VII-1	-1997	745	1650	-2.50	35.08	11.29	132.00	192.00	192.00	4.1
1200	(8+9)-II-1	3357	35	-2652	4.21	1.65	-18.14	132.00	192.00	192.00	7.4
1200	(8+9)-VII-2	-4073	482	3281	-5.10	22.71	22.45	132.00	192.00	192.00	4.2
1200	(8+9)-III-1	-849	846	927	-1.06	39.84	6.34	132.00	192.00	192.00	4.2
1200	(8+9)-VII-3	4219	-482	-3289	5.29	-22.71	-22.50	132.00	192.00	192.00	3.6
1200	(8+9)-I-1	-725	661	791	-0.91	31.12	5.41	132.00	192.00	192.00	5.3
1200	(8+9)-VII-4	2142	-745	-1658	2.68	-35.09	-11.34	132.00	192.00	192.00	3.8
1200	(8+9)-III-3	3070	-584	-2567	3.85	-27.48	-17.56	132.00	192.00	192.00	3.8
1200	(8+9)-IV-3	4121	224	-3247	5.16	10.52	-22.21	132.00	192.00	192.00	4.8
1200	(8+9)-II-3	4533	-394	-3700	5.68	-18.54	-25.31	132.00	192.00	192.00	3.7
1200	(8+9)-VIII-1	2601	622	-1982	3.26	29.29	-13.56	132.00	192.00	192.00	4.0
1200	(8+9)-VIII-2	-4320	-254	3455	-5.41	-11.96	23.64	132.00	192.00	192.00	5.4
1200	(8+9)-VIII-3	4466	254	-3464	5.60	11.95	-23.69	132.00	192.00	192.00	4.4
1200	(8+9)-I-3	3194	-769	-2703	4.00	-36.20	-18.49	132.00	192.00	192.00	3.2
Verifiche nella direzione secondaria											
0	(8+9)-VIII-4	-1082	50	3218	-1.86	4.97	27.70	132.00	192.00	192.00	5.9
0	(8+9)-VII-2	-1504	-85	5711	-2.59	-8.36	49.16	132.00	192.00	192.00	3.3
0	(8+9)-III-3	-642	113	-4619	-1.11	11.18	-39.77	132.00	192.00	192.00	3.8
0	(8+9)-IV-2	-1296	-13	5488	-2.23	-1.28	47.25	132.00	192.00	192.00	4.0
0	(8+9)-III-4	-790	127	-1857	-1.36	12.49	-15.99	132.00	192.00	192.00	6.7
0	(8+9)-VIII-2	-1357	-5	5856	-2.34	-0.47	50.41	132.00	192.00	192.00	3.8
0	(8+9)-IV-1	-803	-57	-3720	-1.38	-5.66	-32.02	132.00	192.00	192.00	5.1
0	(8+9)-VII-4	-590	99	-3082	-1.01	9.80	-26.53	132.00	192.00	192.00	5.3
0	(8+9)-I-1	-1163	-122	1467	-2.00	-12.07	12.63	132.00	192.00	192.00	7.8
0	(8+9)-IV-3	-649	14	-5622	-1.12	1.41	-48.40	132.00	192.00	192.00	3.9
0	(8+9)-I-3	-650	117	-4875	-1.12	11.48	-41.97	132.00	192.00	192.00	3.6
0	(8+9)-IV-4	-1143	59	3586	-1.97	5.78	30.87	132.00	192.00	192.00	5.2
0	(8+9)-II-1	-827	-47	-4571	-1.42	-4.65	-39.36	132.00	192.00	192.00	4.4
0	(8+9)-V-1	-1363	-95	2693	-2.35	-9.37	23.18	132.00	192.00	192.00	5.9

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-II-3	-673	25	-6474	-1.16	2.41	-55.74	132.00	192.00	192.00	3.3
0	(8+9)-V-2	-1497	-88	5966	-2.58	-8.66	51.36	132.00	192.00	192.00	3.2
0	(8+9)-III-1	-1155	-126	1723	-1.99	-12.37	14.83	132.00	192.00	192.00	7.1
0	(8+9)-V-3	-449	89	-6100	-0.77	8.79	-52.51	132.00	192.00	192.00	3.1
0	(8+9)-VIII-3	-589	6	-5990	-1.01	0.60	-51.57	132.00	192.00	192.00	3.7
0	(8+9)-V-4	-582	96	-2827	-1.00	9.49	-24.33	132.00	192.00	192.00	5.7
0	(8+9)-VII-3	-442	86	-5844	-0.76	8.48	-50.31	132.00	192.00	192.00	3.3
0	(8+9)-VI-1	-887	-39	-4204	-1.53	-3.84	-36.19	132.00	192.00	192.00	4.8
0	(8+9)-I-4	-783	124	-1601	-1.35	12.19	-13.79	132.00	192.00	192.00	7.4
0	(8+9)-VI-2	-1333	-15	6708	-2.29	-1.48	57.75	132.00	192.00	192.00	3.2
0	(8+9)-II-4	-1119	48	4438	-1.93	4.77	38.20	132.00	192.00	192.00	4.5
0	(8+9)-VIII-1	-864	-49	-3352	-1.49	-4.85	-28.86	132.00	192.00	192.00	5.7
0	(8+9)-I-2	-1296	-115	4741	-2.23	-11.36	40.81	132.00	192.00	192.00	3.7
0	(8+9)-II-2	-1273	-23	6340	-2.19	-2.29	54.58	132.00	192.00	192.00	3.4
0	(8+9)-III-2	-1303	-112	4485	-2.24	-11.06	38.61	132.00	192.00	192.00	3.9
0	(8+9)-VI-3	-613	16	-6842	-1.06	1.61	-58.90	132.00	192.00	192.00	3.2
0	(8+9)-VI-4	-1058	40	4070	-1.82	3.96	35.04	132.00	192.00	192.00	4.9
0	(8+9)-VII-1	-1356	-98	2948	-2.34	-9.67	25.38	132.00	192.00	192.00	5.5
550	1	-1249	0	129	-2.15	0.03	1.11	79.20	115.20	115.20	98
550	2	-2123	1	218	-3.66	0.12	1.87	118.80	172.80	172.80	84
550	3	-2123	1	218	-3.66	0.12	1.87	118.80	172.80	172.80	84
550	4	-1249	0	129	-2.15	0.03	1.11	105.60	153.60	153.60	>100
550	5	-1249	0	129	-2.15	0.03	1.11	105.60	153.60	153.60	>100
550	6	-1249	0	129	-2.15	0.03	1.11	105.60	153.60	153.60	>100
550	7	-1249	0	129	-2.15	0.03	1.11	105.60	153.60	153.60	>100

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
0	1	8	0.01	3.84	Si	>100
0	2	16	0.02	5.76	Si	>100
0	3	16	0.02	5.76	Si	>100
0	4	8	0.01	5.12	Si	>100
0	5	8	0.01	5.12	Si	>100
0	6	8	0.01	5.12	Si	>100
0	7	8	0.01	5.12	Si	>100
0	(8+9)-V-1	442	0.51	6.40	Si	12
0	(8+9)-VI-1	218	0.25	6.40	Si	25
0	(8+9)-I-2	316	0.37	6.40	Si	17
0	(8+9)-I-3	-305	0.35	6.40	Si	18
0	(8+9)-VII-2	398	0.46	6.40	Si	14
0	(8+9)-I-4	-359	0.42	6.40	Si	15
0	(8+9)-VII-1	432	0.50	6.40	Si	13
0	(8+9)-VII-4	-421	0.49	6.40	Si	13
0	(8+9)-VI-4	-207	0.24	6.40	Si	27
0	(8+9)-II-4	-186	0.22	6.40	Si	30
0	(8+9)-III-2	326	0.38	6.40	Si	17
0	(8+9)-I-1	370	0.43	6.40	Si	15
0	(8+9)-III-4	-349	0.40	6.40	Si	16
0	(8+9)-VII-3	-387	0.45	6.40	Si	14
0	(8+9)-III-1	360	0.42	6.40	Si	15
0	(8+9)-III-3	-315	0.37	6.40	Si	18
0	(8+9)-II-1	197	0.23	6.40	Si	28
0	(8+9)-V-2	388	0.45	6.40	Si	14
0	(8+9)-V-3	-377	0.44	6.40	Si	15
0	(8+9)-V-4	-431	0.50	6.40	Si	13
600	(8+9)-VI-2	82	0.08	6.40	Si	77
600	(8+9)-IV-4	-223	0.23	6.40	Si	28
600	(8+9)-VI-3	-71	0.07	6.40	Si	89
600	(8+9)-VIII-4	-255	0.26	6.40	Si	25
600	(8+9)-VIII-1	266	0.27	6.40	Si	24
600	(8+9)-IV-1	234	0.24	6.40	Si	27
1200	(8+9)-VIII-3	-89	0.08	6.40	Si	79

X	Comb.	Ty	τ_d	fvd	RS	Cs
1200	(8+9)-II-2	-74	0.07	6.40	Si	95
1200	(8+9)-II-3	85	0.08	6.40	Si	83
1200	(8+9)-VIII-2	101	0.09	6.40	Si	70
1200	(8+9)-IV-2	80	0.07	6.40	Si	88
1200	(8+9)-IV-3	-68	0.06	6.40	Si	>100
Verifiche nella direzione secondaria						
0	(8+9)-I-4	25	0.04	6.40	Si	>100
0	(8+9)-VII-4	78	0.12	6.40	Si	52
0	(8+9)-VII-1	-79	0.12	6.40	Si	51
0	(8+9)-V-3	71	0.11	6.40	Si	56
0	(8+9)-V-2	-72	0.11	6.40	Si	56
0	(8+9)-III-3	18	0.03	6.40	Si	>100
0	(8+9)-III-2	-19	0.03	6.40	Si	>100
550	1	-7	0.01	3.84	Si	>100
550	2	-12	0.02	5.76	Si	>100
550	3	-12	0.02	5.76	Si	>100
550	4	-7	0.01	5.12	Si	>100
550	5	-7	0.01	5.12	Si	>100
550	6	-7	0.01	5.12	Si	>100
550	7	-7	0.01	5.12	Si	>100
550	(8+9)-VIII-4	155	0.25	6.40	Si	26
550	(8+9)-V-1	95	0.15	6.40	Si	42
550	(8+9)-I-2	-78	0.12	6.40	Si	52
550	(8+9)-VI-1	95	0.15	6.40	Si	43
550	(8+9)-III-1	-109	0.17	6.40	Si	37
550	(8+9)-VI-2	-58	0.09	6.40	Si	69
550	(8+9)-III-4	99	0.16	6.40	Si	41
550	(8+9)-VI-3	48	0.08	6.40	Si	84
550	(8+9)-IV-2	163	0.26	6.40	Si	25
550	(8+9)-VI-4	-105	0.17	6.40	Si	38
550	(8+9)-IV-4	193	0.31	6.40	Si	21
550	(8+9)-I-1	-32	0.05	6.40	Si	>100
550	(8+9)-II-2	-96	0.15	6.40	Si	42
550	(8+9)-VII-2	127	0.20	6.40	Si	32
550	(8+9)-V-4	-105	0.17	6.40	Si	38
550	(8+9)-VII-3	-137	0.22	6.40	Si	29
550	(8+9)-IV-1	-203	0.32	6.40	Si	20
550	(8+9)-I-3	67	0.11	6.40	Si	60
550	(8+9)-II-4	-67	0.11	6.40	Si	60
550	(8+9)-IV-3	-173	0.28	6.40	Si	23
550	(8+9)-II-1	57	0.09	6.40	Si	71
550	(8+9)-VIII-1	-165	0.26	6.40	Si	24
550	(8+9)-VIII-2	201	0.32	6.40	Si	20
550	(8+9)-VIII-3	-211	0.34	6.40	Si	19
550	(8+9)-II-3	86	0.14	6.40	Si	47

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	(8+9)-V-1	-1766	-4.23	32.00	7.6	-1.02	20.00	20	V	7.6
0	(8+9)-II-2	-4039	-9.66	32.00	3.3	-2.34	20.00	8.6	V	3.3
0	(8+9)-III-2	-2845	-6.81	32.00	4.7	-1.65	20.00	12	V	4.7
0	(8+9)-VIII-4	-2232	-5.34	32.00	6.0	-1.29	20.00	15	V	6.0
0	(8+9)-VII-1	-1920	-4.60	32.00	7.0	-1.11	20.00	18	V	7.0
0	(8+9)-VIII-2	-3743	-8.96	32.00	3.6	-2.17	20.00	9.2	V	3.6
0	(8+9)-V-2	-3730	-8.93	32.00	3.6	-2.16	20.00	9.3	V	3.6
0	(8+9)-VII-2	-3575	-8.56	32.00	3.7	-2.07	20.00	9.7	V	3.7
0	(8+9)-VI-2	-4258	-10.19	32.00	3.1	-2.47	20.00	8.1	V	3.1
0	(8+9)-VI-4	-2747	-6.57	32.00	4.9	-1.59	20.00	13	V	4.9
0	(8+9)-IV-2	-3524	-8.43	32.00	3.8	-2.04	20.00	9.8	V	3.8
0	(8+9)-I-1	-1036	-2.48	32.00	13	-0.60	20.00	33	V	13
0	(8+9)-IV-4	-2451	-5.87	32.00	5.5	-1.42	20.00	14	V	5.5
0	(8+9)-I-2	-2999	-7.18	32.00	4.5	-1.74	20.00	12	V	4.5

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
0	(8+9)-II-4	-2966	-7.10	32.00	4.5	-1.72	20.00	12	V	4.5
0	(8+9)-III-1	-1190	-2.85	32.00	11	-0.69	20.00	29	V	11
1200	1	548	1.03	19.20	19	0.25	12.00	48	V	19
1200	2	912	1.71	28.80	17	0.41	18.00	43	V	17
1200	3	912	1.71	28.80	17	0.41	18.00	43	V	17
1200	4	548	1.03	25.60	25	0.25	16.00	64	V	25
1200	5	548	1.03	25.60	25	0.25	16.00	64	V	25
1200	6	548	1.03	25.60	25	0.25	16.00	64	V	25
1200	7	548	1.03	25.60	25	0.25	16.00	64	V	25
1200	(8+9)-VI-1	3509	6.60	32.00	4.9	1.60	20.00	13	V	4.9
1200	(8+9)-I-3	3875	7.28	32.00	4.4	1.76	20.00	11	V	4.4
1200	(8+9)-II-3	5136	9.66	32.00	3.3	2.34	20.00	8.6	V	3.3
1200	(8+9)-IV-3	4493	8.44	32.00	3.8	2.04	20.00	9.8	V	3.8
1200	(8+9)-II-1	3770	7.09	32.00	4.5	1.71	20.00	12	V	4.5
1200	(8+9)-V-4	2297	4.32	32.00	7.4	1.05	20.00	19	V	7.4
1200	(8+9)-VII-3	4552	8.56	32.00	3.7	2.07	20.00	9.7	V	3.7
1200	(8+9)-III-4	1620	3.05	32.00	11	0.74	20.00	27	V	11
1200	(8+9)-VII-4	2490	4.68	32.00	6.8	1.13	20.00	18	V	6.8
1200	(8+9)-IV-1	3126	5.88	32.00	5.4	1.42	20.00	14	V	5.4
1200	(8+9)-VI-3	5397	10.15	32.00	3.2	2.46	20.00	8.1	V	3.2
1200	(8+9)-V-3	4745	8.92	32.00	3.6	2.16	20.00	9.3	V	3.6
1200	(8+9)-VIII-1	2865	5.39	32.00	5.9	1.30	20.00	15	V	5.9
1200	(8+9)-I-4	1427	2.68	32.00	12	0.65	20.00	31	V	12
1200	(8+9)-VIII-3	4754	8.94	32.00	3.6	2.16	20.00	9.2	V	3.6
1200	(8+9)-III-3	3682	6.92	32.00	4.6	1.67	20.00	12	V	4.6
Verifiche nella direzione secondaria										
0	(8+9)-III-1	1621	2.79	32.00	11	0.68	20.00	30	V	11
0	(8+9)-I-2	4287	7.38	32.00	4.3	1.79	20.00	11	V	4.3
0	(8+9)-VII-4	-2544	-4.38	32.00	7.3	-1.06	20.00	19	V	7.3
0	(8+9)-I-3	-4216	-7.26	32.00	4.4	-1.76	20.00	11	V	4.4
0	(8+9)-V-4	-2321	-4.00	32.00	8.0	-0.97	20.00	21	V	8.0
0	(8+9)-I-4	-1326	-2.28	32.00	14	-0.55	20.00	36	V	14
0	(8+9)-IV-3	-4879	-8.40	32.00	3.8	-2.03	20.00	9.8	V	3.8
0	(8+9)-I-1	1398	2.41	32.00	13	0.58	20.00	34	V	13
0	(8+9)-VII-3	-4988	-8.59	32.00	3.7	-2.08	20.00	9.6	V	3.7
0	(8+9)-V-3	-5211	-8.97	32.00	3.6	-2.17	20.00	9.2	V	3.6
0	(8+9)-III-4	-1549	-2.67	32.00	12	-0.65	20.00	31	V	12
0	(8+9)-III-3	-3993	-6.88	32.00	4.7	-1.66	20.00	12	V	4.7
0	(8+9)-III-2	4064	7.00	32.00	4.6	1.69	20.00	12	V	4.6
0	(8+9)-II-3	-5622	-9.68	32.00	3.3	-2.34	20.00	8.5	V	3.3
550	1	123	0.21	19.20	91	0.05	12.00	>100	V	91
550	2	219	0.38	28.80	76	0.09	18.00	>100	V	76
550	3	219	0.38	28.80	76	0.09	18.00	>100	V	76
550	4	123	0.21	25.60	>100	0.05	16.00	>100	V	>100
550	5	123	0.21	25.60	>100	0.05	16.00	>100	V	>100
550	6	123	0.21	25.60	>100	0.05	16.00	>100	V	>100
550	7	123	0.21	25.60	>100	0.05	16.00	>100	V	>100
550	(8+9)-VIII-4	3120	5.37	32.00	6.0	1.30	20.00	15	V	6.0
550	(8+9)-VI-1	-3666	-6.31	32.00	5.1	-1.53	20.00	13	V	5.1
550	(8+9)-II-4	4186	7.21	32.00	4.4	1.74	20.00	11	V	4.4
550	(8+9)-VII-1	2630	4.53	32.00	7.1	1.10	20.00	18	V	7.1
550	(8+9)-V-1	2414	4.16	32.00	7.7	1.01	20.00	20	V	7.7
550	(8+9)-VII-2	5133	8.84	32.00	3.6	2.14	20.00	9.4	V	3.6
550	(8+9)-IV-4	3464	5.96	32.00	5.4	1.44	20.00	14	V	5.4
550	(8+9)-II-1	-4010	-6.90	32.00	4.6	-1.67	20.00	12	V	4.6
550	(8+9)-IV-1	-3289	-5.66	32.00	5.7	-1.37	20.00	15	V	5.7
550	(8+9)-II-2	5774	9.94	32.00	3.2	2.41	20.00	8.3	V	3.2
550	(8+9)-V-2	5349	9.21	32.00	3.5	2.23	20.00	9.0	V	3.5
550	(8+9)-IV-2	5052	8.70	32.00	3.7	2.11	20.00	9.5	V	3.7
550	(8+9)-VI-2	6118	10.53	32.00	3.0	2.55	20.00	7.8	V	3.0
550	(8+9)-VI-4	3841	6.61	32.00	4.8	1.60	20.00	12	V	4.8
550	(8+9)-VIII-1	-2945	-5.07	32.00	6.3	-1.23	20.00	16	V	6.3
550	(8+9)-VIII-2	5397	9.29	32.00	3.4	2.25	20.00	8.9	V	3.4
550	(8+9)-VIII-3	-5221	-8.99	32.00	3.6	-2.18	20.00	9.2	V	3.6

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
550	(8+9)-VI-3	-5942	-10.23	32.00	3.1	-2.48	20.00	8.1	V	3.1

Verifiche a instabilità

Setto(X)	Comb.	k _{critc}	k _{critm}	λ_{relc}	λ_{relm}	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
(cm)						kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	
6(60.0)	(8+9)-V-2	1.00	--	0.22	--	-5.12	-15.09	8.36	132.00	192.00	192.00	6.7
7(40.0)	(8+9)-V-3	--	--	--	--	2.78	-9.68	-7.26	132.00	192.00	192.00	9.2
8(37.2)	(8+9)-V-3	--	--	--	--	2.38	5.15	-6.59	132.00	192.00	192.00	13
9(150.0)	(8+9)-VI-3	--	--	--	--	5.40	0.81	-17.96	132.00	192.00	192.00	7.2
10(0.0)	(8+9)-V-3	--	--	--	--	17.29	-38.63	11.63	132.00	192.00	192.00	2.5
11(120.0)	(8+9)-V-3	--	--	--	--	5.44	-31.43	-23.43	132.00	192.00	192.00	3.1

Parete Xlam 7 - Nodi: [12-13-101-102] - **Crit.Prog.** Criterio di verifica XLAM 0 - **Verificato:**
[Cs=4.984,Comb=(8+9)-IV-3]

Geometria setti

Setto	Crit.	X	L	S	X90	L90	S90
		mm	cm	cm	mm	cm	cm
12	Criterio di verifica XLAM 0	0	237.0	12.1	0	348.6	12.1
		1743	268.0	12.1	1495	348.6	12.1
		3486	299.0	12.1	--	--	--

Setto 12: origine (1236.0,189.0,118.5), direzione (-0.610958,0.791663,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	
0	1	33	2	52	0.02	0.04	0.08	79.20	115.20	115.20	>100
0	4	33	2	52	0.02	0.04	0.08	105.60	153.60	153.60	>100
0	5	33	2	52	0.02	0.04	0.08	105.60	153.60	153.60	>100
0	6	33	2	52	0.02	0.04	0.08	105.60	153.60	153.60	>100
0	7	33	2	52	0.02	0.04	0.08	105.60	153.60	153.60	>100
0	(8+9)-IV-1	-568	-213	1660	-0.33	-4.65	2.44	132.00	192.00	192.00	27
0	(8+9)-IV-4	619	216	-1574	0.36	4.72	-2.32	132.00	192.00	192.00	25
0	(8+9)-II-4	552	220	-1370	0.32	4.79	-2.02	132.00	192.00	192.00	26
0	(8+9)-II-1	-501	-216	1457	-0.29	-4.72	2.14	132.00	192.00	192.00	28
1743	(8+9)-III-4	-804	-418	-293	-0.41	-8.07	-0.34	132.00	192.00	192.00	23
1743	(8+9)-III-1	811	419	392	0.42	8.09	0.45	132.00	192.00	192.00	21
3486	2	-416	-4	239	-0.19	-0.06	0.22	118.80	172.80	172.80	>100
3486	3	-416	-4	239	-0.19	-0.06	0.22	118.80	172.80	172.80	>100
3486	(8+9)-VIII-4	-209	-77	5852	-0.10	-1.33	5.41	132.00	192.00	192.00	28
3486	(8+9)-V-4	80	102	-3315	0.04	1.76	-3.06	132.00	192.00	192.00	39
3486	(8+9)-II-3	24	220	-8131	0.01	3.82	-7.52	132.00	192.00	192.00	17
3486	(8+9)-VI-1	-60	69	-4998	-0.03	1.20	-4.62	132.00	192.00	192.00	33
3486	(8+9)-I-4	-138	334	-2968	-0.06	5.78	-2.74	132.00	192.00	192.00	23
3486	(8+9)-VI-2	-345	-153	8383	-0.16	-2.64	7.75	132.00	192.00	192.00	18
3486	(8+9)-III-3	-49	402	-7195	-0.02	6.96	-6.65	132.00	192.00	192.00	14
3486	(8+9)-VI-3	90	151	-8235	0.04	2.61	-7.61	132.00	192.00	192.00	19
3486	(8+9)-I-2	-202	-402	7131	-0.09	-6.96	6.59	132.00	192.00	192.00	14
3486	(8+9)-VI-4	-195	-71	5146	-0.09	-1.23	4.76	132.00	192.00	192.00	32
3486	(8+9)-IV-3	38	226	-8838	0.02	3.92	-8.17	132.00	192.00	192.00	16
3486	(8+9)-VII-1	-331	-102	3251	-0.15	-1.76	3.01	132.00	192.00	192.00	40
3486	(8+9)-V-1	-335	-103	3463	-0.15	-1.79	3.20	132.00	192.00	192.00	38
3486	(8+9)-VII-2	-425	-172	7689	-0.20	-2.97	7.11	132.00	192.00	192.00	19
3486	(8+9)-V-3	165	168	-7329	0.08	2.91	-6.78	132.00	192.00	192.00	20
3486	(8+9)-VII-3	169	170	-7541	0.08	2.95	-6.97	132.00	192.00	192.00	19

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
3486	(8+9)-III-2	-207	-404	7343	-0.10	-6.99	6.79	132.00	192.00	192.00	14
3486	(8+9)-VII-4	76	100	-3103	0.03	1.73	-2.87	132.00	192.00	192.00	41
3486	(8+9)-V-2	-420	-170	7477	-0.19	-2.94	6.91	132.00	192.00	192.00	19
3486	(8+9)-II-2	-280	-222	8279	-0.13	-3.84	7.65	132.00	192.00	192.00	17
3486	(8+9)-I-3	-53	400	-6983	-0.02	6.93	-6.46	132.00	192.00	192.00	14
3486	(8+9)-I-1	-117	-335	3116	-0.05	-5.81	2.88	132.00	192.00	192.00	22
3486	(8+9)-VIII-1	-46	75	-5704	-0.02	1.30	-5.27	132.00	192.00	192.00	29
3486	(8+9)-VIII-2	-359	-158	9089	-0.17	-2.74	8.40	132.00	192.00	192.00	17
3486	(8+9)-VIII-3	104	157	-8942	0.05	2.71	-8.27	132.00	192.00	192.00	17
3486	(8+9)-IV-2	-293	-228	8986	-0.14	-3.95	8.31	132.00	192.00	192.00	16
Verifiche nella direzione secondaria											
0	1	-1872	-2	-181	-1.11	-0.08	-0.19	79.20	115.20	115.20	>100
0	2	-2887	5	-242	-1.71	0.15	-0.25	118.80	172.80	172.80	>100
0	3	-2887	5	-242	-1.71	0.15	-0.25	118.80	172.80	172.80	>100
0	4	-1872	-2	-181	-1.11	-0.08	-0.19	105.60	153.60	153.60	>100
0	5	-1872	-2	-181	-1.11	-0.08	-0.19	105.60	153.60	153.60	>100
0	6	-1872	-2	-181	-1.11	-0.08	-0.19	105.60	153.60	153.60	>100
0	7	-1872	-2	-181	-1.11	-0.08	-0.19	105.60	153.60	153.60	>100
0	(8+9)-VIII-4	-6632	54	2250	-3.93	1.82	2.29	132.00	192.00	192.00	46
0	(8+9)-IV-2	-8837	84	4863	-5.24	2.83	4.96	132.00	192.00	192.00	24
0	(8+9)-V-1	-2588	7	4299	-1.53	0.25	4.39	132.00	192.00	192.00	41
0	(8+9)-I-2	-7391	86	4142	-4.38	2.92	4.23	132.00	192.00	192.00	26
0	(8+9)-V-2	-6156	48	6173	-3.65	1.62	6.30	132.00	192.00	192.00	24
0	(8+9)-I-4	1193	-52	-2539	0.71	-1.75	-2.59	132.00	192.00	192.00	36
0	(8+9)-V-3	3527	-54	-6445	2.09	-1.82	-6.57	132.00	192.00	192.00	17
0	(8+9)-II-2	-8549	85	3990	-5.07	2.89	4.07	132.00	192.00	192.00	27
0	(8+9)-V-4	-41	-13	-4571	-0.02	-0.45	-4.66	132.00	192.00	192.00	38
0	(8+9)-II-4	-5974	44	1985	-3.54	1.49	2.03	132.00	192.00	192.00	54
0	(8+9)-VI-1	3716	-61	-1647	2.20	-2.08	-1.68	132.00	192.00	192.00	28
0	(8+9)-III-2	-7477	86	4404	-4.43	2.90	4.49	132.00	192.00	192.00	26
0	(8+9)-VI-2	-8179	74	4599	-4.85	2.50	4.69	132.00	192.00	192.00	26
0	(8+9)-III-4	1107	-52	-2277	0.66	-1.76	-2.32	132.00	192.00	192.00	38
0	(8+9)-VI-3	5550	-80	-4871	3.29	-2.70	-4.97	132.00	192.00	192.00	15
0	(8+9)-I-1	-3822	46	2268	-2.27	1.55	2.31	132.00	192.00	192.00	49
0	(8+9)-VI-4	-6345	55	1376	-3.76	1.88	1.40	132.00	192.00	192.00	57
0	(8+9)-IV-4	-6262	42	2859	-3.71	1.43	2.92	132.00	192.00	192.00	43
0	(8+9)-VII-1	-2501	8	4037	-1.48	0.26	4.12	132.00	192.00	192.00	44
0	(8+9)-II-1	3345	-50	-2257	1.98	-1.69	-2.30	132.00	192.00	192.00	28
0	(8+9)-VII-2	-6242	47	6435	-3.70	1.60	6.56	132.00	192.00	192.00	23
0	(8+9)-III-1	-3736	46	2006	-2.21	1.57	2.05	132.00	192.00	192.00	53
0	(8+9)-VII-3	3613	-53	-6707	2.14	-1.80	-6.84	132.00	192.00	192.00	16
0	(8+9)-IV-1	3633	-48	-3131	2.15	-1.63	-3.19	132.00	192.00	192.00	24
0	(8+9)-VII-4	-128	-14	-4309	-0.08	-0.46	-4.40	132.00	192.00	192.00	40
0	(8+9)-III-3	4848	-92	-4675	2.87	-3.10	-4.77	132.00	192.00	192.00	16
0	(8+9)-IV-3	6208	-89	-5135	3.68	-3.03	-5.24	132.00	192.00	192.00	14
0	(8+9)-II-3	5921	-91	-4261	3.51	-3.09	-4.35	132.00	192.00	192.00	15
0	(8+9)-VIII-1	4004	-60	-2521	2.37	-2.02	-2.57	132.00	192.00	192.00	24
0	(8+9)-VIII-2	-8467	72	5473	-5.02	2.44	5.58	132.00	192.00	192.00	24
0	(8+9)-VIII-3	5838	-78	-5744	3.46	-2.64	-5.86	132.00	192.00	192.00	14
0	(8+9)-I-3	4762	-92	-4413	2.82	-3.12	-4.50	132.00	192.00	192.00	16

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
0	(8+9)-V-1	33	0.01	6.40	Si	>100
0	(8+9)-VII-4	-36	0.02	6.40	Si	>100
0	(8+9)-I-2	-55	0.02	6.40	Si	>100
0	(8+9)-VII-1	30	0.01	6.40	Si	>100
0	(8+9)-III-3	47	0.02	6.40	Si	>100
0	(8+9)-III-2	-53	0.02	6.40	Si	>100
0	(8+9)-V-4	-38	0.02	6.40	Si	>100
0	(8+9)-I-1	-43	0.02	6.40	Si	>100
0	(8+9)-I-3	49	0.02	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
1743	(8+9)-II-3	78	0.03	6.40	Si	>100
1743	(8+9)-V-3	71	0.03	6.40	Si	>100
1743	(8+9)-VII-3	65	0.02	6.40	Si	>100
1743	(8+9)-V-2	-70	0.03	6.40	Si	>100
3486	1	-6	0.00	3.84	Si	>100
3486	2	-13	0.00	5.76	Si	>100
3486	3	-13	0.00	5.76	Si	>100
3486	4	-6	0.00	5.12	Si	>100
3486	5	-6	0.00	5.12	Si	>100
3486	6	-6	0.00	5.12	Si	>100
3486	7	-6	0.00	5.12	Si	>100
3486	(8+9)-VIII-4	-105	0.04	6.40	Si	>100
3486	(8+9)-IV-1	117	0.04	6.40	Si	>100
3486	(8+9)-VI-4	-88	0.03	6.40	Si	>100
3486	(8+9)-IV-3	100	0.03	6.40	Si	>100
3486	(8+9)-II-2	-90	0.03	6.40	Si	>100
3486	(8+9)-IV-2	-108	0.04	6.40	Si	>100
3486	(8+9)-VII-2	-73	0.02	6.40	Si	>100
3486	(8+9)-III-1	57	0.02	6.40	Si	>100
3486	(8+9)-II-1	99	0.03	6.40	Si	>100
3486	(8+9)-VI-1	80	0.03	6.40	Si	>100
3486	(8+9)-I-4	-59	0.02	6.40	Si	>100
3486	(8+9)-III-4	-65	0.02	6.40	Si	>100
3486	(8+9)-II-4	-107	0.04	6.40	Si	>100
3486	(8+9)-VI-2	-109	0.04	6.40	Si	>100
3486	(8+9)-IV-4	-124	0.04	6.40	Si	>100
3486	(8+9)-VIII-1	98	0.03	6.40	Si	>100
3486	(8+9)-VIII-2	-126	0.04	6.40	Si	>100
3486	(8+9)-VIII-3	119	0.04	6.40	Si	>100
3486	(8+9)-VI-3	102	0.03	6.40	Si	>100
Verifiche nella direzione secondaria						
0	1	-4	0.00	3.84	Si	>100
0	2	-19	0.01	5.76	Si	>100
0	3	-19	0.01	5.76	Si	>100
0	4	-4	0.00	5.12	Si	>100
0	5	-4	0.00	5.12	Si	>100
0	6	-4	0.00	5.12	Si	>100
0	7	-4	0.00	5.12	Si	>100
0	(8+9)-VIII-4	-88	0.05	6.40	Si	>100
0	(8+9)-IV-2	-105	0.06	6.40	Si	>100
0	(8+9)-V-1	-13	0.01	6.40	Si	>100
0	(8+9)-I-2	-46	0.03	6.40	Si	>100
0	(8+9)-V-2	-68	0.04	6.40	Si	>100
0	(8+9)-V-3	67	0.04	6.40	Si	>100
0	(8+9)-II-2	-99	0.05	6.40	Si	>100
0	(8+9)-VII-2	-70	0.04	6.40	Si	>100
0	(8+9)-I-3	45	0.02	6.40	Si	>100
0	(8+9)-II-4	-88	0.05	6.40	Si	>100
0	(8+9)-II-1	87	0.05	6.40	Si	>100
0	(8+9)-III-2	-48	0.03	6.40	Si	>100
0	(8+9)-II-3	98	0.05	6.40	Si	>100
0	(8+9)-VIII-2	-112	0.06	6.40	Si	>100
0	(8+9)-VIII-1	87	0.05	6.40	Si	>100
0	(8+9)-VI-1	80	0.04	6.40	Si	>100
0	(8+9)-IV-4	-94	0.05	6.40	Si	>100
0	(8+9)-VI-2	-105	0.06	6.40	Si	>100
0	(8+9)-III-3	47	0.03	6.40	Si	>100
0	(8+9)-IV-3	104	0.06	6.40	Si	>100
0	(8+9)-VIII-3	111	0.06	6.40	Si	>100
0	(8+9)-IV-1	93	0.05	6.40	Si	>100
0	(8+9)-VI-3	104	0.06	6.40	Si	>100
0	(8+9)-VI-4	-81	0.04	6.40	Si	>100
0	(8+9)-VII-3	69	0.04	6.40	Si	>100
1495	(8+9)-I-4	-25	0.01	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
1495	(8+9)-VII-1	12	0.01	6.40	Si	>100
1495	(8+9)-VII-4	-13	0.01	6.40	Si	>100
1495	(8+9)-I-1	24	0.01	6.40	Si	>100
1495	(8+9)-III-4	-25	0.01	6.40	Si	>100
1495	(8+9)-III-1	24	0.01	6.40	Si	>100
1495	(8+9)-V-4	-13	0.01	6.40	Si	>100

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
1743	1	228	0.18	19.20	>100	0.04	12.00	>100	V	>100
1743	2	299	0.23	28.80	>100	0.06	18.00	>100	V	>100
1743	3	299	0.23	28.80	>100	0.06	18.00	>100	V	>100
1743	4	228	0.18	25.60	>100	0.04	16.00	>100	V	>100
1743	5	228	0.18	25.60	>100	0.04	16.00	>100	V	>100
1743	6	228	0.18	25.60	>100	0.04	16.00	>100	V	>100
1743	7	228	0.18	25.60	>100	0.04	16.00	>100	V	>100
1743	(8+9)-IV-1	5045	3.89	32.00	8.2	0.94	20.00	21	V	8.2
1743	(8+9)-VIII-1	4997	3.85	32.00	8.3	0.93	20.00	21	V	8.3
1743	(8+9)-VI-1	4366	3.37	32.00	9.5	0.81	20.00	25	V	9.5
1743	(8+9)-IV-4	-4705	-3.63	32.00	8.8	-0.88	20.00	23	V	8.8
1743	(8+9)-II-1	4414	3.40	32.00	9.4	0.82	20.00	24	V	9.4
1743	(8+9)-VIII-4	-4657	-3.59	32.00	8.9	-0.87	20.00	23	V	8.9
3486	(8+9)-IV-3	9292	6.42	32.00	5.0	1.55	20.00	13	V	5.0
3486	(8+9)-VI-2	-8715	-6.02	32.00	5.3	-1.46	20.00	14	V	5.3
3486	(8+9)-II-4	-4647	-3.21	32.00	10.0	-0.78	20.00	26	V	10.0
3486	(8+9)-VI-3	8801	6.08	32.00	5.3	1.47	20.00	14	V	5.3
3486	(8+9)-III-2	-9080	-6.27	32.00	5.1	-1.52	20.00	13	V	5.1
3486	(8+9)-VI-4	-4766	-3.29	32.00	9.7	-0.80	20.00	25	V	9.7
3486	(8+9)-III-4	4873	3.37	32.00	9.5	0.81	20.00	25	V	9.5
3486	(8+9)-VII-1	-4392	-3.04	32.00	11	-0.73	20.00	27	V	11
3486	(8+9)-IV-2	-9205	-6.36	32.00	5.0	-1.54	20.00	13	V	5.0
3486	(8+9)-VII-2	-8685	-6.00	32.00	5.3	-1.45	20.00	14	V	5.3
3486	(8+9)-I-4	4985	3.44	32.00	9.3	0.83	20.00	24	V	9.3
3486	(8+9)-VII-3	8771	6.06	32.00	5.3	1.47	20.00	14	V	5.3
3486	(8+9)-V-2	-8574	-5.92	32.00	5.4	-1.43	20.00	14	V	5.4
3486	(8+9)-VII-4	4478	3.09	32.00	10	0.75	20.00	27	V	10
3486	(8+9)-V-4	4590	3.17	32.00	10	0.77	20.00	26	V	10
3486	(8+9)-I-2	-8969	-6.20	32.00	5.2	-1.50	20.00	13	V	5.2
3486	(8+9)-III-1	-4787	-3.31	32.00	9.7	-0.80	20.00	25	V	9.7
3486	(8+9)-VIII-2	-9087	-6.28	32.00	5.1	-1.52	20.00	13	V	5.1
3486	(8+9)-II-3	8920	6.16	32.00	5.2	1.49	20.00	13	V	5.2
3486	(8+9)-VIII-3	9173	6.34	32.00	5.0	1.53	20.00	13	V	5.0
3486	(8+9)-V-1	-4504	-3.11	32.00	10	-0.75	20.00	27	V	10
3486	(8+9)-I-3	9055	6.26	32.00	5.1	1.51	20.00	13	V	5.1
3486	(8+9)-III-3	9166	6.33	32.00	5.1	1.53	20.00	13	V	5.1
3486	(8+9)-II-2	-8834	-6.10	32.00	5.2	-1.48	20.00	14	V	5.2
3486	(8+9)-V-3	8660	5.98	32.00	5.3	1.45	20.00	14	V	5.3
3486	(8+9)-I-1	-4899	-3.39	32.00	9.5	-0.82	20.00	24	V	9.5
Verifiche nella direzione secondaria										
0	2	109	0.06	28.80	>100	0.02	18.00	>100	V	>100
0	3	109	0.06	28.80	>100	0.02	18.00	>100	V	>100
1495	1	-14	-0.01	19.20	>100	-0.00	12.00	>100	V	>100
1495	4	-14	-0.01	25.60	>100	-0.00	16.00	>100	V	>100
1495	5	-14	-0.01	25.60	>100	-0.00	16.00	>100	V	>100
1495	6	-14	-0.01	25.60	>100	-0.00	16.00	>100	V	>100
1495	7	-14	-0.01	25.60	>100	-0.00	16.00	>100	V	>100
1495	(8+9)-VIII-4	6724	3.98	32.00	8.0	0.96	20.00	21	V	8.0
1495	(8+9)-IV-3	-10558	-6.26	32.00	5.1	-1.51	20.00	13	V	5.1
1495	(8+9)-V-1	4064	2.41	32.00	13	0.58	20.00	34	V	13
1495	(8+9)-I-2	8500	5.04	32.00	6.4	1.22	20.00	16	V	6.4
1495	(8+9)-V-2	8752	5.19	32.00	6.2	1.26	20.00	16	V	6.2
1495	(8+9)-I-4	-3863	-2.29	32.00	14	-0.55	20.00	36	V	14

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
1495	(8+9)-V-3	-8802	-5.22	32.00	6.1	-1.26	20.00	16	V	6.1
1495	(8+9)-II-2	9643	5.72	32.00	5.6	1.38	20.00	14	V	5.6
1495	(8+9)-V-4	-4114	-2.44	32.00	13	-0.59	20.00	34	V	13
1495	(8+9)-II-4	5934	3.52	32.00	9.1	0.85	20.00	23	V	9.1
1495	(8+9)-VI-1	-5909	-3.50	32.00	9.1	-0.85	20.00	24	V	9.1
1495	(8+9)-III-2	8760	5.19	32.00	6.2	1.26	20.00	16	V	6.2
1495	(8+9)-VI-2	9718	5.76	32.00	5.6	1.39	20.00	14	V	5.6
1495	(8+9)-III-4	-3603	-2.14	32.00	15	-0.52	20.00	39	V	15
1495	(8+9)-VI-3	-9769	-5.79	32.00	5.5	-1.40	20.00	14	V	5.5
1495	(8+9)-IV-2	10508	6.23	32.00	5.1	1.51	20.00	13	V	5.1
1495	(8+9)-VI-4	5858	3.47	32.00	9.2	0.84	20.00	24	V	9.2
1495	(8+9)-IV-4	6799	4.03	32.00	7.9	0.98	20.00	21	V	7.9
1495	(8+9)-VII-1	3804	2.25	32.00	14	0.55	20.00	37	V	14
1495	(8+9)-II-1	-5984	-3.55	32.00	9.0	-0.86	20.00	23	V	9.0
1495	(8+9)-VII-2	9011	5.34	32.00	6.0	1.29	20.00	15	V	6.0
1495	(8+9)-III-1	3553	2.11	32.00	15	0.51	20.00	39	V	15
1495	(8+9)-VII-3	-9062	-5.37	32.00	6.0	-1.30	20.00	15	V	6.0
1495	(8+9)-IV-1	-6849	-4.06	32.00	7.9	-0.98	20.00	20	V	7.9
1495	(8+9)-VII-4	-3855	-2.28	32.00	14	-0.55	20.00	36	V	14
1495	(8+9)-III-3	-8810	-5.22	32.00	6.1	-1.26	20.00	16	V	6.1
1495	(8+9)-I-1	3812	2.26	32.00	14	0.55	20.00	37	V	14
1495	(8+9)-II-3	-9693	-5.75	32.00	5.6	-1.39	20.00	14	V	5.6
1495	(8+9)-VIII-1	-6774	-4.01	32.00	8.0	-0.97	20.00	21	V	8.0
1495	(8+9)-VIII-2	10583	6.27	32.00	5.1	1.52	20.00	13	V	5.1
1495	(8+9)-VIII-3	-10634	-6.30	32.00	5.1	-1.53	20.00	13	V	5.1
1495	(8+9)-I-3	-8551	-5.07	32.00	6.3	-1.23	20.00	16	V	6.3

Verifiche a instabilità

Setto(X)	Comb.	k _{critc}	k _{critm}	λ_{relc}	λ_{relm}	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
(cm)						kg/cm ^q	kg/cm ^q	kg/cm ^q	kg/cm ^q	kg/cm ^q	kg/cm ^q	
12(348.6)	(8+9)-III-2	0.55	--	1.26	--	-0.10	-6.99	6.79	132.00	192.00	192.00	14

Parete Xlam 7 - Nodi: [12-13-101-102] - **Crit.Prog.** Criterio di verifica XLAM 0 - **Verificato:**

[Cs=4.984,Comb=(8+9)-IV-3]

Geometria setti

Setto	Crit.	X	L	S	X90	L90	S90
		mm	cm	cm	mm	cm	cm
12	Criterio di verifica XLAM 0	0	237.0	12.1	0	348.6	12.1
		1743	268.0	12.1	1495	348.6	12.1
		3486	299.0	12.1	--	--	--

Setto 12: origine (1236.0,189.0,118.5), direzione (-0.610958,0.791663,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cm ^q	kg/cm ^q	kg/cm ^q	kg/cm ^q	kg/cm ^q	kg/cm ^q	
0	1	33	2	52	0.02	0.04	0.08	79.20	115.20	115.20	>100
0	4	33	2	52	0.02	0.04	0.08	105.60	153.60	153.60	>100
0	5	33	2	52	0.02	0.04	0.08	105.60	153.60	153.60	>100
0	6	33	2	52	0.02	0.04	0.08	105.60	153.60	153.60	>100
0	7	33	2	52	0.02	0.04	0.08	105.60	153.60	153.60	>100
0	(8+9)-IV-1	-568	-213	1660	-0.33	-4.65	2.44	132.00	192.00	192.00	27
0	(8+9)-IV-4	619	216	-1574	0.36	4.72	-2.32	132.00	192.00	192.00	25
0	(8+9)-II-4	552	220	-1370	0.32	4.79	-2.02	132.00	192.00	192.00	26
0	(8+9)-II-1	-501	-216	1457	-0.29	-4.72	2.14	132.00	192.00	192.00	28
1743	(8+9)-III-4	-804	-418	-293	-0.41	-8.07	-0.34	132.00	192.00	192.00	23
1743	(8+9)-III-1	811	419	392	0.42	8.09	0.45	132.00	192.00	192.00	21
3486	2	-416	-4	239	-0.19	-0.06	0.22	118.80	172.80	172.80	>100
3486	3	-416	-4	239	-0.19	-0.06	0.22	118.80	172.80	172.80	>100

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
3486	(8+9)-VIII-4	-209	-77	5852	-0.10	-1.33	5.41	132.00	192.00	192.00	28
3486	(8+9)-V-4	80	102	-3315	0.04	1.76	-3.06	132.00	192.00	192.00	39
3486	(8+9)-II-3	24	220	-8131	0.01	3.82	-7.52	132.00	192.00	192.00	17
3486	(8+9)-VI-1	-60	69	-4998	-0.03	1.20	-4.62	132.00	192.00	192.00	33
3486	(8+9)-I-4	-138	334	-2968	-0.06	5.78	-2.74	132.00	192.00	192.00	23
3486	(8+9)-VI-2	-345	-153	8383	-0.16	-2.64	7.75	132.00	192.00	192.00	18
3486	(8+9)-III-3	-49	402	-7195	-0.02	6.96	-6.65	132.00	192.00	192.00	14
3486	(8+9)-VI-3	90	151	-8235	0.04	2.61	-7.61	132.00	192.00	192.00	19
3486	(8+9)-I-2	-202	-402	7131	-0.09	-6.96	6.59	132.00	192.00	192.00	14
3486	(8+9)-VI-4	-195	-71	5146	-0.09	-1.23	4.76	132.00	192.00	192.00	32
3486	(8+9)-IV-3	38	226	-8838	0.02	3.92	-8.17	132.00	192.00	192.00	16
3486	(8+9)-VII-1	-331	-102	3251	-0.15	-1.76	3.01	132.00	192.00	192.00	40
3486	(8+9)-V-1	-335	-103	3463	-0.15	-1.79	3.20	132.00	192.00	192.00	38
3486	(8+9)-VII-2	-425	-172	7689	-0.20	-2.97	7.11	132.00	192.00	192.00	19
3486	(8+9)-V-3	165	168	-7329	0.08	2.91	-6.78	132.00	192.00	192.00	20
3486	(8+9)-VII-3	169	170	-7541	0.08	2.95	-6.97	132.00	192.00	192.00	19
3486	(8+9)-III-2	-207	-404	7343	-0.10	-6.99	6.79	132.00	192.00	192.00	14
3486	(8+9)-VII-4	76	100	-3103	0.03	1.73	-2.87	132.00	192.00	192.00	41
3486	(8+9)-V-2	-420	-170	7477	-0.19	-2.94	6.91	132.00	192.00	192.00	19
3486	(8+9)-II-2	-280	-222	8279	-0.13	-3.84	7.65	132.00	192.00	192.00	17
3486	(8+9)-I-3	-53	400	-6983	-0.02	6.93	-6.46	132.00	192.00	192.00	14
3486	(8+9)-I-1	-117	-335	3116	-0.05	-5.81	2.88	132.00	192.00	192.00	22
3486	(8+9)-VIII-1	-46	75	-5704	-0.02	1.30	-5.27	132.00	192.00	192.00	29
3486	(8+9)-VIII-2	-359	-158	9089	-0.17	-2.74	8.40	132.00	192.00	192.00	17
3486	(8+9)-VIII-3	104	157	-8942	0.05	2.71	-8.27	132.00	192.00	192.00	17
3486	(8+9)-IV-2	-293	-228	8986	-0.14	-3.95	8.31	132.00	192.00	192.00	16
Verifiche nella direzione secondaria											
0	1	-1872	-2	-181	-1.11	-0.08	-0.19	79.20	115.20	115.20	>100
0	2	-2887	5	-242	-1.71	0.15	-0.25	118.80	172.80	172.80	>100
0	3	-2887	5	-242	-1.71	0.15	-0.25	118.80	172.80	172.80	>100
0	4	-1872	-2	-181	-1.11	-0.08	-0.19	105.60	153.60	153.60	>100
0	5	-1872	-2	-181	-1.11	-0.08	-0.19	105.60	153.60	153.60	>100
0	6	-1872	-2	-181	-1.11	-0.08	-0.19	105.60	153.60	153.60	>100
0	7	-1872	-2	-181	-1.11	-0.08	-0.19	105.60	153.60	153.60	>100
0	(8+9)-VIII-4	-6632	54	2250	-3.93	1.82	2.29	132.00	192.00	192.00	46
0	(8+9)-IV-2	-8837	84	4863	-5.24	2.83	4.96	132.00	192.00	192.00	24
0	(8+9)-V-1	-2588	7	4299	-1.53	0.25	4.39	132.00	192.00	192.00	41
0	(8+9)-I-2	-7391	86	4142	-4.38	2.92	4.23	132.00	192.00	192.00	26
0	(8+9)-V-2	-6156	48	6173	-3.65	1.62	6.30	132.00	192.00	192.00	24
0	(8+9)-I-4	1193	-52	-2539	0.71	-1.75	-2.59	132.00	192.00	192.00	36
0	(8+9)-V-3	3527	-54	-6445	2.09	-1.82	-6.57	132.00	192.00	192.00	17
0	(8+9)-II-2	-8549	85	3990	-5.07	2.89	4.07	132.00	192.00	192.00	27
0	(8+9)-V-4	-41	-13	-4571	-0.02	-0.45	-4.66	132.00	192.00	192.00	38
0	(8+9)-II-4	-5974	44	1985	-3.54	1.49	2.03	132.00	192.00	192.00	54
0	(8+9)-VI-1	3716	-61	-1647	2.20	-2.08	-1.68	132.00	192.00	192.00	28
0	(8+9)-III-2	-7477	86	4404	-4.43	2.90	4.49	132.00	192.00	192.00	26
0	(8+9)-VI-2	-8179	74	4599	-4.85	2.50	4.69	132.00	192.00	192.00	26
0	(8+9)-III-4	1107	-52	-2277	0.66	-1.76	-2.32	132.00	192.00	192.00	38
0	(8+9)-VI-3	5550	-80	-4871	3.29	-2.70	-4.97	132.00	192.00	192.00	15
0	(8+9)-I-1	-3822	46	2268	-2.27	1.55	2.31	132.00	192.00	192.00	49
0	(8+9)-VI-4	-6345	55	1376	-3.76	1.88	1.40	132.00	192.00	192.00	57
0	(8+9)-IV-4	-6262	42	2859	-3.71	1.43	2.92	132.00	192.00	192.00	43
0	(8+9)-VII-1	-2501	8	4037	-1.48	0.26	4.12	132.00	192.00	192.00	44
0	(8+9)-II-1	3345	-50	-2257	1.98	-1.69	-2.30	132.00	192.00	192.00	28
0	(8+9)-VII-2	-6242	47	6435	-3.70	1.60	6.56	132.00	192.00	192.00	23
0	(8+9)-III-1	-3736	46	2006	-2.21	1.57	2.05	132.00	192.00	192.00	53
0	(8+9)-VII-3	3613	-53	-6707	2.14	-1.80	-6.84	132.00	192.00	192.00	16
0	(8+9)-IV-1	3633	-48	-3131	2.15	-1.63	-3.19	132.00	192.00	192.00	24
0	(8+9)-VII-4	-128	-14	-4309	-0.08	-0.46	-4.40	132.00	192.00	192.00	40
0	(8+9)-III-3	4848	-92	-4675	2.87	-3.10	-4.77	132.00	192.00	192.00	16
0	(8+9)-IV-3	6208	-89	-5135	3.68	-3.03	-5.24	132.00	192.00	192.00	14
0	(8+9)-II-3	5921	-91	-4261	3.51	-3.09	-4.35	132.00	192.00	192.00	15
0	(8+9)-VIII-1	4004	-60	-2521	2.37	-2.02	-2.57	132.00	192.00	192.00	24
0	(8+9)-VIII-2	-8467	72	5473	-5.02	2.44	5.58	132.00	192.00	192.00	24

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-VIII-3	5838	-78	-5744	3.46	-2.64	-5.86	132.00	192.00	192.00	14
0	(8+9)-I-3	4762	-92	-4413	2.82	-3.12	-4.50	132.00	192.00	192.00	16

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Ty kg	τ_d kg/cmq	fvd kg/cmq	RS	Cs
0	(8+9)-V-1	33	0.01	6.40	Si	>100
0	(8+9)-VII-4	-36	0.02	6.40	Si	>100
0	(8+9)-I-2	-55	0.02	6.40	Si	>100
0	(8+9)-VII-1	30	0.01	6.40	Si	>100
0	(8+9)-III-3	47	0.02	6.40	Si	>100
0	(8+9)-III-2	-53	0.02	6.40	Si	>100
0	(8+9)-V-4	-38	0.02	6.40	Si	>100
0	(8+9)-I-1	-43	0.02	6.40	Si	>100
0	(8+9)-I-3	49	0.02	6.40	Si	>100
1743	(8+9)-II-3	78	0.03	6.40	Si	>100
1743	(8+9)-V-3	71	0.03	6.40	Si	>100
1743	(8+9)-VII-3	65	0.02	6.40	Si	>100
1743	(8+9)-V-2	-70	0.03	6.40	Si	>100
3486	1	-6	0.00	3.84	Si	>100
3486	2	-13	0.00	5.76	Si	>100
3486	3	-13	0.00	5.76	Si	>100
3486	4	-6	0.00	5.12	Si	>100
3486	5	-6	0.00	5.12	Si	>100
3486	6	-6	0.00	5.12	Si	>100
3486	7	-6	0.00	5.12	Si	>100
3486	(8+9)-VIII-4	-105	0.04	6.40	Si	>100
3486	(8+9)-IV-1	117	0.04	6.40	Si	>100
3486	(8+9)-VI-4	-88	0.03	6.40	Si	>100
3486	(8+9)-IV-3	100	0.03	6.40	Si	>100
3486	(8+9)-II-2	-90	0.03	6.40	Si	>100
3486	(8+9)-IV-2	-108	0.04	6.40	Si	>100
3486	(8+9)-VII-2	-73	0.02	6.40	Si	>100
3486	(8+9)-III-1	57	0.02	6.40	Si	>100
3486	(8+9)-II-1	99	0.03	6.40	Si	>100
3486	(8+9)-VI-1	80	0.03	6.40	Si	>100
3486	(8+9)-I-4	-59	0.02	6.40	Si	>100
3486	(8+9)-III-4	-65	0.02	6.40	Si	>100
3486	(8+9)-II-4	-107	0.04	6.40	Si	>100
3486	(8+9)-VI-2	-109	0.04	6.40	Si	>100
3486	(8+9)-IV-4	-124	0.04	6.40	Si	>100
3486	(8+9)-VIII-1	98	0.03	6.40	Si	>100
3486	(8+9)-VIII-2	-126	0.04	6.40	Si	>100
3486	(8+9)-VIII-3	119	0.04	6.40	Si	>100
3486	(8+9)-VI-3	102	0.03	6.40	Si	>100
Verifiche nella direzione secondaria						
0	1	-4	0.00	3.84	Si	>100
0	2	-19	0.01	5.76	Si	>100
0	3	-19	0.01	5.76	Si	>100
0	4	-4	0.00	5.12	Si	>100
0	5	-4	0.00	5.12	Si	>100
0	6	-4	0.00	5.12	Si	>100
0	7	-4	0.00	5.12	Si	>100
0	(8+9)-VIII-4	-88	0.05	6.40	Si	>100
0	(8+9)-IV-2	-105	0.06	6.40	Si	>100
0	(8+9)-V-1	-13	0.01	6.40	Si	>100
0	(8+9)-I-2	-46	0.03	6.40	Si	>100
0	(8+9)-V-2	-68	0.04	6.40	Si	>100
0	(8+9)-V-3	67	0.04	6.40	Si	>100
0	(8+9)-II-2	-99	0.05	6.40	Si	>100
0	(8+9)-VII-2	-70	0.04	6.40	Si	>100
0	(8+9)-I-3	45	0.02	6.40	Si	>100
0	(8+9)-II-4	-88	0.05	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
0	(8+9)-II-1	87	0.05	6.40	Si	>100
0	(8+9)-III-2	-48	0.03	6.40	Si	>100
0	(8+9)-II-3	98	0.05	6.40	Si	>100
0	(8+9)-VIII-2	-112	0.06	6.40	Si	>100
0	(8+9)-VIII-1	87	0.05	6.40	Si	>100
0	(8+9)-VI-1	80	0.04	6.40	Si	>100
0	(8+9)-IV-4	-94	0.05	6.40	Si	>100
0	(8+9)-VI-2	-105	0.06	6.40	Si	>100
0	(8+9)-III-3	47	0.03	6.40	Si	>100
0	(8+9)-IV-3	104	0.06	6.40	Si	>100
0	(8+9)-VIII-3	111	0.06	6.40	Si	>100
0	(8+9)-IV-1	93	0.05	6.40	Si	>100
0	(8+9)-VI-3	104	0.06	6.40	Si	>100
0	(8+9)-VI-4	-81	0.04	6.40	Si	>100
0	(8+9)-VII-3	69	0.04	6.40	Si	>100
1495	(8+9)-I-4	-25	0.01	6.40	Si	>100
1495	(8+9)-VII-1	12	0.01	6.40	Si	>100
1495	(8+9)-VII-4	-13	0.01	6.40	Si	>100
1495	(8+9)-I-1	24	0.01	6.40	Si	>100
1495	(8+9)-III-4	-25	0.01	6.40	Si	>100
1495	(8+9)-III-1	24	0.01	6.40	Si	>100
1495	(8+9)-V-4	-13	0.01	6.40	Si	>100

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
1743	1	228	0.18	19.20	>100	0.04	12.00	>100	V	>100
1743	2	299	0.23	28.80	>100	0.06	18.00	>100	V	>100
1743	3	299	0.23	28.80	>100	0.06	18.00	>100	V	>100
1743	4	228	0.18	25.60	>100	0.04	16.00	>100	V	>100
1743	5	228	0.18	25.60	>100	0.04	16.00	>100	V	>100
1743	6	228	0.18	25.60	>100	0.04	16.00	>100	V	>100
1743	7	228	0.18	25.60	>100	0.04	16.00	>100	V	>100
1743	(8+9)-IV-1	5045	3.89	32.00	8.2	0.94	20.00	21	V	8.2
1743	(8+9)-VIII-1	4997	3.85	32.00	8.3	0.93	20.00	21	V	8.3
1743	(8+9)-VI-1	4366	3.37	32.00	9.5	0.81	20.00	25	V	9.5
1743	(8+9)-IV-4	-4705	-3.63	32.00	8.8	-0.88	20.00	23	V	8.8
1743	(8+9)-II-1	4414	3.40	32.00	9.4	0.82	20.00	24	V	9.4
1743	(8+9)-VIII-4	-4657	-3.59	32.00	8.9	-0.87	20.00	23	V	8.9
3486	(8+9)-IV-3	9292	6.42	32.00	5.0	1.55	20.00	13	V	5.0
3486	(8+9)-VI-2	-8715	-6.02	32.00	5.3	-1.46	20.00	14	V	5.3
3486	(8+9)-II-4	-4647	-3.21	32.00	10.0	-0.78	20.00	26	V	10.0
3486	(8+9)-VI-3	8801	6.08	32.00	5.3	1.47	20.00	14	V	5.3
3486	(8+9)-III-2	-9080	-6.27	32.00	5.1	-1.52	20.00	13	V	5.1
3486	(8+9)-VI-4	-4766	-3.29	32.00	9.7	-0.80	20.00	25	V	9.7
3486	(8+9)-III-4	4873	3.37	32.00	9.5	0.81	20.00	25	V	9.5
3486	(8+9)-VII-1	-4392	-3.04	32.00	11	-0.73	20.00	27	V	11
3486	(8+9)-IV-2	-9205	-6.36	32.00	5.0	-1.54	20.00	13	V	5.0
3486	(8+9)-VII-2	-8685	-6.00	32.00	5.3	-1.45	20.00	14	V	5.3
3486	(8+9)-I-4	4985	3.44	32.00	9.3	0.83	20.00	24	V	9.3
3486	(8+9)-VII-3	8771	6.06	32.00	5.3	1.47	20.00	14	V	5.3
3486	(8+9)-V-2	-8574	-5.92	32.00	5.4	-1.43	20.00	14	V	5.4
3486	(8+9)-VII-4	4478	3.09	32.00	10	0.75	20.00	27	V	10
3486	(8+9)-V-4	4590	3.17	32.00	10	0.77	20.00	26	V	10
3486	(8+9)-I-2	-8969	-6.20	32.00	5.2	-1.50	20.00	13	V	5.2
3486	(8+9)-III-1	-4787	-3.31	32.00	9.7	-0.80	20.00	25	V	9.7
3486	(8+9)-VIII-2	-9087	-6.28	32.00	5.1	-1.52	20.00	13	V	5.1
3486	(8+9)-II-3	8920	6.16	32.00	5.2	1.49	20.00	13	V	5.2
3486	(8+9)-VIII-3	9173	6.34	32.00	5.0	1.53	20.00	13	V	5.0
3486	(8+9)-V-1	-4504	-3.11	32.00	10	-0.75	20.00	27	V	10
3486	(8+9)-I-3	9055	6.26	32.00	5.1	1.51	20.00	13	V	5.1
3486	(8+9)-III-3	9166	6.33	32.00	5.1	1.53	20.00	13	V	5.1
3486	(8+9)-II-2	-8834	-6.10	32.00	5.2	-1.48	20.00	14	V	5.2

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
3486	(8+9)-V-3	8660	5.98	32.00	5.3	1.45	20.00	14	V	5.3
3486	(8+9)-I-1	-4899	-3.39	32.00	9.5	-0.82	20.00	24	V	9.5
Verifiche nella direzione secondaria										
0	2	109	0.06	28.80	>100	0.02	18.00	>100	V	>100
0	3	109	0.06	28.80	>100	0.02	18.00	>100	V	>100
1495	1	-14	-0.01	19.20	>100	-0.00	12.00	>100	V	>100
1495	4	-14	-0.01	25.60	>100	-0.00	16.00	>100	V	>100
1495	5	-14	-0.01	25.60	>100	-0.00	16.00	>100	V	>100
1495	6	-14	-0.01	25.60	>100	-0.00	16.00	>100	V	>100
1495	7	-14	-0.01	25.60	>100	-0.00	16.00	>100	V	>100
1495	(8+9)-VIII-4	6724	3.98	32.00	8.0	0.96	20.00	21	V	8.0
1495	(8+9)-IV-3	-10558	-6.26	32.00	5.1	-1.51	20.00	13	V	5.1
1495	(8+9)-V-1	4064	2.41	32.00	13	0.58	20.00	34	V	13
1495	(8+9)-I-2	8500	5.04	32.00	6.4	1.22	20.00	16	V	6.4
1495	(8+9)-V-2	8752	5.19	32.00	6.2	1.26	20.00	16	V	6.2
1495	(8+9)-I-4	-3863	-2.29	32.00	14	-0.55	20.00	36	V	14
1495	(8+9)-V-3	-8802	-5.22	32.00	6.1	-1.26	20.00	16	V	6.1
1495	(8+9)-II-2	9643	5.72	32.00	5.6	1.38	20.00	14	V	5.6
1495	(8+9)-V-4	-4114	-2.44	32.00	13	-0.59	20.00	34	V	13
1495	(8+9)-II-4	5934	3.52	32.00	9.1	0.85	20.00	23	V	9.1
1495	(8+9)-VI-1	-5909	-3.50	32.00	9.1	-0.85	20.00	24	V	9.1
1495	(8+9)-III-2	8760	5.19	32.00	6.2	1.26	20.00	16	V	6.2
1495	(8+9)-VI-2	9718	5.76	32.00	5.6	1.39	20.00	14	V	5.6
1495	(8+9)-III-4	-3603	-2.14	32.00	15	-0.52	20.00	39	V	15
1495	(8+9)-VI-3	-9769	-5.79	32.00	5.5	-1.40	20.00	14	V	5.5
1495	(8+9)-IV-2	10508	6.23	32.00	5.1	1.51	20.00	13	V	5.1
1495	(8+9)-VI-4	5858	3.47	32.00	9.2	0.84	20.00	24	V	9.2
1495	(8+9)-IV-4	6799	4.03	32.00	7.9	0.98	20.00	21	V	7.9
1495	(8+9)-VII-1	3804	2.25	32.00	14	0.55	20.00	37	V	14
1495	(8+9)-II-1	-5984	-3.55	32.00	9.0	-0.86	20.00	23	V	9.0
1495	(8+9)-VII-2	9011	5.34	32.00	6.0	1.29	20.00	15	V	6.0
1495	(8+9)-III-1	3553	2.11	32.00	15	0.51	20.00	39	V	15
1495	(8+9)-VII-3	-9062	-5.37	32.00	6.0	-1.30	20.00	15	V	6.0
1495	(8+9)-IV-1	-6849	-4.06	32.00	7.9	-0.98	20.00	20	V	7.9
1495	(8+9)-VII-4	-3855	-2.28	32.00	14	-0.55	20.00	36	V	14
1495	(8+9)-III-3	-8810	-5.22	32.00	6.1	-1.26	20.00	16	V	6.1
1495	(8+9)-I-1	3812	2.26	32.00	14	0.55	20.00	37	V	14
1495	(8+9)-II-3	-9693	-5.75	32.00	5.6	-1.39	20.00	14	V	5.6
1495	(8+9)-VIII-1	-6774	-4.01	32.00	8.0	-0.97	20.00	21	V	8.0
1495	(8+9)-VIII-2	10583	6.27	32.00	5.1	1.52	20.00	13	V	5.1
1495	(8+9)-VIII-3	-10634	-6.30	32.00	5.1	-1.53	20.00	13	V	5.1
1495	(8+9)-I-3	-8551	-5.07	32.00	6.3	-1.23	20.00	16	V	6.3

Verifiche a instabilità

Setto(X)	Comb.	krit _c	krit _m	λ_{relc}	λ_{relm}	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
(cm)						kg/cm q	kg/cm q	kg/cm q	kg/cm q	kg/cm q	kg/cm q	
12(348 .6)	(8+9)-III-2	0.55	--	1.26	--	-0.10	-6.99	6.79	132.00	192.00	192.00	14

Parete Xlam 9 - Nodi: [14-12-102-103] - **Crit.Prog.** Criterio di verifica XLAM 0 - **Verificato:**
[Cs=1.472,Comb=(8+9)-IV-2]

Geometria setti

Setto	Crit.	X	L	S	X90	L90	S90
		mm	cm	cm	mm	cm	cm
13	Criterio di verifica XLAM 0	0	383.2	12.1	0	20.0	12.1
		100	385.1	12.1	1935	20.0	12.1
		200	387.0	12.1	--	--	--
14	Criterio di verifica XLAM 0	0	299.0	12.1	0	119.0	12.1
		595	310.4	12.1	1609	119.0	12.1
		1190	321.8	12.1	--	--	--

Setto	Crit.	X	L	S	X90	L90	S90
15	Criterio di verifica XLAM 0	0	177.0	12.1	0	320.0	12.1
		1600	177.0	12.1	885	320.0	12.1
		3200	177.0	12.1	1770	320.0	12.1
16	Criterio di verifica XLAM 0	0	49.8	12.1	0	320.0	12.1
		1600	80.5	12.1	556	289.9	12.1
		3200	111.1	12.1	--	--	--

Setto 13: origine (754.3,812.2,191.6), direzione (-0.612129,0.790758,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	1	-994	-2	556	-0.36	-0.02	0.31	79.20	115.20	115.20	>100
0	4	-994	-2	556	-0.36	-0.02	0.31	105.60	153.60	153.60	>100
0	5	-994	-2	556	-0.36	-0.02	0.31	105.60	153.60	153.60	>100
0	6	-994	-2	556	-0.36	-0.02	0.31	105.60	153.60	153.60	>100
0	7	-994	-2	556	-0.36	-0.02	0.31	105.60	153.60	153.60	>100
0	(8+9)-V-1	-3718	-413	8323	-1.34	-5.58	4.68	132.00	192.00	192.00	19
0	(8+9)-V-4	2360	412	-7567	0.85	5.56	-4.26	132.00	192.00	192.00	17
0	(8+9)-VII-4	2216	57	-7154	0.80	0.77	-4.03	132.00	192.00	192.00	32
0	(8+9)-V-2	-7772	-120	17077	-2.79	-1.63	9.61	132.00	192.00	192.00	17
0	(8+9)-V-3	6414	119	-16321	2.31	1.61	-9.19	132.00	192.00	192.00	14
0	(8+9)-VII-1	-3574	-58	7910	-1.28	-0.79	4.45	132.00	192.00	192.00	37
100	(8+9)-VII-2	-7924	-481	17830	-2.83	-6.47	9.94	132.00	192.00	192.00	12
100	(8+9)-II-2	-9048	277	19184	-3.24	3.72	10.69	132.00	192.00	192.00	13
100	(8+9)-II-3	7689	-280	-18484	2.75	-3.76	-10.30	132.00	192.00	192.00	11
100	(8+9)-VI-1	4516	-604	-11060	1.62	-8.11	-6.16	132.00	192.00	192.00	12
100	(8+9)-VI-4	-5875	601	11761	-2.10	8.08	6.55	132.00	192.00	192.00	13
100	(8+9)-VII-3	6565	479	-17130	2.35	6.43	-9.55	132.00	192.00	192.00	9.9
200	2	-1879	-17	838	-0.67	-0.23	0.46	118.80	172.80	172.80	>100
200	3	-1879	-17	838	-0.67	-0.23	0.46	118.80	172.80	172.80	>100
200	(8+9)-VIII-4	-6350	-721	13615	-2.26	-9.64	7.51	132.00	192.00	192.00	11
200	(8+9)-IV-1	5017	523	-13014	1.79	6.99	-7.18	132.00	192.00	192.00	11
200	(8+9)-VI-3	7710	-457	-19005	2.74	-6.11	-10.49	132.00	192.00	192.00	9.3
200	(8+9)-IV-2	-9569	-1049	21049	-3.41	-14.03	11.62	132.00	192.00	192.00	7.5
200	(8+9)-II-1	4491	-785	-11571	1.60	-10.50	-6.39	132.00	192.00	192.00	10.0
200	(8+9)-IV-4	-6375	-527	13656	-2.27	-7.04	7.54	132.00	192.00	192.00	13
200	(8+9)-I-4	2615	1026	-7323	0.93	13.72	-4.04	132.00	192.00	192.00	10
200	(8+9)-III-3	6833	1105	-17109	2.43	14.78	-9.44	132.00	192.00	192.00	6.9
200	(8+9)-I-3	6675	713	-16676	2.38	9.53	-9.20	132.00	192.00	192.00	8.7
200	(8+9)-III-1	-3815	-637	7533	-1.36	-8.52	4.16	132.00	192.00	192.00	15
200	(8+9)-I-2	-8033	-716	17319	-2.86	-9.58	9.56	132.00	192.00	192.00	10
200	(8+9)-VI-2	-9069	453	19648	-3.23	6.06	10.84	132.00	192.00	192.00	11
200	(8+9)-I-1	-3973	-1030	7965	-1.41	-13.77	4.40	132.00	192.00	192.00	11
200	(8+9)-II-4	-5849	781	12214	-2.08	10.45	6.74	132.00	192.00	192.00	11
200	(8+9)-IV-3	8211	1046	-20406	2.92	13.98	-11.26	132.00	192.00	192.00	6.5
200	(8+9)-III-2	-8191	-1109	17751	-2.92	-14.83	9.80	132.00	192.00	192.00	7.8
200	(8+9)-VIII-1	4992	717	-12972	1.78	9.59	-7.16	132.00	192.00	192.00	9.9
200	(8+9)-VIII-2	-9594	-855	21090	-3.41	-11.43	11.64	132.00	192.00	192.00	8.3
200	(8+9)-VIII-3	8236	851	-20447	2.93	11.38	-11.28	132.00	192.00	192.00	7.1
200	(8+9)-III-4	2457	633	-6890	0.87	8.47	-3.80	132.00	192.00	192.00	14
Verifiche nella direzione secondaria											
0	1	-640	4	35	-6.61	2.44	10.81	79.20	115.20	115.20	8.5
0	2	-1296	11	68	-13.39	6.59	20.97	118.80	172.80	172.80	6.0
0	3	-1296	11	68	-13.39	6.59	20.97	118.80	172.80	172.80	6.0
0	4	-640	4	35	-6.61	2.44	10.81	105.60	153.60	153.60	11
0	5	-640	4	35	-6.61	2.44	10.81	105.60	153.60	153.60	11
0	6	-640	4	35	-6.61	2.44	10.81	105.60	153.60	153.60	11
0	7	-640	4	35	-6.61	2.44	10.81	105.60	153.60	153.60	11
0	(8+9)-VIII-4	-2217	24	217	-22.90	14.09	67.25	132.00	192.00	192.00	2.3
0	(8+9)-VI-1	1566	-21	-170	16.18	-12.40	-52.81	132.00	192.00	192.00	2.2
0	(8+9)-VI-4	-2435	26	218	-25.15	15.41	67.65	132.00	192.00	192.00	2.2
0	(8+9)-VI-3	697	-3	-159	7.20	-1.57	-49.30	132.00	192.00	192.00	3.1
0	(8+9)-I-4	-2610	40	110	-26.96	23.83	34.20	132.00	192.00	192.00	3.1

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-III-4	-2544	40	110	-26.28	23.43	34.08	132.00	192.00	192.00	3.1
0	(8+9)-II-2	-1488	7	204	-15.37	4.06	63.13	132.00	192.00	192.00	2.8
0	(8+9)-IV-1	1425	-20	-172	14.73	-11.59	-53.42	132.00	192.00	192.00	2.2
0	(8+9)-II-4	-2512	27	222	-25.95	15.93	68.67	132.00	192.00	192.00	2.2
0	(8+9)-I-1	1741	-35	-62	17.99	-20.81	-19.36	132.00	192.00	192.00	2.9
0	(8+9)-VIII-2	-1348	6	206	-13.92	3.26	63.74	132.00	192.00	192.00	2.8
0	(8+9)-VIII-1	1348	-19	-169	13.93	-11.08	-52.41	132.00	192.00	192.00	2.3
0	(8+9)-III-1	1676	-35	-62	17.31	-20.42	-19.24	132.00	192.00	192.00	3.0
0	(8+9)-II-1	1643	-22	-174	16.97	-12.91	-53.83	132.00	192.00	192.00	2.1
0	(8+9)-VI-2	-1565	8	207	-16.17	4.58	64.14	132.00	192.00	192.00	2.7
0	(8+9)-IV-4	-2294	25	220	-23.70	14.61	68.26	132.00	192.00	192.00	2.2
1935	(8+9)-V-1	2222	-93	44	22.96	-54.70	13.76	132.00	192.00	192.00	1.9
1935	(8+9)-IV-2	-1424	11	198	-14.71	6.22	61.27	132.00	192.00	192.00	2.8
1935	(8+9)-I-2	-930	6	184	-9.61	3.62	56.89	132.00	192.00	192.00	3.1
1935	(8+9)-VII-2	1661	-87	129	17.16	-51.68	39.96	132.00	192.00	192.00	1.6
1935	(8+9)-V-3	-2512	90	-108	-25.95	53.21	-33.56	132.00	192.00	192.00	2.1
1935	(8+9)-VII-3	-2515	90	-113	-25.98	53.20	-35.08	132.00	192.00	192.00	2.1
1935	(8+9)-V-2	1659	-87	124	17.14	-51.70	38.44	132.00	192.00	192.00	1.7
1935	(8+9)-VII-4	-3073	95	-24	-31.75	56.23	-7.37	132.00	192.00	192.00	2.8
1935	(8+9)-VII-1	2220	-93	40	22.93	-54.72	12.24	132.00	192.00	192.00	1.9
1935	(8+9)-V-4	-3076	95	-29	-31.77	56.21	-8.89	132.00	192.00	192.00	2.7
1935	(8+9)-IV-3	570	-8	-182	5.89	-4.71	-56.39	132.00	192.00	192.00	2.8
1935	(8+9)-III-2	-928	6	188	-9.58	3.64	58.41	132.00	192.00	192.00	3.1
1935	(8+9)-II-3	578	-8	-166	5.98	-4.65	-51.32	132.00	192.00	192.00	3.0
1935	(8+9)-I-3	77	-4	-168	0.79	-2.11	-52.01	132.00	192.00	192.00	3.5
1935	(8+9)-VIII-3	-207	20	-164	-2.13	11.89	-50.86	132.00	192.00	192.00	3.1
1935	(8+9)-III-3	74	-4	-173	0.77	-2.13	-53.53	132.00	192.00	192.00	3.4

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Ty kg	τ_d kg/cm ²	fvd kg/cm ²	RS	Cs
0	1	-10	0.00	3.84	Si	>100
0	2	-29	0.01	5.76	Si	>100
0	3	-29	0.01	5.76	Si	>100
0	4	-10	0.00	5.12	Si	>100
0	5	-10	0.00	5.12	Si	>100
0	6	-10	0.00	5.12	Si	>100
0	7	-10	0.00	5.12	Si	>100
0	(8+9)-VII-1	371	0.10	6.40	Si	66
0	(8+9)-V-1	399	0.10	6.40	Si	61
0	(8+9)-VII-3	-422	0.11	6.40	Si	58
0	(8+9)-VIII-1	48	0.01	6.40	Si	>100
0	(8+9)-VII-2	411	0.11	6.40	Si	60
0	(8+9)-VIII-3	-190	0.05	6.40	Si	>100
0	(8+9)-VI-3	-98	0.03	6.40	Si	>100
0	(8+9)-VIII-2	179	0.05	6.40	Si	>100
0	(8+9)-VI-2	86	0.02	6.40	Si	>100
0	(8+9)-VIII-4	-59	0.02	6.40	Si	>100
0	(8+9)-II-1	-50	0.01	6.40	Si	>100
0	(8+9)-II-4	38	0.01	6.40	Si	>100
0	(8+9)-VII-4	-383	0.10	6.40	Si	64
0	(8+9)-V-4	-411	0.11	6.40	Si	60
0	(8+9)-V-3	-394	0.10	6.40	Si	62
0	(8+9)-V-2	383	0.10	6.40	Si	64
100	(8+9)-I-2	-258	0.07	6.40	Si	95
100	(8+9)-III-2	-228	0.06	6.40	Si	>100
100	(8+9)-IV-4	132	0.03	6.40	Si	>100
100	(8+9)-III-1	-267	0.07	6.40	Si	92
100	(8+9)-IV-2	-13	0.00	6.40	Si	>100
100	(8+9)-IV-1	-143	0.04	6.40	Si	>100
100	(8+9)-III-4	256	0.07	6.40	Si	96
100	(8+9)-I-3	246	0.06	6.40	Si	100
100	(8+9)-I-1	-238	0.06	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
100	(8+9)-III-3	217	0.06	6.40	Si	>100
100	(8+9)-IV-3	2	0.00	6.40	Si	>100
100	(8+9)-I-4	226	0.06	6.40	Si	>100
200	(8+9)-II-3	109	0.03	6.40	Si	>100
200	(8+9)-II-2	-120	0.03	6.40	Si	>100
200	(8+9)-VI-1	154	0.04	6.40	Si	>100
200	(8+9)-VI-4	-166	0.04	6.40	Si	>100
Verifiche nella direzione secondaria						
0	2	-9	0.09	5.76	Si	67
0	3	-9	0.09	5.76	Si	67
0	(8+9)-IV-4	-17	0.16	6.40	Si	40
0	(8+9)-VII-3	-10	0.10	6.40	Si	65
0	(8+9)-V-3	-9	0.09	6.40	Si	74
0	(8+9)-VII-4	-14	0.14	6.40	Si	46
0	(8+9)-II-4	-21	0.20	6.40	Si	32
0	(8+9)-VII-2	10	0.10	6.40	Si	64
0	(8+9)-III-1	36	0.34	6.40	Si	19
0	(8+9)-I-1	37	0.35	6.40	Si	18
0	(8+9)-III-2	32	0.30	6.40	Si	21
0	(8+9)-I-3	-30	0.29	6.40	Si	22
0	(8+9)-III-3	-32	0.30	6.40	Si	21
0	(8+9)-II-1	21	0.20	6.40	Si	32
0	(8+9)-III-4	-36	0.34	6.40	Si	19
0	(8+9)-I-2	30	0.29	6.40	Si	22
0	(8+9)-I-4	-37	0.35	6.40	Si	18
0	(8+9)-V-4	-16	0.15	6.40	Si	43
0	(8+9)-VII-1	15	0.14	6.40	Si	46
0	(8+9)-IV-1	17	0.16	6.40	Si	39
0	(8+9)-V-2	9	0.09	6.40	Si	73
0	(8+9)-V-1	16	0.15	6.40	Si	43
1935	1	1	0.01	3.84	Si	>100
1935	4	1	0.01	5.12	Si	>100
1935	5	1	0.01	5.12	Si	>100
1935	6	1	0.01	5.12	Si	>100
1935	7	1	0.01	5.12	Si	>100
1935	(8+9)-VIII-4	-16	0.15	6.40	Si	43
1935	(8+9)-IV-3	22	0.21	6.40	Si	30
1935	(8+9)-II-3	23	0.22	6.40	Si	29
1935	(8+9)-VI-2	-18	0.17	6.40	Si	38
1935	(8+9)-IV-2	-20	0.19	6.40	Si	33
1935	(8+9)-II-2	-21	0.20	6.40	Si	31
1935	(8+9)-VI-3	20	0.19	6.40	Si	34
1935	(8+9)-VI-1	19	0.18	6.40	Si	36
1935	(8+9)-VIII-1	18	0.17	6.40	Si	38
1935	(8+9)-VIII-2	-17	0.16	6.40	Si	40
1935	(8+9)-VIII-3	19	0.18	6.40	Si	36
1935	(8+9)-VI-4	-17	0.16	6.40	Si	40

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	(8+9)-VI-4	-4718	-2.54	32.00	13	-0.62	20.00	32	V	13
0	(8+9)-III-1	-815	-0.44	32.00	73	-0.11	20.00	>100	V	73
0	(8+9)-V-3	2824	1.52	32.00	21	0.37	20.00	54	V	21
0	(8+9)-III-2	-4193	-2.26	32.00	14	-0.55	20.00	37	V	14
0	(8+9)-VIII-3	6144	3.31	32.00	9.7	0.80	20.00	25	V	9.7
0	(8+9)-III-3	4586	2.47	32.00	13	0.60	20.00	33	V	13
0	(8+9)-VIII-1	5509	2.97	32.00	11	0.72	20.00	28	V	11
0	(8+9)-III-4	1208	0.65	32.00	49	0.16	20.00	>100	V	49
0	(8+9)-VII-3	2943	1.59	32.00	20	0.38	20.00	52	V	20
0	(8+9)-IV-1	5016	2.70	32.00	12	0.65	20.00	31	V	12
0	(8+9)-I-2	-4074	-2.20	32.00	15	-0.53	20.00	38	V	15
0	(8+9)-IV-2	-6243	-3.37	32.00	9.5	-0.81	20.00	25	V	9.5

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
0	(8+9)-I-4	1328	0.72	32.00	45	0.17	20.00	>100	V	45
0	(8+9)-IV-3	6636	3.58	32.00	8.9	0.87	20.00	23	V	8.9
0	(8+9)-II-2	-5845	-3.15	32.00	10	-0.76	20.00	26	V	10
0	(8+9)-IV-4	-4623	-2.49	32.00	13	-0.60	20.00	33	V	13
0	(8+9)-II-4	-4225	-2.28	32.00	14	-0.55	20.00	36	V	14
0	(8+9)-VII-2	-2550	-1.38	32.00	23	-0.33	20.00	60	V	23
0	(8+9)-VIII-2	-5751	-3.10	32.00	10	-0.75	20.00	27	V	10
0	(8+9)-V-2	-2431	-1.31	32.00	24	-0.32	20.00	63	V	24
0	(8+9)-I-1	-935	-0.50	32.00	63	-0.12	20.00	>100	V	63
0	(8+9)-II-1	4618	2.49	32.00	13	0.60	20.00	33	V	13
0	(8+9)-VIII-4	-5116	-2.76	32.00	12	-0.67	20.00	30	V	12
0	(8+9)-VI-3	5745	3.10	32.00	10	0.75	20.00	27	V	10
0	(8+9)-I-3	4466	2.41	32.00	13	0.58	20.00	34	V	13
0	(8+9)-II-3	6238	3.36	32.00	9.5	0.81	20.00	25	V	9.5
0	(8+9)-VI-2	-5352	-2.89	32.00	11	-0.70	20.00	29	V	11
0	(8+9)-VI-1	5111	2.76	32.00	12	0.67	20.00	30	V	12
100	(8+9)-VII-1	897	0.48	32.00	66	0.12	20.00	>100	V	66
100	(8+9)-VII-4	-470	-0.25	32.00	>100	-0.06	20.00	>100	V	>100
200	1	311	0.17	19.20	>100	0.04	12.00	>100	V	>100
200	2	255	0.14	28.80	>100	0.03	18.00	>100	V	>100
200	3	255	0.14	28.80	>100	0.03	18.00	>100	V	>100
200	4	311	0.17	25.60	>100	0.04	16.00	>100	V	>100
200	5	311	0.17	25.60	>100	0.04	16.00	>100	V	>100
200	6	311	0.17	25.60	>100	0.04	16.00	>100	V	>100
200	7	311	0.17	25.60	>100	0.04	16.00	>100	V	>100
200	(8+9)-V-4	-448	-0.24	32.00	>100	-0.06	20.00	>100	V	>100
200	(8+9)-V-1	896	0.48	32.00	67	0.12	20.00	>100	V	67
Verifiche nella direzione secondaria										
0	(8+9)-II-1	-421	-4.35	32.00	7.4	-1.05	20.00	19	V	7.4
0	(8+9)-VII-3	-570	-5.89	32.00	5.4	-1.43	20.00	14	V	5.4
0	(8+9)-V-4	-232	-2.39	32.00	13	-0.58	20.00	35	V	13
0	(8+9)-VII-4	-217	-2.24	32.00	14	-0.54	20.00	37	V	14
0	(8+9)-V-3	-555	-5.74	32.00	5.6	-1.39	20.00	14	V	5.6
0	(8+9)-VI-3	-654	-6.75	32.00	4.7	-1.63	20.00	12	V	4.7
0	(8+9)-VII-2	580	6.00	32.00	5.3	1.45	20.00	14	V	5.3
0	(8+9)-VII-1	227	2.35	32.00	14	0.57	20.00	35	V	14
0	(8+9)-V-2	566	5.84	32.00	5.5	1.41	20.00	14	V	5.5
0	(8+9)-V-1	242	2.50	32.00	13	0.61	20.00	33	V	13
0	(8+9)-II-4	431	4.46	32.00	7.2	1.08	20.00	19	V	7.2
1935	1	23	0.24	19.20	80	0.06	12.00	>100	V	80
1935	2	68	0.70	28.80	41	0.17	18.00	>100	V	41
1935	3	68	0.70	28.80	41	0.17	18.00	>100	V	41
1935	4	23	0.24	25.60	>100	0.06	16.00	>100	V	>100
1935	5	23	0.24	25.60	>100	0.06	16.00	>100	V	>100
1935	6	23	0.24	25.60	>100	0.06	16.00	>100	V	>100
1935	7	23	0.24	25.60	>100	0.06	16.00	>100	V	>100
1935	(8+9)-VIII-4	739	7.64	32.00	4.2	1.85	20.00	11	V	4.2
1935	(8+9)-I-1	631	6.52	32.00	4.9	1.58	20.00	13	V	4.9
1935	(8+9)-II-2	895	9.25	32.00	3.5	2.24	20.00	8.9	V	3.5
1935	(8+9)-III-3	-1011	-10.44	32.00	3.1	-2.53	20.00	7.9	V	3.1
1935	(8+9)-IV-2	995	10.28	32.00	3.1	2.49	20.00	8.0	V	3.1
1935	(8+9)-VI-4	639	6.60	32.00	4.8	1.60	20.00	13	V	4.8
1935	(8+9)-IV-4	512	5.29	32.00	6.1	1.28	20.00	16	V	6.1
1935	(8+9)-III-2	1043	10.78	32.00	3.0	2.61	20.00	7.7	V	3.0
1935	(8+9)-I-2	1014	10.47	32.00	3.1	2.53	20.00	7.9	V	3.1
1935	(8+9)-III-1	601	6.21	32.00	5.2	1.50	20.00	13	V	5.2
1935	(8+9)-III-4	-569	-5.87	32.00	5.4	-1.42	20.00	14	V	5.4
1935	(8+9)-I-4	-599	-6.18	32.00	5.2	-1.50	20.00	13	V	5.2
1935	(8+9)-VI-2	668	6.90	32.00	4.6	1.67	20.00	12	V	4.6
1935	(8+9)-II-3	-863	-8.91	32.00	3.6	-2.16	20.00	9.3	V	3.6
1935	(8+9)-VI-1	-607	-6.27	32.00	5.1	-1.52	20.00	13	V	5.1
1935	(8+9)-IV-3	-963	-9.95	32.00	3.2	-2.41	20.00	8.3	V	3.2
1935	(8+9)-IV-1	-479	-4.95	32.00	6.5	-1.20	20.00	17	V	6.5
1935	(8+9)-VIII-1	-707	-7.30	32.00	4.4	-1.77	20.00	11	V	4.4

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
1935	(8+9)-VIII-2	768	7.93	32.00	4.0	1.92	20.00	10	V	4.0
1935	(8+9)-VIII-3	-735	-7.60	32.00	4.2	-1.84	20.00	11	V	4.2
1935	(8+9)-I-3	-981	-10.13	32.00	3.2	-2.45	20.00	8.2	V	3.2

Setto 14: origine (1023.0,465.0,149.5), direzione (-0.612129,0.790758,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	(8+9)-II-4	-395	415	4045	-0.18	7.18	3.74	132.00	192.00	192.00	18
0	(8+9)-VI-4	-408	334	4007	-0.19	5.78	3.70	132.00	192.00	192.00	20
0	(8+9)-I-1	-492	-535	2658	-0.23	-9.25	2.46	132.00	192.00	192.00	16
0	(8+9)-V-1	-450	-265	2785	-0.21	-4.59	2.57	132.00	192.00	192.00	27
595	2	-515	4	411	-0.23	0.07	0.35	118.80	172.80	172.80	>100
595	3	-515	4	411	-0.23	0.07	0.35	118.80	172.80	172.80	>100
595	(8+9)-VII-1	-749	-67	4429	-0.33	-1.12	3.80	132.00	192.00	192.00	39
1190	1	134	-3	-201	0.06	-0.04	-0.16	79.20	115.20	115.20	>100
1190	4	134	-3	-201	0.06	-0.04	-0.16	105.60	153.60	153.60	>100
1190	5	134	-3	-201	0.06	-0.04	-0.16	105.60	153.60	153.60	>100
1190	6	134	-3	-201	0.06	-0.04	-0.16	105.60	153.60	153.60	>100
1190	7	134	-3	-201	0.06	-0.04	-0.16	105.60	153.60	153.60	>100
1190	(8+9)-VIII-4	-2458	292	9492	-1.05	4.69	7.58	132.00	192.00	192.00	16
1190	(8+9)-IV-1	2669	-211	-9883	1.14	-3.39	-7.89	132.00	192.00	192.00	15
1190	(8+9)-V-4	1862	-124	-6489	0.80	-2.00	-5.18	132.00	192.00	192.00	23
1190	(8+9)-II-3	4028	-59	-14408	1.72	-0.95	-11.50	132.00	192.00	192.00	13
1190	(8+9)-VI-1	2414	88	-8645	1.03	1.42	-6.90	132.00	192.00	192.00	20
1190	(8+9)-III-1	-1573	287	5520	-0.67	4.62	4.41	132.00	192.00	192.00	21
1190	(8+9)-VI-2	-3819	-29	14221	-1.63	-0.47	11.35	132.00	192.00	192.00	16
1190	(8+9)-III-3	3805	-486	-13350	1.63	-7.82	-10.65	132.00	192.00	192.00	9.2
1190	(8+9)-VI-3	4029	26	-14510	1.72	0.41	-11.58	132.00	192.00	192.00	13
1190	(8+9)-II-1	2415	173	-8747	1.03	2.78	-6.98	132.00	192.00	192.00	17
1190	(8+9)-I-3	3729	-371	-13009	1.60	-5.97	-10.38	132.00	192.00	192.00	10
1190	(8+9)-IV-3	4282	-443	-15544	1.83	-7.12	-12.41	132.00	192.00	192.00	8.7
1190	(8+9)-I-2	-3519	367	12720	-1.51	5.90	10.15	132.00	192.00	192.00	12
1190	(8+9)-I-4	1859	-406	-6149	0.80	-6.54	-4.91	132.00	192.00	192.00	15
1190	(8+9)-VII-2	-3598	200	13401	-1.54	3.22	10.70	132.00	192.00	192.00	14
1190	(8+9)-V-3	3732	-89	-13349	1.60	-1.43	-10.65	132.00	192.00	192.00	13
1190	(8+9)-VII-3	3808	-204	-13690	1.63	-3.28	-10.93	132.00	192.00	192.00	12
1190	(8+9)-III-2	-3595	482	13061	-1.54	7.76	10.42	132.00	192.00	192.00	11
1190	(8+9)-VII-4	1786	-9	-6148	0.76	-0.15	-4.91	132.00	192.00	192.00	31
1190	(8+9)-V-2	-3522	85	13060	-1.51	1.37	10.42	132.00	192.00	192.00	16
1190	(8+9)-II-2	-3818	55	14119	-1.63	0.89	11.27	132.00	192.00	192.00	16
1190	(8+9)-III-4	1783	-291	-5809	0.76	-4.68	-4.64	132.00	192.00	192.00	18
1190	(8+9)-IV-4	-2458	207	9594	-1.05	3.33	7.66	132.00	192.00	192.00	17
1190	(8+9)-VIII-1	2668	-295	-9781	1.14	-4.75	-7.81	132.00	192.00	192.00	14
1190	(8+9)-VIII-2	-4073	354	15357	-1.74	5.70	12.26	132.00	192.00	192.00	11
1190	(8+9)-VIII-3	4283	-358	-15646	1.83	-5.76	-12.49	132.00	192.00	192.00	9.2
1190	(8+9)-IV-2	-4072	439	15255	-1.74	7.06	12.17	132.00	192.00	192.00	10.0
Verifiche nella direzione secondaria											
0	1	-1311	21	-257	-2.28	2.11	-2.25	79.20	115.20	115.20	26
0	2	-2099	39	-385	-3.64	3.85	-3.37	118.80	172.80	172.80	24
0	3	-2099	39	-385	-3.64	3.85	-3.37	118.80	172.80	172.80	24
0	4	-1311	21	-257	-2.28	2.11	-2.25	105.60	153.60	153.60	35
0	5	-1311	21	-257	-2.28	2.11	-2.25	105.60	153.60	153.60	35
0	6	-1311	21	-257	-2.28	2.11	-2.25	105.60	153.60	153.60	35
0	7	-1311	21	-257	-2.28	2.11	-2.25	105.60	153.60	153.60	35
0	(8+9)-VI-4	-372	32	930	-0.65	3.16	8.14	132.00	192.00	192.00	17
1609	(8+9)-VIII-4	797	38	1165	1.38	3.79	10.20	132.00	192.00	192.00	12
1609	(8+9)-IV-2	2092	17	1905	3.63	1.69	16.67	132.00	192.00	192.00	8.1
1609	(8+9)-V-2	1854	1	1588	3.22	0.13	13.90	132.00	192.00	192.00	10
1609	(8+9)-I-3	-3579	65	-1824	-6.21	6.47	-15.97	132.00	192.00	192.00	8.5
1609	(8+9)-V-3	-3603	13	-2049	-6.26	1.27	-17.94	132.00	192.00	192.00	9.9
1609	(8+9)-II-1	-2093	-22	-1470	-3.63	-2.23	-12.87	132.00	192.00	192.00	13
1609	(8+9)-V-4	-2485	19	-1104	-4.32	1.93	-9.66	132.00	192.00	192.00	16

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
1609	(8+9)-II-3	-3380	14	-2142	-5.87	1.43	-18.75	132.00	192.00	192.00	9.4
1609	(8+9)-VI-1	-2086	-7	-1402	-3.62	-0.67	-12.27	132.00	192.00	192.00	15
1609	(8+9)-III-1	574	-63	350	1.00	-6.25	3.07	132.00	192.00	192.00	18
1609	(8+9)-VI-2	1639	15	1748	2.84	1.53	15.30	132.00	192.00	192.00	9.2
1609	(8+9)-III-3	-3717	60	-1891	-6.45	5.95	-16.56	132.00	192.00	192.00	8.4
1609	(8+9)-VI-3	-3388	-1	-2210	-5.88	-0.13	-19.34	132.00	192.00	192.00	9.8
1609	(8+9)-IV-1	-2553	-40	-1694	-4.43	-3.95	-14.83	132.00	192.00	192.00	10
1609	(8+9)-I-1	712	-58	417	1.24	-5.73	3.65	132.00	192.00	192.00	17
1609	(8+9)-IV-3	-3841	-3	-2366	-6.67	-0.29	-20.72	132.00	192.00	192.00	9.0
1609	(8+9)-VII-1	598	-10	575	1.04	-1.04	5.04	132.00	192.00	192.00	25
1609	(8+9)-V-1	736	-5	643	1.28	-0.53	5.62	132.00	192.00	192.00	24
1609	(8+9)-VII-2	1992	7	1655	3.46	0.65	14.49	132.00	192.00	192.00	9.5
1609	(8+9)-II-2	1631	-0	1681	2.83	-0.03	14.71	132.00	192.00	192.00	10
1609	(8+9)-VII-3	-3741	8	-2116	-6.49	0.75	-18.53	132.00	192.00	192.00	9.8
1609	(8+9)-III-2	1968	-46	1430	3.42	-4.56	12.52	132.00	192.00	192.00	8.7
1609	(8+9)-VII-4	-2347	25	-1037	-4.08	2.44	-9.08	132.00	192.00	192.00	17
1609	(8+9)-I-4	-2461	72	-879	-4.27	7.13	-7.69	132.00	192.00	192.00	13
1609	(8+9)-II-4	344	37	1008	0.60	3.63	8.83	132.00	192.00	192.00	14
1609	(8+9)-III-4	-2323	77	-812	-4.03	7.65	-7.11	132.00	192.00	192.00	13
1609	(8+9)-IV-4	804	54	1232	1.40	5.35	10.79	132.00	192.00	192.00	11
1609	(8+9)-VIII-1	-2546	-24	-1626	-4.42	-2.39	-14.24	132.00	192.00	192.00	11
1609	(8+9)-VIII-2	2099	33	1972	3.64	3.25	17.27	132.00	192.00	192.00	7.4
1609	(8+9)-VIII-3	-3848	-19	-2434	-6.68	-1.85	-21.31	132.00	192.00	192.00	8.2
1609	(8+9)-I-2	1830	-51	1363	3.18	-5.07	11.93	132.00	192.00	192.00	8.9

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
0	2	8	0.00	5.76	Si	>100
0	3	8	0.00	5.76	Si	>100
0	(8+9)-V-1	29	0.01	6.40	Si	>100
0	(8+9)-VI-2	73	0.02	6.40	Si	>100
0	(8+9)-V-4	-29	0.01	6.40	Si	>100
0	(8+9)-VII-1	44	0.01	6.40	Si	>100
0	(8+9)-V-3	-65	0.02	6.40	Si	>100
0	(8+9)-VI-3	-73	0.02	6.40	Si	>100
0	(8+9)-VI-1	-45	0.02	6.40	Si	>100
0	(8+9)-VI-4	45	0.02	6.40	Si	>100
0	(8+9)-VII-4	-45	0.01	6.40	Si	>100
0	(8+9)-V-2	65	0.02	6.40	Si	>100
0	(8+9)-II-2	92	0.03	6.40	Si	>100
0	(8+9)-II-3	-92	0.03	6.40	Si	>100
595	1	-1	0.00	3.84	Si	>100
595	4	-1	0.00	5.12	Si	>100
595	5	-1	0.00	5.12	Si	>100
595	6	-1	0.00	5.12	Si	>100
595	7	-1	0.00	5.12	Si	>100
595	(8+9)-III-1	238	0.08	6.40	Si	83
595	(8+9)-VIII-2	-132	0.04	6.40	Si	>100
595	(8+9)-IV-2	-64	0.02	6.40	Si	>100
595	(8+9)-VIII-3	129	0.04	6.40	Si	>100
595	(8+9)-IV-4	-185	0.06	6.40	Si	>100
595	(8+9)-VIII-4	-117	0.04	6.40	Si	>100
595	(8+9)-II-1	109	0.04	6.40	Si	>100
595	(8+9)-III-2	164	0.05	6.40	Si	>100
595	(8+9)-I-3	-189	0.06	6.40	Si	>100
595	(8+9)-VIII-1	114	0.04	6.40	Si	>100
595	(8+9)-I-1	216	0.07	6.40	Si	92
595	(8+9)-IV-3	61	0.02	6.40	Si	>100
595	(8+9)-III-4	-240	0.08	6.40	Si	83
595	(8+9)-II-4	-112	0.04	6.40	Si	>100
595	(8+9)-VII-2	-63	0.02	6.40	Si	>100
595	(8+9)-I-2	186	0.06	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
595	(8+9)-IV-1	182	0.06	6.40	Si	>100
595	(8+9)-III-3	-167	0.05	6.40	Si	>100
595	(8+9)-VII-3	60	0.02	6.40	Si	>100
595	(8+9)-I-4	-218	0.07	6.40	Si	91
Verifiche nella direzione secondaria						
0	2	-12	0.02	5.76	Si	>100
0	3	-12	0.02	5.76	Si	>100
0	(8+9)-II-3	48	0.08	6.40	Si	83
0	(8+9)-I-2	-30	0.05	6.40	Si	>100
0	(8+9)-VI-4	-45	0.07	6.40	Si	89
0	(8+9)-I-3	27	0.04	6.40	Si	>100
0	(8+9)-VI-2	-46	0.07	6.40	Si	86
0	(8+9)-III-3	25	0.04	6.40	Si	>100
0	(8+9)-VI-3	44	0.07	6.40	Si	90
0	(8+9)-VI-1	43	0.07	6.40	Si	93
0	(8+9)-III-2	-27	0.04	6.40	Si	>100
0	(8+9)-II-1	39	0.06	6.40	Si	>100
0	(8+9)-II-2	-50	0.08	6.40	Si	80
1609	1	4	0.01	3.84	Si	>100
1609	4	4	0.01	5.12	Si	>100
1609	5	4	0.01	5.12	Si	>100
1609	6	4	0.01	5.12	Si	>100
1609	7	4	0.01	5.12	Si	>100
1609	(8+9)-VIII-4	46	0.07	6.40	Si	87
1609	(8+9)-V-4	-22	0.03	6.40	Si	>100
1609	(8+9)-II-4	42	0.07	6.40	Si	95
1609	(8+9)-I-4	37	0.06	6.40	Si	>100
1609	(8+9)-IV-2	49	0.08	6.40	Si	82
1609	(8+9)-III-1	-38	0.06	6.40	Si	>100
1609	(8+9)-IV-4	64	0.10	6.40	Si	63
1609	(8+9)-VII-1	21	0.03	6.40	Si	>100
1609	(8+9)-V-2	46	0.07	6.40	Si	86
1609	(8+9)-VII-2	53	0.08	6.40	Si	76
1609	(8+9)-IV-1	-58	0.09	6.40	Si	69
1609	(8+9)-VII-3	-47	0.08	6.40	Si	85
1609	(8+9)-I-1	-32	0.05	6.40	Si	>100
1609	(8+9)-VII-4	-15	0.02	6.40	Si	>100
1609	(8+9)-III-4	44	0.07	6.40	Si	92
1609	(8+9)-IV-3	-43	0.07	6.40	Si	93
1609	(8+9)-V-3	-41	0.07	6.40	Si	98
1609	(8+9)-VIII-1	-40	0.06	6.40	Si	99
1609	(8+9)-VIII-2	66	0.11	6.40	Si	60
1609	(8+9)-VIII-3	-61	0.10	6.40	Si	66
1609	(8+9)-V-1	27	0.04	6.40	Si	>100

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	(8+9)-VI-1	5034	3.48	32.00	9.2	0.84	20.00	24	V	9.2
0	(8+9)-II-2	-8628	-5.96	32.00	5.4	-1.44	20.00	14	V	5.4
0	(8+9)-III-2	-8411	-5.81	32.00	5.5	-1.41	20.00	14	V	5.5
0	(8+9)-I-3	8147	5.63	32.00	5.7	1.36	20.00	15	V	5.7
0	(8+9)-II-3	8484	5.86	32.00	5.5	1.42	20.00	14	V	5.5
0	(8+9)-I-4	4131	2.85	32.00	11	0.69	20.00	29	V	11
0	(8+9)-VI-3	8207	5.67	32.00	5.6	1.37	20.00	15	V	5.6
0	(8+9)-II-1	4757	3.29	32.00	9.7	0.80	20.00	25	V	9.7
0	(8+9)-III-4	4011	2.77	32.00	12	0.67	20.00	30	V	12
0	(8+9)-III-3	8267	5.71	32.00	5.6	1.38	20.00	14	V	5.6
0	(8+9)-VI-4	-5178	-3.58	32.00	8.9	-0.87	20.00	23	V	8.9
0	(8+9)-I-1	-4275	-2.95	32.00	11	-0.71	20.00	28	V	11
0	(8+9)-VI-2	-8351	-5.77	32.00	5.5	-1.40	20.00	14	V	5.5
0	(8+9)-I-2	-8291	-5.73	32.00	5.6	-1.39	20.00	14	V	5.6
0	(8+9)-II-4	-4901	-3.39	32.00	9.4	-0.82	20.00	24	V	9.4

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
0	(8+9)-III-1	-4155	-2.87	32.00	11	-0.69	20.00	29	V	11
595	1	-163	-0.11	19.20	>100	-0.03	12.00	>100	V	>100
595	2	-261	-0.17	28.80	>100	-0.04	18.00	>100	V	>100
595	3	-261	-0.17	28.80	>100	-0.04	18.00	>100	V	>100
595	4	-163	-0.11	25.60	>100	-0.03	16.00	>100	V	>100
595	5	-163	-0.11	25.60	>100	-0.03	16.00	>100	V	>100
595	6	-163	-0.11	25.60	>100	-0.03	16.00	>100	V	>100
595	7	-163	-0.11	25.60	>100	-0.03	16.00	>100	V	>100
595	(8+9)-IV-3	9252	6.16	32.00	5.2	1.49	20.00	13	V	5.2
595	(8+9)-VII-3	7942	5.29	32.00	6.1	1.28	20.00	16	V	6.1
595	(8+9)-V-2	-7891	-5.25	32.00	6.1	-1.27	20.00	16	V	6.1
595	(8+9)-VII-4	3397	2.26	32.00	14	0.55	20.00	37	V	14
595	(8+9)-V-4	3682	2.45	32.00	13	0.59	20.00	34	V	13
595	(8+9)-VIII-1	5723	3.81	32.00	8.4	0.92	20.00	22	V	8.4
595	(8+9)-IV-4	-5899	-3.93	32.00	8.1	-0.95	20.00	21	V	8.1
595	(8+9)-VIII-2	-9429	-6.28	32.00	5.1	-1.52	20.00	13	V	5.1
595	(8+9)-IV-1	5665	3.77	32.00	8.5	0.91	20.00	22	V	8.5
595	(8+9)-VIII-3	9195	6.12	32.00	5.2	1.48	20.00	14	V	5.2
595	(8+9)-VII-2	-8176	-5.44	32.00	5.9	-1.32	20.00	15	V	5.9
595	(8+9)-V-1	-3916	-2.61	32.00	12	-0.63	20.00	32	V	12
595	(8+9)-IV-2	-9486	-6.31	32.00	5.1	-1.53	20.00	13	V	5.1
595	(8+9)-VII-1	-3631	-2.42	32.00	13	-0.58	20.00	34	V	13
595	(8+9)-V-3	7657	5.10	32.00	6.3	1.23	20.00	16	V	6.3
595	(8+9)-VIII-4	-5957	-3.96	32.00	8.1	-0.96	20.00	21	V	8.1
Verifiche nella direzione secondaria										
0	2	23	0.04	28.80	>100	0.01	18.00	>100	V	>100
0	3	23	0.04	28.80	>100	0.01	18.00	>100	V	>100
0	(8+9)-VIII-4	2238	3.89	32.00	8.2	0.94	20.00	21	V	8.2
0	(8+9)-VI-4	1940	3.37	32.00	9.5	0.81	20.00	25	V	9.5
0	(8+9)-III-3	-2969	-5.15	32.00	6.2	-1.25	20.00	16	V	6.2
0	(8+9)-IV-3	-3513	-6.10	32.00	5.2	-1.48	20.00	14	V	5.2
0	(8+9)-VII-2	3058	5.31	32.00	6.0	1.29	20.00	16	V	6.0
0	(8+9)-VIII-2	3549	6.16	32.00	5.2	1.49	20.00	13	V	5.2
0	(8+9)-IV-1	-2248	-3.90	32.00	8.2	-0.94	20.00	21	V	8.2
0	(8+9)-I-1	1339	2.32	32.00	14	0.56	20.00	36	V	14
0	(8+9)-IV-2	3526	6.12	32.00	5.2	1.48	20.00	13	V	5.2
0	(8+9)-I-3	-2879	-5.00	32.00	6.4	-1.21	20.00	17	V	6.4
0	(8+9)-II-1	-1950	-3.38	32.00	9.5	-0.82	20.00	24	V	9.5
0	(8+9)-IV-4	2261	3.93	32.00	8.2	0.95	20.00	21	V	8.2
0	(8+9)-II-3	-3215	-5.58	32.00	5.7	-1.35	20.00	15	V	5.7
0	(8+9)-V-1	1416	2.46	32.00	13	0.59	20.00	34	V	13
0	(8+9)-III-1	1249	2.17	32.00	15	0.52	20.00	38	V	15
0	(8+9)-V-2	2969	5.15	32.00	6.2	1.25	20.00	16	V	6.2
0	(8+9)-VIII-3	-3536	-6.14	32.00	5.2	-1.49	20.00	13	V	5.2
0	(8+9)-V-3	-2956	-5.13	32.00	6.2	-1.24	20.00	16	V	6.2
0	(8+9)-I-2	2892	5.02	32.00	6.4	1.22	20.00	16	V	6.4
0	(8+9)-VII-1	1326	2.30	32.00	14	0.56	20.00	36	V	14
0	(8+9)-II-2	3228	5.60	32.00	5.7	1.36	20.00	15	V	5.7
0	(8+9)-III-2	2982	5.18	32.00	6.2	1.25	20.00	16	V	6.2
0	(8+9)-VIII-1	-2225	-3.86	32.00	8.3	-0.93	20.00	21	V	8.3
0	(8+9)-VII-3	-3045	-5.29	32.00	6.1	-1.28	20.00	16	V	6.1
0	(8+9)-II-4	1963	3.41	32.00	9.4	0.82	20.00	24	V	9.4
0	(8+9)-VI-1	-1927	-3.35	32.00	9.6	-0.81	20.00	25	V	9.6
0	(8+9)-VI-2	3251	5.64	32.00	5.7	1.37	20.00	15	V	5.7
0	(8+9)-VI-3	-3238	-5.62	32.00	5.7	-1.36	20.00	15	V	5.7
1609	1	-9	-0.01	19.20	>100	-0.00	12.00	>100	V	>100
1609	4	-9	-0.01	25.60	>100	-0.00	16.00	>100	V	>100
1609	5	-9	-0.01	25.60	>100	-0.00	16.00	>100	V	>100
1609	6	-9	-0.01	25.60	>100	-0.00	16.00	>100	V	>100
1609	7	-9	-0.01	25.60	>100	-0.00	16.00	>100	V	>100
1609	(8+9)-V-4	-1412	-2.45	32.00	13	-0.59	20.00	34	V	13
1609	(8+9)-III-4	-1237	-2.15	32.00	15	-0.52	20.00	38	V	15
1609	(8+9)-I-4	-1330	-2.31	32.00	14	-0.56	20.00	36	V	14
1609	(8+9)-VII-4	-1319	-2.29	32.00	14	-0.55	20.00	36	V	14

Setto 15: origine (950.1,559.1,88.5), direzione (-0.612129,0.790758,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	(8+9)-VIII-4	4842	-3	-3179	3.77	-0.09	-8.39	132.00	192.00	192.00	14
0	(8+9)-IV-1	-4842	9	3280	-3.77	0.27	8.65	132.00	192.00	192.00	21
0	(8+9)-VI-4	4218	-5	-2757	3.28	-0.15	-7.27	132.00	192.00	192.00	16
0	(8+9)-III-2	6343	-16	-4124	4.94	-0.47	-10.88	132.00	192.00	192.00	10
0	(8+9)-IV-2	7569	-18	-4971	5.89	-0.52	-13.11	132.00	192.00	192.00	8.6
0	(8+9)-III-3	-6288	14	4181	-4.89	0.40	11.03	132.00	192.00	192.00	17
0	(8+9)-VIII-2	7623	-26	-5015	5.93	-0.76	-13.23	132.00	192.00	192.00	8.5
0	(8+9)-VII-2	6524	-44	-4269	5.08	-1.28	-11.26	132.00	192.00	192.00	9.6
0	(8+9)-VII-4	-2746	33	1850	-2.14	0.98	4.88	132.00	192.00	192.00	33
0	(8+9)-VII-1	2800	-36	-1793	2.18	-1.04	-4.73	132.00	192.00	192.00	21
0	(8+9)-I-2	6156	-17	-3997	4.79	-0.48	-10.54	132.00	192.00	192.00	11
0	(8+9)-VII-3	-6469	41	4326	-5.03	1.21	11.41	132.00	192.00	192.00	15
0	(8+9)-IV-3	-7514	16	5028	-5.85	0.46	13.26	132.00	192.00	192.00	14
0	(8+9)-II-2	6945	-20	-4550	5.40	-0.58	-12.00	132.00	192.00	192.00	9.4
0	(8+9)-IV-4	4897	-11	-3223	3.81	-0.33	-8.50	132.00	192.00	192.00	13
0	(8+9)-II-4	4273	-13	-2801	3.32	-0.39	-7.39	132.00	192.00	192.00	15
0	(8+9)-V-1	2988	-35	-1920	2.32	-1.02	-5.06	132.00	192.00	192.00	20
0	(8+9)-VIII-3	-7568	24	5072	-5.89	0.70	13.38	132.00	192.00	192.00	13
0	(8+9)-V-2	6336	-44	-4142	4.93	-1.29	-10.93	132.00	192.00	192.00	9.9
0	(8+9)-I-1	2807	-7	-1775	2.18	-0.21	-4.68	132.00	192.00	192.00	24
0	(8+9)-V-3	-6282	42	4199	-4.89	1.23	11.08	132.00	192.00	192.00	15
0	(8+9)-II-1	-4218	11	2858	-3.28	0.32	7.54	132.00	192.00	192.00	24
0	(8+9)-V-4	-2933	33	1977	-2.28	0.96	5.21	132.00	192.00	192.00	31
0	(8+9)-III-1	2620	-8	-1648	2.04	-0.23	-4.35	132.00	192.00	192.00	25
0	(8+9)-I-3	-6101	14	4054	-4.75	0.42	10.69	132.00	192.00	192.00	17
0	(8+9)-II-3	-6890	18	4607	-5.36	0.51	12.15	132.00	192.00	192.00	15
0	(8+9)-VIII-1	-4788	1	3236	-3.73	0.02	8.54	132.00	192.00	192.00	22
0	(8+9)-VI-1	-4163	3	2814	-3.24	0.08	7.42	132.00	192.00	192.00	25
0	(8+9)-VI-2	6999	-28	-4593	5.45	-0.82	-12.12	132.00	192.00	192.00	9.2
0	(8+9)-VI-3	-6944	26	4650	-5.40	0.76	12.27	132.00	192.00	192.00	15
3200	1	-241	-1	146	-0.19	-0.04	0.38	79.20	115.20	115.20	>100
3200	2	-542	-9	347	-0.42	-0.25	0.91	118.80	172.80	172.80	>100
3200	3	-542	-9	347	-0.42	-0.25	0.91	118.80	172.80	172.80	>100
3200	4	-241	-1	146	-0.19	-0.04	0.38	105.60	153.60	153.60	>100
3200	5	-241	-1	146	-0.19	-0.04	0.38	105.60	153.60	153.60	>100
3200	6	-241	-1	146	-0.19	-0.04	0.38	105.60	153.60	153.60	>100
3200	7	-241	-1	146	-0.19	-0.04	0.38	105.60	153.60	153.60	>100
3200	(8+9)-III-4	-578	-77	-1087	-0.45	-2.24	-2.87	132.00	192.00	192.00	38
3200	(8+9)-I-4	-609	-78	-1173	-0.47	-2.29	-3.09	132.00	192.00	192.00	36
Verifiche nella direzione secondaria											
0	1	-1734	20	-525	-1.12	0.73	-0.64	79.20	115.20	115.20	84
0	2	-3014	47	-1412	-1.95	1.73	-1.71	118.80	172.80	172.80	50
0	3	-3014	47	-1412	-1.95	1.73	-1.71	118.80	172.80	172.80	50
0	4	-1734	20	-525	-1.12	0.73	-0.64	105.60	153.60	153.60	>100
0	5	-1734	20	-525	-1.12	0.73	-0.64	105.60	153.60	153.60	>100
0	6	-1734	20	-525	-1.12	0.73	-0.64	105.60	153.60	153.60	>100
0	7	-1734	20	-525	-1.12	0.73	-0.64	105.60	153.60	153.60	>100
0	(8+9)-V-1	2345	-126	2734	1.51	-4.64	3.31	132.00	192.00	192.00	19
0	(8+9)-I-4	-4928	119	-3810	-3.18	4.41	-4.61	132.00	192.00	192.00	21
0	(8+9)-II-4	-3071	74	-6035	-1.98	2.75	-7.31	132.00	192.00	192.00	19
0	(8+9)-VII-4	-4625	147	-3368	-2.99	5.43	-4.08	132.00	192.00	192.00	20
0	(8+9)-III-1	2375	-90	3078	1.53	-3.34	3.73	132.00	192.00	192.00	21
0	(8+9)-VII-1	2208	-122	2685	1.43	-4.50	3.25	132.00	192.00	192.00	20
0	(8+9)-VI-4	-3021	84	-5917	-1.95	3.10	-7.16	132.00	192.00	192.00	19
0	(8+9)-VII-3	-4406	135	-399	-2.84	4.98	-0.48	132.00	192.00	192.00	35
0	(8+9)-II-1	654	-49	5351	0.42	-1.82	6.48	132.00	192.00	192.00	22
0	(8+9)-V-4	-4762	151	-3418	-3.07	5.57	-4.14	132.00	192.00	192.00	20
0	(8+9)-V-3	-4269	131	-350	-2.76	4.84	-0.42	132.00	192.00	192.00	36
0	(8+9)-III-4	-4792	116	-3761	-3.09	4.27	-4.55	132.00	192.00	192.00	22

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-I-1	2511	-94	3127	1.62	-3.48	3.79	132.00	192.00	192.00	20
1770	(8+9)-VIII-4	-2156	32	-8297	-1.39	1.17	-10.04	132.00	192.00	192.00	17
1770	(8+9)-IV-2	-875	18	-10374	-0.57	0.66	-12.56	132.00	192.00	192.00	15
1770	(8+9)-II-3	-1144	4	10221	-0.74	0.16	12.37	132.00	192.00	192.00	15
1770	(8+9)-IV-3	-1330	-5	11023	-0.86	-0.18	13.34	132.00	192.00	192.00	14
1770	(8+9)-II-2	-1061	9	-9571	-0.69	0.32	-11.59	132.00	192.00	192.00	16
1770	(8+9)-IV-1	-1140	-24	7338	-0.74	-0.90	8.88	132.00	192.00	192.00	20
1770	(8+9)-VII-2	2891	0	-3112	1.87	0.00	-3.77	132.00	192.00	192.00	30
1770	(8+9)-III-3	-1458	33	9123	-0.94	1.21	11.05	132.00	192.00	192.00	16
1770	(8+9)-I-3	-1402	35	8883	-0.91	1.31	10.75	132.00	192.00	192.00	16
1770	(8+9)-VI-1	137	-9	8145	0.09	-0.34	9.86	132.00	192.00	192.00	19
1770	(8+9)-I-2	-803	-22	-8233	-0.52	-0.83	-9.97	132.00	192.00	192.00	18
1770	(8+9)-V-2	2835	-3	-2871	1.83	-0.10	-3.48	132.00	192.00	192.00	31
1770	(8+9)-III-2	-747	-20	-8474	-0.48	-0.72	-10.26	132.00	192.00	192.00	17
1770	(8+9)-VI-2	30	15	-7963	0.02	0.54	-9.64	132.00	192.00	192.00	19
1770	(8+9)-IV-4	-1065	37	-6688	-0.69	1.39	-8.10	132.00	192.00	192.00	20
1770	(8+9)-VIII-1	-49	-19	8947	-0.03	-0.68	10.83	132.00	192.00	192.00	17
1770	(8+9)-VIII-2	216	24	-8765	0.14	0.88	-10.61	132.00	192.00	192.00	16
1770	(8+9)-VIII-3	-2421	-11	9415	-1.56	-0.40	11.40	132.00	192.00	192.00	16
1770	(8+9)-VI-3	-2235	-2	8612	-1.44	-0.06	10.43	132.00	192.00	192.00	18

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
1600	(8+9)-VI-2	93	0.05	6.40	Si	>100
1600	(8+9)-VI-3	-93	0.05	6.40	Si	>100
1600	(8+9)-VIII-2	97	0.05	6.40	Si	>100
1600	(8+9)-VIII-3	-96	0.05	6.40	Si	>100
3200	1	-3	0.00	3.84	Si	>100
3200	2	-16	0.01	5.76	Si	>100
3200	3	-16	0.01	5.76	Si	>100
3200	4	-3	0.00	5.12	Si	>100
3200	5	-3	0.00	5.12	Si	>100
3200	6	-3	0.00	5.12	Si	>100
3200	7	-3	0.00	5.12	Si	>100
3200	(8+9)-VI-1	185	0.10	6.40	Si	61
3200	(8+9)-VII-3	-363	0.21	6.40	Si	31
3200	(8+9)-II-2	-74	0.04	6.40	Si	>100
3200	(8+9)-VII-4	-397	0.22	6.40	Si	28
3200	(8+9)-II-4	-73	0.04	6.40	Si	>100
3200	(8+9)-VIII-1	169	0.10	6.40	Si	67
3200	(8+9)-III-2	-20	0.01	6.40	Si	>100
3200	(8+9)-I-2	-24	0.01	6.40	Si	>100
3200	(8+9)-III-4	-17	0.01	6.40	Si	>100
3200	(8+9)-I-1	19	0.01	6.40	Si	>100
3200	(8+9)-IV-2	-58	0.03	6.40	Si	>100
3200	(8+9)-VIII-4	-171	0.10	6.40	Si	66
3200	(8+9)-IV-4	-57	0.03	6.40	Si	>100
3200	(8+9)-II-3	72	0.04	6.40	Si	>100
3200	(8+9)-V-2	356	0.20	6.40	Si	32
3200	(8+9)-III-1	14	0.01	6.40	Si	>100
3200	(8+9)-V-4	-402	0.23	6.40	Si	28
3200	(8+9)-III-3	17	0.01	6.40	Si	>100
3200	(8+9)-I-4	-21	0.01	6.40	Si	>100
3200	(8+9)-IV-1	55	0.03	6.40	Si	>100
3200	(8+9)-VI-4	-187	0.11	6.40	Si	60
3200	(8+9)-IV-3	56	0.03	6.40	Si	>100
3200	(8+9)-VII-2	361	0.20	6.40	Si	31
3200	(8+9)-II-1	71	0.04	6.40	Si	>100
3200	(8+9)-I-3	22	0.01	6.40	Si	>100
3200	(8+9)-VII-1	395	0.22	6.40	Si	29
3200	(8+9)-V-3	-359	0.20	6.40	Si	32
3200	(8+9)-V-1	400	0.23	6.40	Si	28

X	Comb.	Ty	τ_d	fvd	RS	Cs
Verifiche nella direzione secondaria						
0	2	-23	0.01	5.76	Si	>100
0	3	-23	0.01	5.76	Si	>100
0	(8+9)-III-1	50	0.03	6.40	Si	>100
0	(8+9)-I-3	-28	0.02	6.40	Si	>100
0	(8+9)-IV-4	-44	0.03	6.40	Si	>100
0	(8+9)-I-4	-55	0.03	6.40	Si	>100
0	(8+9)-III-4	-51	0.03	6.40	Si	>100
0	(8+9)-II-1	57	0.03	6.40	Si	>100
0	(8+9)-I-1	54	0.03	6.40	Si	>100
0	(8+9)-IV-1	44	0.03	6.40	Si	>100
0	(8+9)-III-3	-32	0.02	6.40	Si	>100
0	(8+9)-I-2	27	0.02	6.40	Si	>100
0	(8+9)-III-2	31	0.02	6.40	Si	>100
0	(8+9)-II-3	33	0.02	6.40	Si	>100
0	(8+9)-II-4	-58	0.03	6.40	Si	>100
885	1	-5	0.00	3.84	Si	>100
885	4	-5	0.00	5.12	Si	>100
885	5	-5	0.00	5.12	Si	>100
885	6	-5	0.00	5.12	Si	>100
885	7	-5	0.00	5.12	Si	>100
885	(8+9)-II-2	-36	0.02	6.40	Si	>100
885	(8+9)-IV-2	-26	0.02	6.40	Si	>100
1770	(8+9)-VIII-4	72	0.04	6.40	Si	>100
1770	(8+9)-VI-1	-67	0.04	6.40	Si	>100
1770	(8+9)-VII-1	-309	0.18	6.40	Si	35
1770	(8+9)-V-1	-308	0.18	6.40	Si	35
1770	(8+9)-VII-2	-323	0.19	6.40	Si	33
1770	(8+9)-V-3	326	0.19	6.40	Si	33
1770	(8+9)-VII-3	325	0.19	6.40	Si	33
1770	(8+9)-IV-3	25	0.01	6.40	Si	>100
1770	(8+9)-VII-4	311	0.19	6.40	Si	35
1770	(8+9)-V-2	-324	0.19	6.40	Si	33
1770	(8+9)-V-4	310	0.18	6.40	Si	35
1770	(8+9)-VI-2	-121	0.07	6.40	Si	89
1770	(8+9)-VI-4	69	0.04	6.40	Si	>100
1770	(8+9)-VIII-1	-70	0.04	6.40	Si	>100
1770	(8+9)-VIII-2	-118	0.07	6.40	Si	91
1770	(8+9)-VIII-3	120	0.07	6.40	Si	90
1770	(8+9)-VI-3	123	0.07	6.40	Si	87

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	(8+9)-V-2	-4030	-4.70	32.00	6.8	-1.14	20.00	18	V	6.8
0	(8+9)-II-2	-4500	-5.25	32.00	6.1	-1.27	20.00	16	V	6.1
0	(8+9)-IV-1	3429	4.00	32.00	8.0	0.97	20.00	21	V	8.0
0	(8+9)-II-3	4772	5.57	32.00	5.7	1.35	20.00	15	V	5.7
0	(8+9)-VIII-2	-4963	-5.79	32.00	5.5	-1.40	20.00	14	V	5.5
0	(8+9)-VI-2	-4520	-5.28	32.00	6.1	-1.28	20.00	16	V	6.1
0	(8+9)-VII-2	-4163	-4.86	32.00	6.6	-1.18	20.00	17	V	6.6
0	(8+9)-III-1	-1585	-1.85	32.00	17	-0.45	20.00	45	V	17
0	(8+9)-VI-3	4791	5.59	32.00	5.7	1.35	20.00	15	V	5.7
0	(8+9)-III-2	-4097	-4.78	32.00	6.7	-1.16	20.00	17	V	6.7
0	(8+9)-I-2	-3964	-4.63	32.00	6.9	-1.12	20.00	18	V	6.9
0	(8+9)-III-3	4369	5.10	32.00	6.3	1.23	20.00	16	V	6.3
0	(8+9)-I-4	1990	2.32	32.00	14	0.56	20.00	36	V	14
0	(8+9)-III-4	1857	2.17	32.00	15	0.52	20.00	38	V	15
0	(8+9)-VIII-3	5235	6.11	32.00	5.2	1.48	20.00	14	V	5.2
0	(8+9)-VII-1	-1651	-1.93	32.00	17	-0.47	20.00	43	V	17
0	(8+9)-IV-2	-4944	-5.77	32.00	5.5	-1.40	20.00	14	V	5.5
0	(8+9)-I-3	4235	4.94	32.00	6.5	1.20	20.00	17	V	6.5
0	(8+9)-VII-3	4435	5.18	32.00	6.2	1.25	20.00	16	V	6.2

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
0	(8+9)-I-1	-1718	-2.01	32.00	16	-0.49	20.00	41	V	16
0	(8+9)-II-1	2986	3.49	32.00	9.2	0.84	20.00	24	V	9.2
0	(8+9)-IV-3	5215	6.09	32.00	5.3	1.47	20.00	14	V	5.3
0	(8+9)-V-3	4301	5.02	32.00	6.4	1.22	20.00	16	V	6.4
0	(8+9)-V-1	-1784	-2.08	32.00	15	-0.50	20.00	40	V	15
3200	1	-530	-0.62	19.20	31	-0.15	12.00	80	V	31
3200	2	-1106	-1.29	28.80	22	-0.31	18.00	58	V	22
3200	3	-1106	-1.29	28.80	22	-0.31	18.00	58	V	22
3200	4	-530	-0.62	25.60	41	-0.15	16.00	>100	V	41
3200	5	-530	-0.62	25.60	41	-0.15	16.00	>100	V	41
3200	6	-530	-0.62	25.60	41	-0.15	16.00	>100	V	41
3200	7	-530	-0.62	25.60	41	-0.15	16.00	>100	V	41
3200	(8+9)-VIII-4	-4344	-5.07	32.00	6.3	-1.23	20.00	16	V	6.3
3200	(8+9)-VI-4	-4146	-4.84	32.00	6.6	-1.17	20.00	17	V	6.6
3200	(8+9)-II-4	-3685	-4.30	32.00	7.4	-1.04	20.00	19	V	7.4
3200	(8+9)-VII-4	-2189	-2.55	32.00	13	-0.62	20.00	32	V	13
3200	(8+9)-VIII-1	3624	4.23	32.00	7.6	1.02	20.00	20	V	7.6
3200	(8+9)-VI-1	3427	4.00	32.00	8.0	0.97	20.00	21	V	8.0
3200	(8+9)-V-4	-2130	-2.49	32.00	13	-0.60	20.00	33	V	13
3200	(8+9)-IV-4	-3883	-4.53	32.00	7.1	-1.10	20.00	18	V	7.1
Verifiche nella direzione secondaria										
885	1	252	0.16	19.20	>100	0.04	12.00	>100	V	>100
885	2	529	0.34	28.80	84	0.08	18.00	>100	V	84
885	3	529	0.34	28.80	84	0.08	18.00	>100	V	84
885	4	252	0.16	25.60	>100	0.04	16.00	>100	V	>100
885	5	252	0.16	25.60	>100	0.04	16.00	>100	V	>100
885	6	252	0.16	25.60	>100	0.04	16.00	>100	V	>100
885	7	252	0.16	25.60	>100	0.04	16.00	>100	V	>100
885	(8+9)-VIII-4	6346	4.10	32.00	7.8	0.99	20.00	20	V	7.8
885	(8+9)-IV-2	9785	6.32	32.00	5.1	1.53	20.00	13	V	5.1
885	(8+9)-V-1	3932	2.54	32.00	13	0.61	20.00	33	V	13
885	(8+9)-I-2	7888	5.09	32.00	6.3	1.23	20.00	16	V	6.3
885	(8+9)-V-2	8214	5.30	32.00	6.0	1.28	20.00	16	V	6.0
885	(8+9)-I-4	-3249	-2.10	32.00	15	-0.51	20.00	39	V	15
885	(8+9)-V-3	-7856	-5.07	32.00	6.3	-1.23	20.00	16	V	6.3
885	(8+9)-II-2	8985	5.80	32.00	5.5	1.40	20.00	14	V	5.5
885	(8+9)-V-4	-3575	-2.31	32.00	14	-0.56	20.00	36	V	14
885	(8+9)-II-4	5644	3.64	32.00	8.8	0.88	20.00	23	V	8.8
885	(8+9)-VI-1	-5188	-3.35	32.00	9.6	-0.81	20.00	25	V	9.6
885	(8+9)-III-2	8128	5.25	32.00	6.1	1.27	20.00	16	V	6.1
885	(8+9)-VI-2	9082	5.86	32.00	5.5	1.42	20.00	14	V	5.5
885	(8+9)-III-4	-3009	-1.94	32.00	16	-0.47	20.00	43	V	16
885	(8+9)-VI-3	-8724	-5.63	32.00	5.7	-1.36	20.00	15	V	5.7
885	(8+9)-I-1	3607	2.33	32.00	14	0.56	20.00	35	V	14
885	(8+9)-VI-4	5546	3.58	32.00	8.9	0.87	20.00	23	V	8.9
885	(8+9)-IV-4	6444	4.16	32.00	7.7	1.01	20.00	20	V	7.7
885	(8+9)-VII-1	3692	2.38	32.00	13	0.58	20.00	35	V	13
885	(8+9)-II-1	-5286	-3.41	32.00	9.4	-0.83	20.00	24	V	9.4
885	(8+9)-VII-2	8454	5.46	32.00	5.9	1.32	20.00	15	V	5.9
885	(8+9)-III-1	3367	2.17	32.00	15	0.53	20.00	38	V	15
885	(8+9)-VII-3	-8096	-5.23	32.00	6.1	-1.26	20.00	16	V	6.1
885	(8+9)-IV-1	-6086	-3.93	32.00	8.1	-0.95	20.00	21	V	8.1
885	(8+9)-VII-4	-3334	-2.15	32.00	15	-0.52	20.00	38	V	15
885	(8+9)-III-3	-7770	-5.02	32.00	6.4	-1.21	20.00	16	V	6.4
885	(8+9)-IV-3	-9427	-6.09	32.00	5.3	-1.47	20.00	14	V	5.3
885	(8+9)-II-3	-8627	-5.57	32.00	5.7	-1.35	20.00	15	V	5.7
885	(8+9)-VIII-1	-5988	-3.87	32.00	8.3	-0.94	20.00	21	V	8.3
885	(8+9)-VIII-2	9883	6.38	32.00	5.0	1.54	20.00	13	V	5.0
885	(8+9)-VIII-3	-9525	-6.15	32.00	5.2	-1.49	20.00	13	V	5.2
885	(8+9)-I-3	-7530	-4.86	32.00	6.6	-1.18	20.00	17	V	6.6

Setto 16: origine (950.1,559.1,296.9), direzione (-0.612129,0.790758,0)
 Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	1	104	-1	-127	0.29	-0.12	-4.23	79.20	115.20	115.20	24
0	2	79	-1	-217	0.22	-0.07	-7.21	118.80	172.80	172.80	23
0	3	79	-1	-217	0.22	-0.07	-7.21	118.80	172.80	172.80	23
0	4	104	-1	-127	0.29	-0.12	-4.23	105.60	153.60	153.60	32
0	5	104	-1	-127	0.29	-0.12	-4.23	105.60	153.60	153.60	32
0	6	104	-1	-127	0.29	-0.12	-4.23	105.60	153.60	153.60	32
0	7	104	-1	-127	0.29	-0.12	-4.23	105.60	153.60	153.60	32
0	(8+9)-VIII-4	-7286	279	-699	-20.14	28.95	-23.28	132.00	192.00	192.00	3.5
0	(8+9)-IV-1	7501	-212	542	20.73	-22.01	18.04	132.00	192.00	192.00	2.7
0	(8+9)-V-1	-4600	144	-446	-12.72	14.98	-14.84	132.00	192.00	192.00	6.3
0	(8+9)-I-2	-9669	385	-823	-26.72	40.00	-27.39	132.00	192.00	192.00	2.7
0	(8+9)-V-2	-9868	157	-883	-27.28	16.28	-29.39	132.00	192.00	192.00	3.9
0	(8+9)-I-4	4556	-374	210	12.59	-38.88	7.00	132.00	192.00	192.00	3.0
0	(8+9)-V-3	10024	-159	708	27.71	-16.46	23.56	132.00	192.00	192.00	2.4
0	(8+9)-II-2	-10836	134	-972	-29.95	13.91	-32.33	132.00	192.00	192.00	3.8
0	(8+9)-V-4	4756	-146	271	13.14	-15.16	9.00	132.00	192.00	192.00	4.4
0	(8+9)-VIII-1	7441	-281	524	20.57	-29.13	17.44	132.00	192.00	192.00	2.5
0	(8+9)-III-1	-4168	281	-369	-11.52	29.22	-12.28	132.00	192.00	192.00	4.6
0	(8+9)-III-2	-9902	477	-840	-27.37	49.48	-27.95	132.00	192.00	192.00	2.4
0	(8+9)-III-4	4323	-283	194	11.95	-29.40	6.44	132.00	192.00	192.00	3.6
0	(8+9)-VI-2	-10896	65	-990	-30.12	6.80	-32.93	132.00	192.00	192.00	4.3
0	(8+9)-IV-2	-11613	438	-1028	-32.10	45.50	-34.19	132.00	192.00	192.00	2.3
0	(8+9)-VI-3	11051	-67	814	30.55	-6.98	27.10	132.00	192.00	192.00	2.4
0	(8+9)-IV-4	-7345	210	-718	-20.30	21.83	-23.88	132.00	192.00	192.00	4.0
0	(8+9)-VIII-2	-11673	370	-1046	-32.26	38.38	-34.80	132.00	192.00	192.00	2.4
0	(8+9)-VIII-3	11828	-371	870	32.69	-38.56	28.96	132.00	192.00	192.00	1.7
0	(8+9)-VII-1	-4367	53	-429	-12.07	5.51	-14.28	132.00	192.00	192.00	9.3
0	(8+9)-III-3	10057	-478	664	27.80	-49.66	22.11	132.00	192.00	192.00	1.7
0	(8+9)-IV-3	11768	-440	852	32.53	-45.67	28.36	132.00	192.00	192.00	1.6
0	(8+9)-I-3	9824	-387	648	27.15	-40.18	21.55	132.00	192.00	192.00	1.9
0	(8+9)-II-3	10991	-136	796	30.38	-14.09	26.50	132.00	192.00	192.00	2.3
0	(8+9)-I-1	-4401	373	-386	-12.16	38.70	-12.83	132.00	192.00	192.00	3.7
0	(8+9)-VII-2	-10101	248	-900	-27.92	25.76	-29.95	132.00	192.00	192.00	3.2
0	(8+9)-VII-3	10257	-250	725	28.35	-25.94	24.12	132.00	192.00	192.00	2.1
0	(8+9)-VII-4	4523	-55	254	12.50	-5.69	8.45	132.00	192.00	192.00	5.9
3200	(8+9)-II-4	-6077	788	802	-7.53	36.69	5.36	132.00	192.00	192.00	4.5
3200	(8+9)-VI-4	-6024	609	762	-7.46	28.36	5.10	132.00	192.00	192.00	5.7
3200	(8+9)-II-1	5048	-788	-1307	6.26	-36.70	-8.74	132.00	192.00	192.00	3.5
3200	(8+9)-VI-1	4995	-609	-1267	6.19	-28.37	-8.47	132.00	192.00	192.00	4.2
Verifiche nella direzione secondaria											
0	(8+9)-VIII-4	-843	24	4515	-0.54	0.88	5.47	132.00	192.00	192.00	30
0	(8+9)-VI-2	-759	18	6376	-0.49	0.67	7.72	132.00	192.00	192.00	23
0	(8+9)-VI-4	-966	16	3956	-0.62	0.60	4.79	132.00	192.00	192.00	36
0	(8+9)-IV-2	-601	13	6887	-0.39	0.47	8.34	132.00	192.00	192.00	22
0	(8+9)-III-2	-586	-27	5794	-0.38	-1.01	7.01	132.00	192.00	192.00	24
0	(8+9)-VIII-2	-636	26	6935	-0.41	0.95	8.40	132.00	192.00	192.00	21
0	(8+9)-III-3	-1778	43	-5212	-1.15	1.57	-6.31	132.00	192.00	192.00	24
0	(8+9)-VII-4	-1394	10	-2112	-0.90	0.37	-2.56	132.00	192.00	192.00	66
0	(8+9)-VI-3	-1605	-3	-5794	-1.04	-0.10	-7.01	132.00	192.00	192.00	27
0	(8+9)-VII-2	-704	16	5955	-0.45	0.58	7.21	132.00	192.00	192.00	25
0	(8+9)-IV-1	-1485	-21	-3981	-0.96	-0.79	-4.82	132.00	192.00	192.00	34
0	(8+9)-I-3	-1741	45	-5044	-1.12	1.66	-6.11	132.00	192.00	192.00	25
0	(8+9)-II-1	-1362	-14	-3422	-0.88	-0.51	-4.14	132.00	192.00	192.00	41
0	(8+9)-IV-3	-1763	3	-6305	-1.14	0.10	-7.63	132.00	192.00	192.00	25
0	(8+9)-II-3	-1640	10	-5745	-1.06	0.37	-6.96	132.00	192.00	192.00	26
0	(8+9)-IV-4	-879	37	4563	-0.57	1.36	5.52	132.00	192.00	192.00	28
0	(8+9)-VIII-3	-1728	-10	-6353	-1.12	-0.38	-7.69	132.00	192.00	192.00	24
0	(8+9)-V-1	-932	8	2862	-0.60	0.28	3.46	132.00	192.00	192.00	51
0	(8+9)-VII-3	-1660	-0	-5373	-1.07	-0.01	-6.50	132.00	192.00	192.00	29
0	(8+9)-V-2	-741	13	5787	-0.48	0.50	7.01	132.00	192.00	192.00	26
0	(8+9)-VII-1	-969	5	2694	-0.63	0.20	3.26	132.00	192.00	192.00	55
0	(8+9)-II-4	-1001	29	4004	-0.65	1.08	4.85	132.00	192.00	192.00	32
0	(8+9)-VIII-1	-1520	-9	-3933	-0.98	-0.32	-4.76	132.00	192.00	192.00	38

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-I-2	-623	-30	5626	-0.40	-1.09	6.81	132.00	192.00	192.00	24
0	(8+9)-II-2	-723	5	6327	-0.47	0.19	7.66	132.00	192.00	192.00	24
0	(8+9)-V-3	-1623	2	-5205	-1.05	0.07	-6.30	132.00	192.00	192.00	30
0	(8+9)-V-4	-1431	8	-2280	-0.92	0.28	-2.76	132.00	192.00	192.00	63
0	(8+9)-VI-1	-1398	-1	-3373	-0.90	-0.04	-4.08	132.00	192.00	192.00	47
556	1	-1146	7	-451	-0.82	0.29	-0.66	79.20	115.20	115.20	>100
556	2	-2000	12	-831	-1.43	0.49	-1.23	118.80	172.80	172.80	100
556	3	-2000	12	-831	-1.43	0.49	-1.23	118.80	172.80	172.80	100
556	4	-1146	7	-451	-0.82	0.29	-0.66	105.60	153.60	153.60	>100
556	5	-1146	7	-451	-0.82	0.29	-0.66	105.60	153.60	153.60	>100
556	6	-1146	7	-451	-0.82	0.29	-0.66	105.60	153.60	153.60	>100
556	7	-1146	7	-451	-0.82	0.29	-0.66	105.60	153.60	153.60	>100
556	(8+9)-I-1	-722	110	338	-0.51	4.49	0.50	132.00	192.00	192.00	38
556	(8+9)-I-4	-844	-100	-961	-0.60	-4.09	-1.42	132.00	192.00	192.00	35
556	(8+9)-III-1	-739	116	284	-0.53	4.75	0.42	132.00	192.00	192.00	37
556	(8+9)-III-4	-827	-107	-907	-0.59	-4.35	-1.34	132.00	192.00	192.00	34

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Ty kg	τ_d kg/cm ²	fvd kg/cm ²	RS	Cs
0	(8+9)-VI-4	-114	0.23	6.40	Si	28
0	(8+9)-V-1	12	0.02	6.40	Si	>100
0	(8+9)-IV-4	-101	0.20	6.40	Si	31
0	(8+9)-II-2	-96	0.19	6.40	Si	33
0	(8+9)-VIII-3	84	0.17	6.40	Si	38
0	(8+9)-II-3	96	0.19	6.40	Si	33
0	(8+9)-VIII-1	69	0.14	6.40	Si	46
0	(8+9)-II-4	-146	0.29	6.40	Si	22
0	(8+9)-VII-2	-48	0.10	6.40	Si	67
0	(8+9)-VIII-4	-69	0.14	6.40	Si	46
0	(8+9)-VI-2	-129	0.26	6.40	Si	25
0	(8+9)-V-4	-11	0.02	6.40	Si	>100
0	(8+9)-V-3	62	0.12	6.40	Si	52
0	(8+9)-VIII-2	-84	0.17	6.40	Si	38
0	(8+9)-V-2	-61	0.12	6.40	Si	52
0	(8+9)-VI-3	129	0.26	6.40	Si	25
0	(8+9)-II-1	147	0.30	6.40	Si	22
0	(8+9)-VII-3	48	0.10	6.40	Si	66
0	(8+9)-VI-1	114	0.23	6.40	Si	28
0	(8+9)-IV-1	102	0.20	6.40	Si	31
0	(8+9)-IV-2	-51	0.10	6.40	Si	63
0	(8+9)-IV-3	51	0.10	6.40	Si	62
1600	(8+9)-III-1	-242	0.30	6.40	Si	21
1600	(8+9)-III-2	-185	0.23	6.40	Si	28
1600	(8+9)-III-4	242	0.30	6.40	Si	21
1600	(8+9)-III-3	185	0.23	6.40	Si	28
1600	(8+9)-I-4	221	0.27	6.40	Si	23
1600	(8+9)-I-3	206	0.26	6.40	Si	25
1600	(8+9)-I-2	-206	0.26	6.40	Si	25
1600	(8+9)-I-1	-221	0.27	6.40	Si	23
3200	1	-7	0.01	3.84	Si	>100
3200	2	-13	0.01	5.76	Si	>100
3200	3	-13	0.01	5.76	Si	>100
3200	4	-7	0.01	5.12	Si	>100
3200	5	-7	0.01	5.12	Si	>100
3200	6	-7	0.01	5.12	Si	>100
3200	7	-7	0.01	5.12	Si	>100
3200	(8+9)-VII-1	-51	0.05	6.40	Si	>100
3200	(8+9)-VII-4	42	0.04	6.40	Si	>100
Verifiche nella direzione secondaria						
0	(8+9)-II-2	-67	0.04	6.40	Si	>100
0	(8+9)-VII-3	35	0.02	6.40	Si	>100
0	(8+9)-VI-3	141	0.08	6.40	Si	76

X	Comb.	Ty	τ_d	fvd	RS	Cs
0	(8+9)-VI-2	-131	0.08	6.40	Si	82
0	(8+9)-IV-3	62	0.04	6.40	Si	>100
0	(8+9)-IV-2	-52	0.03	6.40	Si	>100
0	(8+9)-II-3	77	0.05	6.40	Si	>100
556	1	8	0.01	3.84	Si	>100
556	2	12	0.01	5.76	Si	>100
556	3	12	0.01	5.76	Si	>100
556	4	8	0.01	5.12	Si	>100
556	5	8	0.01	5.12	Si	>100
556	6	8	0.01	5.12	Si	>100
556	7	8	0.01	5.12	Si	>100
556	(8+9)-VIII-4	-164	0.11	6.40	Si	59
556	(8+9)-V-1	119	0.08	6.40	Si	82
556	(8+9)-I-2	341	0.22	6.40	Si	29
556	(8+9)-VI-1	146	0.10	6.40	Si	67
556	(8+9)-III-2	332	0.22	6.40	Si	29
556	(8+9)-II-1	233	0.15	6.40	Si	42
556	(8+9)-III-4	-408	0.27	6.40	Si	24
556	(8+9)-I-4	-399	0.26	6.40	Si	24
556	(8+9)-III-1	420	0.28	6.40	Si	23
556	(8+9)-VI-4	-134	0.09	6.40	Si	73
556	(8+9)-IV-4	-251	0.17	6.40	Si	39
556	(8+9)-VII-1	128	0.08	6.40	Si	76
556	(8+9)-V-2	49	0.03	6.40	Si	>100
556	(8+9)-VII-2	40	0.03	6.40	Si	>100
556	(8+9)-V-4	-107	0.07	6.40	Si	91
556	(8+9)-I-3	-329	0.22	6.40	Si	30
556	(8+9)-IV-1	263	0.17	6.40	Si	37
556	(8+9)-VII-4	-116	0.08	6.40	Si	84
556	(8+9)-III-3	-320	0.21	6.40	Si	30
556	(8+9)-II-4	-222	0.15	6.40	Si	44
556	(8+9)-V-3	-38	0.02	6.40	Si	>100
556	(8+9)-VIII-1	175	0.12	6.40	Si	55
556	(8+9)-VIII-2	-117	0.08	6.40	Si	83
556	(8+9)-VIII-3	128	0.08	6.40	Si	76
556	(8+9)-I-1	411	0.27	6.40	Si	24

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Tx kg	τ_{vd} kg/cmq	fvd kg/cmq	Csv	τ_M kg/cmq	fTd kg/cmq	Csm	Mecc.	Cs
0	(8+9)-VIII-4	-1385	-5.74	32.00	5.6	-1.39	20.00	14	V	5.6
0	(8+9)-IV-1	916	3.80	32.00	8.4	0.92	20.00	22	V	8.4
0	(8+9)-VI-2	-1918	-7.95	32.00	4.0	-1.92	20.00	10	V	4.0
0	(8+9)-III-1	-834	-3.46	32.00	9.3	-0.84	20.00	24	V	9.3
0	(8+9)-IV-2	-2026	-8.40	32.00	3.8	-2.03	20.00	9.8	V	3.8
0	(8+9)-III-2	-1717	-7.12	32.00	4.5	-1.72	20.00	12	V	4.5
0	(8+9)-VIII-2	-2050	-8.50	32.00	3.8	-2.06	20.00	9.7	V	3.8
0	(8+9)-III-3	1224	5.08	32.00	6.3	1.23	20.00	16	V	6.3
0	(8+9)-VII-3	1303	5.40	32.00	5.9	1.31	20.00	15	V	5.9
0	(8+9)-VII-1	-913	-3.79	32.00	8.5	-0.92	20.00	22	V	8.5
0	(8+9)-I-2	-1677	-6.95	32.00	4.6	-1.68	20.00	12	V	4.6
0	(8+9)-VI-4	-1253	-5.20	32.00	6.2	-1.26	20.00	16	V	6.2
0	(8+9)-VII-2	-1796	-7.45	32.00	4.3	-1.80	20.00	11	V	4.3
0	(8+9)-II-2	-1895	-7.86	32.00	4.1	-1.90	20.00	11	V	4.1
0	(8+9)-IV-3	1534	6.36	32.00	5.0	1.54	20.00	13	V	5.0
0	(8+9)-II-4	-1277	-5.30	32.00	6.0	-1.28	20.00	16	V	6.0
0	(8+9)-IV-4	-1409	-5.84	32.00	5.5	-1.41	20.00	14	V	5.5
0	(8+9)-VIII-1	893	3.70	32.00	8.6	0.90	20.00	22	V	8.6
0	(8+9)-V-1	-952	-3.95	32.00	8.1	-0.96	20.00	21	V	8.1
0	(8+9)-I-3	1185	4.91	32.00	6.5	1.19	20.00	17	V	6.5
0	(8+9)-V-2	-1756	-7.28	32.00	4.4	-1.76	20.00	11	V	4.4
0	(8+9)-II-3	1402	5.81	32.00	5.5	1.41	20.00	14	V	5.5
0	(8+9)-I-1	-873	-3.62	32.00	8.8	-0.88	20.00	23	V	8.8

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
0	(8+9)-II-1	785	3.25	32.00	9.8	0.79	20.00	25	V	9.8
0	(8+9)-VIII-3	1558	6.46	32.00	5.0	1.56	20.00	13	V	5.0
0	(8+9)-V-3	1264	5.24	32.00	6.1	1.27	20.00	16	V	6.1
0	(8+9)-VI-3	1426	5.91	32.00	5.4	1.43	20.00	14	V	5.4
0	(8+9)-VI-1	761	3.16	32.00	10	0.76	20.00	26	V	10
3200	1	809	1.50	19.20	13	0.36	12.00	33	V	13
3200	2	1330	2.47	28.80	12	0.60	18.00	30	V	12
3200	3	1330	2.47	28.80	12	0.60	18.00	30	V	12
3200	4	809	1.50	25.60	17	0.36	16.00	44	V	17
3200	5	809	1.50	25.60	17	0.36	16.00	44	V	17
3200	6	809	1.50	25.60	17	0.36	16.00	44	V	17
3200	7	809	1.50	25.60	17	0.36	16.00	44	V	17
3200	(8+9)-VII-4	1275	2.37	32.00	13	0.57	20.00	35	V	13
3200	(8+9)-I-4	1271	2.36	32.00	14	0.57	20.00	35	V	14
3200	(8+9)-III-4	1221	2.27	32.00	14	0.55	20.00	36	V	14
3200	(8+9)-V-4	1326	2.46	32.00	13	0.60	20.00	34	V	13
Verifiche nella direzione secondaria										
556	1	-867	-0.62	19.20	31	-0.15	12.00	80	V	31
556	2	-1464	-1.04	28.80	28	-0.25	18.00	71	V	28
556	3	-1464	-1.04	28.80	28	-0.25	18.00	71	V	28
556	4	-867	-0.62	25.60	41	-0.15	16.00	>100	V	41
556	5	-867	-0.62	25.60	41	-0.15	16.00	>100	V	41
556	6	-867	-0.62	25.60	41	-0.15	16.00	>100	V	41
556	7	-867	-0.62	25.60	41	-0.15	16.00	>100	V	41
556	(8+9)-VIII-4	4818	3.43	32.00	9.3	0.83	20.00	24	V	9.3
556	(8+9)-IV-2	7793	5.55	32.00	5.8	1.34	20.00	15	V	5.8
556	(8+9)-V-1	2560	1.82	32.00	18	0.44	20.00	45	V	18
556	(8+9)-I-2	6151	4.38	32.00	7.3	1.06	20.00	19	V	7.3
556	(8+9)-V-2	6326	4.51	32.00	7.1	1.09	20.00	18	V	7.1
556	(8+9)-I-4	-3589	-2.56	32.00	13	-0.62	20.00	32	V	13
556	(8+9)-V-3	-7530	-5.37	32.00	6.0	-1.30	20.00	15	V	6.0
556	(8+9)-II-2	7135	5.09	32.00	6.3	1.23	20.00	16	V	6.3
556	(8+9)-V-4	-3764	-2.68	32.00	12	-0.65	20.00	31	V	12
556	(8+9)-II-4	4213	3.00	32.00	11	0.73	20.00	28	V	11
556	(8+9)-VI-1	-5365	-3.82	32.00	8.4	-0.93	20.00	22	V	8.4
556	(8+9)-III-2	6348	4.52	32.00	7.1	1.09	20.00	18	V	7.1
556	(8+9)-VI-2	7188	5.12	32.00	6.2	1.24	20.00	16	V	6.2
556	(8+9)-III-4	-3392	-2.42	32.00	13	-0.58	20.00	34	V	13
556	(8+9)-VI-3	-8392	-5.98	32.00	5.4	-1.45	20.00	14	V	5.4
556	(8+9)-I-1	2385	1.70	32.00	19	0.41	20.00	49	V	19
556	(8+9)-VI-4	4161	2.97	32.00	11	0.72	20.00	28	V	11
556	(8+9)-IV-4	4871	3.47	32.00	9.2	0.84	20.00	24	V	9.2
556	(8+9)-VII-1	2363	1.68	32.00	19	0.41	20.00	49	V	19
556	(8+9)-II-1	-5418	-3.86	32.00	8.3	-0.93	20.00	21	V	8.3
556	(8+9)-VII-2	6523	4.65	32.00	6.9	1.13	20.00	18	V	6.9
556	(8+9)-III-1	2188	1.56	32.00	21	0.38	20.00	53	V	21
556	(8+9)-VII-3	-7727	-5.51	32.00	5.8	-1.33	20.00	15	V	5.8
556	(8+9)-IV-1	-6075	-4.33	32.00	7.4	-1.05	20.00	19	V	7.4
556	(8+9)-VII-4	-3567	-2.54	32.00	13	-0.62	20.00	33	V	13
556	(8+9)-III-3	-7552	-5.38	32.00	5.9	-1.30	20.00	15	V	5.9
556	(8+9)-IV-3	-8997	-6.41	32.00	5.0	-1.55	20.00	13	V	5.0
556	(8+9)-II-3	-8340	-5.94	32.00	5.4	-1.44	20.00	14	V	5.4
556	(8+9)-VIII-1	-6022	-4.29	32.00	7.5	-1.04	20.00	19	V	7.5
556	(8+9)-VIII-2	7845	5.59	32.00	5.7	1.35	20.00	15	V	5.7
556	(8+9)-VIII-3	-9049	-6.45	32.00	5.0	-1.56	20.00	13	V	5.0
556	(8+9)-I-3	-7355	-5.24	32.00	6.1	-1.27	20.00	16	V	6.1

Verifiche a instabilità

Setto(X)	Comb.	k _{critc}	k _{critm}	λ_{relc}	λ_{relm}	σ_n	σ_{mx}	σ_{my}	f _{td}	f _{cd}	f _{md}	Cs
(cm)						kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	
13(20.	(8+9)-IV-3	--	--	--	--	2.92	13.98	-11.26	132.00	192.00	192.00	6.5

Setto(X)	Comb.	k _{critc}	k _{critm}	λ _{relc}	λ _{relm}	σ _n	σ _{mx}	σ _{my}	ftd	fcd	fmd	Cs
0)												
14(119.0)	(8+9)-IV-3	--	--	--	--	1.83	-7.12	-12.41	132.00	192.00	192.00	8.7
15(0.0)	(8+9)-VIII-3	0.63	--	1.16	--	-5.89	0.70	13.38	132.00	192.00	192.00	8.2
16(0.0)	(8+9)-IV-2	0.63	--	1.16	--	-32.10	45.50	-34.19	132.00	192.00	192.00	1.5

Parete Xlam 9 - Nodi: [14-12-102-103] - **Crit.Prog.** Criterio di verifica XLAM 0 - **Verificato:**
[Cs=1.472,Comb=(8+9)-IV-2]

Geometria setti

Setto	Crit.	X mm	L cm	S cm	X90 mm	L90 cm	S90 cm
13	Criterio di verifica XLAM 0	0	383.2	12.1	0	20.0	12.1
		100	385.1	12.1	1935	20.0	12.1
		200	387.0	12.1	--	--	--
14	Criterio di verifica XLAM 0	0	299.0	12.1	0	119.0	12.1
		595	310.4	12.1	1609	119.0	12.1
		1190	321.8	12.1	--	--	--
15	Criterio di verifica XLAM 0	0	177.0	12.1	0	320.0	12.1
		1600	177.0	12.1	885	320.0	12.1
		3200	177.0	12.1	1770	320.0	12.1
16	Criterio di verifica XLAM 0	0	49.8	12.1	0	320.0	12.1
		1600	80.5	12.1	556	289.9	12.1
		3200	111.1	12.1	--	--	--

Setto 13: origine (754.3,812.2,191.6), direzione (-0.612129,0.790758,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X mm	Comb.	N kg	M _x kg*m	M _y kg*m	σ _n kg/cmq	σ _{mx} kg/cmq	σ _{my} kg/cmq	ftd kg/cmq	fcd kg/cmq	fmd kg/cmq	Cs
0	1	-994	-2	556	-0.36	-0.02	0.31	79.20	115.20	115.20	>100
0	4	-994	-2	556	-0.36	-0.02	0.31	105.60	153.60	153.60	>100
0	5	-994	-2	556	-0.36	-0.02	0.31	105.60	153.60	153.60	>100
0	6	-994	-2	556	-0.36	-0.02	0.31	105.60	153.60	153.60	>100
0	7	-994	-2	556	-0.36	-0.02	0.31	105.60	153.60	153.60	>100
0	(8+9)-V-1	-3718	-413	8323	-1.34	-5.58	4.68	132.00	192.00	192.00	19
0	(8+9)-V-4	2360	412	-7567	0.85	5.56	-4.26	132.00	192.00	192.00	17
0	(8+9)-VII-4	2216	57	-7154	0.80	0.77	-4.03	132.00	192.00	192.00	32
0	(8+9)-V-2	-7772	-120	17077	-2.79	-1.63	9.61	132.00	192.00	192.00	17
0	(8+9)-V-3	6414	119	-16321	2.31	1.61	-9.19	132.00	192.00	192.00	14
0	(8+9)-VII-1	-3574	-58	7910	-1.28	-0.79	4.45	132.00	192.00	192.00	37
100	(8+9)-VII-2	-7924	-481	17830	-2.83	-6.47	9.94	132.00	192.00	192.00	12
100	(8+9)-II-2	-9048	277	19184	-3.24	3.72	10.69	132.00	192.00	192.00	13
100	(8+9)-II-3	7689	-280	-18484	2.75	-3.76	-10.30	132.00	192.00	192.00	11
100	(8+9)-VI-1	4516	-604	-11060	1.62	-8.11	-6.16	132.00	192.00	192.00	12
100	(8+9)-VI-4	-5875	601	11761	-2.10	8.08	6.55	132.00	192.00	192.00	13
100	(8+9)-VII-3	6565	479	-17130	2.35	6.43	-9.55	132.00	192.00	192.00	9.9
200	2	-1879	-17	838	-0.67	-0.23	0.46	118.80	172.80	172.80	>100
200	3	-1879	-17	838	-0.67	-0.23	0.46	118.80	172.80	172.80	>100
200	(8+9)-VIII-4	-6350	-721	13615	-2.26	-9.64	7.51	132.00	192.00	192.00	11
200	(8+9)-IV-1	5017	523	-13014	1.79	6.99	-7.18	132.00	192.00	192.00	11
200	(8+9)-VI-3	7710	-457	-19005	2.74	-6.11	-10.49	132.00	192.00	192.00	9.3
200	(8+9)-IV-2	-9569	-1049	21049	-3.41	-14.03	11.62	132.00	192.00	192.00	7.5
200	(8+9)-II-1	4491	-785	-11571	1.60	-10.50	-6.39	132.00	192.00	192.00	10.0
200	(8+9)-IV-4	-6375	-527	13656	-2.27	-7.04	7.54	132.00	192.00	192.00	13
200	(8+9)-I-4	2615	1026	-7323	0.93	13.72	-4.04	132.00	192.00	192.00	10
200	(8+9)-III-3	6833	1105	-17109	2.43	14.78	-9.44	132.00	192.00	192.00	6.9
200	(8+9)-I-3	6675	713	-16676	2.38	9.53	-9.20	132.00	192.00	192.00	8.7
200	(8+9)-III-1	-3815	-637	7533	-1.36	-8.52	4.16	132.00	192.00	192.00	15
200	(8+9)-I-2	-8033	-716	17319	-2.86	-9.58	9.56	132.00	192.00	192.00	10
200	(8+9)-VI-2	-9069	453	19648	-3.23	6.06	10.84	132.00	192.00	192.00	11

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
200	(8+9)-I-1	-3973	-1030	7965	-1.41	-13.77	4.40	132.00	192.00	192.00	11
200	(8+9)-II-4	-5849	781	12214	-2.08	10.45	6.74	132.00	192.00	192.00	11
200	(8+9)-IV-3	8211	1046	-20406	2.92	13.98	-11.26	132.00	192.00	192.00	6.5
200	(8+9)-III-2	-8191	-1109	17751	-2.92	-14.83	9.80	132.00	192.00	192.00	7.8
200	(8+9)-VIII-1	4992	717	-12972	1.78	9.59	-7.16	132.00	192.00	192.00	9.9
200	(8+9)-VIII-2	-9594	-855	21090	-3.41	-11.43	11.64	132.00	192.00	192.00	8.3
200	(8+9)-VIII-3	8236	851	-20447	2.93	11.38	-11.28	132.00	192.00	192.00	7.1
200	(8+9)-III-4	2457	633	-6890	0.87	8.47	-3.80	132.00	192.00	192.00	14
Verifiche nella direzione secondaria											
0	1	-640	4	35	-6.61	2.44	10.81	79.20	115.20	115.20	8.5
0	2	-1296	11	68	-13.39	6.59	20.97	118.80	172.80	172.80	6.0
0	3	-1296	11	68	-13.39	6.59	20.97	118.80	172.80	172.80	6.0
0	4	-640	4	35	-6.61	2.44	10.81	105.60	153.60	153.60	11
0	5	-640	4	35	-6.61	2.44	10.81	105.60	153.60	153.60	11
0	6	-640	4	35	-6.61	2.44	10.81	105.60	153.60	153.60	11
0	7	-640	4	35	-6.61	2.44	10.81	105.60	153.60	153.60	11
0	(8+9)-VIII-4	-2217	24	217	-22.90	14.09	67.25	132.00	192.00	192.00	2.3
0	(8+9)-VI-1	1566	-21	-170	16.18	-12.40	-52.81	132.00	192.00	192.00	2.2
0	(8+9)-VI-4	-2435	26	218	-25.15	15.41	67.65	132.00	192.00	192.00	2.2
0	(8+9)-VI-3	697	-3	-159	7.20	-1.57	-49.30	132.00	192.00	192.00	3.1
0	(8+9)-I-4	-2610	40	110	-26.96	23.83	34.20	132.00	192.00	192.00	3.1
0	(8+9)-III-4	-2544	40	110	-26.28	23.43	34.08	132.00	192.00	192.00	3.1
0	(8+9)-II-2	-1488	7	204	-15.37	4.06	63.13	132.00	192.00	192.00	2.8
0	(8+9)-IV-1	1425	-20	-172	14.73	-11.59	-53.42	132.00	192.00	192.00	2.2
0	(8+9)-II-4	-2512	27	222	-25.95	15.93	68.67	132.00	192.00	192.00	2.2
0	(8+9)-I-1	1741	-35	-62	17.99	-20.81	-19.36	132.00	192.00	192.00	2.9
0	(8+9)-VIII-2	-1348	6	206	-13.92	3.26	63.74	132.00	192.00	192.00	2.8
0	(8+9)-VIII-1	1348	-19	-169	13.93	-11.08	-52.41	132.00	192.00	192.00	2.3
0	(8+9)-III-1	1676	-35	-62	17.31	-20.42	-19.24	132.00	192.00	192.00	3.0
0	(8+9)-II-1	1643	-22	-174	16.97	-12.91	-53.83	132.00	192.00	192.00	2.1
0	(8+9)-VI-2	-1565	8	207	-16.17	4.58	64.14	132.00	192.00	192.00	2.7
0	(8+9)-IV-4	-2294	25	220	-23.70	14.61	68.26	132.00	192.00	192.00	2.2
1935	(8+9)-V-1	2222	-93	44	22.96	-54.70	13.76	132.00	192.00	192.00	1.9
1935	(8+9)-IV-2	-1424	11	198	-14.71	6.22	61.27	132.00	192.00	192.00	2.8
1935	(8+9)-I-2	-930	6	184	-9.61	3.62	56.89	132.00	192.00	192.00	3.1
1935	(8+9)-VII-2	1661	-87	129	17.16	-51.68	39.96	132.00	192.00	192.00	1.6
1935	(8+9)-V-3	-2512	90	-108	-25.95	53.21	-33.56	132.00	192.00	192.00	2.1
1935	(8+9)-VII-3	-2515	90	-113	-25.98	53.20	-35.08	132.00	192.00	192.00	2.1
1935	(8+9)-V-2	1659	-87	124	17.14	-51.70	38.44	132.00	192.00	192.00	1.7
1935	(8+9)-VII-4	-3073	95	-24	-31.75	56.23	-7.37	132.00	192.00	192.00	2.8
1935	(8+9)-VII-1	2220	-93	40	22.93	-54.72	12.24	132.00	192.00	192.00	1.9
1935	(8+9)-V-4	-3076	95	-29	-31.77	56.21	-8.89	132.00	192.00	192.00	2.7
1935	(8+9)-IV-3	570	-8	-182	5.89	-4.71	-56.39	132.00	192.00	192.00	2.8
1935	(8+9)-III-2	-928	6	188	-9.58	3.64	58.41	132.00	192.00	192.00	3.1
1935	(8+9)-II-3	578	-8	-166	5.98	-4.65	-51.32	132.00	192.00	192.00	3.0
1935	(8+9)-I-3	77	-4	-168	0.79	-2.11	-52.01	132.00	192.00	192.00	3.5
1935	(8+9)-VIII-3	-207	20	-164	-2.13	11.89	-50.86	132.00	192.00	192.00	3.1
1935	(8+9)-III-3	74	-4	-173	0.77	-2.13	-53.53	132.00	192.00	192.00	3.4

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
0	1	-10	0.00	3.84	Si	>100
0	2	-29	0.01	5.76	Si	>100
0	3	-29	0.01	5.76	Si	>100
0	4	-10	0.00	5.12	Si	>100
0	5	-10	0.00	5.12	Si	>100
0	6	-10	0.00	5.12	Si	>100
0	7	-10	0.00	5.12	Si	>100
0	(8+9)-VII-1	371	0.10	6.40	Si	66
0	(8+9)-V-1	399	0.10	6.40	Si	61
0	(8+9)-VII-3	-422	0.11	6.40	Si	58
0	(8+9)-VIII-1	48	0.01	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
0	(8+9)-VII-2	411	0.11	6.40	Si	60
0	(8+9)-VIII-3	-190	0.05	6.40	Si	>100
0	(8+9)-VI-3	-98	0.03	6.40	Si	>100
0	(8+9)-VIII-2	179	0.05	6.40	Si	>100
0	(8+9)-VI-2	86	0.02	6.40	Si	>100
0	(8+9)-VIII-4	-59	0.02	6.40	Si	>100
0	(8+9)-II-1	-50	0.01	6.40	Si	>100
0	(8+9)-II-4	38	0.01	6.40	Si	>100
0	(8+9)-VII-4	-383	0.10	6.40	Si	64
0	(8+9)-V-4	-411	0.11	6.40	Si	60
0	(8+9)-V-3	-394	0.10	6.40	Si	62
0	(8+9)-V-2	383	0.10	6.40	Si	64
100	(8+9)-I-2	-258	0.07	6.40	Si	95
100	(8+9)-III-2	-228	0.06	6.40	Si	>100
100	(8+9)-IV-4	132	0.03	6.40	Si	>100
100	(8+9)-III-1	-267	0.07	6.40	Si	92
100	(8+9)-IV-2	-13	0.00	6.40	Si	>100
100	(8+9)-IV-1	-143	0.04	6.40	Si	>100
100	(8+9)-III-4	256	0.07	6.40	Si	96
100	(8+9)-I-3	246	0.06	6.40	Si	100
100	(8+9)-I-1	-238	0.06	6.40	Si	>100
100	(8+9)-III-3	217	0.06	6.40	Si	>100
100	(8+9)-IV-3	2	0.00	6.40	Si	>100
100	(8+9)-I-4	226	0.06	6.40	Si	>100
200	(8+9)-II-3	109	0.03	6.40	Si	>100
200	(8+9)-II-2	-120	0.03	6.40	Si	>100
200	(8+9)-VI-1	154	0.04	6.40	Si	>100
200	(8+9)-VI-4	-166	0.04	6.40	Si	>100
Verifiche nella direzione secondaria						
0	2	-9	0.09	5.76	Si	67
0	3	-9	0.09	5.76	Si	67
0	(8+9)-IV-4	-17	0.16	6.40	Si	40
0	(8+9)-VII-3	-10	0.10	6.40	Si	65
0	(8+9)-V-3	-9	0.09	6.40	Si	74
0	(8+9)-VII-4	-14	0.14	6.40	Si	46
0	(8+9)-II-4	-21	0.20	6.40	Si	32
0	(8+9)-VII-2	10	0.10	6.40	Si	64
0	(8+9)-III-1	36	0.34	6.40	Si	19
0	(8+9)-I-1	37	0.35	6.40	Si	18
0	(8+9)-III-2	32	0.30	6.40	Si	21
0	(8+9)-I-3	-30	0.29	6.40	Si	22
0	(8+9)-III-3	-32	0.30	6.40	Si	21
0	(8+9)-II-1	21	0.20	6.40	Si	32
0	(8+9)-III-4	-36	0.34	6.40	Si	19
0	(8+9)-I-2	30	0.29	6.40	Si	22
0	(8+9)-I-4	-37	0.35	6.40	Si	18
0	(8+9)-V-4	-16	0.15	6.40	Si	43
0	(8+9)-VII-1	15	0.14	6.40	Si	46
0	(8+9)-IV-1	17	0.16	6.40	Si	39
0	(8+9)-V-2	9	0.09	6.40	Si	73
0	(8+9)-V-1	16	0.15	6.40	Si	43
1935	1	1	0.01	3.84	Si	>100
1935	4	1	0.01	5.12	Si	>100
1935	5	1	0.01	5.12	Si	>100
1935	6	1	0.01	5.12	Si	>100
1935	7	1	0.01	5.12	Si	>100
1935	(8+9)-VIII-4	-16	0.15	6.40	Si	43
1935	(8+9)-IV-3	22	0.21	6.40	Si	30
1935	(8+9)-II-3	23	0.22	6.40	Si	29
1935	(8+9)-VI-2	-18	0.17	6.40	Si	38
1935	(8+9)-IV-2	-20	0.19	6.40	Si	33
1935	(8+9)-II-2	-21	0.20	6.40	Si	31
1935	(8+9)-VI-3	20	0.19	6.40	Si	34
1935	(8+9)-VI-1	19	0.18	6.40	Si	36

X	Comb.	Ty	τ_d	fvd	RS	Cs
1935	(8+9)-VIII-1	18	0.17	6.40	Si	38
1935	(8+9)-VIII-2	-17	0.16	6.40	Si	40
1935	(8+9)-VIII-3	19	0.18	6.40	Si	36
1935	(8+9)-VI-4	-17	0.16	6.40	Si	40

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	(8+9)-VI-4	-4718	-2.54	32.00	13	-0.62	20.00	32	V	13
0	(8+9)-III-1	-815	-0.44	32.00	73	-0.11	20.00	>100	V	73
0	(8+9)-V-3	2824	1.52	32.00	21	0.37	20.00	54	V	21
0	(8+9)-III-2	-4193	-2.26	32.00	14	-0.55	20.00	37	V	14
0	(8+9)-VIII-3	6144	3.31	32.00	9.7	0.80	20.00	25	V	9.7
0	(8+9)-III-3	4586	2.47	32.00	13	0.60	20.00	33	V	13
0	(8+9)-VIII-1	5509	2.97	32.00	11	0.72	20.00	28	V	11
0	(8+9)-III-4	1208	0.65	32.00	49	0.16	20.00	>100	V	49
0	(8+9)-VII-3	2943	1.59	32.00	20	0.38	20.00	52	V	20
0	(8+9)-IV-1	5016	2.70	32.00	12	0.65	20.00	31	V	12
0	(8+9)-I-2	-4074	-2.20	32.00	15	-0.53	20.00	38	V	15
0	(8+9)-IV-2	-6243	-3.37	32.00	9.5	-0.81	20.00	25	V	9.5
0	(8+9)-I-4	1328	0.72	32.00	45	0.17	20.00	>100	V	45
0	(8+9)-IV-3	6636	3.58	32.00	8.9	0.87	20.00	23	V	8.9
0	(8+9)-II-2	-5845	-3.15	32.00	10	-0.76	20.00	26	V	10
0	(8+9)-IV-4	-4623	-2.49	32.00	13	-0.60	20.00	33	V	13
0	(8+9)-II-4	-4225	-2.28	32.00	14	-0.55	20.00	36	V	14
0	(8+9)-VII-2	-2550	-1.38	32.00	23	-0.33	20.00	60	V	23
0	(8+9)-VIII-2	-5751	-3.10	32.00	10	-0.75	20.00	27	V	10
0	(8+9)-V-2	-2431	-1.31	32.00	24	-0.32	20.00	63	V	24
0	(8+9)-I-1	-935	-0.50	32.00	63	-0.12	20.00	>100	V	63
0	(8+9)-II-1	4618	2.49	32.00	13	0.60	20.00	33	V	13
0	(8+9)-VIII-4	-5116	-2.76	32.00	12	-0.67	20.00	30	V	12
0	(8+9)-VI-3	5745	3.10	32.00	10	0.75	20.00	27	V	10
0	(8+9)-I-3	4466	2.41	32.00	13	0.58	20.00	34	V	13
0	(8+9)-II-3	6238	3.36	32.00	9.5	0.81	20.00	25	V	9.5
0	(8+9)-VI-2	-5352	-2.89	32.00	11	-0.70	20.00	29	V	11
0	(8+9)-VI-1	5111	2.76	32.00	12	0.67	20.00	30	V	12
100	(8+9)-VII-1	897	0.48	32.00	66	0.12	20.00	>100	V	66
100	(8+9)-VII-4	-470	-0.25	32.00	>100	-0.06	20.00	>100	V	>100
200	1	311	0.17	19.20	>100	0.04	12.00	>100	V	>100
200	2	255	0.14	28.80	>100	0.03	18.00	>100	V	>100
200	3	255	0.14	28.80	>100	0.03	18.00	>100	V	>100
200	4	311	0.17	25.60	>100	0.04	16.00	>100	V	>100
200	5	311	0.17	25.60	>100	0.04	16.00	>100	V	>100
200	6	311	0.17	25.60	>100	0.04	16.00	>100	V	>100
200	7	311	0.17	25.60	>100	0.04	16.00	>100	V	>100
200	(8+9)-V-4	-448	-0.24	32.00	>100	-0.06	20.00	>100	V	>100
200	(8+9)-V-1	896	0.48	32.00	67	0.12	20.00	>100	V	67
Verifiche nella direzione secondaria										
0	(8+9)-II-1	-421	-4.35	32.00	7.4	-1.05	20.00	19	V	7.4
0	(8+9)-VII-3	-570	-5.89	32.00	5.4	-1.43	20.00	14	V	5.4
0	(8+9)-V-4	-232	-2.39	32.00	13	-0.58	20.00	35	V	13
0	(8+9)-VII-4	-217	-2.24	32.00	14	-0.54	20.00	37	V	14
0	(8+9)-V-3	-555	-5.74	32.00	5.6	-1.39	20.00	14	V	5.6
0	(8+9)-VI-3	-654	-6.75	32.00	4.7	-1.63	20.00	12	V	4.7
0	(8+9)-VII-2	580	6.00	32.00	5.3	1.45	20.00	14	V	5.3
0	(8+9)-VII-1	227	2.35	32.00	14	0.57	20.00	35	V	14
0	(8+9)-V-2	566	5.84	32.00	5.5	1.41	20.00	14	V	5.5
0	(8+9)-V-1	242	2.50	32.00	13	0.61	20.00	33	V	13
0	(8+9)-II-4	431	4.46	32.00	7.2	1.08	20.00	19	V	7.2
1935	1	23	0.24	19.20	80	0.06	12.00	>100	V	80
1935	2	68	0.70	28.80	41	0.17	18.00	>100	V	41
1935	3	68	0.70	28.80	41	0.17	18.00	>100	V	41
1935	4	23	0.24	25.60	>100	0.06	16.00	>100	V	>100

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
1935	5	23	0.24	25.60	>100	0.06	16.00	>100	V	>100
1935	6	23	0.24	25.60	>100	0.06	16.00	>100	V	>100
1935	7	23	0.24	25.60	>100	0.06	16.00	>100	V	>100
1935	(8+9)-VIII-4	739	7.64	32.00	4.2	1.85	20.00	11	V	4.2
1935	(8+9)-I-1	631	6.52	32.00	4.9	1.58	20.00	13	V	4.9
1935	(8+9)-II-2	895	9.25	32.00	3.5	2.24	20.00	8.9	V	3.5
1935	(8+9)-III-3	-1011	-10.44	32.00	3.1	-2.53	20.00	7.9	V	3.1
1935	(8+9)-IV-2	995	10.28	32.00	3.1	2.49	20.00	8.0	V	3.1
1935	(8+9)-VI-4	639	6.60	32.00	4.8	1.60	20.00	13	V	4.8
1935	(8+9)-IV-4	512	5.29	32.00	6.1	1.28	20.00	16	V	6.1
1935	(8+9)-III-2	1043	10.78	32.00	3.0	2.61	20.00	7.7	V	3.0
1935	(8+9)-I-2	1014	10.47	32.00	3.1	2.53	20.00	7.9	V	3.1
1935	(8+9)-III-1	601	6.21	32.00	5.2	1.50	20.00	13	V	5.2
1935	(8+9)-III-4	-569	-5.87	32.00	5.4	-1.42	20.00	14	V	5.4
1935	(8+9)-I-4	-599	-6.18	32.00	5.2	-1.50	20.00	13	V	5.2
1935	(8+9)-VI-2	668	6.90	32.00	4.6	1.67	20.00	12	V	4.6
1935	(8+9)-II-3	-863	-8.91	32.00	3.6	-2.16	20.00	9.3	V	3.6
1935	(8+9)-VI-1	-607	-6.27	32.00	5.1	-1.52	20.00	13	V	5.1
1935	(8+9)-IV-3	-963	-9.95	32.00	3.2	-2.41	20.00	8.3	V	3.2
1935	(8+9)-IV-1	-479	-4.95	32.00	6.5	-1.20	20.00	17	V	6.5
1935	(8+9)-VIII-1	-707	-7.30	32.00	4.4	-1.77	20.00	11	V	4.4
1935	(8+9)-VIII-2	768	7.93	32.00	4.0	1.92	20.00	10	V	4.0
1935	(8+9)-VIII-3	-735	-7.60	32.00	4.2	-1.84	20.00	11	V	4.2
1935	(8+9)-I-3	-981	-10.13	32.00	3.2	-2.45	20.00	8.2	V	3.2

Setto 14: origine (1023.0,465.0,149.5), direzione (-0.612129,0.790758,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	(8+9)-II-4	-395	415	4045	-0.18	7.18	3.74	132.00	192.00	192.00	18
0	(8+9)-VI-4	-408	334	4007	-0.19	5.78	3.70	132.00	192.00	192.00	20
0	(8+9)-I-1	-492	-535	2658	-0.23	-9.25	2.46	132.00	192.00	192.00	16
0	(8+9)-V-1	-450	-265	2785	-0.21	-4.59	2.57	132.00	192.00	192.00	27
595	2	-515	4	411	-0.23	0.07	0.35	118.80	172.80	172.80	>100
595	3	-515	4	411	-0.23	0.07	0.35	118.80	172.80	172.80	>100
595	(8+9)-VII-1	-749	-67	4429	-0.33	-1.12	3.80	132.00	192.00	192.00	39
1190	1	134	-3	-201	0.06	-0.04	-0.16	79.20	115.20	115.20	>100
1190	4	134	-3	-201	0.06	-0.04	-0.16	105.60	153.60	153.60	>100
1190	5	134	-3	-201	0.06	-0.04	-0.16	105.60	153.60	153.60	>100
1190	6	134	-3	-201	0.06	-0.04	-0.16	105.60	153.60	153.60	>100
1190	7	134	-3	-201	0.06	-0.04	-0.16	105.60	153.60	153.60	>100
1190	(8+9)-VIII-4	-2458	292	9492	-1.05	4.69	7.58	132.00	192.00	192.00	16
1190	(8+9)-IV-1	2669	-211	-9883	1.14	-3.39	-7.89	132.00	192.00	192.00	15
1190	(8+9)-V-4	1862	-124	-6489	0.80	-2.00	-5.18	132.00	192.00	192.00	23
1190	(8+9)-II-3	4028	-59	-14408	1.72	-0.95	-11.50	132.00	192.00	192.00	13
1190	(8+9)-VI-1	2414	88	-8645	1.03	1.42	-6.90	132.00	192.00	192.00	20
1190	(8+9)-III-1	-1573	287	5520	-0.67	4.62	4.41	132.00	192.00	192.00	21
1190	(8+9)-VI-2	-3819	-29	14221	-1.63	-0.47	11.35	132.00	192.00	192.00	16
1190	(8+9)-III-3	3805	-486	-13350	1.63	-7.82	-10.65	132.00	192.00	192.00	9.2
1190	(8+9)-VI-3	4029	26	-14510	1.72	0.41	-11.58	132.00	192.00	192.00	13
1190	(8+9)-II-1	2415	173	-8747	1.03	2.78	-6.98	132.00	192.00	192.00	17
1190	(8+9)-I-3	3729	-371	-13009	1.60	-5.97	-10.38	132.00	192.00	192.00	10
1190	(8+9)-IV-3	4282	-443	-15544	1.83	-7.12	-12.41	132.00	192.00	192.00	8.7
1190	(8+9)-I-2	-3519	367	12720	-1.51	5.90	10.15	132.00	192.00	192.00	12
1190	(8+9)-I-4	1859	-406	-6149	0.80	-6.54	-4.91	132.00	192.00	192.00	15
1190	(8+9)-VII-2	-3598	200	13401	-1.54	3.22	10.70	132.00	192.00	192.00	14
1190	(8+9)-V-3	3732	-89	-13349	1.60	-1.43	-10.65	132.00	192.00	192.00	13
1190	(8+9)-VII-3	3808	-204	-13690	1.63	-3.28	-10.93	132.00	192.00	192.00	12
1190	(8+9)-III-2	-3595	482	13061	-1.54	7.76	10.42	132.00	192.00	192.00	11
1190	(8+9)-VII-4	1786	-9	-6148	0.76	-0.15	-4.91	132.00	192.00	192.00	31
1190	(8+9)-V-2	-3522	85	13060	-1.51	1.37	10.42	132.00	192.00	192.00	16
1190	(8+9)-II-2	-3818	55	14119	-1.63	0.89	11.27	132.00	192.00	192.00	16
1190	(8+9)-III-4	1783	-291	-5809	0.76	-4.68	-4.64	132.00	192.00	192.00	18

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
1190	(8+9)-IV-4	-2458	207	9594	-1.05	3.33	7.66	132.00	192.00	192.00	17
1190	(8+9)-VIII-1	2668	-295	-9781	1.14	-4.75	-7.81	132.00	192.00	192.00	14
1190	(8+9)-VIII-2	-4073	354	15357	-1.74	5.70	12.26	132.00	192.00	192.00	11
1190	(8+9)-VIII-3	4283	-358	-15646	1.83	-5.76	-12.49	132.00	192.00	192.00	9.2
1190	(8+9)-IV-2	-4072	439	15255	-1.74	7.06	12.17	132.00	192.00	192.00	10.0
Verifiche nella direzione secondaria											
0	1	-1311	21	-257	-2.28	2.11	-2.25	79.20	115.20	115.20	26
0	2	-2099	39	-385	-3.64	3.85	-3.37	118.80	172.80	172.80	24
0	3	-2099	39	-385	-3.64	3.85	-3.37	118.80	172.80	172.80	24
0	4	-1311	21	-257	-2.28	2.11	-2.25	105.60	153.60	153.60	35
0	5	-1311	21	-257	-2.28	2.11	-2.25	105.60	153.60	153.60	35
0	6	-1311	21	-257	-2.28	2.11	-2.25	105.60	153.60	153.60	35
0	7	-1311	21	-257	-2.28	2.11	-2.25	105.60	153.60	153.60	35
0	(8+9)-VI-4	-372	32	930	-0.65	3.16	8.14	132.00	192.00	192.00	17
1609	(8+9)-VIII-4	797	38	1165	1.38	3.79	10.20	132.00	192.00	192.00	12
1609	(8+9)-IV-2	2092	17	1905	3.63	1.69	16.67	132.00	192.00	192.00	8.1
1609	(8+9)-V-2	1854	1	1588	3.22	0.13	13.90	132.00	192.00	192.00	10
1609	(8+9)-I-3	-3579	65	-1824	-6.21	6.47	-15.97	132.00	192.00	192.00	8.5
1609	(8+9)-V-3	-3603	13	-2049	-6.26	1.27	-17.94	132.00	192.00	192.00	9.9
1609	(8+9)-II-1	-2093	-22	-1470	-3.63	-2.23	-12.87	132.00	192.00	192.00	13
1609	(8+9)-V-4	-2485	19	-1104	-4.32	1.93	-9.66	132.00	192.00	192.00	16
1609	(8+9)-II-3	-3380	14	-2142	-5.87	1.43	-18.75	132.00	192.00	192.00	9.4
1609	(8+9)-VI-1	-2086	-7	-1402	-3.62	-0.67	-12.27	132.00	192.00	192.00	15
1609	(8+9)-III-1	574	-63	350	1.00	-6.25	3.07	132.00	192.00	192.00	18
1609	(8+9)-VI-2	1639	15	1748	2.84	1.53	15.30	132.00	192.00	192.00	9.2
1609	(8+9)-III-3	-3717	60	-1891	-6.45	5.95	-16.56	132.00	192.00	192.00	8.4
1609	(8+9)-VI-3	-3388	-1	-2210	-5.88	-0.13	-19.34	132.00	192.00	192.00	9.8
1609	(8+9)-IV-1	-2553	-40	-1694	-4.43	-3.95	-14.83	132.00	192.00	192.00	10
1609	(8+9)-I-1	712	-58	417	1.24	-5.73	3.65	132.00	192.00	192.00	17
1609	(8+9)-IV-3	-3841	-3	-2366	-6.67	-0.29	-20.72	132.00	192.00	192.00	9.0
1609	(8+9)-VII-1	598	-10	575	1.04	-1.04	5.04	132.00	192.00	192.00	25
1609	(8+9)-V-1	736	-5	643	1.28	-0.53	5.62	132.00	192.00	192.00	24
1609	(8+9)-VII-2	1992	7	1655	3.46	0.65	14.49	132.00	192.00	192.00	9.5
1609	(8+9)-II-2	1631	-0	1681	2.83	-0.03	14.71	132.00	192.00	192.00	10
1609	(8+9)-VII-3	-3741	8	-2116	-6.49	0.75	-18.53	132.00	192.00	192.00	9.8
1609	(8+9)-III-2	1968	-46	1430	3.42	-4.56	12.52	132.00	192.00	192.00	8.7
1609	(8+9)-VII-4	-2347	25	-1037	-4.08	2.44	-9.08	132.00	192.00	192.00	17
1609	(8+9)-I-4	-2461	72	-879	-4.27	7.13	-7.69	132.00	192.00	192.00	13
1609	(8+9)-II-4	344	37	1008	0.60	3.63	8.83	132.00	192.00	192.00	14
1609	(8+9)-III-4	-2323	77	-812	-4.03	7.65	-7.11	132.00	192.00	192.00	13
1609	(8+9)-IV-4	804	54	1232	1.40	5.35	10.79	132.00	192.00	192.00	11
1609	(8+9)-VIII-1	-2546	-24	-1626	-4.42	-2.39	-14.24	132.00	192.00	192.00	11
1609	(8+9)-VIII-2	2099	33	1972	3.64	3.25	17.27	132.00	192.00	192.00	7.4
1609	(8+9)-VIII-3	-3848	-19	-2434	-6.68	-1.85	-21.31	132.00	192.00	192.00	8.2
1609	(8+9)-I-2	1830	-51	1363	3.18	-5.07	11.93	132.00	192.00	192.00	8.9

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Ty kg	τ_d kg/cmq	fvd kg/cmq	RS	Cs
0	2	8	0.00	5.76	Si	>100
0	3	8	0.00	5.76	Si	>100
0	(8+9)-V-1	29	0.01	6.40	Si	>100
0	(8+9)-VI-2	73	0.02	6.40	Si	>100
0	(8+9)-V-4	-29	0.01	6.40	Si	>100
0	(8+9)-VII-1	44	0.01	6.40	Si	>100
0	(8+9)-V-3	-65	0.02	6.40	Si	>100
0	(8+9)-VI-3	-73	0.02	6.40	Si	>100
0	(8+9)-VI-1	-45	0.02	6.40	Si	>100
0	(8+9)-VI-4	45	0.02	6.40	Si	>100
0	(8+9)-VII-4	-45	0.01	6.40	Si	>100
0	(8+9)-V-2	65	0.02	6.40	Si	>100
0	(8+9)-II-2	92	0.03	6.40	Si	>100
0	(8+9)-II-3	-92	0.03	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
595	1	-1	0.00	3.84	Si	>100
595	4	-1	0.00	5.12	Si	>100
595	5	-1	0.00	5.12	Si	>100
595	6	-1	0.00	5.12	Si	>100
595	7	-1	0.00	5.12	Si	>100
595	(8+9)-III-1	238	0.08	6.40	Si	83
595	(8+9)-VIII-2	-132	0.04	6.40	Si	>100
595	(8+9)-IV-2	-64	0.02	6.40	Si	>100
595	(8+9)-VIII-3	129	0.04	6.40	Si	>100
595	(8+9)-IV-4	-185	0.06	6.40	Si	>100
595	(8+9)-VIII-4	-117	0.04	6.40	Si	>100
595	(8+9)-II-1	109	0.04	6.40	Si	>100
595	(8+9)-III-2	164	0.05	6.40	Si	>100
595	(8+9)-I-3	-189	0.06	6.40	Si	>100
595	(8+9)-VIII-1	114	0.04	6.40	Si	>100
595	(8+9)-I-1	216	0.07	6.40	Si	92
595	(8+9)-IV-3	61	0.02	6.40	Si	>100
595	(8+9)-III-4	-240	0.08	6.40	Si	83
595	(8+9)-II-4	-112	0.04	6.40	Si	>100
595	(8+9)-VII-2	-63	0.02	6.40	Si	>100
595	(8+9)-I-2	186	0.06	6.40	Si	>100
595	(8+9)-IV-1	182	0.06	6.40	Si	>100
595	(8+9)-III-3	-167	0.05	6.40	Si	>100
595	(8+9)-VII-3	60	0.02	6.40	Si	>100
595	(8+9)-I-4	-218	0.07	6.40	Si	91
Verifiche nella direzione secondaria						
0	2	-12	0.02	5.76	Si	>100
0	3	-12	0.02	5.76	Si	>100
0	(8+9)-II-3	48	0.08	6.40	Si	83
0	(8+9)-I-2	-30	0.05	6.40	Si	>100
0	(8+9)-VI-4	-45	0.07	6.40	Si	89
0	(8+9)-I-3	27	0.04	6.40	Si	>100
0	(8+9)-VI-2	-46	0.07	6.40	Si	86
0	(8+9)-III-3	25	0.04	6.40	Si	>100
0	(8+9)-VI-3	44	0.07	6.40	Si	90
0	(8+9)-VI-1	43	0.07	6.40	Si	93
0	(8+9)-III-2	-27	0.04	6.40	Si	>100
0	(8+9)-II-1	39	0.06	6.40	Si	>100
0	(8+9)-II-2	-50	0.08	6.40	Si	80
1609	1	4	0.01	3.84	Si	>100
1609	4	4	0.01	5.12	Si	>100
1609	5	4	0.01	5.12	Si	>100
1609	6	4	0.01	5.12	Si	>100
1609	7	4	0.01	5.12	Si	>100
1609	(8+9)-VIII-4	46	0.07	6.40	Si	87
1609	(8+9)-V-4	-22	0.03	6.40	Si	>100
1609	(8+9)-II-4	42	0.07	6.40	Si	95
1609	(8+9)-I-4	37	0.06	6.40	Si	>100
1609	(8+9)-IV-2	49	0.08	6.40	Si	82
1609	(8+9)-III-1	-38	0.06	6.40	Si	>100
1609	(8+9)-IV-4	64	0.10	6.40	Si	63
1609	(8+9)-VII-1	21	0.03	6.40	Si	>100
1609	(8+9)-V-2	46	0.07	6.40	Si	86
1609	(8+9)-VII-2	53	0.08	6.40	Si	76
1609	(8+9)-IV-1	-58	0.09	6.40	Si	69
1609	(8+9)-VII-3	-47	0.08	6.40	Si	85
1609	(8+9)-I-1	-32	0.05	6.40	Si	>100
1609	(8+9)-VII-4	-15	0.02	6.40	Si	>100
1609	(8+9)-III-4	44	0.07	6.40	Si	92
1609	(8+9)-IV-3	-43	0.07	6.40	Si	93
1609	(8+9)-V-3	-41	0.07	6.40	Si	98
1609	(8+9)-VIII-1	-40	0.06	6.40	Si	99
1609	(8+9)-VIII-2	66	0.11	6.40	Si	60
1609	(8+9)-VIII-3	-61	0.10	6.40	Si	66

X	Comb.	Ty	τ_d	fvd	RS	Cs
1609	(8+9)-V-1	27	0.04	6.40	Si	>100

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	(8+9)-VI-1	5034	3.48	32.00	9.2	0.84	20.00	24	V	9.2
0	(8+9)-II-2	-8628	-5.96	32.00	5.4	-1.44	20.00	14	V	5.4
0	(8+9)-III-2	-8411	-5.81	32.00	5.5	-1.41	20.00	14	V	5.5
0	(8+9)-I-3	8147	5.63	32.00	5.7	1.36	20.00	15	V	5.7
0	(8+9)-II-3	8484	5.86	32.00	5.5	1.42	20.00	14	V	5.5
0	(8+9)-I-4	4131	2.85	32.00	11	0.69	20.00	29	V	11
0	(8+9)-VI-3	8207	5.67	32.00	5.6	1.37	20.00	15	V	5.6
0	(8+9)-II-1	4757	3.29	32.00	9.7	0.80	20.00	25	V	9.7
0	(8+9)-III-4	4011	2.77	32.00	12	0.67	20.00	30	V	12
0	(8+9)-III-3	8267	5.71	32.00	5.6	1.38	20.00	14	V	5.6
0	(8+9)-VI-4	-5178	-3.58	32.00	8.9	-0.87	20.00	23	V	8.9
0	(8+9)-I-1	-4275	-2.95	32.00	11	-0.71	20.00	28	V	11
0	(8+9)-VI-2	-8351	-5.77	32.00	5.5	-1.40	20.00	14	V	5.5
0	(8+9)-I-2	-8291	-5.73	32.00	5.6	-1.39	20.00	14	V	5.6
0	(8+9)-II-4	-4901	-3.39	32.00	9.4	-0.82	20.00	24	V	9.4
0	(8+9)-III-1	-4155	-2.87	32.00	11	-0.69	20.00	29	V	11
595	1	-163	-0.11	19.20	>100	-0.03	12.00	>100	V	>100
595	2	-261	-0.17	28.80	>100	-0.04	18.00	>100	V	>100
595	3	-261	-0.17	28.80	>100	-0.04	18.00	>100	V	>100
595	4	-163	-0.11	25.60	>100	-0.03	16.00	>100	V	>100
595	5	-163	-0.11	25.60	>100	-0.03	16.00	>100	V	>100
595	6	-163	-0.11	25.60	>100	-0.03	16.00	>100	V	>100
595	7	-163	-0.11	25.60	>100	-0.03	16.00	>100	V	>100
595	(8+9)-IV-3	9252	6.16	32.00	5.2	1.49	20.00	13	V	5.2
595	(8+9)-VII-3	7942	5.29	32.00	6.1	1.28	20.00	16	V	6.1
595	(8+9)-V-2	-7891	-5.25	32.00	6.1	-1.27	20.00	16	V	6.1
595	(8+9)-VII-4	3397	2.26	32.00	14	0.55	20.00	37	V	14
595	(8+9)-V-4	3682	2.45	32.00	13	0.59	20.00	34	V	13
595	(8+9)-VIII-1	5723	3.81	32.00	8.4	0.92	20.00	22	V	8.4
595	(8+9)-IV-4	-5899	-3.93	32.00	8.1	-0.95	20.00	21	V	8.1
595	(8+9)-VIII-2	-9429	-6.28	32.00	5.1	-1.52	20.00	13	V	5.1
595	(8+9)-IV-1	5665	3.77	32.00	8.5	0.91	20.00	22	V	8.5
595	(8+9)-VIII-3	9195	6.12	32.00	5.2	1.48	20.00	14	V	5.2
595	(8+9)-VII-2	-8176	-5.44	32.00	5.9	-1.32	20.00	15	V	5.9
595	(8+9)-V-1	-3916	-2.61	32.00	12	-0.63	20.00	32	V	12
595	(8+9)-IV-2	-9486	-6.31	32.00	5.1	-1.53	20.00	13	V	5.1
595	(8+9)-VII-1	-3631	-2.42	32.00	13	-0.58	20.00	34	V	13
595	(8+9)-V-3	7657	5.10	32.00	6.3	1.23	20.00	16	V	6.3
595	(8+9)-VIII-4	-5957	-3.96	32.00	8.1	-0.96	20.00	21	V	8.1
Verifiche nella direzione secondaria										
0	2	23	0.04	28.80	>100	0.01	18.00	>100	V	>100
0	3	23	0.04	28.80	>100	0.01	18.00	>100	V	>100
0	(8+9)-VIII-4	2238	3.89	32.00	8.2	0.94	20.00	21	V	8.2
0	(8+9)-VI-4	1940	3.37	32.00	9.5	0.81	20.00	25	V	9.5
0	(8+9)-III-3	-2969	-5.15	32.00	6.2	-1.25	20.00	16	V	6.2
0	(8+9)-IV-3	-3513	-6.10	32.00	5.2	-1.48	20.00	14	V	5.2
0	(8+9)-VII-2	3058	5.31	32.00	6.0	1.29	20.00	16	V	6.0
0	(8+9)-VIII-2	3549	6.16	32.00	5.2	1.49	20.00	13	V	5.2
0	(8+9)-IV-1	-2248	-3.90	32.00	8.2	-0.94	20.00	21	V	8.2
0	(8+9)-I-1	1339	2.32	32.00	14	0.56	20.00	36	V	14
0	(8+9)-IV-2	3526	6.12	32.00	5.2	1.48	20.00	13	V	5.2
0	(8+9)-I-3	-2879	-5.00	32.00	6.4	-1.21	20.00	17	V	6.4
0	(8+9)-II-1	-1950	-3.38	32.00	9.5	-0.82	20.00	24	V	9.5
0	(8+9)-IV-4	2261	3.93	32.00	8.2	0.95	20.00	21	V	8.2
0	(8+9)-II-3	-3215	-5.58	32.00	5.7	-1.35	20.00	15	V	5.7
0	(8+9)-V-1	1416	2.46	32.00	13	0.59	20.00	34	V	13
0	(8+9)-III-1	1249	2.17	32.00	15	0.52	20.00	38	V	15
0	(8+9)-V-2	2969	5.15	32.00	6.2	1.25	20.00	16	V	6.2

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
0	(8+9)-VIII-3	-3536	-6.14	32.00	5.2	-1.49	20.00	13	V	5.2
0	(8+9)-V-3	-2956	-5.13	32.00	6.2	-1.24	20.00	16	V	6.2
0	(8+9)-I-2	2892	5.02	32.00	6.4	1.22	20.00	16	V	6.4
0	(8+9)-VII-1	1326	2.30	32.00	14	0.56	20.00	36	V	14
0	(8+9)-II-2	3228	5.60	32.00	5.7	1.36	20.00	15	V	5.7
0	(8+9)-III-2	2982	5.18	32.00	6.2	1.25	20.00	16	V	6.2
0	(8+9)-VIII-1	-2225	-3.86	32.00	8.3	-0.93	20.00	21	V	8.3
0	(8+9)-VII-3	-3045	-5.29	32.00	6.1	-1.28	20.00	16	V	6.1
0	(8+9)-II-4	1963	3.41	32.00	9.4	0.82	20.00	24	V	9.4
0	(8+9)-VI-1	-1927	-3.35	32.00	9.6	-0.81	20.00	25	V	9.6
0	(8+9)-VI-2	3251	5.64	32.00	5.7	1.37	20.00	15	V	5.7
0	(8+9)-VI-3	-3238	-5.62	32.00	5.7	-1.36	20.00	15	V	5.7
1609	1	-9	-0.01	19.20	>100	-0.00	12.00	>100	V	>100
1609	4	-9	-0.01	25.60	>100	-0.00	16.00	>100	V	>100
1609	5	-9	-0.01	25.60	>100	-0.00	16.00	>100	V	>100
1609	6	-9	-0.01	25.60	>100	-0.00	16.00	>100	V	>100
1609	7	-9	-0.01	25.60	>100	-0.00	16.00	>100	V	>100
1609	(8+9)-V-4	-1412	-2.45	32.00	13	-0.59	20.00	34	V	13
1609	(8+9)-III-4	-1237	-2.15	32.00	15	-0.52	20.00	38	V	15
1609	(8+9)-I-4	-1330	-2.31	32.00	14	-0.56	20.00	36	V	14
1609	(8+9)-VII-4	-1319	-2.29	32.00	14	-0.55	20.00	36	V	14

Setto 15: origine (950.1,559.1,88.5), direzione (-0.612129,0.790758,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_N	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	(8+9)-VIII-4	4842	-3	-3179	3.77	-0.09	-8.39	132.00	192.00	192.00	14
0	(8+9)-IV-1	-4842	9	3280	-3.77	0.27	8.65	132.00	192.00	192.00	21
0	(8+9)-VI-4	4218	-5	-2757	3.28	-0.15	-7.27	132.00	192.00	192.00	16
0	(8+9)-III-2	6343	-16	-4124	4.94	-0.47	-10.88	132.00	192.00	192.00	10
0	(8+9)-IV-2	7569	-18	-4971	5.89	-0.52	-13.11	132.00	192.00	192.00	8.6
0	(8+9)-III-3	-6288	14	4181	-4.89	0.40	11.03	132.00	192.00	192.00	17
0	(8+9)-VIII-2	7623	-26	-5015	5.93	-0.76	-13.23	132.00	192.00	192.00	8.5
0	(8+9)-VII-2	6524	-44	-4269	5.08	-1.28	-11.26	132.00	192.00	192.00	9.6
0	(8+9)-VII-4	-2746	33	1850	-2.14	0.98	4.88	132.00	192.00	192.00	33
0	(8+9)-VII-1	2800	-36	-1793	2.18	-1.04	-4.73	132.00	192.00	192.00	21
0	(8+9)-I-2	6156	-17	-3997	4.79	-0.48	-10.54	132.00	192.00	192.00	11
0	(8+9)-VII-3	-6469	41	4326	-5.03	1.21	11.41	132.00	192.00	192.00	15
0	(8+9)-IV-3	-7514	16	5028	-5.85	0.46	13.26	132.00	192.00	192.00	14
0	(8+9)-II-2	6945	-20	-4550	5.40	-0.58	-12.00	132.00	192.00	192.00	9.4
0	(8+9)-IV-4	4897	-11	-3223	3.81	-0.33	-8.50	132.00	192.00	192.00	13
0	(8+9)-II-4	4273	-13	-2801	3.32	-0.39	-7.39	132.00	192.00	192.00	15
0	(8+9)-V-1	2988	-35	-1920	2.32	-1.02	-5.06	132.00	192.00	192.00	20
0	(8+9)-VIII-3	-7568	24	5072	-5.89	0.70	13.38	132.00	192.00	192.00	13
0	(8+9)-V-2	6336	-44	-4142	4.93	-1.29	-10.93	132.00	192.00	192.00	9.9
0	(8+9)-I-1	2807	-7	-1775	2.18	-0.21	-4.68	132.00	192.00	192.00	24
0	(8+9)-V-3	-6282	42	4199	-4.89	1.23	11.08	132.00	192.00	192.00	15
0	(8+9)-II-1	-4218	11	2858	-3.28	0.32	7.54	132.00	192.00	192.00	24
0	(8+9)-V-4	-2933	33	1977	-2.28	0.96	5.21	132.00	192.00	192.00	31
0	(8+9)-III-1	2620	-8	-1648	2.04	-0.23	-4.35	132.00	192.00	192.00	25
0	(8+9)-I-3	-6101	14	4054	-4.75	0.42	10.69	132.00	192.00	192.00	17
0	(8+9)-II-3	-6890	18	4607	-5.36	0.51	12.15	132.00	192.00	192.00	15
0	(8+9)-VIII-1	-4788	1	3236	-3.73	0.02	8.54	132.00	192.00	192.00	22
0	(8+9)-VI-1	-4163	3	2814	-3.24	0.08	7.42	132.00	192.00	192.00	25
0	(8+9)-VI-2	6999	-28	-4593	5.45	-0.82	-12.12	132.00	192.00	192.00	9.2
0	(8+9)-VI-3	-6944	26	4650	-5.40	0.76	12.27	132.00	192.00	192.00	15
3200	1	-241	-1	146	-0.19	-0.04	0.38	79.20	115.20	115.20	>100
3200	2	-542	-9	347	-0.42	-0.25	0.91	118.80	172.80	172.80	>100
3200	3	-542	-9	347	-0.42	-0.25	0.91	118.80	172.80	172.80	>100
3200	4	-241	-1	146	-0.19	-0.04	0.38	105.60	153.60	153.60	>100
3200	5	-241	-1	146	-0.19	-0.04	0.38	105.60	153.60	153.60	>100
3200	6	-241	-1	146	-0.19	-0.04	0.38	105.60	153.60	153.60	>100
3200	7	-241	-1	146	-0.19	-0.04	0.38	105.60	153.60	153.60	>100

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
3200	(8+9)-III-4	-578	-77	-1087	-0.45	-2.24	-2.87	132.00	192.00	192.00	38
3200	(8+9)-I-4	-609	-78	-1173	-0.47	-2.29	-3.09	132.00	192.00	192.00	36
Verifiche nella direzione secondaria											
0	1	-1734	20	-525	-1.12	0.73	-0.64	79.20	115.20	115.20	84
0	2	-3014	47	-1412	-1.95	1.73	-1.71	118.80	172.80	172.80	50
0	3	-3014	47	-1412	-1.95	1.73	-1.71	118.80	172.80	172.80	50
0	4	-1734	20	-525	-1.12	0.73	-0.64	105.60	153.60	153.60	>100
0	5	-1734	20	-525	-1.12	0.73	-0.64	105.60	153.60	153.60	>100
0	6	-1734	20	-525	-1.12	0.73	-0.64	105.60	153.60	153.60	>100
0	7	-1734	20	-525	-1.12	0.73	-0.64	105.60	153.60	153.60	>100
0	(8+9)-V-1	2345	-126	2734	1.51	-4.64	3.31	132.00	192.00	192.00	19
0	(8+9)-I-4	-4928	119	-3810	-3.18	4.41	-4.61	132.00	192.00	192.00	21
0	(8+9)-II-4	-3071	74	-6035	-1.98	2.75	-7.31	132.00	192.00	192.00	19
0	(8+9)-VII-4	-4625	147	-3368	-2.99	5.43	-4.08	132.00	192.00	192.00	20
0	(8+9)-III-1	2375	-90	3078	1.53	-3.34	3.73	132.00	192.00	192.00	21
0	(8+9)-VII-1	2208	-122	2685	1.43	-4.50	3.25	132.00	192.00	192.00	20
0	(8+9)-VI-4	-3021	84	-5917	-1.95	3.10	-7.16	132.00	192.00	192.00	19
0	(8+9)-VII-3	-4406	135	-399	-2.84	4.98	-0.48	132.00	192.00	192.00	35
0	(8+9)-II-1	654	-49	5351	0.42	-1.82	6.48	132.00	192.00	192.00	22
0	(8+9)-V-4	-4762	151	-3418	-3.07	5.57	-4.14	132.00	192.00	192.00	20
0	(8+9)-V-3	-4269	131	-350	-2.76	4.84	-0.42	132.00	192.00	192.00	36
0	(8+9)-III-4	-4792	116	-3761	-3.09	4.27	-4.55	132.00	192.00	192.00	22
0	(8+9)-I-1	2511	-94	3127	1.62	-3.48	3.79	132.00	192.00	192.00	20
1770	(8+9)-VIII-4	-2156	32	-8297	-1.39	1.17	-10.04	132.00	192.00	192.00	17
1770	(8+9)-IV-2	-875	18	-10374	-0.57	0.66	-12.56	132.00	192.00	192.00	15
1770	(8+9)-II-3	-1144	4	10221	-0.74	0.16	12.37	132.00	192.00	192.00	15
1770	(8+9)-IV-3	-1330	-5	11023	-0.86	-0.18	13.34	132.00	192.00	192.00	14
1770	(8+9)-II-2	-1061	9	-9571	-0.69	0.32	-11.59	132.00	192.00	192.00	16
1770	(8+9)-IV-1	-1140	-24	7338	-0.74	-0.90	8.88	132.00	192.00	192.00	20
1770	(8+9)-VII-2	2891	0	-3112	1.87	0.00	-3.77	132.00	192.00	192.00	30
1770	(8+9)-III-3	-1458	33	9123	-0.94	1.21	11.05	132.00	192.00	192.00	16
1770	(8+9)-I-3	-1402	35	8883	-0.91	1.31	10.75	132.00	192.00	192.00	16
1770	(8+9)-VI-1	137	-9	8145	0.09	-0.34	9.86	132.00	192.00	192.00	19
1770	(8+9)-I-2	-803	-22	-8233	-0.52	-0.83	-9.97	132.00	192.00	192.00	18
1770	(8+9)-V-2	2835	-3	-2871	1.83	-0.10	-3.48	132.00	192.00	192.00	31
1770	(8+9)-III-2	-747	-20	-8474	-0.48	-0.72	-10.26	132.00	192.00	192.00	17
1770	(8+9)-VI-2	30	15	-7963	0.02	0.54	-9.64	132.00	192.00	192.00	19
1770	(8+9)-IV-4	-1065	37	-6688	-0.69	1.39	-8.10	132.00	192.00	192.00	20
1770	(8+9)-VIII-1	-49	-19	8947	-0.03	-0.68	10.83	132.00	192.00	192.00	17
1770	(8+9)-VIII-2	216	24	-8765	0.14	0.88	-10.61	132.00	192.00	192.00	16
1770	(8+9)-VIII-3	-2421	-11	9415	-1.56	-0.40	11.40	132.00	192.00	192.00	16
1770	(8+9)-VI-3	-2235	-2	8612	-1.44	-0.06	10.43	132.00	192.00	192.00	18

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
1600	(8+9)-VI-2	93	0.05	6.40	Si	>100
1600	(8+9)-VI-3	-93	0.05	6.40	Si	>100
1600	(8+9)-VIII-2	97	0.05	6.40	Si	>100
1600	(8+9)-VIII-3	-96	0.05	6.40	Si	>100
3200	1	-3	0.00	3.84	Si	>100
3200	2	-16	0.01	5.76	Si	>100
3200	3	-16	0.01	5.76	Si	>100
3200	4	-3	0.00	5.12	Si	>100
3200	5	-3	0.00	5.12	Si	>100
3200	6	-3	0.00	5.12	Si	>100
3200	7	-3	0.00	5.12	Si	>100
3200	(8+9)-VI-1	185	0.10	6.40	Si	61
3200	(8+9)-VII-3	-363	0.21	6.40	Si	31
3200	(8+9)-II-2	-74	0.04	6.40	Si	>100
3200	(8+9)-VII-4	-397	0.22	6.40	Si	28
3200	(8+9)-II-4	-73	0.04	6.40	Si	>100
3200	(8+9)-VIII-1	169	0.10	6.40	Si	67

X	Comb.	Ty	τ_d	fvd	RS	Cs
3200	(8+9)-III-2	-20	0.01	6.40	Si	>100
3200	(8+9)-I-2	-24	0.01	6.40	Si	>100
3200	(8+9)-III-4	-17	0.01	6.40	Si	>100
3200	(8+9)-I-1	19	0.01	6.40	Si	>100
3200	(8+9)-IV-2	-58	0.03	6.40	Si	>100
3200	(8+9)-VIII-4	-171	0.10	6.40	Si	66
3200	(8+9)-IV-4	-57	0.03	6.40	Si	>100
3200	(8+9)-II-3	72	0.04	6.40	Si	>100
3200	(8+9)-V-2	356	0.20	6.40	Si	32
3200	(8+9)-III-1	14	0.01	6.40	Si	>100
3200	(8+9)-V-4	-402	0.23	6.40	Si	28
3200	(8+9)-III-3	17	0.01	6.40	Si	>100
3200	(8+9)-I-4	-21	0.01	6.40	Si	>100
3200	(8+9)-IV-1	55	0.03	6.40	Si	>100
3200	(8+9)-VI-4	-187	0.11	6.40	Si	60
3200	(8+9)-IV-3	56	0.03	6.40	Si	>100
3200	(8+9)-VII-2	361	0.20	6.40	Si	31
3200	(8+9)-II-1	71	0.04	6.40	Si	>100
3200	(8+9)-I-3	22	0.01	6.40	Si	>100
3200	(8+9)-VII-1	395	0.22	6.40	Si	29
3200	(8+9)-V-3	-359	0.20	6.40	Si	32
3200	(8+9)-V-1	400	0.23	6.40	Si	28
Verifiche nella direzione secondaria						
0	2	-23	0.01	5.76	Si	>100
0	3	-23	0.01	5.76	Si	>100
0	(8+9)-III-1	50	0.03	6.40	Si	>100
0	(8+9)-I-3	-28	0.02	6.40	Si	>100
0	(8+9)-IV-4	-44	0.03	6.40	Si	>100
0	(8+9)-I-4	-55	0.03	6.40	Si	>100
0	(8+9)-III-4	-51	0.03	6.40	Si	>100
0	(8+9)-II-1	57	0.03	6.40	Si	>100
0	(8+9)-I-1	54	0.03	6.40	Si	>100
0	(8+9)-IV-1	44	0.03	6.40	Si	>100
0	(8+9)-III-3	-32	0.02	6.40	Si	>100
0	(8+9)-I-2	27	0.02	6.40	Si	>100
0	(8+9)-III-2	31	0.02	6.40	Si	>100
0	(8+9)-II-3	33	0.02	6.40	Si	>100
0	(8+9)-II-4	-58	0.03	6.40	Si	>100
885	1	-5	0.00	3.84	Si	>100
885	4	-5	0.00	5.12	Si	>100
885	5	-5	0.00	5.12	Si	>100
885	6	-5	0.00	5.12	Si	>100
885	7	-5	0.00	5.12	Si	>100
885	(8+9)-II-2	-36	0.02	6.40	Si	>100
885	(8+9)-IV-2	-26	0.02	6.40	Si	>100
1770	(8+9)-VIII-4	72	0.04	6.40	Si	>100
1770	(8+9)-VI-1	-67	0.04	6.40	Si	>100
1770	(8+9)-VII-1	-309	0.18	6.40	Si	35
1770	(8+9)-V-1	-308	0.18	6.40	Si	35
1770	(8+9)-VII-2	-323	0.19	6.40	Si	33
1770	(8+9)-V-3	326	0.19	6.40	Si	33
1770	(8+9)-VII-3	325	0.19	6.40	Si	33
1770	(8+9)-IV-3	25	0.01	6.40	Si	>100
1770	(8+9)-VII-4	311	0.19	6.40	Si	35
1770	(8+9)-V-2	-324	0.19	6.40	Si	33
1770	(8+9)-V-4	310	0.18	6.40	Si	35
1770	(8+9)-VI-2	-121	0.07	6.40	Si	89
1770	(8+9)-VI-4	69	0.04	6.40	Si	>100
1770	(8+9)-VIII-1	-70	0.04	6.40	Si	>100
1770	(8+9)-VIII-2	-118	0.07	6.40	Si	91
1770	(8+9)-VIII-3	120	0.07	6.40	Si	90
1770	(8+9)-VI-3	123	0.07	6.40	Si	87

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	(8+9)-V-2	-4030	-4.70	32.00	6.8	-1.14	20.00	18	V	6.8
0	(8+9)-II-2	-4500	-5.25	32.00	6.1	-1.27	20.00	16	V	6.1
0	(8+9)-IV-1	3429	4.00	32.00	8.0	0.97	20.00	21	V	8.0
0	(8+9)-II-3	4772	5.57	32.00	5.7	1.35	20.00	15	V	5.7
0	(8+9)-VIII-2	-4963	-5.79	32.00	5.5	-1.40	20.00	14	V	5.5
0	(8+9)-VI-2	-4520	-5.28	32.00	6.1	-1.28	20.00	16	V	6.1
0	(8+9)-VII-2	-4163	-4.86	32.00	6.6	-1.18	20.00	17	V	6.6
0	(8+9)-III-1	-1585	-1.85	32.00	17	-0.45	20.00	45	V	17
0	(8+9)-VI-3	4791	5.59	32.00	5.7	1.35	20.00	15	V	5.7
0	(8+9)-III-2	-4097	-4.78	32.00	6.7	-1.16	20.00	17	V	6.7
0	(8+9)-I-2	-3964	-4.63	32.00	6.9	-1.12	20.00	18	V	6.9
0	(8+9)-III-3	4369	5.10	32.00	6.3	1.23	20.00	16	V	6.3
0	(8+9)-I-4	1990	2.32	32.00	14	0.56	20.00	36	V	14
0	(8+9)-III-4	1857	2.17	32.00	15	0.52	20.00	38	V	15
0	(8+9)-VIII-3	5235	6.11	32.00	5.2	1.48	20.00	14	V	5.2
0	(8+9)-VII-1	-1651	-1.93	32.00	17	-0.47	20.00	43	V	17
0	(8+9)-IV-2	-4944	-5.77	32.00	5.5	-1.40	20.00	14	V	5.5
0	(8+9)-I-3	4235	4.94	32.00	6.5	1.20	20.00	17	V	6.5
0	(8+9)-VII-3	4435	5.18	32.00	6.2	1.25	20.00	16	V	6.2
0	(8+9)-I-1	-1718	-2.01	32.00	16	-0.49	20.00	41	V	16
0	(8+9)-II-1	2986	3.49	32.00	9.2	0.84	20.00	24	V	9.2
0	(8+9)-IV-3	5215	6.09	32.00	5.3	1.47	20.00	14	V	5.3
0	(8+9)-V-3	4301	5.02	32.00	6.4	1.22	20.00	16	V	6.4
0	(8+9)-V-1	-1784	-2.08	32.00	15	-0.50	20.00	40	V	15
3200	1	-530	-0.62	19.20	31	-0.15	12.00	80	V	31
3200	2	-1106	-1.29	28.80	22	-0.31	18.00	58	V	22
3200	3	-1106	-1.29	28.80	22	-0.31	18.00	58	V	22
3200	4	-530	-0.62	25.60	41	-0.15	16.00	>100	V	41
3200	5	-530	-0.62	25.60	41	-0.15	16.00	>100	V	41
3200	6	-530	-0.62	25.60	41	-0.15	16.00	>100	V	41
3200	7	-530	-0.62	25.60	41	-0.15	16.00	>100	V	41
3200	(8+9)-VIII-4	-4344	-5.07	32.00	6.3	-1.23	20.00	16	V	6.3
3200	(8+9)-VI-4	-4146	-4.84	32.00	6.6	-1.17	20.00	17	V	6.6
3200	(8+9)-II-4	-3685	-4.30	32.00	7.4	-1.04	20.00	19	V	7.4
3200	(8+9)-VII-4	-2189	-2.55	32.00	13	-0.62	20.00	32	V	13
3200	(8+9)-VIII-1	3624	4.23	32.00	7.6	1.02	20.00	20	V	7.6
3200	(8+9)-VI-1	3427	4.00	32.00	8.0	0.97	20.00	21	V	8.0
3200	(8+9)-V-4	-2130	-2.49	32.00	13	-0.60	20.00	33	V	13
3200	(8+9)-IV-4	-3883	-4.53	32.00	7.1	-1.10	20.00	18	V	7.1
Verifiche nella direzione secondaria										
885	1	252	0.16	19.20	>100	0.04	12.00	>100	V	>100
885	2	529	0.34	28.80	84	0.08	18.00	>100	V	84
885	3	529	0.34	28.80	84	0.08	18.00	>100	V	84
885	4	252	0.16	25.60	>100	0.04	16.00	>100	V	>100
885	5	252	0.16	25.60	>100	0.04	16.00	>100	V	>100
885	6	252	0.16	25.60	>100	0.04	16.00	>100	V	>100
885	7	252	0.16	25.60	>100	0.04	16.00	>100	V	>100
885	(8+9)-VIII-4	6346	4.10	32.00	7.8	0.99	20.00	20	V	7.8
885	(8+9)-IV-2	9785	6.32	32.00	5.1	1.53	20.00	13	V	5.1
885	(8+9)-V-1	3932	2.54	32.00	13	0.61	20.00	33	V	13
885	(8+9)-I-2	7888	5.09	32.00	6.3	1.23	20.00	16	V	6.3
885	(8+9)-V-2	8214	5.30	32.00	6.0	1.28	20.00	16	V	6.0
885	(8+9)-I-4	-3249	-2.10	32.00	15	-0.51	20.00	39	V	15
885	(8+9)-V-3	-7856	-5.07	32.00	6.3	-1.23	20.00	16	V	6.3
885	(8+9)-II-2	8985	5.80	32.00	5.5	1.40	20.00	14	V	5.5
885	(8+9)-V-4	-3575	-2.31	32.00	14	-0.56	20.00	36	V	14
885	(8+9)-II-4	5644	3.64	32.00	8.8	0.88	20.00	23	V	8.8
885	(8+9)-VI-1	-5188	-3.35	32.00	9.6	-0.81	20.00	25	V	9.6
885	(8+9)-III-2	8128	5.25	32.00	6.1	1.27	20.00	16	V	6.1
885	(8+9)-VI-2	9082	5.86	32.00	5.5	1.42	20.00	14	V	5.5
885	(8+9)-III-4	-3009	-1.94	32.00	16	-0.47	20.00	43	V	16
885	(8+9)-VI-3	-8724	-5.63	32.00	5.7	-1.36	20.00	15	V	5.7

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
885	(8+9)-I-1	3607	2.33	32.00	14	0.56	20.00	35	V	14
885	(8+9)-VI-4	5546	3.58	32.00	8.9	0.87	20.00	23	V	8.9
885	(8+9)-IV-4	6444	4.16	32.00	7.7	1.01	20.00	20	V	7.7
885	(8+9)-VII-1	3692	2.38	32.00	13	0.58	20.00	35	V	13
885	(8+9)-II-1	-5286	-3.41	32.00	9.4	-0.83	20.00	24	V	9.4
885	(8+9)-VII-2	8454	5.46	32.00	5.9	1.32	20.00	15	V	5.9
885	(8+9)-III-1	3367	2.17	32.00	15	0.53	20.00	38	V	15
885	(8+9)-VII-3	-8096	-5.23	32.00	6.1	-1.26	20.00	16	V	6.1
885	(8+9)-IV-1	-6086	-3.93	32.00	8.1	-0.95	20.00	21	V	8.1
885	(8+9)-VII-4	-3334	-2.15	32.00	15	-0.52	20.00	38	V	15
885	(8+9)-III-3	-7770	-5.02	32.00	6.4	-1.21	20.00	16	V	6.4
885	(8+9)-IV-3	-9427	-6.09	32.00	5.3	-1.47	20.00	14	V	5.3
885	(8+9)-II-3	-8627	-5.57	32.00	5.7	-1.35	20.00	15	V	5.7
885	(8+9)-VIII-1	-5988	-3.87	32.00	8.3	-0.94	20.00	21	V	8.3
885	(8+9)-VIII-2	9883	6.38	32.00	5.0	1.54	20.00	13	V	5.0
885	(8+9)-VIII-3	-9525	-6.15	32.00	5.2	-1.49	20.00	13	V	5.2
885	(8+9)-I-3	-7530	-4.86	32.00	6.6	-1.18	20.00	17	V	6.6

Setto 16: origine (950.1,559.1,296.9), direzione (-0.612129,0.790758,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	1	104	-1	-127	0.29	-0.12	-4.23	79.20	115.20	115.20	24
0	2	79	-1	-217	0.22	-0.07	-7.21	118.80	172.80	172.80	23
0	3	79	-1	-217	0.22	-0.07	-7.21	118.80	172.80	172.80	23
0	4	104	-1	-127	0.29	-0.12	-4.23	105.60	153.60	153.60	32
0	5	104	-1	-127	0.29	-0.12	-4.23	105.60	153.60	153.60	32
0	6	104	-1	-127	0.29	-0.12	-4.23	105.60	153.60	153.60	32
0	7	104	-1	-127	0.29	-0.12	-4.23	105.60	153.60	153.60	32
0	(8+9)-VIII-4	-7286	279	-699	-20.14	28.95	-23.28	132.00	192.00	192.00	3.5
0	(8+9)-IV-1	7501	-212	542	20.73	-22.01	18.04	132.00	192.00	192.00	2.7
0	(8+9)-V-1	-4600	144	-446	-12.72	14.98	-14.84	132.00	192.00	192.00	6.3
0	(8+9)-I-2	-9669	385	-823	-26.72	40.00	-27.39	132.00	192.00	192.00	2.7
0	(8+9)-V-2	-9868	157	-883	-27.28	16.28	-29.39	132.00	192.00	192.00	3.9
0	(8+9)-I-4	4556	-374	210	12.59	-38.88	7.00	132.00	192.00	192.00	3.0
0	(8+9)-V-3	10024	-159	708	27.71	-16.46	23.56	132.00	192.00	192.00	2.4
0	(8+9)-II-2	-10836	134	-972	-29.95	13.91	-32.33	132.00	192.00	192.00	3.8
0	(8+9)-V-4	4756	-146	271	13.14	-15.16	9.00	132.00	192.00	192.00	4.4
0	(8+9)-VIII-1	7441	-281	524	20.57	-29.13	17.44	132.00	192.00	192.00	2.5
0	(8+9)-III-1	-4168	281	-369	-11.52	29.22	-12.28	132.00	192.00	192.00	4.6
0	(8+9)-III-2	-9902	477	-840	-27.37	49.48	-27.95	132.00	192.00	192.00	2.4
0	(8+9)-III-4	4323	-283	194	11.95	-29.40	6.44	132.00	192.00	192.00	3.6
0	(8+9)-VI-2	-10896	65	-990	-30.12	6.80	-32.93	132.00	192.00	192.00	4.3
0	(8+9)-IV-2	-11613	438	-1028	-32.10	45.50	-34.19	132.00	192.00	192.00	2.3
0	(8+9)-VI-3	11051	-67	814	30.55	-6.98	27.10	132.00	192.00	192.00	2.4
0	(8+9)-IV-4	-7345	210	-718	-20.30	21.83	-23.88	132.00	192.00	192.00	4.0
0	(8+9)-VIII-2	-11673	370	-1046	-32.26	38.38	-34.80	132.00	192.00	192.00	2.4
0	(8+9)-VIII-3	11828	-371	870	32.69	-38.56	28.96	132.00	192.00	192.00	1.7
0	(8+9)-VII-1	-4367	53	-429	-12.07	5.51	-14.28	132.00	192.00	192.00	9.3
0	(8+9)-III-3	10057	-478	664	27.80	-49.66	22.11	132.00	192.00	192.00	1.7
0	(8+9)-IV-3	11768	-440	852	32.53	-45.67	28.36	132.00	192.00	192.00	1.6
0	(8+9)-I-3	9824	-387	648	27.15	-40.18	21.55	132.00	192.00	192.00	1.9
0	(8+9)-II-3	10991	-136	796	30.38	-14.09	26.50	132.00	192.00	192.00	2.3
0	(8+9)-I-1	-4401	373	-386	-12.16	38.70	-12.83	132.00	192.00	192.00	3.7
0	(8+9)-VII-2	-10101	248	-900	-27.92	25.76	-29.95	132.00	192.00	192.00	3.2
0	(8+9)-VII-3	10257	-250	725	28.35	-25.94	24.12	132.00	192.00	192.00	2.1
0	(8+9)-VII-4	4523	-55	254	12.50	-5.69	8.45	132.00	192.00	192.00	5.9
3200	(8+9)-II-4	-6077	788	802	-7.53	36.69	5.36	132.00	192.00	192.00	4.5
3200	(8+9)-VI-4	-6024	609	762	-7.46	28.36	5.10	132.00	192.00	192.00	5.7
3200	(8+9)-II-1	5048	-788	-1307	6.26	-36.70	-8.74	132.00	192.00	192.00	3.5
3200	(8+9)-VI-1	4995	-609	-1267	6.19	-28.37	-8.47	132.00	192.00	192.00	4.2
Verifiche nella direzione secondaria											
0	(8+9)-VIII-4	-843	24	4515	-0.54	0.88	5.47	132.00	192.00	192.00	30

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-VI-2	-759	18	6376	-0.49	0.67	7.72	132.00	192.00	192.00	23
0	(8+9)-VI-4	-966	16	3956	-0.62	0.60	4.79	132.00	192.00	192.00	36
0	(8+9)-IV-2	-601	13	6887	-0.39	0.47	8.34	132.00	192.00	192.00	22
0	(8+9)-III-2	-586	-27	5794	-0.38	-1.01	7.01	132.00	192.00	192.00	24
0	(8+9)-VIII-2	-636	26	6935	-0.41	0.95	8.40	132.00	192.00	192.00	21
0	(8+9)-III-3	-1778	43	-5212	-1.15	1.57	-6.31	132.00	192.00	192.00	24
0	(8+9)-VII-4	-1394	10	-2112	-0.90	0.37	-2.56	132.00	192.00	192.00	66
0	(8+9)-VI-3	-1605	-3	-5794	-1.04	-0.10	-7.01	132.00	192.00	192.00	27
0	(8+9)-VII-2	-704	16	5955	-0.45	0.58	7.21	132.00	192.00	192.00	25
0	(8+9)-IV-1	-1485	-21	-3981	-0.96	-0.79	-4.82	132.00	192.00	192.00	34
0	(8+9)-I-3	-1741	45	-5044	-1.12	1.66	-6.11	132.00	192.00	192.00	25
0	(8+9)-II-1	-1362	-14	-3422	-0.88	-0.51	-4.14	132.00	192.00	192.00	41
0	(8+9)-IV-3	-1763	3	-6305	-1.14	0.10	-7.63	132.00	192.00	192.00	25
0	(8+9)-II-3	-1640	10	-5745	-1.06	0.37	-6.96	132.00	192.00	192.00	26
0	(8+9)-IV-4	-879	37	4563	-0.57	1.36	5.52	132.00	192.00	192.00	28
0	(8+9)-VIII-3	-1728	-10	-6353	-1.12	-0.38	-7.69	132.00	192.00	192.00	24
0	(8+9)-V-1	-932	8	2862	-0.60	0.28	3.46	132.00	192.00	192.00	51
0	(8+9)-VII-3	-1660	-0	-5373	-1.07	-0.01	-6.50	132.00	192.00	192.00	29
0	(8+9)-V-2	-741	13	5787	-0.48	0.50	7.01	132.00	192.00	192.00	26
0	(8+9)-VII-1	-969	5	2694	-0.63	0.20	3.26	132.00	192.00	192.00	55
0	(8+9)-II-4	-1001	29	4004	-0.65	1.08	4.85	132.00	192.00	192.00	32
0	(8+9)-VIII-1	-1520	-9	-3933	-0.98	-0.32	-4.76	132.00	192.00	192.00	38
0	(8+9)-I-2	-623	-30	5626	-0.40	-1.09	6.81	132.00	192.00	192.00	24
0	(8+9)-II-2	-723	5	6327	-0.47	0.19	7.66	132.00	192.00	192.00	24
0	(8+9)-V-3	-1623	2	-5205	-1.05	0.07	-6.30	132.00	192.00	192.00	30
0	(8+9)-V-4	-1431	8	-2280	-0.92	0.28	-2.76	132.00	192.00	192.00	63
0	(8+9)-VI-1	-1398	-1	-3373	-0.90	-0.04	-4.08	132.00	192.00	192.00	47
556	1	-1146	7	-451	-0.82	0.29	-0.66	79.20	115.20	115.20	>100
556	2	-2000	12	-831	-1.43	0.49	-1.23	118.80	172.80	172.80	100
556	3	-2000	12	-831	-1.43	0.49	-1.23	118.80	172.80	172.80	100
556	4	-1146	7	-451	-0.82	0.29	-0.66	105.60	153.60	153.60	>100
556	5	-1146	7	-451	-0.82	0.29	-0.66	105.60	153.60	153.60	>100
556	6	-1146	7	-451	-0.82	0.29	-0.66	105.60	153.60	153.60	>100
556	7	-1146	7	-451	-0.82	0.29	-0.66	105.60	153.60	153.60	>100
556	(8+9)-I-1	-722	110	338	-0.51	4.49	0.50	132.00	192.00	192.00	38
556	(8+9)-I-4	-844	-100	-961	-0.60	-4.09	-1.42	132.00	192.00	192.00	35
556	(8+9)-III-1	-739	116	284	-0.53	4.75	0.42	132.00	192.00	192.00	37
556	(8+9)-III-4	-827	-107	-907	-0.59	-4.35	-1.34	132.00	192.00	192.00	34

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Ty kg	τ_d kg/cmq	fvd kg/cmq	RS	Cs
0	(8+9)-VI-4	-114	0.23	6.40	Si	28
0	(8+9)-V-1	12	0.02	6.40	Si	>100
0	(8+9)-IV-4	-101	0.20	6.40	Si	31
0	(8+9)-II-2	-96	0.19	6.40	Si	33
0	(8+9)-VIII-3	84	0.17	6.40	Si	38
0	(8+9)-II-3	96	0.19	6.40	Si	33
0	(8+9)-VIII-1	69	0.14	6.40	Si	46
0	(8+9)-II-4	-146	0.29	6.40	Si	22
0	(8+9)-VII-2	-48	0.10	6.40	Si	67
0	(8+9)-VIII-4	-69	0.14	6.40	Si	46
0	(8+9)-VI-2	-129	0.26	6.40	Si	25
0	(8+9)-V-4	-11	0.02	6.40	Si	>100
0	(8+9)-V-3	62	0.12	6.40	Si	52
0	(8+9)-VIII-2	-84	0.17	6.40	Si	38
0	(8+9)-V-2	-61	0.12	6.40	Si	52
0	(8+9)-VI-3	129	0.26	6.40	Si	25
0	(8+9)-II-1	147	0.30	6.40	Si	22
0	(8+9)-VII-3	48	0.10	6.40	Si	66
0	(8+9)-VI-1	114	0.23	6.40	Si	28
0	(8+9)-IV-1	102	0.20	6.40	Si	31
0	(8+9)-IV-2	-51	0.10	6.40	Si	63

X	Comb.	Ty	τ_d	fvd	RS	Cs
0	(8+9)-IV-3	51	0.10	6.40	Si	62
1600	(8+9)-III-1	-242	0.30	6.40	Si	21
1600	(8+9)-III-2	-185	0.23	6.40	Si	28
1600	(8+9)-III-4	242	0.30	6.40	Si	21
1600	(8+9)-III-3	185	0.23	6.40	Si	28
1600	(8+9)-I-4	221	0.27	6.40	Si	23
1600	(8+9)-I-3	206	0.26	6.40	Si	25
1600	(8+9)-I-2	-206	0.26	6.40	Si	25
1600	(8+9)-I-1	-221	0.27	6.40	Si	23
3200	1	-7	0.01	3.84	Si	>100
3200	2	-13	0.01	5.76	Si	>100
3200	3	-13	0.01	5.76	Si	>100
3200	4	-7	0.01	5.12	Si	>100
3200	5	-7	0.01	5.12	Si	>100
3200	6	-7	0.01	5.12	Si	>100
3200	7	-7	0.01	5.12	Si	>100
3200	(8+9)-VII-1	-51	0.05	6.40	Si	>100
3200	(8+9)-VII-4	42	0.04	6.40	Si	>100
Verifiche nella direzione secondaria						
0	(8+9)-II-2	-67	0.04	6.40	Si	>100
0	(8+9)-VII-3	35	0.02	6.40	Si	>100
0	(8+9)-VI-3	141	0.08	6.40	Si	76
0	(8+9)-VI-2	-131	0.08	6.40	Si	82
0	(8+9)-IV-3	62	0.04	6.40	Si	>100
0	(8+9)-IV-2	-52	0.03	6.40	Si	>100
0	(8+9)-II-3	77	0.05	6.40	Si	>100
556	1	8	0.01	3.84	Si	>100
556	2	12	0.01	5.76	Si	>100
556	3	12	0.01	5.76	Si	>100
556	4	8	0.01	5.12	Si	>100
556	5	8	0.01	5.12	Si	>100
556	6	8	0.01	5.12	Si	>100
556	7	8	0.01	5.12	Si	>100
556	(8+9)-VIII-4	-164	0.11	6.40	Si	59
556	(8+9)-V-1	119	0.08	6.40	Si	82
556	(8+9)-I-2	341	0.22	6.40	Si	29
556	(8+9)-VI-1	146	0.10	6.40	Si	67
556	(8+9)-III-2	332	0.22	6.40	Si	29
556	(8+9)-II-1	233	0.15	6.40	Si	42
556	(8+9)-III-4	-408	0.27	6.40	Si	24
556	(8+9)-I-4	-399	0.26	6.40	Si	24
556	(8+9)-III-1	420	0.28	6.40	Si	23
556	(8+9)-VI-4	-134	0.09	6.40	Si	73
556	(8+9)-IV-4	-251	0.17	6.40	Si	39
556	(8+9)-VII-1	128	0.08	6.40	Si	76
556	(8+9)-V-2	49	0.03	6.40	Si	>100
556	(8+9)-VII-2	40	0.03	6.40	Si	>100
556	(8+9)-V-4	-107	0.07	6.40	Si	91
556	(8+9)-I-3	-329	0.22	6.40	Si	30
556	(8+9)-IV-1	263	0.17	6.40	Si	37
556	(8+9)-VII-4	-116	0.08	6.40	Si	84
556	(8+9)-III-3	-320	0.21	6.40	Si	30
556	(8+9)-II-4	-222	0.15	6.40	Si	44
556	(8+9)-V-3	-38	0.02	6.40	Si	>100
556	(8+9)-VIII-1	175	0.12	6.40	Si	55
556	(8+9)-VIII-2	-117	0.08	6.40	Si	83
556	(8+9)-VIII-3	128	0.08	6.40	Si	76
556	(8+9)-I-1	411	0.27	6.40	Si	24

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	(8+9)-VIII-4	-1385	-5.74	32.00	5.6	-1.39	20.00	14	V	5.6

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
0	(8+9)-IV-1	916	3.80	32.00	8.4	0.92	20.00	22	V	8.4
0	(8+9)-VI-2	-1918	-7.95	32.00	4.0	-1.92	20.00	10	V	4.0
0	(8+9)-III-1	-834	-3.46	32.00	9.3	-0.84	20.00	24	V	9.3
0	(8+9)-IV-2	-2026	-8.40	32.00	3.8	-2.03	20.00	9.8	V	3.8
0	(8+9)-III-2	-1717	-7.12	32.00	4.5	-1.72	20.00	12	V	4.5
0	(8+9)-VIII-2	-2050	-8.50	32.00	3.8	-2.06	20.00	9.7	V	3.8
0	(8+9)-III-3	1224	5.08	32.00	6.3	1.23	20.00	16	V	6.3
0	(8+9)-VII-3	1303	5.40	32.00	5.9	1.31	20.00	15	V	5.9
0	(8+9)-VII-1	-913	-3.79	32.00	8.5	-0.92	20.00	22	V	8.5
0	(8+9)-I-2	-1677	-6.95	32.00	4.6	-1.68	20.00	12	V	4.6
0	(8+9)-VI-4	-1253	-5.20	32.00	6.2	-1.26	20.00	16	V	6.2
0	(8+9)-VII-2	-1796	-7.45	32.00	4.3	-1.80	20.00	11	V	4.3
0	(8+9)-II-2	-1895	-7.86	32.00	4.1	-1.90	20.00	11	V	4.1
0	(8+9)-IV-3	1534	6.36	32.00	5.0	1.54	20.00	13	V	5.0
0	(8+9)-II-4	-1277	-5.30	32.00	6.0	-1.28	20.00	16	V	6.0
0	(8+9)-IV-4	-1409	-5.84	32.00	5.5	-1.41	20.00	14	V	5.5
0	(8+9)-VIII-1	893	3.70	32.00	8.6	0.90	20.00	22	V	8.6
0	(8+9)-V-1	-952	-3.95	32.00	8.1	-0.96	20.00	21	V	8.1
0	(8+9)-I-3	1185	4.91	32.00	6.5	1.19	20.00	17	V	6.5
0	(8+9)-V-2	-1756	-7.28	32.00	4.4	-1.76	20.00	11	V	4.4
0	(8+9)-II-3	1402	5.81	32.00	5.5	1.41	20.00	14	V	5.5
0	(8+9)-I-1	-873	-3.62	32.00	8.8	-0.88	20.00	23	V	8.8
0	(8+9)-II-1	785	3.25	32.00	9.8	0.79	20.00	25	V	9.8
0	(8+9)-VIII-3	1558	6.46	32.00	5.0	1.56	20.00	13	V	5.0
0	(8+9)-V-3	1264	5.24	32.00	6.1	1.27	20.00	16	V	6.1
0	(8+9)-VI-3	1426	5.91	32.00	5.4	1.43	20.00	14	V	5.4
0	(8+9)-VI-1	761	3.16	32.00	10	0.76	20.00	26	V	10
3200	1	809	1.50	19.20	13	0.36	12.00	33	V	13
3200	2	1330	2.47	28.80	12	0.60	18.00	30	V	12
3200	3	1330	2.47	28.80	12	0.60	18.00	30	V	12
3200	4	809	1.50	25.60	17	0.36	16.00	44	V	17
3200	5	809	1.50	25.60	17	0.36	16.00	44	V	17
3200	6	809	1.50	25.60	17	0.36	16.00	44	V	17
3200	7	809	1.50	25.60	17	0.36	16.00	44	V	17
3200	(8+9)-VII-4	1275	2.37	32.00	13	0.57	20.00	35	V	13
3200	(8+9)-I-4	1271	2.36	32.00	14	0.57	20.00	35	V	14
3200	(8+9)-III-4	1221	2.27	32.00	14	0.55	20.00	36	V	14
3200	(8+9)-V-4	1326	2.46	32.00	13	0.60	20.00	34	V	13
Verifiche nella direzione secondaria										
556	1	-867	-0.62	19.20	31	-0.15	12.00	80	V	31
556	2	-1464	-1.04	28.80	28	-0.25	18.00	71	V	28
556	3	-1464	-1.04	28.80	28	-0.25	18.00	71	V	28
556	4	-867	-0.62	25.60	41	-0.15	16.00	>100	V	41
556	5	-867	-0.62	25.60	41	-0.15	16.00	>100	V	41
556	6	-867	-0.62	25.60	41	-0.15	16.00	>100	V	41
556	7	-867	-0.62	25.60	41	-0.15	16.00	>100	V	41
556	(8+9)-VIII-4	4818	3.43	32.00	9.3	0.83	20.00	24	V	9.3
556	(8+9)-IV-2	7793	5.55	32.00	5.8	1.34	20.00	15	V	5.8
556	(8+9)-V-1	2560	1.82	32.00	18	0.44	20.00	45	V	18
556	(8+9)-I-2	6151	4.38	32.00	7.3	1.06	20.00	19	V	7.3
556	(8+9)-V-2	6326	4.51	32.00	7.1	1.09	20.00	18	V	7.1
556	(8+9)-I-4	-3589	-2.56	32.00	13	-0.62	20.00	32	V	13
556	(8+9)-V-3	-7530	-5.37	32.00	6.0	-1.30	20.00	15	V	6.0
556	(8+9)-II-2	7135	5.09	32.00	6.3	1.23	20.00	16	V	6.3
556	(8+9)-V-4	-3764	-2.68	32.00	12	-0.65	20.00	31	V	12
556	(8+9)-II-4	4213	3.00	32.00	11	0.73	20.00	28	V	11
556	(8+9)-VI-1	-5365	-3.82	32.00	8.4	-0.93	20.00	22	V	8.4
556	(8+9)-III-2	6348	4.52	32.00	7.1	1.09	20.00	18	V	7.1
556	(8+9)-VI-2	7188	5.12	32.00	6.2	1.24	20.00	16	V	6.2
556	(8+9)-III-4	-3392	-2.42	32.00	13	-0.58	20.00	34	V	13
556	(8+9)-VI-3	-8392	-5.98	32.00	5.4	-1.45	20.00	14	V	5.4
556	(8+9)-I-1	2385	1.70	32.00	19	0.41	20.00	49	V	19
556	(8+9)-VI-4	4161	2.97	32.00	11	0.72	20.00	28	V	11
556	(8+9)-IV-4	4871	3.47	32.00	9.2	0.84	20.00	24	V	9.2

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
556	(8+9)-VII-1	2363	1.68	32.00	19	0.41	20.00	49	V	19
556	(8+9)-II-1	-5418	-3.86	32.00	8.3	-0.93	20.00	21	V	8.3
556	(8+9)-VII-2	6523	4.65	32.00	6.9	1.13	20.00	18	V	6.9
556	(8+9)-III-1	2188	1.56	32.00	21	0.38	20.00	53	V	21
556	(8+9)-VII-3	-7727	-5.51	32.00	5.8	-1.33	20.00	15	V	5.8
556	(8+9)-IV-1	-6075	-4.33	32.00	7.4	-1.05	20.00	19	V	7.4
556	(8+9)-VII-4	-3567	-2.54	32.00	13	-0.62	20.00	33	V	13
556	(8+9)-III-3	-7552	-5.38	32.00	5.9	-1.30	20.00	15	V	5.9
556	(8+9)-IV-3	-8997	-6.41	32.00	5.0	-1.55	20.00	13	V	5.0
556	(8+9)-II-3	-8340	-5.94	32.00	5.4	-1.44	20.00	14	V	5.4
556	(8+9)-VIII-1	-6022	-4.29	32.00	7.5	-1.04	20.00	19	V	7.5
556	(8+9)-VIII-2	7845	5.59	32.00	5.7	1.35	20.00	15	V	5.7
556	(8+9)-VIII-3	-9049	-6.45	32.00	5.0	-1.56	20.00	13	V	5.0
556	(8+9)-I-3	-7355	-5.24	32.00	6.1	-1.27	20.00	16	V	6.1

Verifiche a instabilità

Setto(X)	Comb.	k _{critc}	k _{critm}	λ_{relc}	λ_{relm}	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
(cm)						kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	
13(20.0)	(8+9)-IV-3	--	--	--	--	2.92	13.98	-11.26	132.00	192.00	192.00	6.5
14(119.0)	(8+9)-IV-3	--	--	--	--	1.83	-7.12	-12.41	132.00	192.00	192.00	8.7
15(0.0)	(8+9)-VIII-3	0.63	--	1.16	--	-5.89	0.70	13.38	132.00	192.00	192.00	8.2
16(0.0)	(8+9)-IV-2	0.63	--	1.16	--	-32.10	45.50	-34.19	132.00	192.00	192.00	1.5

Parete Xlam 11 - Nodi: [6-14-103-104] - **Crit.Prog.** Criterio di verifica XLAM 0 - **Verificato:**
[Cs=1.528,Comb=(8+9)-III-3]

Geometria setti

Setto	Crit.	X	L	S	X90	L90	S90
		mm	cm	cm	mm	cm	cm
17	Criterio di verifica XLAM 0	0	387.0	12.1	0	40.0	12.1
		200	387.0	12.1	1935	40.0	12.1
		400	387.0	12.1	3870	40.0	12.1
18	Criterio di verifica XLAM 0	0	387.0	12.1	0	45.3	12.1
		227	387.0	12.1	1935	45.3	12.1
		453	387.0	12.1	3870	45.3	12.1
19	Criterio di verifica XLAM 0	0	90.0	12.1	0	530.0	12.1
		2650	90.0	12.1	450	530.0	12.1
		5300	90.0	12.1	900	530.0	12.1
20	Criterio di verifica XLAM 0	0	117.0	12.1	0	530.0	12.1
		2650	117.0	12.1	585	530.0	12.1
		5300	117.0	12.1	1170	530.0	12.1

Setto 17: origine (390.4,1283.3,193.5), direzione (-0.611124,0.791535,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	
0	(8+9)-III-2	1005	29	-12562	0.36	0.39	-6.93	132.00	192.00	192.00	24
0	(8+9)-I-2	938	28	-12132	0.33	0.38	-6.69	132.00	192.00	192.00	25
0	(8+9)-VIII-4	752	-23	-9412	0.27	-0.31	-5.19	132.00	192.00	192.00	33
0	(8+9)-V-2	1203	12	-13703	0.43	0.16	-7.56	132.00	192.00	192.00	23
0	(8+9)-VII-4	-1082	-32	6847	-0.39	-0.43	3.78	132.00	192.00	192.00	46
0	(8+9)-V-1	470	19	-6921	0.17	0.25	-3.82	132.00	192.00	192.00	45
0	(8+9)-VII-1	403	18	-6491	0.14	0.24	-3.58	132.00	192.00	192.00	48
0	(8+9)-IV-4	831	-28	-9883	0.30	-0.37	-5.45	132.00	192.00	192.00	31
0	(8+9)-V-4	-1149	-32	7277	-0.41	-0.43	4.02	132.00	192.00	192.00	43
0	(8+9)-II-2	1156	-6	-13802	0.41	-0.09	-7.62	132.00	192.00	192.00	23

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-VI-2	1235	-11	-14273	0.44	-0.15	-7.88	132.00	192.00	192.00	22
0	(8+9)-V-3	-1882	-26	14059	-0.67	-0.34	7.76	132.00	192.00	192.00	24
0	(8+9)-VII-2	1269	12	-14133	0.45	0.17	-7.80	132.00	192.00	192.00	22
0	(8+9)-IV-2	1378	-5	-15234	0.49	-0.06	-8.41	132.00	192.00	192.00	21
0	(8+9)-II-4	609	-30	-8451	0.22	-0.39	-4.66	132.00	192.00	192.00	36
0	(8+9)-VIII-2	1457	-10	-15706	0.52	-0.13	-8.67	132.00	192.00	192.00	20
200	1	-1005	-13	843	-0.36	-0.18	0.47	79.20	115.20	115.20	>100
200	2	-1969	-30	1687	-0.70	-0.41	0.93	118.80	172.80	172.80	>100
200	3	-1969	-30	1687	-0.70	-0.41	0.93	118.80	172.80	172.80	>100
200	4	-1005	-13	843	-0.36	-0.18	0.47	105.60	153.60	153.60	>100
200	5	-1005	-13	843	-0.36	-0.18	0.47	105.60	153.60	153.60	>100
200	6	-1005	-13	843	-0.36	-0.18	0.47	105.60	153.60	153.60	>100
200	7	-1005	-13	843	-0.36	-0.18	0.47	105.60	153.60	153.60	>100
200	(8+9)-IV-1	-1436	15	11060	-0.51	0.20	6.10	132.00	192.00	192.00	30
200	(8+9)-III-3	-1698	-54	14156	-0.60	-0.73	7.81	132.00	192.00	192.00	22
200	(8+9)-IV-3	-1866	-14	16804	-0.66	-0.19	9.27	132.00	192.00	192.00	20
200	(8+9)-I-3	-1644	-49	13717	-0.59	-0.66	7.57	132.00	192.00	192.00	23
200	(8+9)-II-3	-1686	3	15341	-0.60	0.04	8.47	132.00	192.00	192.00	23
200	(8+9)-I-4	-1178	-65	6582	-0.42	-0.87	3.63	132.00	192.00	192.00	43
200	(8+9)-VII-3	-1588	-31	14395	-0.57	-0.42	7.94	132.00	192.00	192.00	23
200	(8+9)-II-1	-1257	32	9597	-0.45	0.43	5.30	132.00	192.00	192.00	34
200	(8+9)-VI-4	-101	-42	-8373	-0.04	-0.57	-4.62	132.00	192.00	192.00	37
200	(8+9)-VI-1	-1290	25	9525	-0.46	0.33	5.26	132.00	192.00	192.00	34
200	(8+9)-VI-3	-1653	10	15412	-0.59	0.13	8.50	132.00	192.00	192.00	22
200	(8+9)-VIII-3	-1833	-7	16875	-0.65	-0.10	9.31	132.00	192.00	192.00	20
200	(8+9)-VIII-1	-1469	8	10988	-0.52	0.10	6.06	132.00	192.00	192.00	31
200	(8+9)-III-4	-1125	-60	6143	-0.40	-0.80	3.39	132.00	192.00	192.00	46
400	(8+9)-I-1	-415	73	-4976	-0.15	0.97	-2.75	132.00	192.00	192.00	52
400	(8+9)-III-1	-467	64	-4563	-0.17	0.85	-2.52	132.00	192.00	192.00	57
Verifiche nella direzione secondaria											
0	(8+9)-VIII-4	-6171	44	826	-31.88	13.14	64.03	132.00	192.00	192.00	2.3
0	(8+9)-VII-2	184	-107	554	0.95	-31.76	42.92	132.00	192.00	192.00	2.5
0	(8+9)-III-3	1733	101	-1070	8.95	29.75	-82.92	132.00	192.00	192.00	1.5
0	(8+9)-IV-2	-5766	-20	1163	-29.78	-5.78	90.08	132.00	192.00	192.00	1.9
0	(8+9)-III-4	-1169	106	-567	-6.04	31.31	-43.92	132.00	192.00	192.00	2.5
0	(8+9)-VIII-2	-4801	-23	972	-24.80	-6.75	75.29	132.00	192.00	192.00	2.3
0	(8+9)-IV-1	3908	-37	-515	20.19	-10.99	-39.92	132.00	192.00	192.00	2.4
0	(8+9)-VII-4	-4384	117	70	-22.65	34.52	5.40	132.00	192.00	192.00	4.5
0	(8+9)-I-1	-364	-100	720	-1.88	-29.48	55.82	132.00	192.00	192.00	2.3
0	(8+9)-IV-3	4467	24	-1042	23.07	6.98	-80.77	132.00	192.00	192.00	1.6
0	(8+9)-I-3	1499	103	-1037	7.74	30.40	-80.33	132.00	192.00	192.00	1.6
0	(8+9)-IV-4	-5207	41	636	-26.89	12.18	49.24	132.00	192.00	192.00	2.9
0	(8+9)-II-1	3128	-30	-404	16.16	-8.84	-31.29	132.00	192.00	192.00	3.0
0	(8+9)-V-1	2852	-111	84	14.73	-32.68	6.51	132.00	192.00	192.00	3.2
0	(8+9)-II-3	3687	31	-931	19.04	9.13	-72.14	132.00	192.00	192.00	1.8
0	(8+9)-V-2	418	-110	521	2.16	-32.41	40.33	132.00	192.00	192.00	2.5
0	(8+9)-III-1	-130	-102	687	-0.67	-30.12	53.23	132.00	192.00	192.00	2.3
0	(8+9)-V-3	-1716	114	-400	-8.87	33.60	-31.02	132.00	192.00	192.00	3.0
0	(8+9)-VIII-3	3502	27	-851	18.09	7.94	-65.97	132.00	192.00	192.00	1.9
0	(8+9)-V-4	-4150	115	36	-21.44	33.87	2.81	132.00	192.00	192.00	4.9
0	(8+9)-VII-3	-1482	112	-434	-7.66	32.96	-33.60	132.00	192.00	192.00	2.9
0	(8+9)-VI-1	4093	-33	-595	21.14	-9.80	-46.09	132.00	192.00	192.00	2.2
0	(8+9)-I-4	-935	104	-600	-4.83	30.67	-46.50	132.00	192.00	192.00	2.5
0	(8+9)-VI-2	-4021	-30	860	-20.77	-8.89	66.66	132.00	192.00	192.00	2.5
0	(8+9)-II-4	-4426	34	524	-22.86	10.03	40.61	132.00	192.00	192.00	3.6
0	(8+9)-VIII-1	4873	-40	-706	25.17	-11.95	-54.71	132.00	192.00	192.00	1.9
0	(8+9)-I-2	-2798	-99	1157	-14.45	-29.21	89.65	132.00	192.00	192.00	1.6
0	(8+9)-II-2	-4986	-27	1051	-25.75	-7.93	81.46	132.00	192.00	192.00	2.1
0	(8+9)-III-2	-3032	-97	1190	-15.66	-28.56	92.24	132.00	192.00	192.00	1.6
0	(8+9)-VI-3	2722	34	-740	14.06	10.09	-57.35	132.00	192.00	192.00	2.2
0	(8+9)-VI-4	-5391	37	715	-27.85	10.99	55.41	132.00	192.00	192.00	2.7
0	(8+9)-VII-1	3086	-113	51	15.94	-33.32	3.92	132.00	192.00	192.00	3.2
3870	1	-453	2	162	-2.34	0.61	12.57	79.20	115.20	115.20	8.7
3870	2	-984	3	347	-5.08	0.94	26.92	118.80	172.80	172.80	6.2

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
3870	3	-984	3	347	-5.08	0.94	26.92	118.80	172.80	172.80	6.2
3870	4	-453	2	162	-2.34	0.61	12.57	105.60	153.60	153.60	12
3870	5	-453	2	162	-2.34	0.61	12.57	105.60	153.60	153.60	12
3870	6	-453	2	162	-2.34	0.61	12.57	105.60	153.60	153.60	12
3870	7	-453	2	162	-2.34	0.61	12.57	105.60	153.60	153.60	12

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
0	(8+9)-II-1	-17	0.00	6.40	Si	>100
0	(8+9)-VII-4	47	0.01	6.40	Si	>100
0	(8+9)-VII-1	-58	0.01	6.40	Si	>100
0	(8+9)-V-2	-50	0.01	6.40	Si	>100
0	(8+9)-VI-1	-40	0.01	6.40	Si	>100
0	(8+9)-V-4	51	0.01	6.40	Si	>100
0	(8+9)-VI-4	29	0.01	6.40	Si	>100
0	(8+9)-VII-3	43	0.01	6.40	Si	>100
0	(8+9)-V-1	-62	0.02	6.40	Si	>100
0	(8+9)-VIII-1	-27	0.01	6.40	Si	>100
0	(8+9)-IV-2	9	0.00	6.40	Si	>100
0	(8+9)-VII-2	-54	0.01	6.40	Si	>100
200	(8+9)-III-2	40	0.01	6.40	Si	>100
200	(8+9)-I-3	-66	0.02	6.40	Si	>100
200	(8+9)-II-3	-43	0.01	6.40	Si	>100
200	(8+9)-I-2	46	0.01	6.40	Si	>100
200	(8+9)-III-1	41	0.01	6.40	Si	>100
200	(8+9)-I-1	36	0.01	6.40	Si	>100
200	(8+9)-III-3	-60	0.02	6.40	Si	>100
200	(8+9)-III-4	-61	0.02	6.40	Si	>100
200	(8+9)-I-4	-55	0.01	6.40	Si	>100
200	(8+9)-IV-3	-23	0.01	6.40	Si	>100
200	(8+9)-VIII-2	-20	0.01	6.40	Si	>100
200	(8+9)-II-2	23	0.01	6.40	Si	>100
400	1	-15	0.00	3.84	Si	>100
400	2	-41	0.01	5.76	Si	>100
400	3	-41	0.01	5.76	Si	>100
400	4	-15	0.00	5.12	Si	>100
400	5	-15	0.00	5.12	Si	>100
400	6	-15	0.00	5.12	Si	>100
400	7	-15	0.00	5.12	Si	>100
400	(8+9)-VIII-4	-28	0.01	6.40	Si	>100
400	(8+9)-VI-3	-27	0.01	6.40	Si	>100
400	(8+9)-VI-2	7	0.00	6.40	Si	>100
400	(8+9)-V-3	-43	0.01	6.40	Si	>100
400	(8+9)-IV-4	-32	0.01	6.40	Si	>100
400	(8+9)-II-4	-16	0.00	6.40	Si	>100
400	(8+9)-VIII-3	-10	0.00	6.40	Si	>100
400	(8+9)-IV-1	12	0.00	6.40	Si	>100
Verifiche nella direzione secondaria						
0	1	-9	0.04	3.84	Si	94
0	2	-30	0.14	5.76	Si	40
0	3	-30	0.14	5.76	Si	40
0	4	-9	0.04	5.12	Si	>100
0	5	-9	0.04	5.12	Si	>100
0	6	-9	0.04	5.12	Si	>100
0	7	-9	0.04	5.12	Si	>100
0	(8+9)-VIII-4	-24	0.12	6.40	Si	55
0	(8+9)-VI-1	-6	0.03	6.40	Si	>100
0	(8+9)-III-4	-47	0.22	6.40	Si	29
0	(8+9)-I-2	37	0.18	6.40	Si	36
0	(8+9)-IV-1	17	0.08	6.40	Si	80
0	(8+9)-I-4	-41	0.19	6.40	Si	33
0	(8+9)-I-1	31	0.15	6.40	Si	44

X	Comb.	Ty	τ_d	fvd	RS	Cs
0	(8+9)-VIII-1	14	0.07	6.40	Si	94
0	(8+9)-VII-1	28	0.14	6.40	Si	47
0	(8+9)-VII-4	-38	0.18	6.40	Si	35
0	(8+9)-IV-4	-27	0.13	6.40	Si	50
0	(8+9)-VII-3	-32	0.15	6.40	Si	42
0	(8+9)-I-3	-47	0.22	6.40	Si	29
0	(8+9)-II-3	-27	0.13	6.40	Si	50
0	(8+9)-III-1	37	0.18	6.40	Si	36
0	(8+9)-III-3	-41	0.19	6.40	Si	33
0	(8+9)-V-4	-32	0.15	6.40	Si	42
0	(8+9)-VI-3	-24	0.12	6.40	Si	55
0	(8+9)-V-3	-38	0.18	6.40	Si	35
1935	(8+9)-II-1	-5	0.02	6.40	Si	>100
3870	(8+9)-IV-2	24	0.11	6.40	Si	56
3870	(8+9)-V-1	25	0.12	6.40	Si	54
3870	(8+9)-III-2	34	0.16	6.40	Si	40
3870	(8+9)-VI-2	28	0.13	6.40	Si	48
3870	(8+9)-II-4	14	0.07	6.40	Si	98
3870	(8+9)-VII-2	33	0.16	6.40	Si	41
3870	(8+9)-V-2	34	0.16	6.40	Si	40
3870	(8+9)-IV-3	-12	0.06	6.40	Si	>100
3870	(8+9)-II-2	28	0.14	6.40	Si	47
3870	(8+9)-VIII-2	24	0.11	6.40	Si	57
3870	(8+9)-VIII-3	-12	0.06	6.40	Si	>100
3870	(8+9)-VI-4	14	0.07	6.40	Si	96

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	1	1200	0.64	19.20	30	0.16	12.00	77	V	30
0	2	2459	1.31	28.80	22	0.32	18.00	57	V	22
0	3	2459	1.31	28.80	22	0.32	18.00	57	V	22
0	4	1200	0.64	25.60	40	0.16	16.00	>100	V	40
0	5	1200	0.64	25.60	40	0.16	16.00	>100	V	40
0	6	1200	0.64	25.60	40	0.16	16.00	>100	V	40
0	7	1200	0.64	25.60	40	0.16	16.00	>100	V	40
0	(8+9)-VII-4	2302	1.23	32.00	26	0.30	20.00	67	V	26
0	(8+9)-VII-3	5437	2.90	32.00	11	0.70	20.00	28	V	11
0	(8+9)-VII-2	-3775	-2.02	32.00	16	-0.49	20.00	41	V	16
0	(8+9)-V-4	2445	1.31	32.00	25	0.32	20.00	63	V	25
0	(8+9)-V-3	5295	2.83	32.00	11	0.68	20.00	29	V	11
0	(8+9)-V-2	-3633	-1.94	32.00	17	-0.47	20.00	43	V	17
200	(8+9)-VIII-4	-6787	-3.62	32.00	8.8	-0.88	20.00	23	V	8.8
200	(8+9)-IV-1	7413	3.96	32.00	8.1	0.96	20.00	21	V	8.1
200	(8+9)-I-4	3003	1.60	32.00	20	0.39	20.00	52	V	20
200	(8+9)-II-4	-5208	-2.78	32.00	12	-0.67	20.00	30	V	12
200	(8+9)-VI-1	7617	4.07	32.00	7.9	0.98	20.00	20	V	7.9
200	(8+9)-III-2	-6070	-3.24	32.00	9.9	-0.78	20.00	26	V	9.9
200	(8+9)-VI-2	-6977	-3.73	32.00	8.6	-0.90	20.00	22	V	8.6
200	(8+9)-III-4	2797	1.49	32.00	21	0.36	20.00	55	V	21
200	(8+9)-VI-3	8495	4.54	32.00	7.1	1.10	20.00	18	V	7.1
200	(8+9)-IV-2	-8556	-4.57	32.00	7.0	-1.11	20.00	18	V	7.0
200	(8+9)-VI-4	-6099	-3.26	32.00	9.8	-0.79	20.00	25	V	9.8
200	(8+9)-IV-4	-5896	-3.15	32.00	10	-0.76	20.00	26	V	10
200	(8+9)-II-2	-7868	-4.20	32.00	7.6	-1.02	20.00	20	V	7.6
200	(8+9)-I-3	7381	3.94	32.00	8.1	0.95	20.00	21	V	8.1
200	(8+9)-III-1	-1279	-0.68	32.00	47	-0.17	20.00	>100	V	47
200	(8+9)-I-2	-5864	-3.13	32.00	10	-0.76	20.00	26	V	10
200	(8+9)-II-3	9386	5.01	32.00	6.4	1.21	20.00	16	V	6.4
200	(8+9)-I-1	-1486	-0.79	32.00	40	-0.19	20.00	>100	V	40
200	(8+9)-II-1	6726	3.59	32.00	8.9	0.87	20.00	23	V	8.9
200	(8+9)-III-3	7587	4.05	32.00	7.9	0.98	20.00	20	V	7.9
200	(8+9)-IV-3	10073	5.38	32.00	6.0	1.30	20.00	15	V	6.0

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
200	(8+9)-VIII-3	9182	4.90	32.00	6.5	1.19	20.00	17	V	6.5
200	(8+9)-VIII-1	8304	4.43	32.00	7.2	1.07	20.00	19	V	7.2
200	(8+9)-VIII-2	-7665	-4.09	32.00	7.8	-0.99	20.00	20	V	7.8
400	(8+9)-VII-1	2782	1.49	32.00	22	0.36	20.00	56	V	22
400	(8+9)-V-1	2532	1.35	32.00	24	0.33	20.00	61	V	24
Verifiche nella direzione secondaria										
0	(8+9)-VIII-4	1103	5.70	32.00	5.6	1.38	20.00	15	V	5.6
0	(8+9)-III-2	1392	7.19	32.00	4.5	1.74	20.00	11	V	4.5
0	(8+9)-V-2	1321	6.83	32.00	4.7	1.65	20.00	12	V	4.7
0	(8+9)-IV-2	1672	8.64	32.00	3.7	2.09	20.00	9.6	V	3.7
0	(8+9)-V-1	597	3.08	32.00	10	0.75	20.00	27	V	10
0	(8+9)-VII-2	1368	7.06	32.00	4.5	1.71	20.00	12	V	4.5
0	(8+9)-IV-4	1096	5.66	32.00	5.7	1.37	20.00	15	V	5.7
0	(8+9)-VI-4	949	4.90	32.00	6.5	1.19	20.00	17	V	6.5
0	(8+9)-II-2	1518	7.84	32.00	4.1	1.90	20.00	11	V	4.1
0	(8+9)-VIII-2	1665	8.60	32.00	3.7	2.08	20.00	9.6	V	3.7
0	(8+9)-VII-1	551	2.85	32.00	11	0.69	20.00	29	V	11
0	(8+9)-VI-2	1511	7.80	32.00	4.1	1.89	20.00	11	V	4.1
0	(8+9)-I-2	1345	6.95	32.00	4.6	1.68	20.00	12	V	4.6
0	(8+9)-I-1	621	3.21	32.00	10.0	0.78	20.00	26	V	10.0
0	(8+9)-II-4	942	4.86	32.00	6.6	1.18	20.00	17	V	6.6
0	(8+9)-III-1	575	2.97	32.00	11	0.72	20.00	28	V	11
3870	1	-741	-3.83	19.20	5.0	-0.93	12.00	13	V	5.0
3870	2	-1536	-7.93	28.80	3.6	-1.92	18.00	9.4	V	3.6
3870	3	-1536	-7.93	28.80	3.6	-1.92	18.00	9.4	V	3.6
3870	4	-741	-3.83	25.60	6.7	-0.93	16.00	17	V	6.7
3870	5	-741	-3.83	25.60	6.7	-0.93	16.00	17	V	6.7
3870	6	-741	-3.83	25.60	6.7	-0.93	16.00	17	V	6.7
3870	7	-741	-3.83	25.60	6.7	-0.93	16.00	17	V	6.7
3870	(8+9)-III-3	-1809	-9.35	32.00	3.4	-2.26	20.00	8.8	V	3.4
3870	(8+9)-II-3	-1801	-9.31	32.00	3.4	-2.25	20.00	8.9	V	3.4
3870	(8+9)-I-4	-1177	-6.08	32.00	5.3	-1.47	20.00	14	V	5.3
3870	(8+9)-IV-1	-1331	-6.88	32.00	4.7	-1.66	20.00	12	V	4.7
3870	(8+9)-V-3	-1373	-7.09	32.00	4.5	-1.72	20.00	12	V	4.5
3870	(8+9)-VII-3	-1405	-7.26	32.00	4.4	-1.76	20.00	11	V	4.4
3870	(8+9)-VI-1	-1344	-6.94	32.00	4.6	-1.68	20.00	12	V	4.6
3870	(8+9)-VII-4	-741	-3.83	32.00	8.4	-0.93	20.00	22	V	8.4
3870	(8+9)-I-3	-1777	-9.18	32.00	3.5	-2.22	20.00	9.0	V	3.5
3870	(8+9)-V-4	-773	-3.99	32.00	8.0	-0.97	20.00	21	V	8.0
3870	(8+9)-II-1	-1223	-6.32	32.00	5.1	-1.53	20.00	13	V	5.1
3870	(8+9)-IV-3	-1910	-9.86	32.00	3.2	-2.39	20.00	8.4	V	3.2
3870	(8+9)-VIII-1	-1452	-7.50	32.00	4.3	-1.82	20.00	11	V	4.3
3870	(8+9)-III-4	-1145	-5.91	32.00	5.4	-1.43	20.00	14	V	5.4
3870	(8+9)-VIII-3	-1788	-9.24	32.00	3.5	-2.24	20.00	8.9	V	3.5
3870	(8+9)-VI-3	-1680	-8.68	32.00	3.7	-2.10	20.00	9.5	V	3.7

Setto 18: origine (742.0,828.0,193.5), direzione (-0.611124,0.791535,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	
0	(8+9)-VIII-4	-5188	-213	10101	-1.85	-2.85	5.57	132.00	192.00	192.00	23
0	(8+9)-IV-1	3581	174	-8878	1.27	2.33	-4.90	132.00	192.00	192.00	21
0	(8+9)-II-1	3184	-164	-7839	1.13	-2.19	-4.33	132.00	192.00	192.00	24
0	(8+9)-VIII-1	3522	226	-8761	1.25	3.02	-4.83	132.00	192.00	192.00	20
0	(8+9)-IV-4	-5248	-161	10218	-1.87	-2.16	5.64	132.00	192.00	192.00	25
227	1	-1216	8	1149	-0.43	0.11	0.63	79.20	115.20	115.20	>100
227	2	-2242	16	2020	-0.80	0.21	1.11	118.80	172.80	172.80	>100
227	3	-2242	16	2020	-0.80	0.21	1.11	118.80	172.80	172.80	>100
227	4	-1216	8	1149	-0.43	0.11	0.63	105.60	153.60	153.60	>100
227	5	-1216	8	1149	-0.43	0.11	0.63	105.60	153.60	153.60	>100
227	6	-1216	8	1149	-0.43	0.11	0.63	105.60	153.60	153.60	>100
227	7	-1216	8	1149	-0.43	0.11	0.63	105.60	153.60	153.60	>100
227	(8+9)-IV-2	-7553	-235	16953	-2.69	-3.14	9.36	132.00	192.00	192.00	15

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
227	(8+9)-V-1	-3738	-98	7385	-1.33	-1.30	4.08	132.00	192.00	192.00	36
227	(8+9)-I-2	-6273	-178	14007	-2.23	-2.38	7.73	132.00	192.00	192.00	19
227	(8+9)-V-4	2071	109	-5799	0.74	1.46	-3.20	132.00	192.00	192.00	34
227	(8+9)-II-4	-4794	163	9755	-1.71	2.18	5.38	132.00	192.00	192.00	25
227	(8+9)-VI-1	2965	-111	-8021	1.06	-1.48	-4.43	132.00	192.00	192.00	26
227	(8+9)-III-2	-6398	-259	14428	-2.28	-3.46	7.96	132.00	192.00	192.00	17
227	(8+9)-VI-2	-7297	77	15697	-2.60	1.03	8.66	132.00	192.00	192.00	20
227	(8+9)-III-4	1402	164	-4884	0.50	2.20	-2.70	132.00	192.00	192.00	34
227	(8+9)-VI-3	5631	-66	-14111	2.00	-0.88	-7.79	132.00	192.00	192.00	17
227	(8+9)-II-2	-7134	36	15549	-2.54	0.48	8.58	132.00	192.00	192.00	21
227	(8+9)-VI-4	-4631	122	9607	-1.65	1.63	5.30	132.00	192.00	192.00	28
227	(8+9)-I-1	-3194	-234	6892	-1.14	-3.13	3.80	132.00	192.00	192.00	28
227	(8+9)-VII-1	-3612	-16	6963	-1.29	-0.22	3.84	132.00	192.00	192.00	47
227	(8+9)-V-2	-6816	-41	14500	-2.43	-0.55	8.00	132.00	192.00	192.00	22
227	(8+9)-VII-2	-6942	-123	14921	-2.47	-1.64	8.23	132.00	192.00	192.00	19
227	(8+9)-III-1	-3069	-153	6470	-1.09	-2.04	3.57	132.00	192.00	192.00	34
227	(8+9)-VII-3	5275	134	-13336	1.88	1.79	-7.36	132.00	192.00	192.00	16
227	(8+9)-II-3	5468	-25	-13963	1.95	-0.33	-7.70	132.00	192.00	192.00	18
227	(8+9)-VII-4	1946	28	-5377	0.69	0.37	-2.97	132.00	192.00	192.00	44
227	(8+9)-III-3	4732	270	-12842	1.68	3.62	-7.09	132.00	192.00	192.00	15
227	(8+9)-IV-3	5886	246	-15367	2.10	3.29	-8.48	132.00	192.00	192.00	13
227	(8+9)-V-3	5150	53	-12914	1.83	0.70	-7.13	132.00	192.00	192.00	18
227	(8+9)-I-3	4606	189	-12421	1.64	2.53	-6.85	132.00	192.00	192.00	16
227	(8+9)-VIII-2	-7716	-194	17101	-2.75	-2.59	9.44	132.00	192.00	192.00	16
227	(8+9)-VIII-3	6049	205	-15515	2.15	2.74	-8.56	132.00	192.00	192.00	13
227	(8+9)-I-4	1528	245	-5306	0.54	3.28	-2.93	132.00	192.00	192.00	27
Verifiche nella direzione secondaria											
0	(8+9)-VIII-4	1438	19	376	6.56	4.98	22.74	132.00	192.00	192.00	5.2
0	(8+9)-VII-2	3368	-86	436	15.36	-22.36	26.36	132.00	192.00	192.00	2.7
0	(8+9)-III-3	-5543	45	-674	-25.28	11.83	-40.72	132.00	192.00	192.00	3.4
0	(8+9)-IV-2	3525	-18	609	16.08	-4.78	36.79	132.00	192.00	192.00	3.0
0	(8+9)-III-4	-3589	39	-339	-16.37	10.17	-20.48	132.00	192.00	192.00	6.0
0	(8+9)-VIII-2	3381	-33	584	15.42	-8.54	35.31	132.00	192.00	192.00	2.9
0	(8+9)-IV-1	-2989	3	-508	-13.63	0.78	-30.66	132.00	192.00	192.00	5.9
0	(8+9)-VII-4	-3109	87	-257	-14.18	22.70	-15.53	132.00	192.00	192.00	4.9
0	(8+9)-I-1	2551	-60	91	11.63	-15.69	5.49	132.00	192.00	192.00	5.0
0	(8+9)-IV-3	-5219	26	-765	-23.81	6.78	-46.20	132.00	192.00	192.00	3.4
0	(8+9)-I-3	-4886	16	-767	-22.28	4.30	-46.31	132.00	192.00	192.00	3.6
0	(8+9)-IV-4	1294	5	352	5.90	1.22	21.25	132.00	192.00	192.00	6.2
0	(8+9)-II-1	-799	-93	-816	-3.64	-24.32	-49.29	132.00	192.00	192.00	2.6
0	(8+9)-V-1	2071	-108	9	9.45	-28.22	0.53	132.00	192.00	192.00	4.5
0	(8+9)-II-3	-3030	-70	-1073	-13.82	-18.32	-64.83	132.00	192.00	192.00	2.3
0	(8+9)-V-2	2711	-57	529	12.37	-14.83	31.95	132.00	192.00	192.00	3.0
0	(8+9)-III-1	1894	-31	183	8.64	-8.16	11.07	132.00	192.00	192.00	6.0
0	(8+9)-V-3	-4406	65	-685	-20.10	16.83	-41.35	132.00	192.00	192.00	3.2
0	(8+9)-VIII-3	-5076	40	-740	-23.15	10.54	-44.71	132.00	192.00	192.00	3.3
0	(8+9)-V-4	-3766	116	-165	-17.18	30.23	-9.94	132.00	192.00	192.00	4.6
0	(8+9)-VII-3	-5063	93	-592	-23.09	24.37	-35.77	132.00	192.00	192.00	3.1
0	(8+9)-VI-1	-943	-108	-841	-4.30	-28.08	-50.78	132.00	192.00	192.00	2.4
0	(8+9)-I-4	-4245	68	-247	-19.36	17.70	-14.89	132.00	192.00	192.00	5.6
0	(8+9)-VI-2	1191	63	893	5.43	16.57	53.93	132.00	192.00	192.00	2.4
0	(8+9)-II-4	-896	101	660	-4.09	26.33	39.88	132.00	192.00	192.00	2.9
0	(8+9)-VIII-1	-3132	-11	-532	-14.29	-2.97	-32.15	132.00	192.00	192.00	5.3
0	(8+9)-I-2	3191	-9	611	14.55	-2.30	36.90	132.00	192.00	192.00	3.2
0	(8+9)-II-2	1335	78	917	6.09	20.33	55.42	132.00	192.00	192.00	2.3
0	(8+9)-III-2	3848	-38	518	17.55	-9.83	31.31	132.00	192.00	192.00	2.9
0	(8+9)-VI-3	-2886	-56	-1049	-13.16	-14.56	-63.34	132.00	192.00	192.00	2.4
0	(8+9)-VI-4	-752	115	685	-3.43	30.09	41.37	132.00	192.00	192.00	2.7
0	(8+9)-VII-1	1414	-79	101	6.45	-20.69	6.12	132.00	192.00	192.00	5.3
3870	1	-560	4	-149	-2.55	1.16	-8.99	79.20	115.20	115.20	11
3870	2	-1178	7	-326	-5.37	1.73	-19.69	118.80	172.80	172.80	8.0
3870	3	-1178	7	-326	-5.37	1.73	-19.69	118.80	172.80	172.80	8.0
3870	4	-560	4	-149	-2.55	1.16	-8.99	105.60	153.60	153.60	15
3870	5	-560	4	-149	-2.55	1.16	-8.99	105.60	153.60	153.60	15

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
3870	6	-560	4	-149	-2.55	1.16	-8.99	105.60	153.60	153.60	15
3870	7	-560	4	-149	-2.55	1.16	-8.99	105.60	153.60	153.60	15

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Ty kg	τ_d kg/cmq	fvd kg/cmq	RS	Cs
0	(8+9)-VI-1	-98	0.03	6.40	Si	>100
0	(8+9)-II-4	90	0.02	6.40	Si	>100
0	(8+9)-III-2	-185	0.05	6.40	Si	>100
0	(8+9)-I-2	-159	0.04	6.40	Si	>100
0	(8+9)-III-1	-156	0.04	6.40	Si	>100
0	(8+9)-I-3	157	0.04	6.40	Si	>100
0	(8+9)-III-3	184	0.05	6.40	Si	>100
0	(8+9)-I-1	-183	0.05	6.40	Si	>100
0	(8+9)-IV-3	98	0.03	6.40	Si	>100
0	(8+9)-III-4	154	0.04	6.40	Si	>100
0	(8+9)-I-4	181	0.05	6.40	Si	>100
0	(8+9)-II-1	-92	0.02	6.40	Si	>100
0	(8+9)-VI-4	96	0.02	6.40	Si	>100
0	(8+9)-IV-2	-100	0.03	6.40	Si	>100
227	(8+9)-VI-3	56	0.01	6.40	Si	>100
227	(8+9)-VIII-2	-113	0.03	6.40	Si	>100
227	(8+9)-VII-4	214	0.06	6.40	Si	>100
227	(8+9)-VIII-3	111	0.03	6.40	Si	>100
227	(8+9)-VI-2	-58	0.01	6.40	Si	>100
227	(8+9)-VII-1	-216	0.06	6.40	Si	>100
227	(8+9)-V-1	-233	0.06	6.40	Si	>100
227	(8+9)-IV-1	62	0.02	6.40	Si	>100
227	(8+9)-VII-2	-242	0.06	6.40	Si	>100
227	(8+9)-VII-3	240	0.06	6.40	Si	>100
227	(8+9)-V-2	-226	0.06	6.40	Si	>100
227	(8+9)-V-3	224	0.06	6.40	Si	>100
227	(8+9)-V-4	231	0.06	6.40	Si	>100
453	1	-4	0.00	3.84	Si	>100
453	2	-6	0.00	5.76	Si	>100
453	3	-6	0.00	5.76	Si	>100
453	4	-4	0.00	5.12	Si	>100
453	5	-4	0.00	5.12	Si	>100
453	6	-4	0.00	5.12	Si	>100
453	7	-4	0.00	5.12	Si	>100
453	(8+9)-VIII-4	-47	0.01	6.40	Si	>100
453	(8+9)-VIII-1	41	0.01	6.40	Si	>100
453	(8+9)-II-2	41	0.01	6.40	Si	>100
453	(8+9)-II-3	-48	0.01	6.40	Si	>100
453	(8+9)-IV-4	-67	0.02	6.40	Si	>100
Verifiche nella direzione secondaria						
0	(8+9)-VII-3	-217	0.91	6.40	Si	7.0
0	(8+9)-V-4	-234	0.99	6.40	Si	6.5
0	(8+9)-VII-2	220	0.92	6.40	Si	6.9
0	(8+9)-VII-4	-232	0.98	6.40	Si	6.5
0	(8+9)-V-2	218	0.92	6.40	Si	7.0
0	(8+9)-V-1	237	1.00	6.40	Si	6.4
0	(8+9)-VII-1	235	0.99	6.40	Si	6.5
0	(8+9)-VI-4	-99	0.42	6.40	Si	15
0	(8+9)-V-3	-215	0.90	6.40	Si	7.1
0	(8+9)-VI-1	102	0.43	6.40	Si	15
1935	(8+9)-IV-2	-53	0.22	6.40	Si	29
1935	(8+9)-VI-2	-56	0.23	6.40	Si	27
1935	(8+9)-II-2	-56	0.23	6.40	Si	27
1935	(8+9)-II-3	57	0.24	6.40	Si	26
1935	(8+9)-VI-3	58	0.24	6.40	Si	26
1935	(8+9)-VIII-3	55	0.23	6.40	Si	28
1935	(8+9)-VIII-2	-53	0.22	6.40	Si	29

X	Comb.	Ty	τ_d	fvd	RS	Cs
1935	(8+9)-IV-3	55	0.23	6.40	Si	28
3870	1	8	0.04	3.84	Si	>100
3870	2	10	0.04	5.76	Si	>100
3870	3	10	0.04	5.76	Si	>100
3870	4	8	0.04	5.12	Si	>100
3870	5	8	0.04	5.12	Si	>100
3870	6	8	0.04	5.12	Si	>100
3870	7	8	0.04	5.12	Si	>100
3870	(8+9)-VIII-4	-94	0.40	6.40	Si	16
3870	(8+9)-I-2	226	0.95	6.40	Si	6.7
3870	(8+9)-IV-1	142	0.60	6.40	Si	11
3870	(8+9)-III-2	218	0.92	6.40	Si	7.0
3870	(8+9)-I-4	-238	1.00	6.40	Si	6.4
3870	(8+9)-IV-4	-130	0.55	6.40	Si	12
3870	(8+9)-II-4	-102	0.43	6.40	Si	15
3870	(8+9)-III-1	258	1.09	6.40	Si	5.9
3870	(8+9)-I-3	-214	0.90	6.40	Si	7.1
3870	(8+9)-I-1	250	1.05	6.40	Si	6.1
3870	(8+9)-VIII-1	107	0.45	6.40	Si	14
3870	(8+9)-III-3	-206	0.87	6.40	Si	7.4
3870	(8+9)-III-4	-246	1.03	6.40	Si	6.2
3870	(8+9)-II-1	114	0.48	6.40	Si	13

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	(8+9)-VII-2	-5949	-3.18	32.00	10	-0.77	20.00	26	V	10
0	(8+9)-III-2	-8059	-4.30	32.00	7.4	-1.04	20.00	19	V	7.4
0	(8+9)-III-1	-4636	-2.48	32.00	13	-0.60	20.00	33	V	13
0	(8+9)-I-3	6649	3.55	32.00	9.0	0.86	20.00	23	V	9.0
0	(8+9)-III-3	6965	3.72	32.00	8.6	0.90	20.00	22	V	8.6
0	(8+9)-I-4	3859	2.06	32.00	16	0.50	20.00	40	V	16
0	(8+9)-V-4	1748	0.93	32.00	34	0.23	20.00	89	V	34
0	(8+9)-V-3	4539	2.42	32.00	13	0.59	20.00	34	V	13
0	(8+9)-I-2	-7743	-4.13	32.00	7.7	-1.00	20.00	20	V	7.7
0	(8+9)-VII-1	-2526	-1.35	32.00	24	-0.33	20.00	61	V	24
0	(8+9)-VII-4	1433	0.76	32.00	42	0.19	20.00	>100	V	42
0	(8+9)-I-1	-4952	-2.64	32.00	12	-0.64	20.00	31	V	12
0	(8+9)-V-2	-5633	-3.01	32.00	11	-0.73	20.00	27	V	11
0	(8+9)-V-1	-2842	-1.52	32.00	21	-0.37	20.00	54	V	21
0	(8+9)-III-4	3543	1.89	32.00	17	0.46	20.00	44	V	17
0	(8+9)-VII-3	4855	2.59	32.00	12	0.63	20.00	32	V	12
227	(8+9)-VI-4	-4292	-2.29	32.00	14	-0.55	20.00	36	V	14
227	(8+9)-VIII-3	6510	3.48	32.00	9.2	0.84	20.00	24	V	9.2
227	(8+9)-II-1	2681	1.43	32.00	22	0.35	20.00	58	V	22
227	(8+9)-VIII-4	-5370	-2.87	32.00	11	-0.69	20.00	29	V	11
227	(8+9)-VIII-1	4388	2.34	32.00	14	0.57	20.00	35	V	14
227	(8+9)-IV-1	3759	2.01	32.00	16	0.49	20.00	41	V	16
227	(8+9)-VI-1	3310	1.77	32.00	18	0.43	20.00	47	V	18
227	(8+9)-IV-3	7139	3.81	32.00	8.4	0.92	20.00	22	V	8.4
227	(8+9)-VI-2	-6414	-3.42	32.00	9.3	-0.83	20.00	24	V	9.3
227	(8+9)-II-4	-3663	-1.96	32.00	16	-0.47	20.00	42	V	16
227	(8+9)-IV-2	-8121	-4.34	32.00	7.4	-1.05	20.00	19	V	7.4
227	(8+9)-IV-4	-4741	-2.53	32.00	13	-0.61	20.00	33	V	13
227	(8+9)-II-2	-7043	-3.76	32.00	8.5	-0.91	20.00	22	V	8.5
227	(8+9)-VI-3	5432	2.90	32.00	11	0.70	20.00	28	V	11
227	(8+9)-II-3	6061	3.24	32.00	9.9	0.78	20.00	26	V	9.9
227	(8+9)-VIII-2	-7492	-4.00	32.00	8.0	-0.97	20.00	21	V	8.0
453	1	-956	-0.51	19.20	38	-0.12	12.00	97	V	38
453	2	-1968	-1.05	28.80	27	-0.25	18.00	71	V	27
453	3	-1968	-1.05	28.80	27	-0.25	18.00	71	V	27
453	4	-956	-0.51	25.60	50	-0.12	16.00	>100	V	50
453	5	-956	-0.51	25.60	50	-0.12	16.00	>100	V	50

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
453	6	-956	-0.51	25.60	50	-0.12	16.00	>100	V	50
453	7	-956	-0.51	25.60	50	-0.12	16.00	>100	V	50
Verifiche nella direzione secondaria										
1935	(8+9)-IV-2	2735	12.47	32.00	2.6	3.02	20.00	6.6	V	2.6
1935	(8+9)-VI-2	2539	11.58	32.00	2.8	2.80	20.00	7.1	V	2.8
1935	(8+9)-II-1	-1373	-6.26	32.00	5.1	-1.52	20.00	13	V	5.1
1935	(8+9)-VIII-3	-2551	-11.64	32.00	2.8	-2.82	20.00	7.1	V	2.8
1935	(8+9)-II-2	2518	11.49	32.00	2.8	2.78	20.00	7.2	V	2.8
1935	(8+9)-VIII-1	-1569	-7.16	32.00	4.5	-1.73	20.00	12	V	4.5
1935	(8+9)-II-3	-2314	-10.55	32.00	3.0	-2.55	20.00	7.8	V	3.0
1935	(8+9)-VII-3	-2184	-9.96	32.00	3.2	-2.41	20.00	8.3	V	3.2
1935	(8+9)-V-4	-952	-4.34	32.00	7.4	-1.05	20.00	19	V	7.4
1935	(8+9)-V-3	-2119	-9.66	32.00	3.3	-2.34	20.00	8.6	V	3.3
1935	(8+9)-I-3	-2050	-9.35	32.00	3.4	-2.26	20.00	8.8	V	3.4
1935	(8+9)-IV-3	-2531	-11.54	32.00	2.8	-2.79	20.00	7.2	V	2.8
1935	(8+9)-VIII-2	2756	12.57	32.00	2.5	3.04	20.00	6.6	V	2.5
1935	(8+9)-VI-3	-2334	-10.65	32.00	3.0	-2.58	20.00	7.8	V	3.0
1935	(8+9)-VI-1	-1352	-6.17	32.00	5.2	-1.49	20.00	13	V	5.2
1935	(8+9)-I-4	-883	-4.03	32.00	7.9	-0.97	20.00	21	V	7.9
1935	(8+9)-VII-4	-887	-4.04	32.00	7.9	-0.98	20.00	20	V	7.9
1935	(8+9)-III-3	-2115	-9.65	32.00	3.3	-2.33	20.00	8.6	V	3.3
1935	(8+9)-III-4	-818	-3.73	32.00	8.6	-0.90	20.00	22	V	8.6
1935	(8+9)-IV-1	-1589	-7.25	32.00	4.4	-1.75	20.00	11	V	4.4
3870	1	648	2.96	19.20	6.5	0.72	12.00	17	V	6.5
3870	2	1342	6.12	28.80	4.7	1.48	18.00	12	V	4.7
3870	3	1342	6.12	28.80	4.7	1.48	18.00	12	V	4.7
3870	4	648	2.96	25.60	8.7	0.72	16.00	22	V	8.7
3870	5	648	2.96	25.60	8.7	0.72	16.00	22	V	8.7
3870	6	648	2.96	25.60	8.7	0.72	16.00	22	V	8.7
3870	7	648	2.96	25.60	8.7	0.72	16.00	22	V	8.7
3870	(8+9)-VIII-4	1800	8.21	32.00	3.9	1.99	20.00	10	V	3.9
3870	(8+9)-VI-4	1619	7.39	32.00	4.3	1.79	20.00	11	V	4.3
3870	(8+9)-III-2	2413	11.00	32.00	2.9	2.66	20.00	7.5	V	2.9
3870	(8+9)-III-1	1332	6.08	32.00	5.3	1.47	20.00	14	V	5.3
3870	(8+9)-VII-1	1407	6.42	32.00	5.0	1.55	20.00	13	V	5.0
3870	(8+9)-VII-2	2488	11.35	32.00	2.8	2.75	20.00	7.3	V	2.8
3870	(8+9)-II-4	1642	7.49	32.00	4.3	1.81	20.00	11	V	4.3
3870	(8+9)-I-2	2359	10.76	32.00	3.0	2.60	20.00	7.7	V	3.0
3870	(8+9)-V-2	2433	11.10	32.00	2.9	2.69	20.00	7.4	V	2.9
3870	(8+9)-V-1	1461	6.66	32.00	4.8	1.61	20.00	12	V	4.8
3870	(8+9)-IV-4	1822	8.31	32.00	3.9	2.01	20.00	9.9	V	3.9
3870	(8+9)-I-1	1386	6.32	32.00	5.1	1.53	20.00	13	V	5.1

Setto 19: origine (714.3,863.8,45.0), direzione (-0.611124,0.791535,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	(8+9)-V-1	1451	17	-539	2.22	0.99	-5.49	132.00	192.00	192.00	20
0	(8+9)-VII-1	1350	17	-497	2.07	0.99	-5.08	132.00	192.00	192.00	21
2650	1	361	-1	-60	0.55	-0.07	-0.61	79.20	115.20	115.20	78
2650	2	718	-2	-119	1.10	-0.10	-1.21	118.80	172.80	172.80	59
2650	3	718	-2	-119	1.10	-0.10	-1.21	118.80	172.80	172.80	59
2650	4	361	-1	-60	0.55	-0.07	-0.61	105.60	153.60	153.60	>100
2650	5	361	-1	-60	0.55	-0.07	-0.61	105.60	153.60	153.60	>100
2650	6	361	-1	-60	0.55	-0.07	-0.61	105.60	153.60	153.60	>100
2650	7	361	-1	-60	0.55	-0.07	-0.61	105.60	153.60	153.60	>100
5300	(8+9)-V-4	2805	-17	-707	4.29	-0.95	-7.21	132.00	192.00	192.00	13
5300	(8+9)-I-1	-2580	15	1035	-3.95	0.88	10.56	132.00	192.00	192.00	17
5300	(8+9)-I-4	2611	-17	-1021	4.00	-0.95	-10.41	132.00	192.00	192.00	11
5300	(8+9)-VII-2	-5833	11	1824	-8.93	0.64	18.61	132.00	192.00	192.00	9.8
5300	(8+9)-II-2	-6001	-3	2201	-9.18	-0.20	22.46	132.00	192.00	192.00	8.3
5300	(8+9)-VII-3	5864	-12	-1810	8.97	-0.70	-18.46	132.00	192.00	192.00	6.0
5300	(8+9)-II-4	-3579	-12	1273	-5.48	-0.68	12.99	132.00	192.00	192.00	14

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
5300	(8+9)-VII-4	2630	-17	-641	4.02	-0.96	-6.54	132.00	192.00	192.00	14
5300	(8+9)-III-2	-5639	11	2138	-8.63	0.63	21.82	132.00	192.00	192.00	8.4
5300	(8+9)-VIII-1	4136	11	-1570	6.33	0.64	-16.02	132.00	192.00	192.00	7.4
5300	(8+9)-III-4	2435	-17	-955	3.73	-0.96	-9.75	132.00	192.00	192.00	12
5300	(8+9)-VIII-2	-6645	-4	2324	-10.17	-0.23	23.71	132.00	192.00	192.00	7.8
5300	(8+9)-IV-2	-6586	-4	2418	-10.08	-0.23	24.68	132.00	192.00	192.00	7.5
5300	(8+9)-VIII-3	6675	3	-2309	10.22	0.16	-23.56	132.00	192.00	192.00	5.0
5300	(8+9)-IV-4	-4164	-12	1490	-6.37	-0.70	15.21	132.00	192.00	192.00	12
5300	(8+9)-VIII-4	-4106	-12	1585	-6.28	-0.71	16.17	132.00	192.00	192.00	11
5300	(8+9)-V-2	-5658	11	1759	-8.66	0.64	17.95	132.00	192.00	192.00	10
5300	(8+9)-III-3	5670	-12	-2124	8.68	-0.70	-21.67	132.00	192.00	192.00	5.5
5300	(8+9)-I-2	-5463	11	2073	-8.36	0.64	21.15	132.00	192.00	192.00	8.7
5300	(8+9)-IV-1	4195	11	-1475	6.42	0.64	-15.05	132.00	192.00	192.00	7.7
5300	(8+9)-VI-2	-6059	-3	2107	-9.27	-0.20	21.50	132.00	192.00	192.00	8.7
5300	(8+9)-IV-3	6617	3	-2404	10.13	0.16	-24.52	132.00	192.00	192.00	4.9
5300	(8+9)-VI-4	-3521	-12	1367	-5.39	-0.68	13.95	132.00	192.00	192.00	13
5300	(8+9)-I-3	5494	-12	-2058	8.41	-0.71	-21.00	132.00	192.00	192.00	5.7
5300	(8+9)-II-3	6032	2	-2186	9.23	0.13	-22.31	132.00	192.00	192.00	5.4
5300	(8+9)-VI-1	3551	11	-1352	5.44	0.61	-13.80	132.00	192.00	192.00	8.6
5300	(8+9)-VI-3	6090	2	-2092	9.32	0.13	-21.35	132.00	192.00	192.00	5.5
5300	(8+9)-II-1	3610	11	-1258	5.52	0.61	-12.84	132.00	192.00	192.00	8.9
5300	(8+9)-III-1	-2405	16	970	-3.68	0.89	9.90	132.00	192.00	192.00	18
5300	(8+9)-V-3	5689	-12	-1744	8.71	-0.71	-17.80	132.00	192.00	192.00	6.2
Verifiche nella direzione secondaria											
0	2	-3755	29	1320	-1.46	0.64	0.58	118.80	172.80	172.80	>100
0	3	-3755	29	1320	-1.46	0.64	0.58	118.80	172.80	172.80	>100
0	(8+9)-III-1	-753	-45	-7304	-0.29	-1.01	-3.22	132.00	192.00	192.00	45
0	(8+9)-V-4	-4603	212	444	-1.79	4.72	0.20	132.00	192.00	192.00	39
0	(8+9)-VII-4	-4699	213	-175	-1.83	4.74	-0.08	132.00	192.00	192.00	40
0	(8+9)-V-3	-4146	215	8664	-1.62	4.80	3.82	132.00	192.00	192.00	22
0	(8+9)-VII-2	1328	-203	-8106	0.52	-4.54	-3.58	132.00	192.00	192.00	22
0	(8+9)-VI-2	-1219	-63	-14302	-0.48	-1.40	-6.31	132.00	192.00	192.00	25
0	(8+9)-VII-3	-4050	214	9282	-1.58	4.78	4.10	132.00	192.00	192.00	22
0	(8+9)-VI-3	-1503	73	15478	-0.59	1.63	6.83	132.00	192.00	192.00	23
0	(8+9)-I-4	-1873	55	9098	-0.73	1.23	4.02	132.00	192.00	192.00	37
0	(8+9)-V-2	1424	-204	-7488	0.56	-4.56	-3.30	132.00	192.00	192.00	22
0	(8+9)-III-4	-1969	56	8480	-0.77	1.25	3.74	132.00	192.00	192.00	38
450	1	-2629	7	1049	-1.02	0.15	0.46	79.20	115.20	115.20	>100
450	4	-2629	7	1049	-1.02	0.15	0.46	105.60	153.60	153.60	>100
450	5	-2629	7	1049	-1.02	0.15	0.46	105.60	153.60	153.60	>100
450	6	-2629	7	1049	-1.02	0.15	0.46	105.60	153.60	153.60	>100
450	7	-2629	7	1049	-1.02	0.15	0.46	105.60	153.60	153.60	>100
450	(8+9)-VIII-4	-5403	15	-23040	-2.11	0.33	-10.17	132.00	192.00	192.00	18
450	(8+9)-II-4	-5332	17	-10596	-2.08	0.38	-4.68	132.00	192.00	192.00	38
450	(8+9)-VII-1	5893	-36	8561	2.30	-0.79	3.78	132.00	192.00	192.00	24
450	(8+9)-IV-1	436	-8	20474	0.17	-0.17	9.04	132.00	192.00	192.00	20
450	(8+9)-IV-2	-2385	-11	-26587	-0.93	-0.24	-11.73	132.00	192.00	192.00	16
450	(8+9)-VI-1	3064	-7	16058	1.19	-0.16	7.09	132.00	192.00	192.00	21
450	(8+9)-II-1	1714	-9	12044	0.67	-0.19	5.32	132.00	192.00	192.00	30
450	(8+9)-VIII-1	1785	-6	24488	0.70	-0.14	10.81	132.00	192.00	192.00	16
450	(8+9)-IV-3	-1233	19	28035	-0.48	0.42	12.37	132.00	192.00	192.00	15
450	(8+9)-V-1	6276	-36	6032	2.45	-0.80	2.66	132.00	192.00	192.00	27
450	(8+9)-I-1	1779	-40	-7348	0.69	-0.90	-3.24	132.00	192.00	192.00	37
450	(8+9)-IV-4	-4054	16	-19026	-1.58	0.36	-8.40	132.00	192.00	192.00	22
450	(8+9)-VI-4	-6681	15	-14610	-2.60	0.35	-6.45	132.00	192.00	192.00	28
900	(8+9)-I-2	-184	-17	-18521	-0.07	-0.37	-8.17	132.00	192.00	192.00	22
900	(8+9)-III-3	-3662	24	22257	-1.43	0.55	9.82	132.00	192.00	192.00	19
900	(8+9)-III-2	132	-18	-20740	0.05	-0.41	-9.15	132.00	192.00	192.00	20
900	(8+9)-II-3	-432	4	20964	-0.17	0.10	9.25	132.00	192.00	192.00	21
900	(8+9)-I-3	-3346	23	20038	-1.30	0.51	8.84	132.00	192.00	192.00	21
900	(8+9)-VIII-2	-1230	-9	-23950	-0.48	-0.21	-10.57	132.00	192.00	192.00	18
900	(8+9)-VIII-3	-2300	15	25467	-0.90	0.34	11.24	132.00	192.00	192.00	17
900	(8+9)-II-2	-3098	2	-19447	-1.21	0.04	-8.58	132.00	192.00	192.00	22

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Ty kg	τ_d kg/cmq	fvd kg/cmq	RS	Cs
0	(8+9)-VIII-4	-11	0.01	6.40	Si	>100
0	(8+9)-IV-1	-13	0.01	6.40	Si	>100
0	(8+9)-VI-3	-28	0.03	6.40	Si	>100
0	(8+9)-III-2	-12	0.01	6.40	Si	>100
0	(8+9)-IV-2	2	0.00	6.40	Si	>100
0	(8+9)-III-3	10	0.01	6.40	Si	>100
0	(8+9)-VIII-2	23	0.03	6.40	Si	>100
0	(8+9)-III-4	14	0.02	6.40	Si	>100
0	(8+9)-VII-4	-56	0.06	6.40	Si	>100
0	(8+9)-VII-1	53	0.06	6.40	Si	>100
0	(8+9)-I-2	-11	0.01	6.40	Si	>100
0	(8+9)-I-4	15	0.02	6.40	Si	>100
0	(8+9)-IV-3	-5	0.01	6.40	Si	>100
0	(8+9)-VII-3	-60	0.07	6.40	Si	95
0	(8+9)-IV-4	10	0.01	6.40	Si	>100
0	(8+9)-II-4	13	0.01	6.40	Si	>100
0	(8+9)-V-1	52	0.06	6.40	Si	>100
0	(8+9)-VIII-3	-26	0.03	6.40	Si	>100
0	(8+9)-V-2	59	0.07	6.40	Si	98
0	(8+9)-I-1	-17	0.02	6.40	Si	>100
0	(8+9)-V-3	-61	0.07	6.40	Si	94
0	(8+9)-II-1	-15	0.02	6.40	Si	>100
0	(8+9)-III-1	-17	0.02	6.40	Si	>100
0	(8+9)-VIII-1	8	0.01	6.40	Si	>100
0	(8+9)-I-3	9	0.01	6.40	Si	>100
0	(8+9)-VII-2	58	0.06	6.40	Si	100
0	(8+9)-V-4	-55	0.06	6.40	Si	>100
0	(8+9)-VI-4	-8	0.01	6.40	Si	>100
0	(8+9)-VI-2	26	0.03	6.40	Si	>100
5300	1	-2	0.00	3.84	Si	>100
5300	2	-8	0.01	5.76	Si	>100
5300	3	-8	0.01	5.76	Si	>100
5300	4	-2	0.00	5.12	Si	>100
5300	5	-2	0.00	5.12	Si	>100
5300	6	-2	0.00	5.12	Si	>100
5300	7	-2	0.00	5.12	Si	>100
5300	(8+9)-II-2	7	0.01	6.40	Si	>100
5300	(8+9)-II-3	-9	0.01	6.40	Si	>100
5300	(8+9)-VI-1	-9	0.01	6.40	Si	>100
Verifiche nella direzione secondaria						
0	(8+9)-VIII-4	-55	0.02	6.40	Si	>100
0	(8+9)-IV-1	44	0.02	6.40	Si	>100
0	(8+9)-V-3	-78	0.03	6.40	Si	>100
0	(8+9)-IV-2	-14	0.01	6.40	Si	>100
0	(8+9)-II-1	33	0.01	6.40	Si	>100
0	(8+9)-VII-4	-93	0.03	6.40	Si	>100
0	(8+9)-V-2	76	0.03	6.40	Si	>100
0	(8+9)-VII-2	72	0.03	6.40	Si	>100
0	(8+9)-V-1	87	0.03	6.40	Si	>100
0	(8+9)-VI-4	-44	0.02	6.40	Si	>100
0	(8+9)-II-4	-36	0.01	6.40	Si	>100
0	(8+9)-VII-3	-75	0.03	6.40	Si	>100
0	(8+9)-VII-1	90	0.03	6.40	Si	>100
0	(8+9)-VI-1	42	0.01	6.40	Si	>100
0	(8+9)-VIII-1	53	0.02	6.40	Si	>100
0	(8+9)-IV-4	-47	0.02	6.40	Si	>100
0	(8+9)-IV-3	11	0.00	6.40	Si	>100
0	(8+9)-V-4	-89	0.03	6.40	Si	>100
450	1	-9	0.00	3.84	Si	>100
450	2	-36	0.01	5.76	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
450	3	-36	0.01	5.76	Si	>100
450	4	-9	0.00	5.12	Si	>100
450	5	-9	0.00	5.12	Si	>100
450	6	-9	0.00	5.12	Si	>100
450	7	-9	0.00	5.12	Si	>100
450	(8+9)-III-4	-75	0.03	6.40	Si	>100
450	(8+9)-VIII-2	-17	0.01	6.40	Si	>100
450	(8+9)-VIII-3	6	0.00	6.40	Si	>100
450	(8+9)-I-3	-66	0.02	6.40	Si	>100
450	(8+9)-VI-2	-7	0.00	6.40	Si	>100
450	(8+9)-I-1	62	0.02	6.40	Si	>100
450	(8+9)-I-2	55	0.02	6.40	Si	>100
450	(8+9)-I-4	-72	0.03	6.40	Si	>100
450	(8+9)-III-1	65	0.02	6.40	Si	>100
450	(8+9)-III-2	52	0.02	6.40	Si	>100
450	(8+9)-III-3	-63	0.02	6.40	Si	>100
900	(8+9)-VI-3	-10	0.00	6.40	Si	>100
900	(8+9)-II-2	8	0.00	6.40	Si	>100
900	(8+9)-II-3	-17	0.01	6.40	Si	>100

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Tx kg	τ_{vd} kg/cmq	fvd kg/cmq	Csv	τ_M kg/cmq	fTd kg/cmq	Csm	Mecc.	Cs
0	1	381	0.87	19.20	22	0.21	12.00	57	V	22
0	2	753	1.73	28.80	17	0.42	18.00	43	V	17
0	3	753	1.73	28.80	17	0.42	18.00	43	V	17
0	4	381	0.87	25.60	29	0.21	16.00	76	V	29
0	5	381	0.87	25.60	29	0.21	16.00	76	V	29
0	6	381	0.87	25.60	29	0.21	16.00	76	V	29
0	7	381	0.87	25.60	29	0.21	16.00	76	V	29
0	(8+9)-IV-1	1884	4.32	32.00	7.4	1.05	20.00	19	V	7.4
0	(8+9)-V-2	-1937	-4.45	32.00	7.2	-1.08	20.00	19	V	7.2
0	(8+9)-VII-2	-2019	-4.64	32.00	6.9	-1.12	20.00	18	V	6.9
0	(8+9)-V-1	-826	-1.90	32.00	17	-0.46	20.00	44	V	17
0	(8+9)-VII-1	-744	-1.71	32.00	19	-0.41	20.00	48	V	19
0	(8+9)-VII-3	2541	5.83	32.00	5.5	1.41	20.00	14	V	5.5
0	(8+9)-VIII-3	2880	6.61	32.00	4.8	1.60	20.00	13	V	4.8
0	(8+9)-II-1	1609	3.69	32.00	8.7	0.89	20.00	22	V	8.7
0	(8+9)-VI-3	2605	5.98	32.00	5.4	1.45	20.00	14	V	5.4
0	(8+9)-V-4	1348	3.10	32.00	10	0.75	20.00	27	V	10
0	(8+9)-V-3	2459	5.64	32.00	5.7	1.37	20.00	15	V	5.7
0	(8+9)-VII-4	1266	2.91	32.00	11	0.70	20.00	28	V	11
5300	(8+9)-VIII-4	-2404	-5.52	32.00	5.8	-1.34	20.00	15	V	5.8
5300	(8+9)-I-2	-3499	-8.03	32.00	4.0	-1.94	20.00	10	V	4.0
5300	(8+9)-III-1	-2111	-4.85	32.00	6.6	-1.17	20.00	17	V	6.6
5300	(8+9)-IV-2	-3429	-7.87	32.00	4.1	-1.91	20.00	10	V	4.1
5300	(8+9)-VI-4	-2079	-4.77	32.00	6.7	-1.15	20.00	17	V	6.7
5300	(8+9)-IV-4	-1801	-4.14	32.00	7.7	-1.00	20.00	20	V	7.7
5300	(8+9)-II-4	-1476	-3.39	32.00	9.4	-0.82	20.00	24	V	9.4
5300	(8+9)-III-4	1831	4.20	32.00	7.6	1.02	20.00	20	V	7.6
5300	(8+9)-II-3	2824	6.48	32.00	4.9	1.57	20.00	13	V	4.9
5300	(8+9)-III-2	-3596	-8.26	32.00	3.9	-2.00	20.00	10	V	3.9
5300	(8+9)-II-2	-3104	-7.13	32.00	4.5	-1.72	20.00	12	V	4.5
5300	(8+9)-VI-2	-2501	-5.74	32.00	5.6	-1.39	20.00	14	V	5.6
5300	(8+9)-I-4	1928	4.43	32.00	7.2	1.07	20.00	19	V	7.2
5300	(8+9)-VI-1	1798	4.13	32.00	7.8	1.00	20.00	20	V	7.8
5300	(8+9)-IV-3	3149	7.23	32.00	4.4	1.75	20.00	11	V	4.4
5300	(8+9)-III-3	3316	7.61	32.00	4.2	1.84	20.00	11	V	4.2
5300	(8+9)-VIII-1	2124	4.88	32.00	6.6	1.18	20.00	17	V	6.6
5300	(8+9)-VIII-2	-2827	-6.49	32.00	4.9	-1.57	20.00	13	V	4.9
5300	(8+9)-I-3	3218	7.39	32.00	4.3	1.79	20.00	11	V	4.3
5300	(8+9)-I-1	-2209	-5.07	32.00	6.3	-1.23	20.00	16	V	6.3

Verifiche nella direzione secondaria

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
0	(8+9)-VIII-4	7507	2.93	32.00	11	0.71	20.00	28	V	11
0	(8+9)-VII-2	9844	3.84	32.00	8.3	0.93	20.00	22	V	8.3
0	(8+9)-III-3	-9930	-3.87	32.00	8.3	-0.94	20.00	21	V	8.3
0	(8+9)-IV-2	11705	4.56	32.00	7.0	1.10	20.00	18	V	7.0
0	(8+9)-III-4	-4150	-1.62	32.00	20	-0.39	20.00	51	V	20
0	(8+9)-VIII-2	11697	4.56	32.00	7.0	1.10	20.00	18	V	7.0
0	(8+9)-IV-1	-7559	-2.95	32.00	11	-0.71	20.00	28	V	11
0	(8+9)-VII-4	-4125	-1.61	32.00	20	-0.39	20.00	51	V	20
0	(8+9)-I-1	4407	1.72	32.00	19	0.42	20.00	48	V	19
0	(8+9)-IV-3	-11765	-4.59	32.00	7.0	-1.11	20.00	18	V	7.0
0	(8+9)-I-3	-9613	-3.75	32.00	8.5	-0.91	20.00	22	V	8.5
0	(8+9)-IV-4	7499	2.92	32.00	11	0.71	20.00	28	V	11
0	(8+9)-II-1	-6505	-2.54	32.00	13	-0.61	20.00	33	V	13
0	(8+9)-V-1	4381	1.71	32.00	19	0.41	20.00	48	V	19
0	(8+9)-II-3	-10711	-4.18	32.00	7.7	-1.01	20.00	20	V	7.7
0	(8+9)-V-2	9528	3.71	32.00	8.6	0.90	20.00	22	V	8.6
0	(8+9)-III-1	4091	1.59	32.00	20	0.39	20.00	52	V	20
0	(8+9)-V-3	-9588	-3.74	32.00	8.6	-0.90	20.00	22	V	8.6
0	(8+9)-VIII-3	-11757	-4.58	32.00	7.0	-1.11	20.00	18	V	7.0
0	(8+9)-V-4	-4441	-1.73	32.00	18	-0.42	20.00	48	V	18
0	(8+9)-VII-3	-9904	-3.86	32.00	8.3	-0.93	20.00	21	V	8.3
0	(8+9)-VI-1	-6513	-2.54	32.00	13	-0.61	20.00	33	V	13
0	(8+9)-I-4	-4467	-1.74	32.00	18	-0.42	20.00	47	V	18
0	(8+9)-VI-2	10643	4.15	32.00	7.7	1.00	20.00	20	V	7.7
0	(8+9)-II-4	6445	2.51	32.00	13	0.61	20.00	33	V	13
0	(8+9)-VIII-1	-7566	-2.95	32.00	11	-0.71	20.00	28	V	11
0	(8+9)-I-2	9554	3.72	32.00	8.6	0.90	20.00	22	V	8.6
0	(8+9)-II-2	10651	4.15	32.00	7.7	1.00	20.00	20	V	7.7
0	(8+9)-III-2	9870	3.85	32.00	8.3	0.93	20.00	21	V	8.3
0	(8+9)-VI-3	-10703	-4.17	32.00	7.7	-1.01	20.00	20	V	7.7
0	(8+9)-VI-4	6453	2.52	32.00	13	0.61	20.00	33	V	13
0	(8+9)-VII-1	4065	1.58	32.00	20	0.38	20.00	52	V	20
450	1	-70	-0.03	19.20	>100	-0.01	12.00	>100	V	>100
450	2	-139	-0.05	28.80	>100	-0.01	18.00	>100	V	>100
450	3	-139	-0.05	28.80	>100	-0.01	18.00	>100	V	>100
450	4	-70	-0.03	25.60	>100	-0.01	16.00	>100	V	>100
450	5	-70	-0.03	25.60	>100	-0.01	16.00	>100	V	>100
450	6	-70	-0.03	25.60	>100	-0.01	16.00	>100	V	>100
450	7	-70	-0.03	25.60	>100	-0.01	16.00	>100	V	>100

Setto 20: origine (714.3,863.8,328.5), direzione (-0.611124,0.791535,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_N	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	(8+9)-III-3	7850	162	1856	9.24	7.14	11.21	132.00	192.00	192.00	6.0
0	(8+9)-I-3	7613	104	1792	8.96	4.60	10.82	132.00	192.00	192.00	6.7
0	(8+9)-IV-1	5803	50	1339	6.83	2.20	8.09	132.00	192.00	192.00	9.5
0	(8+9)-I-4	3227	168	683	3.80	7.43	4.12	132.00	192.00	192.00	11
0	(8+9)-VIII-1	5725	82	1337	6.74	3.63	8.07	132.00	192.00	192.00	8.9
0	(8+9)-II-1	5012	-142	1124	5.90	-6.30	6.79	132.00	192.00	192.00	8.9
0	(8+9)-VI-3	8652	-96	2032	10.19	-4.23	12.27	132.00	192.00	192.00	6.1
0	(8+9)-IV-3	9365	129	2244	11.02	5.70	13.55	132.00	192.00	192.00	5.4
0	(8+9)-V-4	3486	60	690	4.10	2.65	4.16	132.00	192.00	192.00	15
0	(8+9)-II-3	8574	-63	2030	10.09	-2.79	12.25	132.00	192.00	192.00	6.5
0	(8+9)-VII-3	8109	53	1863	9.55	2.37	11.25	132.00	192.00	192.00	7.0
0	(8+9)-VI-1	4935	-110	1122	5.81	-4.87	6.78	132.00	192.00	192.00	9.6
0	(8+9)-I-1	-4259	-160	-1225	-5.01	-7.09	-7.40	132.00	192.00	192.00	13
0	(8+9)-VIII-3	9442	96	2247	11.12	4.27	13.56	132.00	192.00	192.00	5.6
0	(8+9)-V-3	7872	-4	1799	9.27	-0.18	10.86	132.00	192.00	192.00	7.8
0	(8+9)-III-1	-4022	-103	-1161	-4.74	-4.54	-7.01	132.00	192.00	192.00	16
0	(8+9)-III-4	2990	110	618	3.52	4.88	3.73	132.00	192.00	192.00	14
2650	1	1712	-3	401	2.02	-0.15	2.42	79.20	115.20	115.20	21
2650	2	3648	-7	853	4.30	-0.32	5.15	118.80	172.80	172.80	15

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
2650	3	3648	-7	853	4.30	-0.32	5.15	118.80	172.80	172.80	15
2650	4	1712	-3	401	2.02	-0.15	2.42	105.60	153.60	153.60	28
2650	5	1712	-3	401	2.02	-0.15	2.42	105.60	153.60	153.60	28
2650	6	1712	-3	401	2.02	-0.15	2.42	105.60	153.60	153.60	28
2650	7	1712	-3	401	2.02	-0.15	2.42	105.60	153.60	153.60	28
5300	(8+9)-VIII-4	5006	-4	1756	5.89	-0.19	10.60	132.00	192.00	192.00	9.9
5300	(8+9)-VI-2	7251	-14	2648	8.54	-0.62	15.99	132.00	192.00	192.00	6.6
5300	(8+9)-III-2	6612	20	2382	7.78	0.88	14.38	132.00	192.00	192.00	7.2
5300	(8+9)-VII-2	6793	3	2450	8.00	0.14	14.79	132.00	192.00	192.00	7.2
5300	(8+9)-I-2	6370	15	2294	7.50	0.68	13.85	132.00	192.00	192.00	7.5
5300	(8+9)-II-2	7197	-9	2627	8.47	-0.40	15.86	132.00	192.00	192.00	6.7
5300	(8+9)-V-1	2903	5	930	3.42	0.22	5.61	132.00	192.00	192.00	18
5300	(8+9)-VII-4	-3371	-13	-1504	-3.97	-0.57	-9.08	132.00	192.00	192.00	20
5300	(8+9)-V-2	6551	-1	2361	7.71	-0.06	14.26	132.00	192.00	192.00	7.5
5300	(8+9)-IV-4	5061	-9	1777	5.96	-0.41	10.73	132.00	192.00	192.00	9.7
5300	(8+9)-VII-1	2661	1	841	3.13	0.02	5.08	132.00	192.00	192.00	20
5300	(8+9)-IV-2	8001	6	2922	9.42	0.25	17.64	132.00	192.00	192.00	6.1
5300	(8+9)-VIII-2	8055	1	2943	9.48	0.03	17.77	132.00	192.00	192.00	6.1
5300	(8+9)-II-4	4256	-24	1482	5.01	-1.06	8.95	132.00	192.00	192.00	11
5300	(8+9)-VI-4	4202	-19	1462	4.95	-0.83	8.82	132.00	192.00	192.00	11
Verifiche nella direzione secondaria											
0	1	-3194	5	768	-1.25	0.11	0.34	79.20	115.20	115.20	>100
0	2	-6606	9	1315	-2.58	0.21	0.58	118.80	172.80	172.80	>100
0	3	-6606	9	1315	-2.58	0.21	0.58	118.80	172.80	172.80	>100
0	4	-3194	5	768	-1.25	0.11	0.34	105.60	153.60	153.60	>100
0	5	-3194	5	768	-1.25	0.11	0.34	105.60	153.60	153.60	>100
0	6	-3194	5	768	-1.25	0.11	0.34	105.60	153.60	153.60	>100
0	7	-3194	5	768	-1.25	0.11	0.34	105.60	153.60	153.60	>100
0	(8+9)-VIII-4	-4099	-5	6782	-1.60	-0.10	2.99	132.00	192.00	192.00	62
0	(8+9)-IV-2	-3296	-8	9663	-1.28	-0.19	4.26	132.00	192.00	192.00	43
0	(8+9)-V-1	-472	12	3284	-0.18	0.26	1.45	132.00	192.00	192.00	>100
0	(8+9)-I-2	-1251	-17	7387	-0.49	-0.38	3.26	132.00	192.00	192.00	53
0	(8+9)-V-2	-1263	6	7780	-0.49	0.14	3.43	132.00	192.00	192.00	54
0	(8+9)-I-4	-3940	19	-1823	-1.54	0.42	-0.80	132.00	192.00	192.00	>100
0	(8+9)-V-3	-3138	1	-6713	-1.22	0.02	-2.96	132.00	192.00	192.00	64
0	(8+9)-II-2	-3115	-11	9408	-1.21	-0.24	4.15	132.00	192.00	192.00	44
0	(8+9)-V-4	-3928	-4	-2217	-1.53	-0.10	-0.98	132.00	192.00	192.00	>100
0	(8+9)-II-4	-3922	-0	6646	-1.53	-0.00	2.93	132.00	192.00	192.00	65
0	(8+9)-VI-1	-482	14	-5460	-0.19	0.32	-2.41	132.00	192.00	192.00	70
0	(8+9)-III-2	-1305	-16	7463	-0.51	-0.36	3.29	132.00	192.00	192.00	52
0	(8+9)-VI-2	-3118	-4	9527	-1.22	-0.09	4.20	132.00	192.00	192.00	45
0	(8+9)-III-4	-3994	19	-1747	-1.56	0.43	-0.77	132.00	192.00	192.00	>100
0	(8+9)-VI-3	-1282	11	-8459	-0.50	0.25	-3.73	132.00	192.00	192.00	48
0	(8+9)-I-1	-460	-12	2891	-0.18	-0.26	1.28	132.00	192.00	192.00	>100
0	(8+9)-VI-4	-3918	-7	6527	-1.53	-0.16	2.88	132.00	192.00	192.00	63
0	(8+9)-IV-4	-4102	2	6900	-1.60	0.05	3.05	132.00	192.00	192.00	62
0	(8+9)-VII-1	-418	11	3208	-0.16	0.24	1.42	132.00	192.00	192.00	>100
0	(8+9)-II-1	-479	7	-5578	-0.19	0.16	-2.46	132.00	192.00	192.00	73
0	(8+9)-VII-2	-1317	7	7857	-0.51	0.15	3.47	132.00	192.00	192.00	53
0	(8+9)-III-1	-406	-12	2814	-0.16	-0.27	1.24	132.00	192.00	192.00	>100
0	(8+9)-VII-3	-3083	0	-6789	-1.20	0.00	-3.00	132.00	192.00	192.00	64
0	(8+9)-IV-1	-298	5	-5832	-0.12	0.11	-2.57	132.00	192.00	192.00	72
0	(8+9)-I-3	-3149	24	-6319	-1.23	0.54	-2.79	132.00	192.00	192.00	58
0	(8+9)-III-3	-3095	23	-6395	-1.21	0.52	-2.82	132.00	192.00	192.00	57
0	(8+9)-IV-3	-1105	15	-8595	-0.43	0.35	-3.79	132.00	192.00	192.00	46
0	(8+9)-II-3	-1286	18	-8341	-0.50	0.40	-3.68	132.00	192.00	192.00	47
0	(8+9)-VIII-1	-302	12	-5714	-0.12	0.26	-2.52	132.00	192.00	192.00	69
0	(8+9)-VIII-2	-3299	-1	9781	-1.29	-0.03	4.32	132.00	192.00	192.00	44
0	(8+9)-VIII-3	-1101	9	-8713	-0.43	0.19	-3.85	132.00	192.00	192.00	48
585	(8+9)-VII-4	-2813	-12	-1795	-1.10	-0.26	-0.79	132.00	192.00	192.00	>100

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
0	(8+9)-VI-3	12	0.01	6.40	Si	>100
0	(8+9)-III-1	69	0.06	6.40	Si	>100
0	(8+9)-IV-3	18	0.02	6.40	Si	>100
0	(8+9)-III-2	46	0.04	6.40	Si	>100
0	(8+9)-VIII-3	38	0.03	6.40	Si	>100
0	(8+9)-III-3	-50	0.04	6.40	Si	>100
0	(8+9)-VIII-1	35	0.03	6.40	Si	>100
0	(8+9)-III-4	-73	0.06	6.40	Si	>100
0	(8+9)-VII-3	15	0.01	6.40	Si	>100
0	(8+9)-IV-1	54	0.05	6.40	Si	>100
0	(8+9)-I-2	54	0.05	6.40	Si	>100
0	(8+9)-IV-2	-22	0.02	6.40	Si	>100
0	(8+9)-I-4	-65	0.06	6.40	Si	>100
0	(8+9)-II-2	3	0.00	6.40	Si	>100
0	(8+9)-IV-4	-58	0.05	6.40	Si	>100
0	(8+9)-II-4	-32	0.03	6.40	Si	>100
0	(8+9)-VI-2	-16	0.01	6.40	Si	>100
0	(8+9)-VIII-4	-38	0.03	6.40	Si	>100
0	(8+9)-VIII-2	-41	0.04	6.40	Si	>100
0	(8+9)-I-1	61	0.05	6.40	Si	>100
0	(8+9)-V-2	-11	0.01	6.40	Si	>100
0	(8+9)-II-1	29	0.02	6.40	Si	>100
0	(8+9)-VII-4	-8	0.01	6.40	Si	>100
0	(8+9)-I-3	-57	0.05	6.40	Si	>100
0	(8+9)-VII-2	-18	0.02	6.40	Si	>100
0	(8+9)-VII-1	5	0.00	6.40	Si	>100
0	(8+9)-VI-4	-13	0.01	6.40	Si	>100
0	(8+9)-VI-1	9	0.01	6.40	Si	>100
2650	(8+9)-V-1	4	0.00	6.40	Si	>100
5300	1	-6	0.01	3.84	Si	>100
5300	2	-13	0.01	5.76	Si	>100
5300	3	-13	0.01	5.76	Si	>100
5300	4	-6	0.01	5.12	Si	>100
5300	5	-6	0.01	5.12	Si	>100
5300	6	-6	0.01	5.12	Si	>100
5300	7	-6	0.01	5.12	Si	>100
5300	(8+9)-V-4	-7	0.01	6.40	Si	>100
5300	(8+9)-II-3	-11	0.01	6.40	Si	>100
5300	(8+9)-V-3	-8	0.01	6.40	Si	>100
Verifiche nella direzione secondaria						
0	(8+9)-II-2	-38	0.01	6.40	Si	>100
0	(8+9)-II-3	41	0.01	6.40	Si	>100
585	1	11	0.00	3.84	Si	>100
585	4	11	0.00	5.12	Si	>100
585	5	11	0.00	5.12	Si	>100
585	6	11	0.00	5.12	Si	>100
585	7	11	0.00	5.12	Si	>100
585	(8+9)-V-1	32	0.01	6.40	Si	>100
585	(8+9)-VII-2	37	0.01	6.40	Si	>100
585	(8+9)-VII-4	-19	0.01	6.40	Si	>100
585	(8+9)-V-4	-16	0.01	6.40	Si	>100
585	(8+9)-V-2	40	0.01	6.40	Si	>100
585	(8+9)-VII-1	35	0.01	6.40	Si	>100
1170	2	14	0.00	5.76	Si	>100
1170	3	14	0.00	5.76	Si	>100
1170	(8+9)-VIII-4	-63	0.02	6.40	Si	>100
1170	(8+9)-IV-3	53	0.02	6.40	Si	>100
1170	(8+9)-VI-1	37	0.01	6.40	Si	>100
1170	(8+9)-III-2	74	0.03	6.40	Si	>100
1170	(8+9)-VI-2	-35	0.01	6.40	Si	>100
1170	(8+9)-III-4	-107	0.04	6.40	Si	>100
1170	(8+9)-VI-3	47	0.02	6.40	Si	>100
1170	(8+9)-IV-2	-41	0.01	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
1170	(8+9)-VI-4	-25	0.01	6.40	Si	>100
1170	(8+9)-IV-4	-95	0.03	6.40	Si	>100
1170	(8+9)-I-3	-74	0.03	6.40	Si	>100
1170	(8+9)-II-1	69	0.02	6.40	Si	>100
1170	(8+9)-I-2	86	0.03	6.40	Si	>100
1170	(8+9)-I-4	-95	0.03	6.40	Si	>100
1170	(8+9)-VII-3	45	0.02	6.40	Si	>100
1170	(8+9)-IV-1	107	0.04	6.40	Si	>100
1170	(8+9)-I-1	107	0.04	6.40	Si	>100
1170	(8+9)-III-3	-62	0.02	6.40	Si	>100
1170	(8+9)-III-1	119	0.04	6.40	Si	>100
1170	(8+9)-V-3	33	0.01	6.40	Si	>100
1170	(8+9)-VIII-1	75	0.03	6.40	Si	>100
1170	(8+9)-VIII-2	-73	0.03	6.40	Si	>100
1170	(8+9)-VIII-3	85	0.03	6.40	Si	>100
1170	(8+9)-II-4	-57	0.02	6.40	Si	>100

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Tx kg	τ_{vd} kg/cm ²	fvd kg/cm ²	Csv	τ_M kg/cm ²	fTd kg/cm ²	Csm	Mecc.	Cs
0	(8+9)-III-2	-3319	-5.86	32.00	5.5	-1.42	20.00	14	V	5.5
0	(8+9)-I-2	-3165	-5.59	32.00	5.7	-1.35	20.00	15	V	5.7
0	(8+9)-VIII-4	-2697	-4.76	32.00	6.7	-1.15	20.00	17	V	6.7
0	(8+9)-V-1	-1701	-3.00	32.00	11	-0.73	20.00	28	V	11
0	(8+9)-VII-2	-2838	-5.01	32.00	6.4	-1.21	20.00	16	V	6.4
0	(8+9)-IV-4	-2553	-4.51	32.00	7.1	-1.09	20.00	18	V	7.1
0	(8+9)-VI-4	-2186	-3.86	32.00	8.3	-0.93	20.00	21	V	8.3
0	(8+9)-IV-2	-3601	-6.36	32.00	5.0	-1.54	20.00	13	V	5.0
0	(8+9)-V-2	-2685	-4.74	32.00	6.7	-1.15	20.00	17	V	6.7
0	(8+9)-II-2	-3090	-5.46	32.00	5.9	-1.32	20.00	15	V	5.9
0	(8+9)-VI-2	-2946	-5.20	32.00	6.2	-1.26	20.00	16	V	6.2
0	(8+9)-I-1	-2181	-3.85	32.00	8.3	-0.93	20.00	21	V	8.3
0	(8+9)-VII-1	-1547	-2.73	32.00	12	-0.66	20.00	30	V	12
0	(8+9)-VIII-2	-3457	-6.11	32.00	5.2	-1.48	20.00	14	V	5.2
0	(8+9)-II-4	-2042	-3.61	32.00	8.9	-0.87	20.00	23	V	8.9
0	(8+9)-III-1	-2027	-3.58	32.00	8.9	-0.87	20.00	23	V	8.9
5300	1	1404	2.48	19.20	7.7	0.60	12.00	20	V	7.7
5300	2	2891	5.11	28.80	5.6	1.24	18.00	15	V	5.6
5300	3	2891	5.11	28.80	5.6	1.24	18.00	15	V	5.6
5300	4	1404	2.48	25.60	10	0.60	16.00	27	V	10
5300	5	1404	2.48	25.60	10	0.60	16.00	27	V	10
5300	6	1404	2.48	25.60	10	0.60	16.00	27	V	10
5300	7	1404	2.48	25.60	10	0.60	16.00	27	V	10
5300	(8+9)-IV-1	2820	4.98	32.00	6.4	1.21	20.00	17	V	6.4
5300	(8+9)-III-3	3337	5.89	32.00	5.4	1.43	20.00	14	V	5.4
5300	(8+9)-II-1	2619	4.63	32.00	6.9	1.12	20.00	18	V	6.9
5300	(8+9)-I-3	3276	5.79	32.00	5.5	1.40	20.00	14	V	5.5
5300	(8+9)-II-3	3616	6.39	32.00	5.0	1.55	20.00	13	V	5.0
5300	(8+9)-V-4	2029	3.58	32.00	8.9	0.87	20.00	23	V	8.9
5300	(8+9)-VII-3	3377	5.96	32.00	5.4	1.44	20.00	14	V	5.4
5300	(8+9)-I-4	1989	3.51	32.00	9.1	0.85	20.00	24	V	9.1
5300	(8+9)-VII-4	1968	3.48	32.00	9.2	0.84	20.00	24	V	9.2
5300	(8+9)-VI-1	2607	4.60	32.00	7.0	1.11	20.00	18	V	7.0
5300	(8+9)-VI-3	3628	6.41	32.00	5.0	1.55	20.00	13	V	5.0
5300	(8+9)-V-3	3316	5.86	32.00	5.5	1.42	20.00	14	V	5.5
5300	(8+9)-VIII-1	2808	4.96	32.00	6.5	1.20	20.00	17	V	6.5
5300	(8+9)-III-4	1928	3.41	32.00	9.4	0.82	20.00	24	V	9.4
5300	(8+9)-VIII-3	3829	6.76	32.00	4.7	1.64	20.00	12	V	4.7
5300	(8+9)-IV-3	3817	6.74	32.00	4.7	1.63	20.00	12	V	4.7
Verifiche nella direzione secondaria										
1170	1	214	0.08	19.20	>100	0.02	12.00	>100	V	>100
1170	2	324	0.13	28.80	>100	0.03	18.00	>100	V	>100
1170	3	324	0.13	28.80	>100	0.03	18.00	>100	V	>100

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
1170	4	214	0.08	25.60	>100	0.02	16.00	>100	V	>100
1170	5	214	0.08	25.60	>100	0.02	16.00	>100	V	>100
1170	6	214	0.08	25.60	>100	0.02	16.00	>100	V	>100
1170	7	214	0.08	25.60	>100	0.02	16.00	>100	V	>100
1170	(8+9)-VIII-4	12146	4.73	32.00	6.8	1.15	20.00	17	V	6.8
1170	(8+9)-IV-2	19025	7.42	32.00	4.3	1.79	20.00	11	V	4.3
1170	(8+9)-V-1	7684	3.00	32.00	11	0.72	20.00	28	V	11
1170	(8+9)-I-2	15540	6.06	32.00	5.3	1.47	20.00	14	V	5.3
1170	(8+9)-V-2	15996	6.24	32.00	5.1	1.51	20.00	13	V	5.1
1170	(8+9)-I-4	-6935	-2.70	32.00	12	-0.65	20.00	31	V	12
1170	(8+9)-V-3	-15704	-6.12	32.00	5.2	-1.48	20.00	13	V	5.2
1170	(8+9)-II-2	17372	6.77	32.00	4.7	1.64	20.00	12	V	4.7
1170	(8+9)-V-4	-7392	-2.88	32.00	11	-0.70	20.00	29	V	11
1170	(8+9)-II-4	10629	4.14	32.00	7.7	1.00	20.00	20	V	7.7
1170	(8+9)-VI-1	-10200	-3.98	32.00	8.0	-0.96	20.00	21	V	8.0
1170	(8+9)-III-2	16036	6.25	32.00	5.1	1.51	20.00	13	V	5.1
1170	(8+9)-VI-2	17508	6.83	32.00	4.7	1.65	20.00	12	V	4.7
1170	(8+9)-III-4	-6439	-2.51	32.00	13	-0.61	20.00	33	V	13
1170	(8+9)-VI-3	-17216	-6.71	32.00	4.8	-1.62	20.00	12	V	4.8
1170	(8+9)-I-1	7228	2.82	32.00	11	0.68	20.00	29	V	11
1170	(8+9)-VI-4	10492	4.09	32.00	7.8	0.99	20.00	20	V	7.8
1170	(8+9)-IV-4	12283	4.79	32.00	6.7	1.16	20.00	17	V	6.7
1170	(8+9)-VII-1	7188	2.80	32.00	11	0.68	20.00	29	V	11
1170	(8+9)-II-1	-10337	-4.03	32.00	7.9	-0.98	20.00	21	V	7.9
1170	(8+9)-VII-2	16493	6.43	32.00	5.0	1.56	20.00	13	V	5.0
1170	(8+9)-III-1	6731	2.62	32.00	12	0.64	20.00	31	V	12
1170	(8+9)-VII-3	-16200	-6.32	32.00	5.1	-1.53	20.00	13	V	5.1
1170	(8+9)-IV-1	-11990	-4.67	32.00	6.8	-1.13	20.00	18	V	6.8
1170	(8+9)-VII-4	-6895	-2.69	32.00	12	-0.65	20.00	31	V	12
1170	(8+9)-III-3	-15744	-6.14	32.00	5.2	-1.49	20.00	13	V	5.2
1170	(8+9)-IV-3	-18733	-7.30	32.00	4.4	-1.77	20.00	11	V	4.4
1170	(8+9)-II-3	-17079	-6.66	32.00	4.8	-1.61	20.00	12	V	4.8
1170	(8+9)-VIII-1	-11854	-4.62	32.00	6.9	-1.12	20.00	18	V	6.9
1170	(8+9)-VIII-2	19162	7.47	32.00	4.3	1.81	20.00	11	V	4.3
1170	(8+9)-VIII-3	-18870	-7.36	32.00	4.4	-1.78	20.00	11	V	4.4
1170	(8+9)-I-3	-15248	-5.94	32.00	5.4	-1.44	20.00	14	V	5.4

Verifiche a instabilità

Setto(X)	Comb.	k _{critc}	k _{critm}	λ_{relc}	λ_{relm}	σ_n	σ_{mx}	σ_{my}	f _{td}	f _{cd}	f _{md}	Cs
(cm)						kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	
17(20.0)	(8+9)-IV-3	1.00	--	0.15	--	-0.66	-0.19	9.27	132.00	192.00	192.00	19
18(22.7)	(8+9)-IV-2	1.00	--	0.16	--	-2.69	-3.14	9.36	132.00	192.00	192.00	13
19(530.0)	(8+9)-IV-2	0.26	--	1.92	--	-10.08	-0.23	24.68	132.00	192.00	192.00	3.0
20(0.0)	(8+9)-IV-3	--	--	--	--	11.02	5.70	13.55	132.00	192.00	192.00	5.4

Parete Xlam 11 - Nodi: [6-14-103-104] - **Crit.Prog.** Criterio di verifica XLAM 0 - **Verificato:**

[Cs=1.528,Comb=(8+9)-III-3]

Geometria setti

Setto	Crit.	X	L	S	X90	L90	S90
		mm	cm	cm	mm	cm	cm
17	Criterio di verifica XLAM 0	0	387.0	12.1	0	40.0	12.1
		200	387.0	12.1	1935	40.0	12.1
		400	387.0	12.1	3870	40.0	12.1
18	Criterio di verifica XLAM 0	0	387.0	12.1	0	45.3	12.1
		227	387.0	12.1	1935	45.3	12.1
		453	387.0	12.1	3870	45.3	12.1

Setto	Crit.	X	L	S	X90	L90	S90
19	Criterio di verifica XLAM 0	0	90.0	12.1	0	530.0	12.1
		2650	90.0	12.1	450	530.0	12.1
		5300	90.0	12.1	900	530.0	12.1
20	Criterio di verifica XLAM 0	0	117.0	12.1	0	530.0	12.1
		2650	117.0	12.1	585	530.0	12.1
		5300	117.0	12.1	1170	530.0	12.1

Setto 17: origine (390.4,1283.3,193.5), direzione (-0.611124,0.791535,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	(8+9)-III-2	1005	29	-12562	0.36	0.39	-6.93	132.00	192.00	192.00	24
0	(8+9)-I-2	938	28	-12132	0.33	0.38	-6.69	132.00	192.00	192.00	25
0	(8+9)-VIII-4	752	-23	-9412	0.27	-0.31	-5.19	132.00	192.00	192.00	33
0	(8+9)-V-2	1203	12	-13703	0.43	0.16	-7.56	132.00	192.00	192.00	23
0	(8+9)-VII-4	-1082	-32	6847	-0.39	-0.43	3.78	132.00	192.00	192.00	46
0	(8+9)-V-1	470	19	-6921	0.17	0.25	-3.82	132.00	192.00	192.00	45
0	(8+9)-VII-1	403	18	-6491	0.14	0.24	-3.58	132.00	192.00	192.00	48
0	(8+9)-IV-4	831	-28	-9883	0.30	-0.37	-5.45	132.00	192.00	192.00	31
0	(8+9)-V-4	-1149	-32	7277	-0.41	-0.43	4.02	132.00	192.00	192.00	43
0	(8+9)-II-2	1156	-6	-13802	0.41	-0.09	-7.62	132.00	192.00	192.00	23
0	(8+9)-VI-2	1235	-11	-14273	0.44	-0.15	-7.88	132.00	192.00	192.00	22
0	(8+9)-V-3	-1882	-26	14059	-0.67	-0.34	7.76	132.00	192.00	192.00	24
0	(8+9)-VII-2	1269	12	-14133	0.45	0.17	-7.80	132.00	192.00	192.00	22
0	(8+9)-IV-2	1378	-5	-15234	0.49	-0.06	-8.41	132.00	192.00	192.00	21
0	(8+9)-II-4	609	-30	-8451	0.22	-0.39	-4.66	132.00	192.00	192.00	36
0	(8+9)-VIII-2	1457	-10	-15706	0.52	-0.13	-8.67	132.00	192.00	192.00	20
200	1	-1005	-13	843	-0.36	-0.18	0.47	79.20	115.20	115.20	>100
200	2	-1969	-30	1687	-0.70	-0.41	0.93	118.80	172.80	172.80	>100
200	3	-1969	-30	1687	-0.70	-0.41	0.93	118.80	172.80	172.80	>100
200	4	-1005	-13	843	-0.36	-0.18	0.47	105.60	153.60	153.60	>100
200	5	-1005	-13	843	-0.36	-0.18	0.47	105.60	153.60	153.60	>100
200	6	-1005	-13	843	-0.36	-0.18	0.47	105.60	153.60	153.60	>100
200	7	-1005	-13	843	-0.36	-0.18	0.47	105.60	153.60	153.60	>100
200	(8+9)-IV-1	-1436	15	11060	-0.51	0.20	6.10	132.00	192.00	192.00	30
200	(8+9)-III-3	-1698	-54	14156	-0.60	-0.73	7.81	132.00	192.00	192.00	22
200	(8+9)-IV-3	-1866	-14	16804	-0.66	-0.19	9.27	132.00	192.00	192.00	20
200	(8+9)-I-3	-1644	-49	13717	-0.59	-0.66	7.57	132.00	192.00	192.00	23
200	(8+9)-II-3	-1686	3	15341	-0.60	0.04	8.47	132.00	192.00	192.00	23
200	(8+9)-I-4	-1178	-65	6582	-0.42	-0.87	3.63	132.00	192.00	192.00	43
200	(8+9)-VII-3	-1588	-31	14395	-0.57	-0.42	7.94	132.00	192.00	192.00	23
200	(8+9)-II-1	-1257	32	9597	-0.45	0.43	5.30	132.00	192.00	192.00	34
200	(8+9)-VI-4	-101	-42	-8373	-0.04	-0.57	-4.62	132.00	192.00	192.00	37
200	(8+9)-VI-1	-1290	25	9525	-0.46	0.33	5.26	132.00	192.00	192.00	34
200	(8+9)-VI-3	-1653	10	15412	-0.59	0.13	8.50	132.00	192.00	192.00	22
200	(8+9)-VIII-3	-1833	-7	16875	-0.65	-0.10	9.31	132.00	192.00	192.00	20
200	(8+9)-VIII-1	-1469	8	10988	-0.52	0.10	6.06	132.00	192.00	192.00	31
200	(8+9)-III-4	-1125	-60	6143	-0.40	-0.80	3.39	132.00	192.00	192.00	46
400	(8+9)-I-1	-415	73	-4976	-0.15	0.97	-2.75	132.00	192.00	192.00	52
400	(8+9)-III-1	-467	64	-4563	-0.17	0.85	-2.52	132.00	192.00	192.00	57
Verifiche nella direzione secondaria											
0	(8+9)-VIII-4	-6171	44	826	-31.88	13.14	64.03	132.00	192.00	192.00	2.3
0	(8+9)-VII-2	184	-107	554	0.95	-31.76	42.92	132.00	192.00	192.00	2.5
0	(8+9)-III-3	1733	101	-1070	8.95	29.75	-82.92	132.00	192.00	192.00	1.5
0	(8+9)-IV-2	-5766	-20	1163	-29.78	-5.78	90.08	132.00	192.00	192.00	1.9
0	(8+9)-III-4	-1169	106	-567	-6.04	31.31	-43.92	132.00	192.00	192.00	2.5
0	(8+9)-VIII-2	-4801	-23	972	-24.80	-6.75	75.29	132.00	192.00	192.00	2.3
0	(8+9)-IV-1	3908	-37	-515	20.19	-10.99	-39.92	132.00	192.00	192.00	2.4
0	(8+9)-VII-4	-4384	117	70	-22.65	34.52	5.40	132.00	192.00	192.00	4.5
0	(8+9)-I-1	-364	-100	720	-1.88	-29.48	55.82	132.00	192.00	192.00	2.3
0	(8+9)-IV-3	4467	24	-1042	23.07	6.98	-80.77	132.00	192.00	192.00	1.6
0	(8+9)-I-3	1499	103	-1037	7.74	30.40	-80.33	132.00	192.00	192.00	1.6
0	(8+9)-IV-4	-5207	41	636	-26.89	12.18	49.24	132.00	192.00	192.00	2.9

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-II-1	3128	-30	-404	16.16	-8.84	-31.29	132.00	192.00	192.00	3.0
0	(8+9)-V-1	2852	-111	84	14.73	-32.68	6.51	132.00	192.00	192.00	3.2
0	(8+9)-II-3	3687	31	-931	19.04	9.13	-72.14	132.00	192.00	192.00	1.8
0	(8+9)-V-2	418	-110	521	2.16	-32.41	40.33	132.00	192.00	192.00	2.5
0	(8+9)-III-1	-130	-102	687	-0.67	-30.12	53.23	132.00	192.00	192.00	2.3
0	(8+9)-V-3	-1716	114	-400	-8.87	33.60	-31.02	132.00	192.00	192.00	3.0
0	(8+9)-VIII-3	3502	27	-851	18.09	7.94	-65.97	132.00	192.00	192.00	1.9
0	(8+9)-V-4	-4150	115	36	-21.44	33.87	2.81	132.00	192.00	192.00	4.9
0	(8+9)-VII-3	-1482	112	-434	-7.66	32.96	-33.60	132.00	192.00	192.00	2.9
0	(8+9)-VI-1	4093	-33	-595	21.14	-9.80	-46.09	132.00	192.00	192.00	2.2
0	(8+9)-I-4	-935	104	-600	-4.83	30.67	-46.50	132.00	192.00	192.00	2.5
0	(8+9)-VI-2	-4021	-30	860	-20.77	-8.89	66.66	132.00	192.00	192.00	2.5
0	(8+9)-II-4	-4426	34	524	-22.86	10.03	40.61	132.00	192.00	192.00	3.6
0	(8+9)-VIII-1	4873	-40	-706	25.17	-11.95	-54.71	132.00	192.00	192.00	1.9
0	(8+9)-I-2	-2798	-99	1157	-14.45	-29.21	89.65	132.00	192.00	192.00	1.6
0	(8+9)-II-2	-4986	-27	1051	-25.75	-7.93	81.46	132.00	192.00	192.00	2.1
0	(8+9)-III-2	-3032	-97	1190	-15.66	-28.56	92.24	132.00	192.00	192.00	1.6
0	(8+9)-VI-3	2722	34	-740	14.06	10.09	-57.35	132.00	192.00	192.00	2.2
0	(8+9)-VI-4	-5391	37	715	-27.85	10.99	55.41	132.00	192.00	192.00	2.7
0	(8+9)-VII-1	3086	-113	51	15.94	-33.32	3.92	132.00	192.00	192.00	3.2
3870	1	-453	2	162	-2.34	0.61	12.57	79.20	115.20	115.20	8.7
3870	2	-984	3	347	-5.08	0.94	26.92	118.80	172.80	172.80	6.2
3870	3	-984	3	347	-5.08	0.94	26.92	118.80	172.80	172.80	6.2
3870	4	-453	2	162	-2.34	0.61	12.57	105.60	153.60	153.60	12
3870	5	-453	2	162	-2.34	0.61	12.57	105.60	153.60	153.60	12
3870	6	-453	2	162	-2.34	0.61	12.57	105.60	153.60	153.60	12
3870	7	-453	2	162	-2.34	0.61	12.57	105.60	153.60	153.60	12

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Ty kg	τ_d kg/cmq	fvd kg/cmq	RS	Cs
0	(8+9)-II-1	-17	0.00	6.40	Si	>100
0	(8+9)-VII-4	47	0.01	6.40	Si	>100
0	(8+9)-VII-1	-58	0.01	6.40	Si	>100
0	(8+9)-V-2	-50	0.01	6.40	Si	>100
0	(8+9)-VI-1	-40	0.01	6.40	Si	>100
0	(8+9)-V-4	51	0.01	6.40	Si	>100
0	(8+9)-VI-4	29	0.01	6.40	Si	>100
0	(8+9)-VII-3	43	0.01	6.40	Si	>100
0	(8+9)-V-1	-62	0.02	6.40	Si	>100
0	(8+9)-VIII-1	-27	0.01	6.40	Si	>100
0	(8+9)-IV-2	9	0.00	6.40	Si	>100
0	(8+9)-VII-2	-54	0.01	6.40	Si	>100
200	(8+9)-III-2	40	0.01	6.40	Si	>100
200	(8+9)-I-3	-66	0.02	6.40	Si	>100
200	(8+9)-II-3	-43	0.01	6.40	Si	>100
200	(8+9)-I-2	46	0.01	6.40	Si	>100
200	(8+9)-III-1	41	0.01	6.40	Si	>100
200	(8+9)-I-1	36	0.01	6.40	Si	>100
200	(8+9)-III-3	-60	0.02	6.40	Si	>100
200	(8+9)-III-4	-61	0.02	6.40	Si	>100
200	(8+9)-I-4	-55	0.01	6.40	Si	>100
200	(8+9)-IV-3	-23	0.01	6.40	Si	>100
200	(8+9)-VIII-2	-20	0.01	6.40	Si	>100
200	(8+9)-II-2	23	0.01	6.40	Si	>100
400	1	-15	0.00	3.84	Si	>100
400	2	-41	0.01	5.76	Si	>100
400	3	-41	0.01	5.76	Si	>100
400	4	-15	0.00	5.12	Si	>100
400	5	-15	0.00	5.12	Si	>100
400	6	-15	0.00	5.12	Si	>100
400	7	-15	0.00	5.12	Si	>100
400	(8+9)-VIII-4	-28	0.01	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
400	(8+9)-VI-3	-27	0.01	6.40	Si	>100
400	(8+9)-VI-2	7	0.00	6.40	Si	>100
400	(8+9)-V-3	-43	0.01	6.40	Si	>100
400	(8+9)-IV-4	-32	0.01	6.40	Si	>100
400	(8+9)-II-4	-16	0.00	6.40	Si	>100
400	(8+9)-VIII-3	-10	0.00	6.40	Si	>100
400	(8+9)-IV-1	12	0.00	6.40	Si	>100
Verifiche nella direzione secondaria						
0	1	-9	0.04	3.84	Si	94
0	2	-30	0.14	5.76	Si	40
0	3	-30	0.14	5.76	Si	40
0	4	-9	0.04	5.12	Si	>100
0	5	-9	0.04	5.12	Si	>100
0	6	-9	0.04	5.12	Si	>100
0	7	-9	0.04	5.12	Si	>100
0	(8+9)-VIII-4	-24	0.12	6.40	Si	55
0	(8+9)-VI-1	-6	0.03	6.40	Si	>100
0	(8+9)-III-4	-47	0.22	6.40	Si	29
0	(8+9)-I-2	37	0.18	6.40	Si	36
0	(8+9)-IV-1	17	0.08	6.40	Si	80
0	(8+9)-I-4	-41	0.19	6.40	Si	33
0	(8+9)-I-1	31	0.15	6.40	Si	44
0	(8+9)-VIII-1	14	0.07	6.40	Si	94
0	(8+9)-VII-1	28	0.14	6.40	Si	47
0	(8+9)-VII-4	-38	0.18	6.40	Si	35
0	(8+9)-IV-4	-27	0.13	6.40	Si	50
0	(8+9)-VII-3	-32	0.15	6.40	Si	42
0	(8+9)-I-3	-47	0.22	6.40	Si	29
0	(8+9)-II-3	-27	0.13	6.40	Si	50
0	(8+9)-III-1	37	0.18	6.40	Si	36
0	(8+9)-III-3	-41	0.19	6.40	Si	33
0	(8+9)-V-4	-32	0.15	6.40	Si	42
0	(8+9)-VI-3	-24	0.12	6.40	Si	55
0	(8+9)-V-3	-38	0.18	6.40	Si	35
1935	(8+9)-II-1	-5	0.02	6.40	Si	>100
3870	(8+9)-IV-2	24	0.11	6.40	Si	56
3870	(8+9)-V-1	25	0.12	6.40	Si	54
3870	(8+9)-III-2	34	0.16	6.40	Si	40
3870	(8+9)-VI-2	28	0.13	6.40	Si	48
3870	(8+9)-II-4	14	0.07	6.40	Si	98
3870	(8+9)-VII-2	33	0.16	6.40	Si	41
3870	(8+9)-V-2	34	0.16	6.40	Si	40
3870	(8+9)-IV-3	-12	0.06	6.40	Si	>100
3870	(8+9)-II-2	28	0.14	6.40	Si	47
3870	(8+9)-VIII-2	24	0.11	6.40	Si	57
3870	(8+9)-VIII-3	-12	0.06	6.40	Si	>100
3870	(8+9)-VI-4	14	0.07	6.40	Si	96

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cm ²	kg/cm ²		kg/cm ²	kg/cm ²			
0	1	1200	0.64	19.20	30	0.16	12.00	77	V	30
0	2	2459	1.31	28.80	22	0.32	18.00	57	V	22
0	3	2459	1.31	28.80	22	0.32	18.00	57	V	22
0	4	1200	0.64	25.60	40	0.16	16.00	>100	V	40
0	5	1200	0.64	25.60	40	0.16	16.00	>100	V	40
0	6	1200	0.64	25.60	40	0.16	16.00	>100	V	40
0	7	1200	0.64	25.60	40	0.16	16.00	>100	V	40
0	(8+9)-VII-4	2302	1.23	32.00	26	0.30	20.00	67	V	26
0	(8+9)-VII-3	5437	2.90	32.00	11	0.70	20.00	28	V	11
0	(8+9)-VII-2	-3775	-2.02	32.00	16	-0.49	20.00	41	V	16
0	(8+9)-V-4	2445	1.31	32.00	25	0.32	20.00	63	V	25
0	(8+9)-V-3	5295	2.83	32.00	11	0.68	20.00	29	V	11

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
0	(8+9)-V-2	-3633	-1.94	32.00	17	-0.47	20.00	43	V	17
200	(8+9)-VIII-4	-6787	-3.62	32.00	8.8	-0.88	20.00	23	V	8.8
200	(8+9)-IV-1	7413	3.96	32.00	8.1	0.96	20.00	21	V	8.1
200	(8+9)-I-4	3003	1.60	32.00	20	0.39	20.00	52	V	20
200	(8+9)-II-4	-5208	-2.78	32.00	12	-0.67	20.00	30	V	12
200	(8+9)-VI-1	7617	4.07	32.00	7.9	0.98	20.00	20	V	7.9
200	(8+9)-III-2	-6070	-3.24	32.00	9.9	-0.78	20.00	26	V	9.9
200	(8+9)-VI-2	-6977	-3.73	32.00	8.6	-0.90	20.00	22	V	8.6
200	(8+9)-III-4	2797	1.49	32.00	21	0.36	20.00	55	V	21
200	(8+9)-VI-3	8495	4.54	32.00	7.1	1.10	20.00	18	V	7.1
200	(8+9)-IV-2	-8556	-4.57	32.00	7.0	-1.11	20.00	18	V	7.0
200	(8+9)-VI-4	-6099	-3.26	32.00	9.8	-0.79	20.00	25	V	9.8
200	(8+9)-IV-4	-5896	-3.15	32.00	10	-0.76	20.00	26	V	10
200	(8+9)-II-2	-7868	-4.20	32.00	7.6	-1.02	20.00	20	V	7.6
200	(8+9)-I-3	7381	3.94	32.00	8.1	0.95	20.00	21	V	8.1
200	(8+9)-III-1	-1279	-0.68	32.00	47	-0.17	20.00	>100	V	47
200	(8+9)-I-2	-5864	-3.13	32.00	10	-0.76	20.00	26	V	10
200	(8+9)-II-3	9386	5.01	32.00	6.4	1.21	20.00	16	V	6.4
200	(8+9)-I-1	-1486	-0.79	32.00	40	-0.19	20.00	>100	V	40
200	(8+9)-II-1	6726	3.59	32.00	8.9	0.87	20.00	23	V	8.9
200	(8+9)-III-3	7587	4.05	32.00	7.9	0.98	20.00	20	V	7.9
200	(8+9)-IV-3	10073	5.38	32.00	6.0	1.30	20.00	15	V	6.0
200	(8+9)-VIII-3	9182	4.90	32.00	6.5	1.19	20.00	17	V	6.5
200	(8+9)-VIII-1	8304	4.43	32.00	7.2	1.07	20.00	19	V	7.2
200	(8+9)-VIII-2	-7665	-4.09	32.00	7.8	-0.99	20.00	20	V	7.8
400	(8+9)-VII-1	2782	1.49	32.00	22	0.36	20.00	56	V	22
400	(8+9)-V-1	2532	1.35	32.00	24	0.33	20.00	61	V	24
Verifiche nella direzione secondaria										
0	(8+9)-VIII-4	1103	5.70	32.00	5.6	1.38	20.00	15	V	5.6
0	(8+9)-III-2	1392	7.19	32.00	4.5	1.74	20.00	11	V	4.5
0	(8+9)-V-2	1321	6.83	32.00	4.7	1.65	20.00	12	V	4.7
0	(8+9)-IV-2	1672	8.64	32.00	3.7	2.09	20.00	9.6	V	3.7
0	(8+9)-V-1	597	3.08	32.00	10	0.75	20.00	27	V	10
0	(8+9)-VII-2	1368	7.06	32.00	4.5	1.71	20.00	12	V	4.5
0	(8+9)-IV-4	1096	5.66	32.00	5.7	1.37	20.00	15	V	5.7
0	(8+9)-VI-4	949	4.90	32.00	6.5	1.19	20.00	17	V	6.5
0	(8+9)-II-2	1518	7.84	32.00	4.1	1.90	20.00	11	V	4.1
0	(8+9)-VIII-2	1665	8.60	32.00	3.7	2.08	20.00	9.6	V	3.7
0	(8+9)-VII-1	551	2.85	32.00	11	0.69	20.00	29	V	11
0	(8+9)-VI-2	1511	7.80	32.00	4.1	1.89	20.00	11	V	4.1
0	(8+9)-I-2	1345	6.95	32.00	4.6	1.68	20.00	12	V	4.6
0	(8+9)-I-1	621	3.21	32.00	10.0	0.78	20.00	26	V	10.0
0	(8+9)-II-4	942	4.86	32.00	6.6	1.18	20.00	17	V	6.6
0	(8+9)-III-1	575	2.97	32.00	11	0.72	20.00	28	V	11
3870	1	-741	-3.83	19.20	5.0	-0.93	12.00	13	V	5.0
3870	2	-1536	-7.93	28.80	3.6	-1.92	18.00	9.4	V	3.6
3870	3	-1536	-7.93	28.80	3.6	-1.92	18.00	9.4	V	3.6
3870	4	-741	-3.83	25.60	6.7	-0.93	16.00	17	V	6.7
3870	5	-741	-3.83	25.60	6.7	-0.93	16.00	17	V	6.7
3870	6	-741	-3.83	25.60	6.7	-0.93	16.00	17	V	6.7
3870	7	-741	-3.83	25.60	6.7	-0.93	16.00	17	V	6.7
3870	(8+9)-III-3	-1809	-9.35	32.00	3.4	-2.26	20.00	8.8	V	3.4
3870	(8+9)-II-3	-1801	-9.31	32.00	3.4	-2.25	20.00	8.9	V	3.4
3870	(8+9)-I-4	-1177	-6.08	32.00	5.3	-1.47	20.00	14	V	5.3
3870	(8+9)-IV-1	-1331	-6.88	32.00	4.7	-1.66	20.00	12	V	4.7
3870	(8+9)-V-3	-1373	-7.09	32.00	4.5	-1.72	20.00	12	V	4.5
3870	(8+9)-VII-3	-1405	-7.26	32.00	4.4	-1.76	20.00	11	V	4.4
3870	(8+9)-VI-1	-1344	-6.94	32.00	4.6	-1.68	20.00	12	V	4.6
3870	(8+9)-VII-4	-741	-3.83	32.00	8.4	-0.93	20.00	22	V	8.4
3870	(8+9)-I-3	-1777	-9.18	32.00	3.5	-2.22	20.00	9.0	V	3.5
3870	(8+9)-V-4	-773	-3.99	32.00	8.0	-0.97	20.00	21	V	8.0
3870	(8+9)-II-1	-1223	-6.32	32.00	5.1	-1.53	20.00	13	V	5.1
3870	(8+9)-IV-3	-1910	-9.86	32.00	3.2	-2.39	20.00	8.4	V	3.2
3870	(8+9)-VIII-1	-1452	-7.50	32.00	4.3	-1.82	20.00	11	V	4.3

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
3870	(8+9)-III-4	-1145	-5.91	32.00	5.4	-1.43	20.00	14	V	5.4
3870	(8+9)-VIII-3	-1788	-9.24	32.00	3.5	-2.24	20.00	8.9	V	3.5
3870	(8+9)-VI-3	-1680	-8.68	32.00	3.7	-2.10	20.00	9.5	V	3.7

Setto 18: origine (742.0,828.0,193.5), direzione (-0.611124,0.791535,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	(8+9)-VIII-4	-5188	-213	10101	-1.85	-2.85	5.57	132.00	192.00	192.00	23
0	(8+9)-IV-1	3581	174	-8878	1.27	2.33	-4.90	132.00	192.00	192.00	21
0	(8+9)-II-1	3184	-164	-7839	1.13	-2.19	-4.33	132.00	192.00	192.00	24
0	(8+9)-VIII-1	3522	226	-8761	1.25	3.02	-4.83	132.00	192.00	192.00	20
0	(8+9)-IV-4	-5248	-161	10218	-1.87	-2.16	5.64	132.00	192.00	192.00	25
227	1	-1216	8	1149	-0.43	0.11	0.63	79.20	115.20	115.20	>100
227	2	-2242	16	2020	-0.80	0.21	1.11	118.80	172.80	172.80	>100
227	3	-2242	16	2020	-0.80	0.21	1.11	118.80	172.80	172.80	>100
227	4	-1216	8	1149	-0.43	0.11	0.63	105.60	153.60	153.60	>100
227	5	-1216	8	1149	-0.43	0.11	0.63	105.60	153.60	153.60	>100
227	6	-1216	8	1149	-0.43	0.11	0.63	105.60	153.60	153.60	>100
227	7	-1216	8	1149	-0.43	0.11	0.63	105.60	153.60	153.60	>100
227	(8+9)-IV-2	-7553	-235	16953	-2.69	-3.14	9.36	132.00	192.00	192.00	15
227	(8+9)-V-1	-3738	-98	7385	-1.33	-1.30	4.08	132.00	192.00	192.00	36
227	(8+9)-I-2	-6273	-178	14007	-2.23	-2.38	7.73	132.00	192.00	192.00	19
227	(8+9)-V-4	2071	109	-5799	0.74	1.46	-3.20	132.00	192.00	192.00	34
227	(8+9)-II-4	-4794	163	9755	-1.71	2.18	5.38	132.00	192.00	192.00	25
227	(8+9)-VI-1	2965	-111	-8021	1.06	-1.48	-4.43	132.00	192.00	192.00	26
227	(8+9)-III-2	-6398	-259	14428	-2.28	-3.46	7.96	132.00	192.00	192.00	17
227	(8+9)-VI-2	-7297	77	15697	-2.60	1.03	8.66	132.00	192.00	192.00	20
227	(8+9)-III-4	1402	164	-4884	0.50	2.20	-2.70	132.00	192.00	192.00	34
227	(8+9)-VI-3	5631	-66	-14111	2.00	-0.88	-7.79	132.00	192.00	192.00	17
227	(8+9)-II-2	-7134	36	15549	-2.54	0.48	8.58	132.00	192.00	192.00	21
227	(8+9)-VI-4	-4631	122	9607	-1.65	1.63	5.30	132.00	192.00	192.00	28
227	(8+9)-I-1	-3194	-234	6892	-1.14	-3.13	3.80	132.00	192.00	192.00	28
227	(8+9)-VII-1	-3612	-16	6963	-1.29	-0.22	3.84	132.00	192.00	192.00	47
227	(8+9)-V-2	-6816	-41	14500	-2.43	-0.55	8.00	132.00	192.00	192.00	22
227	(8+9)-VII-2	-6942	-123	14921	-2.47	-1.64	8.23	132.00	192.00	192.00	19
227	(8+9)-III-1	-3069	-153	6470	-1.09	-2.04	3.57	132.00	192.00	192.00	34
227	(8+9)-VII-3	5275	134	-13336	1.88	1.79	-7.36	132.00	192.00	192.00	16
227	(8+9)-II-3	5468	-25	-13963	1.95	-0.33	-7.70	132.00	192.00	192.00	18
227	(8+9)-VII-4	1946	28	-5377	0.69	0.37	-2.97	132.00	192.00	192.00	44
227	(8+9)-III-3	4732	270	-12842	1.68	3.62	-7.09	132.00	192.00	192.00	15
227	(8+9)-IV-3	5886	246	-15367	2.10	3.29	-8.48	132.00	192.00	192.00	13
227	(8+9)-V-3	5150	53	-12914	1.83	0.70	-7.13	132.00	192.00	192.00	18
227	(8+9)-I-3	4606	189	-12421	1.64	2.53	-6.85	132.00	192.00	192.00	16
227	(8+9)-VIII-2	-7716	-194	17101	-2.75	-2.59	9.44	132.00	192.00	192.00	16
227	(8+9)-VIII-3	6049	205	-15515	2.15	2.74	-8.56	132.00	192.00	192.00	13
227	(8+9)-I-4	1528	245	-5306	0.54	3.28	-2.93	132.00	192.00	192.00	27
Verifiche nella direzione secondaria											
0	(8+9)-VIII-4	1438	19	376	6.56	4.98	22.74	132.00	192.00	192.00	5.2
0	(8+9)-VII-2	3368	-86	436	15.36	-22.36	26.36	132.00	192.00	192.00	2.7
0	(8+9)-III-3	-5543	45	-674	-25.28	11.83	-40.72	132.00	192.00	192.00	3.4
0	(8+9)-IV-2	3525	-18	609	16.08	-4.78	36.79	132.00	192.00	192.00	3.0
0	(8+9)-III-4	-3589	39	-339	-16.37	10.17	-20.48	132.00	192.00	192.00	6.0
0	(8+9)-VIII-2	3381	-33	584	15.42	-8.54	35.31	132.00	192.00	192.00	2.9
0	(8+9)-IV-1	-2989	3	-508	-13.63	0.78	-30.66	132.00	192.00	192.00	5.9
0	(8+9)-VII-4	-3109	87	-257	-14.18	22.70	-15.53	132.00	192.00	192.00	4.9
0	(8+9)-I-1	2551	-60	91	11.63	-15.69	5.49	132.00	192.00	192.00	5.0
0	(8+9)-IV-3	-5219	26	-765	-23.81	6.78	-46.20	132.00	192.00	192.00	3.4
0	(8+9)-I-3	-4886	16	-767	-22.28	4.30	-46.31	132.00	192.00	192.00	3.6
0	(8+9)-IV-4	1294	5	352	5.90	1.22	21.25	132.00	192.00	192.00	6.2
0	(8+9)-II-1	-799	-93	-816	-3.64	-24.32	-49.29	132.00	192.00	192.00	2.6
0	(8+9)-V-1	2071	-108	9	9.45	-28.22	0.53	132.00	192.00	192.00	4.5
0	(8+9)-II-3	-3030	-70	-1073	-13.82	-18.32	-64.83	132.00	192.00	192.00	2.3

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-V-2	2711	-57	529	12.37	-14.83	31.95	132.00	192.00	192.00	3.0
0	(8+9)-III-1	1894	-31	183	8.64	-8.16	11.07	132.00	192.00	192.00	6.0
0	(8+9)-V-3	-4406	65	-685	-20.10	16.83	-41.35	132.00	192.00	192.00	3.2
0	(8+9)-VIII-3	-5076	40	-740	-23.15	10.54	-44.71	132.00	192.00	192.00	3.3
0	(8+9)-V-4	-3766	116	-165	-17.18	30.23	-9.94	132.00	192.00	192.00	4.6
0	(8+9)-VII-3	-5063	93	-592	-23.09	24.37	-35.77	132.00	192.00	192.00	3.1
0	(8+9)-VI-1	-943	-108	-841	-4.30	-28.08	-50.78	132.00	192.00	192.00	2.4
0	(8+9)-I-4	-4245	68	-247	-19.36	17.70	-14.89	132.00	192.00	192.00	5.6
0	(8+9)-I-2	1191	63	893	5.43	16.57	53.93	132.00	192.00	192.00	2.4
0	(8+9)-II-4	-896	101	660	-4.09	26.33	39.88	132.00	192.00	192.00	2.9
0	(8+9)-VIII-1	-3132	-11	-532	-14.29	-2.97	-32.15	132.00	192.00	192.00	5.3
0	(8+9)-I-2	3191	-9	611	14.55	-2.30	36.90	132.00	192.00	192.00	3.2
0	(8+9)-II-2	1335	78	917	6.09	20.33	55.42	132.00	192.00	192.00	2.3
0	(8+9)-III-2	3848	-38	518	17.55	-9.83	31.31	132.00	192.00	192.00	2.9
0	(8+9)-VI-3	-2886	-56	-1049	-13.16	-14.56	-63.34	132.00	192.00	192.00	2.4
0	(8+9)-VI-4	-752	115	685	-3.43	30.09	41.37	132.00	192.00	192.00	2.7
0	(8+9)-VII-1	1414	-79	101	6.45	-20.69	6.12	132.00	192.00	192.00	5.3
3870	1	-560	4	-149	-2.55	1.16	-8.99	79.20	115.20	115.20	11
3870	2	-1178	7	-326	-5.37	1.73	-19.69	118.80	172.80	172.80	8.0
3870	3	-1178	7	-326	-5.37	1.73	-19.69	118.80	172.80	172.80	8.0
3870	4	-560	4	-149	-2.55	1.16	-8.99	105.60	153.60	153.60	15
3870	5	-560	4	-149	-2.55	1.16	-8.99	105.60	153.60	153.60	15
3870	6	-560	4	-149	-2.55	1.16	-8.99	105.60	153.60	153.60	15
3870	7	-560	4	-149	-2.55	1.16	-8.99	105.60	153.60	153.60	15

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
0	(8+9)-VI-1	-98	0.03	6.40	Si	>100
0	(8+9)-II-4	90	0.02	6.40	Si	>100
0	(8+9)-III-2	-185	0.05	6.40	Si	>100
0	(8+9)-I-2	-159	0.04	6.40	Si	>100
0	(8+9)-III-1	-156	0.04	6.40	Si	>100
0	(8+9)-I-3	157	0.04	6.40	Si	>100
0	(8+9)-III-3	184	0.05	6.40	Si	>100
0	(8+9)-I-1	-183	0.05	6.40	Si	>100
0	(8+9)-IV-3	98	0.03	6.40	Si	>100
0	(8+9)-III-4	154	0.04	6.40	Si	>100
0	(8+9)-I-4	181	0.05	6.40	Si	>100
0	(8+9)-II-1	-92	0.02	6.40	Si	>100
0	(8+9)-VI-4	96	0.02	6.40	Si	>100
0	(8+9)-IV-2	-100	0.03	6.40	Si	>100
227	(8+9)-VI-3	56	0.01	6.40	Si	>100
227	(8+9)-VIII-2	-113	0.03	6.40	Si	>100
227	(8+9)-VII-4	214	0.06	6.40	Si	>100
227	(8+9)-VIII-3	111	0.03	6.40	Si	>100
227	(8+9)-VI-2	-58	0.01	6.40	Si	>100
227	(8+9)-VII-1	-216	0.06	6.40	Si	>100
227	(8+9)-V-1	-233	0.06	6.40	Si	>100
227	(8+9)-IV-1	62	0.02	6.40	Si	>100
227	(8+9)-VII-2	-242	0.06	6.40	Si	>100
227	(8+9)-VII-3	240	0.06	6.40	Si	>100
227	(8+9)-V-2	-226	0.06	6.40	Si	>100
227	(8+9)-V-3	224	0.06	6.40	Si	>100
227	(8+9)-V-4	231	0.06	6.40	Si	>100
453	1	-4	0.00	3.84	Si	>100
453	2	-6	0.00	5.76	Si	>100
453	3	-6	0.00	5.76	Si	>100
453	4	-4	0.00	5.12	Si	>100
453	5	-4	0.00	5.12	Si	>100
453	6	-4	0.00	5.12	Si	>100
453	7	-4	0.00	5.12	Si	>100
453	(8+9)-VIII-4	-47	0.01	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
453	(8+9)-VIII-1	41	0.01	6.40	Si	>100
453	(8+9)-II-2	41	0.01	6.40	Si	>100
453	(8+9)-II-3	-48	0.01	6.40	Si	>100
453	(8+9)-IV-4	-67	0.02	6.40	Si	>100
Verifiche nella direzione secondaria						
0	(8+9)-VII-3	-217	0.91	6.40	Si	7.0
0	(8+9)-V-4	-234	0.99	6.40	Si	6.5
0	(8+9)-VII-2	220	0.92	6.40	Si	6.9
0	(8+9)-VII-4	-232	0.98	6.40	Si	6.5
0	(8+9)-V-2	218	0.92	6.40	Si	7.0
0	(8+9)-V-1	237	1.00	6.40	Si	6.4
0	(8+9)-VII-1	235	0.99	6.40	Si	6.5
0	(8+9)-VI-4	-99	0.42	6.40	Si	15
0	(8+9)-V-3	-215	0.90	6.40	Si	7.1
0	(8+9)-VI-1	102	0.43	6.40	Si	15
1935	(8+9)-IV-2	-53	0.22	6.40	Si	29
1935	(8+9)-VI-2	-56	0.23	6.40	Si	27
1935	(8+9)-II-2	-56	0.23	6.40	Si	27
1935	(8+9)-II-3	57	0.24	6.40	Si	26
1935	(8+9)-VI-3	58	0.24	6.40	Si	26
1935	(8+9)-VIII-3	55	0.23	6.40	Si	28
1935	(8+9)-VIII-2	-53	0.22	6.40	Si	29
1935	(8+9)-IV-3	55	0.23	6.40	Si	28
3870	1	8	0.04	3.84	Si	>100
3870	2	10	0.04	5.76	Si	>100
3870	3	10	0.04	5.76	Si	>100
3870	4	8	0.04	5.12	Si	>100
3870	5	8	0.04	5.12	Si	>100
3870	6	8	0.04	5.12	Si	>100
3870	7	8	0.04	5.12	Si	>100
3870	(8+9)-VIII-4	-94	0.40	6.40	Si	16
3870	(8+9)-I-2	226	0.95	6.40	Si	6.7
3870	(8+9)-IV-1	142	0.60	6.40	Si	11
3870	(8+9)-III-2	218	0.92	6.40	Si	7.0
3870	(8+9)-I-4	-238	1.00	6.40	Si	6.4
3870	(8+9)-IV-4	-130	0.55	6.40	Si	12
3870	(8+9)-II-4	-102	0.43	6.40	Si	15
3870	(8+9)-III-1	258	1.09	6.40	Si	5.9
3870	(8+9)-I-3	-214	0.90	6.40	Si	7.1
3870	(8+9)-I-1	250	1.05	6.40	Si	6.1
3870	(8+9)-VIII-1	107	0.45	6.40	Si	14
3870	(8+9)-III-3	-206	0.87	6.40	Si	7.4
3870	(8+9)-III-4	-246	1.03	6.40	Si	6.2
3870	(8+9)-II-1	114	0.48	6.40	Si	13

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	(8+9)-VII-2	-5949	-3.18	32.00	10	-0.77	20.00	26	V	10
0	(8+9)-III-2	-8059	-4.30	32.00	7.4	-1.04	20.00	19	V	7.4
0	(8+9)-III-1	-4636	-2.48	32.00	13	-0.60	20.00	33	V	13
0	(8+9)-I-3	6649	3.55	32.00	9.0	0.86	20.00	23	V	9.0
0	(8+9)-III-3	6965	3.72	32.00	8.6	0.90	20.00	22	V	8.6
0	(8+9)-I-4	3859	2.06	32.00	16	0.50	20.00	40	V	16
0	(8+9)-V-4	1748	0.93	32.00	34	0.23	20.00	89	V	34
0	(8+9)-V-3	4539	2.42	32.00	13	0.59	20.00	34	V	13
0	(8+9)-I-2	-7743	-4.13	32.00	7.7	-1.00	20.00	20	V	7.7
0	(8+9)-VII-1	-2526	-1.35	32.00	24	-0.33	20.00	61	V	24
0	(8+9)-VII-4	1433	0.76	32.00	42	0.19	20.00	>100	V	42
0	(8+9)-I-1	-4952	-2.64	32.00	12	-0.64	20.00	31	V	12
0	(8+9)-V-2	-5633	-3.01	32.00	11	-0.73	20.00	27	V	11
0	(8+9)-V-1	-2842	-1.52	32.00	21	-0.37	20.00	54	V	21
0	(8+9)-III-4	3543	1.89	32.00	17	0.46	20.00	44	V	17

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
0	(8+9)-VII-3	4855	2.59	32.00	12	0.63	20.00	32	V	12
227	(8+9)-VI-4	-4292	-2.29	32.00	14	-0.55	20.00	36	V	14
227	(8+9)-VIII-3	6510	3.48	32.00	9.2	0.84	20.00	24	V	9.2
227	(8+9)-II-1	2681	1.43	32.00	22	0.35	20.00	58	V	22
227	(8+9)-VIII-4	-5370	-2.87	32.00	11	-0.69	20.00	29	V	11
227	(8+9)-VIII-1	4388	2.34	32.00	14	0.57	20.00	35	V	14
227	(8+9)-IV-1	3759	2.01	32.00	16	0.49	20.00	41	V	16
227	(8+9)-VI-1	3310	1.77	32.00	18	0.43	20.00	47	V	18
227	(8+9)-IV-3	7139	3.81	32.00	8.4	0.92	20.00	22	V	8.4
227	(8+9)-VI-2	-6414	-3.42	32.00	9.3	-0.83	20.00	24	V	9.3
227	(8+9)-II-4	-3663	-1.96	32.00	16	-0.47	20.00	42	V	16
227	(8+9)-IV-2	-8121	-4.34	32.00	7.4	-1.05	20.00	19	V	7.4
227	(8+9)-IV-4	-4741	-2.53	32.00	13	-0.61	20.00	33	V	13
227	(8+9)-II-2	-7043	-3.76	32.00	8.5	-0.91	20.00	22	V	8.5
227	(8+9)-VI-3	5432	2.90	32.00	11	0.70	20.00	28	V	11
227	(8+9)-II-3	6061	3.24	32.00	9.9	0.78	20.00	26	V	9.9
227	(8+9)-VIII-2	-7492	-4.00	32.00	8.0	-0.97	20.00	21	V	8.0
453	1	-956	-0.51	19.20	38	-0.12	12.00	97	V	38
453	2	-1968	-1.05	28.80	27	-0.25	18.00	71	V	27
453	3	-1968	-1.05	28.80	27	-0.25	18.00	71	V	27
453	4	-956	-0.51	25.60	50	-0.12	16.00	>100	V	50
453	5	-956	-0.51	25.60	50	-0.12	16.00	>100	V	50
453	6	-956	-0.51	25.60	50	-0.12	16.00	>100	V	50
453	7	-956	-0.51	25.60	50	-0.12	16.00	>100	V	50
Verifiche nella direzione secondaria										
1935	(8+9)-IV-2	2735	12.47	32.00	2.6	3.02	20.00	6.6	V	2.6
1935	(8+9)-VI-2	2539	11.58	32.00	2.8	2.80	20.00	7.1	V	2.8
1935	(8+9)-II-1	-1373	-6.26	32.00	5.1	-1.52	20.00	13	V	5.1
1935	(8+9)-VIII-3	-2551	-11.64	32.00	2.8	-2.82	20.00	7.1	V	2.8
1935	(8+9)-II-2	2518	11.49	32.00	2.8	2.78	20.00	7.2	V	2.8
1935	(8+9)-VIII-1	-1569	-7.16	32.00	4.5	-1.73	20.00	12	V	4.5
1935	(8+9)-II-3	-2314	-10.55	32.00	3.0	-2.55	20.00	7.8	V	3.0
1935	(8+9)-VII-3	-2184	-9.96	32.00	3.2	-2.41	20.00	8.3	V	3.2
1935	(8+9)-V-4	-952	-4.34	32.00	7.4	-1.05	20.00	19	V	7.4
1935	(8+9)-V-3	-2119	-9.66	32.00	3.3	-2.34	20.00	8.6	V	3.3
1935	(8+9)-I-3	-2050	-9.35	32.00	3.4	-2.26	20.00	8.8	V	3.4
1935	(8+9)-IV-3	-2531	-11.54	32.00	2.8	-2.79	20.00	7.2	V	2.8
1935	(8+9)-VIII-2	2756	12.57	32.00	2.5	3.04	20.00	6.6	V	2.5
1935	(8+9)-VI-3	-2334	-10.65	32.00	3.0	-2.58	20.00	7.8	V	3.0
1935	(8+9)-VI-1	-1352	-6.17	32.00	5.2	-1.49	20.00	13	V	5.2
1935	(8+9)-I-4	-883	-4.03	32.00	7.9	-0.97	20.00	21	V	7.9
1935	(8+9)-VII-4	-887	-4.04	32.00	7.9	-0.98	20.00	20	V	7.9
1935	(8+9)-III-3	-2115	-9.65	32.00	3.3	-2.33	20.00	8.6	V	3.3
1935	(8+9)-III-4	-818	-3.73	32.00	8.6	-0.90	20.00	22	V	8.6
1935	(8+9)-IV-1	-1589	-7.25	32.00	4.4	-1.75	20.00	11	V	4.4
3870	1	648	2.96	19.20	6.5	0.72	12.00	17	V	6.5
3870	2	1342	6.12	28.80	4.7	1.48	18.00	12	V	4.7
3870	3	1342	6.12	28.80	4.7	1.48	18.00	12	V	4.7
3870	4	648	2.96	25.60	8.7	0.72	16.00	22	V	8.7
3870	5	648	2.96	25.60	8.7	0.72	16.00	22	V	8.7
3870	6	648	2.96	25.60	8.7	0.72	16.00	22	V	8.7
3870	7	648	2.96	25.60	8.7	0.72	16.00	22	V	8.7
3870	(8+9)-VIII-4	1800	8.21	32.00	3.9	1.99	20.00	10	V	3.9
3870	(8+9)-VI-4	1619	7.39	32.00	4.3	1.79	20.00	11	V	4.3
3870	(8+9)-III-2	2413	11.00	32.00	2.9	2.66	20.00	7.5	V	2.9
3870	(8+9)-III-1	1332	6.08	32.00	5.3	1.47	20.00	14	V	5.3
3870	(8+9)-VII-1	1407	6.42	32.00	5.0	1.55	20.00	13	V	5.0
3870	(8+9)-VII-2	2488	11.35	32.00	2.8	2.75	20.00	7.3	V	2.8
3870	(8+9)-II-4	1642	7.49	32.00	4.3	1.81	20.00	11	V	4.3
3870	(8+9)-I-2	2359	10.76	32.00	3.0	2.60	20.00	7.7	V	3.0
3870	(8+9)-V-2	2433	11.10	32.00	2.9	2.69	20.00	7.4	V	2.9
3870	(8+9)-V-1	1461	6.66	32.00	4.8	1.61	20.00	12	V	4.8
3870	(8+9)-IV-4	1822	8.31	32.00	3.9	2.01	20.00	9.9	V	3.9
3870	(8+9)-I-1	1386	6.32	32.00	5.1	1.53	20.00	13	V	5.1

Setto 19: origine (714.3,863.8,45.0), direzione (-0.611124,0.791535,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	(8+9)-V-1	1451	17	-539	2.22	0.99	-5.49	132.00	192.00	192.00	20
0	(8+9)-VII-1	1350	17	-497	2.07	0.99	-5.08	132.00	192.00	192.00	21
2650	1	361	-1	-60	0.55	-0.07	-0.61	79.20	115.20	115.20	78
2650	2	718	-2	-119	1.10	-0.10	-1.21	118.80	172.80	172.80	59
2650	3	718	-2	-119	1.10	-0.10	-1.21	118.80	172.80	172.80	59
2650	4	361	-1	-60	0.55	-0.07	-0.61	105.60	153.60	153.60	>100
2650	5	361	-1	-60	0.55	-0.07	-0.61	105.60	153.60	153.60	>100
2650	6	361	-1	-60	0.55	-0.07	-0.61	105.60	153.60	153.60	>100
2650	7	361	-1	-60	0.55	-0.07	-0.61	105.60	153.60	153.60	>100
5300	(8+9)-V-4	2805	-17	-707	4.29	-0.95	-7.21	132.00	192.00	192.00	13
5300	(8+9)-I-1	-2580	15	1035	-3.95	0.88	10.56	132.00	192.00	192.00	17
5300	(8+9)-I-4	2611	-17	-1021	4.00	-0.95	-10.41	132.00	192.00	192.00	11
5300	(8+9)-VII-2	-5833	11	1824	-8.93	0.64	18.61	132.00	192.00	192.00	9.8
5300	(8+9)-II-2	-6001	-3	2201	-9.18	-0.20	22.46	132.00	192.00	192.00	8.3
5300	(8+9)-VII-3	5864	-12	-1810	8.97	-0.70	-18.46	132.00	192.00	192.00	6.0
5300	(8+9)-II-4	-3579	-12	1273	-5.48	-0.68	12.99	132.00	192.00	192.00	14
5300	(8+9)-VII-4	2630	-17	-641	4.02	-0.96	-6.54	132.00	192.00	192.00	14
5300	(8+9)-III-2	-5639	11	2138	-8.63	0.63	21.82	132.00	192.00	192.00	8.4
5300	(8+9)-VIII-1	4136	11	-1570	6.33	0.64	-16.02	132.00	192.00	192.00	7.4
5300	(8+9)-III-4	2435	-17	-955	3.73	-0.96	-9.75	132.00	192.00	192.00	12
5300	(8+9)-VIII-2	-6645	-4	2324	-10.17	-0.23	23.71	132.00	192.00	192.00	7.8
5300	(8+9)-IV-2	-6586	-4	2418	-10.08	-0.23	24.68	132.00	192.00	192.00	7.5
5300	(8+9)-VIII-3	6675	3	-2309	10.22	0.16	-23.56	132.00	192.00	192.00	5.0
5300	(8+9)-IV-4	-4164	-12	1490	-6.37	-0.70	15.21	132.00	192.00	192.00	12
5300	(8+9)-VIII-4	-4106	-12	1585	-6.28	-0.71	16.17	132.00	192.00	192.00	11
5300	(8+9)-V-2	-5658	11	1759	-8.66	0.64	17.95	132.00	192.00	192.00	10
5300	(8+9)-III-3	5670	-12	-2124	8.68	-0.70	-21.67	132.00	192.00	192.00	5.5
5300	(8+9)-I-2	-5463	11	2073	-8.36	0.64	21.15	132.00	192.00	192.00	8.7
5300	(8+9)-IV-1	4195	11	-1475	6.42	0.64	-15.05	132.00	192.00	192.00	7.7
5300	(8+9)-VI-2	-6059	-3	2107	-9.27	-0.20	21.50	132.00	192.00	192.00	8.7
5300	(8+9)-IV-3	6617	3	-2404	10.13	0.16	-24.52	132.00	192.00	192.00	4.9
5300	(8+9)-VI-4	-3521	-12	1367	-5.39	-0.68	13.95	132.00	192.00	192.00	13
5300	(8+9)-I-3	5494	-12	-2058	8.41	-0.71	-21.00	132.00	192.00	192.00	5.7
5300	(8+9)-II-3	6032	2	-2186	9.23	0.13	-22.31	132.00	192.00	192.00	5.4
5300	(8+9)-VI-1	3551	11	-1352	5.44	0.61	-13.80	132.00	192.00	192.00	8.6
5300	(8+9)-VI-3	6090	2	-2092	9.32	0.13	-21.35	132.00	192.00	192.00	5.5
5300	(8+9)-II-1	3610	11	-1258	5.52	0.61	-12.84	132.00	192.00	192.00	8.9
5300	(8+9)-III-1	-2405	16	970	-3.68	0.89	9.90	132.00	192.00	192.00	18
5300	(8+9)-V-3	5689	-12	-1744	8.71	-0.71	-17.80	132.00	192.00	192.00	6.2
Verifiche nella direzione secondaria											
0	2	-3755	29	1320	-1.46	0.64	0.58	118.80	172.80	172.80	>100
0	3	-3755	29	1320	-1.46	0.64	0.58	118.80	172.80	172.80	>100
0	(8+9)-III-1	-753	-45	-7304	-0.29	-1.01	-3.22	132.00	192.00	192.00	45
0	(8+9)-V-4	-4603	212	444	-1.79	4.72	0.20	132.00	192.00	192.00	39
0	(8+9)-VII-4	-4699	213	-175	-1.83	4.74	-0.08	132.00	192.00	192.00	40
0	(8+9)-V-3	-4146	215	8664	-1.62	4.80	3.82	132.00	192.00	192.00	22
0	(8+9)-VII-2	1328	-203	-8106	0.52	-4.54	-3.58	132.00	192.00	192.00	22
0	(8+9)-VI-2	-1219	-63	-14302	-0.48	-1.40	-6.31	132.00	192.00	192.00	25
0	(8+9)-VII-3	-4050	214	9282	-1.58	4.78	4.10	132.00	192.00	192.00	22
0	(8+9)-VI-3	-1503	73	15478	-0.59	1.63	6.83	132.00	192.00	192.00	23
0	(8+9)-I-4	-1873	55	9098	-0.73	1.23	4.02	132.00	192.00	192.00	37
0	(8+9)-V-2	1424	-204	-7488	0.56	-4.56	-3.30	132.00	192.00	192.00	22
0	(8+9)-III-4	-1969	56	8480	-0.77	1.25	3.74	132.00	192.00	192.00	38
450	1	-2629	7	1049	-1.02	0.15	0.46	79.20	115.20	115.20	>100
450	4	-2629	7	1049	-1.02	0.15	0.46	105.60	153.60	153.60	>100
450	5	-2629	7	1049	-1.02	0.15	0.46	105.60	153.60	153.60	>100
450	6	-2629	7	1049	-1.02	0.15	0.46	105.60	153.60	153.60	>100
450	7	-2629	7	1049	-1.02	0.15	0.46	105.60	153.60	153.60	>100
450	(8+9)-VIII-4	-5403	15	-23040	-2.11	0.33	-10.17	132.00	192.00	192.00	18

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
450	(8+9)-II-4	-5332	17	-10596	-2.08	0.38	-4.68	132.00	192.00	192.00	38
450	(8+9)-VII-1	5893	-36	8561	2.30	-0.79	3.78	132.00	192.00	192.00	24
450	(8+9)-IV-1	436	-8	20474	0.17	-0.17	9.04	132.00	192.00	192.00	20
450	(8+9)-IV-2	-2385	-11	-26587	-0.93	-0.24	-11.73	132.00	192.00	192.00	16
450	(8+9)-VI-1	3064	-7	16058	1.19	-0.16	7.09	132.00	192.00	192.00	21
450	(8+9)-II-1	1714	-9	12044	0.67	-0.19	5.32	132.00	192.00	192.00	30
450	(8+9)-VIII-1	1785	-6	24488	0.70	-0.14	10.81	132.00	192.00	192.00	16
450	(8+9)-IV-3	-1233	19	28035	-0.48	0.42	12.37	132.00	192.00	192.00	15
450	(8+9)-V-1	6276	-36	6032	2.45	-0.80	2.66	132.00	192.00	192.00	27
450	(8+9)-I-1	1779	-40	-7348	0.69	-0.90	-3.24	132.00	192.00	192.00	37
450	(8+9)-IV-4	-4054	16	-19026	-1.58	0.36	-8.40	132.00	192.00	192.00	22
450	(8+9)-VI-4	-6681	15	-14610	-2.60	0.35	-6.45	132.00	192.00	192.00	28
900	(8+9)-I-2	-184	-17	-18521	-0.07	-0.37	-8.17	132.00	192.00	192.00	22
900	(8+9)-III-3	-3662	24	22257	-1.43	0.55	9.82	132.00	192.00	192.00	19
900	(8+9)-III-2	132	-18	-20740	0.05	-0.41	-9.15	132.00	192.00	192.00	20
900	(8+9)-II-3	-432	4	20964	-0.17	0.10	9.25	132.00	192.00	192.00	21
900	(8+9)-I-3	-3346	23	20038	-1.30	0.51	8.84	132.00	192.00	192.00	21
900	(8+9)-VIII-2	-1230	-9	-23950	-0.48	-0.21	-10.57	132.00	192.00	192.00	18
900	(8+9)-VIII-3	-2300	15	25467	-0.90	0.34	11.24	132.00	192.00	192.00	17
900	(8+9)-II-2	-3098	2	-19447	-1.21	0.04	-8.58	132.00	192.00	192.00	22

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
0	(8+9)-VIII-4	-11	0.01	6.40	Si	>100
0	(8+9)-IV-1	-13	0.01	6.40	Si	>100
0	(8+9)-VI-3	-28	0.03	6.40	Si	>100
0	(8+9)-III-2	-12	0.01	6.40	Si	>100
0	(8+9)-IV-2	2	0.00	6.40	Si	>100
0	(8+9)-III-3	10	0.01	6.40	Si	>100
0	(8+9)-VIII-2	23	0.03	6.40	Si	>100
0	(8+9)-III-4	14	0.02	6.40	Si	>100
0	(8+9)-VII-4	-56	0.06	6.40	Si	>100
0	(8+9)-VII-1	53	0.06	6.40	Si	>100
0	(8+9)-I-2	-11	0.01	6.40	Si	>100
0	(8+9)-I-4	15	0.02	6.40	Si	>100
0	(8+9)-IV-3	-5	0.01	6.40	Si	>100
0	(8+9)-VII-3	-60	0.07	6.40	Si	95
0	(8+9)-IV-4	10	0.01	6.40	Si	>100
0	(8+9)-II-4	13	0.01	6.40	Si	>100
0	(8+9)-V-1	52	0.06	6.40	Si	>100
0	(8+9)-VIII-3	-26	0.03	6.40	Si	>100
0	(8+9)-V-2	59	0.07	6.40	Si	98
0	(8+9)-I-1	-17	0.02	6.40	Si	>100
0	(8+9)-V-3	-61	0.07	6.40	Si	94
0	(8+9)-II-1	-15	0.02	6.40	Si	>100
0	(8+9)-III-1	-17	0.02	6.40	Si	>100
0	(8+9)-VIII-1	8	0.01	6.40	Si	>100
0	(8+9)-I-3	9	0.01	6.40	Si	>100
0	(8+9)-VII-2	58	0.06	6.40	Si	100
0	(8+9)-V-4	-55	0.06	6.40	Si	>100
0	(8+9)-VI-4	-8	0.01	6.40	Si	>100
0	(8+9)-VI-2	26	0.03	6.40	Si	>100
5300	1	-2	0.00	3.84	Si	>100
5300	2	-8	0.01	5.76	Si	>100
5300	3	-8	0.01	5.76	Si	>100
5300	4	-2	0.00	5.12	Si	>100
5300	5	-2	0.00	5.12	Si	>100
5300	6	-2	0.00	5.12	Si	>100
5300	7	-2	0.00	5.12	Si	>100
5300	(8+9)-II-2	7	0.01	6.40	Si	>100
5300	(8+9)-II-3	-9	0.01	6.40	Si	>100
5300	(8+9)-VI-1	-9	0.01	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
Verifiche nella direzione secondaria						
0	(8+9)-VIII-4	-55	0.02	6.40	Si	>100
0	(8+9)-IV-1	44	0.02	6.40	Si	>100
0	(8+9)-V-3	-78	0.03	6.40	Si	>100
0	(8+9)-IV-2	-14	0.01	6.40	Si	>100
0	(8+9)-II-1	33	0.01	6.40	Si	>100
0	(8+9)-VII-4	-93	0.03	6.40	Si	>100
0	(8+9)-V-2	76	0.03	6.40	Si	>100
0	(8+9)-VII-2	72	0.03	6.40	Si	>100
0	(8+9)-V-1	87	0.03	6.40	Si	>100
0	(8+9)-VI-4	-44	0.02	6.40	Si	>100
0	(8+9)-II-4	-36	0.01	6.40	Si	>100
0	(8+9)-VII-3	-75	0.03	6.40	Si	>100
0	(8+9)-VII-1	90	0.03	6.40	Si	>100
0	(8+9)-VI-1	42	0.01	6.40	Si	>100
0	(8+9)-VIII-1	53	0.02	6.40	Si	>100
0	(8+9)-IV-4	-47	0.02	6.40	Si	>100
0	(8+9)-IV-3	11	0.00	6.40	Si	>100
0	(8+9)-V-4	-89	0.03	6.40	Si	>100
450	1	-9	0.00	3.84	Si	>100
450	2	-36	0.01	5.76	Si	>100
450	3	-36	0.01	5.76	Si	>100
450	4	-9	0.00	5.12	Si	>100
450	5	-9	0.00	5.12	Si	>100
450	6	-9	0.00	5.12	Si	>100
450	7	-9	0.00	5.12	Si	>100
450	(8+9)-III-4	-75	0.03	6.40	Si	>100
450	(8+9)-VIII-2	-17	0.01	6.40	Si	>100
450	(8+9)-VIII-3	6	0.00	6.40	Si	>100
450	(8+9)-I-3	-66	0.02	6.40	Si	>100
450	(8+9)-VI-2	-7	0.00	6.40	Si	>100
450	(8+9)-I-1	62	0.02	6.40	Si	>100
450	(8+9)-I-2	55	0.02	6.40	Si	>100
450	(8+9)-I-4	-72	0.03	6.40	Si	>100
450	(8+9)-III-1	65	0.02	6.40	Si	>100
450	(8+9)-III-2	52	0.02	6.40	Si	>100
450	(8+9)-III-3	-63	0.02	6.40	Si	>100
900	(8+9)-VI-3	-10	0.00	6.40	Si	>100
900	(8+9)-II-2	8	0.00	6.40	Si	>100
900	(8+9)-II-3	-17	0.01	6.40	Si	>100

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	1	381	0.87	19.20	22	0.21	12.00	57	V	22
0	2	753	1.73	28.80	17	0.42	18.00	43	V	17
0	3	753	1.73	28.80	17	0.42	18.00	43	V	17
0	4	381	0.87	25.60	29	0.21	16.00	76	V	29
0	5	381	0.87	25.60	29	0.21	16.00	76	V	29
0	6	381	0.87	25.60	29	0.21	16.00	76	V	29
0	7	381	0.87	25.60	29	0.21	16.00	76	V	29
0	(8+9)-IV-1	1884	4.32	32.00	7.4	1.05	20.00	19	V	7.4
0	(8+9)-V-2	-1937	-4.45	32.00	7.2	-1.08	20.00	19	V	7.2
0	(8+9)-VII-2	-2019	-4.64	32.00	6.9	-1.12	20.00	18	V	6.9
0	(8+9)-V-1	-826	-1.90	32.00	17	-0.46	20.00	44	V	17
0	(8+9)-VII-1	-744	-1.71	32.00	19	-0.41	20.00	48	V	19
0	(8+9)-VII-3	2541	5.83	32.00	5.5	1.41	20.00	14	V	5.5
0	(8+9)-VIII-3	2880	6.61	32.00	4.8	1.60	20.00	13	V	4.8
0	(8+9)-II-1	1609	3.69	32.00	8.7	0.89	20.00	22	V	8.7
0	(8+9)-VI-3	2605	5.98	32.00	5.4	1.45	20.00	14	V	5.4
0	(8+9)-V-4	1348	3.10	32.00	10	0.75	20.00	27	V	10
0	(8+9)-V-3	2459	5.64	32.00	5.7	1.37	20.00	15	V	5.7
0	(8+9)-VII-4	1266	2.91	32.00	11	0.70	20.00	28	V	11

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
5300	(8+9)-VIII-4	-2404	-5.52	32.00	5.8	-1.34	20.00	15	V	5.8
5300	(8+9)-I-2	-3499	-8.03	32.00	4.0	-1.94	20.00	10	V	4.0
5300	(8+9)-III-1	-2111	-4.85	32.00	6.6	-1.17	20.00	17	V	6.6
5300	(8+9)-IV-2	-3429	-7.87	32.00	4.1	-1.91	20.00	10	V	4.1
5300	(8+9)-VI-4	-2079	-4.77	32.00	6.7	-1.15	20.00	17	V	6.7
5300	(8+9)-IV-4	-1801	-4.14	32.00	7.7	-1.00	20.00	20	V	7.7
5300	(8+9)-II-4	-1476	-3.39	32.00	9.4	-0.82	20.00	24	V	9.4
5300	(8+9)-III-4	1831	4.20	32.00	7.6	1.02	20.00	20	V	7.6
5300	(8+9)-II-3	2824	6.48	32.00	4.9	1.57	20.00	13	V	4.9
5300	(8+9)-III-2	-3596	-8.26	32.00	3.9	-2.00	20.00	10	V	3.9
5300	(8+9)-II-2	-3104	-7.13	32.00	4.5	-1.72	20.00	12	V	4.5
5300	(8+9)-VI-2	-2501	-5.74	32.00	5.6	-1.39	20.00	14	V	5.6
5300	(8+9)-I-4	1928	4.43	32.00	7.2	1.07	20.00	19	V	7.2
5300	(8+9)-VI-1	1798	4.13	32.00	7.8	1.00	20.00	20	V	7.8
5300	(8+9)-IV-3	3149	7.23	32.00	4.4	1.75	20.00	11	V	4.4
5300	(8+9)-III-3	3316	7.61	32.00	4.2	1.84	20.00	11	V	4.2
5300	(8+9)-VIII-1	2124	4.88	32.00	6.6	1.18	20.00	17	V	6.6
5300	(8+9)-VIII-2	-2827	-6.49	32.00	4.9	-1.57	20.00	13	V	4.9
5300	(8+9)-I-3	3218	7.39	32.00	4.3	1.79	20.00	11	V	4.3
5300	(8+9)-I-1	-2209	-5.07	32.00	6.3	-1.23	20.00	16	V	6.3
Verifiche nella direzione secondaria										
0	(8+9)-VIII-4	7507	2.93	32.00	11	0.71	20.00	28	V	11
0	(8+9)-VII-2	9844	3.84	32.00	8.3	0.93	20.00	22	V	8.3
0	(8+9)-III-3	-9930	-3.87	32.00	8.3	-0.94	20.00	21	V	8.3
0	(8+9)-IV-2	11705	4.56	32.00	7.0	1.10	20.00	18	V	7.0
0	(8+9)-III-4	-4150	-1.62	32.00	20	-0.39	20.00	51	V	20
0	(8+9)-VIII-2	11697	4.56	32.00	7.0	1.10	20.00	18	V	7.0
0	(8+9)-IV-1	-7559	-2.95	32.00	11	-0.71	20.00	28	V	11
0	(8+9)-VII-4	-4125	-1.61	32.00	20	-0.39	20.00	51	V	20
0	(8+9)-I-1	4407	1.72	32.00	19	0.42	20.00	48	V	19
0	(8+9)-IV-3	-11765	-4.59	32.00	7.0	-1.11	20.00	18	V	7.0
0	(8+9)-I-3	-9613	-3.75	32.00	8.5	-0.91	20.00	22	V	8.5
0	(8+9)-IV-4	7499	2.92	32.00	11	0.71	20.00	28	V	11
0	(8+9)-II-1	-6505	-2.54	32.00	13	-0.61	20.00	33	V	13
0	(8+9)-V-1	4381	1.71	32.00	19	0.41	20.00	48	V	19
0	(8+9)-II-3	-10711	-4.18	32.00	7.7	-1.01	20.00	20	V	7.7
0	(8+9)-V-2	9528	3.71	32.00	8.6	0.90	20.00	22	V	8.6
0	(8+9)-III-1	4091	1.59	32.00	20	0.39	20.00	52	V	20
0	(8+9)-V-3	-9588	-3.74	32.00	8.6	-0.90	20.00	22	V	8.6
0	(8+9)-VIII-3	-11757	-4.58	32.00	7.0	-1.11	20.00	18	V	7.0
0	(8+9)-V-4	-4441	-1.73	32.00	18	-0.42	20.00	48	V	18
0	(8+9)-VII-3	-9904	-3.86	32.00	8.3	-0.93	20.00	21	V	8.3
0	(8+9)-VI-1	-6513	-2.54	32.00	13	-0.61	20.00	33	V	13
0	(8+9)-I-4	-4467	-1.74	32.00	18	-0.42	20.00	47	V	18
0	(8+9)-VI-2	10643	4.15	32.00	7.7	1.00	20.00	20	V	7.7
0	(8+9)-II-4	6445	2.51	32.00	13	0.61	20.00	33	V	13
0	(8+9)-VIII-1	-7566	-2.95	32.00	11	-0.71	20.00	28	V	11
0	(8+9)-I-2	9554	3.72	32.00	8.6	0.90	20.00	22	V	8.6
0	(8+9)-II-2	10651	4.15	32.00	7.7	1.00	20.00	20	V	7.7
0	(8+9)-III-2	9870	3.85	32.00	8.3	0.93	20.00	21	V	8.3
0	(8+9)-VI-3	-10703	-4.17	32.00	7.7	-1.01	20.00	20	V	7.7
0	(8+9)-VI-4	6453	2.52	32.00	13	0.61	20.00	33	V	13
0	(8+9)-VII-1	4065	1.58	32.00	20	0.38	20.00	52	V	20
450	1	-70	-0.03	19.20	>100	-0.01	12.00	>100	V	>100
450	2	-139	-0.05	28.80	>100	-0.01	18.00	>100	V	>100
450	3	-139	-0.05	28.80	>100	-0.01	18.00	>100	V	>100
450	4	-70	-0.03	25.60	>100	-0.01	16.00	>100	V	>100
450	5	-70	-0.03	25.60	>100	-0.01	16.00	>100	V	>100
450	6	-70	-0.03	25.60	>100	-0.01	16.00	>100	V	>100
450	7	-70	-0.03	25.60	>100	-0.01	16.00	>100	V	>100

Setto 20: origine (714.3,863.8,328.5), direzione (-0.611124,0.791535,0)
Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	(8+9)-III-3	7850	162	1856	9.24	7.14	11.21	132.00	192.00	192.00	6.0
0	(8+9)-I-3	7613	104	1792	8.96	4.60	10.82	132.00	192.00	192.00	6.7
0	(8+9)-IV-1	5803	50	1339	6.83	2.20	8.09	132.00	192.00	192.00	9.5
0	(8+9)-I-4	3227	168	683	3.80	7.43	4.12	132.00	192.00	192.00	11
0	(8+9)-VIII-1	5725	82	1337	6.74	3.63	8.07	132.00	192.00	192.00	8.9
0	(8+9)-II-1	5012	-142	1124	5.90	-6.30	6.79	132.00	192.00	192.00	8.9
0	(8+9)-VI-3	8652	-96	2032	10.19	-4.23	12.27	132.00	192.00	192.00	6.1
0	(8+9)-IV-3	9365	129	2244	11.02	5.70	13.55	132.00	192.00	192.00	5.4
0	(8+9)-V-4	3486	60	690	4.10	2.65	4.16	132.00	192.00	192.00	15
0	(8+9)-II-3	8574	-63	2030	10.09	-2.79	12.25	132.00	192.00	192.00	6.5
0	(8+9)-VII-3	8109	53	1863	9.55	2.37	11.25	132.00	192.00	192.00	7.0
0	(8+9)-VI-1	4935	-110	1122	5.81	-4.87	6.78	132.00	192.00	192.00	9.6
0	(8+9)-I-1	-4259	-160	-1225	-5.01	-7.09	-7.40	132.00	192.00	192.00	13
0	(8+9)-VIII-3	9442	96	2247	11.12	4.27	13.56	132.00	192.00	192.00	5.6
0	(8+9)-V-3	7872	-4	1799	9.27	-0.18	10.86	132.00	192.00	192.00	7.8
0	(8+9)-III-1	-4022	-103	-1161	-4.74	-4.54	-7.01	132.00	192.00	192.00	16
0	(8+9)-III-4	2990	110	618	3.52	4.88	3.73	132.00	192.00	192.00	14
2650	1	1712	-3	401	2.02	-0.15	2.42	79.20	115.20	115.20	21
2650	2	3648	-7	853	4.30	-0.32	5.15	118.80	172.80	172.80	15
2650	3	3648	-7	853	4.30	-0.32	5.15	118.80	172.80	172.80	15
2650	4	1712	-3	401	2.02	-0.15	2.42	105.60	153.60	153.60	28
2650	5	1712	-3	401	2.02	-0.15	2.42	105.60	153.60	153.60	28
2650	6	1712	-3	401	2.02	-0.15	2.42	105.60	153.60	153.60	28
2650	7	1712	-3	401	2.02	-0.15	2.42	105.60	153.60	153.60	28
5300	(8+9)-VIII-4	5006	-4	1756	5.89	-0.19	10.60	132.00	192.00	192.00	9.9
5300	(8+9)-VI-2	7251	-14	2648	8.54	-0.62	15.99	132.00	192.00	192.00	6.6
5300	(8+9)-III-2	6612	20	2382	7.78	0.88	14.38	132.00	192.00	192.00	7.2
5300	(8+9)-VII-2	6793	3	2450	8.00	0.14	14.79	132.00	192.00	192.00	7.2
5300	(8+9)-I-2	6370	15	2294	7.50	0.68	13.85	132.00	192.00	192.00	7.5
5300	(8+9)-II-2	7197	-9	2627	8.47	-0.40	15.86	132.00	192.00	192.00	6.7
5300	(8+9)-V-1	2903	5	930	3.42	0.22	5.61	132.00	192.00	192.00	18
5300	(8+9)-VII-4	-3371	-13	-1504	-3.97	-0.57	-9.08	132.00	192.00	192.00	20
5300	(8+9)-V-2	6551	-1	2361	7.71	-0.06	14.26	132.00	192.00	192.00	7.5
5300	(8+9)-IV-4	5061	-9	1777	5.96	-0.41	10.73	132.00	192.00	192.00	9.7
5300	(8+9)-VII-1	2661	1	841	3.13	0.02	5.08	132.00	192.00	192.00	20
5300	(8+9)-IV-2	8001	6	2922	9.42	0.25	17.64	132.00	192.00	192.00	6.1
5300	(8+9)-VIII-2	8055	1	2943	9.48	0.03	17.77	132.00	192.00	192.00	6.1
5300	(8+9)-II-4	4256	-24	1482	5.01	-1.06	8.95	132.00	192.00	192.00	11
5300	(8+9)-VI-4	4202	-19	1462	4.95	-0.83	8.82	132.00	192.00	192.00	11
Verifiche nella direzione secondaria											
0	1	-3194	5	768	-1.25	0.11	0.34	79.20	115.20	115.20	>100
0	2	-6606	9	1315	-2.58	0.21	0.58	118.80	172.80	172.80	>100
0	3	-6606	9	1315	-2.58	0.21	0.58	118.80	172.80	172.80	>100
0	4	-3194	5	768	-1.25	0.11	0.34	105.60	153.60	153.60	>100
0	5	-3194	5	768	-1.25	0.11	0.34	105.60	153.60	153.60	>100
0	6	-3194	5	768	-1.25	0.11	0.34	105.60	153.60	153.60	>100
0	7	-3194	5	768	-1.25	0.11	0.34	105.60	153.60	153.60	>100
0	(8+9)-VIII-4	-4099	-5	6782	-1.60	-0.10	2.99	132.00	192.00	192.00	62
0	(8+9)-IV-2	-3296	-8	9663	-1.28	-0.19	4.26	132.00	192.00	192.00	43
0	(8+9)-V-1	-472	12	3284	-0.18	0.26	1.45	132.00	192.00	192.00	>100
0	(8+9)-I-2	-1251	-17	7387	-0.49	-0.38	3.26	132.00	192.00	192.00	53
0	(8+9)-V-2	-1263	6	7780	-0.49	0.14	3.43	132.00	192.00	192.00	54
0	(8+9)-I-4	-3940	19	-1823	-1.54	0.42	-0.80	132.00	192.00	192.00	>100
0	(8+9)-V-3	-3138	1	-6713	-1.22	0.02	-2.96	132.00	192.00	192.00	64
0	(8+9)-II-2	-3115	-11	9408	-1.21	-0.24	4.15	132.00	192.00	192.00	44
0	(8+9)-V-4	-3928	-4	-2217	-1.53	-0.10	-0.98	132.00	192.00	192.00	>100
0	(8+9)-II-4	-3922	-0	6646	-1.53	-0.00	2.93	132.00	192.00	192.00	65
0	(8+9)-VI-1	-482	14	-5460	-0.19	0.32	-2.41	132.00	192.00	192.00	70
0	(8+9)-III-2	-1305	-16	7463	-0.51	-0.36	3.29	132.00	192.00	192.00	52
0	(8+9)-VI-2	-3118	-4	9527	-1.22	-0.09	4.20	132.00	192.00	192.00	45
0	(8+9)-III-4	-3994	19	-1747	-1.56	0.43	-0.77	132.00	192.00	192.00	>100
0	(8+9)-VI-3	-1282	11	-8459	-0.50	0.25	-3.73	132.00	192.00	192.00	48
0	(8+9)-I-1	-460	-12	2891	-0.18	-0.26	1.28	132.00	192.00	192.00	>100

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-VI-4	-3918	-7	6527	-1.53	-0.16	2.88	132.00	192.00	192.00	63
0	(8+9)-IV-4	-4102	2	6900	-1.60	0.05	3.05	132.00	192.00	192.00	62
0	(8+9)-VII-1	-418	11	3208	-0.16	0.24	1.42	132.00	192.00	192.00	>100
0	(8+9)-II-1	-479	7	-5578	-0.19	0.16	-2.46	132.00	192.00	192.00	73
0	(8+9)-VII-2	-1317	7	7857	-0.51	0.15	3.47	132.00	192.00	192.00	53
0	(8+9)-III-1	-406	-12	2814	-0.16	-0.27	1.24	132.00	192.00	192.00	>100
0	(8+9)-VII-3	-3083	0	-6789	-1.20	0.00	-3.00	132.00	192.00	192.00	64
0	(8+9)-IV-1	-298	5	-5832	-0.12	0.11	-2.57	132.00	192.00	192.00	72
0	(8+9)-I-3	-3149	24	-6319	-1.23	0.54	-2.79	132.00	192.00	192.00	58
0	(8+9)-III-3	-3095	23	-6395	-1.21	0.52	-2.82	132.00	192.00	192.00	57
0	(8+9)-IV-3	-1105	15	-8595	-0.43	0.35	-3.79	132.00	192.00	192.00	46
0	(8+9)-II-3	-1286	18	-8341	-0.50	0.40	-3.68	132.00	192.00	192.00	47
0	(8+9)-VIII-1	-302	12	-5714	-0.12	0.26	-2.52	132.00	192.00	192.00	69
0	(8+9)-VIII-2	-3299	-1	9781	-1.29	-0.03	4.32	132.00	192.00	192.00	44
0	(8+9)-VIII-3	-1101	9	-8713	-0.43	0.19	-3.85	132.00	192.00	192.00	48
585	(8+9)-VII-4	-2813	-12	-1795	-1.10	-0.26	-0.79	132.00	192.00	192.00	>100

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Ty kg	τ_d kg/cm ²	fvd kg/cm ²	RS	Cs
0	(8+9)-VI-3	12	0.01	6.40	Si	>100
0	(8+9)-III-1	69	0.06	6.40	Si	>100
0	(8+9)-IV-3	18	0.02	6.40	Si	>100
0	(8+9)-III-2	46	0.04	6.40	Si	>100
0	(8+9)-VIII-3	38	0.03	6.40	Si	>100
0	(8+9)-III-3	-50	0.04	6.40	Si	>100
0	(8+9)-VIII-1	35	0.03	6.40	Si	>100
0	(8+9)-III-4	-73	0.06	6.40	Si	>100
0	(8+9)-VII-3	15	0.01	6.40	Si	>100
0	(8+9)-IV-1	54	0.05	6.40	Si	>100
0	(8+9)-I-2	54	0.05	6.40	Si	>100
0	(8+9)-IV-2	-22	0.02	6.40	Si	>100
0	(8+9)-I-4	-65	0.06	6.40	Si	>100
0	(8+9)-II-2	3	0.00	6.40	Si	>100
0	(8+9)-IV-4	-58	0.05	6.40	Si	>100
0	(8+9)-II-4	-32	0.03	6.40	Si	>100
0	(8+9)-VI-2	-16	0.01	6.40	Si	>100
0	(8+9)-VIII-4	-38	0.03	6.40	Si	>100
0	(8+9)-VIII-2	-41	0.04	6.40	Si	>100
0	(8+9)-I-1	61	0.05	6.40	Si	>100
0	(8+9)-V-2	-11	0.01	6.40	Si	>100
0	(8+9)-II-1	29	0.02	6.40	Si	>100
0	(8+9)-VII-4	-8	0.01	6.40	Si	>100
0	(8+9)-I-3	-57	0.05	6.40	Si	>100
0	(8+9)-VII-2	-18	0.02	6.40	Si	>100
0	(8+9)-VII-1	5	0.00	6.40	Si	>100
0	(8+9)-VI-4	-13	0.01	6.40	Si	>100
0	(8+9)-VI-1	9	0.01	6.40	Si	>100
2650	(8+9)-V-1	4	0.00	6.40	Si	>100
5300	1	-6	0.01	3.84	Si	>100
5300	2	-13	0.01	5.76	Si	>100
5300	3	-13	0.01	5.76	Si	>100
5300	4	-6	0.01	5.12	Si	>100
5300	5	-6	0.01	5.12	Si	>100
5300	6	-6	0.01	5.12	Si	>100
5300	7	-6	0.01	5.12	Si	>100
5300	(8+9)-V-4	-7	0.01	6.40	Si	>100
5300	(8+9)-II-3	-11	0.01	6.40	Si	>100
5300	(8+9)-V-3	-8	0.01	6.40	Si	>100
Verifiche nella direzione secondaria						
0	(8+9)-II-2	-38	0.01	6.40	Si	>100
0	(8+9)-II-3	41	0.01	6.40	Si	>100
585	1	11	0.00	3.84	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
585	4	11	0.00	5.12	Si	>100
585	5	11	0.00	5.12	Si	>100
585	6	11	0.00	5.12	Si	>100
585	7	11	0.00	5.12	Si	>100
585	(8+9)-V-1	32	0.01	6.40	Si	>100
585	(8+9)-VII-2	37	0.01	6.40	Si	>100
585	(8+9)-VII-4	-19	0.01	6.40	Si	>100
585	(8+9)-V-4	-16	0.01	6.40	Si	>100
585	(8+9)-V-2	40	0.01	6.40	Si	>100
585	(8+9)-VII-1	35	0.01	6.40	Si	>100
1170	2	14	0.00	5.76	Si	>100
1170	3	14	0.00	5.76	Si	>100
1170	(8+9)-VIII-4	-63	0.02	6.40	Si	>100
1170	(8+9)-IV-3	53	0.02	6.40	Si	>100
1170	(8+9)-VI-1	37	0.01	6.40	Si	>100
1170	(8+9)-III-2	74	0.03	6.40	Si	>100
1170	(8+9)-VI-2	-35	0.01	6.40	Si	>100
1170	(8+9)-III-4	-107	0.04	6.40	Si	>100
1170	(8+9)-VI-3	47	0.02	6.40	Si	>100
1170	(8+9)-IV-2	-41	0.01	6.40	Si	>100
1170	(8+9)-VI-4	-25	0.01	6.40	Si	>100
1170	(8+9)-IV-4	-95	0.03	6.40	Si	>100
1170	(8+9)-I-3	-74	0.03	6.40	Si	>100
1170	(8+9)-II-1	69	0.02	6.40	Si	>100
1170	(8+9)-I-2	86	0.03	6.40	Si	>100
1170	(8+9)-I-4	-95	0.03	6.40	Si	>100
1170	(8+9)-VII-3	45	0.02	6.40	Si	>100
1170	(8+9)-IV-1	107	0.04	6.40	Si	>100
1170	(8+9)-I-1	107	0.04	6.40	Si	>100
1170	(8+9)-III-3	-62	0.02	6.40	Si	>100
1170	(8+9)-III-1	119	0.04	6.40	Si	>100
1170	(8+9)-V-3	33	0.01	6.40	Si	>100
1170	(8+9)-VIII-1	75	0.03	6.40	Si	>100
1170	(8+9)-VIII-2	-73	0.03	6.40	Si	>100
1170	(8+9)-VIII-3	85	0.03	6.40	Si	>100
1170	(8+9)-II-4	-57	0.02	6.40	Si	>100

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Tx kg	τ_{vd} kg/cmq	fvd kg/cmq	Csv	τ_M kg/cmq	fTd kg/cmq	Csm	Mecc.	Cs
0	(8+9)-III-2	-3319	-5.86	32.00	5.5	-1.42	20.00	14	V	5.5
0	(8+9)-I-2	-3165	-5.59	32.00	5.7	-1.35	20.00	15	V	5.7
0	(8+9)-VIII-4	-2697	-4.76	32.00	6.7	-1.15	20.00	17	V	6.7
0	(8+9)-V-1	-1701	-3.00	32.00	11	-0.73	20.00	28	V	11
0	(8+9)-VII-2	-2838	-5.01	32.00	6.4	-1.21	20.00	16	V	6.4
0	(8+9)-IV-4	-2553	-4.51	32.00	7.1	-1.09	20.00	18	V	7.1
0	(8+9)-VI-4	-2186	-3.86	32.00	8.3	-0.93	20.00	21	V	8.3
0	(8+9)-IV-2	-3601	-6.36	32.00	5.0	-1.54	20.00	13	V	5.0
0	(8+9)-V-2	-2685	-4.74	32.00	6.7	-1.15	20.00	17	V	6.7
0	(8+9)-II-2	-3090	-5.46	32.00	5.9	-1.32	20.00	15	V	5.9
0	(8+9)-VI-2	-2946	-5.20	32.00	6.2	-1.26	20.00	16	V	6.2
0	(8+9)-I-1	-2181	-3.85	32.00	8.3	-0.93	20.00	21	V	8.3
0	(8+9)-VII-1	-1547	-2.73	32.00	12	-0.66	20.00	30	V	12
0	(8+9)-VIII-2	-3457	-6.11	32.00	5.2	-1.48	20.00	14	V	5.2
0	(8+9)-II-4	-2042	-3.61	32.00	8.9	-0.87	20.00	23	V	8.9
0	(8+9)-III-1	-2027	-3.58	32.00	8.9	-0.87	20.00	23	V	8.9
5300	1	1404	2.48	19.20	7.7	0.60	12.00	20	V	7.7
5300	2	2891	5.11	28.80	5.6	1.24	18.00	15	V	5.6
5300	3	2891	5.11	28.80	5.6	1.24	18.00	15	V	5.6
5300	4	1404	2.48	25.60	10	0.60	16.00	27	V	10
5300	5	1404	2.48	25.60	10	0.60	16.00	27	V	10
5300	6	1404	2.48	25.60	10	0.60	16.00	27	V	10
5300	7	1404	2.48	25.60	10	0.60	16.00	27	V	10

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
5300	(8+9)-IV-1	2820	4.98	32.00	6.4	1.21	20.00	17	V	6.4
5300	(8+9)-III-3	3337	5.89	32.00	5.4	1.43	20.00	14	V	5.4
5300	(8+9)-II-1	2619	4.63	32.00	6.9	1.12	20.00	18	V	6.9
5300	(8+9)-I-3	3276	5.79	32.00	5.5	1.40	20.00	14	V	5.5
5300	(8+9)-II-3	3616	6.39	32.00	5.0	1.55	20.00	13	V	5.0
5300	(8+9)-V-4	2029	3.58	32.00	8.9	0.87	20.00	23	V	8.9
5300	(8+9)-VII-3	3377	5.96	32.00	5.4	1.44	20.00	14	V	5.4
5300	(8+9)-I-4	1989	3.51	32.00	9.1	0.85	20.00	24	V	9.1
5300	(8+9)-VII-4	1968	3.48	32.00	9.2	0.84	20.00	24	V	9.2
5300	(8+9)-VI-1	2607	4.60	32.00	7.0	1.11	20.00	18	V	7.0
5300	(8+9)-VI-3	3628	6.41	32.00	5.0	1.55	20.00	13	V	5.0
5300	(8+9)-V-3	3316	5.86	32.00	5.5	1.42	20.00	14	V	5.5
5300	(8+9)-VIII-1	2808	4.96	32.00	6.5	1.20	20.00	17	V	6.5
5300	(8+9)-III-4	1928	3.41	32.00	9.4	0.82	20.00	24	V	9.4
5300	(8+9)-VIII-3	3829	6.76	32.00	4.7	1.64	20.00	12	V	4.7
5300	(8+9)-IV-3	3817	6.74	32.00	4.7	1.63	20.00	12	V	4.7
Verifiche nella direzione secondaria										
1170	1	214	0.08	19.20	>100	0.02	12.00	>100	V	>100
1170	2	324	0.13	28.80	>100	0.03	18.00	>100	V	>100
1170	3	324	0.13	28.80	>100	0.03	18.00	>100	V	>100
1170	4	214	0.08	25.60	>100	0.02	16.00	>100	V	>100
1170	5	214	0.08	25.60	>100	0.02	16.00	>100	V	>100
1170	6	214	0.08	25.60	>100	0.02	16.00	>100	V	>100
1170	7	214	0.08	25.60	>100	0.02	16.00	>100	V	>100
1170	(8+9)-VIII-4	12146	4.73	32.00	6.8	1.15	20.00	17	V	6.8
1170	(8+9)-IV-2	19025	7.42	32.00	4.3	1.79	20.00	11	V	4.3
1170	(8+9)-V-1	7684	3.00	32.00	11	0.72	20.00	28	V	11
1170	(8+9)-I-2	15540	6.06	32.00	5.3	1.47	20.00	14	V	5.3
1170	(8+9)-V-2	15996	6.24	32.00	5.1	1.51	20.00	13	V	5.1
1170	(8+9)-I-4	-6935	-2.70	32.00	12	-0.65	20.00	31	V	12
1170	(8+9)-V-3	-15704	-6.12	32.00	5.2	-1.48	20.00	13	V	5.2
1170	(8+9)-II-2	17372	6.77	32.00	4.7	1.64	20.00	12	V	4.7
1170	(8+9)-V-4	-7392	-2.88	32.00	11	-0.70	20.00	29	V	11
1170	(8+9)-II-4	10629	4.14	32.00	7.7	1.00	20.00	20	V	7.7
1170	(8+9)-VI-1	-10200	-3.98	32.00	8.0	-0.96	20.00	21	V	8.0
1170	(8+9)-III-2	16036	6.25	32.00	5.1	1.51	20.00	13	V	5.1
1170	(8+9)-VI-2	17508	6.83	32.00	4.7	1.65	20.00	12	V	4.7
1170	(8+9)-III-4	-6439	-2.51	32.00	13	-0.61	20.00	33	V	13
1170	(8+9)-VI-3	-17216	-6.71	32.00	4.8	-1.62	20.00	12	V	4.8
1170	(8+9)-I-1	7228	2.82	32.00	11	0.68	20.00	29	V	11
1170	(8+9)-VI-4	10492	4.09	32.00	7.8	0.99	20.00	20	V	7.8
1170	(8+9)-IV-4	12283	4.79	32.00	6.7	1.16	20.00	17	V	6.7
1170	(8+9)-VII-1	7188	2.80	32.00	11	0.68	20.00	29	V	11
1170	(8+9)-II-1	-10337	-4.03	32.00	7.9	-0.98	20.00	21	V	7.9
1170	(8+9)-VII-2	16493	6.43	32.00	5.0	1.56	20.00	13	V	5.0
1170	(8+9)-III-1	6731	2.62	32.00	12	0.64	20.00	31	V	12
1170	(8+9)-VII-3	-16200	-6.32	32.00	5.1	-1.53	20.00	13	V	5.1
1170	(8+9)-IV-1	-11990	-4.67	32.00	6.8	-1.13	20.00	18	V	6.8
1170	(8+9)-VII-4	-6895	-2.69	32.00	12	-0.65	20.00	31	V	12
1170	(8+9)-III-3	-15744	-6.14	32.00	5.2	-1.49	20.00	13	V	5.2
1170	(8+9)-IV-3	-18733	-7.30	32.00	4.4	-1.77	20.00	11	V	4.4
1170	(8+9)-II-3	-17079	-6.66	32.00	4.8	-1.61	20.00	12	V	4.8
1170	(8+9)-VIII-1	-11854	-4.62	32.00	6.9	-1.12	20.00	18	V	6.9
1170	(8+9)-VIII-2	19162	7.47	32.00	4.3	1.81	20.00	11	V	4.3
1170	(8+9)-VIII-3	-18870	-7.36	32.00	4.4	-1.78	20.00	11	V	4.4
1170	(8+9)-I-3	-15248	-5.94	32.00	5.4	-1.44	20.00	14	V	5.4

Verifiche a instabilità

Setto(X)	Comb.	k _{critc}	k _{critm}	λ_{relc}	λ_{relm}	σ_n	σ_{mx}	σ_{my}	f _{td}	f _{cd}	f _{md}	Cs
(cm)						kg/cm ² q	kg/cm ² q	kg/cm ² q	kg/cm ² q	kg/cm ² q	kg/cm ² q	
17(20.	(8+9)-IV-3	1.00	--	0.15	--	-0.66	-0.19	9.27	132.00	192.00	192.00	19

Setto(X)	Comb.	k _{critc}	k _{critm}	λ_{relc}	λ_{relm}	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0)												
18(22.7)	(8+9)-IV-2	1.00	--	0.16	--	-2.69	-3.14	9.36	132.00	192.00	192.00	13
19(530.0)	(8+9)-IV-2	0.26	--	1.92	--	-10.08	-0.23	24.68	132.00	192.00	192.00	3.0
20(0.0)	(8+9)-IV-3	--	--	--	--	11.02	5.70	13.55	132.00	192.00	192.00	5.4

Parete Xlam 5 - Nodi: [7-15-107-7-6-5-4-3-2-1-106] - **Crit.Prog.** Criterio di verifica XLAM 0 - **Verificato:** [Cs=1.372,Comb=(8+9)-VII-1]

Geometria setti

Setto	Crit.	X mm	L cm	S cm	X90 mm	L90 cm	S90 cm
21	Criterio di verifica XLAM 0	0	387.0	12.1	0	200.0	12.1
		1000	387.0	12.1	1935	200.0	12.1
		2000	387.0	12.1	3870	200.0	12.1
22	Criterio di verifica XLAM 0	0	387.0	12.1	0	250.0	12.1
		1250	387.0	12.1	1935	250.0	12.1
		2500	387.0	12.1	3870	250.0	12.1
23	Criterio di verifica XLAM 0	0	387.0	12.1	0	145.9	12.1
		730	387.0	12.1	1935	145.9	12.1
		1459	387.0	12.1	3870	145.9	12.1
24	Criterio di verifica XLAM 0	0	50.0	12.1	0	350.0	12.1
		1750	50.0	12.1	250	350.0	12.1
		3500	50.0	12.1	500	350.0	12.1
25	Criterio di verifica XLAM 0	0	117.0	12.1	0	350.0	12.1
		1750	117.0	12.1	585	350.0	12.1
		3500	117.0	12.1	1170	350.0	12.1
26	Criterio di verifica XLAM 0	0	50.0	12.1	0	350.0	12.1
		1750	50.0	12.1	250	350.0	12.1
		3500	50.0	12.1	500	350.0	12.1
27	Criterio di verifica XLAM 0	0	117.0	12.1	0	350.0	12.1
		1750	117.0	12.1	585	350.0	12.1
		3500	117.0	12.1	1170	350.0	12.1

Setto 21: origine (48.0,2013.0,193.5), direzione (0.825704,0.564103,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X mm	Comb.	N kg	M _x kg*m	M _y kg*m	σ_n kg/cm ²	σ_{mx} kg/cm ²	σ_{my} kg/cm ²	ftd kg/cm ²	fcd kg/cm ²	fmd kg/cm ²	Cs
2000	1	-499	2	1101	-0.18	0.03	0.61	79.20	115.20	115.20	>100
2000	2	-1042	4	2239	-0.37	0.06	1.24	118.80	172.80	172.80	>100
2000	3	-1042	4	2239	-0.37	0.06	1.24	118.80	172.80	172.80	>100
2000	4	-499	2	1101	-0.18	0.03	0.61	105.60	153.60	153.60	>100
2000	5	-499	2	1101	-0.18	0.03	0.61	105.60	153.60	153.60	>100
2000	6	-499	2	1101	-0.18	0.03	0.61	105.60	153.60	153.60	>100
2000	7	-499	2	1101	-0.18	0.03	0.61	105.60	153.60	153.60	>100
2000	(8+9)-VIII-4	-2601	-6	11747	-0.93	-0.08	6.48	132.00	192.00	192.00	29
2000	(8+9)-IV-1	1704	9	-9236	0.61	0.13	-5.10	132.00	192.00	192.00	31
2000	(8+9)-V-1	2142	-3	-11516	0.76	-0.04	-6.35	132.00	192.00	192.00	26
2000	(8+9)-I-2	797	-6	-4182	0.28	-0.08	-2.31	132.00	192.00	192.00	68
2000	(8+9)-V-2	1493	-8	-7466	0.53	-0.11	-4.12	132.00	192.00	192.00	38
2000	(8+9)-I-4	-2134	4	9758	-0.76	0.06	5.38	132.00	192.00	192.00	35
2000	(8+9)-V-3	-2181	11	8992	-0.78	0.14	4.96	132.00	192.00	192.00	38
2000	(8+9)-II-2	-986	-8	5422	-0.35	-0.11	2.99	132.00	192.00	192.00	62
2000	(8+9)-V-4	-2830	6	13042	-1.01	0.08	7.20	132.00	192.00	192.00	26
2000	(8+9)-II-4	-1865	-5	9604	-0.66	-0.07	5.30	132.00	192.00	192.00	36
2000	(8+9)-VI-1	1386	7	-9063	0.49	0.10	-5.00	132.00	192.00	192.00	33
2000	(8+9)-III-2	639	-7	-3834	0.23	-0.09	-2.12	132.00	192.00	192.00	76
2000	(8+9)-VI-2	-777	-9	4436	-0.28	-0.12	2.45	132.00	192.00	192.00	75
2000	(8+9)-III-4	-2292	4	10105	-0.82	0.05	5.58	132.00	192.00	192.00	34
2000	(8+9)-VI-3	89	12	-2911	0.03	0.15	-1.61	132.00	192.00	192.00	>100

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
2000	(8+9)-IV-2	-1513	-10	6580	-0.54	-0.13	3.63	132.00	192.00	192.00	51
2000	(8+9)-VI-4	-2074	-5	10589	-0.74	-0.06	5.84	132.00	192.00	192.00	32
2000	(8+9)-IV-4	-2392	-7	10762	-0.85	-0.09	5.94	132.00	192.00	192.00	32
2000	(8+9)-VII-1	2300	-3	-11864	0.82	-0.04	-6.55	132.00	192.00	192.00	25
2000	(8+9)-II-1	1177	8	-8078	0.42	0.11	-4.46	132.00	192.00	192.00	37
2000	(8+9)-VII-2	1335	-8	-7119	0.48	-0.11	-3.93	132.00	192.00	192.00	41
2000	(8+9)-III-1	1604	-1	-8579	0.57	-0.01	-4.73	132.00	192.00	192.00	34
2000	(8+9)-VII-3	-2023	11	8645	-0.72	0.15	4.77	132.00	192.00	192.00	39
2000	(8+9)-I-1	1446	-1	-8232	0.51	-0.02	-4.54	132.00	192.00	192.00	36
2000	(8+9)-VII-4	-2989	5	13390	-1.06	0.07	7.39	132.00	192.00	192.00	26
2000	(8+9)-III-3	-1327	9	5360	-0.47	0.13	2.96	132.00	192.00	192.00	62
2000	(8+9)-IV-3	825	13	-5054	0.29	0.17	-2.79	132.00	192.00	192.00	57
2000	(8+9)-II-3	298	11	-3896	0.11	0.15	-2.15	132.00	192.00	192.00	78
2000	(8+9)-VIII-1	1913	9	-10221	0.68	0.12	-5.64	132.00	192.00	192.00	28
2000	(8+9)-VIII-2	-1304	-10	5595	-0.46	-0.14	3.09	132.00	192.00	192.00	59
2000	(8+9)-VIII-3	616	13	-4069	0.22	0.18	-2.25	132.00	192.00	192.00	70
2000	(8+9)-I-3	-1485	9	5708	-0.53	0.12	3.15	132.00	192.00	192.00	59
Verifiche nella direzione secondaria											
0	(8+9)-VIII-4	4225	39	-3297	4.36	2.31	-10.22	132.00	192.00	192.00	10
0	(8+9)-VII-2	-5454	55	8405	-5.63	3.27	26.05	132.00	192.00	192.00	6.5
0	(8+9)-III-3	-6380	-76	-3446	-6.59	-4.48	-10.68	132.00	192.00	192.00	12
0	(8+9)-IV-2	2949	70	677	3.05	4.17	2.10	132.00	192.00	192.00	18
0	(8+9)-III-4	-1202	-49	-4842	-1.24	-2.91	-15.01	132.00	192.00	192.00	11
0	(8+9)-VIII-2	2546	61	1352	2.63	3.60	4.19	132.00	192.00	192.00	17
0	(8+9)-IV-1	-14312	-18	5331	-14.78	-1.06	16.52	132.00	192.00	192.00	10
0	(8+9)-VII-4	142	-17	-7093	0.15	-1.02	-21.98	132.00	192.00	192.00	8.3
0	(8+9)-I-1	-9066	36	7292	-9.37	2.12	22.60	132.00	192.00	192.00	7.6
0	(8+9)-IV-3	-13439	-59	2032	-13.88	-3.48	6.30	132.00	192.00	192.00	18
0	(8+9)-I-3	-6158	-101	-3705	-6.36	-5.95	-11.48	132.00	192.00	192.00	11
0	(8+9)-IV-4	3822	30	-2622	3.95	1.75	-8.13	132.00	192.00	192.00	12
0	(8+9)-II-1	-13571	-101	4469	-14.02	-5.96	13.85	132.00	192.00	192.00	9.2
0	(8+9)-V-1	-10410	4	9543	-10.75	0.23	29.57	132.00	192.00	192.00	6.3
0	(8+9)-II-3	-12698	-142	1170	-13.12	-8.38	3.62	132.00	192.00	192.00	15
0	(8+9)-V-2	-5676	80	8664	-5.86	4.74	26.85	132.00	192.00	192.00	6.0
0	(8+9)-III-1	-9288	61	7551	-9.60	3.59	23.40	132.00	192.00	192.00	7.0
0	(8+9)-V-3	-4814	-69	-5955	-4.97	-4.06	-18.46	132.00	192.00	192.00	8.5
0	(8+9)-VIII-3	-13036	-49	1357	-13.47	-2.92	4.21	132.00	192.00	192.00	24
0	(8+9)-V-4	-80	8	-6834	-0.08	0.45	-21.18	132.00	192.00	192.00	8.9
0	(8+9)-VII-3	-5036	-44	-5696	-5.20	-2.59	-17.65	132.00	192.00	192.00	9.4
0	(8+9)-VI-1	-13974	-110	5144	-14.44	-6.53	15.94	132.00	192.00	192.00	8.2
0	(8+9)-I-4	-1424	-24	-4583	-1.47	-1.44	-14.20	132.00	192.00	192.00	12
0	(8+9)-VI-2	1805	144	2214	1.86	8.49	6.86	132.00	192.00	192.00	11
0	(8+9)-II-4	3081	112	-1760	3.18	6.64	-5.45	132.00	192.00	192.00	11
0	(8+9)-VIII-1	-14715	-28	6006	-15.20	-1.63	18.61	132.00	192.00	192.00	9.0
0	(8+9)-I-2	-4332	112	6413	-4.48	6.63	19.88	132.00	192.00	192.00	7.2
0	(8+9)-II-2	2208	153	1539	2.28	9.06	4.77	132.00	192.00	192.00	11
0	(8+9)-III-2	-4110	87	6155	-4.25	5.16	19.07	132.00	192.00	192.00	7.9
0	(8+9)-VI-3	-12295	-132	494	-12.70	-7.81	1.53	132.00	192.00	192.00	19
0	(8+9)-VI-4	3484	122	-2435	3.60	7.21	-7.55	132.00	192.00	192.00	9.6
0	(8+9)-VII-1	-10632	29	9801	-10.98	1.70	30.38	132.00	192.00	192.00	5.9
1935	1	-7954	8	2670	-8.22	0.46	8.27	79.20	115.20	115.20	12
1935	2	-16256	16	5442	-16.79	0.92	16.86	118.80	172.80	172.80	8.9
1935	3	-16256	16	5442	-16.79	0.92	16.86	118.80	172.80	172.80	8.9
1935	4	-7954	8	2670	-8.22	0.46	8.27	105.60	153.60	153.60	17
1935	5	-7954	8	2670	-8.22	0.46	8.27	105.60	153.60	153.60	17
1935	6	-7954	8	2670	-8.22	0.46	8.27	105.60	153.60	153.60	17
1935	7	-7954	8	2670	-8.22	0.46	8.27	105.60	153.60	153.60	17

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
0	(8+9)-V-4	55	0.01	6.40	Si	>100
0	(8+9)-II-3	-44	0.01	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
0	(8+9)-V-2	-38	0.01	6.40	Si	>100
0	(8+9)-VI-1	-31	0.01	6.40	Si	>100
0	(8+9)-VIII-2	-16	0.00	6.40	Si	>100
0	(8+9)-III-1	92	0.02	6.40	Si	>100
0	(8+9)-VII-3	50	0.01	6.40	Si	>100
0	(8+9)-III-2	89	0.02	6.40	Si	>100
0	(8+9)-VII-1	-43	0.01	6.40	Si	>100
0	(8+9)-III-3	-84	0.02	6.40	Si	>100
0	(8+9)-I-2	96	0.02	6.40	Si	>100
0	(8+9)-III-4	-87	0.02	6.40	Si	>100
0	(8+9)-I-4	-79	0.02	6.40	Si	>100
0	(8+9)-IV-1	33	0.01	6.40	Si	>100
0	(8+9)-II-2	49	0.01	6.40	Si	>100
0	(8+9)-IV-2	24	0.01	6.40	Si	>100
0	(8+9)-VII-4	48	0.01	6.40	Si	>100
0	(8+9)-IV-3	-20	0.01	6.40	Si	>100
0	(8+9)-I-1	84	0.02	6.40	Si	>100
0	(8+9)-IV-4	-28	0.01	6.40	Si	>100
0	(8+9)-VII-2	-46	0.01	6.40	Si	>100
0	(8+9)-I-3	-91	0.02	6.40	Si	>100
0	(8+9)-VIII-3	21	0.01	6.40	Si	>100
0	(8+9)-V-1	-50	0.01	6.40	Si	>100
0	(8+9)-VI-4	36	0.01	6.40	Si	>100
0	(8+9)-V-3	43	0.01	6.40	Si	>100
1000	1	5	0.00	3.84	Si	>100
1000	2	11	0.00	5.76	Si	>100
1000	3	11	0.00	5.76	Si	>100
1000	4	5	0.00	5.12	Si	>100
1000	5	5	0.00	5.12	Si	>100
1000	6	5	0.00	5.12	Si	>100
1000	7	5	0.00	5.12	Si	>100
1000	(8+9)-II-4	22	0.01	6.40	Si	>100
1000	(8+9)-II-1	-15	0.00	6.40	Si	>100
1000	(8+9)-VIII-1	-8	0.00	6.40	Si	>100
1000	(8+9)-VI-3	-7	0.00	6.40	Si	>100
1000	(8+9)-VI-2	14	0.00	6.40	Si	>100
1000	(8+9)-VIII-4	15	0.00	6.40	Si	>100
Verifiche nella direzione secondaria						
0	(8+9)-II-4	31	0.03	6.40	Si	>100
0	(8+9)-VII-3	36	0.03	6.40	Si	>100
0	(8+9)-VII-2	-41	0.04	6.40	Si	>100
0	(8+9)-VI-4	36	0.03	6.40	Si	>100
0	(8+9)-VI-3	-19	0.02	6.40	Si	>100
0	(8+9)-VI-1	-42	0.04	6.40	Si	>100
0	(8+9)-V-2	-32	0.03	6.40	Si	>100
0	(8+9)-V-1	-49	0.05	6.40	Si	>100
1935	(8+9)-VIII-4	-79	0.08	6.40	Si	85
1935	(8+9)-V-3	-32	0.03	6.40	Si	>100
1935	(8+9)-VII-1	46	0.04	6.40	Si	>100
1935	(8+9)-VIII-2	-60	0.06	6.40	Si	>100
1935	(8+9)-VIII-1	68	0.07	6.40	Si	98
1935	(8+9)-VII-4	-57	0.05	6.40	Si	>100
1935	(8+9)-IV-4	-74	0.07	6.40	Si	91
1935	(8+9)-V-4	-44	0.04	6.40	Si	>100
1935	(8+9)-VIII-3	49	0.05	6.40	Si	>100
1935	(8+9)-IV-1	63	0.06	6.40	Si	>100
3870	1	11	0.01	3.84	Si	>100
3870	2	23	0.02	5.76	Si	>100
3870	3	23	0.02	5.76	Si	>100
3870	4	11	0.01	5.12	Si	>100
3870	5	11	0.01	5.12	Si	>100
3870	6	11	0.01	5.12	Si	>100
3870	7	11	0.01	5.12	Si	>100
3870	(8+9)-I-3	-154	0.15	6.40	Si	44

X	Comb.	Ty	τ_d	fvd	RS	Cs
3870	(8+9)-III-1	159	0.15	6.40	Si	42
3870	(8+9)-I-1	161	0.15	6.40	Si	42
3870	(8+9)-I-2	169	0.16	6.40	Si	40
3870	(8+9)-IV-2	74	0.07	6.40	Si	91
3870	(8+9)-II-3	-53	0.05	6.40	Si	>100
3870	(8+9)-III-2	171	0.16	6.40	Si	39
3870	(8+9)-IV-3	-58	0.06	6.40	Si	>100
3870	(8+9)-VI-2	23	0.02	6.40	Si	>100
3870	(8+9)-III-3	-155	0.15	6.40	Si	43
3870	(8+9)-II-2	69	0.07	6.40	Si	98
3870	(8+9)-II-1	41	0.04	6.40	Si	>100
3870	(8+9)-I-4	-145	0.14	6.40	Si	46
3870	(8+9)-III-4	-144	0.14	6.40	Si	47

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
1000	(8+9)-VIII-4	-10258	-5.48	32.00	5.8	-1.33	20.00	15	V	5.8
1000	(8+9)-IV-1	9637	5.14	32.00	6.2	1.25	20.00	16	V	6.2
1000	(8+9)-IV-4	-9398	-5.02	32.00	6.4	-1.21	20.00	16	V	6.4
1000	(8+9)-VI-3	-2126	-1.13	32.00	28	-0.27	20.00	73	V	28
1000	(8+9)-V-3	-8886	-4.74	32.00	6.7	-1.15	20.00	17	V	6.7
1000	(8+9)-VIII-1	10497	5.60	32.00	5.7	1.36	20.00	15	V	5.7
1000	(8+9)-V-2	9125	4.87	32.00	6.6	1.18	20.00	17	V	6.6
1000	(8+9)-VII-3	-6747	-3.60	32.00	8.9	-0.87	20.00	23	V	8.9
1000	(8+9)-III-1	8696	4.64	32.00	6.9	1.12	20.00	18	V	6.9
1000	(8+9)-I-2	6257	3.34	32.00	9.6	0.81	20.00	25	V	9.6
1000	(8+9)-III-2	4118	2.20	32.00	15	0.53	20.00	38	V	15
1000	(8+9)-VII-2	6986	3.73	32.00	8.6	0.90	20.00	22	V	8.6
1000	(8+9)-V-1	9425	5.03	32.00	6.4	1.22	20.00	16	V	6.4
1000	(8+9)-VIII-3	5004	2.67	32.00	12	0.65	20.00	31	V	12
1000	(8+9)-III-4	-8457	-4.52	32.00	7.1	-1.09	20.00	18	V	7.1
1000	(8+9)-I-1	6557	3.50	32.00	9.1	0.85	20.00	24	V	9.1
1000	(8+9)-VII-1	11564	6.17	32.00	5.2	1.49	20.00	13	V	5.2
1000	(8+9)-VII-4	-11325	-6.05	32.00	5.3	-1.46	20.00	14	V	5.3
1000	(8+9)-I-3	-6018	-3.21	32.00	10.0	-0.78	20.00	26	V	10.0
1000	(8+9)-IV-3	5864	3.13	32.00	10	0.76	20.00	26	V	10
2000	1	-2565	-1.37	19.20	14	-0.33	12.00	36	V	14
2000	2	-5339	-2.85	28.80	10	-0.69	18.00	26	V	10
2000	3	-5339	-2.85	28.80	10	-0.69	18.00	26	V	10
2000	4	-2565	-1.37	25.60	19	-0.33	16.00	48	V	19
2000	5	-2565	-1.37	25.60	19	-0.33	16.00	48	V	19
2000	6	-2565	-1.37	25.60	19	-0.33	16.00	48	V	19
2000	7	-2565	-1.37	25.60	19	-0.33	16.00	48	V	19
2000	(8+9)-IV-2	-5838	-3.12	32.00	10	-0.75	20.00	27	V	10
2000	(8+9)-II-1	4621	2.47	32.00	13	0.60	20.00	34	V	13
2000	(8+9)-III-3	-4309	-2.30	32.00	14	-0.56	20.00	36	V	14
2000	(8+9)-V-4	-9454	-5.05	32.00	6.3	-1.22	20.00	16	V	6.3
2000	(8+9)-VI-2	-5072	-2.71	32.00	12	-0.66	20.00	31	V	12
2000	(8+9)-I-4	-7447	-3.98	32.00	8.0	-0.96	20.00	21	V	8.0
2000	(8+9)-VI-1	5223	2.79	32.00	11	0.67	20.00	30	V	11
2000	(8+9)-VI-4	-8758	-4.68	32.00	6.8	-1.13	20.00	18	V	6.8
2000	(8+9)-II-3	2140	1.14	32.00	28	0.28	20.00	72	V	28
2000	(8+9)-VIII-2	-5236	-2.80	32.00	11	-0.68	20.00	30	V	11
2000	(8+9)-II-4	-8155	-4.35	32.00	7.3	-1.05	20.00	19	V	7.3
2000	(8+9)-II-2	-5675	-3.03	32.00	11	-0.73	20.00	27	V	11
Verifiche nella direzione secondaria										
1935	(8+9)-VIII-4	-7294	-7.54	32.00	4.2	-1.82	20.00	11	V	4.2
1935	(8+9)-VII-2	3997	4.13	32.00	7.7	1.00	20.00	20	V	7.7
1935	(8+9)-III-3	-2869	-2.96	32.00	11	-0.72	20.00	28	V	11
1935	(8+9)-IV-2	-4342	-4.49	32.00	7.1	-1.09	20.00	18	V	7.1
1935	(8+9)-III-4	-5844	-6.04	32.00	5.3	-1.46	20.00	14	V	5.3
1935	(8+9)-VIII-2	-3685	-3.81	32.00	8.4	-0.92	20.00	22	V	8.4

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
1935	(8+9)-IV-1	5574	5.76	32.00	5.6	1.39	20.00	14	V	5.6
1935	(8+9)-VII-4	-8035	-8.30	32.00	3.9	-2.01	20.00	10.0	V	3.9
1935	(8+9)-I-1	4607	4.76	32.00	6.7	1.15	20.00	17	V	6.7
1935	(8+9)-IV-3	3279	3.39	32.00	9.4	0.82	20.00	24	V	9.4
1935	(8+9)-I-3	-3042	-3.14	32.00	10	-0.76	20.00	26	V	10
1935	(8+9)-IV-4	-6637	-6.86	32.00	4.7	-1.66	20.00	12	V	4.7
1935	(8+9)-II-1	4997	5.16	32.00	6.2	1.25	20.00	16	V	6.2
1935	(8+9)-V-1	6799	7.02	32.00	4.6	1.70	20.00	12	V	4.6
1935	(8+9)-II-3	2702	2.79	32.00	11	0.68	20.00	30	V	11
1935	(8+9)-V-2	4170	4.31	32.00	7.4	1.04	20.00	19	V	7.4
1935	(8+9)-III-1	4781	4.94	32.00	6.5	1.20	20.00	17	V	6.5
1935	(8+9)-V-3	-5233	-5.41	32.00	5.9	-1.31	20.00	15	V	5.9
1935	(8+9)-VIII-3	2622	2.71	32.00	12	0.66	20.00	31	V	12
1935	(8+9)-V-4	-7862	-8.12	32.00	3.9	-1.97	20.00	10	V	3.9
1935	(8+9)-VII-3	-5060	-5.23	32.00	6.1	-1.27	20.00	16	V	6.1
1935	(8+9)-VI-1	5654	5.84	32.00	5.5	1.41	20.00	14	V	5.5
1935	(8+9)-I-4	-5670	-5.86	32.00	5.5	-1.42	20.00	14	V	5.5
1935	(8+9)-VI-2	-3108	-3.21	32.00	10.0	-0.78	20.00	26	V	10.0
1935	(8+9)-II-4	-6060	-6.26	32.00	5.1	-1.51	20.00	13	V	5.1
1935	(8+9)-VIII-1	6231	6.44	32.00	5.0	1.56	20.00	13	V	5.0
1935	(8+9)-I-2	1979	2.04	32.00	16	0.49	20.00	40	V	16
1935	(8+9)-II-2	-3765	-3.89	32.00	8.2	-0.94	20.00	21	V	8.2
1935	(8+9)-III-2	1806	1.87	32.00	17	0.45	20.00	44	V	17
1935	(8+9)-VI-3	2045	2.11	32.00	15	0.51	20.00	39	V	15
1935	(8+9)-VI-4	-6717	-6.94	32.00	4.6	-1.68	20.00	12	V	4.6
1935	(8+9)-VII-1	6972	7.20	32.00	4.4	1.74	20.00	11	V	4.4
3870	1	-1599	-1.65	19.20	12	-0.40	12.00	30	V	12
3870	2	-3322	-3.43	28.80	8.4	-0.83	18.00	22	V	8.4
3870	3	-3322	-3.43	28.80	8.4	-0.83	18.00	22	V	8.4
3870	4	-1599	-1.65	25.60	15	-0.40	16.00	40	V	15
3870	5	-1599	-1.65	25.60	15	-0.40	16.00	40	V	15
3870	6	-1599	-1.65	25.60	15	-0.40	16.00	40	V	15
3870	7	-1599	-1.65	25.60	15	-0.40	16.00	40	V	15

Setto 22: origine (502.1,2323.3,193.5), direzione (0.825704,0.564103,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	(8+9)-IV-3	-1015	0	3374	-0.36	0.01	1.86	132.00	192.00	192.00	>100
0	(8+9)-VIII-3	-925	1	2759	-0.33	0.01	1.52	132.00	192.00	192.00	>100
0	(8+9)-VI-4	853	-15	-7367	0.30	-0.21	-4.07	132.00	192.00	192.00	41
0	(8+9)-II-4	762	-16	-6752	0.27	-0.21	-3.73	132.00	192.00	192.00	44
0	(8+9)-V-1	-1513	-3	7298	-0.54	-0.04	4.03	132.00	192.00	192.00	47
0	(8+9)-V-4	590	-3	-8083	0.21	-0.04	-4.46	132.00	192.00	192.00	40
0	(8+9)-VI-1	-1776	10	6582	-0.63	0.13	3.63	132.00	192.00	192.00	51
0	(8+9)-I-1	-1212	-2	5248	-0.43	-0.03	2.90	132.00	192.00	192.00	66
0	(8+9)-I-4	289	-4	-6033	0.10	-0.05	-3.33	132.00	192.00	192.00	54
2500	1	-1850	0	1508	-0.66	0.01	0.83	79.20	115.20	115.20	>100
2500	2	-3789	1	3061	-1.35	0.01	1.69	118.80	172.80	172.80	>100
2500	3	-3789	1	3061	-1.35	0.01	1.69	118.80	172.80	172.80	>100
2500	4	-1850	0	1508	-0.66	0.01	0.83	105.60	153.60	153.60	>100
2500	5	-1850	0	1508	-0.66	0.01	0.83	105.60	153.60	153.60	>100
2500	6	-1850	0	1508	-0.66	0.01	0.83	105.60	153.60	153.60	>100
2500	7	-1850	0	1508	-0.66	0.01	0.83	105.60	153.60	153.60	>100
2500	(8+9)-VIII-4	-3022	-5	9492	-1.08	-0.06	5.24	132.00	192.00	192.00	36
2500	(8+9)-IV-1	304	6	-6555	0.11	0.07	-3.62	132.00	192.00	192.00	50
2500	(8+9)-VI-2	344	-7	-9278	0.12	-0.09	-5.12	132.00	192.00	192.00	36
2500	(8+9)-III-3	-1845	5	4908	-0.66	0.07	2.71	132.00	192.00	192.00	69
2500	(8+9)-VI-3	-2902	7	11369	-1.03	0.10	6.27	132.00	192.00	192.00	30
2500	(8+9)-III-2	-714	-5	-2817	-0.25	-0.06	-1.55	132.00	192.00	192.00	>100
2500	(8+9)-I-3	-2588	5	9017	-0.92	0.07	4.98	132.00	192.00	192.00	38
2500	(8+9)-III-1	65	-1	-6363	0.02	-0.01	-3.51	132.00	192.00	192.00	54
2500	(8+9)-VII-1	593	-3	-9183	0.21	-0.04	-5.07	132.00	192.00	192.00	35

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
2500	(8+9)-II-3	-2744	7	10523	-0.98	0.09	5.81	132.00	192.00	192.00	33
2500	(8+9)-VII-2	-185	-6	-5637	-0.07	-0.09	-3.11	132.00	192.00	192.00	60
2500	(8+9)-V-3	-3116	7	11837	-1.11	0.09	6.53	132.00	192.00	192.00	29
2500	(8+9)-VII-3	-2374	7	7727	-0.84	0.09	4.26	132.00	192.00	192.00	44
2500	(8+9)-II-1	-2171	5	7142	-0.77	0.07	3.94	132.00	192.00	192.00	48
2500	(8+9)-VII-4	-3152	3	11273	-1.12	0.04	6.22	132.00	192.00	192.00	31
2500	(8+9)-V-2	557	-6	-9746	0.20	-0.08	-5.38	132.00	192.00	192.00	33
2500	(8+9)-II-2	185	-6	-8432	0.07	-0.09	-4.65	132.00	192.00	192.00	40
2500	(8+9)-III-4	-2624	2	8454	-0.93	0.02	4.66	132.00	192.00	192.00	41
2500	(8+9)-IV-4	-2863	-5	8646	-1.02	-0.07	4.77	132.00	192.00	192.00	40
2500	(8+9)-VIII-1	463	5	-7401	0.16	0.07	-4.08	132.00	192.00	192.00	44
2500	(8+9)-VIII-2	-2132	-7	4419	-0.76	-0.10	2.44	132.00	192.00	192.00	76
2500	(8+9)-I-2	29	-5	-6926	0.01	-0.06	-3.82	132.00	192.00	192.00	49
2500	(8+9)-IV-2	-2290	-7	5265	-0.82	-0.09	2.91	132.00	192.00	192.00	64
Verifiche nella direzione secondaria											
0	1	-13116	19	27	-10.84	0.90	0.05	79.20	115.20	115.20	58
0	2	-26555	37	150	-21.95	1.77	0.30	118.80	172.80	172.80	36
0	3	-26555	37	150	-21.95	1.77	0.30	118.80	172.80	172.80	36
0	4	-13116	19	27	-10.84	0.90	0.05	105.60	153.60	153.60	89
0	5	-13116	19	27	-10.84	0.90	0.05	105.60	153.60	153.60	89
0	6	-13116	19	27	-10.84	0.90	0.05	105.60	153.60	153.60	89
0	7	-13116	19	27	-10.84	0.90	0.05	105.60	153.60	153.60	89
0	(8+9)-VIII-4	-8895	17	-17885	-7.35	0.78	-35.47	132.00	192.00	192.00	5.3
0	(8+9)-IV-2	-8856	36	-9373	-7.32	1.72	-18.59	132.00	192.00	192.00	9.3
0	(8+9)-V-1	-10992	-133	18667	-9.08	-6.29	37.03	132.00	192.00	192.00	4.4
0	(8+9)-I-2	-7073	226	9728	-5.85	10.67	19.29	132.00	192.00	192.00	6.4
0	(8+9)-V-2	-7016	245	15035	-5.80	11.61	29.82	132.00	192.00	192.00	4.6
0	(8+9)-I-4	-7143	180	-13337	-5.90	8.49	-26.45	132.00	192.00	192.00	5.5
0	(8+9)-V-3	-11176	-219	-15012	-9.24	-10.34	-29.78	132.00	192.00	192.00	4.7
0	(8+9)-II-2	-2459	651	-2583	-2.03	30.79	-5.12	132.00	192.00	192.00	5.3
0	(8+9)-V-4	-7200	160	-18645	-5.95	7.55	-36.98	132.00	192.00	192.00	4.3
0	(8+9)-II-4	-2480	637	-9502	-2.05	30.13	-18.85	132.00	192.00	192.00	3.9
0	(8+9)-VI-1	-15695	-605	11117	-12.97	-28.59	22.05	132.00	192.00	192.00	3.7
0	(8+9)-III-2	-8992	41	7691	-7.43	1.95	15.25	132.00	192.00	192.00	11
0	(8+9)-VI-2	-2442	657	-991	-2.02	31.07	-1.97	132.00	192.00	192.00	5.8
0	(8+9)-III-4	-9063	-5	-15374	-7.49	-0.23	-30.49	132.00	192.00	192.00	6.2
0	(8+9)-VI-3	-15750	-630	1014	-13.02	-29.80	2.01	132.00	192.00	192.00	5.9
0	(8+9)-I-1	-11049	-153	13360	-9.13	-7.23	26.50	132.00	192.00	192.00	5.6
0	(8+9)-VI-4	-2497	631	-11095	-2.06	29.85	-22.01	132.00	192.00	192.00	3.7
0	(8+9)-IV-4	-8878	23	-16292	-7.34	1.06	-32.32	132.00	192.00	192.00	5.7
0	(8+9)-VII-1	-9073	51	20704	-7.50	2.43	41.07	132.00	192.00	192.00	4.4
0	(8+9)-II-1	-15712	-611	9525	-12.99	-28.87	18.89	132.00	192.00	192.00	3.9
0	(8+9)-VII-2	-8936	61	12998	-7.38	2.89	25.78	132.00	192.00	192.00	6.6
0	(8+9)-III-1	-9130	32	15397	-7.55	1.49	30.54	132.00	192.00	192.00	5.9
0	(8+9)-VII-3	-9257	-34	-12975	-7.65	-1.62	-25.74	132.00	192.00	192.00	6.9
0	(8+9)-IV-1	-9315	4	16315	-7.70	0.20	32.36	132.00	192.00	192.00	5.8
0	(8+9)-VII-4	-9119	-25	-20682	-7.54	-1.17	-41.02	132.00	192.00	192.00	4.5
0	(8+9)-III-3	-9200	-14	-7668	-7.60	-0.68	-15.21	132.00	192.00	192.00	12
0	(8+9)-IV-3	-9336	-10	9396	-7.72	-0.45	18.64	132.00	192.00	192.00	9.9
0	(8+9)-II-3	-15733	-624	2606	-13.00	-29.52	5.17	132.00	192.00	192.00	5.4
0	(8+9)-VIII-1	-9298	10	17907	-7.68	0.48	35.52	132.00	192.00	192.00	5.3
0	(8+9)-VIII-2	-8839	42	-7781	-7.31	2.00	-15.43	132.00	192.00	192.00	11
0	(8+9)-VIII-3	-9353	-16	7804	-7.73	-0.74	15.48	132.00	192.00	192.00	12
0	(8+9)-I-3	-11119	-199	-9705	-9.19	-9.41	-19.25	132.00	192.00	192.00	6.6

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Ty kg	τ_d kg/cm ²	fvd kg/cm ²	RS	Cs
0	(8+9)-V-2	54	0.01	6.40	Si	>100
0	(8+9)-II-2	163	0.04	6.40	Si	>100
0	(8+9)-IV-1	5	0.00	6.40	Si	>100
0	(8+9)-II-3	-158	0.04	6.40	Si	>100
0	(8+9)-VIII-1	6	0.00	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
0	(8+9)-II-4	161	0.04	6.40	Si	>100
0	(8+9)-VII-1	7	0.00	6.40	Si	>100
0	(8+9)-III-1	6	0.00	6.40	Si	>100
0	(8+9)-VI-3	-158	0.04	6.40	Si	>100
0	(8+9)-III-2	5	0.00	6.40	Si	>100
0	(8+9)-I-2	53	0.01	6.40	Si	>100
0	(8+9)-VI-2	163	0.04	6.40	Si	>100
0	(8+9)-I-4	48	0.01	6.40	Si	>100
0	(8+9)-VI-1	-156	0.04	6.40	Si	>100
0	(8+9)-VIII-3	4	0.00	6.40	Si	>100
0	(8+9)-VI-4	161	0.04	6.40	Si	>100
0	(8+9)-V-4	47	0.01	6.40	Si	>100
0	(8+9)-I-3	-48	0.01	6.40	Si	>100
0	(8+9)-VII-2	6	0.00	6.40	Si	>100
0	(8+9)-I-1	-43	0.01	6.40	Si	>100
0	(8+9)-II-1	-156	0.04	6.40	Si	>100
0	(8+9)-IV-3	4	0.00	6.40	Si	>100
0	(8+9)-V-3	-49	0.01	6.40	Si	>100
0	(8+9)-V-1	-42	0.01	6.40	Si	>100
2500	1	5	0.00	3.84	Si	>100
2500	2	12	0.00	5.76	Si	>100
2500	3	12	0.00	5.76	Si	>100
2500	4	5	0.00	5.12	Si	>100
2500	5	5	0.00	5.12	Si	>100
2500	6	5	0.00	5.12	Si	>100
2500	7	5	0.00	5.12	Si	>100
2500	(8+9)-VIII-4	6	0.00	6.40	Si	>100
2500	(8+9)-III-3	4	0.00	6.40	Si	>100
2500	(8+9)-VII-3	6	0.00	6.40	Si	>100
2500	(8+9)-VII-4	6	0.00	6.40	Si	>100
2500	(8+9)-III-4	5	0.00	6.40	Si	>100
2500	(8+9)-VIII-2	4	0.00	6.40	Si	>100
2500	(8+9)-IV-2	5	0.00	6.40	Si	>100
2500	(8+9)-IV-4	5	0.00	6.40	Si	>100
Verifiche nella direzione secondaria						
0	(8+9)-VIII-4	-34	0.03	6.40	Si	>100
0	(8+9)-III-2	-17	0.01	6.40	Si	>100
0	(8+9)-IV-4	-35	0.03	6.40	Si	>100
0	(8+9)-IV-2	-37	0.03	6.40	Si	>100
0	(8+9)-IV-3	32	0.02	6.40	Si	>100
0	(8+9)-VIII-2	-38	0.03	6.40	Si	>100
0	(8+9)-VII-3	13	0.01	6.40	Si	>100
0	(8+9)-VIII-3	33	0.02	6.40	Si	>100
0	(8+9)-VIII-1	29	0.02	6.40	Si	>100
0	(8+9)-VII-2	-19	0.01	6.40	Si	>100
0	(8+9)-IV-1	30	0.02	6.40	Si	>100
0	(8+9)-III-4	-9	0.01	6.40	Si	>100
0	(8+9)-III-3	11	0.01	6.40	Si	>100
1935	1	-6	0.00	3.84	Si	>100
1935	2	-13	0.01	5.76	Si	>100
1935	3	-13	0.01	5.76	Si	>100
1935	4	-6	0.00	5.12	Si	>100
1935	5	-6	0.00	5.12	Si	>100
1935	6	-6	0.00	5.12	Si	>100
1935	7	-6	0.00	5.12	Si	>100
1935	(8+9)-V-4	-200	0.15	6.40	Si	42
1935	(8+9)-II-4	-699	0.53	6.40	Si	12
1935	(8+9)-VI-4	-697	0.53	6.40	Si	12
1935	(8+9)-I-2	-221	0.17	6.40	Si	38
1935	(8+9)-VII-1	-20	0.02	6.40	Si	>100
1935	(8+9)-V-1	191	0.15	6.40	Si	44
1935	(8+9)-I-4	-206	0.16	6.40	Si	41
1935	(8+9)-V-3	218	0.17	6.40	Si	38
1935	(8+9)-II-1	690	0.53	6.40	Si	12

X	Comb.	Ty	τ_d	fvd	RS	Cs
1935	(8+9)-VI-1	688	0.53	6.40	Si	12
1935	(8+9)-VI-3	697	0.53	6.40	Si	12
1935	(8+9)-V-2	-227	0.17	6.40	Si	37
1935	(8+9)-I-3	212	0.16	6.40	Si	40
1935	(8+9)-VI-2	-706	0.54	6.40	Si	12
1935	(8+9)-I-1	197	0.15	6.40	Si	43
1935	(8+9)-II-2	-704	0.54	6.40	Si	12
1935	(8+9)-II-3	695	0.53	6.40	Si	12
1935	(8+9)-III-1	-13	0.01	6.40	Si	>100
3870	(8+9)-VII-4	11	0.01	6.40	Si	>100

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	(8+9)-II-2	1089	0.58	32.00	55	0.14	20.00	>100	V	55
1250	(8+9)-VIII-4	-9719	-5.19	32.00	6.2	-1.26	20.00	16	V	6.2
1250	(8+9)-IV-1	10498	5.60	32.00	5.7	1.36	20.00	15	V	5.7
1250	(8+9)-V-4	-9862	-5.26	32.00	6.1	-1.27	20.00	16	V	6.1
1250	(8+9)-III-1	10057	5.37	32.00	6.0	1.30	20.00	15	V	6.0
1250	(8+9)-IV-3	6344	3.39	32.00	9.4	0.82	20.00	24	V	9.4
1250	(8+9)-III-2	5526	2.95	32.00	11	0.71	20.00	28	V	11
1250	(8+9)-VIII-1	11455	6.12	32.00	5.2	1.48	20.00	14	V	5.2
1250	(8+9)-VI-2	1845	0.98	32.00	32	0.24	20.00	84	V	32
1250	(8+9)-I-1	8409	4.49	32.00	7.1	1.09	20.00	18	V	7.1
1250	(8+9)-III-4	-8322	-4.44	32.00	7.2	-1.08	20.00	19	V	7.2
1250	(8+9)-VII-2	8715	4.65	32.00	6.9	1.13	20.00	18	V	6.9
1250	(8+9)-VI-1	5958	3.18	32.00	10	0.77	20.00	26	V	10
1250	(8+9)-II-1	5002	2.67	32.00	12	0.65	20.00	31	V	12
1250	(8+9)-IV-2	-4608	-2.46	32.00	13	-0.60	20.00	34	V	13
1250	(8+9)-VI-4	-4223	-2.25	32.00	14	-0.55	20.00	37	V	14
1250	(8+9)-VIII-3	5387	2.88	32.00	11	0.70	20.00	29	V	11
1250	(8+9)-IV-4	-8762	-4.68	32.00	6.8	-1.13	20.00	18	V	6.8
1250	(8+9)-I-2	7175	3.83	32.00	8.4	0.93	20.00	22	V	8.4
1250	(8+9)-VII-1	13246	7.07	32.00	4.5	1.71	20.00	12	V	4.5
1250	(8+9)-II-4	-3266	-1.74	32.00	18	-0.42	20.00	47	V	18
1250	(8+9)-VII-4	-11511	-6.15	32.00	5.2	-1.49	20.00	13	V	5.2
1250	(8+9)-I-4	-6673	-3.56	32.00	9.0	-0.86	20.00	23	V	9.0
1250	(8+9)-V-1	11597	6.19	32.00	5.2	1.50	20.00	13	V	5.2
1250	(8+9)-V-2	10363	5.53	32.00	5.8	1.34	20.00	15	V	5.8
1250	(8+9)-V-3	-8628	-4.61	32.00	6.9	-1.11	20.00	18	V	6.9
2500	1	-3056	-1.63	19.20	12	-0.39	12.00	30	V	12
2500	2	-6320	-3.37	28.80	8.5	-0.82	18.00	22	V	8.5
2500	3	-6320	-3.37	28.80	8.5	-0.82	18.00	22	V	8.5
2500	4	-3056	-1.63	25.60	16	-0.39	16.00	41	V	16
2500	5	-3056	-1.63	25.60	16	-0.39	16.00	41	V	16
2500	6	-3056	-1.63	25.60	16	-0.39	16.00	41	V	16
2500	7	-3056	-1.63	25.60	16	-0.39	16.00	41	V	16
2500	(8+9)-VII-3	-7002	-3.74	32.00	8.6	-0.90	20.00	22	V	8.6
2500	(8+9)-III-3	-5081	-2.71	32.00	12	-0.66	20.00	30	V	12
2500	(8+9)-I-3	-6280	-3.35	32.00	9.5	-0.81	20.00	25	V	9.5
2500	(8+9)-VIII-2	-3966	-2.12	32.00	15	-0.51	20.00	39	V	15
2500	(8+9)-VI-3	-4252	-2.27	32.00	14	-0.55	20.00	36	V	14
2500	(8+9)-II-3	-3676	-1.96	32.00	16	-0.47	20.00	42	V	16
Verifiche nella direzione secondaria										
1935	(8+9)-VIII-4	-9083	-7.51	32.00	4.3	-1.82	20.00	11	V	4.3
1935	(8+9)-VII-2	6568	5.43	32.00	5.9	1.31	20.00	15	V	5.9
1935	(8+9)-III-3	-3876	-3.20	32.00	10.0	-0.78	20.00	26	V	10.0
1935	(8+9)-IV-2	-4779	-3.95	32.00	8.1	-0.96	20.00	21	V	8.1
1935	(8+9)-III-4	-7780	-6.43	32.00	5.0	-1.56	20.00	13	V	5.0
1935	(8+9)-VIII-2	-3962	-3.27	32.00	9.8	-0.79	20.00	25	V	9.8
1935	(8+9)-IV-1	8235	6.81	32.00	4.7	1.65	20.00	12	V	4.7
1935	(8+9)-VII-4	-10503	-8.68	32.00	3.7	-2.10	20.00	9.5	V	3.7
1935	(8+9)-I-1	5799	4.79	32.00	6.7	1.16	20.00	17	V	6.7

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
1935	(8+9)-IV-3	4748	3.92	32.00	8.2	0.95	20.00	21	V	8.2
1935	(8+9)-I-3	-5825	-4.81	32.00	6.6	-1.17	20.00	17	V	6.6
1935	(8+9)-IV-4	-8266	-6.83	32.00	4.7	-1.65	20.00	12	V	4.7
1935	(8+9)-II-1	1737	1.44	32.00	22	0.35	20.00	58	V	22
1935	(8+9)-V-1	8522	7.04	32.00	4.5	1.70	20.00	12	V	4.5
1935	(8+9)-II-3	-1751	-1.45	32.00	22	-0.35	20.00	57	V	22
1935	(8+9)-V-2	8517	7.04	32.00	4.5	1.70	20.00	12	V	4.5
1935	(8+9)-III-1	7749	6.40	32.00	5.0	1.55	20.00	13	V	5.0
1935	(8+9)-V-3	-8548	-7.06	32.00	4.5	-1.71	20.00	12	V	4.5
1935	(8+9)-VIII-3	3931	3.25	32.00	9.9	0.79	20.00	25	V	9.9
1935	(8+9)-V-4	-8553	-7.07	32.00	4.5	-1.71	20.00	12	V	4.5
1935	(8+9)-VII-3	-6599	-5.45	32.00	5.9	-1.32	20.00	15	V	5.9
1935	(8+9)-VI-1	2553	2.11	32.00	15	0.51	20.00	39	V	15
1935	(8+9)-I-4	-5830	-4.82	32.00	6.6	-1.17	20.00	17	V	6.6
1935	(8+9)-VI-2	2537	2.10	32.00	15	0.51	20.00	39	V	15
1935	(8+9)-II-4	-1768	-1.46	32.00	22	-0.35	20.00	57	V	22
1935	(8+9)-VIII-1	9052	7.48	32.00	4.3	1.81	20.00	11	V	4.3
1935	(8+9)-I-2	5794	4.79	32.00	6.7	1.16	20.00	17	V	6.7
1935	(8+9)-II-2	1720	1.42	32.00	23	0.34	20.00	58	V	23
1935	(8+9)-III-2	3845	3.18	32.00	10	0.77	20.00	26	V	10
1935	(8+9)-VI-3	-2568	-2.12	32.00	15	-0.51	20.00	39	V	15
1935	(8+9)-VI-4	-2584	-2.14	32.00	15	-0.52	20.00	39	V	15
1935	(8+9)-VII-1	10472	8.65	32.00	3.7	2.09	20.00	9.5	V	3.7
3870	1	-368	-0.30	19.20	63	-0.07	12.00	>100	V	63
3870	2	-765	-0.63	28.80	46	-0.15	18.00	>100	V	46
3870	3	-765	-0.63	28.80	46	-0.15	18.00	>100	V	46
3870	4	-368	-0.30	25.60	84	-0.07	16.00	>100	V	84
3870	5	-368	-0.30	25.60	84	-0.07	16.00	>100	V	84
3870	6	-368	-0.30	25.60	84	-0.07	16.00	>100	V	84
3870	7	-368	-0.30	25.60	84	-0.07	16.00	>100	V	84

Setto 23: origine (997.5,2661.7,193.5), direzione (0.825704,0.564103,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	1	-383	-2	1384	-0.14	-0.03	0.76	79.20	115.20	115.20	>100
0	2	-827	-4	2919	-0.29	-0.05	1.61	118.80	172.80	172.80	>100
0	3	-827	-4	2919	-0.29	-0.05	1.61	118.80	172.80	172.80	>100
0	4	-383	-2	1384	-0.14	-0.03	0.76	105.60	153.60	153.60	>100
0	5	-383	-2	1384	-0.14	-0.03	0.76	105.60	153.60	153.60	>100
0	6	-383	-2	1384	-0.14	-0.03	0.76	105.60	153.60	153.60	>100
0	7	-383	-2	1384	-0.14	-0.03	0.76	105.60	153.60	153.60	>100
0	(8+9)-VIII-4	1606	-9	-8043	0.57	-0.12	-4.44	132.00	192.00	192.00	36
0	(8+9)-IV-1	-1955	8	9073	-0.70	0.11	5.01	132.00	192.00	192.00	37
0	(8+9)-V-1	-1748	-13	7825	-0.62	-0.18	4.32	132.00	192.00	192.00	43
0	(8+9)-I-2	-1762	-19	8692	-0.63	-0.26	4.80	132.00	192.00	192.00	38
0	(8+9)-V-2	-2343	-26	11597	-0.83	-0.34	6.40	132.00	192.00	192.00	28
0	(8+9)-I-4	644	4	-3017	0.23	0.05	-1.66	132.00	192.00	192.00	94
0	(8+9)-V-3	1819	23	-9695	0.65	0.31	-5.35	132.00	192.00	192.00	29
0	(8+9)-II-2	-1613	-26	8995	-0.57	-0.34	4.96	132.00	192.00	192.00	36
0	(8+9)-V-4	1225	11	-5923	0.44	0.14	-3.27	132.00	192.00	192.00	47
0	(8+9)-II-4	-892	-19	5482	-0.32	-0.25	3.03	132.00	192.00	192.00	59
0	(8+9)-VI-1	194	14	-2708	0.07	0.19	-1.49	132.00	192.00	192.00	>100
0	(8+9)-III-2	-1065	-17	4896	-0.38	-0.23	2.70	132.00	192.00	192.00	66
0	(8+9)-VI-2	-1788	-28	9867	-0.64	-0.37	5.44	132.00	192.00	192.00	33
0	(8+9)-III-4	1341	6	-6813	0.48	0.09	-3.76	132.00	192.00	192.00	42
0	(8+9)-VI-3	1264	25	-7964	0.45	0.33	-4.39	132.00	192.00	192.00	36
0	(8+9)-IV-2	710	-18	-3659	0.25	-0.24	-2.02	132.00	192.00	192.00	73
0	(8+9)-VI-4	-717	-17	4611	-0.26	-0.22	2.54	132.00	192.00	192.00	69
0	(8+9)-IV-4	1432	-11	-7171	0.51	-0.15	-3.96	132.00	192.00	192.00	40
0	(8+9)-VII-1	-2445	-16	11621	-0.87	-0.21	6.41	132.00	192.00	192.00	29
0	(8+9)-II-1	368	16	-3580	0.13	0.21	-1.98	132.00	192.00	192.00	81
0	(8+9)-VII-2	-1646	-23	7801	-0.59	-0.31	4.30	132.00	192.00	192.00	42

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-III-1	-1865	-9	8715	-0.66	-0.12	4.81	132.00	192.00	192.00	39
0	(8+9)-VII-3	1122	21	-5899	0.40	0.28	-3.26	132.00	192.00	192.00	47
0	(8+9)-I-1	-1168	-7	4919	-0.42	-0.09	2.71	132.00	192.00	192.00	68
0	(8+9)-VII-4	1922	13	-9719	0.68	0.17	-5.36	132.00	192.00	192.00	29
0	(8+9)-III-3	541	14	-2994	0.19	0.19	-1.65	132.00	192.00	192.00	90
0	(8+9)-IV-3	-1234	15	5561	-0.44	0.21	3.07	132.00	192.00	192.00	59
0	(8+9)-II-3	1090	23	-7093	0.39	0.31	-3.91	132.00	192.00	192.00	40
0	(8+9)-VIII-1	-2130	6	9945	-0.76	0.09	5.49	132.00	192.00	192.00	34
0	(8+9)-I-3	1238	17	-6790	0.44	0.22	-3.75	132.00	192.00	192.00	42
0	(8+9)-VIII-3	-1059	17	4689	-0.38	0.23	2.59	132.00	192.00	192.00	68
1459	(8+9)-VIII-2	1143	81	-789	0.41	1.08	-0.44	132.00	192.00	192.00	91
Verifiche nella direzione secondaria											
0	(8+9)-VIII-4	-5864	84	-6034	-8.30	6.77	-35.14	132.00	192.00	192.00	4.5
0	(8+9)-VII-2	4695	180	1857	6.65	14.61	10.81	132.00	192.00	192.00	5.5
0	(8+9)-III-3	-9880	-109	-1885	-13.99	-8.86	-10.98	132.00	192.00	192.00	9.2
0	(8+9)-IV-2	-1653	149	-4162	-2.34	12.09	-24.24	132.00	192.00	192.00	5.3
0	(8+9)-III-4	-9341	-38	-4385	-13.23	-3.11	-25.54	132.00	192.00	192.00	6.5
0	(8+9)-VIII-2	-700	166	-3739	-0.99	13.48	-21.77	132.00	192.00	192.00	5.4
0	(8+9)-IV-1	-3449	-87	4171	-4.88	-7.08	24.29	132.00	192.00	192.00	6.1
0	(8+9)-VII-4	-12517	-96	-5796	-17.73	-7.77	-33.76	132.00	192.00	192.00	4.4
0	(8+9)-I-1	-1654	8	1104	-2.34	0.64	6.43	132.00	192.00	192.00	27
0	(8+9)-IV-3	-6708	-136	2722	-9.50	-11.00	15.85	132.00	192.00	192.00	7.0
0	(8+9)-I-3	-12515	-153	-3726	-17.72	-12.43	-21.70	132.00	192.00	192.00	5.4
0	(8+9)-IV-4	-4911	101	-5611	-6.95	8.17	-32.68	132.00	192.00	192.00	4.7
0	(8+9)-II-1	-12232	-234	-1965	-17.32	-18.96	-11.44	132.00	192.00	192.00	6.0
0	(8+9)-V-1	1522	65	2516	2.15	5.29	14.65	132.00	192.00	192.00	8.3
0	(8+9)-II-3	-15491	-282	-3414	-21.94	-22.88	-19.88	132.00	192.00	192.00	4.2
0	(8+9)-V-2	7330	224	3697	10.38	18.17	21.53	132.00	192.00	192.00	3.5
0	(8+9)-III-1	981	52	2945	1.39	4.20	17.15	132.00	192.00	192.00	8.2
0	(8+9)-V-3	-15691	-211	-5137	-22.22	-17.08	-29.92	132.00	192.00	192.00	3.9
0	(8+9)-VIII-3	-7660	-153	2299	-10.85	-12.39	13.39	132.00	192.00	192.00	7.3
0	(8+9)-V-4	-9882	-52	-3956	-13.99	-4.21	-23.04	132.00	192.00	192.00	6.8
0	(8+9)-VII-3	-13056	-167	-3296	-18.49	-13.52	-19.20	132.00	192.00	192.00	5.6
0	(8+9)-VI-1	-11280	-217	-1542	-15.97	-17.56	-8.98	132.00	192.00	192.00	6.9
0	(8+9)-I-4	-6706	6	-2544	-9.50	0.45	-14.82	132.00	192.00	192.00	12
0	(8+9)-VI-2	8083	313	2398	11.45	25.36	13.96	132.00	192.00	192.00	3.4
0	(8+9)-II-4	3872	247	525	5.48	20.04	3.06	132.00	192.00	192.00	6.2
0	(8+9)-VIII-1	-2497	-70	4595	-3.54	-5.68	26.76	132.00	192.00	192.00	5.9
0	(8+9)-I-2	4155	167	2286	5.88	13.51	13.31	132.00	192.00	192.00	5.4
0	(8+9)-II-2	7131	296	1974	10.10	23.96	11.50	132.00	192.00	192.00	3.8
0	(8+9)-III-2	1520	123	445	2.15	9.95	2.59	132.00	192.00	192.00	12
0	(8+9)-VI-3	-16443	-300	-3838	-23.29	-24.27	-22.35	132.00	192.00	192.00	3.9
0	(8+9)-VI-4	2919	230	102	4.13	18.65	0.59	132.00	192.00	192.00	7.6
0	(8+9)-VII-1	4156	109	4357	5.89	8.86	25.37	132.00	192.00	192.00	4.5
1935	1	-6602	4	-1366	-9.35	0.36	-7.96	79.20	115.20	115.20	13
1935	2	-13450	9	-2787	-19.05	0.73	-16.23	118.80	172.80	172.80	9.1
1935	3	-13450	9	-2787	-19.05	0.73	-16.23	118.80	172.80	172.80	9.1
1935	4	-6602	4	-1366	-9.35	0.36	-7.96	105.60	153.60	153.60	17
1935	5	-6602	4	-1366	-9.35	0.36	-7.96	105.60	153.60	153.60	17
1935	6	-6602	4	-1366	-9.35	0.36	-7.96	105.60	153.60	153.60	17
1935	7	-6602	4	-1366	-9.35	0.36	-7.96	105.60	153.60	153.60	17

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
730	(8+9)-VI-1	-200	0.05	6.40	Si	>100
730	(8+9)-VI-4	198	0.05	6.40	Si	>100
730	(8+9)-II-3	-224	0.06	6.40	Si	>100
730	(8+9)-VII-3	-136	0.04	6.40	Si	>100
730	(8+9)-II-1	-206	0.05	6.40	Si	>100
730	(8+9)-VII-2	133	0.03	6.40	Si	>100
730	(8+9)-VI-3	-230	0.06	6.40	Si	>100
730	(8+9)-I-1	-36	0.01	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
730	(8+9)-VI-2	227	0.06	6.40	Si	>100
730	(8+9)-III-2	113	0.03	6.40	Si	>100
730	(8+9)-II-4	204	0.05	6.40	Si	>100
730	(8+9)-III-3	-115	0.03	6.40	Si	>100
730	(8+9)-II-2	221	0.06	6.40	Si	>100
1459	1	-17	0.00	3.84	Si	>100
1459	2	-38	0.01	5.76	Si	>100
1459	3	-38	0.01	5.76	Si	>100
1459	4	-17	0.00	5.12	Si	>100
1459	5	-17	0.00	5.12	Si	>100
1459	6	-17	0.00	5.12	Si	>100
1459	7	-17	0.00	5.12	Si	>100
1459	(8+9)-VIII-4	-397	0.10	6.40	Si	62
1459	(8+9)-IV-1	358	0.09	6.40	Si	69
1459	(8+9)-I-4	-44	0.01	6.40	Si	>100
1459	(8+9)-IV-3	317	0.08	6.40	Si	78
1459	(8+9)-VII-1	211	0.05	6.40	Si	>100
1459	(8+9)-V-1	70	0.02	6.40	Si	>100
1459	(8+9)-I-3	-116	0.03	6.40	Si	>100
1459	(8+9)-V-3	-166	0.04	6.40	Si	>100
1459	(8+9)-I-2	92	0.02	6.40	Si	>100
1459	(8+9)-IV-2	-341	0.09	6.40	Si	73
1459	(8+9)-VII-4	-234	0.06	6.40	Si	>100
1459	(8+9)-V-2	142	0.04	6.40	Si	>100
1459	(8+9)-V-4	-93	0.02	6.40	Si	>100
1459	(8+9)-III-4	-184	0.05	6.40	Si	>100
1459	(8+9)-IV-4	-382	0.10	6.40	Si	65
1459	(8+9)-VIII-1	373	0.10	6.40	Si	66
1459	(8+9)-VIII-2	-326	0.08	6.40	Si	76
1459	(8+9)-VIII-3	302	0.08	6.40	Si	82
1459	(8+9)-III-1	161	0.04	6.40	Si	>100
Verifiche nella direzione secondaria						
0	(8+9)-VIII-4	-504	0.66	6.40	Si	9.7
0	(8+9)-VII-2	-337	0.44	6.40	Si	15
0	(8+9)-III-3	259	0.34	6.40	Si	19
0	(8+9)-IV-2	-584	0.76	6.40	Si	8.4
0	(8+9)-III-4	-70	0.09	6.40	Si	70
0	(8+9)-VIII-2	-604	0.79	6.40	Si	8.1
0	(8+9)-IV-1	514	0.67	6.40	Si	9.5
0	(8+9)-VI-4	-134	0.17	6.40	Si	37
0	(8+9)-VII-3	327	0.43	6.40	Si	15
0	(8+9)-I-1	-50	0.07	6.40	Si	97
0	(8+9)-I-3	148	0.19	6.40	Si	33
0	(8+9)-IV-3	574	0.75	6.40	Si	8.5
0	(8+9)-II-1	144	0.19	6.40	Si	34
0	(8+9)-IV-4	-524	0.68	6.40	Si	9.3
0	(8+9)-II-3	204	0.27	6.40	Si	24
0	(8+9)-V-1	-119	0.16	6.40	Si	41
0	(8+9)-III-1	61	0.08	6.40	Si	81
0	(8+9)-V-2	-226	0.30	6.40	Si	22
0	(8+9)-VIII-3	594	0.78	6.40	Si	8.2
0	(8+9)-V-3	216	0.28	6.40	Si	23
0	(8+9)-I-2	-158	0.21	6.40	Si	31
0	(8+9)-V-4	109	0.14	6.40	Si	45
0	(8+9)-II-2	-214	0.28	6.40	Si	23
0	(8+9)-III-2	-269	0.35	6.40	Si	18
0	(8+9)-VIII-1	494	0.65	6.40	Si	9.9
0	(8+9)-I-4	41	0.05	6.40	Si	>100
0	(8+9)-II-4	-154	0.20	6.40	Si	32
0	(8+9)-VI-1	124	0.16	6.40	Si	40
0	(8+9)-VI-2	-234	0.31	6.40	Si	21
0	(8+9)-VI-3	224	0.29	6.40	Si	22
1935	(8+9)-VII-4	90	0.12	6.40	Si	54
1935	(8+9)-VII-1	-99	0.13	6.40	Si	49

X	Comb.	Ty	τ_d	fvd	RS	Cs
3870	1	-14	0.02	3.84	Si	>100
3870	2	-31	0.04	5.76	Si	>100
3870	3	-31	0.04	5.76	Si	>100
3870	4	-14	0.02	5.12	Si	>100
3870	5	-14	0.02	5.12	Si	>100
3870	6	-14	0.02	5.12	Si	>100
3870	7	-14	0.02	5.12	Si	>100

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	1	2694	1.44	19.20	13	0.35	12.00	34	V	13
0	2	5642	3.01	28.80	9.6	0.73	18.00	25	V	9.6
0	3	5642	3.01	28.80	9.6	0.73	18.00	25	V	9.6
0	4	2694	1.44	25.60	18	0.35	16.00	46	V	18
0	5	2694	1.44	25.60	18	0.35	16.00	46	V	18
0	6	2694	1.44	25.60	18	0.35	16.00	46	V	18
0	7	2694	1.44	25.60	18	0.35	16.00	46	V	18
0	(8+9)-VIII-4	-6309	-3.37	32.00	9.5	-0.82	20.00	25	V	9.5
0	(8+9)-IV-3	7117	3.80	32.00	8.4	0.92	20.00	22	V	8.4
0	(8+9)-IV-1	9439	5.04	32.00	6.4	1.22	20.00	16	V	6.4
0	(8+9)-VIII-1	10018	5.35	32.00	6.0	1.29	20.00	15	V	6.0
0	(8+9)-VIII-3	6537	3.49	32.00	9.2	0.84	20.00	24	V	9.2
0	(8+9)-IV-4	-5730	-3.06	32.00	10	-0.74	20.00	27	V	10
730	(8+9)-II-1	-3838	-2.05	32.00	16	-0.50	20.00	40	V	16
730	(8+9)-VII-4	-10877	-5.81	32.00	5.5	-1.41	20.00	14	V	5.5
730	(8+9)-V-4	-8678	-4.63	32.00	6.9	-1.12	20.00	18	V	6.9
730	(8+9)-VI-1	-2792	-1.49	32.00	21	-0.36	20.00	55	V	21
1459	(8+9)-V-1	10211	5.45	32.00	5.9	1.32	20.00	15	V	5.9
1459	(8+9)-I-2	12084	6.45	32.00	5.0	1.56	20.00	13	V	5.0
1459	(8+9)-VI-2	10871	5.80	32.00	5.5	1.40	20.00	14	V	5.5
1459	(8+9)-III-4	-8429	-4.50	32.00	7.1	-1.09	20.00	18	V	7.1
1459	(8+9)-VI-3	-9191	-4.91	32.00	6.5	-1.19	20.00	17	V	6.5
1459	(8+9)-IV-2	3580	1.91	32.00	17	0.46	20.00	43	V	17
1459	(8+9)-VI-4	4056	2.17	32.00	15	0.52	20.00	38	V	15
1459	(8+9)-III-2	10086	5.38	32.00	5.9	1.30	20.00	15	V	5.9
1459	(8+9)-VII-1	12209	6.52	32.00	4.9	1.58	20.00	13	V	4.9
1459	(8+9)-V-2	14185	7.57	32.00	4.2	1.83	20.00	11	V	4.2
1459	(8+9)-VII-2	12187	6.51	32.00	4.9	1.57	20.00	13	V	4.9
1459	(8+9)-II-4	4686	2.50	32.00	13	0.61	20.00	33	V	13
1459	(8+9)-VII-3	-10508	-5.61	32.00	5.7	-1.36	20.00	15	V	5.7
1459	(8+9)-I-1	8110	4.33	32.00	7.4	1.05	20.00	19	V	7.4
1459	(8+9)-II-2	10240	5.47	32.00	5.9	1.32	20.00	15	V	5.9
1459	(8+9)-II-3	-8561	-4.57	32.00	7.0	-1.11	20.00	18	V	7.0
1459	(8+9)-III-3	-8407	-4.49	32.00	7.1	-1.09	20.00	18	V	7.1
1459	(8+9)-V-3	-12506	-6.68	32.00	4.8	-1.62	20.00	12	V	4.8
1459	(8+9)-I-4	-6431	-3.43	32.00	9.3	-0.83	20.00	24	V	9.3
1459	(8+9)-VIII-2	4210	2.25	32.00	14	0.54	20.00	37	V	14
1459	(8+9)-I-3	-10405	-5.55	32.00	5.8	-1.34	20.00	15	V	5.8
1459	(8+9)-III-1	10108	5.40	32.00	5.9	1.31	20.00	15	V	5.9
Verifiche nella direzione secondaria										
1935	(8+9)-VIII-4	-3690	-5.23	32.00	6.1	-1.26	20.00	16	V	6.1
1935	(8+9)-VII-1	6339	8.98	32.00	3.6	2.17	20.00	9.2	V	3.6
1935	(8+9)-III-2	3016	4.27	32.00	7.5	1.03	20.00	19	V	7.5
1935	(8+9)-III-3	-2168	-3.07	32.00	10	-0.74	20.00	27	V	10
1935	(8+9)-VIII-1	4537	6.43	32.00	5.0	1.55	20.00	13	V	5.0
1935	(8+9)-III-4	-3711	-5.25	32.00	6.1	-1.27	20.00	16	V	6.1
1935	(8+9)-VII-3	-3949	-5.59	32.00	5.7	-1.35	20.00	15	V	5.7
1935	(8+9)-IV-1	4003	5.67	32.00	5.6	1.37	20.00	15	V	5.6
1935	(8+9)-I-1	2582	3.66	32.00	8.8	0.88	20.00	23	V	8.8
1935	(8+9)-VI-4	2896	4.10	32.00	7.8	0.99	20.00	20	V	7.8
1935	(8+9)-I-3	-4144	-5.87	32.00	5.5	-1.42	20.00	14	V	5.5
1935	(8+9)-IV-3	1985	2.81	32.00	11	0.68	20.00	29	V	11

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
1935	(8+9)-II-1	-2582	-3.66	32.00	8.8	-0.88	20.00	23	V	8.8
1935	(8+9)-IV-4	-3156	-4.47	32.00	7.2	-1.08	20.00	18	V	7.2
1935	(8+9)-II-3	-4600	-6.51	32.00	4.9	-1.58	20.00	13	V	4.9
1935	(8+9)-V-1	4363	6.18	32.00	5.2	1.50	20.00	13	V	5.2
1935	(8+9)-III-1	4558	6.45	32.00	5.0	1.56	20.00	13	V	5.0
1935	(8+9)-V-2	6772	9.59	32.00	3.3	2.32	20.00	8.6	V	3.3
1935	(8+9)-VII-4	-5491	-7.78	32.00	4.1	-1.88	20.00	11	V	4.1
1935	(8+9)-V-3	-5925	-8.39	32.00	3.8	-2.03	20.00	9.9	V	3.8
1935	(8+9)-I-2	4991	7.07	32.00	4.5	1.71	20.00	12	V	4.5
1935	(8+9)-V-4	-3516	-4.98	32.00	6.4	-1.20	20.00	17	V	6.4
1935	(8+9)-II-2	5448	7.71	32.00	4.1	1.87	20.00	11	V	4.1
1935	(8+9)-VIII-3	1451	2.05	32.00	16	0.50	20.00	40	V	16
1935	(8+9)-VII-2	4797	6.79	32.00	4.7	1.64	20.00	12	V	4.7
1935	(8+9)-I-4	-1735	-2.46	32.00	13	-0.59	20.00	34	V	13
1935	(8+9)-II-4	3430	4.86	32.00	6.6	1.18	20.00	17	V	6.6
1935	(8+9)-VI-1	-2048	-2.90	32.00	11	-0.70	20.00	28	V	11
1935	(8+9)-VI-2	5982	8.47	32.00	3.8	2.05	20.00	9.8	V	3.8
1935	(8+9)-VI-3	-5135	-7.27	32.00	4.4	-1.76	20.00	11	V	4.4
3870	1	894	1.27	19.20	15	0.31	12.00	39	V	15
3870	2	1858	2.63	28.80	11	0.64	18.00	28	V	11
3870	3	1858	2.63	28.80	11	0.64	18.00	28	V	11
3870	4	894	1.27	25.60	20	0.31	16.00	52	V	20
3870	5	894	1.27	25.60	20	0.31	16.00	52	V	20
3870	6	894	1.27	25.60	20	0.31	16.00	52	V	20
3870	7	894	1.27	25.60	20	0.31	16.00	52	V	20
3870	(8+9)-VIII-2	1240	1.76	32.00	18	0.42	20.00	47	V	18
3870	(8+9)-IV-2	1159	1.64	32.00	19	0.40	20.00	50	V	19

Setto 24: origine (213.1,2125.8,25.0), direzione (0.825704,0.564103,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	1	237	0	-80	0.65	0.02	-2.66	79.20	115.20	115.20	32
0	2	470	0	-162	1.30	0.05	-5.37	118.80	172.80	172.80	24
0	3	470	0	-162	1.30	0.05	-5.37	118.80	172.80	172.80	24
0	4	237	0	-80	0.65	0.02	-2.66	105.60	153.60	153.60	42
0	5	237	0	-80	0.65	0.02	-2.66	105.60	153.60	153.60	42
0	6	237	0	-80	0.65	0.02	-2.66	105.60	153.60	153.60	42
0	7	237	0	-80	0.65	0.02	-2.66	105.60	153.60	153.60	42
0	(8+9)-V-3	2737	1	-536	7.54	0.09	-17.71	132.00	192.00	192.00	6.7
0	(8+9)-V-4	4173	1	-800	11.50	0.15	-26.46	132.00	192.00	192.00	4.4
0	(8+9)-VII-3	2682	1	-525	7.39	0.08	-17.34	132.00	192.00	192.00	6.8
0	(8+9)-III-3	1632	1	-341	4.50	0.06	-11.26	132.00	192.00	192.00	11
0	(8+9)-I-4	3124	1	-617	8.61	0.12	-20.38	132.00	192.00	192.00	5.8
0	(8+9)-III-4	3179	1	-628	8.76	0.13	-20.75	132.00	192.00	192.00	5.7
0	(8+9)-II-2	1888	1	-368	5.20	0.09	-12.18	132.00	192.00	192.00	9.7
0	(8+9)-VI-4	3547	1	-681	9.77	0.14	-22.50	132.00	192.00	192.00	5.2
0	(8+9)-II-4	3232	1	-625	8.90	0.14	-20.68	132.00	192.00	192.00	5.7
0	(8+9)-IV-2	2070	1	-406	5.70	0.11	-13.41	132.00	192.00	192.00	8.8
0	(8+9)-I-3	1687	1	-352	4.65	0.06	-11.63	132.00	192.00	192.00	10
0	(8+9)-VIII-2	1756	1	-350	4.84	0.10	-11.58	132.00	192.00	192.00	10
0	(8+9)-VII-4	4228	1	-812	11.65	0.15	-26.83	132.00	192.00	192.00	4.4
0	(8+9)-VIII-4	3730	2	-718	10.27	0.16	-23.73	132.00	192.00	192.00	4.9
0	(8+9)-VI-2	1573	1	-313	4.33	0.08	-10.36	132.00	192.00	192.00	11
0	(8+9)-IV-4	3415	2	-663	9.41	0.16	-21.90	132.00	192.00	192.00	5.4
3500	(8+9)-I-2	961	1	-217	2.65	0.07	-7.17	132.00	192.00	192.00	17
3500	(8+9)-VI-3	933	-1	-337	2.57	-0.09	-11.13	132.00	192.00	192.00	13
3500	(8+9)-II-1	2200	-0	-679	6.06	-0.05	-22.44	132.00	192.00	192.00	6.1
3500	(8+9)-I-1	2080	0	-581	5.73	0.04	-19.21	132.00	192.00	192.00	7.0
3500	(8+9)-V-2	1795	1	-421	4.95	0.06	-13.93	132.00	192.00	192.00	9.1
3500	(8+9)-III-2	928	1	-244	2.56	0.08	-8.07	132.00	192.00	192.00	16
3500	(8+9)-VI-1	2450	-1	-740	6.75	-0.05	-24.46	132.00	192.00	192.00	5.6
3500	(8+9)-III-1	2113	0	-554	5.82	0.04	-18.31	132.00	192.00	192.00	7.2

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
3500	(8+9)-VII-1	2947	0	-758	8.12	0.03	-25.06	132.00	192.00	192.00	5.2
3500	(8+9)-VII-2	1763	1	-449	4.86	0.06	-14.83	132.00	192.00	192.00	8.7
3500	(8+9)-V-1	2915	0	-786	8.03	0.03	-25.97	132.00	192.00	192.00	5.1
3500	(8+9)-IV-1	2309	-1	-587	6.36	-0.05	-19.42	132.00	192.00	192.00	6.7
3500	(8+9)-VIII-1	2559	-1	-649	7.05	-0.06	-21.44	132.00	192.00	192.00	6.0
3500	(8+9)-II-3	1183	-1	-398	3.26	-0.09	-13.15	132.00	192.00	192.00	11
3500	(8+9)-VIII-3	1042	-1	-245	2.87	-0.09	-8.11	132.00	192.00	192.00	16
3500	(8+9)-IV-3	1292	-1	-307	3.56	-0.09	-10.13	132.00	192.00	192.00	12
Verifiche nella direzione secondaria											
0	(8+9)-II-1	-5900	-158	-11870	-3.48	-5.34	-12.01	132.00	192.00	192.00	11
0	(8+9)-II-4	-911	165	9049	-0.54	5.59	9.16	132.00	192.00	192.00	13
0	(8+9)-VI-3	-5622	-166	-4088	-3.32	-5.61	-4.14	132.00	192.00	192.00	20
0	(8+9)-II-3	-5698	-167	-5597	-3.36	-5.64	-5.66	132.00	192.00	192.00	17
0	(8+9)-VI-1	-5976	-159	-13378	-3.53	-5.37	-13.54	132.00	192.00	192.00	10
0	(8+9)-V-2	-3276	65	-14697	-1.93	2.20	-14.87	132.00	192.00	192.00	11
0	(8+9)-VI-2	-1189	173	1268	-0.70	5.86	1.28	132.00	192.00	192.00	27
0	(8+9)-V-3	-3535	-58	11876	-2.09	-1.95	12.02	132.00	192.00	192.00	14
0	(8+9)-I-2	-3025	69	-9668	-1.79	2.32	-9.78	132.00	192.00	192.00	16
0	(8+9)-I-3	-3786	-61	6847	-2.24	-2.07	6.93	132.00	192.00	192.00	21
0	(8+9)-II-2	-1113	174	2776	-0.66	5.89	2.81	132.00	192.00	192.00	22
250	(8+9)-VIII-4	-2436	25	17228	-1.44	0.83	17.43	132.00	192.00	192.00	11
250	(8+9)-VII-2	-3717	21	-14397	-2.19	0.72	-14.57	132.00	192.00	192.00	13
250	(8+9)-IV-4	-2511	23	15559	-1.48	0.78	15.75	132.00	192.00	192.00	12
250	(8+9)-I-4	-2782	-6	13776	-1.64	-0.21	13.94	132.00	192.00	192.00	14
250	(8+9)-V-1	-4165	9	-21946	-2.46	0.30	-22.21	132.00	192.00	192.00	8.5
250	(8+9)-VIII-3	-3907	-24	-9568	-2.31	-0.81	-9.68	132.00	192.00	192.00	18
250	(8+9)-VIII-2	-2789	31	6960	-1.65	1.05	7.04	132.00	192.00	192.00	24
250	(8+9)-III-2	-3466	26	-8835	-2.05	0.87	-8.94	132.00	192.00	192.00	20
250	(8+9)-III-4	-2790	-4	14266	-1.65	-0.15	14.44	132.00	192.00	192.00	13
250	(8+9)-V-4	-2531	-2	19338	-1.49	-0.06	19.57	132.00	192.00	192.00	9.8
250	(8+9)-IV-2	-2714	32	8629	-1.60	1.09	8.73	132.00	192.00	192.00	20
250	(8+9)-VIII-1	-4261	-18	-19836	-2.52	-0.60	-20.07	132.00	192.00	192.00	9.3
250	(8+9)-I-1	-3914	13	-16383	-2.31	0.45	-16.58	132.00	192.00	192.00	11
250	(8+9)-VII-4	-2539	0	19828	-1.50	0.00	20.07	132.00	192.00	192.00	9.6
250	(8+9)-III-3	-3231	-19	6227	-1.91	-0.64	6.30	132.00	192.00	192.00	28
250	(8+9)-IV-3	-3982	-25	-11237	-2.35	-0.86	-11.37	132.00	192.00	192.00	16
250	(8+9)-III-1	-3907	11	-16874	-2.31	0.38	-17.08	132.00	192.00	192.00	11
250	(8+9)-IV-1	-4185	-16	-18167	-2.47	-0.55	-18.38	132.00	192.00	192.00	10
250	(8+9)-VII-3	-2980	-14	11790	-1.76	-0.49	11.93	132.00	192.00	192.00	15
250	(8+9)-VI-4	-2412	18	15593	-1.42	0.61	15.78	132.00	192.00	192.00	12
250	(8+9)-VII-1	-4158	7	-22436	-2.45	0.23	-22.70	132.00	192.00	192.00	8.4
500	1	-4347	4	-3003	-2.57	0.14	-3.04	79.20	115.20	115.20	36
500	2	-8803	8	-6092	-5.20	0.26	-6.16	118.80	172.80	172.80	26
500	3	-8803	8	-6092	-5.20	0.26	-6.16	118.80	172.80	172.80	26
500	4	-4347	4	-3003	-2.57	0.14	-3.04	105.60	153.60	153.60	48
500	5	-4347	4	-3003	-2.57	0.14	-3.04	105.60	153.60	153.60	48
500	6	-4347	4	-3003	-2.57	0.14	-3.04	105.60	153.60	153.60	48
500	7	-4347	4	-3003	-2.57	0.14	-3.04	105.60	153.60	153.60	48

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
0	1	-1	0.00	3.84	Si	>100
0	2	-2	0.01	5.76	Si	>100
0	3	-2	0.01	5.76	Si	>100
0	4	-1	0.00	5.12	Si	>100
0	5	-1	0.00	5.12	Si	>100
0	6	-1	0.00	5.12	Si	>100
0	7	-1	0.00	5.12	Si	>100
0	(8+9)-III-2	-3	0.01	6.40	Si	>100
0	(8+9)-I-1	-4	0.01	6.40	Si	>100
0	(8+9)-VIII-3	1	0.00	6.40	Si	>100
0	(8+9)-VIII-2	-3	0.01	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
0	(8+9)-VII-2	-4	0.01	6.40	Si	>100
0	(8+9)-I-2	-2	0.00	6.40	Si	>100
0	(8+9)-IV-2	-3	0.01	6.40	Si	>100
0	(8+9)-III-3	1	0.00	6.40	Si	>100
3500	(8+9)-V-2	3	0.01	6.40	Si	>100
3500	(8+9)-II-1	6	0.01	6.40	Si	>100
3500	(8+9)-III-1	3	0.01	6.40	Si	>100
3500	(8+9)-VII-3	-3	0.01	6.40	Si	>100
3500	(8+9)-III-4	-2	0.00	6.40	Si	>100
3500	(8+9)-VII-4	-5	0.01	6.40	Si	>100
3500	(8+9)-II-3	5	0.01	6.40	Si	>100
3500	(8+9)-VIII-1	4	0.01	6.40	Si	>100
3500	(8+9)-IV-4	-2	0.00	6.40	Si	>100
3500	(8+9)-I-4	-3	0.01	6.40	Si	>100
3500	(8+9)-II-2	-5	0.01	6.40	Si	>100
3500	(8+9)-I-3	1	0.00	6.40	Si	>100
3500	(8+9)-V-4	-6	0.01	6.40	Si	>100
3500	(8+9)-VIII-4	-3	0.01	6.40	Si	>100
3500	(8+9)-VI-2	-4	0.01	6.40	Si	>100
3500	(8+9)-VI-3	4	0.01	6.40	Si	>100
3500	(8+9)-IV-3	2	0.00	6.40	Si	>100
3500	(8+9)-II-4	-5	0.01	6.40	Si	>100
3500	(8+9)-IV-1	3	0.01	6.40	Si	>100
3500	(8+9)-VII-1	5	0.01	6.40	Si	>100
3500	(8+9)-V-1	6	0.01	6.40	Si	>100
3500	(8+9)-V-3	-2	0.00	6.40	Si	>100
3500	(8+9)-VI-1	7	0.01	6.40	Si	>100
3500	(8+9)-VI-4	-6	0.01	6.40	Si	>100
Verifiche nella direzione secondaria						
0	(8+9)-III-2	-9	0.00	6.40	Si	>100
0	(8+9)-IV-4	-3	0.00	6.40	Si	>100
0	(8+9)-VIII-3	5	0.00	6.40	Si	>100
0	(8+9)-VII-3	9	0.01	6.40	Si	>100
0	(8+9)-VII-2	-11	0.01	6.40	Si	>100
0	(8+9)-VIII-2	-7	0.00	6.40	Si	>100
0	(8+9)-IV-3	5	0.00	6.40	Si	>100
0	(8+9)-IV-2	-7	0.00	6.40	Si	>100
0	(8+9)-III-3	7	0.00	6.40	Si	>100
250	(8+9)-VIII-4	3	0.00	6.40	Si	>100
250	(8+9)-IV-1	-3	0.00	6.40	Si	>100
250	(8+9)-III-1	-7	0.00	6.40	Si	>100
250	(8+9)-III-4	5	0.00	6.40	Si	>100
250	(8+9)-VIII-1	-5	0.00	6.40	Si	>100
250	(8+9)-VII-4	9	0.00	6.40	Si	>100
250	(8+9)-VII-1	-11	0.01	6.40	Si	>100
500	1	-2	0.00	3.84	Si	>100
500	2	-3	0.00	5.76	Si	>100
500	3	-3	0.00	5.76	Si	>100
500	4	-2	0.00	5.12	Si	>100
500	5	-2	0.00	5.12	Si	>100
500	6	-2	0.00	5.12	Si	>100
500	7	-2	0.00	5.12	Si	>100
500	(8+9)-V-2	-171	0.09	6.40	Si	68
500	(8+9)-I-4	-160	0.09	6.40	Si	73
500	(8+9)-I-1	157	0.09	6.40	Si	75
500	(8+9)-V-1	155	0.08	6.40	Si	76
500	(8+9)-I-2	-169	0.09	6.40	Si	70
500	(8+9)-V-4	-157	0.09	6.40	Si	75
500	(8+9)-I-3	166	0.09	6.40	Si	71
500	(8+9)-VI-2	-547	0.30	6.40	Si	21
500	(8+9)-II-4	-544	0.30	6.40	Si	22
500	(8+9)-VI-1	540	0.29	6.40	Si	22
500	(8+9)-VI-3	545	0.30	6.40	Si	22
500	(8+9)-V-3	169	0.09	6.40	Si	69

X	Comb.	Ty	τ_d	fvd	RS	Cs
500	(8+9)-II-3	544	0.30	6.40	Si	22
500	(8+9)-II-2	-546	0.30	6.40	Si	21
500	(8+9)-II-1	541	0.29	6.40	Si	22
500	(8+9)-VI-4	-543	0.30	6.40	Si	22

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	1	1400	5.79	19.20	3.3	1.40	12.00	8.6	V	3.3
0	2	2831	11.70	28.80	2.5	2.83	18.00	6.4	V	2.5
0	3	2831	11.70	28.80	2.5	2.83	18.00	6.4	V	2.5
0	4	1400	5.79	25.60	4.4	1.40	16.00	11	V	4.4
0	5	1400	5.79	25.60	4.4	1.40	16.00	11	V	4.4
0	6	1400	5.79	25.60	4.4	1.40	16.00	11	V	4.4
0	7	1400	5.79	25.60	4.4	1.40	16.00	11	V	4.4
0	(8+9)-VIII-4	-3189	-13.18	32.00	2.4	-3.19	20.00	6.3	V	2.4
0	(8+9)-IV-1	4762	19.68	32.00	1.6	4.76	20.00	4.2	V	1.6
0	(8+9)-V-1	5542	22.90	32.00	1.4	5.54	20.00	3.6	V	1.4
0	(8+9)-I-2	2697	11.15	32.00	2.9	2.70	20.00	7.4	V	2.9
0	(8+9)-V-2	3925	16.22	32.00	2.0	3.93	20.00	5.1	V	2.0
0	(8+9)-VI-3	2537	10.48	32.00	3.1	2.54	20.00	7.9	V	3.1
0	(8+9)-IV-3	3242	13.39	32.00	2.4	3.24	20.00	6.2	V	2.4
0	(8+9)-IV-4	-2821	-11.66	32.00	2.7	-2.82	20.00	7.1	V	2.7
0	(8+9)-VIII-3	2873	11.87	32.00	2.7	2.87	20.00	7.0	V	2.7
0	(8+9)-VII-1	5643	23.32	32.00	1.4	5.64	20.00	3.5	V	1.4
0	(8+9)-III-2	2596	10.73	32.00	3.0	2.60	20.00	7.7	V	3.0
0	(8+9)-II-1	4426	18.29	32.00	1.7	4.43	20.00	4.5	V	1.7
0	(8+9)-VII-4	-3701	-15.29	32.00	2.1	-3.70	20.00	5.4	V	2.1
0	(8+9)-VI-4	-2853	-11.79	32.00	2.7	-2.85	20.00	7.0	V	2.7
0	(8+9)-I-1	4314	17.83	32.00	1.8	4.31	20.00	4.6	V	1.8
0	(8+9)-III-1	4415	18.24	32.00	1.8	4.42	20.00	4.5	V	1.8
0	(8+9)-VIII-1	5131	21.20	32.00	1.5	5.13	20.00	3.9	V	1.5
0	(8+9)-II-3	2906	12.01	32.00	2.7	2.91	20.00	6.9	V	2.7
0	(8+9)-VII-2	3824	15.80	32.00	2.0	3.82	20.00	5.2	V	2.0
0	(8+9)-V-4	-3600	-14.88	32.00	2.2	-3.60	20.00	5.6	V	2.2
0	(8+9)-VI-1	4795	19.81	32.00	1.6	4.79	20.00	4.2	V	1.6
3500	(8+9)-I-4	-2528	-10.45	32.00	3.1	-2.53	20.00	7.9	V	3.1
3500	(8+9)-V-3	-2233	-9.23	32.00	3.5	-2.23	20.00	9.0	V	3.5
3500	(8+9)-II-2	-1694	-7.00	32.00	4.6	-1.69	20.00	12	V	4.6
3500	(8+9)-III-4	-2542	-10.50	32.00	3.0	-2.54	20.00	7.9	V	3.0
3500	(8+9)-IV-2	-1740	-7.19	32.00	4.4	-1.74	20.00	11	V	4.4
3500	(8+9)-VII-3	-2219	-9.17	32.00	3.5	-2.22	20.00	9.0	V	3.5
3500	(8+9)-I-3	-1518	-6.27	32.00	5.1	-1.52	20.00	13	V	5.1
3500	(8+9)-III-3	-1504	-6.21	32.00	5.1	-1.50	20.00	13	V	5.1
3500	(8+9)-VIII-2	-1526	-6.30	32.00	5.1	-1.53	20.00	13	V	5.1
3500	(8+9)-II-4	-2624	-10.84	32.00	3.0	-2.62	20.00	7.6	V	3.0
3500	(8+9)-VI-2	-1480	-6.11	32.00	5.2	-1.48	20.00	14	V	5.2
Verifiche nella direzione secondaria										
0	1	-625	-0.37	19.20	52	-0.09	12.00	>100	V	52
0	2	-1258	-0.74	28.80	39	-0.18	18.00	>100	V	39
0	3	-1258	-0.74	28.80	39	-0.18	18.00	>100	V	39
0	4	-625	-0.37	25.60	69	-0.09	16.00	>100	V	69
0	5	-625	-0.37	25.60	69	-0.09	16.00	>100	V	69
0	6	-625	-0.37	25.60	69	-0.09	16.00	>100	V	69
0	7	-625	-0.37	25.60	69	-0.09	16.00	>100	V	69
0	(8+9)-V-3	-5634	-3.33	32.00	9.6	-0.80	20.00	25	V	9.6
0	(8+9)-II-3	2493	1.47	32.00	22	0.36	20.00	56	V	22
0	(8+9)-III-3	-3690	-2.18	32.00	15	-0.53	20.00	38	V	15
0	(8+9)-VII-3	-5685	-3.36	32.00	9.5	-0.81	20.00	25	V	9.5
0	(8+9)-VI-3	1894	1.12	32.00	29	0.27	20.00	74	V	29
0	(8+9)-I-4	-6203	-3.66	32.00	8.7	-0.89	20.00	23	V	8.7
0	(8+9)-VI-2	-2762	-1.63	32.00	20	-0.39	20.00	51	V	20
0	(8+9)-II-2	-3361	-1.98	32.00	16	-0.48	20.00	42	V	16

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
0	(8+9)-II-4	-6053	-3.57	32.00	9.0	-0.86	20.00	23	V	9.0
0	(8+9)-VI-1	5783	3.41	32.00	9.4	0.83	20.00	24	V	9.4
0	(8+9)-III-2	2822	1.67	32.00	19	0.40	20.00	50	V	19
0	(8+9)-II-1	5185	3.06	32.00	10	0.74	20.00	27	V	10
0	(8+9)-I-1	5335	3.15	32.00	10	0.76	20.00	26	V	10
0	(8+9)-VI-4	-6651	-3.93	32.00	8.1	-0.95	20.00	21	V	8.1
0	(8+9)-VII-2	4817	2.84	32.00	11	0.69	20.00	29	V	11
0	(8+9)-V-4	-8198	-4.84	32.00	6.6	-1.17	20.00	17	V	6.6
0	(8+9)-V-1	7330	4.33	32.00	7.4	1.05	20.00	19	V	7.4
0	(8+9)-V-2	4766	2.81	32.00	11	0.68	20.00	29	V	11
250	(8+9)-VIII-4	-7266	-4.29	32.00	7.5	-1.04	20.00	19	V	7.5
250	(8+9)-IV-2	-4007	-2.37	32.00	14	-0.57	20.00	35	V	14
250	(8+9)-I-3	-3687	-2.18	32.00	15	-0.53	20.00	38	V	15
250	(8+9)-IV-4	-6684	-3.95	32.00	8.1	-0.95	20.00	21	V	8.1
250	(8+9)-I-2	2819	1.66	32.00	19	0.40	20.00	50	V	19
250	(8+9)-IV-1	5816	3.43	32.00	9.3	0.83	20.00	24	V	9.3
250	(8+9)-VII-4	-8310	-4.91	32.00	6.5	-1.19	20.00	17	V	6.5
250	(8+9)-IV-3	3139	1.85	32.00	17	0.45	20.00	45	V	17
250	(8+9)-III-4	-6369	-3.76	32.00	8.5	-0.91	20.00	22	V	8.5
250	(8+9)-VII-1	7442	4.39	32.00	7.3	1.06	20.00	19	V	7.3
250	(8+9)-VIII-1	6398	3.78	32.00	8.5	0.91	20.00	22	V	8.5
250	(8+9)-VIII-2	-3425	-2.02	32.00	16	-0.49	20.00	41	V	16
250	(8+9)-VIII-3	2557	1.51	32.00	21	0.37	20.00	55	V	21
250	(8+9)-III-1	5501	3.25	32.00	9.9	0.79	20.00	25	V	9.9

Setto 25: origine (213.1,2125.9,328.5), direzione (0.825704,0.564103,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	(8+9)-VIII-4	-6327	-8	-2338	-7.45	-0.36	-14.11	132.00	192.00	192.00	13
0	(8+9)-IV-1	4785	11	1847	5.63	0.47	11.15	132.00	192.00	192.00	9.7
0	(8+9)-VI-1	3101	8	1704	3.65	0.38	10.29	132.00	192.00	192.00	12
0	(8+9)-III-1	4451	-0	1713	5.24	-0.02	10.34	132.00	192.00	192.00	11
0	(8+9)-IV-2	-3580	-11	-1309	-4.22	-0.49	-7.90	132.00	192.00	192.00	23
0	(8+9)-VII-1	6196	-0	2369	7.29	-0.01	14.30	132.00	192.00	192.00	7.7
0	(8+9)-VIII-2	-3057	-11	-1112	-3.60	-0.48	-6.71	132.00	192.00	192.00	26
0	(8+9)-III-3	-2959	9	-1060	-3.48	0.41	-6.40	132.00	192.00	192.00	28
0	(8+9)-VII-3	-4705	9	-1716	-5.54	0.40	-10.36	132.00	192.00	192.00	18
0	(8+9)-III-4	-5469	3	-2007	-6.44	0.13	-12.11	132.00	192.00	192.00	15
0	(8+9)-I-2	2603	-6	868	3.06	-0.28	5.24	132.00	192.00	192.00	19
0	(8+9)-VI-4	-4119	-6	-1998	-4.85	-0.27	-12.06	132.00	192.00	192.00	15
0	(8+9)-I-4	-4807	4	-1905	-5.66	0.16	-11.50	132.00	192.00	192.00	16
0	(8+9)-II-2	-1373	-9	-970	-1.62	-0.39	-5.85	132.00	192.00	192.00	31
0	(8+9)-IV-3	2562	13	1015	3.02	0.60	6.13	132.00	192.00	192.00	17
0	(8+9)-II-4	-3596	-6	-1801	-4.23	-0.26	-10.88	132.00	192.00	192.00	17
0	(8+9)-IV-4	-5803	-8	-2141	-6.83	-0.36	-12.92	132.00	192.00	192.00	14
0	(8+9)-VIII-1	5309	11	2044	6.25	0.47	12.34	132.00	192.00	192.00	8.8
0	(8+9)-V-1	5534	-1	2267	6.51	-0.04	13.69	132.00	192.00	192.00	8.3
0	(8+9)-I-3	-3622	9	-1162	-4.26	0.39	-7.01	132.00	192.00	192.00	26
0	(8+9)-VII-2	3687	-7	1422	4.34	-0.30	8.59	132.00	192.00	192.00	13
0	(8+9)-VIII-3	2038	13	818	2.40	0.59	4.94	132.00	192.00	192.00	21
0	(8+9)-I-1	3788	-1	1611	4.46	-0.05	9.73	132.00	192.00	192.00	12
0	(8+9)-II-1	2577	8	1508	3.03	0.37	9.10	132.00	192.00	192.00	14
0	(8+9)-V-2	4349	-6	1524	5.12	-0.27	9.20	132.00	192.00	192.00	11
0	(8+9)-V-3	-5367	9	-1818	-6.32	0.38	-10.98	132.00	192.00	192.00	17
0	(8+9)-V-4	-6552	3	-2561	-7.71	0.15	-15.46	132.00	192.00	192.00	12
1750	1	2690	1	677	3.17	0.02	4.09	79.20	115.20	115.20	13
1750	2	5519	1	1392	6.50	0.05	8.40	118.80	172.80	172.80	9.7
1750	3	5519	1	1392	6.50	0.05	8.40	118.80	172.80	172.80	9.7
1750	4	2690	1	677	3.17	0.02	4.09	105.60	153.60	153.60	18
1750	5	2690	1	677	3.17	0.02	4.09	105.60	153.60	153.60	18
1750	6	2690	1	677	3.17	0.02	4.09	105.60	153.60	153.60	18
1750	7	2690	1	677	3.17	0.02	4.09	105.60	153.60	153.60	18

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
1750	(8+9)-VI-2	2493	-2	335	2.93	-0.08	2.02	132.00	192.00	192.00	30
3500	(8+9)-VII-4	3768	1	1680	4.44	0.06	10.14	132.00	192.00	192.00	12
3500	(8+9)-II-3	-1883	14	-1261	-2.22	0.61	-7.61	132.00	192.00	192.00	23
3500	(8+9)-III-2	-1643	-8	-1363	-1.93	-0.35	-8.23	132.00	192.00	192.00	22
3500	(8+9)-VI-3	-1554	14	-1092	-1.83	0.62	-6.59	132.00	192.00	192.00	27
Verifiche nella direzione secondaria											
0	1	-7419	3	-2555	-4.38	0.11	-2.59	79.20	115.20	115.20	40
0	2	-15215	7	-5229	-8.98	0.22	-5.29	118.80	172.80	172.80	29
0	3	-15215	7	-5229	-8.98	0.22	-5.29	118.80	172.80	172.80	29
0	4	-7419	3	-2555	-4.38	0.11	-2.59	105.60	153.60	153.60	54
0	5	-7419	3	-2555	-4.38	0.11	-2.59	105.60	153.60	153.60	54
0	6	-7419	3	-2555	-4.38	0.11	-2.59	105.60	153.60	153.60	54
0	7	-7419	3	-2555	-4.38	0.11	-2.59	105.60	153.60	153.60	54
0	(8+9)-VIII-4	-4285	4	-7516	-2.53	0.13	-7.61	132.00	192.00	192.00	25
0	(8+9)-V-2	-5114	14	3498	-3.02	0.49	3.54	132.00	192.00	192.00	47
0	(8+9)-VI-4	-2697	42	-4428	-1.59	1.40	-4.48	132.00	192.00	192.00	33
0	(8+9)-IV-2	-4606	4	-4700	-2.72	0.13	-4.76	132.00	192.00	192.00	39
0	(8+9)-III-3	-4910	2	-4366	-2.90	0.07	-4.42	132.00	192.00	192.00	42
0	(8+9)-I-4	-4045	14	-5887	-2.39	0.49	-5.96	132.00	192.00	192.00	30
0	(8+9)-III-4	-4521	3	-6813	-2.67	0.11	-6.89	132.00	192.00	192.00	27
0	(8+9)-II-2	-3017	41	-1612	-1.78	1.40	-1.63	132.00	192.00	192.00	63
0	(8+9)-VI-3	-7170	-37	-2446	-4.23	-1.26	-2.47	132.00	192.00	192.00	50
0	(8+9)-II-4	-2769	42	-3905	-1.63	1.41	-3.95	132.00	192.00	192.00	36
0	(8+9)-V-4	-3804	14	-7628	-2.25	0.46	-7.72	132.00	192.00	192.00	23
0	(8+9)-VII-4	-4280	2	-8555	-2.53	0.08	-8.66	132.00	192.00	192.00	22
0	(8+9)-VII-3	-4669	1	-6107	-2.76	0.05	-6.18	132.00	192.00	192.00	31
0	(8+9)-VIII-2	-4678	4	-4178	-2.76	0.14	-4.23	132.00	192.00	192.00	44
0	(8+9)-V-3	-5146	-10	-7034	-3.04	-0.33	-7.12	132.00	192.00	192.00	26
0	(8+9)-IV-4	-4358	4	-6993	-2.57	0.14	-7.08	132.00	192.00	192.00	26
0	(8+9)-I-3	-5387	-9	-5292	-3.18	-0.31	-5.36	132.00	192.00	192.00	34
585	(8+9)-V-1	-4497	8	5254	-2.65	0.26	5.32	132.00	192.00	192.00	34
585	(8+9)-I-2	-4290	-8	2041	-2.53	-0.26	2.07	132.00	192.00	192.00	81
585	(8+9)-VII-2	-4369	-2	3393	-2.58	-0.06	3.43	132.00	192.00	192.00	54
585	(8+9)-IV-3	-4406	8	2537	-2.60	0.27	2.57	132.00	192.00	192.00	67
585	(8+9)-III-1	-4418	2	3902	-2.61	0.07	3.95	132.00	192.00	192.00	47
585	(8+9)-VI-1	-4559	26	5018	-2.69	0.88	5.08	132.00	192.00	192.00	32
585	(8+9)-II-3	-4480	27	3129	-2.64	0.91	3.17	132.00	192.00	192.00	47
585	(8+9)-VII-1	-4475	2	5076	-2.64	0.07	5.14	132.00	192.00	192.00	37
585	(8+9)-I-1	-4440	8	4080	-2.62	0.26	4.13	132.00	192.00	192.00	43
585	(8+9)-VI-2	-4058	-25	-1778	-2.40	-0.83	-1.80	132.00	192.00	192.00	72
585	(8+9)-III-2	-4312	-2	2219	-2.55	-0.07	2.25	132.00	192.00	192.00	82
585	(8+9)-VIII-1	-4486	7	4426	-2.65	0.25	4.48	132.00	192.00	192.00	40
585	(8+9)-II-1	-4542	26	4665	-2.68	0.88	4.72	132.00	192.00	192.00	34
585	(8+9)-VIII-3	-4389	8	2185	-2.59	0.27	2.21	132.00	192.00	192.00	76
585	(8+9)-IV-1	-4469	7	4074	-2.64	0.25	4.12	132.00	192.00	192.00	44

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Ty kg	τ_d kg/cm ²	fvd kg/cm ²	RS	Cs
0	1	6	0.01	3.84	Si	>100
0	2	13	0.01	5.76	Si	>100
0	3	13	0.01	5.76	Si	>100
0	4	6	0.01	5.12	Si	>100
0	5	6	0.01	5.12	Si	>100
0	6	6	0.01	5.12	Si	>100
0	7	6	0.01	5.12	Si	>100
0	(8+9)-IV-3	3	0.00	6.40	Si	>100
0	(8+9)-VII-4	5	0.00	6.40	Si	>100
0	(8+9)-III-1	4	0.00	6.40	Si	>100
0	(8+9)-VIII-3	4	0.00	6.40	Si	>100
0	(8+9)-II-2	4	0.00	6.40	Si	>100
0	(8+9)-VIII-1	3	0.00	6.40	Si	>100
0	(8+9)-III-3	4	0.00	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
0	(8+9)-IV-4	5	0.00	6.40	Si	>100
0	(8+9)-VIII-2	5	0.00	6.40	Si	>100
0	(8+9)-VIII-4	5	0.00	6.40	Si	>100
0	(8+9)-VII-3	5	0.00	6.40	Si	>100
0	(8+9)-III-4	5	0.00	6.40	Si	>100
0	(8+9)-IV-1	3	0.00	6.40	Si	>100
0	(8+9)-IV-2	5	0.00	6.40	Si	>100
1750	(8+9)-VII-2	-4	0.00	6.40	Si	>100
1750	(8+9)-VII-1	-4	0.00	6.40	Si	>100
3500	(8+9)-I-1	-46	0.04	6.40	Si	>100
3500	(8+9)-VI-4	163	0.14	6.40	Si	46
3500	(8+9)-II-4	163	0.14	6.40	Si	46
3500	(8+9)-II-3	-159	0.14	6.40	Si	47
3500	(8+9)-V-3	-46	0.04	6.40	Si	>100
3500	(8+9)-II-2	163	0.14	6.40	Si	46
3500	(8+9)-VI-1	-159	0.14	6.40	Si	47
3500	(8+9)-II-1	-159	0.14	6.40	Si	47
3500	(8+9)-V-1	-47	0.04	6.40	Si	>100
3500	(8+9)-V-4	51	0.04	6.40	Si	>100
3500	(8+9)-VI-2	163	0.14	6.40	Si	46
3500	(8+9)-V-2	50	0.04	6.40	Si	>100
3500	(8+9)-I-4	51	0.04	6.40	Si	>100
3500	(8+9)-I-3	-46	0.04	6.40	Si	>100
3500	(8+9)-I-2	50	0.04	6.40	Si	>100
3500	(8+9)-VI-3	-159	0.14	6.40	Si	47
Verifiche nella direzione secondaria						
0	(8+9)-V-2	-256	0.14	6.40	Si	46
0	(8+9)-VII-3	2	0.00	6.40	Si	>100
0	(8+9)-II-3	837	0.46	6.40	Si	14
0	(8+9)-II-4	-838	0.46	6.40	Si	14
0	(8+9)-VII-4	3	0.00	6.40	Si	>100
0	(8+9)-III-1	-4	0.00	6.40	Si	>100
0	(8+9)-VII-1	-5	0.00	6.40	Si	>100
0	(8+9)-VI-3	838	0.46	6.40	Si	14
0	(8+9)-I-1	248	0.13	6.40	Si	47
0	(8+9)-VI-2	-840	0.46	6.40	Si	14
0	(8+9)-I-3	253	0.14	6.40	Si	46
0	(8+9)-VI-1	835	0.46	6.40	Si	14
0	(8+9)-II-1	836	0.46	6.40	Si	14
0	(8+9)-IV-1	-3	0.00	6.40	Si	>100
0	(8+9)-VIII-1	-4	0.00	6.40	Si	>100
0	(8+9)-V-4	-249	0.14	6.40	Si	47
0	(8+9)-VI-4	-838	0.46	6.40	Si	14
0	(8+9)-I-4	-250	0.14	6.40	Si	47
0	(8+9)-II-2	-840	0.46	6.40	Si	14
0	(8+9)-V-3	254	0.14	6.40	Si	46
0	(8+9)-I-2	-255	0.14	6.40	Si	46
0	(8+9)-V-1	247	0.13	6.40	Si	48
585	(8+9)-VIII-3	-2	0.00	6.40	Si	>100
585	(8+9)-IV-3	-2	0.00	6.40	Si	>100
1170	1	-4	0.00	3.84	Si	>100
1170	2	-8	0.00	5.76	Si	>100
1170	3	-8	0.00	5.76	Si	>100
1170	4	-4	0.00	5.12	Si	>100
1170	5	-4	0.00	5.12	Si	>100
1170	6	-4	0.00	5.12	Si	>100
1170	7	-4	0.00	5.12	Si	>100
1170	(8+9)-VIII-4	-3	0.00	6.40	Si	>100
1170	(8+9)-VII-2	-5	0.00	6.40	Si	>100
1170	(8+9)-III-2	-4	0.00	6.40	Si	>100
1170	(8+9)-III-3	-1	0.00	6.40	Si	>100
1170	(8+9)-III-4	-2	0.00	6.40	Si	>100
1170	(8+9)-VIII-2	-4	0.00	6.40	Si	>100
1170	(8+9)-IV-2	-4	0.00	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
1170	(8+9)-IV-4	-4	0.00	6.40	Si	>100

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	1	-3970	-7.01	19.20	2.7	-1.70	12.00	7.1	V	2.7
0	2	-8176	-14.44	28.80	2.0	-3.49	18.00	5.2	V	2.0
0	3	-8176	-14.44	28.80	2.0	-3.49	18.00	5.2	V	2.0
0	4	-3970	-7.01	25.60	3.7	-1.70	16.00	9.4	V	3.7
0	5	-3970	-7.01	25.60	3.7	-1.70	16.00	9.4	V	3.7
0	6	-3970	-7.01	25.60	3.7	-1.70	16.00	9.4	V	3.7
0	7	-3970	-7.01	25.60	3.7	-1.70	16.00	9.4	V	3.7
0	(8+9)-IV-4	-5110	-9.02	32.00	3.5	-2.18	20.00	9.2	V	3.5
0	(8+9)-VII-4	-5758	-10.17	32.00	3.1	-2.46	20.00	8.1	V	3.1
0	(8+9)-VI-4	-4029	-7.12	32.00	4.5	-1.72	20.00	12	V	4.5
0	(8+9)-VIII-2	-3868	-6.83	32.00	4.7	-1.65	20.00	12	V	4.7
0	(8+9)-VI-2	-2556	-4.51	32.00	7.1	-1.09	20.00	18	V	7.1
0	(8+9)-I-4	-4592	-8.11	32.00	3.9	-1.96	20.00	10	V	3.9
0	(8+9)-III-3	-3868	-6.83	32.00	4.7	-1.65	20.00	12	V	4.7
0	(8+9)-II-2	-2787	-4.92	32.00	6.5	-1.19	20.00	17	V	6.5
0	(8+9)-III-4	-4985	-8.80	32.00	3.6	-2.13	20.00	9.4	V	3.6
0	(8+9)-VIII-4	-5342	-9.43	32.00	3.4	-2.28	20.00	8.8	V	3.4
0	(8+9)-VII-3	-4640	-8.19	32.00	3.9	-1.98	20.00	10	V	3.9
0	(8+9)-I-3	-4262	-7.53	32.00	4.3	-1.82	20.00	11	V	4.3
0	(8+9)-V-4	-5364	-9.47	32.00	3.4	-2.29	20.00	8.7	V	3.4
0	(8+9)-IV-2	-4100	-7.24	32.00	4.4	-1.75	20.00	11	V	4.4
0	(8+9)-V-3	-5034	-8.89	32.00	3.6	-2.15	20.00	9.3	V	3.6
0	(8+9)-II-4	-3798	-6.71	32.00	4.8	-1.62	20.00	12	V	4.8
3500	(8+9)-V-1	5273	9.31	32.00	3.4	2.25	20.00	8.9	V	3.4
3500	(8+9)-VIII-1	4936	8.72	32.00	3.7	2.11	20.00	9.5	V	3.7
3500	(8+9)-V-2	4202	7.42	32.00	4.3	1.80	20.00	11	V	4.3
3500	(8+9)-I-2	3476	6.14	32.00	5.2	1.49	20.00	13	V	5.2
3500	(8+9)-IV-1	4718	8.33	32.00	3.8	2.02	20.00	9.9	V	3.8
3500	(8+9)-VIII-3	3554	6.28	32.00	5.1	1.52	20.00	13	V	5.1
3500	(8+9)-III-2	3468	6.12	32.00	5.2	1.48	20.00	13	V	5.2
3500	(8+9)-I-1	4547	8.03	32.00	4.0	1.94	20.00	10	V	4.0
3500	(8+9)-III-1	4555	8.04	32.00	4.0	1.95	20.00	10	V	4.0
3500	(8+9)-VII-2	4194	7.41	32.00	4.3	1.79	20.00	11	V	4.3
3500	(8+9)-II-3	3746	6.62	32.00	4.8	1.60	20.00	12	V	4.8
3500	(8+9)-II-1	4692	8.29	32.00	3.9	2.01	20.00	10.0	V	3.9
3500	(8+9)-IV-3	3772	6.66	32.00	4.8	1.61	20.00	12	V	4.8
3500	(8+9)-VI-1	4910	8.67	32.00	3.7	2.10	20.00	9.5	V	3.7
3500	(8+9)-VI-3	3528	6.23	32.00	5.1	1.51	20.00	13	V	5.1
3500	(8+9)-VII-1	5280	9.32	32.00	3.4	2.26	20.00	8.9	V	3.4
Verifiche nella direzione secondaria										
585	(8+9)-I-2	5219	3.08	32.00	10	0.75	20.00	27	V	10
585	(8+9)-VIII-2	-3808	-2.25	32.00	14	-0.54	20.00	37	V	14
585	(8+9)-V-3	-7100	-4.19	32.00	7.6	-1.01	20.00	20	V	7.6
585	(8+9)-V-2	7899	4.66	32.00	6.9	1.13	20.00	18	V	6.9
585	(8+9)-IV-2	-4612	-2.72	32.00	12	-0.66	20.00	30	V	12
585	(8+9)-I-3	-4420	-2.61	32.00	12	-0.63	20.00	32	V	12
1170	1	712	0.42	19.20	46	0.10	12.00	>100	V	46
1170	2	1478	0.87	28.80	33	0.21	18.00	85	V	33
1170	3	1478	0.87	28.80	33	0.21	18.00	85	V	33
1170	4	712	0.42	25.60	61	0.10	16.00	>100	V	61
1170	5	712	0.42	25.60	61	0.10	16.00	>100	V	61
1170	6	712	0.42	25.60	61	0.10	16.00	>100	V	61
1170	7	712	0.42	25.60	61	0.10	16.00	>100	V	61
1170	(8+9)-VIII-4	-8795	-5.19	32.00	6.2	-1.26	20.00	16	V	6.2
1170	(8+9)-V-1	11125	6.57	32.00	4.9	1.59	20.00	13	V	4.9
1170	(8+9)-I-1	8429	4.98	32.00	6.4	1.20	20.00	17	V	6.4
1170	(8+9)-VI-1	10031	5.92	32.00	5.4	1.43	20.00	14	V	5.4
1170	(8+9)-III-1	8353	4.93	32.00	6.5	1.19	20.00	17	V	6.5

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
1170	(8+9)-VI-2	-3925	-2.32	32.00	14	-0.56	20.00	36	V	14
1170	(8+9)-III-3	-3338	-1.97	32.00	16	-0.48	20.00	42	V	16
1170	(8+9)-VI-3	4906	2.90	32.00	11	0.70	20.00	29	V	11
1170	(8+9)-IV-1	8967	5.29	32.00	6.0	1.28	20.00	16	V	6.0
1170	(8+9)-VI-4	-9050	-5.34	32.00	6.0	-1.29	20.00	15	V	6.0
1170	(8+9)-IV-3	5460	3.22	32.00	9.9	0.78	20.00	26	V	9.9
1170	(8+9)-VII-1	11049	6.52	32.00	4.9	1.58	20.00	13	V	4.9
1170	(8+9)-II-3	5715	3.37	32.00	9.5	0.82	20.00	24	V	9.5
1170	(8+9)-VII-2	7015	4.14	32.00	7.7	1.00	20.00	20	V	7.7
1170	(8+9)-II-1	9222	5.44	32.00	5.9	1.32	20.00	15	V	5.9
1170	(8+9)-VII-3	-6034	-3.56	32.00	9.0	-0.86	20.00	23	V	9.0
1170	(8+9)-III-2	4319	2.55	32.00	13	0.62	20.00	32	V	13
1170	(8+9)-VII-4	-10068	-5.94	32.00	5.4	-1.44	20.00	14	V	5.4
1170	(8+9)-II-2	-4734	-2.79	32.00	11	-0.68	20.00	30	V	11
1170	(8+9)-V-4	-10144	-5.99	32.00	5.3	-1.45	20.00	14	V	5.3
1170	(8+9)-III-4	-7372	-4.35	32.00	7.4	-1.05	20.00	19	V	7.4
1170	(8+9)-IV-4	-7986	-4.71	32.00	6.8	-1.14	20.00	18	V	6.8
1170	(8+9)-VIII-1	9776	5.77	32.00	5.5	1.40	20.00	14	V	5.5
1170	(8+9)-I-4	-7448	-4.40	32.00	7.3	-1.06	20.00	19	V	7.3
1170	(8+9)-VIII-3	4651	2.75	32.00	12	0.66	20.00	30	V	12
1170	(8+9)-II-4	-8241	-4.86	32.00	6.6	-1.18	20.00	17	V	6.6

Setto 26: origine (708.6,2464.3,25.0), direzione (0.825704,0.564103,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_N	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	2	-656	1	153	-1.81	0.07	5.06	118.80	172.80	172.80	34
0	3	-656	1	153	-1.81	0.07	5.06	118.80	172.80	172.80	34
0	(8+9)-III-3	1089	-1	-244	3.00	-0.07	-8.06	132.00	192.00	192.00	15
0	(8+9)-I-3	2413	-1	-481	6.65	-0.06	-15.91	132.00	192.00	192.00	7.5
0	(8+9)-V-4	2036	-0	-516	5.61	-0.02	-17.07	132.00	192.00	192.00	7.6
0	(8+9)-VII-4	3360	-0	-754	9.26	-0.02	-24.92	132.00	192.00	192.00	5.0
0	(8+9)-IV-4	2560	1	-577	7.05	0.13	-19.06	132.00	192.00	192.00	6.5
0	(8+9)-VIII-4	2847	1	-641	7.84	0.12	-21.18	132.00	192.00	192.00	5.9
0	(8+9)-III-4	2401	0	-540	6.61	0.01	-17.86	132.00	192.00	192.00	7.0
0	(8+9)-V-3	3371	-1	-695	9.29	-0.09	-22.97	132.00	192.00	192.00	5.3
0	(8+9)-I-4	1078	0	-303	2.97	0.00	-10.02	132.00	192.00	192.00	13
0	(8+9)-VII-3	2048	-1	-457	5.64	-0.09	-15.12	132.00	192.00	192.00	8.2
1750	1	370	-0	-31	1.02	-0.01	-1.03	79.20	115.20	115.20	46
1750	4	370	-0	-31	1.02	-0.01	-1.03	105.60	153.60	153.60	61
1750	5	370	-0	-31	1.02	-0.01	-1.03	105.60	153.60	153.60	61
1750	6	370	-0	-31	1.02	-0.01	-1.03	105.60	153.60	153.60	61
1750	7	370	-0	-31	1.02	-0.01	-1.03	105.60	153.60	153.60	61
3500	(8+9)-VI-1	-1077	4	359	-2.97	0.44	11.85	132.00	192.00	192.00	16
3500	(8+9)-VIII-2	-1142	-6	411	-3.15	-0.66	13.60	132.00	192.00	192.00	13
3500	(8+9)-III-2	1554	-5	-297	4.28	-0.50	-9.83	132.00	192.00	192.00	12
3500	(8+9)-VIII-3	1582	7	-447	4.36	0.69	-14.78	132.00	192.00	192.00	8.8
3500	(8+9)-IV-2	-1443	-6	485	-3.98	-0.59	16.04	132.00	192.00	192.00	11
3500	(8+9)-I-1	1573	-2	-313	4.33	-0.17	-10.36	132.00	192.00	192.00	11
3500	(8+9)-III-1	2914	-2	-684	8.03	-0.20	-22.63	132.00	192.00	192.00	5.6
3500	(8+9)-V-1	2576	-4	-560	7.10	-0.39	-18.50	132.00	192.00	192.00	6.6
3500	(8+9)-VII-1	3917	-4	-931	10.79	-0.41	-30.77	132.00	192.00	192.00	4.1
3500	(8+9)-V-2	3897	-7	-915	10.74	-0.74	-30.25	132.00	192.00	192.00	4.1
3500	(8+9)-VII-2	2556	-7	-544	7.04	-0.71	-17.98	132.00	192.00	192.00	6.6
3500	(8+9)-II-3	-2586	7	716	-7.12	0.72	23.68	132.00	192.00	192.00	7.8
3500	(8+9)-II-1	-1378	5	432	-3.80	0.50	14.30	132.00	192.00	192.00	13
3500	(8+9)-VI-2	3326	-7	-826	9.16	-0.75	-27.31	132.00	192.00	192.00	4.6
3500	(8+9)-I-2	2894	-5	-669	7.97	-0.53	-22.10	132.00	192.00	192.00	5.6
3500	(8+9)-II-2	3025	-7	-752	8.33	-0.68	-24.86	132.00	192.00	192.00	5.1
3500	(8+9)-VI-3	-2887	8	790	-7.95	0.78	26.12	132.00	192.00	192.00	7.0
3500	(8+9)-II-4	1817	-4	-468	5.00	-0.46	-15.48	132.00	192.00	192.00	8.3
3500	(8+9)-VIII-1	3392	3	-879	9.34	0.34	-29.05	132.00	192.00	192.00	4.5
3500	(8+9)-IV-1	3091	4	-805	8.52	0.41	-26.61	132.00	192.00	192.00	4.9

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
3500	(8+9)-IV-3	1882	6	-521	5.19	0.63	-17.22	132.00	192.00	192.00	7.6
3500	(8+9)-VI-4	1516	-4	-394	4.18	-0.40	-13.04	132.00	192.00	192.00	9.8
Verifiche nella direzione secondaria											
0	(8+9)-V-2	-1190	127	-17490	-0.70	4.28	-17.70	132.00	192.00	192.00	8.7
0	(8+9)-I-2	-1289	111	-11810	-0.76	3.76	-11.95	132.00	192.00	192.00	12
0	(8+9)-VI-4	4970	292	5071	2.93	9.87	5.13	132.00	192.00	192.00	10.0
0	(8+9)-I-3	-5262	-99	10139	-3.11	-3.36	10.26	132.00	192.00	192.00	14
0	(8+9)-I-2	4757	311	-5072	2.81	10.52	-5.13	132.00	192.00	192.00	9.7
0	(8+9)-I-4	-378	78	10640	-0.22	2.64	10.77	132.00	192.00	192.00	14
0	(8+9)-V-4	-478	63	16320	-0.28	2.12	16.52	132.00	192.00	192.00	10
0	(8+9)-II-1	-11551	-285	-5038	-6.82	-9.63	-5.10	132.00	192.00	192.00	13
0	(8+9)-I-1	-6173	-66	-12311	-3.64	-2.24	-12.46	132.00	192.00	192.00	13
0	(8+9)-VI-1	-11521	-280	-6742	-6.80	-9.47	-6.82	132.00	192.00	192.00	12
0	(8+9)-V-3	-5362	-115	15819	-3.17	-3.88	16.01	132.00	192.00	192.00	9.6
0	(8+9)-VI-3	-11308	-300	3401	-6.68	-10.12	3.44	132.00	192.00	192.00	14
0	(8+9)-II-2	4727	307	-3368	2.79	10.36	-3.41	132.00	192.00	192.00	11
0	(8+9)-II-3	-11278	-295	1697	-6.66	-9.97	1.72	132.00	192.00	192.00	16
0	(8+9)-II-4	5000	297	3367	2.95	10.03	3.41	132.00	192.00	192.00	11
250	1	-4670	7	-1406	-2.76	0.24	-1.42	79.20	115.20	115.20	67
250	2	-9366	14	-3048	-5.53	0.47	-3.08	118.80	172.80	172.80	46
250	3	-9366	14	-3048	-5.53	0.47	-3.08	118.80	172.80	172.80	46
250	4	-4670	7	-1406	-2.76	0.24	-1.42	105.60	153.60	153.60	90
250	5	-4670	7	-1406	-2.76	0.24	-1.42	105.60	153.60	153.60	90
250	6	-4670	7	-1406	-2.76	0.24	-1.42	105.60	153.60	153.60	90
250	7	-4670	7	-1406	-2.76	0.24	-1.42	105.60	153.60	153.60	90
250	(8+9)-VIII-4	-2315	107	17970	-1.37	3.62	18.19	132.00	192.00	192.00	8.8
250	(8+9)-III-2	-3454	57	-9246	-2.04	1.94	-9.36	132.00	192.00	192.00	17
250	(8+9)-VII-1	-3849	-3	-23466	-2.27	-0.10	-23.75	132.00	192.00	192.00	8.0
250	(8+9)-V-1	-6044	14	-19443	-3.57	0.49	-19.68	132.00	192.00	192.00	9.5
250	(8+9)-VII-2	-3355	63	-15436	-1.98	2.12	-15.62	132.00	192.00	192.00	11
250	(8+9)-IV-4	-2285	109	16113	-1.35	3.68	16.31	132.00	192.00	192.00	9.6
250	(8+9)-VII-3	-3137	-53	13518	-1.85	-1.78	13.68	132.00	192.00	192.00	12
250	(8+9)-IV-2	-2558	121	8732	-1.51	4.07	8.84	132.00	192.00	192.00	15
250	(8+9)-VII-4	-2642	13	21547	-1.56	0.44	21.80	132.00	192.00	192.00	8.6
250	(8+9)-III-1	-3949	-8	-17276	-2.33	-0.28	-17.48	132.00	192.00	192.00	11
250	(8+9)-IV-3	-3933	-111	-10651	-2.32	-3.73	-10.78	132.00	192.00	192.00	13
250	(8+9)-IV-1	-4206	-99	-18032	-2.48	-3.34	-18.25	132.00	192.00	192.00	8.9
250	(8+9)-III-3	-3037	-47	7328	-1.79	-1.60	7.42	132.00	192.00	192.00	21
250	(8+9)-VIII-1	-4176	-97	-19889	-2.47	-3.28	-20.13	132.00	192.00	192.00	8.2
250	(8+9)-VIII-2	-2529	122	6875	-1.49	4.13	6.96	132.00	192.00	192.00	17
250	(8+9)-VIII-3	-3963	-112	-8794	-2.34	-3.79	-8.90	132.00	192.00	192.00	15
250	(8+9)-III-4	-2543	18	15357	-1.50	0.62	15.54	132.00	192.00	192.00	12

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
0	1	-3	0.01	3.84	Si	>100
0	2	-6	0.01	5.76	Si	>100
0	3	-6	0.01	5.76	Si	>100
0	4	-3	0.01	5.12	Si	>100
0	5	-3	0.01	5.12	Si	>100
0	6	-3	0.01	5.12	Si	>100
0	7	-3	0.01	5.12	Si	>100
0	(8+9)-V-1	-6	0.01	6.40	Si	>100
0	(8+9)-I-1	-3	0.01	6.40	Si	>100
0	(8+9)-VII-1	-9	0.02	6.40	Si	>100
0	(8+9)-I-2	-7	0.01	6.40	Si	>100
0	(8+9)-III-2	-4	0.01	6.40	Si	>100
0	(8+9)-I-4	-1	0.00	6.40	Si	>100
0	(8+9)-VI-4	-8	0.02	6.40	Si	>100
0	(8+9)-II-2	-10	0.02	6.40	Si	>100
0	(8+9)-VI-3	7	0.01	6.40	Si	>100
0	(8+9)-II-1	5	0.01	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
0	(8+9)-VII-2	-7	0.01	6.40	Si	>100
0	(8+9)-VII-3	3	0.01	6.40	Si	>100
0	(8+9)-VI-2	-11	0.02	6.40	Si	>100
0	(8+9)-II-4	-8	0.02	6.40	Si	>100
0	(8+9)-V-2	-10	0.02	6.40	Si	>100
3500	(8+9)-VI-1	-4	0.01	6.40	Si	>100
3500	(8+9)-VII-4	-6	0.01	6.40	Si	>100
3500	(8+9)-IV-4	-5	0.01	6.40	Si	>100
3500	(8+9)-VIII-1	8	0.02	6.40	Si	>100
3500	(8+9)-V-3	-6	0.01	6.40	Si	>100
3500	(8+9)-VIII-2	-2	0.00	6.40	Si	>100
3500	(8+9)-IV-2	-3	0.01	6.40	Si	>100
3500	(8+9)-VIII-3	5	0.01	6.40	Si	>100
3500	(8+9)-III-4	-3	0.01	6.40	Si	>100
3500	(8+9)-VIII-4	-5	0.01	6.40	Si	>100
3500	(8+9)-III-1	6	0.01	6.40	Si	>100
3500	(8+9)-I-3	-4	0.01	6.40	Si	>100
3500	(8+9)-IV-3	5	0.01	6.40	Si	>100
3500	(8+9)-V-4	-2	0.00	6.40	Si	>100
3500	(8+9)-IV-1	7	0.01	6.40	Si	>100
3500	(8+9)-III-3	-0	0.00	6.40	Si	>100
3500	(8+9)-II-3	-6	0.01	6.40	Si	>100
Verifiche nella direzione secondaria						
0	(8+9)-I-1	171	0.09	6.40	Si	69
0	(8+9)-VIII-2	-8	0.00	6.40	Si	>100
0	(8+9)-V-4	-172	0.09	6.40	Si	68
0	(8+9)-V-1	166	0.09	6.40	Si	71
0	(8+9)-IV-2	-7	0.00	6.40	Si	>100
0	(8+9)-I-4	-177	0.10	6.40	Si	66
250	1	-5	0.00	3.84	Si	>100
250	2	-9	0.01	5.76	Si	>100
250	3	-9	0.01	5.76	Si	>100
250	4	-5	0.00	5.12	Si	>100
250	5	-5	0.00	5.12	Si	>100
250	6	-5	0.00	5.12	Si	>100
250	7	-5	0.00	5.12	Si	>100
250	(8+9)-I-3	180	0.10	6.40	Si	65
250	(8+9)-II-3	591	0.32	6.40	Si	20
250	(8+9)-VI-3	593	0.32	6.40	Si	20
250	(8+9)-VI-4	-592	0.32	6.40	Si	20
250	(8+9)-VI-1	585	0.32	6.40	Si	20
250	(8+9)-II-1	587	0.32	6.40	Si	20
250	(8+9)-III-3	2	0.00	6.40	Si	>100
250	(8+9)-V-2	-193	0.11	6.40	Si	61
250	(8+9)-VII-3	9	0.00	6.40	Si	>100
250	(8+9)-V-3	187	0.10	6.40	Si	63
250	(8+9)-I-2	-187	0.10	6.40	Si	63
250	(8+9)-II-2	-597	0.33	6.40	Si	20
250	(8+9)-III-2	-9	0.00	6.40	Si	>100
250	(8+9)-II-4	-594	0.32	6.40	Si	20
250	(8+9)-VII-2	-15	0.01	6.40	Si	>100
250	(8+9)-VI-2	-599	0.33	6.40	Si	20
500	(8+9)-VIII-4	8	0.00	6.40	Si	>100
500	(8+9)-III-1	-12	0.01	6.40	Si	>100
500	(8+9)-VII-4	12	0.01	6.40	Si	>100
500	(8+9)-IV-3	-8	0.00	6.40	Si	>100
500	(8+9)-IV-1	-12	0.01	6.40	Si	>100
500	(8+9)-VII-1	-18	0.01	6.40	Si	>100
500	(8+9)-VIII-1	-14	0.01	6.40	Si	>100
500	(8+9)-III-4	6	0.00	6.40	Si	>100
500	(8+9)-VIII-3	-6	0.00	6.40	Si	>100
500	(8+9)-IV-4	7	0.00	6.40	Si	>100

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	1	1386	5.73	19.20	3.4	1.39	12.00	8.7	V	3.4
0	2	2837	11.72	28.80	2.5	2.84	18.00	6.3	V	2.5
0	3	2837	11.72	28.80	2.5	2.84	18.00	6.3	V	2.5
0	4	1386	5.73	25.60	4.5	1.39	16.00	12	V	4.5
0	5	1386	5.73	25.60	4.5	1.39	16.00	12	V	4.5
0	6	1386	5.73	25.60	4.5	1.39	16.00	12	V	4.5
0	7	1386	5.73	25.60	4.5	1.39	16.00	12	V	4.5
0	(8+9)-V-1	5370	22.19	32.00	1.4	5.37	20.00	3.7	V	1.4
0	(8+9)-VI-1	4725	19.52	32.00	1.6	4.72	20.00	4.2	V	1.6
0	(8+9)-I-2	2615	10.81	32.00	3.0	2.62	20.00	7.6	V	3.0
0	(8+9)-V-4	-3453	-14.27	32.00	2.2	-3.45	20.00	5.8	V	2.2
0	(8+9)-VII-1	5391	22.28	32.00	1.4	5.39	20.00	3.7	V	1.4
0	(8+9)-I-4	-2309	-9.54	32.00	3.4	-2.31	20.00	8.7	V	3.4
0	(8+9)-IV-1	4451	18.39	32.00	1.7	4.45	20.00	4.5	V	1.7
0	(8+9)-VIII-3	2630	10.87	32.00	2.9	2.63	20.00	7.6	V	2.9
0	(8+9)-VI-4	-2808	-11.60	32.00	2.8	-2.81	20.00	7.1	V	2.8
0	(8+9)-II-4	-2464	-10.18	32.00	3.1	-2.46	20.00	8.1	V	3.1
0	(8+9)-IV-3	2973	12.29	32.00	2.6	2.97	20.00	6.7	V	2.6
0	(8+9)-II-1	4382	18.11	32.00	1.8	4.38	20.00	4.6	V	1.8
0	(8+9)-VIII-1	4794	19.81	32.00	1.6	4.79	20.00	4.2	V	1.6
0	(8+9)-III-1	4247	17.55	32.00	1.8	4.25	20.00	4.7	V	1.8
0	(8+9)-VII-2	3739	15.45	32.00	2.1	3.74	20.00	5.3	V	2.1
0	(8+9)-III-2	2595	10.72	32.00	3.0	2.59	20.00	7.7	V	3.0
0	(8+9)-I-1	4226	17.46	32.00	1.8	4.23	20.00	4.7	V	1.8
0	(8+9)-V-2	3760	15.54	32.00	2.1	3.76	20.00	5.3	V	2.1
3500	(8+9)-VI-2	2912	12.03	32.00	2.7	2.91	20.00	6.9	V	2.7
3500	(8+9)-VIII-2	-1810	-7.48	32.00	4.3	-1.81	20.00	11	V	4.3
3500	(8+9)-V-3	-4290	-17.73	32.00	1.8	-4.29	20.00	4.7	V	1.8
3500	(8+9)-II-2	2587	10.69	32.00	3.0	2.59	20.00	7.7	V	3.0
3500	(8+9)-IV-4	-3336	-13.79	32.00	2.3	-3.34	20.00	6.0	V	2.3
3500	(8+9)-VIII-4	-3661	-15.13	32.00	2.1	-3.66	20.00	5.5	V	2.1
3500	(8+9)-IV-2	-2135	-8.82	32.00	3.6	-2.13	20.00	9.4	V	3.6
3500	(8+9)-III-3	-1791	-7.40	32.00	4.3	-1.79	20.00	11	V	4.3
3500	(8+9)-VII-3	-2873	-11.87	32.00	2.7	-2.87	20.00	7.0	V	2.7
3500	(8+9)-VII-4	-4233	-17.49	32.00	1.8	-4.23	20.00	4.7	V	1.8
3500	(8+9)-II-3	-3524	-14.56	32.00	2.2	-3.52	20.00	5.7	V	2.2
3500	(8+9)-I-3	-3208	-13.25	32.00	2.4	-3.21	20.00	6.2	V	2.4
3500	(8+9)-VI-3	-3849	-15.91	32.00	2.0	-3.85	20.00	5.2	V	2.0
3500	(8+9)-III-4	-3151	-13.02	32.00	2.5	-3.15	20.00	6.3	V	2.5
Verifiche nella direzione secondaria										
0	(8+9)-II-1	-1216	-0.72	32.00	45	-0.17	20.00	>100	V	45
0	(8+9)-VIII-3	3556	2.10	32.00	15	0.51	20.00	39	V	15
0	(8+9)-VIII-2	-2637	-1.56	32.00	21	-0.38	20.00	53	V	21
0	(8+9)-VI-4	1533	0.90	32.00	35	0.22	20.00	91	V	35
0	(8+9)-II-4	2135	1.26	32.00	25	0.31	20.00	66	V	25
0	(8+9)-II-3	-3816	-2.25	32.00	14	-0.55	20.00	37	V	14
0	(8+9)-II-2	4735	2.79	32.00	11	0.68	20.00	30	V	11
250	1	669	0.40	19.20	49	0.10	12.00	>100	V	49
250	2	1416	0.84	28.80	34	0.20	18.00	89	V	34
250	3	1416	0.84	28.80	34	0.20	18.00	89	V	34
250	4	669	0.40	25.60	65	0.10	16.00	>100	V	65
250	5	669	0.40	25.60	65	0.10	16.00	>100	V	65
250	6	669	0.40	25.60	65	0.10	16.00	>100	V	65
250	7	669	0.40	25.60	65	0.10	16.00	>100	V	65
250	(8+9)-VIII-4	-6548	-3.87	32.00	8.3	-0.94	20.00	21	V	8.3
250	(8+9)-V-1	6095	3.60	32.00	8.9	0.87	20.00	23	V	8.9
250	(8+9)-I-2	5703	3.37	32.00	9.5	0.81	20.00	25	V	9.5
250	(8+9)-III-2	3299	1.95	32.00	16	0.47	20.00	42	V	16
250	(8+9)-VI-2	5383	3.18	32.00	10	0.77	20.00	26	V	10
250	(8+9)-III-4	-5409	-3.19	32.00	10	-0.77	20.00	26	V	10
250	(8+9)-VI-3	-4464	-2.64	32.00	12	-0.64	20.00	31	V	12
250	(8+9)-IV-2	-3284	-1.94	32.00	17	-0.47	20.00	43	V	17

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
250	(8+9)-I-1	3924	2.32	32.00	14	0.56	20.00	36	V	14
250	(8+9)-IV-4	-5896	-3.48	32.00	9.2	-0.84	20.00	24	V	9.2
250	(8+9)-VII-1	8499	5.02	32.00	6.4	1.21	20.00	16	V	6.4
250	(8+9)-V-2	7874	4.65	32.00	6.9	1.12	20.00	18	V	6.9
250	(8+9)-VII-2	5470	3.23	32.00	9.9	0.78	20.00	26	V	9.9
250	(8+9)-V-4	-5176	-3.06	32.00	10	-0.74	20.00	27	V	10
250	(8+9)-VII-3	-4551	-2.69	32.00	12	-0.65	20.00	31	V	12
250	(8+9)-IV-1	6815	4.02	32.00	8.0	0.97	20.00	21	V	8.0
250	(8+9)-VII-4	-7581	-4.47	32.00	7.2	-1.08	20.00	18	V	7.2
250	(8+9)-III-1	6328	3.74	32.00	8.6	0.90	20.00	22	V	8.6
250	(8+9)-III-3	-2380	-1.40	32.00	23	-0.34	20.00	59	V	23
250	(8+9)-IV-3	4203	2.48	32.00	13	0.60	20.00	33	V	13
250	(8+9)-V-3	-6956	-4.11	32.00	7.8	-0.99	20.00	20	V	7.8
250	(8+9)-VIII-1	7466	4.41	32.00	7.3	1.07	20.00	19	V	7.3
250	(8+9)-I-4	-3005	-1.77	32.00	18	-0.43	20.00	47	V	18
250	(8+9)-I-3	-4785	-2.82	32.00	11	-0.68	20.00	29	V	11
500	(8+9)-VI-1	-914	-0.54	32.00	59	-0.13	20.00	>100	V	59

Setto 27: origine (708.5,2464.3,328.5), direzione (0.825704,0.564103,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	(8+9)-III-1	2837	-1	1486	3.34	-0.06	8.97	132.00	192.00	192.00	14
0	(8+9)-V-1	2228	-4	1271	2.62	-0.16	7.67	132.00	192.00	192.00	16
0	(8+9)-VII-2	2375	-8	1298	2.80	-0.35	7.84	132.00	192.00	192.00	16
0	(8+9)-VII-1	4323	-3	2069	5.09	-0.15	12.49	132.00	192.00	192.00	9.6
0	(8+9)-V-2	4471	-8	2097	5.26	-0.34	12.66	132.00	192.00	192.00	9.3
0	(8+9)-VIII-1	3505	6	1734	4.13	0.26	10.47	132.00	192.00	192.00	11
0	(8+9)-IV-3	1302	9	850	1.53	0.38	5.13	132.00	192.00	192.00	25
0	(8+9)-IV-1	3059	6	1559	3.60	0.29	9.41	132.00	192.00	192.00	13
0	(8+9)-I-2	2984	-6	1513	3.51	-0.25	9.14	132.00	192.00	192.00	13
1750	1	2975	6	723	3.50	0.25	4.37	79.20	115.20	115.20	12
1750	2	6117	12	1491	7.20	0.53	9.00	118.80	172.80	172.80	8.6
1750	3	6117	12	1491	7.20	0.53	9.00	118.80	172.80	172.80	8.6
1750	4	2975	6	723	3.50	0.25	4.37	105.60	153.60	153.60	16
1750	5	2975	6	723	3.50	0.25	4.37	105.60	153.60	153.60	16
1750	6	2975	6	723	3.50	0.25	4.37	105.60	153.60	153.60	16
1750	7	2975	6	723	3.50	0.25	4.37	105.60	153.60	153.60	16
1750	(8+9)-VIII-3	1902	11	474	2.24	0.47	2.86	132.00	192.00	192.00	29
3500	(8+9)-VIII-4	4533	-8	2053	5.34	-0.35	12.39	132.00	192.00	192.00	9.4
3500	(8+9)-I-4	1950	-25	775	2.30	-1.12	4.68	132.00	192.00	192.00	21
3500	(8+9)-VI-2	-4462	-114	-2347	-5.25	-5.02	-14.17	132.00	192.00	192.00	9.9
3500	(8+9)-III-4	3790	4	1735	4.46	0.18	10.48	132.00	192.00	192.00	11
3500	(8+9)-VI-3	3499	111	2244	4.12	4.89	13.55	132.00	192.00	192.00	7.9
3500	(8+9)-IV-2	2142	-14	1052	2.52	-0.64	6.35	132.00	192.00	192.00	18
3500	(8+9)-VI-4	-1598	-106	-1147	-1.88	-4.67	-6.93	132.00	192.00	192.00	17
3500	(8+9)-IV-4	4060	-9	1853	4.78	-0.41	11.19	132.00	192.00	192.00	10
3500	(8+9)-II-4	-2071	-107	-1347	-2.44	-4.73	-8.13	132.00	192.00	192.00	15
3500	(8+9)-I-3	3480	40	1793	4.10	1.75	10.82	132.00	192.00	192.00	10
3500	(8+9)-II-3	3026	109	2045	3.56	4.83	12.35	132.00	192.00	192.00	8.6
3500	(8+9)-V-4	3527	-21	1440	4.15	-0.91	8.69	132.00	192.00	192.00	12
3500	(8+9)-VII-3	3217	15	1497	3.79	0.66	9.04	132.00	192.00	192.00	13
3500	(8+9)-I-1	-2913	22	-878	-3.43	0.98	-5.30	132.00	192.00	192.00	30
3500	(8+9)-VII-4	5366	9	2400	6.32	0.38	14.49	132.00	192.00	192.00	8.0
3500	(8+9)-VI-1	635	103	1044	0.75	4.54	6.31	132.00	192.00	192.00	16
3500	(8+9)-III-3	1640	10	833	1.93	0.45	5.03	132.00	192.00	192.00	23
3500	(8+9)-V-3	5057	44	2457	5.95	1.95	14.83	132.00	192.00	192.00	7.5
3500	(8+9)-II-2	-3989	-112	-2148	-4.70	-4.96	-12.97	132.00	192.00	192.00	11
3500	(8+9)-VIII-2	1669	-16	853	1.96	-0.70	5.15	132.00	192.00	192.00	22
3500	(8+9)-II-1	1109	104	1244	1.31	4.60	7.51	132.00	192.00	192.00	14
3500	(8+9)-III-2	-2603	-13	-935	-3.06	-0.59	-5.65	132.00	192.00	192.00	31
Verifiche nella direzione secondaria											
0	1	-7387	-2	951	-4.36	-0.06	0.96	79.20	115.20	115.20	97

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	2	-15167	-4	1969	-8.95	-0.13	1.99	118.80	172.80	172.80	67
0	3	-15167	-4	1969	-8.95	-0.13	1.99	118.80	172.80	172.80	67
0	4	-7387	-2	951	-4.36	-0.06	0.96	105.60	153.60	153.60	>100
0	5	-7387	-2	951	-4.36	-0.06	0.96	105.60	153.60	153.60	>100
0	6	-7387	-2	951	-4.36	-0.06	0.96	105.60	153.60	153.60	>100
0	7	-7387	-2	951	-4.36	-0.06	0.96	105.60	153.60	153.60	>100
0	(8+9)-VIII-4	-4872	-11	-8627	-2.88	-0.37	-8.73	132.00	192.00	192.00	21
0	(8+9)-IV-2	-4874	-16	-4398	-2.88	-0.55	-4.45	132.00	192.00	192.00	38
0	(8+9)-V-1	-6038	-5	8924	-3.56	-0.19	9.03	132.00	192.00	192.00	21
0	(8+9)-I-2	-4185	-15	6486	-2.47	-0.50	6.56	132.00	192.00	192.00	27
0	(8+9)-V-2	-4065	-20	9059	-2.40	-0.69	9.17	132.00	192.00	192.00	19
0	(8+9)-I-4	-4057	-3	-5039	-2.40	-0.09	-5.10	132.00	192.00	192.00	37
0	(8+9)-V-3	-6152	18	-7746	-3.63	0.60	-7.84	132.00	192.00	192.00	23
0	(8+9)-VII-3	-5241	14	-5643	-3.09	0.48	-5.71	132.00	192.00	192.00	31
0	(8+9)-II-1	-8417	22	2160	-4.97	0.73	2.19	132.00	192.00	192.00	63
0	(8+9)-V-4	-4178	3	-7611	-2.47	0.10	-7.70	132.00	192.00	192.00	25
0	(8+9)-VIII-3	-5379	15	4939	-3.18	0.52	5.00	132.00	192.00	192.00	34
0	(8+9)-III-2	-5096	-11	4384	-3.01	-0.38	4.44	132.00	192.00	192.00	39
0	(8+9)-III-4	-4968	1	-7141	-2.93	0.03	-7.23	132.00	192.00	192.00	26
0	(8+9)-VI-1	-8381	20	2932	-4.95	0.67	2.97	132.00	192.00	192.00	51
0	(8+9)-I-1	-6159	0	6351	-3.64	0.00	6.43	132.00	192.00	192.00	30
0	(8+9)-VIII-2	-4838	-18	-3626	-2.86	-0.60	-3.67	132.00	192.00	192.00	45
0	(8+9)-IV-4	-4836	-12	-7855	-2.85	-0.42	-7.95	132.00	192.00	192.00	23
0	(8+9)-VIII-1	-5345	8	9940	-3.16	0.28	10.06	132.00	192.00	192.00	18
0	(8+9)-III-1	-5248	-3	8454	-3.10	-0.12	8.55	132.00	192.00	192.00	22
0	(8+9)-IV-1	-5381	10	9168	-3.18	0.34	9.28	132.00	192.00	192.00	20
0	(8+9)-IV-3	-5342	14	5711	-3.15	0.46	5.78	132.00	192.00	192.00	31
0	(8+9)-I-3	-6031	12	-5174	-3.56	0.42	-5.24	132.00	192.00	192.00	34
0	(8+9)-III-3	-5120	9	-3071	-3.02	0.30	-3.11	132.00	192.00	192.00	56
0	(8+9)-VII-4	-5089	6	-9713	-3.00	0.22	-9.83	132.00	192.00	192.00	19
0	(8+9)-VII-1	-5128	-9	11026	-3.03	-0.30	11.16	132.00	192.00	192.00	17
0	(8+9)-VII-2	-4976	-17	6956	-2.94	-0.57	7.04	132.00	192.00	192.00	25
585	(8+9)-II-2	-4032	-46	3536	-2.38	-1.56	3.58	132.00	192.00	192.00	37
585	(8+9)-VI-4	-3863	-42	1504	-2.28	-1.42	1.52	132.00	192.00	192.00	65
585	(8+9)-VI-3	-4689	37	-2827	-2.77	1.24	-2.86	132.00	192.00	192.00	46
585	(8+9)-VI-2	-4047	-48	3899	-2.39	-1.61	3.95	132.00	192.00	192.00	34
585	(8+9)-II-3	-4704	35	-2464	-2.78	1.19	-2.49	132.00	192.00	192.00	52
585	(8+9)-II-4	-3878	-44	1867	-2.29	-1.48	1.89	132.00	192.00	192.00	57

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Ty kg	τ_d kg/cmq	fvd kg/cmq	RS	Cs
0	1	8	0.01	3.84	Si	>100
0	2	17	0.01	5.76	Si	>100
0	3	17	0.01	5.76	Si	>100
0	4	8	0.01	5.12	Si	>100
0	5	8	0.01	5.12	Si	>100
0	6	8	0.01	5.12	Si	>100
0	7	8	0.01	5.12	Si	>100
0	(8+9)-IV-1	7	0.01	6.40	Si	>100
0	(8+9)-IV-2	5	0.00	6.40	Si	>100
0	(8+9)-VII-1	9	0.01	6.40	Si	>100
0	(8+9)-VIII-2	5	0.00	6.40	Si	>100
0	(8+9)-VIII-1	8	0.01	6.40	Si	>100
0	(8+9)-VII-2	8	0.01	6.40	Si	>100
0	(8+9)-VIII-3	6	0.01	6.40	Si	>100
0	(8+9)-IV-3	7	0.01	6.40	Si	>100
0	(8+9)-III-1	8	0.01	6.40	Si	>100
0	(8+9)-III-2	7	0.01	6.40	Si	>100
3500	(8+9)-VIII-4	-7	0.01	6.40	Si	>100
3500	(8+9)-V-1	-160	0.14	6.40	Si	47
3500	(8+9)-I-2	158	0.14	6.40	Si	47
3500	(8+9)-VI-3	-539	0.46	6.40	Si	14

X	Comb.	Ty	τ_d	fvd	RS	Cs
3500	(8+9)-I-1	-162	0.14	6.40	Si	46
3500	(8+9)-VI-4	528	0.45	6.40	Si	14
3500	(8+9)-III-3	-6	0.01	6.40	Si	>100
3500	(8+9)-II-3	-539	0.46	6.40	Si	14
3500	(8+9)-II-4	529	0.45	6.40	Si	14
3500	(8+9)-II-2	530	0.45	6.40	Si	14
3500	(8+9)-V-3	-169	0.14	6.40	Si	44
3500	(8+9)-VII-3	-8	0.01	6.40	Si	>100
3500	(8+9)-VI-1	-537	0.46	6.40	Si	14
3500	(8+9)-VII-4	-9	0.01	6.40	Si	>100
3500	(8+9)-V-2	160	0.14	6.40	Si	47
3500	(8+9)-V-4	152	0.13	6.40	Si	49
3500	(8+9)-VI-2	531	0.45	6.40	Si	14
3500	(8+9)-IV-4	-6	0.01	6.40	Si	>100
3500	(8+9)-II-1	-537	0.46	6.40	Si	14
3500	(8+9)-I-4	154	0.13	6.40	Si	49
3500	(8+9)-I-3	-167	0.14	6.40	Si	45
3500	(8+9)-III-4	-7	0.01	6.40	Si	>100
Verifiche nella direzione secondaria						
0	(8+9)-VIII-4	-30	0.02	6.40	Si	>100
0	(8+9)-IV-4	-32	0.02	6.40	Si	>100
0	(8+9)-IV-2	-35	0.02	6.40	Si	>100
0	(8+9)-V-2	-24	0.01	6.40	Si	>100
0	(8+9)-VII-2	-28	0.02	6.40	Si	>100
0	(8+9)-II-4	-19	0.01	6.40	Si	>100
0	(8+9)-VII-1	-12	0.01	6.40	Si	>100
0	(8+9)-III-2	-21	0.01	6.40	Si	>100
0	(8+9)-I-2	-17	0.01	6.40	Si	>100
0	(8+9)-VIII-2	-37	0.02	6.40	Si	>100
0	(8+9)-VI-2	-25	0.01	6.40	Si	>100
0	(8+9)-VI-4	-17	0.01	6.40	Si	>100
0	(8+9)-II-2	-23	0.01	6.40	Si	>100
0	(8+9)-V-1	-15	0.01	6.40	Si	>100
585	(8+9)-VI-1	-14	0.01	6.40	Si	>100
585	(8+9)-III-1	-10	0.01	6.40	Si	>100
585	(8+9)-I-1	-8	0.00	6.40	Si	>100
585	(8+9)-II-1	-14	0.01	6.40	Si	>100
1170	1	-13	0.01	3.84	Si	>100
1170	2	-28	0.02	5.76	Si	>100
1170	3	-28	0.02	5.76	Si	>100
1170	4	-13	0.01	5.12	Si	>100
1170	5	-13	0.01	5.12	Si	>100
1170	6	-13	0.01	5.12	Si	>100
1170	7	-13	0.01	5.12	Si	>100
1170	(8+9)-VI-3	-16	0.01	6.40	Si	>100
1170	(8+9)-IV-1	-21	0.01	6.40	Si	>100
1170	(8+9)-IV-3	-25	0.01	6.40	Si	>100
1170	(8+9)-V-4	-17	0.01	6.40	Si	>100
1170	(8+9)-VII-3	-22	0.01	6.40	Si	>100
1170	(8+9)-V-3	-19	0.01	6.40	Si	>100
1170	(8+9)-VII-4	-14	0.01	6.40	Si	>100
1170	(8+9)-I-3	-16	0.01	6.40	Si	>100
1170	(8+9)-I-4	-14	0.01	6.40	Si	>100
1170	(8+9)-III-3	-19	0.01	6.40	Si	>100
1170	(8+9)-VIII-1	-21	0.01	6.40	Si	>100
1170	(8+9)-III-4	-11	0.01	6.40	Si	>100
1170	(8+9)-VIII-3	-26	0.01	6.40	Si	>100
1170	(8+9)-II-3	-15	0.01	6.40	Si	>100

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	1	-4446	-7.85	19.20	2.4	-1.90	12.00	6.3	V	2.4

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
0	2	-9161	-16.18	28.80	1.8	-3.92	18.00	4.6	V	1.8
0	3	-9161	-16.18	28.80	1.8	-3.92	18.00	4.6	V	1.8
0	4	-4446	-7.85	25.60	3.3	-1.90	16.00	8.4	V	3.3
0	5	-4446	-7.85	25.60	3.3	-1.90	16.00	8.4	V	3.3
0	6	-4446	-7.85	25.60	3.3	-1.90	16.00	8.4	V	3.3
0	7	-4446	-7.85	25.60	3.3	-1.90	16.00	8.4	V	3.3
0	(8+9)-VIII-4	-5645	-9.97	32.00	3.2	-2.41	20.00	8.3	V	3.2
0	(8+9)-V-3	-6121	-10.81	32.00	3.0	-2.62	20.00	7.6	V	3.0
0	(8+9)-III-3	-4181	-7.38	32.00	4.3	-1.79	20.00	11	V	4.3
0	(8+9)-III-4	-5281	-9.33	32.00	3.4	-2.26	20.00	8.9	V	3.4
0	(8+9)-I-4	-4149	-7.33	32.00	4.4	-1.77	20.00	11	V	4.4
0	(8+9)-VI-3	-5754	-10.16	32.00	3.1	-2.46	20.00	8.1	V	3.1
0	(8+9)-VIII-2	-4165	-7.35	32.00	4.4	-1.78	20.00	11	V	4.4
0	(8+9)-IV-2	-4407	-7.78	32.00	4.1	-1.88	20.00	11	V	4.1
0	(8+9)-VII-4	-6088	-10.75	32.00	3.0	-2.60	20.00	7.7	V	3.0
0	(8+9)-VI-1	-4275	-7.55	32.00	4.2	-1.83	20.00	11	V	4.2
0	(8+9)-VI-4	-1870	-3.30	32.00	9.7	-0.80	20.00	25	V	9.7
0	(8+9)-II-1	-4517	-7.98	32.00	4.0	-1.93	20.00	10	V	4.0
0	(8+9)-II-3	-5512	-9.73	32.00	3.3	-2.36	20.00	8.5	V	3.3
0	(8+9)-VII-3	-4989	-8.81	32.00	3.6	-2.13	20.00	9.4	V	3.6
0	(8+9)-I-3	-5314	-9.38	32.00	3.4	-2.27	20.00	8.8	V	3.4
0	(8+9)-IV-4	-5402	-9.54	32.00	3.4	-2.31	20.00	8.7	V	3.4
0	(8+9)-V-4	-4956	-8.75	32.00	3.7	-2.12	20.00	9.4	V	3.7
3500	(8+9)-V-1	4917	8.68	32.00	3.7	2.10	20.00	9.5	V	3.7
3500	(8+9)-IV-1	4651	8.21	32.00	3.9	1.99	20.00	10	V	3.9
3500	(8+9)-I-2	4164	7.35	32.00	4.4	1.78	20.00	11	V	4.4
3500	(8+9)-VII-2	4415	7.80	32.00	4.1	1.89	20.00	11	V	4.1
3500	(8+9)-V-2	4981	8.80	32.00	3.6	2.13	20.00	9.4	V	3.6
3500	(8+9)-III-1	4666	8.24	32.00	3.9	1.99	20.00	10	V	3.9
3500	(8+9)-VI-2	3223	5.69	32.00	5.6	1.38	20.00	15	V	5.6
3500	(8+9)-II-4	1897	3.35	32.00	9.6	0.81	20.00	25	V	9.6
3500	(8+9)-IV-3	3571	6.31	32.00	5.1	1.53	20.00	13	V	5.1
3500	(8+9)-I-1	4100	7.24	32.00	4.4	1.75	20.00	11	V	4.4
3500	(8+9)-VII-1	5483	9.68	32.00	3.3	2.34	20.00	8.5	V	3.3
3500	(8+9)-VIII-1	4896	8.65	32.00	3.7	2.09	20.00	9.6	V	3.7
3500	(8+9)-II-2	2978	5.26	32.00	6.1	1.27	20.00	16	V	6.1
3500	(8+9)-VIII-3	3326	5.87	32.00	5.4	1.42	20.00	14	V	5.4
3500	(8+9)-III-2	3598	6.35	32.00	5.0	1.54	20.00	13	V	5.0
Verifiche nella direzione secondaria										
585	1	-693	-0.41	19.20	47	-0.10	12.00	>100	V	47
585	2	-1348	-0.80	28.80	36	-0.19	18.00	93	V	36
585	3	-1348	-0.80	28.80	36	-0.19	18.00	93	V	36
585	4	-693	-0.41	25.60	63	-0.10	16.00	>100	V	63
585	5	-693	-0.41	25.60	63	-0.10	16.00	>100	V	63
585	6	-693	-0.41	25.60	63	-0.10	16.00	>100	V	63
585	7	-693	-0.41	25.60	63	-0.10	16.00	>100	V	63
585	(8+9)-VII-3	-7431	-4.39	32.00	7.3	-1.06	20.00	19	V	7.3
585	(8+9)-VI-1	-3463	-2.04	32.00	16	-0.49	20.00	40	V	16
585	(8+9)-III-3	-4645	-2.74	32.00	12	-0.66	20.00	30	V	12
585	(8+9)-I-4	-4467	-2.64	32.00	12	-0.64	20.00	31	V	12
1170	(8+9)-VIII-4	-9170	-5.41	32.00	5.9	-1.31	20.00	15	V	5.9
1170	(8+9)-IV-2	-4764	-2.81	32.00	11	-0.68	20.00	29	V	11
1170	(8+9)-V-3	-10856	-6.41	32.00	5.0	-1.55	20.00	13	V	5.0
1170	(8+9)-II-2	7260	4.29	32.00	7.5	1.04	20.00	19	V	7.5
1170	(8+9)-V-4	-7375	-4.35	32.00	7.4	-1.05	20.00	19	V	7.4
1170	(8+9)-II-4	3736	2.21	32.00	15	0.53	20.00	37	V	15
1170	(8+9)-I-2	7311	4.32	32.00	7.4	1.04	20.00	19	V	7.4
1170	(8+9)-III-2	3704	2.19	32.00	15	0.53	20.00	38	V	15
1170	(8+9)-VI-2	8142	4.81	32.00	6.7	1.16	20.00	17	V	6.7
1170	(8+9)-III-4	-8043	-4.75	32.00	6.7	-1.15	20.00	17	V	6.7
1170	(8+9)-VI-3	-8747	-5.16	32.00	6.2	-1.25	20.00	16	V	6.2
1170	(8+9)-I-3	-7917	-4.67	32.00	6.8	-1.13	20.00	18	V	6.8
1170	(8+9)-VI-4	2854	1.68	32.00	19	0.41	20.00	49	V	19
1170	(8+9)-IV-4	-8288	-4.89	32.00	6.5	-1.18	20.00	17	V	6.5

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
1170	(8+9)-VII-1	10377	6.13	32.00	5.2	1.48	20.00	13	V	5.2
1170	(8+9)-V-2	10250	6.05	32.00	5.3	1.46	20.00	14	V	5.3
1170	(8+9)-VII-2	6643	3.92	32.00	8.2	0.95	20.00	21	V	8.2
1170	(8+9)-III-1	7438	4.39	32.00	7.3	1.06	20.00	19	V	7.3
1170	(8+9)-I-1	3831	2.26	32.00	14	0.55	20.00	37	V	14
1170	(8+9)-IV-1	7682	4.54	32.00	7.1	1.10	20.00	18	V	7.1
1170	(8+9)-VII-4	-10982	-6.48	32.00	4.9	-1.57	20.00	13	V	4.9
1170	(8+9)-II-1	-4341	-2.56	32.00	12	-0.62	20.00	32	V	12
1170	(8+9)-IV-3	4158	2.45	32.00	13	0.59	20.00	34	V	13
1170	(8+9)-II-3	-7866	-4.64	32.00	6.9	-1.12	20.00	18	V	6.9
1170	(8+9)-VIII-1	8564	5.06	32.00	6.3	1.22	20.00	16	V	6.3
1170	(8+9)-VIII-2	-3882	-2.29	32.00	14	-0.55	20.00	36	V	14
1170	(8+9)-VIII-3	3277	1.93	32.00	17	0.47	20.00	43	V	17
1170	(8+9)-V-1	6770	4.00	32.00	8.0	0.97	20.00	21	V	8.0

Verifiche a instabilità

Setto(X)	Comb.	k _{critc}	k _{critm}	λ_{relc}	λ_{relm}	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
(cm)						kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	
21(200.0)	(8+9)-VII-4	0.92	--	0.73	--	-1.06	0.07	7.39	132.00	192.00	192.00	22
22(250.0)	(8+9)-V-3	0.84	--	0.91	--	-1.11	0.09	6.53	132.00	192.00	192.00	24
23(0.0)	(8+9)-V-2	0.97	--	0.53	--	-0.83	-0.34	6.40	132.00	192.00	192.00	25
24(0.0)	(8+9)-VII-4	--	--	--	--	11.65	0.15	-26.83	132.00	192.00	192.00	4.4
25(0.0)	(8+9)-V-4	0.55	--	1.27	--	-7.71	0.15	-15.46	132.00	192.00	192.00	6.5
26(350.0)	(8+9)-VII-1	--	--	--	--	10.79	-0.41	-30.77	132.00	192.00	192.00	4.1
27(350.0)	(8+9)-VI-2	0.55	--	1.27	--	-5.25	-5.02	-14.17	132.00	192.00	192.00	6.7

Parete Xlam 5 - Nodi: [7-15-107-7-6-5-4-3-2-1-106] - **Crit.Prog.** Criterio di verifica XLAM 0 - **Verificato:** [Cs=1.372,Comb=(8+9)-VII-1]

Geometria setti

Setto	Crit.	X	L	S	X90	L90	S90
		mm	cm	cm	mm	cm	cm
21	Criterio di verifica XLAM 0	0	387.0	12.1	0	200.0	12.1
		1000	387.0	12.1	1935	200.0	12.1
		2000	387.0	12.1	3870	200.0	12.1
22	Criterio di verifica XLAM 0	0	387.0	12.1	0	250.0	12.1
		1250	387.0	12.1	1935	250.0	12.1
		2500	387.0	12.1	3870	250.0	12.1
23	Criterio di verifica XLAM 0	0	387.0	12.1	0	145.9	12.1
		730	387.0	12.1	1935	145.9	12.1
		1459	387.0	12.1	3870	145.9	12.1
24	Criterio di verifica XLAM 0	0	50.0	12.1	0	350.0	12.1
		1750	50.0	12.1	250	350.0	12.1
		3500	50.0	12.1	500	350.0	12.1
25	Criterio di verifica XLAM 0	0	117.0	12.1	0	350.0	12.1
		1750	117.0	12.1	585	350.0	12.1
		3500	117.0	12.1	1170	350.0	12.1
26	Criterio di verifica XLAM 0	0	50.0	12.1	0	350.0	12.1
		1750	50.0	12.1	250	350.0	12.1
		3500	50.0	12.1	500	350.0	12.1
27	Criterio di verifica XLAM 0	0	117.0	12.1	0	350.0	12.1
		1750	117.0	12.1	585	350.0	12.1
		3500	117.0	12.1	1170	350.0	12.1

Setto 21: origine (48.0,2013.0,193.5), direzione (0.825704,0.564103,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
2000	1	-499	2	1101	-0.18	0.03	0.61	79.20	115.20	115.20	>100
2000	2	-1042	4	2239	-0.37	0.06	1.24	118.80	172.80	172.80	>100
2000	3	-1042	4	2239	-0.37	0.06	1.24	118.80	172.80	172.80	>100
2000	4	-499	2	1101	-0.18	0.03	0.61	105.60	153.60	153.60	>100
2000	5	-499	2	1101	-0.18	0.03	0.61	105.60	153.60	153.60	>100
2000	6	-499	2	1101	-0.18	0.03	0.61	105.60	153.60	153.60	>100
2000	7	-499	2	1101	-0.18	0.03	0.61	105.60	153.60	153.60	>100
2000	(8+9)-VIII-4	-2601	-6	11747	-0.93	-0.08	6.48	132.00	192.00	192.00	29
2000	(8+9)-IV-1	1704	9	-9236	0.61	0.13	-5.10	132.00	192.00	192.00	31
2000	(8+9)-V-1	2142	-3	-11516	0.76	-0.04	-6.35	132.00	192.00	192.00	26
2000	(8+9)-I-2	797	-6	-4182	0.28	-0.08	-2.31	132.00	192.00	192.00	68
2000	(8+9)-V-2	1493	-8	-7466	0.53	-0.11	-4.12	132.00	192.00	192.00	38
2000	(8+9)-I-4	-2134	4	9758	-0.76	0.06	5.38	132.00	192.00	192.00	35
2000	(8+9)-V-3	-2181	11	8992	-0.78	0.14	4.96	132.00	192.00	192.00	38
2000	(8+9)-II-2	-986	-8	5422	-0.35	-0.11	2.99	132.00	192.00	192.00	62
2000	(8+9)-V-4	-2830	6	13042	-1.01	0.08	7.20	132.00	192.00	192.00	26
2000	(8+9)-II-4	-1865	-5	9604	-0.66	-0.07	5.30	132.00	192.00	192.00	36
2000	(8+9)-VI-1	1386	7	-9063	0.49	0.10	-5.00	132.00	192.00	192.00	33
2000	(8+9)-III-2	639	-7	-3834	0.23	-0.09	-2.12	132.00	192.00	192.00	76
2000	(8+9)-VI-2	-777	-9	4436	-0.28	-0.12	2.45	132.00	192.00	192.00	75
2000	(8+9)-III-4	-2292	4	10105	-0.82	0.05	5.58	132.00	192.00	192.00	34
2000	(8+9)-VI-3	89	12	-2911	0.03	0.15	-1.61	132.00	192.00	192.00	>100
2000	(8+9)-IV-2	-1513	-10	6580	-0.54	-0.13	3.63	132.00	192.00	192.00	51
2000	(8+9)-VI-4	-2074	-5	10589	-0.74	-0.06	5.84	132.00	192.00	192.00	32
2000	(8+9)-IV-4	-2392	-7	10762	-0.85	-0.09	5.94	132.00	192.00	192.00	32
2000	(8+9)-VII-1	2300	-3	-11864	0.82	-0.04	-6.55	132.00	192.00	192.00	25
2000	(8+9)-II-1	1177	8	-8078	0.42	0.11	-4.46	132.00	192.00	192.00	37
2000	(8+9)-VII-2	1335	-8	-7119	0.48	-0.11	-3.93	132.00	192.00	192.00	41
2000	(8+9)-III-1	1604	-1	-8579	0.57	-0.01	-4.73	132.00	192.00	192.00	34
2000	(8+9)-VII-3	-2023	11	8645	-0.72	0.15	4.77	132.00	192.00	192.00	39
2000	(8+9)-I-1	1446	-1	-8232	0.51	-0.02	-4.54	132.00	192.00	192.00	36
2000	(8+9)-VII-4	-2989	5	13390	-1.06	0.07	7.39	132.00	192.00	192.00	26
2000	(8+9)-III-3	-1327	9	5360	-0.47	0.13	2.96	132.00	192.00	192.00	62
2000	(8+9)-IV-3	825	13	-5054	0.29	0.17	-2.79	132.00	192.00	192.00	57
2000	(8+9)-II-3	298	11	-3896	0.11	0.15	-2.15	132.00	192.00	192.00	78
2000	(8+9)-VIII-1	1913	9	-10221	0.68	0.12	-5.64	132.00	192.00	192.00	28
2000	(8+9)-VIII-2	-1304	-10	5595	-0.46	-0.14	3.09	132.00	192.00	192.00	59
2000	(8+9)-VIII-3	616	13	-4069	0.22	0.18	-2.25	132.00	192.00	192.00	70
2000	(8+9)-I-3	-1485	9	5708	-0.53	0.12	3.15	132.00	192.00	192.00	59
Verifiche nella direzione secondaria											
0	(8+9)-VIII-4	4225	39	-3297	4.36	2.31	-10.22	132.00	192.00	192.00	10
0	(8+9)-VII-2	-5454	55	8405	-5.63	3.27	26.05	132.00	192.00	192.00	6.5
0	(8+9)-III-3	-6380	-76	-3446	-6.59	-4.48	-10.68	132.00	192.00	192.00	12
0	(8+9)-IV-2	2949	70	677	3.05	4.17	2.10	132.00	192.00	192.00	18
0	(8+9)-III-4	-1202	-49	-4842	-1.24	-2.91	-15.01	132.00	192.00	192.00	11
0	(8+9)-VIII-2	2546	61	1352	2.63	3.60	4.19	132.00	192.00	192.00	17
0	(8+9)-IV-1	-14312	-18	5331	-14.78	-1.06	16.52	132.00	192.00	192.00	10
0	(8+9)-VII-4	142	-17	-7093	0.15	-1.02	-21.98	132.00	192.00	192.00	8.3
0	(8+9)-I-1	-9066	36	7292	-9.37	2.12	22.60	132.00	192.00	192.00	7.6
0	(8+9)-IV-3	-13439	-59	2032	-13.88	-3.48	6.30	132.00	192.00	192.00	18
0	(8+9)-I-3	-6158	-101	-3705	-6.36	-5.95	-11.48	132.00	192.00	192.00	11
0	(8+9)-IV-4	3822	30	-2622	3.95	1.75	-8.13	132.00	192.00	192.00	12
0	(8+9)-II-1	-13571	-101	4469	-14.02	-5.96	13.85	132.00	192.00	192.00	9.2
0	(8+9)-V-1	-10410	4	9543	-10.75	0.23	29.57	132.00	192.00	192.00	6.3
0	(8+9)-II-3	-12698	-142	1170	-13.12	-8.38	3.62	132.00	192.00	192.00	15
0	(8+9)-V-2	-5676	80	8664	-5.86	4.74	26.85	132.00	192.00	192.00	6.0
0	(8+9)-III-1	-9288	61	7551	-9.60	3.59	23.40	132.00	192.00	192.00	7.0
0	(8+9)-V-3	-4814	-69	-5955	-4.97	-4.06	-18.46	132.00	192.00	192.00	8.5
0	(8+9)-VIII-3	-13036	-49	1357	-13.47	-2.92	4.21	132.00	192.00	192.00	24
0	(8+9)-V-4	-80	8	-6834	-0.08	0.45	-21.18	132.00	192.00	192.00	8.9

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-VII-3	-5036	-44	-5696	-5.20	-2.59	-17.65	132.00	192.00	192.00	9.4
0	(8+9)-VI-1	-13974	-110	5144	-14.44	-6.53	15.94	132.00	192.00	192.00	8.2
0	(8+9)-I-4	-1424	-24	-4583	-1.47	-1.44	-14.20	132.00	192.00	192.00	12
0	(8+9)-VI-2	1805	144	2214	1.86	8.49	6.86	132.00	192.00	192.00	11
0	(8+9)-II-4	3081	112	-1760	3.18	6.64	-5.45	132.00	192.00	192.00	11
0	(8+9)-VIII-1	-14715	-28	6006	-15.20	-1.63	18.61	132.00	192.00	192.00	9.0
0	(8+9)-I-2	-4332	112	6413	-4.48	6.63	19.88	132.00	192.00	192.00	7.2
0	(8+9)-II-2	2208	153	1539	2.28	9.06	4.77	132.00	192.00	192.00	11
0	(8+9)-III-2	-4110	87	6155	-4.25	5.16	19.07	132.00	192.00	192.00	7.9
0	(8+9)-VI-3	-12295	-132	494	-12.70	-7.81	1.53	132.00	192.00	192.00	19
0	(8+9)-VI-4	3484	122	-2435	3.60	7.21	-7.55	132.00	192.00	192.00	9.6
0	(8+9)-VII-1	-10632	29	9801	-10.98	1.70	30.38	132.00	192.00	192.00	5.9
1935	1	-7954	8	2670	-8.22	0.46	8.27	79.20	115.20	115.20	12
1935	2	-16256	16	5442	-16.79	0.92	16.86	118.80	172.80	172.80	8.9
1935	3	-16256	16	5442	-16.79	0.92	16.86	118.80	172.80	172.80	8.9
1935	4	-7954	8	2670	-8.22	0.46	8.27	105.60	153.60	153.60	17
1935	5	-7954	8	2670	-8.22	0.46	8.27	105.60	153.60	153.60	17
1935	6	-7954	8	2670	-8.22	0.46	8.27	105.60	153.60	153.60	17
1935	7	-7954	8	2670	-8.22	0.46	8.27	105.60	153.60	153.60	17

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Ty kg	τ_d kg/cmq	fvd kg/cmq	RS	Cs
0	(8+9)-V-4	55	0.01	6.40	Si	>100
0	(8+9)-II-3	-44	0.01	6.40	Si	>100
0	(8+9)-V-2	-38	0.01	6.40	Si	>100
0	(8+9)-VI-1	-31	0.01	6.40	Si	>100
0	(8+9)-VIII-2	-16	0.00	6.40	Si	>100
0	(8+9)-III-1	92	0.02	6.40	Si	>100
0	(8+9)-VII-3	50	0.01	6.40	Si	>100
0	(8+9)-III-2	89	0.02	6.40	Si	>100
0	(8+9)-VII-1	-43	0.01	6.40	Si	>100
0	(8+9)-III-3	-84	0.02	6.40	Si	>100
0	(8+9)-I-2	96	0.02	6.40	Si	>100
0	(8+9)-III-4	-87	0.02	6.40	Si	>100
0	(8+9)-I-4	-79	0.02	6.40	Si	>100
0	(8+9)-IV-1	33	0.01	6.40	Si	>100
0	(8+9)-II-2	49	0.01	6.40	Si	>100
0	(8+9)-IV-2	24	0.01	6.40	Si	>100
0	(8+9)-VII-4	48	0.01	6.40	Si	>100
0	(8+9)-IV-3	-20	0.01	6.40	Si	>100
0	(8+9)-I-1	84	0.02	6.40	Si	>100
0	(8+9)-IV-4	-28	0.01	6.40	Si	>100
0	(8+9)-VII-2	-46	0.01	6.40	Si	>100
0	(8+9)-I-3	-91	0.02	6.40	Si	>100
0	(8+9)-VIII-3	21	0.01	6.40	Si	>100
0	(8+9)-V-1	-50	0.01	6.40	Si	>100
0	(8+9)-VI-4	36	0.01	6.40	Si	>100
0	(8+9)-V-3	43	0.01	6.40	Si	>100
1000	1	5	0.00	3.84	Si	>100
1000	2	11	0.00	5.76	Si	>100
1000	3	11	0.00	5.76	Si	>100
1000	4	5	0.00	5.12	Si	>100
1000	5	5	0.00	5.12	Si	>100
1000	6	5	0.00	5.12	Si	>100
1000	7	5	0.00	5.12	Si	>100
1000	(8+9)-II-4	22	0.01	6.40	Si	>100
1000	(8+9)-II-1	-15	0.00	6.40	Si	>100
1000	(8+9)-VIII-1	-8	0.00	6.40	Si	>100
1000	(8+9)-VI-3	-7	0.00	6.40	Si	>100
1000	(8+9)-VI-2	14	0.00	6.40	Si	>100
1000	(8+9)-VIII-4	15	0.00	6.40	Si	>100

Verifiche nella direzione secondaria

X	Comb.	Ty	τ_d	fvd	RS	Cs
0	(8+9)-II-4	31	0.03	6.40	Si	>100
0	(8+9)-VII-3	36	0.03	6.40	Si	>100
0	(8+9)-VII-2	-41	0.04	6.40	Si	>100
0	(8+9)-VI-4	36	0.03	6.40	Si	>100
0	(8+9)-VI-3	-19	0.02	6.40	Si	>100
0	(8+9)-VI-1	-42	0.04	6.40	Si	>100
0	(8+9)-V-2	-32	0.03	6.40	Si	>100
0	(8+9)-V-1	-49	0.05	6.40	Si	>100
1935	(8+9)-VIII-4	-79	0.08	6.40	Si	85
1935	(8+9)-V-3	-32	0.03	6.40	Si	>100
1935	(8+9)-VII-1	46	0.04	6.40	Si	>100
1935	(8+9)-VIII-2	-60	0.06	6.40	Si	>100
1935	(8+9)-VIII-1	68	0.07	6.40	Si	98
1935	(8+9)-VII-4	-57	0.05	6.40	Si	>100
1935	(8+9)-IV-4	-74	0.07	6.40	Si	91
1935	(8+9)-V-4	-44	0.04	6.40	Si	>100
1935	(8+9)-VIII-3	49	0.05	6.40	Si	>100
1935	(8+9)-IV-1	63	0.06	6.40	Si	>100
3870	1	11	0.01	3.84	Si	>100
3870	2	23	0.02	5.76	Si	>100
3870	3	23	0.02	5.76	Si	>100
3870	4	11	0.01	5.12	Si	>100
3870	5	11	0.01	5.12	Si	>100
3870	6	11	0.01	5.12	Si	>100
3870	7	11	0.01	5.12	Si	>100
3870	(8+9)-I-3	-154	0.15	6.40	Si	44
3870	(8+9)-III-1	159	0.15	6.40	Si	42
3870	(8+9)-I-1	161	0.15	6.40	Si	42
3870	(8+9)-I-2	169	0.16	6.40	Si	40
3870	(8+9)-IV-2	74	0.07	6.40	Si	91
3870	(8+9)-II-3	-53	0.05	6.40	Si	>100
3870	(8+9)-III-2	171	0.16	6.40	Si	39
3870	(8+9)-IV-3	-58	0.06	6.40	Si	>100
3870	(8+9)-VI-2	23	0.02	6.40	Si	>100
3870	(8+9)-III-3	-155	0.15	6.40	Si	43
3870	(8+9)-II-2	69	0.07	6.40	Si	98
3870	(8+9)-II-1	41	0.04	6.40	Si	>100
3870	(8+9)-I-4	-145	0.14	6.40	Si	46
3870	(8+9)-III-4	-144	0.14	6.40	Si	47

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
1000	(8+9)-VIII-4	-10258	-5.48	32.00	5.8	-1.33	20.00	15	V	5.8
1000	(8+9)-IV-1	9637	5.14	32.00	6.2	1.25	20.00	16	V	6.2
1000	(8+9)-IV-4	-9398	-5.02	32.00	6.4	-1.21	20.00	16	V	6.4
1000	(8+9)-VI-3	-2126	-1.13	32.00	28	-0.27	20.00	73	V	28
1000	(8+9)-V-3	-8886	-4.74	32.00	6.7	-1.15	20.00	17	V	6.7
1000	(8+9)-VIII-1	10497	5.60	32.00	5.7	1.36	20.00	15	V	5.7
1000	(8+9)-V-2	9125	4.87	32.00	6.6	1.18	20.00	17	V	6.6
1000	(8+9)-VII-3	-6747	-3.60	32.00	8.9	-0.87	20.00	23	V	8.9
1000	(8+9)-III-1	8696	4.64	32.00	6.9	1.12	20.00	18	V	6.9
1000	(8+9)-I-2	6257	3.34	32.00	9.6	0.81	20.00	25	V	9.6
1000	(8+9)-III-2	4118	2.20	32.00	15	0.53	20.00	38	V	15
1000	(8+9)-VII-2	6986	3.73	32.00	8.6	0.90	20.00	22	V	8.6
1000	(8+9)-V-1	9425	5.03	32.00	6.4	1.22	20.00	16	V	6.4
1000	(8+9)-VIII-3	5004	2.67	32.00	12	0.65	20.00	31	V	12
1000	(8+9)-III-4	-8457	-4.52	32.00	7.1	-1.09	20.00	18	V	7.1
1000	(8+9)-I-1	6557	3.50	32.00	9.1	0.85	20.00	24	V	9.1
1000	(8+9)-VII-1	11564	6.17	32.00	5.2	1.49	20.00	13	V	5.2
1000	(8+9)-VII-4	-11325	-6.05	32.00	5.3	-1.46	20.00	14	V	5.3
1000	(8+9)-I-3	-6018	-3.21	32.00	10.0	-0.78	20.00	26	V	10.0
1000	(8+9)-IV-3	5864	3.13	32.00	10	0.76	20.00	26	V	10

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
2000	1	-2565	-1.37	19.20	14	-0.33	12.00	36	V	14
2000	2	-5339	-2.85	28.80	10	-0.69	18.00	26	V	10
2000	3	-5339	-2.85	28.80	10	-0.69	18.00	26	V	10
2000	4	-2565	-1.37	25.60	19	-0.33	16.00	48	V	19
2000	5	-2565	-1.37	25.60	19	-0.33	16.00	48	V	19
2000	6	-2565	-1.37	25.60	19	-0.33	16.00	48	V	19
2000	7	-2565	-1.37	25.60	19	-0.33	16.00	48	V	19
2000	(8+9)-IV-2	-5838	-3.12	32.00	10	-0.75	20.00	27	V	10
2000	(8+9)-II-1	4621	2.47	32.00	13	0.60	20.00	34	V	13
2000	(8+9)-III-3	-4309	-2.30	32.00	14	-0.56	20.00	36	V	14
2000	(8+9)-V-4	-9454	-5.05	32.00	6.3	-1.22	20.00	16	V	6.3
2000	(8+9)-VI-2	-5072	-2.71	32.00	12	-0.66	20.00	31	V	12
2000	(8+9)-I-4	-7447	-3.98	32.00	8.0	-0.96	20.00	21	V	8.0
2000	(8+9)-VI-1	5223	2.79	32.00	11	0.67	20.00	30	V	11
2000	(8+9)-VI-4	-8758	-4.68	32.00	6.8	-1.13	20.00	18	V	6.8
2000	(8+9)-II-3	2140	1.14	32.00	28	0.28	20.00	72	V	28
2000	(8+9)-VIII-2	-5236	-2.80	32.00	11	-0.68	20.00	30	V	11
2000	(8+9)-II-4	-8155	-4.35	32.00	7.3	-1.05	20.00	19	V	7.3
2000	(8+9)-II-2	-5675	-3.03	32.00	11	-0.73	20.00	27	V	11
Verifiche nella direzione secondaria										
1935	(8+9)-VIII-4	-7294	-7.54	32.00	4.2	-1.82	20.00	11	V	4.2
1935	(8+9)-VII-2	3997	4.13	32.00	7.7	1.00	20.00	20	V	7.7
1935	(8+9)-III-3	-2869	-2.96	32.00	11	-0.72	20.00	28	V	11
1935	(8+9)-IV-2	-4342	-4.49	32.00	7.1	-1.09	20.00	18	V	7.1
1935	(8+9)-III-4	-5844	-6.04	32.00	5.3	-1.46	20.00	14	V	5.3
1935	(8+9)-VIII-2	-3685	-3.81	32.00	8.4	-0.92	20.00	22	V	8.4
1935	(8+9)-IV-1	5574	5.76	32.00	5.6	1.39	20.00	14	V	5.6
1935	(8+9)-VII-4	-8035	-8.30	32.00	3.9	-2.01	20.00	10.0	V	3.9
1935	(8+9)-I-1	4607	4.76	32.00	6.7	1.15	20.00	17	V	6.7
1935	(8+9)-IV-3	3279	3.39	32.00	9.4	0.82	20.00	24	V	9.4
1935	(8+9)-I-3	-3042	-3.14	32.00	10	-0.76	20.00	26	V	10
1935	(8+9)-IV-4	-6637	-6.86	32.00	4.7	-1.66	20.00	12	V	4.7
1935	(8+9)-II-1	4997	5.16	32.00	6.2	1.25	20.00	16	V	6.2
1935	(8+9)-V-1	6799	7.02	32.00	4.6	1.70	20.00	12	V	4.6
1935	(8+9)-II-3	2702	2.79	32.00	11	0.68	20.00	30	V	11
1935	(8+9)-V-2	4170	4.31	32.00	7.4	1.04	20.00	19	V	7.4
1935	(8+9)-III-1	4781	4.94	32.00	6.5	1.20	20.00	17	V	6.5
1935	(8+9)-V-3	-5233	-5.41	32.00	5.9	-1.31	20.00	15	V	5.9
1935	(8+9)-VIII-3	2622	2.71	32.00	12	0.66	20.00	31	V	12
1935	(8+9)-V-4	-7862	-8.12	32.00	3.9	-1.97	20.00	10	V	3.9
1935	(8+9)-VII-3	-5060	-5.23	32.00	6.1	-1.27	20.00	16	V	6.1
1935	(8+9)-VI-1	5654	5.84	32.00	5.5	1.41	20.00	14	V	5.5
1935	(8+9)-I-4	-5670	-5.86	32.00	5.5	-1.42	20.00	14	V	5.5
1935	(8+9)-VI-2	-3108	-3.21	32.00	10.0	-0.78	20.00	26	V	10.0
1935	(8+9)-II-4	-6060	-6.26	32.00	5.1	-1.51	20.00	13	V	5.1
1935	(8+9)-VIII-1	6231	6.44	32.00	5.0	1.56	20.00	13	V	5.0
1935	(8+9)-I-2	1979	2.04	32.00	16	0.49	20.00	40	V	16
1935	(8+9)-II-2	-3765	-3.89	32.00	8.2	-0.94	20.00	21	V	8.2
1935	(8+9)-III-2	1806	1.87	32.00	17	0.45	20.00	44	V	17
1935	(8+9)-VI-3	2045	2.11	32.00	15	0.51	20.00	39	V	15
1935	(8+9)-VI-4	-6717	-6.94	32.00	4.6	-1.68	20.00	12	V	4.6
1935	(8+9)-VII-1	6972	7.20	32.00	4.4	1.74	20.00	11	V	4.4
3870	1	-1599	-1.65	19.20	12	-0.40	12.00	30	V	12
3870	2	-3322	-3.43	28.80	8.4	-0.83	18.00	22	V	8.4
3870	3	-3322	-3.43	28.80	8.4	-0.83	18.00	22	V	8.4
3870	4	-1599	-1.65	25.60	15	-0.40	16.00	40	V	15
3870	5	-1599	-1.65	25.60	15	-0.40	16.00	40	V	15
3870	6	-1599	-1.65	25.60	15	-0.40	16.00	40	V	15
3870	7	-1599	-1.65	25.60	15	-0.40	16.00	40	V	15

Setto 22: origine (502.1,2323.3,193.5), direzione (0.825704,0.564103,0)
 Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	(8+9)-IV-3	-1015	0	3374	-0.36	0.01	1.86	132.00	192.00	192.00	>100
0	(8+9)-VIII-3	-925	1	2759	-0.33	0.01	1.52	132.00	192.00	192.00	>100
0	(8+9)-VI-4	853	-15	-7367	0.30	-0.21	-4.07	132.00	192.00	192.00	41
0	(8+9)-II-4	762	-16	-6752	0.27	-0.21	-3.73	132.00	192.00	192.00	44
0	(8+9)-V-1	-1513	-3	7298	-0.54	-0.04	4.03	132.00	192.00	192.00	47
0	(8+9)-V-4	590	-3	-8083	0.21	-0.04	-4.46	132.00	192.00	192.00	40
0	(8+9)-VI-1	-1776	10	6582	-0.63	0.13	3.63	132.00	192.00	192.00	51
0	(8+9)-I-1	-1212	-2	5248	-0.43	-0.03	2.90	132.00	192.00	192.00	66
0	(8+9)-I-4	289	-4	-6033	0.10	-0.05	-3.33	132.00	192.00	192.00	54
2500	1	-1850	0	1508	-0.66	0.01	0.83	79.20	115.20	115.20	>100
2500	2	-3789	1	3061	-1.35	0.01	1.69	118.80	172.80	172.80	>100
2500	3	-3789	1	3061	-1.35	0.01	1.69	118.80	172.80	172.80	>100
2500	4	-1850	0	1508	-0.66	0.01	0.83	105.60	153.60	153.60	>100
2500	5	-1850	0	1508	-0.66	0.01	0.83	105.60	153.60	153.60	>100
2500	6	-1850	0	1508	-0.66	0.01	0.83	105.60	153.60	153.60	>100
2500	7	-1850	0	1508	-0.66	0.01	0.83	105.60	153.60	153.60	>100
2500	(8+9)-VIII-4	-3022	-5	9492	-1.08	-0.06	5.24	132.00	192.00	192.00	36
2500	(8+9)-IV-1	304	6	-6555	0.11	0.07	-3.62	132.00	192.00	192.00	50
2500	(8+9)-VI-2	344	-7	-9278	0.12	-0.09	-5.12	132.00	192.00	192.00	36
2500	(8+9)-III-3	-1845	5	4908	-0.66	0.07	2.71	132.00	192.00	192.00	69
2500	(8+9)-VI-3	-2902	7	11369	-1.03	0.10	6.27	132.00	192.00	192.00	30
2500	(8+9)-III-2	-714	-5	-2817	-0.25	-0.06	-1.55	132.00	192.00	192.00	>100
2500	(8+9)-I-3	-2588	5	9017	-0.92	0.07	4.98	132.00	192.00	192.00	38
2500	(8+9)-III-1	65	-1	-6363	0.02	-0.01	-3.51	132.00	192.00	192.00	54
2500	(8+9)-VII-1	593	-3	-9183	0.21	-0.04	-5.07	132.00	192.00	192.00	35
2500	(8+9)-II-3	-2744	7	10523	-0.98	0.09	5.81	132.00	192.00	192.00	33
2500	(8+9)-VII-2	-185	-6	-5637	-0.07	-0.09	-3.11	132.00	192.00	192.00	60
2500	(8+9)-V-3	-3116	7	11837	-1.11	0.09	6.53	132.00	192.00	192.00	29
2500	(8+9)-VII-3	-2374	7	7727	-0.84	0.09	4.26	132.00	192.00	192.00	44
2500	(8+9)-II-1	-2171	5	7142	-0.77	0.07	3.94	132.00	192.00	192.00	48
2500	(8+9)-VII-4	-3152	3	11273	-1.12	0.04	6.22	132.00	192.00	192.00	31
2500	(8+9)-V-2	557	-6	-9746	0.20	-0.08	-5.38	132.00	192.00	192.00	33
2500	(8+9)-II-2	185	-6	-8432	0.07	-0.09	-4.65	132.00	192.00	192.00	40
2500	(8+9)-III-4	-2624	2	8454	-0.93	0.02	4.66	132.00	192.00	192.00	41
2500	(8+9)-IV-4	-2863	-5	8646	-1.02	-0.07	4.77	132.00	192.00	192.00	40
2500	(8+9)-VIII-1	463	5	-7401	0.16	0.07	-4.08	132.00	192.00	192.00	44
2500	(8+9)-VIII-2	-2132	-7	4419	-0.76	-0.10	2.44	132.00	192.00	192.00	76
2500	(8+9)-I-2	29	-5	-6926	0.01	-0.06	-3.82	132.00	192.00	192.00	49
2500	(8+9)-IV-2	-2290	-7	5265	-0.82	-0.09	2.91	132.00	192.00	192.00	64
Verifiche nella direzione secondaria											
0	1	-13116	19	27	-10.84	0.90	0.05	79.20	115.20	115.20	58
0	2	-26555	37	150	-21.95	1.77	0.30	118.80	172.80	172.80	36
0	3	-26555	37	150	-21.95	1.77	0.30	118.80	172.80	172.80	36
0	4	-13116	19	27	-10.84	0.90	0.05	105.60	153.60	153.60	89
0	5	-13116	19	27	-10.84	0.90	0.05	105.60	153.60	153.60	89
0	6	-13116	19	27	-10.84	0.90	0.05	105.60	153.60	153.60	89
0	7	-13116	19	27	-10.84	0.90	0.05	105.60	153.60	153.60	89
0	(8+9)-VIII-4	-8895	17	-17885	-7.35	0.78	-35.47	132.00	192.00	192.00	5.3
0	(8+9)-IV-2	-8856	36	-9373	-7.32	1.72	-18.59	132.00	192.00	192.00	9.3
0	(8+9)-V-1	-10992	-133	18667	-9.08	-6.29	37.03	132.00	192.00	192.00	4.4
0	(8+9)-I-2	-7073	226	9728	-5.85	10.67	19.29	132.00	192.00	192.00	6.4
0	(8+9)-V-2	-7016	245	15035	-5.80	11.61	29.82	132.00	192.00	192.00	4.6
0	(8+9)-I-4	-7143	180	-13337	-5.90	8.49	-26.45	132.00	192.00	192.00	5.5
0	(8+9)-V-3	-11176	-219	-15012	-9.24	-10.34	-29.78	132.00	192.00	192.00	4.7
0	(8+9)-II-2	-2459	651	-2583	-2.03	30.79	-5.12	132.00	192.00	192.00	5.3
0	(8+9)-V-4	-7200	160	-18645	-5.95	7.55	-36.98	132.00	192.00	192.00	4.3
0	(8+9)-II-4	-2480	637	-9502	-2.05	30.13	-18.85	132.00	192.00	192.00	3.9
0	(8+9)-VI-1	-15695	-605	11117	-12.97	-28.59	22.05	132.00	192.00	192.00	3.7
0	(8+9)-III-2	-8992	41	7691	-7.43	1.95	15.25	132.00	192.00	192.00	11
0	(8+9)-VI-2	-2442	657	-991	-2.02	31.07	-1.97	132.00	192.00	192.00	5.8
0	(8+9)-III-4	-9063	-5	-15374	-7.49	-0.23	-30.49	132.00	192.00	192.00	6.2
0	(8+9)-VI-3	-15750	-630	1014	-13.02	-29.80	2.01	132.00	192.00	192.00	5.9
0	(8+9)-I-1	-11049	-153	13360	-9.13	-7.23	26.50	132.00	192.00	192.00	5.6

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-VI-4	-2497	631	-11095	-2.06	29.85	-22.01	132.00	192.00	192.00	3.7
0	(8+9)-IV-4	-8878	23	-16292	-7.34	1.06	-32.32	132.00	192.00	192.00	5.7
0	(8+9)-VII-1	-9073	51	20704	-7.50	2.43	41.07	132.00	192.00	192.00	4.4
0	(8+9)-II-1	-15712	-611	9525	-12.99	-28.87	18.89	132.00	192.00	192.00	3.9
0	(8+9)-VII-2	-8936	61	12998	-7.38	2.89	25.78	132.00	192.00	192.00	6.6
0	(8+9)-III-1	-9130	32	15397	-7.55	1.49	30.54	132.00	192.00	192.00	5.9
0	(8+9)-VII-3	-9257	-34	-12975	-7.65	-1.62	-25.74	132.00	192.00	192.00	6.9
0	(8+9)-IV-1	-9315	4	16315	-7.70	0.20	32.36	132.00	192.00	192.00	5.8
0	(8+9)-VII-4	-9119	-25	-20682	-7.54	-1.17	-41.02	132.00	192.00	192.00	4.5
0	(8+9)-III-3	-9200	-14	-7668	-7.60	-0.68	-15.21	132.00	192.00	192.00	12
0	(8+9)-IV-3	-9336	-10	9396	-7.72	-0.45	18.64	132.00	192.00	192.00	9.9
0	(8+9)-II-3	-15733	-624	2606	-13.00	-29.52	5.17	132.00	192.00	192.00	5.4
0	(8+9)-VIII-1	-9298	10	17907	-7.68	0.48	35.52	132.00	192.00	192.00	5.3
0	(8+9)-VIII-2	-8839	42	-7781	-7.31	2.00	-15.43	132.00	192.00	192.00	11
0	(8+9)-VIII-3	-9353	-16	7804	-7.73	-0.74	15.48	132.00	192.00	192.00	12
0	(8+9)-I-3	-11119	-199	-9705	-9.19	-9.41	-19.25	132.00	192.00	192.00	6.6

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Ty kg	τ_d kg/cmq	fvd kg/cmq	RS	Cs
0	(8+9)-V-2	54	0.01	6.40	Si	>100
0	(8+9)-II-2	163	0.04	6.40	Si	>100
0	(8+9)-IV-1	5	0.00	6.40	Si	>100
0	(8+9)-II-3	-158	0.04	6.40	Si	>100
0	(8+9)-VIII-1	6	0.00	6.40	Si	>100
0	(8+9)-II-4	161	0.04	6.40	Si	>100
0	(8+9)-VII-1	7	0.00	6.40	Si	>100
0	(8+9)-III-1	6	0.00	6.40	Si	>100
0	(8+9)-VI-3	-158	0.04	6.40	Si	>100
0	(8+9)-III-2	5	0.00	6.40	Si	>100
0	(8+9)-I-2	53	0.01	6.40	Si	>100
0	(8+9)-VI-2	163	0.04	6.40	Si	>100
0	(8+9)-I-4	48	0.01	6.40	Si	>100
0	(8+9)-VI-1	-156	0.04	6.40	Si	>100
0	(8+9)-VIII-3	4	0.00	6.40	Si	>100
0	(8+9)-VI-4	161	0.04	6.40	Si	>100
0	(8+9)-V-4	47	0.01	6.40	Si	>100
0	(8+9)-I-3	-48	0.01	6.40	Si	>100
0	(8+9)-VII-2	6	0.00	6.40	Si	>100
0	(8+9)-I-1	-43	0.01	6.40	Si	>100
0	(8+9)-II-1	-156	0.04	6.40	Si	>100
0	(8+9)-IV-3	4	0.00	6.40	Si	>100
0	(8+9)-V-3	-49	0.01	6.40	Si	>100
0	(8+9)-V-1	-42	0.01	6.40	Si	>100
2500	1	5	0.00	3.84	Si	>100
2500	2	12	0.00	5.76	Si	>100
2500	3	12	0.00	5.76	Si	>100
2500	4	5	0.00	5.12	Si	>100
2500	5	5	0.00	5.12	Si	>100
2500	6	5	0.00	5.12	Si	>100
2500	7	5	0.00	5.12	Si	>100
2500	(8+9)-VIII-4	6	0.00	6.40	Si	>100
2500	(8+9)-III-3	4	0.00	6.40	Si	>100
2500	(8+9)-VII-3	6	0.00	6.40	Si	>100
2500	(8+9)-VII-4	6	0.00	6.40	Si	>100
2500	(8+9)-III-4	5	0.00	6.40	Si	>100
2500	(8+9)-VIII-2	4	0.00	6.40	Si	>100
2500	(8+9)-IV-2	5	0.00	6.40	Si	>100
2500	(8+9)-IV-4	5	0.00	6.40	Si	>100
Verifiche nella direzione secondaria						
0	(8+9)-VIII-4	-34	0.03	6.40	Si	>100
0	(8+9)-II-2	-17	0.01	6.40	Si	>100
0	(8+9)-IV-4	-35	0.03	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
0	(8+9)-IV-2	-37	0.03	6.40	Si	>100
0	(8+9)-IV-3	32	0.02	6.40	Si	>100
0	(8+9)-VIII-2	-38	0.03	6.40	Si	>100
0	(8+9)-VII-3	13	0.01	6.40	Si	>100
0	(8+9)-VIII-3	33	0.02	6.40	Si	>100
0	(8+9)-VIII-1	29	0.02	6.40	Si	>100
0	(8+9)-VII-2	-19	0.01	6.40	Si	>100
0	(8+9)-IV-1	30	0.02	6.40	Si	>100
0	(8+9)-III-4	-9	0.01	6.40	Si	>100
0	(8+9)-III-3	11	0.01	6.40	Si	>100
1935	1	-6	0.00	3.84	Si	>100
1935	2	-13	0.01	5.76	Si	>100
1935	3	-13	0.01	5.76	Si	>100
1935	4	-6	0.00	5.12	Si	>100
1935	5	-6	0.00	5.12	Si	>100
1935	6	-6	0.00	5.12	Si	>100
1935	7	-6	0.00	5.12	Si	>100
1935	(8+9)-V-4	-200	0.15	6.40	Si	42
1935	(8+9)-II-4	-699	0.53	6.40	Si	12
1935	(8+9)-VI-4	-697	0.53	6.40	Si	12
1935	(8+9)-I-2	-221	0.17	6.40	Si	38
1935	(8+9)-VII-1	-20	0.02	6.40	Si	>100
1935	(8+9)-V-1	191	0.15	6.40	Si	44
1935	(8+9)-I-4	-206	0.16	6.40	Si	41
1935	(8+9)-V-3	218	0.17	6.40	Si	38
1935	(8+9)-II-1	690	0.53	6.40	Si	12
1935	(8+9)-VI-1	688	0.53	6.40	Si	12
1935	(8+9)-VI-3	697	0.53	6.40	Si	12
1935	(8+9)-V-2	-227	0.17	6.40	Si	37
1935	(8+9)-I-3	212	0.16	6.40	Si	40
1935	(8+9)-VI-2	-706	0.54	6.40	Si	12
1935	(8+9)-I-1	197	0.15	6.40	Si	43
1935	(8+9)-II-2	-704	0.54	6.40	Si	12
1935	(8+9)-II-3	695	0.53	6.40	Si	12
1935	(8+9)-III-1	-13	0.01	6.40	Si	>100
3870	(8+9)-VII-4	11	0.01	6.40	Si	>100

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Tx kg	τ_{vd} kg/cmq	fvd kg/cmq	Csv	τ_M kg/cmq	fTd kg/cmq	Csm	Mecc.	Cs
0	(8+9)-II-2	1089	0.58	32.00	55	0.14	20.00	>100	V	55
1250	(8+9)-VIII-4	-9719	-5.19	32.00	6.2	-1.26	20.00	16	V	6.2
1250	(8+9)-IV-1	10498	5.60	32.00	5.7	1.36	20.00	15	V	5.7
1250	(8+9)-V-4	-9862	-5.26	32.00	6.1	-1.27	20.00	16	V	6.1
1250	(8+9)-III-1	10057	5.37	32.00	6.0	1.30	20.00	15	V	6.0
1250	(8+9)-IV-3	6344	3.39	32.00	9.4	0.82	20.00	24	V	9.4
1250	(8+9)-III-2	5526	2.95	32.00	11	0.71	20.00	28	V	11
1250	(8+9)-VIII-1	11455	6.12	32.00	5.2	1.48	20.00	14	V	5.2
1250	(8+9)-VI-2	1845	0.98	32.00	32	0.24	20.00	84	V	32
1250	(8+9)-I-1	8409	4.49	32.00	7.1	1.09	20.00	18	V	7.1
1250	(8+9)-III-4	-8322	-4.44	32.00	7.2	-1.08	20.00	19	V	7.2
1250	(8+9)-VII-2	8715	4.65	32.00	6.9	1.13	20.00	18	V	6.9
1250	(8+9)-VI-1	5958	3.18	32.00	10	0.77	20.00	26	V	10
1250	(8+9)-II-1	5002	2.67	32.00	12	0.65	20.00	31	V	12
1250	(8+9)-IV-2	-4608	-2.46	32.00	13	-0.60	20.00	34	V	13
1250	(8+9)-VI-4	-4223	-2.25	32.00	14	-0.55	20.00	37	V	14
1250	(8+9)-VIII-3	5387	2.88	32.00	11	0.70	20.00	29	V	11
1250	(8+9)-IV-4	-8762	-4.68	32.00	6.8	-1.13	20.00	18	V	6.8
1250	(8+9)-I-2	7175	3.83	32.00	8.4	0.93	20.00	22	V	8.4
1250	(8+9)-VII-1	13246	7.07	32.00	4.5	1.71	20.00	12	V	4.5
1250	(8+9)-II-4	-3266	-1.74	32.00	18	-0.42	20.00	47	V	18
1250	(8+9)-VII-4	-11511	-6.15	32.00	5.2	-1.49	20.00	13	V	5.2
1250	(8+9)-I-4	-6673	-3.56	32.00	9.0	-0.86	20.00	23	V	9.0

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
1250	(8+9)-V-1	11597	6.19	32.00	5.2	1.50	20.00	13	V	5.2
1250	(8+9)-V-2	10363	5.53	32.00	5.8	1.34	20.00	15	V	5.8
1250	(8+9)-V-3	-8628	-4.61	32.00	6.9	-1.11	20.00	18	V	6.9
2500	1	-3056	-1.63	19.20	12	-0.39	12.00	30	V	12
2500	2	-6320	-3.37	28.80	8.5	-0.82	18.00	22	V	8.5
2500	3	-6320	-3.37	28.80	8.5	-0.82	18.00	22	V	8.5
2500	4	-3056	-1.63	25.60	16	-0.39	16.00	41	V	16
2500	5	-3056	-1.63	25.60	16	-0.39	16.00	41	V	16
2500	6	-3056	-1.63	25.60	16	-0.39	16.00	41	V	16
2500	7	-3056	-1.63	25.60	16	-0.39	16.00	41	V	16
2500	(8+9)-VII-3	-7002	-3.74	32.00	8.6	-0.90	20.00	22	V	8.6
2500	(8+9)-III-3	-5081	-2.71	32.00	12	-0.66	20.00	30	V	12
2500	(8+9)-I-3	-6280	-3.35	32.00	9.5	-0.81	20.00	25	V	9.5
2500	(8+9)-VIII-2	-3966	-2.12	32.00	15	-0.51	20.00	39	V	15
2500	(8+9)-VI-3	-4252	-2.27	32.00	14	-0.55	20.00	36	V	14
2500	(8+9)-II-3	-3676	-1.96	32.00	16	-0.47	20.00	42	V	16
Verifiche nella direzione secondaria										
1935	(8+9)-VIII-4	-9083	-7.51	32.00	4.3	-1.82	20.00	11	V	4.3
1935	(8+9)-VII-2	6568	5.43	32.00	5.9	1.31	20.00	15	V	5.9
1935	(8+9)-III-3	-3876	-3.20	32.00	10.0	-0.78	20.00	26	V	10.0
1935	(8+9)-IV-2	-4779	-3.95	32.00	8.1	-0.96	20.00	21	V	8.1
1935	(8+9)-III-4	-7780	-6.43	32.00	5.0	-1.56	20.00	13	V	5.0
1935	(8+9)-VIII-2	-3962	-3.27	32.00	9.8	-0.79	20.00	25	V	9.8
1935	(8+9)-IV-1	8235	6.81	32.00	4.7	1.65	20.00	12	V	4.7
1935	(8+9)-VII-4	-10503	-8.68	32.00	3.7	-2.10	20.00	9.5	V	3.7
1935	(8+9)-I-1	5799	4.79	32.00	6.7	1.16	20.00	17	V	6.7
1935	(8+9)-IV-3	4748	3.92	32.00	8.2	0.95	20.00	21	V	8.2
1935	(8+9)-I-3	-5825	-4.81	32.00	6.6	-1.17	20.00	17	V	6.6
1935	(8+9)-IV-4	-8266	-6.83	32.00	4.7	-1.65	20.00	12	V	4.7
1935	(8+9)-II-1	1737	1.44	32.00	22	0.35	20.00	58	V	22
1935	(8+9)-V-1	8522	7.04	32.00	4.5	1.70	20.00	12	V	4.5
1935	(8+9)-II-3	-1751	-1.45	32.00	22	-0.35	20.00	57	V	22
1935	(8+9)-V-2	8517	7.04	32.00	4.5	1.70	20.00	12	V	4.5
1935	(8+9)-III-1	7749	6.40	32.00	5.0	1.55	20.00	13	V	5.0
1935	(8+9)-V-3	-8548	-7.06	32.00	4.5	-1.71	20.00	12	V	4.5
1935	(8+9)-VIII-3	3931	3.25	32.00	9.9	0.79	20.00	25	V	9.9
1935	(8+9)-V-4	-8553	-7.07	32.00	4.5	-1.71	20.00	12	V	4.5
1935	(8+9)-VII-3	-6599	-5.45	32.00	5.9	-1.32	20.00	15	V	5.9
1935	(8+9)-VI-1	2553	2.11	32.00	15	0.51	20.00	39	V	15
1935	(8+9)-I-4	-5830	-4.82	32.00	6.6	-1.17	20.00	17	V	6.6
1935	(8+9)-VI-2	2537	2.10	32.00	15	0.51	20.00	39	V	15
1935	(8+9)-II-4	-1768	-1.46	32.00	22	-0.35	20.00	57	V	22
1935	(8+9)-VIII-1	9052	7.48	32.00	4.3	1.81	20.00	11	V	4.3
1935	(8+9)-I-2	5794	4.79	32.00	6.7	1.16	20.00	17	V	6.7
1935	(8+9)-II-2	1720	1.42	32.00	23	0.34	20.00	58	V	23
1935	(8+9)-III-2	3845	3.18	32.00	10	0.77	20.00	26	V	10
1935	(8+9)-VI-3	-2568	-2.12	32.00	15	-0.51	20.00	39	V	15
1935	(8+9)-VI-4	-2584	-2.14	32.00	15	-0.52	20.00	39	V	15
1935	(8+9)-VII-1	10472	8.65	32.00	3.7	2.09	20.00	9.5	V	3.7
3870	1	-368	-0.30	19.20	63	-0.07	12.00	>100	V	63
3870	2	-765	-0.63	28.80	46	-0.15	18.00	>100	V	46
3870	3	-765	-0.63	28.80	46	-0.15	18.00	>100	V	46
3870	4	-368	-0.30	25.60	84	-0.07	16.00	>100	V	84
3870	5	-368	-0.30	25.60	84	-0.07	16.00	>100	V	84
3870	6	-368	-0.30	25.60	84	-0.07	16.00	>100	V	84
3870	7	-368	-0.30	25.60	84	-0.07	16.00	>100	V	84

Setto 23: origine (997.5,2661.7,193.5), direzione (0.825704,0.564103,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	1	-383	-2	1384	-0.14	-0.03	0.76	79.20	115.20	115.20	>100
0	2	-827	-4	2919	-0.29	-0.05	1.61	118.80	172.80	172.80	>100

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	3	-827	-4	2919	-0.29	-0.05	1.61	118.80	172.80	172.80	>100
0	4	-383	-2	1384	-0.14	-0.03	0.76	105.60	153.60	153.60	>100
0	5	-383	-2	1384	-0.14	-0.03	0.76	105.60	153.60	153.60	>100
0	6	-383	-2	1384	-0.14	-0.03	0.76	105.60	153.60	153.60	>100
0	7	-383	-2	1384	-0.14	-0.03	0.76	105.60	153.60	153.60	>100
0	(8+9)-VIII-4	1606	-9	-8043	0.57	-0.12	-4.44	132.00	192.00	192.00	36
0	(8+9)-IV-1	-1955	8	9073	-0.70	0.11	5.01	132.00	192.00	192.00	37
0	(8+9)-V-1	-1748	-13	7825	-0.62	-0.18	4.32	132.00	192.00	192.00	43
0	(8+9)-I-2	-1762	-19	8692	-0.63	-0.26	4.80	132.00	192.00	192.00	38
0	(8+9)-V-2	-2343	-26	11597	-0.83	-0.34	6.40	132.00	192.00	192.00	28
0	(8+9)-I-4	644	4	-3017	0.23	0.05	-1.66	132.00	192.00	192.00	94
0	(8+9)-V-3	1819	23	-9695	0.65	0.31	-5.35	132.00	192.00	192.00	29
0	(8+9)-II-2	-1613	-26	8995	-0.57	-0.34	4.96	132.00	192.00	192.00	36
0	(8+9)-V-4	1225	11	-5923	0.44	0.14	-3.27	132.00	192.00	192.00	47
0	(8+9)-II-4	-892	-19	5482	-0.32	-0.25	3.03	132.00	192.00	192.00	59
0	(8+9)-VI-1	194	14	-2708	0.07	0.19	-1.49	132.00	192.00	192.00	>100
0	(8+9)-III-2	-1065	-17	4896	-0.38	-0.23	2.70	132.00	192.00	192.00	66
0	(8+9)-VI-2	-1788	-28	9867	-0.64	-0.37	5.44	132.00	192.00	192.00	33
0	(8+9)-III-4	1341	6	-6813	0.48	0.09	-3.76	132.00	192.00	192.00	42
0	(8+9)-VI-3	1264	25	-7964	0.45	0.33	-4.39	132.00	192.00	192.00	36
0	(8+9)-IV-2	710	-18	-3659	0.25	-0.24	-2.02	132.00	192.00	192.00	73
0	(8+9)-VI-4	-717	-17	4611	-0.26	-0.22	2.54	132.00	192.00	192.00	69
0	(8+9)-IV-4	1432	-11	-7171	0.51	-0.15	-3.96	132.00	192.00	192.00	40
0	(8+9)-VII-1	-2445	-16	11621	-0.87	-0.21	6.41	132.00	192.00	192.00	29
0	(8+9)-II-1	368	16	-3580	0.13	0.21	-1.98	132.00	192.00	192.00	81
0	(8+9)-VII-2	-1646	-23	7801	-0.59	-0.31	4.30	132.00	192.00	192.00	42
0	(8+9)-III-1	-1865	-9	8715	-0.66	-0.12	4.81	132.00	192.00	192.00	39
0	(8+9)-VII-3	1122	21	-5899	0.40	0.28	-3.26	132.00	192.00	192.00	47
0	(8+9)-I-1	-1168	-7	4919	-0.42	-0.09	2.71	132.00	192.00	192.00	68
0	(8+9)-VII-4	1922	13	-9719	0.68	0.17	-5.36	132.00	192.00	192.00	29
0	(8+9)-III-3	541	14	-2994	0.19	0.19	-1.65	132.00	192.00	192.00	90
0	(8+9)-IV-3	-1234	15	5561	-0.44	0.21	3.07	132.00	192.00	192.00	59
0	(8+9)-II-3	1090	23	-7093	0.39	0.31	-3.91	132.00	192.00	192.00	40
0	(8+9)-VIII-1	-2130	6	9945	-0.76	0.09	5.49	132.00	192.00	192.00	34
0	(8+9)-I-3	1238	17	-6790	0.44	0.22	-3.75	132.00	192.00	192.00	42
0	(8+9)-VIII-3	-1059	17	4689	-0.38	0.23	2.59	132.00	192.00	192.00	68
1459	(8+9)-VIII-2	1143	81	-789	0.41	1.08	-0.44	132.00	192.00	192.00	91
Verifiche nella direzione secondaria											
0	(8+9)-VIII-4	-5864	84	-6034	-8.30	6.77	-35.14	132.00	192.00	192.00	4.5
0	(8+9)-VII-2	4695	180	1857	6.65	14.61	10.81	132.00	192.00	192.00	5.5
0	(8+9)-III-3	-9880	-109	-1885	-13.99	-8.86	-10.98	132.00	192.00	192.00	9.2
0	(8+9)-IV-2	-1653	149	-4162	-2.34	12.09	-24.24	132.00	192.00	192.00	5.3
0	(8+9)-III-4	-9341	-38	-4385	-13.23	-3.11	-25.54	132.00	192.00	192.00	6.5
0	(8+9)-VIII-2	-700	166	-3739	-0.99	13.48	-21.77	132.00	192.00	192.00	5.4
0	(8+9)-IV-1	-3449	-87	4171	-4.88	-7.08	24.29	132.00	192.00	192.00	6.1
0	(8+9)-VII-4	-12517	-96	-5796	-17.73	-7.77	-33.76	132.00	192.00	192.00	4.4
0	(8+9)-I-1	-1654	8	1104	-2.34	0.64	6.43	132.00	192.00	192.00	27
0	(8+9)-IV-3	-6708	-136	2722	-9.50	-11.00	15.85	132.00	192.00	192.00	7.0
0	(8+9)-I-3	-12515	-153	-3726	-17.72	-12.43	-21.70	132.00	192.00	192.00	5.4
0	(8+9)-IV-4	-4911	101	-5611	-6.95	8.17	-32.68	132.00	192.00	192.00	4.7
0	(8+9)-II-1	-12232	-234	-1965	-17.32	-18.96	-11.44	132.00	192.00	192.00	6.0
0	(8+9)-V-1	1522	65	2516	2.15	5.29	14.65	132.00	192.00	192.00	8.3
0	(8+9)-II-3	-15491	-282	-3414	-21.94	-22.88	-19.88	132.00	192.00	192.00	4.2
0	(8+9)-V-2	7330	224	3697	10.38	18.17	21.53	132.00	192.00	192.00	3.5
0	(8+9)-III-1	981	52	2945	1.39	4.20	17.15	132.00	192.00	192.00	8.2
0	(8+9)-V-3	-15691	-211	-5137	-22.22	-17.08	-29.92	132.00	192.00	192.00	3.9
0	(8+9)-VIII-3	-7660	-153	2299	-10.85	-12.39	13.39	132.00	192.00	192.00	7.3
0	(8+9)-V-4	-9882	-52	-3956	-13.99	-4.21	-23.04	132.00	192.00	192.00	6.8
0	(8+9)-VII-3	-13056	-167	-3296	-18.49	-13.52	-19.20	132.00	192.00	192.00	5.6
0	(8+9)-VI-1	-11280	-217	-1542	-15.97	-17.56	-8.98	132.00	192.00	192.00	6.9
0	(8+9)-I-4	-6706	6	-2544	-9.50	0.45	-14.82	132.00	192.00	192.00	12
0	(8+9)-VI-2	8083	313	2398	11.45	25.36	13.96	132.00	192.00	192.00	3.4
0	(8+9)-II-4	3872	247	525	5.48	20.04	3.06	132.00	192.00	192.00	6.2
0	(8+9)-VIII-1	-2497	-70	4595	-3.54	-5.68	26.76	132.00	192.00	192.00	5.9

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-I-2	4155	167	2286	5.88	13.51	13.31	132.00	192.00	192.00	5.4
0	(8+9)-II-2	7131	296	1974	10.10	23.96	11.50	132.00	192.00	192.00	3.8
0	(8+9)-III-2	1520	123	445	2.15	9.95	2.59	132.00	192.00	192.00	12
0	(8+9)-VI-3	-16443	-300	-3838	-23.29	-24.27	-22.35	132.00	192.00	192.00	3.9
0	(8+9)-VI-4	2919	230	102	4.13	18.65	0.59	132.00	192.00	192.00	7.6
0	(8+9)-VII-1	4156	109	4357	5.89	8.86	25.37	132.00	192.00	192.00	4.5
1935	1	-6602	4	-1366	-9.35	0.36	-7.96	79.20	115.20	115.20	13
1935	2	-13450	9	-2787	-19.05	0.73	-16.23	118.80	172.80	172.80	9.1
1935	3	-13450	9	-2787	-19.05	0.73	-16.23	118.80	172.80	172.80	9.1
1935	4	-6602	4	-1366	-9.35	0.36	-7.96	105.60	153.60	153.60	17
1935	5	-6602	4	-1366	-9.35	0.36	-7.96	105.60	153.60	153.60	17
1935	6	-6602	4	-1366	-9.35	0.36	-7.96	105.60	153.60	153.60	17
1935	7	-6602	4	-1366	-9.35	0.36	-7.96	105.60	153.60	153.60	17

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
730	(8+9)-VI-1	-200	0.05	6.40	Si	>100
730	(8+9)-VI-4	198	0.05	6.40	Si	>100
730	(8+9)-II-3	-224	0.06	6.40	Si	>100
730	(8+9)-VII-3	-136	0.04	6.40	Si	>100
730	(8+9)-II-1	-206	0.05	6.40	Si	>100
730	(8+9)-VII-2	133	0.03	6.40	Si	>100
730	(8+9)-VI-3	-230	0.06	6.40	Si	>100
730	(8+9)-I-1	-36	0.01	6.40	Si	>100
730	(8+9)-VI-2	227	0.06	6.40	Si	>100
730	(8+9)-III-2	113	0.03	6.40	Si	>100
730	(8+9)-II-4	204	0.05	6.40	Si	>100
730	(8+9)-III-3	-115	0.03	6.40	Si	>100
730	(8+9)-II-2	221	0.06	6.40	Si	>100
1459	1	-17	0.00	3.84	Si	>100
1459	2	-38	0.01	5.76	Si	>100
1459	3	-38	0.01	5.76	Si	>100
1459	4	-17	0.00	5.12	Si	>100
1459	5	-17	0.00	5.12	Si	>100
1459	6	-17	0.00	5.12	Si	>100
1459	7	-17	0.00	5.12	Si	>100
1459	(8+9)-VIII-4	-397	0.10	6.40	Si	62
1459	(8+9)-IV-1	358	0.09	6.40	Si	69
1459	(8+9)-I-4	-44	0.01	6.40	Si	>100
1459	(8+9)-IV-3	317	0.08	6.40	Si	78
1459	(8+9)-VII-1	211	0.05	6.40	Si	>100
1459	(8+9)-V-1	70	0.02	6.40	Si	>100
1459	(8+9)-I-3	-116	0.03	6.40	Si	>100
1459	(8+9)-V-3	-166	0.04	6.40	Si	>100
1459	(8+9)-I-2	92	0.02	6.40	Si	>100
1459	(8+9)-IV-2	-341	0.09	6.40	Si	73
1459	(8+9)-VII-4	-234	0.06	6.40	Si	>100
1459	(8+9)-V-2	142	0.04	6.40	Si	>100
1459	(8+9)-V-4	-93	0.02	6.40	Si	>100
1459	(8+9)-III-4	-184	0.05	6.40	Si	>100
1459	(8+9)-IV-4	-382	0.10	6.40	Si	65
1459	(8+9)-VIII-1	373	0.10	6.40	Si	66
1459	(8+9)-VIII-2	-326	0.08	6.40	Si	76
1459	(8+9)-VIII-3	302	0.08	6.40	Si	82
1459	(8+9)-III-1	161	0.04	6.40	Si	>100
Verifiche nella direzione secondaria						
0	(8+9)-VIII-4	-504	0.66	6.40	Si	9.7
0	(8+9)-VII-2	-337	0.44	6.40	Si	15
0	(8+9)-III-3	259	0.34	6.40	Si	19
0	(8+9)-IV-2	-584	0.76	6.40	Si	8.4
0	(8+9)-III-4	-70	0.09	6.40	Si	70
0	(8+9)-VIII-2	-604	0.79	6.40	Si	8.1

X	Comb.	Ty	τ_d	fvd	RS	Cs
0	(8+9)-IV-1	514	0.67	6.40	Si	9.5
0	(8+9)-VI-4	-134	0.17	6.40	Si	37
0	(8+9)-VII-3	327	0.43	6.40	Si	15
0	(8+9)-I-1	-50	0.07	6.40	Si	97
0	(8+9)-I-3	148	0.19	6.40	Si	33
0	(8+9)-IV-3	574	0.75	6.40	Si	8.5
0	(8+9)-II-1	144	0.19	6.40	Si	34
0	(8+9)-IV-4	-524	0.68	6.40	Si	9.3
0	(8+9)-II-3	204	0.27	6.40	Si	24
0	(8+9)-V-1	-119	0.16	6.40	Si	41
0	(8+9)-III-1	61	0.08	6.40	Si	81
0	(8+9)-V-2	-226	0.30	6.40	Si	22
0	(8+9)-VIII-3	594	0.78	6.40	Si	8.2
0	(8+9)-V-3	216	0.28	6.40	Si	23
0	(8+9)-I-2	-158	0.21	6.40	Si	31
0	(8+9)-V-4	109	0.14	6.40	Si	45
0	(8+9)-II-2	-214	0.28	6.40	Si	23
0	(8+9)-III-2	-269	0.35	6.40	Si	18
0	(8+9)-VIII-1	494	0.65	6.40	Si	9.9
0	(8+9)-I-4	41	0.05	6.40	Si	>100
0	(8+9)-II-4	-154	0.20	6.40	Si	32
0	(8+9)-VI-1	124	0.16	6.40	Si	40
0	(8+9)-VI-2	-234	0.31	6.40	Si	21
0	(8+9)-VI-3	224	0.29	6.40	Si	22
1935	(8+9)-VII-4	90	0.12	6.40	Si	54
1935	(8+9)-VII-1	-99	0.13	6.40	Si	49
3870	1	-14	0.02	3.84	Si	>100
3870	2	-31	0.04	5.76	Si	>100
3870	3	-31	0.04	5.76	Si	>100
3870	4	-14	0.02	5.12	Si	>100
3870	5	-14	0.02	5.12	Si	>100
3870	6	-14	0.02	5.12	Si	>100
3870	7	-14	0.02	5.12	Si	>100

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	1	2694	1.44	19.20	13	0.35	12.00	34	V	13
0	2	5642	3.01	28.80	9.6	0.73	18.00	25	V	9.6
0	3	5642	3.01	28.80	9.6	0.73	18.00	25	V	9.6
0	4	2694	1.44	25.60	18	0.35	16.00	46	V	18
0	5	2694	1.44	25.60	18	0.35	16.00	46	V	18
0	6	2694	1.44	25.60	18	0.35	16.00	46	V	18
0	7	2694	1.44	25.60	18	0.35	16.00	46	V	18
0	(8+9)-VIII-4	-6309	-3.37	32.00	9.5	-0.82	20.00	25	V	9.5
0	(8+9)-IV-3	7117	3.80	32.00	8.4	0.92	20.00	22	V	8.4
0	(8+9)-IV-1	9439	5.04	32.00	6.4	1.22	20.00	16	V	6.4
0	(8+9)-VIII-1	10018	5.35	32.00	6.0	1.29	20.00	15	V	6.0
0	(8+9)-VIII-3	6537	3.49	32.00	9.2	0.84	20.00	24	V	9.2
0	(8+9)-IV-4	-5730	-3.06	32.00	10	-0.74	20.00	27	V	10
730	(8+9)-II-1	-3838	-2.05	32.00	16	-0.50	20.00	40	V	16
730	(8+9)-VII-4	-10877	-5.81	32.00	5.5	-1.41	20.00	14	V	5.5
730	(8+9)-V-4	-8678	-4.63	32.00	6.9	-1.12	20.00	18	V	6.9
730	(8+9)-VI-1	-2792	-1.49	32.00	21	-0.36	20.00	55	V	21
1459	(8+9)-V-1	10211	5.45	32.00	5.9	1.32	20.00	15	V	5.9
1459	(8+9)-I-2	12084	6.45	32.00	5.0	1.56	20.00	13	V	5.0
1459	(8+9)-VI-2	10871	5.80	32.00	5.5	1.40	20.00	14	V	5.5
1459	(8+9)-III-4	-8429	-4.50	32.00	7.1	-1.09	20.00	18	V	7.1
1459	(8+9)-VI-3	-9191	-4.91	32.00	6.5	-1.19	20.00	17	V	6.5
1459	(8+9)-IV-2	3580	1.91	32.00	17	0.46	20.00	43	V	17
1459	(8+9)-VI-4	4056	2.17	32.00	15	0.52	20.00	38	V	15
1459	(8+9)-III-2	10086	5.38	32.00	5.9	1.30	20.00	15	V	5.9
1459	(8+9)-VII-1	12209	6.52	32.00	4.9	1.58	20.00	13	V	4.9

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
1459	(8+9)-V-2	14185	7.57	32.00	4.2	1.83	20.00	11	V	4.2
1459	(8+9)-VII-2	12187	6.51	32.00	4.9	1.57	20.00	13	V	4.9
1459	(8+9)-II-4	4686	2.50	32.00	13	0.61	20.00	33	V	13
1459	(8+9)-VII-3	-10508	-5.61	32.00	5.7	-1.36	20.00	15	V	5.7
1459	(8+9)-I-1	8110	4.33	32.00	7.4	1.05	20.00	19	V	7.4
1459	(8+9)-II-2	10240	5.47	32.00	5.9	1.32	20.00	15	V	5.9
1459	(8+9)-II-3	-8561	-4.57	32.00	7.0	-1.11	20.00	18	V	7.0
1459	(8+9)-III-3	-8407	-4.49	32.00	7.1	-1.09	20.00	18	V	7.1
1459	(8+9)-V-3	-12506	-6.68	32.00	4.8	-1.62	20.00	12	V	4.8
1459	(8+9)-I-4	-6431	-3.43	32.00	9.3	-0.83	20.00	24	V	9.3
1459	(8+9)-VIII-2	4210	2.25	32.00	14	0.54	20.00	37	V	14
1459	(8+9)-I-3	-10405	-5.55	32.00	5.8	-1.34	20.00	15	V	5.8
1459	(8+9)-III-1	10108	5.40	32.00	5.9	1.31	20.00	15	V	5.9
Verifiche nella direzione secondaria										
1935	(8+9)-VIII-4	-3690	-5.23	32.00	6.1	-1.26	20.00	16	V	6.1
1935	(8+9)-VII-1	6339	8.98	32.00	3.6	2.17	20.00	9.2	V	3.6
1935	(8+9)-III-2	3016	4.27	32.00	7.5	1.03	20.00	19	V	7.5
1935	(8+9)-III-3	-2168	-3.07	32.00	10	-0.74	20.00	27	V	10
1935	(8+9)-VIII-1	4537	6.43	32.00	5.0	1.55	20.00	13	V	5.0
1935	(8+9)-III-4	-3711	-5.25	32.00	6.1	-1.27	20.00	16	V	6.1
1935	(8+9)-VII-3	-3949	-5.59	32.00	5.7	-1.35	20.00	15	V	5.7
1935	(8+9)-IV-1	4003	5.67	32.00	5.6	1.37	20.00	15	V	5.6
1935	(8+9)-I-1	2582	3.66	32.00	8.8	0.88	20.00	23	V	8.8
1935	(8+9)-VI-4	2896	4.10	32.00	7.8	0.99	20.00	20	V	7.8
1935	(8+9)-I-3	-4144	-5.87	32.00	5.5	-1.42	20.00	14	V	5.5
1935	(8+9)-IV-3	1985	2.81	32.00	11	0.68	20.00	29	V	11
1935	(8+9)-II-1	-2582	-3.66	32.00	8.8	-0.88	20.00	23	V	8.8
1935	(8+9)-IV-4	-3156	-4.47	32.00	7.2	-1.08	20.00	18	V	7.2
1935	(8+9)-II-3	-4600	-6.51	32.00	4.9	-1.58	20.00	13	V	4.9
1935	(8+9)-V-1	4363	6.18	32.00	5.2	1.50	20.00	13	V	5.2
1935	(8+9)-III-1	4558	6.45	32.00	5.0	1.56	20.00	13	V	5.0
1935	(8+9)-V-2	6772	9.59	32.00	3.3	2.32	20.00	8.6	V	3.3
1935	(8+9)-VII-4	-5491	-7.78	32.00	4.1	-1.88	20.00	11	V	4.1
1935	(8+9)-V-3	-5925	-8.39	32.00	3.8	-2.03	20.00	9.9	V	3.8
1935	(8+9)-I-2	4991	7.07	32.00	4.5	1.71	20.00	12	V	4.5
1935	(8+9)-V-4	-3516	-4.98	32.00	6.4	-1.20	20.00	17	V	6.4
1935	(8+9)-II-2	5448	7.71	32.00	4.1	1.87	20.00	11	V	4.1
1935	(8+9)-VIII-3	1451	2.05	32.00	16	0.50	20.00	40	V	16
1935	(8+9)-VII-2	4797	6.79	32.00	4.7	1.64	20.00	12	V	4.7
1935	(8+9)-I-4	-1735	-2.46	32.00	13	-0.59	20.00	34	V	13
1935	(8+9)-II-4	3430	4.86	32.00	6.6	1.18	20.00	17	V	6.6
1935	(8+9)-VI-1	-2048	-2.90	32.00	11	-0.70	20.00	28	V	11
1935	(8+9)-VI-2	5982	8.47	32.00	3.8	2.05	20.00	9.8	V	3.8
1935	(8+9)-VI-3	-5135	-7.27	32.00	4.4	-1.76	20.00	11	V	4.4
3870	1	894	1.27	19.20	15	0.31	12.00	39	V	15
3870	2	1858	2.63	28.80	11	0.64	18.00	28	V	11
3870	3	1858	2.63	28.80	11	0.64	18.00	28	V	11
3870	4	894	1.27	25.60	20	0.31	16.00	52	V	20
3870	5	894	1.27	25.60	20	0.31	16.00	52	V	20
3870	6	894	1.27	25.60	20	0.31	16.00	52	V	20
3870	7	894	1.27	25.60	20	0.31	16.00	52	V	20
3870	(8+9)-VIII-2	1240	1.76	32.00	18	0.42	20.00	47	V	18
3870	(8+9)-IV-2	1159	1.64	32.00	19	0.40	20.00	50	V	19

Setto 24: origine (213.1,2125.8,25.0), direzione (0.825704,0.564103,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	1	237	0	-80	0.65	0.02	-2.66	79.20	115.20	115.20	32
0	2	470	0	-162	1.30	0.05	-5.37	118.80	172.80	172.80	24
0	3	470	0	-162	1.30	0.05	-5.37	118.80	172.80	172.80	24
0	4	237	0	-80	0.65	0.02	-2.66	105.60	153.60	153.60	42
0	5	237	0	-80	0.65	0.02	-2.66	105.60	153.60	153.60	42

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	6	237	0	-80	0.65	0.02	-2.66	105.60	153.60	153.60	42
0	7	237	0	-80	0.65	0.02	-2.66	105.60	153.60	153.60	42
0	(8+9)-V-3	2737	1	-536	7.54	0.09	-17.71	132.00	192.00	192.00	6.7
0	(8+9)-V-4	4173	1	-800	11.50	0.15	-26.46	132.00	192.00	192.00	4.4
0	(8+9)-VII-3	2682	1	-525	7.39	0.08	-17.34	132.00	192.00	192.00	6.8
0	(8+9)-III-3	1632	1	-341	4.50	0.06	-11.26	132.00	192.00	192.00	11
0	(8+9)-I-4	3124	1	-617	8.61	0.12	-20.38	132.00	192.00	192.00	5.8
0	(8+9)-III-4	3179	1	-628	8.76	0.13	-20.75	132.00	192.00	192.00	5.7
0	(8+9)-II-2	1888	1	-368	5.20	0.09	-12.18	132.00	192.00	192.00	9.7
0	(8+9)-VI-4	3547	1	-681	9.77	0.14	-22.50	132.00	192.00	192.00	5.2
0	(8+9)-II-4	3232	1	-625	8.90	0.14	-20.68	132.00	192.00	192.00	5.7
0	(8+9)-IV-2	2070	1	-406	5.70	0.11	-13.41	132.00	192.00	192.00	8.8
0	(8+9)-I-3	1687	1	-352	4.65	0.06	-11.63	132.00	192.00	192.00	10
0	(8+9)-VIII-2	1756	1	-350	4.84	0.10	-11.58	132.00	192.00	192.00	10
0	(8+9)-VII-4	4228	1	-812	11.65	0.15	-26.83	132.00	192.00	192.00	4.4
0	(8+9)-VIII-4	3730	2	-718	10.27	0.16	-23.73	132.00	192.00	192.00	4.9
0	(8+9)-VI-2	1573	1	-313	4.33	0.08	-10.36	132.00	192.00	192.00	11
0	(8+9)-IV-4	3415	2	-663	9.41	0.16	-21.90	132.00	192.00	192.00	5.4
3500	(8+9)-I-2	961	1	-217	2.65	0.07	-7.17	132.00	192.00	192.00	17
3500	(8+9)-VI-3	933	-1	-337	2.57	-0.09	-11.13	132.00	192.00	192.00	13
3500	(8+9)-II-1	2200	-0	-679	6.06	-0.05	-22.44	132.00	192.00	192.00	6.1
3500	(8+9)-I-1	2080	0	-581	5.73	0.04	-19.21	132.00	192.00	192.00	7.0
3500	(8+9)-V-2	1795	1	-421	4.95	0.06	-13.93	132.00	192.00	192.00	9.1
3500	(8+9)-III-2	928	1	-244	2.56	0.08	-8.07	132.00	192.00	192.00	16
3500	(8+9)-VI-1	2450	-1	-740	6.75	-0.05	-24.46	132.00	192.00	192.00	5.6
3500	(8+9)-III-1	2113	0	-554	5.82	0.04	-18.31	132.00	192.00	192.00	7.2
3500	(8+9)-VII-1	2947	0	-758	8.12	0.03	-25.06	132.00	192.00	192.00	5.2
3500	(8+9)-VII-2	1763	1	-449	4.86	0.06	-14.83	132.00	192.00	192.00	8.7
3500	(8+9)-V-1	2915	0	-786	8.03	0.03	-25.97	132.00	192.00	192.00	5.1
3500	(8+9)-IV-1	2309	-1	-587	6.36	-0.05	-19.42	132.00	192.00	192.00	6.7
3500	(8+9)-VIII-1	2559	-1	-649	7.05	-0.06	-21.44	132.00	192.00	192.00	6.0
3500	(8+9)-II-3	1183	-1	-398	3.26	-0.09	-13.15	132.00	192.00	192.00	11
3500	(8+9)-VIII-3	1042	-1	-245	2.87	-0.09	-8.11	132.00	192.00	192.00	16
3500	(8+9)-IV-3	1292	-1	-307	3.56	-0.09	-10.13	132.00	192.00	192.00	12
Verifiche nella direzione secondaria											
0	(8+9)-II-1	-5900	-158	-11870	-3.48	-5.34	-12.01	132.00	192.00	192.00	11
0	(8+9)-II-4	-911	165	9049	-0.54	5.59	9.16	132.00	192.00	192.00	13
0	(8+9)-VI-3	-5622	-166	-4088	-3.32	-5.61	-4.14	132.00	192.00	192.00	20
0	(8+9)-II-3	-5698	-167	-5597	-3.36	-5.64	-5.66	132.00	192.00	192.00	17
0	(8+9)-VI-1	-5976	-159	-13378	-3.53	-5.37	-13.54	132.00	192.00	192.00	10
0	(8+9)-V-2	-3276	65	-14697	-1.93	2.20	-14.87	132.00	192.00	192.00	11
0	(8+9)-VI-2	-1189	173	1268	-0.70	5.86	1.28	132.00	192.00	192.00	27
0	(8+9)-V-3	-3535	-58	11876	-2.09	-1.95	12.02	132.00	192.00	192.00	14
0	(8+9)-I-2	-3025	69	-9668	-1.79	2.32	-9.78	132.00	192.00	192.00	16
0	(8+9)-I-3	-3786	-61	6847	-2.24	-2.07	6.93	132.00	192.00	192.00	21
0	(8+9)-II-2	-1113	174	2776	-0.66	5.89	2.81	132.00	192.00	192.00	22
250	(8+9)-VIII-4	-2436	25	17228	-1.44	0.83	17.43	132.00	192.00	192.00	11
250	(8+9)-VII-2	-3717	21	-14397	-2.19	0.72	-14.57	132.00	192.00	192.00	13
250	(8+9)-IV-4	-2511	23	15559	-1.48	0.78	15.75	132.00	192.00	192.00	12
250	(8+9)-I-4	-2782	-6	13776	-1.64	-0.21	13.94	132.00	192.00	192.00	14
250	(8+9)-V-1	-4165	9	-21946	-2.46	0.30	-22.21	132.00	192.00	192.00	8.5
250	(8+9)-VIII-3	-3907	-24	-9568	-2.31	-0.81	-9.68	132.00	192.00	192.00	18
250	(8+9)-VIII-2	-2789	31	6960	-1.65	1.05	7.04	132.00	192.00	192.00	24
250	(8+9)-III-2	-3466	26	-8835	-2.05	0.87	-8.94	132.00	192.00	192.00	20
250	(8+9)-III-4	-2790	-4	14266	-1.65	-0.15	14.44	132.00	192.00	192.00	13
250	(8+9)-V-4	-2531	-2	19338	-1.49	-0.06	19.57	132.00	192.00	192.00	9.8
250	(8+9)-IV-2	-2714	32	8629	-1.60	1.09	8.73	132.00	192.00	192.00	20
250	(8+9)-VIII-1	-4261	-18	-19836	-2.52	-0.60	-20.07	132.00	192.00	192.00	9.3
250	(8+9)-I-1	-3914	13	-16383	-2.31	0.45	-16.58	132.00	192.00	192.00	11
250	(8+9)-VII-4	-2539	0	19828	-1.50	0.00	20.07	132.00	192.00	192.00	9.6
250	(8+9)-III-3	-3231	-19	6227	-1.91	-0.64	6.30	132.00	192.00	192.00	28
250	(8+9)-IV-3	-3982	-25	-11237	-2.35	-0.86	-11.37	132.00	192.00	192.00	16
250	(8+9)-III-1	-3907	11	-16874	-2.31	0.38	-17.08	132.00	192.00	192.00	11
250	(8+9)-IV-1	-4185	-16	-18167	-2.47	-0.55	-18.38	132.00	192.00	192.00	10

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
250	(8+9)-VII-3	-2980	-14	11790	-1.76	-0.49	11.93	132.00	192.00	192.00	15
250	(8+9)-VI-4	-2412	18	15593	-1.42	0.61	15.78	132.00	192.00	192.00	12
250	(8+9)-VII-1	-4158	7	-22436	-2.45	0.23	-22.70	132.00	192.00	192.00	8.4
500	1	-4347	4	-3003	-2.57	0.14	-3.04	79.20	115.20	115.20	36
500	2	-8803	8	-6092	-5.20	0.26	-6.16	118.80	172.80	172.80	26
500	3	-8803	8	-6092	-5.20	0.26	-6.16	118.80	172.80	172.80	26
500	4	-4347	4	-3003	-2.57	0.14	-3.04	105.60	153.60	153.60	48
500	5	-4347	4	-3003	-2.57	0.14	-3.04	105.60	153.60	153.60	48
500	6	-4347	4	-3003	-2.57	0.14	-3.04	105.60	153.60	153.60	48
500	7	-4347	4	-3003	-2.57	0.14	-3.04	105.60	153.60	153.60	48

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Ty kg	τ_d kg/cmq	fvd kg/cmq	RS	Cs
0	1	-1	0.00	3.84	Si	>100
0	2	-2	0.01	5.76	Si	>100
0	3	-2	0.01	5.76	Si	>100
0	4	-1	0.00	5.12	Si	>100
0	5	-1	0.00	5.12	Si	>100
0	6	-1	0.00	5.12	Si	>100
0	7	-1	0.00	5.12	Si	>100
0	(8+9)-III-2	-3	0.01	6.40	Si	>100
0	(8+9)-I-1	-4	0.01	6.40	Si	>100
0	(8+9)-VIII-3	1	0.00	6.40	Si	>100
0	(8+9)-VIII-2	-3	0.01	6.40	Si	>100
0	(8+9)-VII-2	-4	0.01	6.40	Si	>100
0	(8+9)-I-2	-2	0.00	6.40	Si	>100
0	(8+9)-IV-2	-3	0.01	6.40	Si	>100
0	(8+9)-III-3	1	0.00	6.40	Si	>100
3500	(8+9)-V-2	3	0.01	6.40	Si	>100
3500	(8+9)-II-1	6	0.01	6.40	Si	>100
3500	(8+9)-III-1	3	0.01	6.40	Si	>100
3500	(8+9)-VII-3	-3	0.01	6.40	Si	>100
3500	(8+9)-III-4	-2	0.00	6.40	Si	>100
3500	(8+9)-VII-4	-5	0.01	6.40	Si	>100
3500	(8+9)-II-3	5	0.01	6.40	Si	>100
3500	(8+9)-VIII-1	4	0.01	6.40	Si	>100
3500	(8+9)-IV-4	-2	0.00	6.40	Si	>100
3500	(8+9)-I-4	-3	0.01	6.40	Si	>100
3500	(8+9)-II-2	-5	0.01	6.40	Si	>100
3500	(8+9)-I-3	1	0.00	6.40	Si	>100
3500	(8+9)-V-4	-6	0.01	6.40	Si	>100
3500	(8+9)-VIII-4	-3	0.01	6.40	Si	>100
3500	(8+9)-VI-2	-4	0.01	6.40	Si	>100
3500	(8+9)-VI-3	4	0.01	6.40	Si	>100
3500	(8+9)-IV-3	2	0.00	6.40	Si	>100
3500	(8+9)-II-4	-5	0.01	6.40	Si	>100
3500	(8+9)-IV-1	3	0.01	6.40	Si	>100
3500	(8+9)-VII-1	5	0.01	6.40	Si	>100
3500	(8+9)-V-1	6	0.01	6.40	Si	>100
3500	(8+9)-V-3	-2	0.00	6.40	Si	>100
3500	(8+9)-VI-1	7	0.01	6.40	Si	>100
3500	(8+9)-VI-4	-6	0.01	6.40	Si	>100
Verifiche nella direzione secondaria						
0	(8+9)-III-2	-9	0.00	6.40	Si	>100
0	(8+9)-IV-4	-3	0.00	6.40	Si	>100
0	(8+9)-VIII-3	5	0.00	6.40	Si	>100
0	(8+9)-VII-3	9	0.01	6.40	Si	>100
0	(8+9)-VII-2	-11	0.01	6.40	Si	>100
0	(8+9)-VIII-2	-7	0.00	6.40	Si	>100
0	(8+9)-IV-3	5	0.00	6.40	Si	>100
0	(8+9)-IV-2	-7	0.00	6.40	Si	>100
0	(8+9)-III-3	7	0.00	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
250	(8+9)-VIII-4	3	0.00	6.40	Si	>100
250	(8+9)-IV-1	-3	0.00	6.40	Si	>100
250	(8+9)-III-1	-7	0.00	6.40	Si	>100
250	(8+9)-III-4	5	0.00	6.40	Si	>100
250	(8+9)-VIII-1	-5	0.00	6.40	Si	>100
250	(8+9)-VII-4	9	0.00	6.40	Si	>100
250	(8+9)-VII-1	-11	0.01	6.40	Si	>100
500	1	-2	0.00	3.84	Si	>100
500	2	-3	0.00	5.76	Si	>100
500	3	-3	0.00	5.76	Si	>100
500	4	-2	0.00	5.12	Si	>100
500	5	-2	0.00	5.12	Si	>100
500	6	-2	0.00	5.12	Si	>100
500	7	-2	0.00	5.12	Si	>100
500	(8+9)-V-2	-171	0.09	6.40	Si	68
500	(8+9)-I-4	-160	0.09	6.40	Si	73
500	(8+9)-I-1	157	0.09	6.40	Si	75
500	(8+9)-V-1	155	0.08	6.40	Si	76
500	(8+9)-I-2	-169	0.09	6.40	Si	70
500	(8+9)-V-4	-157	0.09	6.40	Si	75
500	(8+9)-I-3	166	0.09	6.40	Si	71
500	(8+9)-VI-2	-547	0.30	6.40	Si	21
500	(8+9)-II-4	-544	0.30	6.40	Si	22
500	(8+9)-VI-1	540	0.29	6.40	Si	22
500	(8+9)-VI-3	545	0.30	6.40	Si	22
500	(8+9)-V-3	169	0.09	6.40	Si	69
500	(8+9)-II-3	544	0.30	6.40	Si	22
500	(8+9)-II-2	-546	0.30	6.40	Si	21
500	(8+9)-II-1	541	0.29	6.40	Si	22
500	(8+9)-VI-4	-543	0.30	6.40	Si	22

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	1	1400	5.79	19.20	3.3	1.40	12.00	8.6	V	3.3
0	2	2831	11.70	28.80	2.5	2.83	18.00	6.4	V	2.5
0	3	2831	11.70	28.80	2.5	2.83	18.00	6.4	V	2.5
0	4	1400	5.79	25.60	4.4	1.40	16.00	11	V	4.4
0	5	1400	5.79	25.60	4.4	1.40	16.00	11	V	4.4
0	6	1400	5.79	25.60	4.4	1.40	16.00	11	V	4.4
0	7	1400	5.79	25.60	4.4	1.40	16.00	11	V	4.4
0	(8+9)-VIII-4	-3189	-13.18	32.00	2.4	-3.19	20.00	6.3	V	2.4
0	(8+9)-IV-1	4762	19.68	32.00	1.6	4.76	20.00	4.2	V	1.6
0	(8+9)-V-1	5542	22.90	32.00	1.4	5.54	20.00	3.6	V	1.4
0	(8+9)-I-2	2697	11.15	32.00	2.9	2.70	20.00	7.4	V	2.9
0	(8+9)-V-2	3925	16.22	32.00	2.0	3.93	20.00	5.1	V	2.0
0	(8+9)-VI-3	2537	10.48	32.00	3.1	2.54	20.00	7.9	V	3.1
0	(8+9)-IV-3	3242	13.39	32.00	2.4	3.24	20.00	6.2	V	2.4
0	(8+9)-IV-4	-2821	-11.66	32.00	2.7	-2.82	20.00	7.1	V	2.7
0	(8+9)-VIII-3	2873	11.87	32.00	2.7	2.87	20.00	7.0	V	2.7
0	(8+9)-VII-1	5643	23.32	32.00	1.4	5.64	20.00	3.5	V	1.4
0	(8+9)-III-2	2596	10.73	32.00	3.0	2.60	20.00	7.7	V	3.0
0	(8+9)-II-1	4426	18.29	32.00	1.7	4.43	20.00	4.5	V	1.7
0	(8+9)-VII-4	-3701	-15.29	32.00	2.1	-3.70	20.00	5.4	V	2.1
0	(8+9)-VI-4	-2853	-11.79	32.00	2.7	-2.85	20.00	7.0	V	2.7
0	(8+9)-I-1	4314	17.83	32.00	1.8	4.31	20.00	4.6	V	1.8
0	(8+9)-III-1	4415	18.24	32.00	1.8	4.42	20.00	4.5	V	1.8
0	(8+9)-VIII-1	5131	21.20	32.00	1.5	5.13	20.00	3.9	V	1.5
0	(8+9)-II-3	2906	12.01	32.00	2.7	2.91	20.00	6.9	V	2.7
0	(8+9)-VII-2	3824	15.80	32.00	2.0	3.82	20.00	5.2	V	2.0
0	(8+9)-V-4	-3600	-14.88	32.00	2.2	-3.60	20.00	5.6	V	2.2
0	(8+9)-VI-1	4795	19.81	32.00	1.6	4.79	20.00	4.2	V	1.6
3500	(8+9)-I-4	-2528	-10.45	32.00	3.1	-2.53	20.00	7.9	V	3.1

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
3500	(8+9)-V-3	-2233	-9.23	32.00	3.5	-2.23	20.00	9.0	V	3.5
3500	(8+9)-II-2	-1694	-7.00	32.00	4.6	-1.69	20.00	12	V	4.6
3500	(8+9)-III-4	-2542	-10.50	32.00	3.0	-2.54	20.00	7.9	V	3.0
3500	(8+9)-IV-2	-1740	-7.19	32.00	4.4	-1.74	20.00	11	V	4.4
3500	(8+9)-VII-3	-2219	-9.17	32.00	3.5	-2.22	20.00	9.0	V	3.5
3500	(8+9)-I-3	-1518	-6.27	32.00	5.1	-1.52	20.00	13	V	5.1
3500	(8+9)-III-3	-1504	-6.21	32.00	5.1	-1.50	20.00	13	V	5.1
3500	(8+9)-VIII-2	-1526	-6.30	32.00	5.1	-1.53	20.00	13	V	5.1
3500	(8+9)-II-4	-2624	-10.84	32.00	3.0	-2.62	20.00	7.6	V	3.0
3500	(8+9)-VI-2	-1480	-6.11	32.00	5.2	-1.48	20.00	14	V	5.2
Verifiche nella direzione secondaria										
0	1	-625	-0.37	19.20	52	-0.09	12.00	>100	V	52
0	2	-1258	-0.74	28.80	39	-0.18	18.00	>100	V	39
0	3	-1258	-0.74	28.80	39	-0.18	18.00	>100	V	39
0	4	-625	-0.37	25.60	69	-0.09	16.00	>100	V	69
0	5	-625	-0.37	25.60	69	-0.09	16.00	>100	V	69
0	6	-625	-0.37	25.60	69	-0.09	16.00	>100	V	69
0	7	-625	-0.37	25.60	69	-0.09	16.00	>100	V	69
0	(8+9)-V-3	-5634	-3.33	32.00	9.6	-0.80	20.00	25	V	9.6
0	(8+9)-II-3	2493	1.47	32.00	22	0.36	20.00	56	V	22
0	(8+9)-III-3	-3690	-2.18	32.00	15	-0.53	20.00	38	V	15
0	(8+9)-VII-3	-5685	-3.36	32.00	9.5	-0.81	20.00	25	V	9.5
0	(8+9)-VI-3	1894	1.12	32.00	29	0.27	20.00	74	V	29
0	(8+9)-I-4	-6203	-3.66	32.00	8.7	-0.89	20.00	23	V	8.7
0	(8+9)-VI-2	-2762	-1.63	32.00	20	-0.39	20.00	51	V	20
0	(8+9)-II-2	-3361	-1.98	32.00	16	-0.48	20.00	42	V	16
0	(8+9)-II-4	-6053	-3.57	32.00	9.0	-0.86	20.00	23	V	9.0
0	(8+9)-VI-1	5783	3.41	32.00	9.4	0.83	20.00	24	V	9.4
0	(8+9)-III-2	2822	1.67	32.00	19	0.40	20.00	50	V	19
0	(8+9)-II-1	5185	3.06	32.00	10	0.74	20.00	27	V	10
0	(8+9)-I-1	5335	3.15	32.00	10	0.76	20.00	26	V	10
0	(8+9)-VI-4	-6651	-3.93	32.00	8.1	-0.95	20.00	21	V	8.1
0	(8+9)-VII-2	4817	2.84	32.00	11	0.69	20.00	29	V	11
0	(8+9)-V-4	-8198	-4.84	32.00	6.6	-1.17	20.00	17	V	6.6
0	(8+9)-V-1	7330	4.33	32.00	7.4	1.05	20.00	19	V	7.4
0	(8+9)-V-2	4766	2.81	32.00	11	0.68	20.00	29	V	11
250	(8+9)-VIII-4	-7266	-4.29	32.00	7.5	-1.04	20.00	19	V	7.5
250	(8+9)-IV-2	-4007	-2.37	32.00	14	-0.57	20.00	35	V	14
250	(8+9)-I-3	-3687	-2.18	32.00	15	-0.53	20.00	38	V	15
250	(8+9)-IV-4	-6684	-3.95	32.00	8.1	-0.95	20.00	21	V	8.1
250	(8+9)-I-2	2819	1.66	32.00	19	0.40	20.00	50	V	19
250	(8+9)-IV-1	5816	3.43	32.00	9.3	0.83	20.00	24	V	9.3
250	(8+9)-VII-4	-8310	-4.91	32.00	6.5	-1.19	20.00	17	V	6.5
250	(8+9)-IV-3	3139	1.85	32.00	17	0.45	20.00	45	V	17
250	(8+9)-III-4	-6369	-3.76	32.00	8.5	-0.91	20.00	22	V	8.5
250	(8+9)-VII-1	7442	4.39	32.00	7.3	1.06	20.00	19	V	7.3
250	(8+9)-VIII-1	6398	3.78	32.00	8.5	0.91	20.00	22	V	8.5
250	(8+9)-VIII-2	-3425	-2.02	32.00	16	-0.49	20.00	41	V	16
250	(8+9)-VIII-3	2557	1.51	32.00	21	0.37	20.00	55	V	21
250	(8+9)-III-1	5501	3.25	32.00	9.9	0.79	20.00	25	V	9.9

Setto 25: origine (213.1,2125.9,328.5), direzione (0.825704,0.564103,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	(8+9)-VIII-4	-6327	-8	-2338	-7.45	-0.36	-14.11	132.00	192.00	192.00	13
0	(8+9)-IV-1	4785	11	1847	5.63	0.47	11.15	132.00	192.00	192.00	9.7
0	(8+9)-VI-1	3101	8	1704	3.65	0.38	10.29	132.00	192.00	192.00	12
0	(8+9)-III-1	4451	-0	1713	5.24	-0.02	10.34	132.00	192.00	192.00	11
0	(8+9)-IV-2	-3580	-11	-1309	-4.22	-0.49	-7.90	132.00	192.00	192.00	23
0	(8+9)-VII-1	6196	-0	2369	7.29	-0.01	14.30	132.00	192.00	192.00	7.7
0	(8+9)-VIII-2	-3057	-11	-1112	-3.60	-0.48	-6.71	132.00	192.00	192.00	26
0	(8+9)-III-3	-2959	9	-1060	-3.48	0.41	-6.40	132.00	192.00	192.00	28

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-VII-3	-4705	9	-1716	-5.54	0.40	-10.36	132.00	192.00	192.00	18
0	(8+9)-III-4	-5469	3	-2007	-6.44	0.13	-12.11	132.00	192.00	192.00	15
0	(8+9)-I-2	2603	-6	868	3.06	-0.28	5.24	132.00	192.00	192.00	19
0	(8+9)-VI-4	-4119	-6	-1998	-4.85	-0.27	-12.06	132.00	192.00	192.00	15
0	(8+9)-I-4	-4807	4	-1905	-5.66	0.16	-11.50	132.00	192.00	192.00	16
0	(8+9)-II-2	-1373	-9	-970	-1.62	-0.39	-5.85	132.00	192.00	192.00	31
0	(8+9)-IV-3	2562	13	1015	3.02	0.60	6.13	132.00	192.00	192.00	17
0	(8+9)-II-4	-3596	-6	-1801	-4.23	-0.26	-10.88	132.00	192.00	192.00	17
0	(8+9)-IV-4	-5803	-8	-2141	-6.83	-0.36	-12.92	132.00	192.00	192.00	14
0	(8+9)-VIII-1	5309	11	2044	6.25	0.47	12.34	132.00	192.00	192.00	8.8
0	(8+9)-V-1	5534	-1	2267	6.51	-0.04	13.69	132.00	192.00	192.00	8.3
0	(8+9)-I-3	-3622	9	-1162	-4.26	0.39	-7.01	132.00	192.00	192.00	26
0	(8+9)-VII-2	3687	-7	1422	4.34	-0.30	8.59	132.00	192.00	192.00	13
0	(8+9)-VIII-3	2038	13	818	2.40	0.59	4.94	132.00	192.00	192.00	21
0	(8+9)-I-1	3788	-1	1611	4.46	-0.05	9.73	132.00	192.00	192.00	12
0	(8+9)-II-1	2577	8	1508	3.03	0.37	9.10	132.00	192.00	192.00	14
0	(8+9)-V-2	4349	-6	1524	5.12	-0.27	9.20	132.00	192.00	192.00	11
0	(8+9)-V-3	-5367	9	-1818	-6.32	0.38	-10.98	132.00	192.00	192.00	17
0	(8+9)-V-4	-6552	3	-2561	-7.71	0.15	-15.46	132.00	192.00	192.00	12
1750	1	2690	1	677	3.17	0.02	4.09	79.20	115.20	115.20	13
1750	2	5519	1	1392	6.50	0.05	8.40	118.80	172.80	172.80	9.7
1750	3	5519	1	1392	6.50	0.05	8.40	118.80	172.80	172.80	9.7
1750	4	2690	1	677	3.17	0.02	4.09	105.60	153.60	153.60	18
1750	5	2690	1	677	3.17	0.02	4.09	105.60	153.60	153.60	18
1750	6	2690	1	677	3.17	0.02	4.09	105.60	153.60	153.60	18
1750	7	2690	1	677	3.17	0.02	4.09	105.60	153.60	153.60	18
1750	(8+9)-VI-2	2493	-2	335	2.93	-0.08	2.02	132.00	192.00	192.00	30
3500	(8+9)-VII-4	3768	1	1680	4.44	0.06	10.14	132.00	192.00	192.00	12
3500	(8+9)-II-3	-1883	14	-1261	-2.22	0.61	-7.61	132.00	192.00	192.00	23
3500	(8+9)-III-2	-1643	-8	-1363	-1.93	-0.35	-8.23	132.00	192.00	192.00	22
3500	(8+9)-VI-3	-1554	14	-1092	-1.83	0.62	-6.59	132.00	192.00	192.00	27
Verifiche nella direzione secondaria											
0	1	-7419	3	-2555	-4.38	0.11	-2.59	79.20	115.20	115.20	40
0	2	-15215	7	-5229	-8.98	0.22	-5.29	118.80	172.80	172.80	29
0	3	-15215	7	-5229	-8.98	0.22	-5.29	118.80	172.80	172.80	29
0	4	-7419	3	-2555	-4.38	0.11	-2.59	105.60	153.60	153.60	54
0	5	-7419	3	-2555	-4.38	0.11	-2.59	105.60	153.60	153.60	54
0	6	-7419	3	-2555	-4.38	0.11	-2.59	105.60	153.60	153.60	54
0	7	-7419	3	-2555	-4.38	0.11	-2.59	105.60	153.60	153.60	54
0	(8+9)-VIII-4	-4285	4	-7516	-2.53	0.13	-7.61	132.00	192.00	192.00	25
0	(8+9)-V-2	-5114	14	3498	-3.02	0.49	3.54	132.00	192.00	192.00	47
0	(8+9)-VI-4	-2697	42	-4428	-1.59	1.40	-4.48	132.00	192.00	192.00	33
0	(8+9)-IV-2	-4606	4	-4700	-2.72	0.13	-4.76	132.00	192.00	192.00	39
0	(8+9)-III-3	-4910	2	-4366	-2.90	0.07	-4.42	132.00	192.00	192.00	42
0	(8+9)-I-4	-4045	14	-5887	-2.39	0.49	-5.96	132.00	192.00	192.00	30
0	(8+9)-III-4	-4521	3	-6813	-2.67	0.11	-6.89	132.00	192.00	192.00	27
0	(8+9)-II-2	-3017	41	-1612	-1.78	1.40	-1.63	132.00	192.00	192.00	63
0	(8+9)-VI-3	-7170	-37	-2446	-4.23	-1.26	-2.47	132.00	192.00	192.00	50
0	(8+9)-II-4	-2769	42	-3905	-1.63	1.41	-3.95	132.00	192.00	192.00	36
0	(8+9)-V-4	-3804	14	-7628	-2.25	0.46	-7.72	132.00	192.00	192.00	23
0	(8+9)-VII-4	-4280	2	-8555	-2.53	0.08	-8.66	132.00	192.00	192.00	22
0	(8+9)-VII-3	-4669	1	-6107	-2.76	0.05	-6.18	132.00	192.00	192.00	31
0	(8+9)-VIII-2	-4678	4	-4178	-2.76	0.14	-4.23	132.00	192.00	192.00	44
0	(8+9)-V-3	-5146	-10	-7034	-3.04	-0.33	-7.12	132.00	192.00	192.00	26
0	(8+9)-IV-4	-4358	4	-6993	-2.57	0.14	-7.08	132.00	192.00	192.00	26
0	(8+9)-I-3	-5387	-9	-5292	-3.18	-0.31	-5.36	132.00	192.00	192.00	34
585	(8+9)-V-1	-4497	8	5254	-2.65	0.26	5.32	132.00	192.00	192.00	34
585	(8+9)-I-2	-4290	-8	2041	-2.53	-0.26	2.07	132.00	192.00	192.00	81
585	(8+9)-VII-2	-4369	-2	3393	-2.58	-0.06	3.43	132.00	192.00	192.00	54
585	(8+9)-IV-3	-4406	8	2537	-2.60	0.27	2.57	132.00	192.00	192.00	67
585	(8+9)-III-1	-4418	2	3902	-2.61	0.07	3.95	132.00	192.00	192.00	47
585	(8+9)-VI-1	-4559	26	5018	-2.69	0.88	5.08	132.00	192.00	192.00	32
585	(8+9)-II-3	-4480	27	3129	-2.64	0.91	3.17	132.00	192.00	192.00	47
585	(8+9)-VII-1	-4475	2	5076	-2.64	0.07	5.14	132.00	192.00	192.00	37

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
585	(8+9)-I-1	-4440	8	4080	-2.62	0.26	4.13	132.00	192.00	192.00	43
585	(8+9)-VI-2	-4058	-25	-1778	-2.40	-0.83	-1.80	132.00	192.00	192.00	72
585	(8+9)-III-2	-4312	-2	2219	-2.55	-0.07	2.25	132.00	192.00	192.00	82
585	(8+9)-VIII-1	-4486	7	4426	-2.65	0.25	4.48	132.00	192.00	192.00	40
585	(8+9)-II-1	-4542	26	4665	-2.68	0.88	4.72	132.00	192.00	192.00	34
585	(8+9)-VIII-3	-4389	8	2185	-2.59	0.27	2.21	132.00	192.00	192.00	76
585	(8+9)-IV-1	-4469	7	4074	-2.64	0.25	4.12	132.00	192.00	192.00	44

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
0	1	6	0.01	3.84	Si	>100
0	2	13	0.01	5.76	Si	>100
0	3	13	0.01	5.76	Si	>100
0	4	6	0.01	5.12	Si	>100
0	5	6	0.01	5.12	Si	>100
0	6	6	0.01	5.12	Si	>100
0	7	6	0.01	5.12	Si	>100
0	(8+9)-IV-3	3	0.00	6.40	Si	>100
0	(8+9)-VII-4	5	0.00	6.40	Si	>100
0	(8+9)-III-1	4	0.00	6.40	Si	>100
0	(8+9)-VIII-3	4	0.00	6.40	Si	>100
0	(8+9)-III-2	4	0.00	6.40	Si	>100
0	(8+9)-VIII-1	3	0.00	6.40	Si	>100
0	(8+9)-III-3	4	0.00	6.40	Si	>100
0	(8+9)-IV-4	5	0.00	6.40	Si	>100
0	(8+9)-VIII-2	5	0.00	6.40	Si	>100
0	(8+9)-VIII-4	5	0.00	6.40	Si	>100
0	(8+9)-VII-3	5	0.00	6.40	Si	>100
0	(8+9)-III-4	5	0.00	6.40	Si	>100
0	(8+9)-IV-1	3	0.00	6.40	Si	>100
0	(8+9)-IV-2	5	0.00	6.40	Si	>100
1750	(8+9)-VII-2	-4	0.00	6.40	Si	>100
1750	(8+9)-VII-1	-4	0.00	6.40	Si	>100
3500	(8+9)-I-1	-46	0.04	6.40	Si	>100
3500	(8+9)-VI-4	163	0.14	6.40	Si	46
3500	(8+9)-II-4	163	0.14	6.40	Si	46
3500	(8+9)-II-3	-159	0.14	6.40	Si	47
3500	(8+9)-V-3	-46	0.04	6.40	Si	>100
3500	(8+9)-II-2	163	0.14	6.40	Si	46
3500	(8+9)-VI-1	-159	0.14	6.40	Si	47
3500	(8+9)-II-1	-159	0.14	6.40	Si	47
3500	(8+9)-V-1	-47	0.04	6.40	Si	>100
3500	(8+9)-V-4	51	0.04	6.40	Si	>100
3500	(8+9)-VI-2	163	0.14	6.40	Si	46
3500	(8+9)-V-2	50	0.04	6.40	Si	>100
3500	(8+9)-I-4	51	0.04	6.40	Si	>100
3500	(8+9)-I-3	-46	0.04	6.40	Si	>100
3500	(8+9)-I-2	50	0.04	6.40	Si	>100
3500	(8+9)-VI-3	-159	0.14	6.40	Si	47
Verifiche nella direzione secondaria						
0	(8+9)-V-2	-256	0.14	6.40	Si	46
0	(8+9)-VII-3	2	0.00	6.40	Si	>100
0	(8+9)-II-3	837	0.46	6.40	Si	14
0	(8+9)-II-4	-838	0.46	6.40	Si	14
0	(8+9)-VII-4	3	0.00	6.40	Si	>100
0	(8+9)-III-1	-4	0.00	6.40	Si	>100
0	(8+9)-VII-1	-5	0.00	6.40	Si	>100
0	(8+9)-VI-3	838	0.46	6.40	Si	14
0	(8+9)-I-1	248	0.13	6.40	Si	47
0	(8+9)-VI-2	-840	0.46	6.40	Si	14
0	(8+9)-I-3	253	0.14	6.40	Si	46
0	(8+9)-VI-1	835	0.46	6.40	Si	14

X	Comb.	Ty	τ_d	fvd	RS	Cs
0	(8+9)-II-1	836	0.46	6.40	Si	14
0	(8+9)-IV-1	-3	0.00	6.40	Si	>100
0	(8+9)-VIII-1	-4	0.00	6.40	Si	>100
0	(8+9)-V-4	-249	0.14	6.40	Si	47
0	(8+9)-VI-4	-838	0.46	6.40	Si	14
0	(8+9)-I-4	-250	0.14	6.40	Si	47
0	(8+9)-II-2	-840	0.46	6.40	Si	14
0	(8+9)-V-3	254	0.14	6.40	Si	46
0	(8+9)-I-2	-255	0.14	6.40	Si	46
0	(8+9)-V-1	247	0.13	6.40	Si	48
585	(8+9)-VIII-3	-2	0.00	6.40	Si	>100
585	(8+9)-IV-3	-2	0.00	6.40	Si	>100
1170	1	-4	0.00	3.84	Si	>100
1170	2	-8	0.00	5.76	Si	>100
1170	3	-8	0.00	5.76	Si	>100
1170	4	-4	0.00	5.12	Si	>100
1170	5	-4	0.00	5.12	Si	>100
1170	6	-4	0.00	5.12	Si	>100
1170	7	-4	0.00	5.12	Si	>100
1170	(8+9)-VIII-4	-3	0.00	6.40	Si	>100
1170	(8+9)-VII-2	-5	0.00	6.40	Si	>100
1170	(8+9)-III-2	-4	0.00	6.40	Si	>100
1170	(8+9)-III-3	-1	0.00	6.40	Si	>100
1170	(8+9)-III-4	-2	0.00	6.40	Si	>100
1170	(8+9)-VIII-2	-4	0.00	6.40	Si	>100
1170	(8+9)-IV-2	-4	0.00	6.40	Si	>100
1170	(8+9)-IV-4	-4	0.00	6.40	Si	>100

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	1	-3970	-7.01	19.20	2.7	-1.70	12.00	7.1	V	2.7
0	2	-8176	-14.44	28.80	2.0	-3.49	18.00	5.2	V	2.0
0	3	-8176	-14.44	28.80	2.0	-3.49	18.00	5.2	V	2.0
0	4	-3970	-7.01	25.60	3.7	-1.70	16.00	9.4	V	3.7
0	5	-3970	-7.01	25.60	3.7	-1.70	16.00	9.4	V	3.7
0	6	-3970	-7.01	25.60	3.7	-1.70	16.00	9.4	V	3.7
0	7	-3970	-7.01	25.60	3.7	-1.70	16.00	9.4	V	3.7
0	(8+9)-IV-4	-5110	-9.02	32.00	3.5	-2.18	20.00	9.2	V	3.5
0	(8+9)-VII-4	-5758	-10.17	32.00	3.1	-2.46	20.00	8.1	V	3.1
0	(8+9)-VI-4	-4029	-7.12	32.00	4.5	-1.72	20.00	12	V	4.5
0	(8+9)-VIII-2	-3868	-6.83	32.00	4.7	-1.65	20.00	12	V	4.7
0	(8+9)-VI-2	-2556	-4.51	32.00	7.1	-1.09	20.00	18	V	7.1
0	(8+9)-I-4	-4592	-8.11	32.00	3.9	-1.96	20.00	10	V	3.9
0	(8+9)-III-3	-3868	-6.83	32.00	4.7	-1.65	20.00	12	V	4.7
0	(8+9)-II-2	-2787	-4.92	32.00	6.5	-1.19	20.00	17	V	6.5
0	(8+9)-III-4	-4985	-8.80	32.00	3.6	-2.13	20.00	9.4	V	3.6
0	(8+9)-VIII-4	-5342	-9.43	32.00	3.4	-2.28	20.00	8.8	V	3.4
0	(8+9)-VII-3	-4640	-8.19	32.00	3.9	-1.98	20.00	10	V	3.9
0	(8+9)-I-3	-4262	-7.53	32.00	4.3	-1.82	20.00	11	V	4.3
0	(8+9)-V-4	-5364	-9.47	32.00	3.4	-2.29	20.00	8.7	V	3.4
0	(8+9)-IV-2	-4100	-7.24	32.00	4.4	-1.75	20.00	11	V	4.4
0	(8+9)-V-3	-5034	-8.89	32.00	3.6	-2.15	20.00	9.3	V	3.6
0	(8+9)-II-4	-3798	-6.71	32.00	4.8	-1.62	20.00	12	V	4.8
3500	(8+9)-V-1	5273	9.31	32.00	3.4	2.25	20.00	8.9	V	3.4
3500	(8+9)-VIII-1	4936	8.72	32.00	3.7	2.11	20.00	9.5	V	3.7
3500	(8+9)-V-2	4202	7.42	32.00	4.3	1.80	20.00	11	V	4.3
3500	(8+9)-I-2	3476	6.14	32.00	5.2	1.49	20.00	13	V	5.2
3500	(8+9)-IV-1	4718	8.33	32.00	3.8	2.02	20.00	9.9	V	3.8
3500	(8+9)-VIII-3	3554	6.28	32.00	5.1	1.52	20.00	13	V	5.1
3500	(8+9)-III-2	3468	6.12	32.00	5.2	1.48	20.00	13	V	5.2
3500	(8+9)-I-1	4547	8.03	32.00	4.0	1.94	20.00	10	V	4.0
3500	(8+9)-III-1	4555	8.04	32.00	4.0	1.95	20.00	10	V	4.0

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
3500	(8+9)-VII-2	4194	7.41	32.00	4.3	1.79	20.00	11	V	4.3
3500	(8+9)-II-3	3746	6.62	32.00	4.8	1.60	20.00	12	V	4.8
3500	(8+9)-II-1	4692	8.29	32.00	3.9	2.01	20.00	10.0	V	3.9
3500	(8+9)-IV-3	3772	6.66	32.00	4.8	1.61	20.00	12	V	4.8
3500	(8+9)-VI-1	4910	8.67	32.00	3.7	2.10	20.00	9.5	V	3.7
3500	(8+9)-VI-3	3528	6.23	32.00	5.1	1.51	20.00	13	V	5.1
3500	(8+9)-VII-1	5280	9.32	32.00	3.4	2.26	20.00	8.9	V	3.4
Verifiche nella direzione secondaria										
585	(8+9)-I-2	5219	3.08	32.00	10	0.75	20.00	27	V	10
585	(8+9)-VIII-2	-3808	-2.25	32.00	14	-0.54	20.00	37	V	14
585	(8+9)-V-3	-7100	-4.19	32.00	7.6	-1.01	20.00	20	V	7.6
585	(8+9)-V-2	7899	4.66	32.00	6.9	1.13	20.00	18	V	6.9
585	(8+9)-IV-2	-4612	-2.72	32.00	12	-0.66	20.00	30	V	12
585	(8+9)-I-3	-4420	-2.61	32.00	12	-0.63	20.00	32	V	12
1170	1	712	0.42	19.20	46	0.10	12.00	>100	V	46
1170	2	1478	0.87	28.80	33	0.21	18.00	85	V	33
1170	3	1478	0.87	28.80	33	0.21	18.00	85	V	33
1170	4	712	0.42	25.60	61	0.10	16.00	>100	V	61
1170	5	712	0.42	25.60	61	0.10	16.00	>100	V	61
1170	6	712	0.42	25.60	61	0.10	16.00	>100	V	61
1170	7	712	0.42	25.60	61	0.10	16.00	>100	V	61
1170	(8+9)-VIII-4	-8795	-5.19	32.00	6.2	-1.26	20.00	16	V	6.2
1170	(8+9)-V-1	11125	6.57	32.00	4.9	1.59	20.00	13	V	4.9
1170	(8+9)-I-1	8429	4.98	32.00	6.4	1.20	20.00	17	V	6.4
1170	(8+9)-VI-1	10031	5.92	32.00	5.4	1.43	20.00	14	V	5.4
1170	(8+9)-III-1	8353	4.93	32.00	6.5	1.19	20.00	17	V	6.5
1170	(8+9)-VI-2	-3925	-2.32	32.00	14	-0.56	20.00	36	V	14
1170	(8+9)-III-3	-3338	-1.97	32.00	16	-0.48	20.00	42	V	16
1170	(8+9)-VI-3	4906	2.90	32.00	11	0.70	20.00	29	V	11
1170	(8+9)-IV-1	8967	5.29	32.00	6.0	1.28	20.00	16	V	6.0
1170	(8+9)-VI-4	-9050	-5.34	32.00	6.0	-1.29	20.00	15	V	6.0
1170	(8+9)-IV-3	5460	3.22	32.00	9.9	0.78	20.00	26	V	9.9
1170	(8+9)-VII-1	11049	6.52	32.00	4.9	1.58	20.00	13	V	4.9
1170	(8+9)-II-3	5715	3.37	32.00	9.5	0.82	20.00	24	V	9.5
1170	(8+9)-VII-2	7015	4.14	32.00	7.7	1.00	20.00	20	V	7.7
1170	(8+9)-II-1	9222	5.44	32.00	5.9	1.32	20.00	15	V	5.9
1170	(8+9)-VII-3	-6034	-3.56	32.00	9.0	-0.86	20.00	23	V	9.0
1170	(8+9)-III-2	4319	2.55	32.00	13	0.62	20.00	32	V	13
1170	(8+9)-VII-4	-10068	-5.94	32.00	5.4	-1.44	20.00	14	V	5.4
1170	(8+9)-II-2	-4734	-2.79	32.00	11	-0.68	20.00	30	V	11
1170	(8+9)-V-4	-10144	-5.99	32.00	5.3	-1.45	20.00	14	V	5.3
1170	(8+9)-III-4	-7372	-4.35	32.00	7.4	-1.05	20.00	19	V	7.4
1170	(8+9)-IV-4	-7986	-4.71	32.00	6.8	-1.14	20.00	18	V	6.8
1170	(8+9)-VIII-1	9776	5.77	32.00	5.5	1.40	20.00	14	V	5.5
1170	(8+9)-I-4	-7448	-4.40	32.00	7.3	-1.06	20.00	19	V	7.3
1170	(8+9)-VIII-3	4651	2.75	32.00	12	0.66	20.00	30	V	12
1170	(8+9)-II-4	-8241	-4.86	32.00	6.6	-1.18	20.00	17	V	6.6

Setto 26: origine (708.6,2464.3,25.0), direzione (0.825704,0.564103,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	2	-656	1	153	-1.81	0.07	5.06	118.80	172.80	172.80	34
0	3	-656	1	153	-1.81	0.07	5.06	118.80	172.80	172.80	34
0	(8+9)-III-3	1089	-1	-244	3.00	-0.07	-8.06	132.00	192.00	192.00	15
0	(8+9)-I-3	2413	-1	-481	6.65	-0.06	-15.91	132.00	192.00	192.00	7.5
0	(8+9)-V-4	2036	-0	-516	5.61	-0.02	-17.07	132.00	192.00	192.00	7.6
0	(8+9)-VII-4	3360	-0	-754	9.26	-0.02	-24.92	132.00	192.00	192.00	5.0
0	(8+9)-IV-4	2560	1	-577	7.05	0.13	-19.06	132.00	192.00	192.00	6.5
0	(8+9)-VIII-4	2847	1	-641	7.84	0.12	-21.18	132.00	192.00	192.00	5.9
0	(8+9)-III-4	2401	0	-540	6.61	0.01	-17.86	132.00	192.00	192.00	7.0
0	(8+9)-V-3	3371	-1	-695	9.29	-0.09	-22.97	132.00	192.00	192.00	5.3
0	(8+9)-I-4	1078	0	-303	2.97	0.00	-10.02	132.00	192.00	192.00	13

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-VII-3	2048	-1	-457	5.64	-0.09	-15.12	132.00	192.00	192.00	8.2
1750	1	370	-0	-31	1.02	-0.01	-1.03	79.20	115.20	115.20	46
1750	4	370	-0	-31	1.02	-0.01	-1.03	105.60	153.60	153.60	61
1750	5	370	-0	-31	1.02	-0.01	-1.03	105.60	153.60	153.60	61
1750	6	370	-0	-31	1.02	-0.01	-1.03	105.60	153.60	153.60	61
1750	7	370	-0	-31	1.02	-0.01	-1.03	105.60	153.60	153.60	61
3500	(8+9)-VI-1	-1077	4	359	-2.97	0.44	11.85	132.00	192.00	192.00	16
3500	(8+9)-VIII-2	-1142	-6	411	-3.15	-0.66	13.60	132.00	192.00	192.00	13
3500	(8+9)-III-2	1554	-5	-297	4.28	-0.50	-9.83	132.00	192.00	192.00	12
3500	(8+9)-VIII-3	1582	7	-447	4.36	0.69	-14.78	132.00	192.00	192.00	8.8
3500	(8+9)-IV-2	-1443	-6	485	-3.98	-0.59	16.04	132.00	192.00	192.00	11
3500	(8+9)-I-1	1573	-2	-313	4.33	-0.17	-10.36	132.00	192.00	192.00	11
3500	(8+9)-III-1	2914	-2	-684	8.03	-0.20	-22.63	132.00	192.00	192.00	5.6
3500	(8+9)-V-1	2576	-4	-560	7.10	-0.39	-18.50	132.00	192.00	192.00	6.6
3500	(8+9)-VII-1	3917	-4	-931	10.79	-0.41	-30.77	132.00	192.00	192.00	4.1
3500	(8+9)-V-2	3897	-7	-915	10.74	-0.74	-30.25	132.00	192.00	192.00	4.1
3500	(8+9)-VII-2	2556	-7	-544	7.04	-0.71	-17.98	132.00	192.00	192.00	6.6
3500	(8+9)-II-3	-2586	7	716	-7.12	0.72	23.68	132.00	192.00	192.00	7.8
3500	(8+9)-II-1	-1378	5	432	-3.80	0.50	14.30	132.00	192.00	192.00	13
3500	(8+9)-VI-2	3326	-7	-826	9.16	-0.75	-27.31	132.00	192.00	192.00	4.6
3500	(8+9)-I-2	2894	-5	-669	7.97	-0.53	-22.10	132.00	192.00	192.00	5.6
3500	(8+9)-II-2	3025	-7	-752	8.33	-0.68	-24.86	132.00	192.00	192.00	5.1
3500	(8+9)-VI-3	-2887	8	790	-7.95	0.78	26.12	132.00	192.00	192.00	7.0
3500	(8+9)-II-4	1817	-4	-468	5.00	-0.46	-15.48	132.00	192.00	192.00	8.3
3500	(8+9)-VIII-1	3392	3	-879	9.34	0.34	-29.05	132.00	192.00	192.00	4.5
3500	(8+9)-IV-1	3091	4	-805	8.52	0.41	-26.61	132.00	192.00	192.00	4.9
3500	(8+9)-IV-3	1882	6	-521	5.19	0.63	-17.22	132.00	192.00	192.00	7.6
3500	(8+9)-VI-4	1516	-4	-394	4.18	-0.40	-13.04	132.00	192.00	192.00	9.8
Verifiche nella direzione secondaria											
0	(8+9)-V-2	-1190	127	-17490	-0.70	4.28	-17.70	132.00	192.00	192.00	8.7
0	(8+9)-I-2	-1289	111	-11810	-0.76	3.76	-11.95	132.00	192.00	192.00	12
0	(8+9)-VI-4	4970	292	5071	2.93	9.87	5.13	132.00	192.00	192.00	10.0
0	(8+9)-I-3	-5262	-99	10139	-3.11	-3.36	10.26	132.00	192.00	192.00	14
0	(8+9)-VI-2	4757	311	-5072	2.81	10.52	-5.13	132.00	192.00	192.00	9.7
0	(8+9)-I-4	-378	78	10640	-0.22	2.64	10.77	132.00	192.00	192.00	14
0	(8+9)-V-4	-478	63	16320	-0.28	2.12	16.52	132.00	192.00	192.00	10
0	(8+9)-II-1	-11551	-285	-5038	-6.82	-9.63	-5.10	132.00	192.00	192.00	13
0	(8+9)-I-1	-6173	-66	-12311	-3.64	-2.24	-12.46	132.00	192.00	192.00	13
0	(8+9)-VI-1	-11521	-280	-6742	-6.80	-9.47	-6.82	132.00	192.00	192.00	12
0	(8+9)-V-3	-5362	-115	15819	-3.17	-3.88	16.01	132.00	192.00	192.00	9.6
0	(8+9)-VI-3	-11308	-300	3401	-6.68	-10.12	3.44	132.00	192.00	192.00	14
0	(8+9)-II-2	4727	307	-3368	2.79	10.36	-3.41	132.00	192.00	192.00	11
0	(8+9)-II-3	-11278	-295	1697	-6.66	-9.97	1.72	132.00	192.00	192.00	16
0	(8+9)-II-4	5000	297	3367	2.95	10.03	3.41	132.00	192.00	192.00	11
250	1	-4670	7	-1406	-2.76	0.24	-1.42	79.20	115.20	115.20	67
250	2	-9366	14	-3048	-5.53	0.47	-3.08	118.80	172.80	172.80	46
250	3	-9366	14	-3048	-5.53	0.47	-3.08	118.80	172.80	172.80	46
250	4	-4670	7	-1406	-2.76	0.24	-1.42	105.60	153.60	153.60	90
250	5	-4670	7	-1406	-2.76	0.24	-1.42	105.60	153.60	153.60	90
250	6	-4670	7	-1406	-2.76	0.24	-1.42	105.60	153.60	153.60	90
250	7	-4670	7	-1406	-2.76	0.24	-1.42	105.60	153.60	153.60	90
250	(8+9)-VIII-4	-2315	107	17970	-1.37	3.62	18.19	132.00	192.00	192.00	8.8
250	(8+9)-III-2	-3454	57	-9246	-2.04	1.94	-9.36	132.00	192.00	192.00	17
250	(8+9)-VII-1	-3849	-3	-23466	-2.27	-0.10	-23.75	132.00	192.00	192.00	8.0
250	(8+9)-V-1	-6044	14	-19443	-3.57	0.49	-19.68	132.00	192.00	192.00	9.5
250	(8+9)-VII-2	-3355	63	-15436	-1.98	2.12	-15.62	132.00	192.00	192.00	11
250	(8+9)-IV-4	-2285	109	16113	-1.35	3.68	16.31	132.00	192.00	192.00	9.6
250	(8+9)-VII-3	-3137	-53	13518	-1.85	-1.78	13.68	132.00	192.00	192.00	12
250	(8+9)-IV-2	-2558	121	8732	-1.51	4.07	8.84	132.00	192.00	192.00	15
250	(8+9)-VII-4	-2642	13	21547	-1.56	0.44	21.80	132.00	192.00	192.00	8.6
250	(8+9)-III-1	-3949	-8	-17276	-2.33	-0.28	-17.48	132.00	192.00	192.00	11
250	(8+9)-IV-3	-3933	-111	-10651	-2.32	-3.73	-10.78	132.00	192.00	192.00	13
250	(8+9)-IV-1	-4206	-99	-18032	-2.48	-3.34	-18.25	132.00	192.00	192.00	8.9
250	(8+9)-III-3	-3037	-47	7328	-1.79	-1.60	7.42	132.00	192.00	192.00	21

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
250	(8+9)-VIII-1	-4176	-97	-19889	-2.47	-3.28	-20.13	132.00	192.00	192.00	8.2
250	(8+9)-VIII-2	-2529	122	6875	-1.49	4.13	6.96	132.00	192.00	192.00	17
250	(8+9)-VIII-3	-3963	-112	-8794	-2.34	-3.79	-8.90	132.00	192.00	192.00	15
250	(8+9)-III-4	-2543	18	15357	-1.50	0.62	15.54	132.00	192.00	192.00	12

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
0	1	-3	0.01	3.84	Si	>100
0	2	-6	0.01	5.76	Si	>100
0	3	-6	0.01	5.76	Si	>100
0	4	-3	0.01	5.12	Si	>100
0	5	-3	0.01	5.12	Si	>100
0	6	-3	0.01	5.12	Si	>100
0	7	-3	0.01	5.12	Si	>100
0	(8+9)-V-1	-6	0.01	6.40	Si	>100
0	(8+9)-I-1	-3	0.01	6.40	Si	>100
0	(8+9)-VII-1	-9	0.02	6.40	Si	>100
0	(8+9)-I-2	-7	0.01	6.40	Si	>100
0	(8+9)-III-2	-4	0.01	6.40	Si	>100
0	(8+9)-I-4	-1	0.00	6.40	Si	>100
0	(8+9)-VI-4	-8	0.02	6.40	Si	>100
0	(8+9)-II-2	-10	0.02	6.40	Si	>100
0	(8+9)-VI-3	7	0.01	6.40	Si	>100
0	(8+9)-II-1	5	0.01	6.40	Si	>100
0	(8+9)-VII-2	-7	0.01	6.40	Si	>100
0	(8+9)-VII-3	3	0.01	6.40	Si	>100
0	(8+9)-VI-2	-11	0.02	6.40	Si	>100
0	(8+9)-II-4	-8	0.02	6.40	Si	>100
0	(8+9)-V-2	-10	0.02	6.40	Si	>100
3500	(8+9)-VI-1	-4	0.01	6.40	Si	>100
3500	(8+9)-VII-4	-6	0.01	6.40	Si	>100
3500	(8+9)-IV-4	-5	0.01	6.40	Si	>100
3500	(8+9)-VIII-1	8	0.02	6.40	Si	>100
3500	(8+9)-V-3	-6	0.01	6.40	Si	>100
3500	(8+9)-VIII-2	-2	0.00	6.40	Si	>100
3500	(8+9)-IV-2	-3	0.01	6.40	Si	>100
3500	(8+9)-VIII-3	5	0.01	6.40	Si	>100
3500	(8+9)-III-4	-3	0.01	6.40	Si	>100
3500	(8+9)-VIII-4	-5	0.01	6.40	Si	>100
3500	(8+9)-III-1	6	0.01	6.40	Si	>100
3500	(8+9)-I-3	-4	0.01	6.40	Si	>100
3500	(8+9)-IV-3	5	0.01	6.40	Si	>100
3500	(8+9)-V-4	-2	0.00	6.40	Si	>100
3500	(8+9)-IV-1	7	0.01	6.40	Si	>100
3500	(8+9)-III-3	-0	0.00	6.40	Si	>100
3500	(8+9)-II-3	-6	0.01	6.40	Si	>100
Verifiche nella direzione secondaria						
0	(8+9)-I-1	171	0.09	6.40	Si	69
0	(8+9)-VIII-2	-8	0.00	6.40	Si	>100
0	(8+9)-V-4	-172	0.09	6.40	Si	68
0	(8+9)-V-1	166	0.09	6.40	Si	71
0	(8+9)-IV-2	-7	0.00	6.40	Si	>100
0	(8+9)-I-4	-177	0.10	6.40	Si	66
250	1	-5	0.00	3.84	Si	>100
250	2	-9	0.01	5.76	Si	>100
250	3	-9	0.01	5.76	Si	>100
250	4	-5	0.00	5.12	Si	>100
250	5	-5	0.00	5.12	Si	>100
250	6	-5	0.00	5.12	Si	>100
250	7	-5	0.00	5.12	Si	>100
250	(8+9)-I-3	180	0.10	6.40	Si	65
250	(8+9)-II-3	591	0.32	6.40	Si	20

X	Comb.	Ty	τ_d	fvd	RS	Cs
250	(8+9)-VI-3	593	0.32	6.40	Si	20
250	(8+9)-VI-4	-592	0.32	6.40	Si	20
250	(8+9)-VI-1	585	0.32	6.40	Si	20
250	(8+9)-II-1	587	0.32	6.40	Si	20
250	(8+9)-III-3	2	0.00	6.40	Si	>100
250	(8+9)-V-2	-193	0.11	6.40	Si	61
250	(8+9)-VII-3	9	0.00	6.40	Si	>100
250	(8+9)-V-3	187	0.10	6.40	Si	63
250	(8+9)-I-2	-187	0.10	6.40	Si	63
250	(8+9)-II-2	-597	0.33	6.40	Si	20
250	(8+9)-III-2	-9	0.00	6.40	Si	>100
250	(8+9)-II-4	-594	0.32	6.40	Si	20
250	(8+9)-VII-2	-15	0.01	6.40	Si	>100
250	(8+9)-VI-2	-599	0.33	6.40	Si	20
500	(8+9)-VIII-4	8	0.00	6.40	Si	>100
500	(8+9)-III-1	-12	0.01	6.40	Si	>100
500	(8+9)-VII-4	12	0.01	6.40	Si	>100
500	(8+9)-IV-3	-8	0.00	6.40	Si	>100
500	(8+9)-IV-1	-12	0.01	6.40	Si	>100
500	(8+9)-VII-1	-18	0.01	6.40	Si	>100
500	(8+9)-VIII-1	-14	0.01	6.40	Si	>100
500	(8+9)-III-4	6	0.00	6.40	Si	>100
500	(8+9)-VIII-3	-6	0.00	6.40	Si	>100
500	(8+9)-IV-4	7	0.00	6.40	Si	>100

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	1	1386	5.73	19.20	3.4	1.39	12.00	8.7	V	3.4
0	2	2837	11.72	28.80	2.5	2.84	18.00	6.3	V	2.5
0	3	2837	11.72	28.80	2.5	2.84	18.00	6.3	V	2.5
0	4	1386	5.73	25.60	4.5	1.39	16.00	12	V	4.5
0	5	1386	5.73	25.60	4.5	1.39	16.00	12	V	4.5
0	6	1386	5.73	25.60	4.5	1.39	16.00	12	V	4.5
0	7	1386	5.73	25.60	4.5	1.39	16.00	12	V	4.5
0	(8+9)-V-1	5370	22.19	32.00	1.4	5.37	20.00	3.7	V	1.4
0	(8+9)-VI-1	4725	19.52	32.00	1.6	4.72	20.00	4.2	V	1.6
0	(8+9)-I-2	2615	10.81	32.00	3.0	2.62	20.00	7.6	V	3.0
0	(8+9)-V-4	-3453	-14.27	32.00	2.2	-3.45	20.00	5.8	V	2.2
0	(8+9)-VII-1	5391	22.28	32.00	1.4	5.39	20.00	3.7	V	1.4
0	(8+9)-I-4	-2309	-9.54	32.00	3.4	-2.31	20.00	8.7	V	3.4
0	(8+9)-IV-1	4451	18.39	32.00	1.7	4.45	20.00	4.5	V	1.7
0	(8+9)-VIII-3	2630	10.87	32.00	2.9	2.63	20.00	7.6	V	2.9
0	(8+9)-VI-4	-2808	-11.60	32.00	2.8	-2.81	20.00	7.1	V	2.8
0	(8+9)-II-4	-2464	-10.18	32.00	3.1	-2.46	20.00	8.1	V	3.1
0	(8+9)-IV-3	2973	12.29	32.00	2.6	2.97	20.00	6.7	V	2.6
0	(8+9)-II-1	4382	18.11	32.00	1.8	4.38	20.00	4.6	V	1.8
0	(8+9)-VIII-1	4794	19.81	32.00	1.6	4.79	20.00	4.2	V	1.6
0	(8+9)-III-1	4247	17.55	32.00	1.8	4.25	20.00	4.7	V	1.8
0	(8+9)-VII-2	3739	15.45	32.00	2.1	3.74	20.00	5.3	V	2.1
0	(8+9)-III-2	2595	10.72	32.00	3.0	2.59	20.00	7.7	V	3.0
0	(8+9)-I-1	4226	17.46	32.00	1.8	4.23	20.00	4.7	V	1.8
0	(8+9)-V-2	3760	15.54	32.00	2.1	3.76	20.00	5.3	V	2.1
3500	(8+9)-VI-2	2912	12.03	32.00	2.7	2.91	20.00	6.9	V	2.7
3500	(8+9)-VIII-2	-1810	-7.48	32.00	4.3	-1.81	20.00	11	V	4.3
3500	(8+9)-V-3	-4290	-17.73	32.00	1.8	-4.29	20.00	4.7	V	1.8
3500	(8+9)-II-2	2587	10.69	32.00	3.0	2.59	20.00	7.7	V	3.0
3500	(8+9)-IV-4	-3336	-13.79	32.00	2.3	-3.34	20.00	6.0	V	2.3
3500	(8+9)-VIII-4	-3661	-15.13	32.00	2.1	-3.66	20.00	5.5	V	2.1
3500	(8+9)-IV-2	-2135	-8.82	32.00	3.6	-2.13	20.00	9.4	V	3.6
3500	(8+9)-III-3	-1791	-7.40	32.00	4.3	-1.79	20.00	11	V	4.3
3500	(8+9)-VII-3	-2873	-11.87	32.00	2.7	-2.87	20.00	7.0	V	2.7
3500	(8+9)-VII-4	-4233	-17.49	32.00	1.8	-4.23	20.00	4.7	V	1.8

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
3500	(8+9)-II-3	-3524	-14.56	32.00	2.2	-3.52	20.00	5.7	V	2.2
3500	(8+9)-I-3	-3208	-13.25	32.00	2.4	-3.21	20.00	6.2	V	2.4
3500	(8+9)-VI-3	-3849	-15.91	32.00	2.0	-3.85	20.00	5.2	V	2.0
3500	(8+9)-III-4	-3151	-13.02	32.00	2.5	-3.15	20.00	6.3	V	2.5
Verifiche nella direzione secondaria										
0	(8+9)-II-1	-1216	-0.72	32.00	45	-0.17	20.00	>100	V	45
0	(8+9)-VIII-3	3556	2.10	32.00	15	0.51	20.00	39	V	15
0	(8+9)-VIII-2	-2637	-1.56	32.00	21	-0.38	20.00	53	V	21
0	(8+9)-VI-4	1533	0.90	32.00	35	0.22	20.00	91	V	35
0	(8+9)-II-4	2135	1.26	32.00	25	0.31	20.00	66	V	25
0	(8+9)-II-3	-3816	-2.25	32.00	14	-0.55	20.00	37	V	14
0	(8+9)-II-2	4735	2.79	32.00	11	0.68	20.00	30	V	11
250	1	669	0.40	19.20	49	0.10	12.00	>100	V	49
250	2	1416	0.84	28.80	34	0.20	18.00	89	V	34
250	3	1416	0.84	28.80	34	0.20	18.00	89	V	34
250	4	669	0.40	25.60	65	0.10	16.00	>100	V	65
250	5	669	0.40	25.60	65	0.10	16.00	>100	V	65
250	6	669	0.40	25.60	65	0.10	16.00	>100	V	65
250	7	669	0.40	25.60	65	0.10	16.00	>100	V	65
250	(8+9)-VIII-4	-6548	-3.87	32.00	8.3	-0.94	20.00	21	V	8.3
250	(8+9)-V-1	6095	3.60	32.00	8.9	0.87	20.00	23	V	8.9
250	(8+9)-I-2	5703	3.37	32.00	9.5	0.81	20.00	25	V	9.5
250	(8+9)-III-2	3299	1.95	32.00	16	0.47	20.00	42	V	16
250	(8+9)-VI-2	5383	3.18	32.00	10	0.77	20.00	26	V	10
250	(8+9)-III-4	-5409	-3.19	32.00	10	-0.77	20.00	26	V	10
250	(8+9)-VI-3	-4464	-2.64	32.00	12	-0.64	20.00	31	V	12
250	(8+9)-IV-2	-3284	-1.94	32.00	17	-0.47	20.00	43	V	17
250	(8+9)-I-1	3924	2.32	32.00	14	0.56	20.00	36	V	14
250	(8+9)-IV-4	-5896	-3.48	32.00	9.2	-0.84	20.00	24	V	9.2
250	(8+9)-VII-1	8499	5.02	32.00	6.4	1.21	20.00	16	V	6.4
250	(8+9)-V-2	7874	4.65	32.00	6.9	1.12	20.00	18	V	6.9
250	(8+9)-VII-2	5470	3.23	32.00	9.9	0.78	20.00	26	V	9.9
250	(8+9)-V-4	-5176	-3.06	32.00	10	-0.74	20.00	27	V	10
250	(8+9)-VII-3	-4551	-2.69	32.00	12	-0.65	20.00	31	V	12
250	(8+9)-IV-1	6815	4.02	32.00	8.0	0.97	20.00	21	V	8.0
250	(8+9)-VII-4	-7581	-4.47	32.00	7.2	-1.08	20.00	18	V	7.2
250	(8+9)-III-1	6328	3.74	32.00	8.6	0.90	20.00	22	V	8.6
250	(8+9)-III-3	-2380	-1.40	32.00	23	-0.34	20.00	59	V	23
250	(8+9)-IV-3	4203	2.48	32.00	13	0.60	20.00	33	V	13
250	(8+9)-V-3	-6956	-4.11	32.00	7.8	-0.99	20.00	20	V	7.8
250	(8+9)-VIII-1	7466	4.41	32.00	7.3	1.07	20.00	19	V	7.3
250	(8+9)-I-4	-3005	-1.77	32.00	18	-0.43	20.00	47	V	18
250	(8+9)-I-3	-4785	-2.82	32.00	11	-0.68	20.00	29	V	11
500	(8+9)-VI-1	-914	-0.54	32.00	59	-0.13	20.00	>100	V	59

Setto 27: origine (708.5,2464.3,328.5), direzione (0.825704,0.564103,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	
0	(8+9)-III-1	2837	-1	1486	3.34	-0.06	8.97	132.00	192.00	192.00	14
0	(8+9)-V-1	2228	-4	1271	2.62	-0.16	7.67	132.00	192.00	192.00	16
0	(8+9)-VII-2	2375	-8	1298	2.80	-0.35	7.84	132.00	192.00	192.00	16
0	(8+9)-VII-1	4323	-3	2069	5.09	-0.15	12.49	132.00	192.00	192.00	9.6
0	(8+9)-V-2	4471	-8	2097	5.26	-0.34	12.66	132.00	192.00	192.00	9.3
0	(8+9)-VIII-1	3505	6	1734	4.13	0.26	10.47	132.00	192.00	192.00	11
0	(8+9)-IV-3	1302	9	850	1.53	0.38	5.13	132.00	192.00	192.00	25
0	(8+9)-IV-1	3059	6	1559	3.60	0.29	9.41	132.00	192.00	192.00	13
0	(8+9)-I-2	2984	-6	1513	3.51	-0.25	9.14	132.00	192.00	192.00	13
1750	1	2975	6	723	3.50	0.25	4.37	79.20	115.20	115.20	12
1750	2	6117	12	1491	7.20	0.53	9.00	118.80	172.80	172.80	8.6
1750	3	6117	12	1491	7.20	0.53	9.00	118.80	172.80	172.80	8.6
1750	4	2975	6	723	3.50	0.25	4.37	105.60	153.60	153.60	16
1750	5	2975	6	723	3.50	0.25	4.37	105.60	153.60	153.60	16

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
1750	6	2975	6	723	3.50	0.25	4.37	105.60	153.60	153.60	16
1750	7	2975	6	723	3.50	0.25	4.37	105.60	153.60	153.60	16
1750	(8+9)-VIII-3	1902	11	474	2.24	0.47	2.86	132.00	192.00	192.00	29
3500	(8+9)-VIII-4	4533	-8	2053	5.34	-0.35	12.39	132.00	192.00	192.00	9.4
3500	(8+9)-I-4	1950	-25	775	2.30	-1.12	4.68	132.00	192.00	192.00	21
3500	(8+9)-VI-2	-4462	-114	-2347	-5.25	-5.02	-14.17	132.00	192.00	192.00	9.9
3500	(8+9)-III-4	3790	4	1735	4.46	0.18	10.48	132.00	192.00	192.00	11
3500	(8+9)-VI-3	3499	111	2244	4.12	4.89	13.55	132.00	192.00	192.00	7.9
3500	(8+9)-IV-2	2142	-14	1052	2.52	-0.64	6.35	132.00	192.00	192.00	18
3500	(8+9)-VI-4	-1598	-106	-1147	-1.88	-4.67	-6.93	132.00	192.00	192.00	17
3500	(8+9)-IV-4	4060	-9	1853	4.78	-0.41	11.19	132.00	192.00	192.00	10
3500	(8+9)-II-4	-2071	-107	-1347	-2.44	-4.73	-8.13	132.00	192.00	192.00	15
3500	(8+9)-I-3	3480	40	1793	4.10	1.75	10.82	132.00	192.00	192.00	10
3500	(8+9)-II-3	3026	109	2045	3.56	4.83	12.35	132.00	192.00	192.00	8.6
3500	(8+9)-V-4	3527	-21	1440	4.15	-0.91	8.69	132.00	192.00	192.00	12
3500	(8+9)-VII-3	3217	15	1497	3.79	0.66	9.04	132.00	192.00	192.00	13
3500	(8+9)-I-1	-2913	22	-878	-3.43	0.98	-5.30	132.00	192.00	192.00	30
3500	(8+9)-VII-4	5366	9	2400	6.32	0.38	14.49	132.00	192.00	192.00	8.0
3500	(8+9)-VI-1	635	103	1044	0.75	4.54	6.31	132.00	192.00	192.00	16
3500	(8+9)-III-3	1640	10	833	1.93	0.45	5.03	132.00	192.00	192.00	23
3500	(8+9)-V-3	5057	44	2457	5.95	1.95	14.83	132.00	192.00	192.00	7.5
3500	(8+9)-II-2	-3989	-112	-2148	-4.70	-4.96	-12.97	132.00	192.00	192.00	11
3500	(8+9)-VIII-2	1669	-16	853	1.96	-0.70	5.15	132.00	192.00	192.00	22
3500	(8+9)-II-1	1109	104	1244	1.31	4.60	7.51	132.00	192.00	192.00	14
3500	(8+9)-III-2	-2603	-13	-935	-3.06	-0.59	-5.65	132.00	192.00	192.00	31
Verifiche nella direzione secondaria											
0	1	-7387	-2	951	-4.36	-0.06	0.96	79.20	115.20	115.20	97
0	2	-15167	-4	1969	-8.95	-0.13	1.99	118.80	172.80	172.80	67
0	3	-15167	-4	1969	-8.95	-0.13	1.99	118.80	172.80	172.80	67
0	4	-7387	-2	951	-4.36	-0.06	0.96	105.60	153.60	153.60	>100
0	5	-7387	-2	951	-4.36	-0.06	0.96	105.60	153.60	153.60	>100
0	6	-7387	-2	951	-4.36	-0.06	0.96	105.60	153.60	153.60	>100
0	7	-7387	-2	951	-4.36	-0.06	0.96	105.60	153.60	153.60	>100
0	(8+9)-VIII-4	-4872	-11	-8627	-2.88	-0.37	-8.73	132.00	192.00	192.00	21
0	(8+9)-IV-2	-4874	-16	-4398	-2.88	-0.55	-4.45	132.00	192.00	192.00	38
0	(8+9)-V-1	-6038	-5	8924	-3.56	-0.19	9.03	132.00	192.00	192.00	21
0	(8+9)-I-2	-4185	-15	6486	-2.47	-0.50	6.56	132.00	192.00	192.00	27
0	(8+9)-V-2	-4065	-20	9059	-2.40	-0.69	9.17	132.00	192.00	192.00	19
0	(8+9)-I-4	-4057	-3	-5039	-2.40	-0.09	-5.10	132.00	192.00	192.00	37
0	(8+9)-V-3	-6152	18	-7746	-3.63	0.60	-7.84	132.00	192.00	192.00	23
0	(8+9)-VII-3	-5241	14	-5643	-3.09	0.48	-5.71	132.00	192.00	192.00	31
0	(8+9)-II-1	-8417	22	2160	-4.97	0.73	2.19	132.00	192.00	192.00	63
0	(8+9)-V-4	-4178	3	-7611	-2.47	0.10	-7.70	132.00	192.00	192.00	25
0	(8+9)-VIII-3	-5379	15	4939	-3.18	0.52	5.00	132.00	192.00	192.00	34
0	(8+9)-III-2	-5096	-11	4384	-3.01	-0.38	4.44	132.00	192.00	192.00	39
0	(8+9)-III-4	-4968	1	-7141	-2.93	0.03	-7.23	132.00	192.00	192.00	26
0	(8+9)-VI-1	-8381	20	2932	-4.95	0.67	2.97	132.00	192.00	192.00	51
0	(8+9)-I-1	-6159	0	6351	-3.64	0.00	6.43	132.00	192.00	192.00	30
0	(8+9)-VIII-2	-4838	-18	-3626	-2.86	-0.60	-3.67	132.00	192.00	192.00	45
0	(8+9)-IV-4	-4836	-12	-7855	-2.85	-0.42	-7.95	132.00	192.00	192.00	23
0	(8+9)-VIII-1	-5345	8	9940	-3.16	0.28	10.06	132.00	192.00	192.00	18
0	(8+9)-III-1	-5248	-3	8454	-3.10	-0.12	8.55	132.00	192.00	192.00	22
0	(8+9)-IV-1	-5381	10	9168	-3.18	0.34	9.28	132.00	192.00	192.00	20
0	(8+9)-IV-3	-5342	14	5711	-3.15	0.46	5.78	132.00	192.00	192.00	31
0	(8+9)-I-3	-6031	12	-5174	-3.56	0.42	-5.24	132.00	192.00	192.00	34
0	(8+9)-III-3	-5120	9	-3071	-3.02	0.30	-3.11	132.00	192.00	192.00	56
0	(8+9)-VII-4	-5089	6	-9713	-3.00	0.22	-9.83	132.00	192.00	192.00	19
0	(8+9)-VII-1	-5128	-9	11026	-3.03	-0.30	11.16	132.00	192.00	192.00	17
0	(8+9)-VII-2	-4976	-17	6956	-2.94	-0.57	7.04	132.00	192.00	192.00	25
585	(8+9)-II-2	-4032	-46	3536	-2.38	-1.56	3.58	132.00	192.00	192.00	37
585	(8+9)-VI-4	-3863	-42	1504	-2.28	-1.42	1.52	132.00	192.00	192.00	65
585	(8+9)-VI-3	-4689	37	-2827	-2.77	1.24	-2.86	132.00	192.00	192.00	46
585	(8+9)-VI-2	-4047	-48	3899	-2.39	-1.61	3.95	132.00	192.00	192.00	34
585	(8+9)-II-3	-4704	35	-2464	-2.78	1.19	-2.49	132.00	192.00	192.00	52

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
585	(8+9)-II-4	-3878	-44	1867	-2.29	-1.48	1.89	132.00	192.00	192.00	57

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Ty kg	τ_d kg/cmq	fvd kg/cmq	RS	Cs
0	1	8	0.01	3.84	Si	>100
0	2	17	0.01	5.76	Si	>100
0	3	17	0.01	5.76	Si	>100
0	4	8	0.01	5.12	Si	>100
0	5	8	0.01	5.12	Si	>100
0	6	8	0.01	5.12	Si	>100
0	7	8	0.01	5.12	Si	>100
0	(8+9)-IV-1	7	0.01	6.40	Si	>100
0	(8+9)-IV-2	5	0.00	6.40	Si	>100
0	(8+9)-VII-1	9	0.01	6.40	Si	>100
0	(8+9)-VIII-2	5	0.00	6.40	Si	>100
0	(8+9)-VIII-1	8	0.01	6.40	Si	>100
0	(8+9)-VII-2	8	0.01	6.40	Si	>100
0	(8+9)-VIII-3	6	0.01	6.40	Si	>100
0	(8+9)-IV-3	7	0.01	6.40	Si	>100
0	(8+9)-III-1	8	0.01	6.40	Si	>100
0	(8+9)-III-2	7	0.01	6.40	Si	>100
3500	(8+9)-VIII-4	-7	0.01	6.40	Si	>100
3500	(8+9)-V-1	-160	0.14	6.40	Si	47
3500	(8+9)-I-2	158	0.14	6.40	Si	47
3500	(8+9)-VI-3	-539	0.46	6.40	Si	14
3500	(8+9)-I-1	-162	0.14	6.40	Si	46
3500	(8+9)-VI-4	528	0.45	6.40	Si	14
3500	(8+9)-III-3	-6	0.01	6.40	Si	>100
3500	(8+9)-II-3	-539	0.46	6.40	Si	14
3500	(8+9)-II-4	529	0.45	6.40	Si	14
3500	(8+9)-II-2	530	0.45	6.40	Si	14
3500	(8+9)-V-3	-169	0.14	6.40	Si	44
3500	(8+9)-VII-3	-8	0.01	6.40	Si	>100
3500	(8+9)-VI-1	-537	0.46	6.40	Si	14
3500	(8+9)-VII-4	-9	0.01	6.40	Si	>100
3500	(8+9)-V-2	160	0.14	6.40	Si	47
3500	(8+9)-V-4	152	0.13	6.40	Si	49
3500	(8+9)-VI-2	531	0.45	6.40	Si	14
3500	(8+9)-IV-4	-6	0.01	6.40	Si	>100
3500	(8+9)-II-1	-537	0.46	6.40	Si	14
3500	(8+9)-I-4	154	0.13	6.40	Si	49
3500	(8+9)-I-3	-167	0.14	6.40	Si	45
3500	(8+9)-III-4	-7	0.01	6.40	Si	>100
Verifiche nella direzione secondaria						
0	(8+9)-VIII-4	-30	0.02	6.40	Si	>100
0	(8+9)-IV-4	-32	0.02	6.40	Si	>100
0	(8+9)-IV-2	-35	0.02	6.40	Si	>100
0	(8+9)-V-2	-24	0.01	6.40	Si	>100
0	(8+9)-VII-2	-28	0.02	6.40	Si	>100
0	(8+9)-II-4	-19	0.01	6.40	Si	>100
0	(8+9)-VII-1	-12	0.01	6.40	Si	>100
0	(8+9)-III-2	-21	0.01	6.40	Si	>100
0	(8+9)-I-2	-17	0.01	6.40	Si	>100
0	(8+9)-VIII-2	-37	0.02	6.40	Si	>100
0	(8+9)-VI-2	-25	0.01	6.40	Si	>100
0	(8+9)-VI-4	-17	0.01	6.40	Si	>100
0	(8+9)-II-2	-23	0.01	6.40	Si	>100
0	(8+9)-V-1	-15	0.01	6.40	Si	>100
585	(8+9)-VI-1	-14	0.01	6.40	Si	>100
585	(8+9)-III-1	-10	0.01	6.40	Si	>100
585	(8+9)-I-1	-8	0.00	6.40	Si	>100
585	(8+9)-II-1	-14	0.01	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
1170	1	-13	0.01	3.84	Si	>100
1170	2	-28	0.02	5.76	Si	>100
1170	3	-28	0.02	5.76	Si	>100
1170	4	-13	0.01	5.12	Si	>100
1170	5	-13	0.01	5.12	Si	>100
1170	6	-13	0.01	5.12	Si	>100
1170	7	-13	0.01	5.12	Si	>100
1170	(8+9)-VI-3	-16	0.01	6.40	Si	>100
1170	(8+9)-IV-1	-21	0.01	6.40	Si	>100
1170	(8+9)-IV-3	-25	0.01	6.40	Si	>100
1170	(8+9)-V-4	-17	0.01	6.40	Si	>100
1170	(8+9)-VII-3	-22	0.01	6.40	Si	>100
1170	(8+9)-V-3	-19	0.01	6.40	Si	>100
1170	(8+9)-VII-4	-14	0.01	6.40	Si	>100
1170	(8+9)-I-3	-16	0.01	6.40	Si	>100
1170	(8+9)-I-4	-14	0.01	6.40	Si	>100
1170	(8+9)-III-3	-19	0.01	6.40	Si	>100
1170	(8+9)-VIII-1	-21	0.01	6.40	Si	>100
1170	(8+9)-III-4	-11	0.01	6.40	Si	>100
1170	(8+9)-VIII-3	-26	0.01	6.40	Si	>100
1170	(8+9)-II-3	-15	0.01	6.40	Si	>100

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	1	-4446	-7.85	19.20	2.4	-1.90	12.00	6.3	V	2.4
0	2	-9161	-16.18	28.80	1.8	-3.92	18.00	4.6	V	1.8
0	3	-9161	-16.18	28.80	1.8	-3.92	18.00	4.6	V	1.8
0	4	-4446	-7.85	25.60	3.3	-1.90	16.00	8.4	V	3.3
0	5	-4446	-7.85	25.60	3.3	-1.90	16.00	8.4	V	3.3
0	6	-4446	-7.85	25.60	3.3	-1.90	16.00	8.4	V	3.3
0	7	-4446	-7.85	25.60	3.3	-1.90	16.00	8.4	V	3.3
0	(8+9)-VIII-4	-5645	-9.97	32.00	3.2	-2.41	20.00	8.3	V	3.2
0	(8+9)-V-3	-6121	-10.81	32.00	3.0	-2.62	20.00	7.6	V	3.0
0	(8+9)-III-3	-4181	-7.38	32.00	4.3	-1.79	20.00	11	V	4.3
0	(8+9)-III-4	-5281	-9.33	32.00	3.4	-2.26	20.00	8.9	V	3.4
0	(8+9)-I-4	-4149	-7.33	32.00	4.4	-1.77	20.00	11	V	4.4
0	(8+9)-VI-3	-5754	-10.16	32.00	3.1	-2.46	20.00	8.1	V	3.1
0	(8+9)-VIII-2	-4165	-7.35	32.00	4.4	-1.78	20.00	11	V	4.4
0	(8+9)-IV-2	-4407	-7.78	32.00	4.1	-1.88	20.00	11	V	4.1
0	(8+9)-VII-4	-6088	-10.75	32.00	3.0	-2.60	20.00	7.7	V	3.0
0	(8+9)-VI-1	-4275	-7.55	32.00	4.2	-1.83	20.00	11	V	4.2
0	(8+9)-VI-4	-1870	-3.30	32.00	9.7	-0.80	20.00	25	V	9.7
0	(8+9)-II-1	-4517	-7.98	32.00	4.0	-1.93	20.00	10	V	4.0
0	(8+9)-II-3	-5512	-9.73	32.00	3.3	-2.36	20.00	8.5	V	3.3
0	(8+9)-VII-3	-4989	-8.81	32.00	3.6	-2.13	20.00	9.4	V	3.6
0	(8+9)-I-3	-5314	-9.38	32.00	3.4	-2.27	20.00	8.8	V	3.4
0	(8+9)-IV-4	-5402	-9.54	32.00	3.4	-2.31	20.00	8.7	V	3.4
0	(8+9)-V-4	-4956	-8.75	32.00	3.7	-2.12	20.00	9.4	V	3.7
3500	(8+9)-V-1	4917	8.68	32.00	3.7	2.10	20.00	9.5	V	3.7
3500	(8+9)-IV-1	4651	8.21	32.00	3.9	1.99	20.00	10	V	3.9
3500	(8+9)-I-2	4164	7.35	32.00	4.4	1.78	20.00	11	V	4.4
3500	(8+9)-VII-2	4415	7.80	32.00	4.1	1.89	20.00	11	V	4.1
3500	(8+9)-V-2	4981	8.80	32.00	3.6	2.13	20.00	9.4	V	3.6
3500	(8+9)-III-1	4666	8.24	32.00	3.9	1.99	20.00	10	V	3.9
3500	(8+9)-VI-2	3223	5.69	32.00	5.6	1.38	20.00	15	V	5.6
3500	(8+9)-II-4	1897	3.35	32.00	9.6	0.81	20.00	25	V	9.6
3500	(8+9)-IV-3	3571	6.31	32.00	5.1	1.53	20.00	13	V	5.1
3500	(8+9)-I-1	4100	7.24	32.00	4.4	1.75	20.00	11	V	4.4
3500	(8+9)-VII-1	5483	9.68	32.00	3.3	2.34	20.00	8.5	V	3.3
3500	(8+9)-VIII-1	4896	8.65	32.00	3.7	2.09	20.00	9.6	V	3.7
3500	(8+9)-II-2	2978	5.26	32.00	6.1	1.27	20.00	16	V	6.1
3500	(8+9)-VIII-3	3326	5.87	32.00	5.4	1.42	20.00	14	V	5.4

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
3500	(8+9)-III-2	3598	6.35	32.00	5.0	1.54	20.00	13	V	5.0
Verifiche nella direzione secondaria										
585	1	-693	-0.41	19.20	47	-0.10	12.00	>100	V	47
585	2	-1348	-0.80	28.80	36	-0.19	18.00	93	V	36
585	3	-1348	-0.80	28.80	36	-0.19	18.00	93	V	36
585	4	-693	-0.41	25.60	63	-0.10	16.00	>100	V	63
585	5	-693	-0.41	25.60	63	-0.10	16.00	>100	V	63
585	6	-693	-0.41	25.60	63	-0.10	16.00	>100	V	63
585	7	-693	-0.41	25.60	63	-0.10	16.00	>100	V	63
585	(8+9)-VII-3	-7431	-4.39	32.00	7.3	-1.06	20.00	19	V	7.3
585	(8+9)-VI-1	-3463	-2.04	32.00	16	-0.49	20.00	40	V	16
585	(8+9)-III-3	-4645	-2.74	32.00	12	-0.66	20.00	30	V	12
585	(8+9)-I-4	-4467	-2.64	32.00	12	-0.64	20.00	31	V	12
1170	(8+9)-VIII-4	-9170	-5.41	32.00	5.9	-1.31	20.00	15	V	5.9
1170	(8+9)-IV-2	-4764	-2.81	32.00	11	-0.68	20.00	29	V	11
1170	(8+9)-V-3	-10856	-6.41	32.00	5.0	-1.55	20.00	13	V	5.0
1170	(8+9)-II-2	7260	4.29	32.00	7.5	1.04	20.00	19	V	7.5
1170	(8+9)-V-4	-7375	-4.35	32.00	7.4	-1.05	20.00	19	V	7.4
1170	(8+9)-II-4	3736	2.21	32.00	15	0.53	20.00	37	V	15
1170	(8+9)-I-2	7311	4.32	32.00	7.4	1.04	20.00	19	V	7.4
1170	(8+9)-III-2	3704	2.19	32.00	15	0.53	20.00	38	V	15
1170	(8+9)-VI-2	8142	4.81	32.00	6.7	1.16	20.00	17	V	6.7
1170	(8+9)-III-4	-8043	-4.75	32.00	6.7	-1.15	20.00	17	V	6.7
1170	(8+9)-VI-3	-8747	-5.16	32.00	6.2	-1.25	20.00	16	V	6.2
1170	(8+9)-I-3	-7917	-4.67	32.00	6.8	-1.13	20.00	18	V	6.8
1170	(8+9)-VI-4	2854	1.68	32.00	19	0.41	20.00	49	V	19
1170	(8+9)-IV-4	-8288	-4.89	32.00	6.5	-1.18	20.00	17	V	6.5
1170	(8+9)-VII-1	10377	6.13	32.00	5.2	1.48	20.00	13	V	5.2
1170	(8+9)-V-2	10250	6.05	32.00	5.3	1.46	20.00	14	V	5.3
1170	(8+9)-VII-2	6643	3.92	32.00	8.2	0.95	20.00	21	V	8.2
1170	(8+9)-III-1	7438	4.39	32.00	7.3	1.06	20.00	19	V	7.3
1170	(8+9)-I-1	3831	2.26	32.00	14	0.55	20.00	37	V	14
1170	(8+9)-IV-1	7682	4.54	32.00	7.1	1.10	20.00	18	V	7.1
1170	(8+9)-VII-4	-10982	-6.48	32.00	4.9	-1.57	20.00	13	V	4.9
1170	(8+9)-II-1	-4341	-2.56	32.00	12	-0.62	20.00	32	V	12
1170	(8+9)-IV-3	4158	2.45	32.00	13	0.59	20.00	34	V	13
1170	(8+9)-II-3	-7866	-4.64	32.00	6.9	-1.12	20.00	18	V	6.9
1170	(8+9)-VIII-1	8564	5.06	32.00	6.3	1.22	20.00	16	V	6.3
1170	(8+9)-VIII-2	-3882	-2.29	32.00	14	-0.55	20.00	36	V	14
1170	(8+9)-VIII-3	3277	1.93	32.00	17	0.47	20.00	43	V	17
1170	(8+9)-V-1	6770	4.00	32.00	8.0	0.97	20.00	21	V	8.0

Verifiche a instabilità

Setto(X)	Comb.	k _{critc}	k _{critm}	λ_{relc}	λ_{relm}	σ_n	σ_{mx}	σ_{my}	f _{td}	f _{cd}	f _{md}	Cs
(cm)						kg/cm q	kg/cm q	kg/cm q	kg/cm q	kg/cm q	kg/cm q	
21(200 .0)	(8+9)-VII-4	0.92	--	0.73	--	-1.06	0.07	7.39	132.00	192.00	192.00	22
22(250 .0)	(8+9)-V-3	0.84	--	0.91	--	-1.11	0.09	6.53	132.00	192.00	192.00	24
23(0.0)	(8+9)-V-2	0.97	--	0.53	--	-0.83	-0.34	6.40	132.00	192.00	192.00	25
24(0.0)	(8+9)-VII-4	--	--	--	--	11.65	0.15	-26.83	132.00	192.00	192.00	4.4
25(0.0)	(8+9)-V-4	0.55	--	1.27	--	-7.71	0.15	-15.46	132.00	192.00	192.00	6.5
26(350 .0)	(8+9)-VII-1	--	--	--	--	10.79	-0.41	-30.77	132.00	192.00	192.00	4.1
27(350 .0)	(8+9)-VI-2	0.55	--	1.27	--	-5.25	-5.02	-14.17	132.00	192.00	192.00	6.7

Parete Xlam 6 - Nodi: [15-16-6-7-17-18-108-107] - **Crit.Prog.** Criterio di verifica XLAM 0 - **Verificato:**

[Cs=1.269,Comb=(8+9)-VIII-3]

Geometria setti

Setto	Crit.	X mm	L cm	S cm	X90 mm	L90 cm	S90 cm
28	Criterio di verifica XLAM 0	0	387.0	12.1	0	50.0	12.1
		250	387.0	12.1	1935	50.0	12.1
		500	387.0	12.1	3870	50.0	12.1
29	Criterio di verifica XLAM 0	0	387.0	12.1	0	68.2	12.1
		341	387.0	12.1	1935	68.2	12.1
		682	387.0	12.1	3870	68.2	12.1
30	Criterio di verifica XLAM 0	0	117.0	12.1	0	120.0	12.1
		600	117.0	12.1	585	120.0	12.1
		1200	117.0	12.1	1170	120.0	12.1

Setto 28: origine (1118.0,2744.0,193.5), direzione (0.927376,-0.374131,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X mm	Comb.	N kg	Mx kg*m	My kg*m	σ_n kg/cmq	σ_{mx} kg/cmq	σ_{my} kg/cmq	ftd kg/cmq	fcd kg/cmq	fmd kg/cmq	Cs
0	1	-23	-14	239	-0.01	-0.19	0.13	79.20	115.20	115.20	>100
0	2	-67	-31	498	-0.02	-0.41	0.27	118.80	172.80	172.80	>100
0	3	-67	-31	498	-0.02	-0.41	0.27	118.80	172.80	172.80	>100
0	4	-23	-14	239	-0.01	-0.19	0.13	105.60	153.60	153.60	>100
0	5	-23	-14	239	-0.01	-0.19	0.13	105.60	153.60	153.60	>100
0	6	-23	-14	239	-0.01	-0.19	0.13	105.60	153.60	153.60	>100
0	7	-23	-14	239	-0.01	-0.19	0.13	105.60	153.60	153.60	>100
0	(8+9)-VIII-4	537	29	1514	0.19	0.39	0.84	132.00	192.00	192.00	>100
0	(8+9)-IV-1	-779	-56	-1265	-0.28	-0.75	-0.70	132.00	192.00	192.00	>100
0	(8+9)-VIII-1	-567	-48	-1184	-0.20	-0.65	-0.65	132.00	192.00	192.00	>100
0	(8+9)-IV-4	749	37	1594	0.27	0.49	0.88	132.00	192.00	192.00	>100
500	(8+9)-V-1	544	17	-2269	0.19	0.23	-1.25	132.00	192.00	192.00	>100
500	(8+9)-I-2	766	27	-3085	0.27	0.36	-1.70	132.00	192.00	192.00	78
500	(8+9)-V-3	-1022	-48	3965	-0.36	-0.64	2.19	132.00	192.00	192.00	68
500	(8+9)-II-2	1023	37	-3995	0.36	0.49	-2.20	132.00	192.00	192.00	59
500	(8+9)-V-4	-507	-27	2003	-0.18	-0.35	1.11	132.00	192.00	192.00	>100
500	(8+9)-II-4	729	24	-2813	0.26	0.32	-1.55	132.00	192.00	192.00	85
500	(8+9)-VI-1	-605	-30	2202	-0.22	-0.40	1.22	132.00	192.00	192.00	>100
500	(8+9)-III-2	712	26	-2833	0.25	0.34	-1.56	132.00	192.00	192.00	84
500	(8+9)-VI-2	1111	40	-4339	0.40	0.54	-2.39	132.00	192.00	192.00	55
500	(8+9)-III-4	-268	-17	1109	-0.10	-0.23	0.61	132.00	192.00	192.00	>100
500	(8+9)-VI-3	-1074	-50	4073	-0.38	-0.66	2.25	132.00	192.00	192.00	66
500	(8+9)-IV-2	843	32	-3153	0.30	0.42	-1.74	132.00	192.00	192.00	74
500	(8+9)-VI-4	642	21	-2469	0.23	0.28	-1.36	132.00	192.00	192.00	97
500	(8+9)-II-1	-692	-33	2546	-0.25	-0.45	1.41	132.00	192.00	192.00	>100
500	(8+9)-VII-1	598	19	-2522	0.21	0.25	-1.39	132.00	192.00	192.00	98
500	(8+9)-V-2	1059	38	-4232	0.38	0.51	-2.34	132.00	192.00	192.00	57
500	(8+9)-VII-2	1005	37	-3979	0.36	0.49	-2.20	132.00	192.00	192.00	60
500	(8+9)-III-1	305	8	-1375	0.11	0.10	-0.76	132.00	192.00	192.00	>100
500	(8+9)-VII-3	-968	-46	3713	-0.34	-0.62	2.05	132.00	192.00	192.00	72
500	(8+9)-I-1	251	6	-1123	0.09	0.08	-0.62	132.00	192.00	192.00	>100
500	(8+9)-VII-4	-561	-28	2255	-0.20	-0.38	1.24	132.00	192.00	192.00	>100
500	(8+9)-III-3	-675	-35	2566	-0.24	-0.47	1.42	132.00	192.00	192.00	>100
500	(8+9)-IV-3	-806	-41	2887	-0.29	-0.55	1.59	132.00	192.00	192.00	90
500	(8+9)-II-3	-986	-46	3729	-0.35	-0.62	2.06	132.00	192.00	192.00	72
500	(8+9)-I-3	-729	-37	2819	-0.26	-0.49	1.56	132.00	192.00	192.00	94
500	(8+9)-VIII-2	931	35	-3497	0.33	0.47	-1.93	132.00	192.00	192.00	67
500	(8+9)-VIII-3	-894	-44	3231	-0.32	-0.59	1.78	132.00	192.00	192.00	81
500	(8+9)-I-4	-214	-16	856	-0.08	-0.21	0.47	132.00	192.00	192.00	>100
Verifiche nella direzione secondaria											
0	1	-1371	-3	62	-5.66	-0.70	3.06	79.20	115.20	115.20	29
0	2	-2754	-7	115	-11.38	-1.73	5.71	118.80	172.80	172.80	21
0	3	-2754	-7	115	-11.38	-1.73	5.71	118.80	172.80	172.80	21
0	4	-1371	-3	62	-5.66	-0.70	3.06	105.60	153.60	153.60	39
0	5	-1371	-3	62	-5.66	-0.70	3.06	105.60	153.60	153.60	39

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	6	-1371	-3	62	-5.66	-0.70	3.06	105.60	153.60	153.60	39
0	7	-1371	-3	62	-5.66	-0.70	3.06	105.60	153.60	153.60	39
0	(8+9)-VIII-4	-1464	233	884	-6.05	55.14	43.83	132.00	192.00	192.00	1.9
0	(8+9)-IV-2	-4988	240	1366	-20.61	56.69	67.76	132.00	192.00	192.00	1.5
0	(8+9)-V-1	-6899	6	567	-28.51	1.50	28.11	132.00	192.00	192.00	5.7
0	(8+9)-I-2	-6750	12	1129	-27.89	2.74	55.96	132.00	192.00	192.00	3.1
0	(8+9)-V-2	-9221	21	1575	-38.10	4.87	78.08	132.00	192.00	192.00	2.1
0	(8+9)-I-4	2525	-1	-34	10.43	-0.30	-1.70	132.00	192.00	192.00	11
0	(8+9)-V-3	7317	-24	-1488	30.24	-5.79	-73.78	132.00	192.00	192.00	1.6
0	(8+9)-II-2	-6212	24	1897	-25.67	5.60	94.07	132.00	192.00	192.00	1.9
0	(8+9)-V-4	4996	-10	-480	20.64	-2.43	-23.81	132.00	192.00	192.00	3.4
0	(8+9)-II-4	-3430	20	1548	-14.17	4.69	76.77	132.00	192.00	192.00	2.3
0	(8+9)-VI-1	785	-21	-1328	3.24	-4.97	-65.84	132.00	192.00	192.00	2.5
0	(8+9)-III-2	-6383	76	969	-26.38	18.06	48.07	132.00	192.00	192.00	2.8
0	(8+9)-VI-2	-6954	26	2031	-28.73	6.24	100.70	132.00	192.00	192.00	1.7
0	(8+9)-III-4	2893	64	-193	11.95	15.03	-9.59	132.00	192.00	192.00	4.6
0	(8+9)-VI-3	5050	-30	-1944	20.87	-7.16	-96.41	132.00	192.00	192.00	1.4
0	(8+9)-VI-4	-2689	17	1414	-11.11	4.05	70.14	132.00	192.00	192.00	2.6
0	(8+9)-IV-4	-2205	236	1018	-9.11	55.78	50.46	132.00	192.00	192.00	1.8
0	(8+9)-VII-1	-7267	-58	726	-30.03	-13.82	36.01	132.00	192.00	192.00	3.5
0	(8+9)-II-1	1526	-24	-1462	6.31	-5.61	-72.47	132.00	192.00	192.00	2.2
0	(8+9)-VII-2	-8853	85	1415	-36.58	20.19	70.18	132.00	192.00	192.00	2.0
0	(8+9)-III-1	-4796	-67	280	-19.82	-15.95	13.89	132.00	192.00	192.00	6.0
0	(8+9)-VII-3	6950	-89	-1329	28.72	-21.11	-65.88	132.00	192.00	192.00	1.5
0	(8+9)-IV-1	302	-240	-931	1.25	-56.70	-46.16	132.00	192.00	192.00	1.8
0	(8+9)-VII-4	5363	55	-639	22.16	12.90	-31.71	132.00	192.00	192.00	2.5
0	(8+9)-I-3	4847	-15	-1042	20.03	-3.66	-51.66	132.00	192.00	192.00	2.3
0	(8+9)-III-3	4479	-80	-883	18.51	-18.99	-43.77	132.00	192.00	192.00	2.1
0	(8+9)-IV-3	3084	-244	-1280	12.74	-57.61	-63.46	132.00	192.00	192.00	1.4
0	(8+9)-II-3	4309	-28	-1810	17.80	-6.52	-89.77	132.00	192.00	192.00	1.6
0	(8+9)-VIII-1	-440	-237	-797	-1.82	-56.06	-39.53	132.00	192.00	192.00	2.0
0	(8+9)-VIII-2	-5729	242	1500	-23.67	57.32	74.39	132.00	192.00	192.00	1.4
0	(8+9)-VIII-3	3825	-246	-1414	15.81	-58.25	-70.10	132.00	192.00	192.00	1.3
1935	(8+9)-I-1	-470	1	-207	-1.94	0.27	-10.24	132.00	192.00	192.00	18

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
0	(8+9)-VIII-4	-51	0.01	6.40	Si	>100
0	(8+9)-IV-1	111	0.03	6.40	Si	>100
0	(8+9)-VI-3	168	0.04	6.40	Si	>100
0	(8+9)-III-2	-88	0.02	6.40	Si	>100
0	(8+9)-IV-2	-128	0.03	6.40	Si	>100
0	(8+9)-III-3	108	0.03	6.40	Si	>100
0	(8+9)-VIII-2	-168	0.04	6.40	Si	>100
0	(8+9)-VII-2	-221	0.06	6.40	Si	>100
0	(8+9)-VII-4	170	0.04	6.40	Si	>100
0	(8+9)-VII-1	-149	0.04	6.40	Si	>100
0	(8+9)-I-2	-82	0.02	6.40	Si	>100
0	(8+9)-I-4	42	0.01	6.40	Si	>100
0	(8+9)-IV-3	148	0.04	6.40	Si	>100
0	(8+9)-II-2	-108	0.03	6.40	Si	>100
0	(8+9)-IV-4	-91	0.02	6.40	Si	>100
0	(8+9)-II-4	-71	0.02	6.40	Si	>100
0	(8+9)-V-1	-155	0.04	6.40	Si	>100
0	(8+9)-VIII-3	188	0.05	6.40	Si	>100
0	(8+9)-V-2	-215	0.06	6.40	Si	>100
0	(8+9)-I-1	-22	0.01	6.40	Si	>100
0	(8+9)-V-3	235	0.06	6.40	Si	>100
0	(8+9)-VII-3	241	0.06	6.40	Si	>100
0	(8+9)-VI-2	-148	0.04	6.40	Si	>100
0	(8+9)-VIII-1	71	0.02	6.40	Si	>100
0	(8+9)-I-3	102	0.03	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
0	(8+9)-II-3	128	0.03	6.40	Si	>100
0	(8+9)-V-4	176	0.05	6.40	Si	>100
250	(8+9)-III-1	-20	0.01	6.40	Si	>100
250	(8+9)-VI-4	-61	0.02	6.40	Si	>100
500	1	19	0.00	3.84	Si	>100
500	2	41	0.01	5.76	Si	>100
500	3	41	0.01	5.76	Si	>100
500	4	19	0.00	5.12	Si	>100
500	5	19	0.00	5.12	Si	>100
500	6	19	0.00	5.12	Si	>100
500	7	19	0.00	5.12	Si	>100
500	(8+9)-II-1	92	0.02	6.40	Si	>100
500	(8+9)-III-4	45	0.01	6.40	Si	>100
500	(8+9)-VI-1	83	0.02	6.40	Si	>100
Verifiche nella direzione secondaria						
0	(8+9)-VIII-4	-24	0.09	6.40	Si	70
0	(8+9)-III-3	44	0.17	6.40	Si	38
0	(8+9)-IV-2	-44	0.17	6.40	Si	38
0	(8+9)-III-4	19	0.07	6.40	Si	87
0	(8+9)-VIII-2	-48	0.18	6.40	Si	35
0	(8+9)-IV-1	39	0.15	6.40	Si	43
0	(8+9)-VII-4	33	0.13	6.40	Si	50
0	(8+9)-V-3	62	0.24	6.40	Si	27
0	(8+9)-VI-2	-60	0.23	6.40	Si	28
0	(8+9)-VIII-3	59	0.23	6.40	Si	28
0	(8+9)-I-3	48	0.18	6.40	Si	35
0	(8+9)-VIII-1	35	0.13	6.40	Si	48
0	(8+9)-II-1	51	0.20	6.40	Si	33
0	(8+9)-VII-3	58	0.22	6.40	Si	29
0	(8+9)-II-3	67	0.26	6.40	Si	25
0	(8+9)-V-4	30	0.11	6.40	Si	56
0	(8+9)-VI-3	71	0.27	6.40	Si	24
0	(8+9)-I-4	16	0.06	6.40	Si	>100
0	(8+9)-II-2	-56	0.21	6.40	Si	30
0	(8+9)-II-4	-40	0.15	6.40	Si	42
0	(8+9)-VI-4	-36	0.14	6.40	Si	47
0	(8+9)-IV-3	55	0.21	6.40	Si	31
0	(8+9)-IV-4	-28	0.11	6.40	Si	60
0	(8+9)-VI-1	47	0.18	6.40	Si	36
1935	(8+9)-VII-2	54	0.21	6.40	Si	31
1935	(8+9)-I-1	24	0.09	6.40	Si	71
1935	(8+9)-V-2	54	0.21	6.40	Si	31
1935	(8+9)-V-1	40	0.15	6.40	Si	42
1935	(8+9)-III-2	38	0.14	6.40	Si	45
1935	(8+9)-III-1	24	0.09	6.40	Si	69
1935	(8+9)-I-2	38	0.15	6.40	Si	44
1935	(8+9)-VII-1	41	0.15	6.40	Si	41
3870	1	14	0.06	3.84	Si	70
3870	2	30	0.11	5.76	Si	51
3870	3	30	0.11	5.76	Si	51
3870	4	14	0.06	5.12	Si	93
3870	5	14	0.06	5.12	Si	93
3870	6	14	0.06	5.12	Si	93
3870	7	14	0.06	5.12	Si	93

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	(8+9)-VII-1	7320	3.91	32.00	8.2	0.95	20.00	21	V	8.2
0	(8+9)-VII-4	-6489	-3.46	32.00	9.2	-0.84	20.00	24	V	9.2
250	(8+9)-VIII-4	6896	3.68	32.00	8.7	0.89	20.00	22	V	8.7
250	(8+9)-IV-1	-6696	-3.57	32.00	9.0	-0.87	20.00	23	V	9.0
250	(8+9)-VII-2	12209	6.52	32.00	4.9	1.58	20.00	13	V	4.9

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
250	(8+9)-III-4	-3125	-1.67	32.00	19	-0.40	20.00	50	V	19
250	(8+9)-IV-3	-10505	-5.61	32.00	5.7	-1.36	20.00	15	V	5.7
250	(8+9)-VIII-1	-5905	-3.15	32.00	10	-0.76	20.00	26	V	10
250	(8+9)-VIII-2	12287	6.56	32.00	4.9	1.59	20.00	13	V	4.9
250	(8+9)-IV-2	11496	6.14	32.00	5.2	1.49	20.00	13	V	5.2
250	(8+9)-I-2	9484	5.06	32.00	6.3	1.23	20.00	16	V	6.3
250	(8+9)-I-4	-3215	-1.72	32.00	19	-0.42	20.00	48	V	19
250	(8+9)-IV-4	7687	4.10	32.00	7.8	0.99	20.00	20	V	7.8
250	(8+9)-II-2	11197	5.98	32.00	5.4	1.45	20.00	14	V	5.4
250	(8+9)-V-1	6841	3.65	32.00	8.8	0.88	20.00	23	V	8.8
250	(8+9)-II-4	7388	3.94	32.00	8.1	0.95	20.00	21	V	8.1
250	(8+9)-V-2	12119	6.47	32.00	4.9	1.57	20.00	13	V	4.9
250	(8+9)-III-2	9574	5.11	32.00	6.3	1.24	20.00	16	V	6.3
250	(8+9)-V-3	-11128	-5.94	32.00	5.4	-1.44	20.00	14	V	5.4
250	(8+9)-VIII-3	-11296	-6.03	32.00	5.3	-1.46	20.00	14	V	5.3
250	(8+9)-V-4	-5850	-3.12	32.00	10	-0.76	20.00	26	V	10
250	(8+9)-I-3	-8493	-4.53	32.00	7.1	-1.10	20.00	18	V	7.1
250	(8+9)-VI-1	-5606	-2.99	32.00	11	-0.72	20.00	28	V	11
250	(8+9)-II-3	-10206	-5.45	32.00	5.9	-1.32	20.00	15	V	5.9
250	(8+9)-VI-2	11988	6.40	32.00	5.0	1.55	20.00	13	V	5.0
250	(8+9)-III-3	-8583	-4.58	32.00	7.0	-1.11	20.00	18	V	7.0
250	(8+9)-II-1	-6397	-3.42	32.00	9.4	-0.83	20.00	24	V	9.4
250	(8+9)-III-1	4116	2.20	32.00	15	0.53	20.00	38	V	15
250	(8+9)-I-1	4206	2.25	32.00	14	0.54	20.00	37	V	14
250	(8+9)-VI-3	-10997	-5.87	32.00	5.5	-1.42	20.00	14	V	5.5
250	(8+9)-VI-4	6597	3.52	32.00	9.1	0.85	20.00	23	V	9.1
250	(8+9)-VII-3	-11218	-5.99	32.00	5.3	-1.45	20.00	14	V	5.3
500	1	793	0.42	19.20	45	0.10	12.00	>100	V	45
500	2	1582	0.84	28.80	34	0.20	18.00	88	V	34
500	3	1582	0.84	28.80	34	0.20	18.00	88	V	34
500	4	793	0.42	25.60	60	0.10	16.00	>100	V	60
500	5	793	0.42	25.60	60	0.10	16.00	>100	V	60
500	6	793	0.42	25.60	60	0.10	16.00	>100	V	60
500	7	793	0.42	25.60	60	0.10	16.00	>100	V	60
Verifiche nella direzione secondaria										
1935	1	128	0.53	19.20	36	0.13	12.00	94	V	36
1935	2	260	1.08	28.80	27	0.26	18.00	69	V	27
1935	3	260	1.08	28.80	27	0.26	18.00	69	V	27
1935	4	128	0.53	25.60	49	0.13	16.00	>100	V	49
1935	5	128	0.53	25.60	49	0.13	16.00	>100	V	49
1935	6	128	0.53	25.60	49	0.13	16.00	>100	V	49
1935	7	128	0.53	25.60	49	0.13	16.00	>100	V	49
1935	(8+9)-VIII-4	954	3.94	32.00	8.1	0.95	20.00	21	V	8.1
1935	(8+9)-IV-2	1807	7.47	32.00	4.3	1.81	20.00	11	V	4.3
1935	(8+9)-V-1	1324	5.47	32.00	5.8	1.32	20.00	15	V	5.8
1935	(8+9)-I-2	1695	7.01	32.00	4.6	1.70	20.00	12	V	4.6
1935	(8+9)-V-2	2364	9.77	32.00	3.3	2.36	20.00	8.5	V	3.3
1935	(8+9)-I-4	-479	-1.98	32.00	16	-0.48	20.00	42	V	16
1935	(8+9)-V-3	-2187	-9.04	32.00	3.5	-2.19	20.00	9.1	V	3.5
1935	(8+9)-II-2	2147	8.87	32.00	3.6	2.15	20.00	9.3	V	3.6
1935	(8+9)-V-4	-1147	-4.74	32.00	6.7	-1.15	20.00	17	V	6.7
1935	(8+9)-II-4	1495	6.18	32.00	5.2	1.50	20.00	13	V	5.2
1935	(8+9)-VI-1	-1118	-4.62	32.00	6.9	-1.12	20.00	18	V	6.9
1935	(8+9)-III-2	1593	6.58	32.00	4.9	1.59	20.00	13	V	4.9
1935	(8+9)-VI-2	2348	9.70	32.00	3.3	2.35	20.00	8.5	V	3.3
1935	(8+9)-III-4	-581	-2.40	32.00	13	-0.58	20.00	34	V	13
1935	(8+9)-VI-3	-2171	-8.97	32.00	3.6	-2.17	20.00	9.2	V	3.6
1935	(8+9)-I-1	656	2.71	32.00	12	0.66	20.00	31	V	12
1935	(8+9)-VI-4	1295	5.35	32.00	6.0	1.29	20.00	15	V	6.0
1935	(8+9)-IV-4	1155	4.77	32.00	6.7	1.15	20.00	17	V	6.7
1935	(8+9)-VII-1	1426	5.89	32.00	5.4	1.43	20.00	14	V	5.4
1935	(8+9)-II-1	-1319	-5.45	32.00	5.9	-1.32	20.00	15	V	5.9
1935	(8+9)-VII-2	2262	9.35	32.00	3.4	2.26	20.00	8.8	V	3.4
1935	(8+9)-III-1	758	3.13	32.00	10	0.76	20.00	26	V	10

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
1935	(8+9)-VII-3	-2085	-8.62	32.00	3.7	-2.09	20.00	9.6	V	3.7
1935	(8+9)-IV-1	-978	-4.04	32.00	7.9	-0.98	20.00	20	V	7.9
1935	(8+9)-VII-4	-1250	-5.16	32.00	6.2	-1.25	20.00	16	V	6.2
1935	(8+9)-III-3	-1417	-5.85	32.00	5.5	-1.42	20.00	14	V	5.5
1935	(8+9)-IV-3	-1631	-6.74	32.00	4.7	-1.63	20.00	12	V	4.7
1935	(8+9)-II-3	-1971	-8.14	32.00	3.9	-1.97	20.00	10	V	3.9
1935	(8+9)-VIII-1	-778	-3.21	32.00	10.0	-0.78	20.00	26	V	10.0
1935	(8+9)-VIII-2	2008	8.30	32.00	3.9	2.01	20.00	10.0	V	3.9
1935	(8+9)-VIII-3	-1831	-7.57	32.00	4.2	-1.83	20.00	11	V	4.2
1935	(8+9)-I-3	-1519	-6.28	32.00	5.1	-1.52	20.00	13	V	5.1

Setto 29: origine (1275.7,2680.4,193.5), direzione (0.927376,-0.374131,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	(8+9)-VIII-4	-820	-7	3376	-0.29	-0.09	1.86	132.00	192.00	192.00	98
0	(8+9)-IV-1	1042	26	-3662	0.37	0.35	-2.02	132.00	192.00	192.00	66
0	(8+9)-VII-2	-1861	-16	6978	-0.66	-0.22	3.85	132.00	192.00	192.00	47
0	(8+9)-III-3	1325	26	-4620	0.47	0.34	-2.55	132.00	192.00	192.00	54
0	(8+9)-IV-2	-1543	-16	5987	-0.55	-0.21	3.30	132.00	192.00	192.00	55
0	(8+9)-III-4	549	13	-1726	0.20	0.18	-0.95	132.00	192.00	192.00	>100
0	(8+9)-VIII-2	-1718	-18	6597	-0.61	-0.24	3.64	132.00	192.00	192.00	49
0	(8+9)-VII-3	1908	33	-6654	0.68	0.44	-3.67	132.00	192.00	192.00	38
0	(8+9)-VII-4	1133	21	-3759	0.40	0.28	-2.07	132.00	192.00	192.00	65
0	(8+9)-I-2	-1334	-11	5242	-0.47	-0.15	2.89	132.00	192.00	192.00	63
0	(8+9)-IV-3	1590	33	-5663	0.57	0.43	-3.12	132.00	192.00	192.00	44
0	(8+9)-I-4	493	11	-1428	0.18	0.15	-0.79	132.00	192.00	192.00	>100
0	(8+9)-IV-4	-995	-9	3986	-0.35	-0.12	2.20	132.00	192.00	192.00	83
0	(8+9)-II-2	-1731	-23	6979	-0.62	-0.30	3.85	132.00	192.00	192.00	46
0	(8+9)-V-1	-1029	-2	3786	-0.37	-0.02	2.09	132.00	192.00	192.00	91
0	(8+9)-II-4	-1183	-16	4978	-0.42	-0.21	2.75	132.00	192.00	192.00	65
0	(8+9)-V-2	-1918	-18	7275	-0.68	-0.25	4.01	132.00	192.00	192.00	45
0	(8+9)-III-2	-1278	-9	4944	-0.45	-0.12	2.73	132.00	192.00	192.00	67
0	(8+9)-V-3	1965	35	-6952	0.70	0.47	-3.84	132.00	192.00	192.00	36
0	(8+9)-VIII-1	867	24	-3052	0.31	0.32	-1.68	132.00	192.00	192.00	78
0	(8+9)-V-4	1076	19	-3462	0.38	0.25	-1.91	132.00	192.00	192.00	71
0	(8+9)-I-3	1381	28	-4918	0.49	0.37	-2.71	132.00	192.00	192.00	51
0	(8+9)-VI-1	1055	31	-4044	0.38	0.41	-2.23	132.00	192.00	192.00	60
0	(8+9)-II-3	1778	39	-6655	0.63	0.53	-3.67	132.00	192.00	192.00	38
0	(8+9)-VI-2	-1906	-25	7589	-0.68	-0.33	4.19	132.00	192.00	192.00	42
0	(8+9)-VIII-3	1765	35	-6273	0.63	0.46	-3.46	132.00	192.00	192.00	40
0	(8+9)-II-1	1230	33	-4654	0.44	0.44	-2.57	132.00	192.00	192.00	53
0	(8+9)-III-1	-502	4	2049	-0.18	0.05	1.13	132.00	192.00	192.00	>100
0	(8+9)-I-1	-446	6	1752	-0.16	0.08	0.97	132.00	192.00	192.00	>100
0	(8+9)-VI-3	1953	42	-7265	0.70	0.56	-4.01	132.00	192.00	192.00	34
0	(8+9)-VI-4	-1008	-14	4367	-0.36	-0.18	2.41	132.00	192.00	192.00	74
0	(8+9)-VII-1	-1086	-4	4083	-0.39	-0.05	2.25	132.00	192.00	192.00	83
682	1	27	28	-85	0.01	0.38	-0.05	79.20	115.20	115.20	>100
682	2	50	58	-164	0.02	0.77	-0.09	118.80	172.80	172.80	>100
682	3	50	58	-164	0.02	0.77	-0.09	118.80	172.80	172.80	>100
682	4	27	28	-85	0.01	0.38	-0.05	105.60	153.60	153.60	>100
682	5	27	28	-85	0.01	0.38	-0.05	105.60	153.60	153.60	>100
682	6	27	28	-85	0.01	0.38	-0.05	105.60	153.60	153.60	>100
682	7	27	28	-85	0.01	0.38	-0.05	105.60	153.60	153.60	>100
Verifiche nella direzione secondaria											
0	1	-371	4	56	-1.12	0.77	1.50	79.20	115.20	115.20	51
0	2	-739	7	119	-2.24	1.25	3.17	118.80	172.80	172.80	39
0	3	-739	7	119	-2.24	1.25	3.17	118.80	172.80	172.80	39
0	4	-371	4	56	-1.12	0.77	1.50	105.60	153.60	153.60	68
0	5	-371	4	56	-1.12	0.77	1.50	105.60	153.60	153.60	68
0	6	-371	4	56	-1.12	0.77	1.50	105.60	153.60	153.60	68
0	7	-371	4	56	-1.12	0.77	1.50	105.60	153.60	153.60	68
0	(8+9)-VIII-4	5942	44	634	18.00	7.66	16.89	132.00	192.00	192.00	3.8

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-IV-2	9020	61	1813	27.33	10.63	48.31	132.00	192.00	192.00	1.9
0	(8+9)-V-1	3212	17	1872	9.73	2.87	49.90	132.00	192.00	192.00	2.9
0	(8+9)-I-2	6528	47	2135	19.78	8.12	56.89	132.00	192.00	192.00	2.0
0	(8+9)-V-2	9090	50	2924	27.54	8.72	77.94	132.00	192.00	192.00	1.5
0	(8+9)-I-4	-1169	-7	-1006	-3.54	-1.16	-26.81	132.00	192.00	192.00	6.8
0	(8+9)-V-3	-9609	-44	-2847	-29.11	-7.61	-75.89	132.00	192.00	192.00	2.2
0	(8+9)-II-2	10692	68	2263	32.39	11.70	60.31	132.00	192.00	192.00	1.6
0	(8+9)-V-4	-3731	-10	-1795	-11.30	-1.76	-47.85	132.00	192.00	192.00	3.8
0	(8+9)-II-4	8383	51	1321	25.40	8.92	35.20	132.00	192.00	192.00	2.4
0	(8+9)-VI-1	-8133	-44	-1007	-24.64	-7.63	-26.83	132.00	192.00	192.00	5.1
0	(8+9)-III-2	6026	45	2000	18.26	7.80	53.29	132.00	192.00	192.00	2.2
0	(8+9)-VI-2	11461	69	2500	34.72	11.88	66.62	132.00	192.00	192.00	1.5
0	(8+9)-III-4	-1670	-9	-1141	-5.06	-1.48	-30.40	132.00	192.00	192.00	6.0
0	(8+9)-VI-3	-11979	-62	-2423	-36.29	-10.77	-64.57	132.00	192.00	192.00	2.3
0	(8+9)-I-1	650	13	1083	1.97	2.27	28.86	132.00	192.00	192.00	5.6
0	(8+9)-VI-4	7614	50	1084	23.07	8.74	28.88	132.00	192.00	192.00	2.7
0	(8+9)-IV-4	6711	45	870	20.33	7.84	23.20	132.00	192.00	192.00	3.2
0	(8+9)-VII-1	3714	18	2007	11.25	3.19	53.50	132.00	192.00	192.00	2.6
0	(8+9)-II-1	-8902	-45	-1244	-26.97	-7.81	-33.15	132.00	192.00	192.00	4.3
0	(8+9)-VII-2	8589	48	2789	26.02	8.40	74.34	132.00	192.00	192.00	1.6
0	(8+9)-III-1	1152	15	1218	3.49	2.59	32.46	132.00	192.00	192.00	4.8
0	(8+9)-VII-3	-9107	-42	-2712	-27.59	-7.29	-72.29	132.00	192.00	192.00	2.3
0	(8+9)-IV-1	-7230	-39	-793	-21.90	-6.74	-21.15	132.00	192.00	192.00	6.3
0	(8+9)-VII-4	-4233	-12	-1930	-12.82	-2.08	-51.45	132.00	192.00	192.00	3.5
0	(8+9)-III-3	-6545	-39	-1923	-19.83	-6.69	-51.24	132.00	192.00	192.00	3.2
0	(8+9)-IV-3	-9538	-55	-1736	-28.90	-9.52	-46.26	132.00	192.00	192.00	3.2
0	(8+9)-II-3	-11211	-61	-2186	-33.96	-10.59	-58.26	132.00	192.00	192.00	2.6
0	(8+9)-VIII-1	-6461	-38	-557	-19.57	-6.56	-14.84	132.00	192.00	192.00	8.2
0	(8+9)-VIII-2	9788	62	2049	29.65	10.81	54.62	132.00	192.00	192.00	1.8
0	(8+9)-VIII-3	-10307	-56	-1972	-31.23	-9.70	-52.57	132.00	192.00	192.00	2.9
0	(8+9)-I-3	-7047	-40	-2058	-21.35	-7.01	-54.84	132.00	192.00	192.00	3.0

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
0	(8+9)-II-4	-42	0.01	6.40	Si	>100
0	(8+9)-VI-4	-36	0.01	6.40	Si	>100
0	(8+9)-VI-3	94	0.02	6.40	Si	>100
0	(8+9)-II-3	88	0.02	6.40	Si	>100
0	(8+9)-II-2	-56	0.01	6.40	Si	>100
0	(8+9)-II-1	74	0.02	6.40	Si	>100
0	(8+9)-VI-1	68	0.02	6.40	Si	>100
0	(8+9)-VI-2	-62	0.02	6.40	Si	>100
341	1	25	0.01	3.84	Si	>100
341	2	51	0.01	5.76	Si	>100
341	3	51	0.01	5.76	Si	>100
341	4	25	0.01	5.12	Si	>100
341	5	25	0.01	5.12	Si	>100
341	6	25	0.01	5.12	Si	>100
341	7	25	0.01	5.12	Si	>100
341	(8+9)-IV-1	43	0.01	6.40	Si	>100
341	(8+9)-IV-3	64	0.02	6.40	Si	>100
341	(8+9)-VIII-3	72	0.02	6.40	Si	>100
341	(8+9)-VIII-2	-38	0.01	6.40	Si	>100
341	(8+9)-VIII-1	35	0.01	6.40	Si	>100
341	(8+9)-IV-2	-30	0.01	6.40	Si	>100
682	(8+9)-VIII-4	52	0.01	6.40	Si	>100
682	(8+9)-I-4	91	0.02	6.40	Si	>100
682	(8+9)-III-2	-63	0.02	6.40	Si	>100
682	(8+9)-VII-1	-94	0.02	6.40	Si	>100
682	(8+9)-V-1	-87	0.02	6.40	Si	>100
682	(8+9)-VII-2	-93	0.02	6.40	Si	>100
682	(8+9)-V-3	134	0.03	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
682	(8+9)-VII-3	127	0.03	6.40	Si	>100
682	(8+9)-IV-4	43	0.01	6.40	Si	>100
682	(8+9)-VII-4	129	0.03	6.40	Si	>100
682	(8+9)-V-2	-100	0.03	6.40	Si	>100
682	(8+9)-V-4	122	0.03	6.40	Si	>100
682	(8+9)-I-3	104	0.03	6.40	Si	>100
682	(8+9)-I-1	-57	0.01	6.40	Si	>100
682	(8+9)-III-1	-64	0.02	6.40	Si	>100
682	(8+9)-III-4	98	0.03	6.40	Si	>100
682	(8+9)-III-3	97	0.03	6.40	Si	>100
682	(8+9)-I-2	-69	0.02	6.40	Si	>100
Verifiche nella direzione secondaria						
0	1	-9	0.02	3.84	Si	>100
0	2	-15	0.04	5.76	Si	>100
0	3	-15	0.04	5.76	Si	>100
0	4	-9	0.02	5.12	Si	>100
0	5	-9	0.02	5.12	Si	>100
0	6	-9	0.02	5.12	Si	>100
0	7	-9	0.02	5.12	Si	>100
0	(8+9)-VIII-4	-77	0.22	6.40	Si	30
0	(8+9)-IV-2	-111	0.31	6.40	Si	21
0	(8+9)-V-1	-37	0.10	6.40	Si	62
0	(8+9)-I-2	-87	0.24	6.40	Si	26
0	(8+9)-V-2	-103	0.29	6.40	Si	22
0	(8+9)-V-3	90	0.25	6.40	Si	25
0	(8+9)-II-2	-130	0.36	6.40	Si	18
0	(8+9)-VIII-3	103	0.29	6.40	Si	22
0	(8+9)-II-4	-101	0.28	6.40	Si	23
0	(8+9)-VI-1	84	0.24	6.40	Si	27
0	(8+9)-III-2	-81	0.23	6.40	Si	28
0	(8+9)-VI-2	-135	0.38	6.40	Si	17
0	(8+9)-III-4	14	0.04	6.40	Si	>100
0	(8+9)-VI-3	122	0.34	6.40	Si	19
0	(8+9)-I-1	-21	0.06	6.40	Si	>100
0	(8+9)-VI-4	-97	0.27	6.40	Si	24
0	(8+9)-IV-4	-82	0.23	6.40	Si	28
0	(8+9)-VII-1	-43	0.12	6.40	Si	54
0	(8+9)-II-1	89	0.25	6.40	Si	26
0	(8+9)-VII-2	-97	0.27	6.40	Si	24
0	(8+9)-III-1	-27	0.08	6.40	Si	85
0	(8+9)-VII-3	84	0.24	6.40	Si	27
0	(8+9)-IV-1	70	0.19	6.40	Si	33
0	(8+9)-I-3	74	0.21	6.40	Si	31
0	(8+9)-II-3	117	0.33	6.40	Si	19
0	(8+9)-III-3	69	0.19	6.40	Si	33
0	(8+9)-IV-3	98	0.27	6.40	Si	23
0	(8+9)-VII-4	30	0.08	6.40	Si	76
0	(8+9)-VIII-1	65	0.18	6.40	Si	35
0	(8+9)-VIII-2	-115	0.32	6.40	Si	20
3870	(8+9)-I-4	15	0.04	6.40	Si	>100
3870	(8+9)-V-4	29	0.08	6.40	Si	80

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	(8+9)-VIII-4	6900	3.68	32.00	8.7	0.89	20.00	22	V	8.7
0	(8+9)-IV-1	-7692	-4.11	32.00	7.8	-0.99	20.00	20	V	7.8
0	(8+9)-IV-3	-11934	-6.37	32.00	5.0	-1.54	20.00	13	V	5.0
0	(8+9)-II-1	-8692	-4.64	32.00	6.9	-1.12	20.00	18	V	6.9
0	(8+9)-IV-2	12334	6.58	32.00	4.9	1.59	20.00	13	V	4.9
0	(8+9)-VIII-2	13527	7.22	32.00	4.4	1.75	20.00	11	V	4.4
0	(8+9)-V-4	-7541	-4.03	32.00	7.9	-0.97	20.00	21	V	7.9
0	(8+9)-VII-4	-7841	-4.19	32.00	7.6	-1.01	20.00	20	V	7.6

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
0	(8+9)-IV-4	8093	4.32	32.00	7.4	1.05	20.00	19	V	7.4
0	(8+9)-VII-3	-13849	-7.39	32.00	4.3	-1.79	20.00	11	V	4.3
0	(8+9)-VII-2	14250	7.61	32.00	4.2	1.84	20.00	11	V	4.2
0	(8+9)-VI-3	-14126	-7.54	32.00	4.2	-1.83	20.00	11	V	4.2
0	(8+9)-VIII-1	-6499	-3.47	32.00	9.2	-0.84	20.00	24	V	9.2
0	(8+9)-VII-1	8242	4.40	32.00	7.3	1.06	20.00	19	V	7.3
0	(8+9)-VIII-3	-13127	-7.01	32.00	4.6	-1.70	20.00	12	V	4.6
0	(8+9)-V-3	-14149	-7.55	32.00	4.2	-1.83	20.00	11	V	4.2
0	(8+9)-V-2	14550	7.77	32.00	4.1	1.88	20.00	11	V	4.1
0	(8+9)-V-1	7942	4.24	32.00	7.5	1.03	20.00	19	V	7.5
341	(8+9)-VI-2	14595	7.79	32.00	4.1	1.89	20.00	11	V	4.1
341	(8+9)-II-4	9217	4.92	32.00	6.5	1.19	20.00	17	V	6.5
682	1	622	0.33	19.20	58	0.08	12.00	>100	V	58
682	2	1127	0.60	28.80	48	0.15	18.00	>100	V	48
682	3	1127	0.60	28.80	48	0.15	18.00	>100	V	48
682	4	622	0.33	25.60	77	0.08	16.00	>100	V	77
682	5	622	0.33	25.60	77	0.08	16.00	>100	V	77
682	6	622	0.33	25.60	77	0.08	16.00	>100	V	77
682	7	622	0.33	25.60	77	0.08	16.00	>100	V	77
682	(8+9)-VI-4	8997	4.80	32.00	6.7	1.16	20.00	17	V	6.7
682	(8+9)-I-3	-13404	-7.16	32.00	4.5	-1.73	20.00	12	V	4.5
682	(8+9)-III-3	-12135	-6.48	32.00	4.9	-1.57	20.00	13	V	4.9
682	(8+9)-VI-1	-8116	-4.33	32.00	7.4	-1.05	20.00	19	V	7.4
682	(8+9)-II-2	14869	7.94	32.00	4.0	1.92	20.00	10	V	4.0
682	(8+9)-I-2	14285	7.63	32.00	4.2	1.85	20.00	11	V	4.2
682	(8+9)-I-1	7510	4.01	32.00	8.0	0.97	20.00	21	V	8.0
682	(8+9)-III-4	-7898	-4.22	32.00	7.6	-1.02	20.00	20	V	7.6
682	(8+9)-II-3	-13989	-7.47	32.00	4.3	-1.81	20.00	11	V	4.3
682	(8+9)-III-1	8779	4.69	32.00	6.8	1.13	20.00	18	V	6.8
682	(8+9)-III-2	13016	6.95	32.00	4.6	1.68	20.00	12	V	4.6
682	(8+9)-I-4	-6629	-3.54	32.00	9.0	-0.86	20.00	23	V	9.0
Verifiche nella direzione secondaria										
0	(8+9)-VIII-4	1588	4.81	32.00	6.7	1.16	20.00	17	V	6.7
0	(8+9)-V-2	3583	10.85	32.00	2.9	2.63	20.00	7.6	V	2.9
0	(8+9)-II-2	3458	10.48	32.00	3.1	2.54	20.00	7.9	V	3.1
0	(8+9)-IV-2	2874	8.71	32.00	3.7	2.11	20.00	9.5	V	3.7
0	(8+9)-II-3	-3289	-9.96	32.00	3.2	-2.41	20.00	8.3	V	3.2
0	(8+9)-VIII-2	3169	9.60	32.00	3.3	2.32	20.00	8.6	V	3.3
0	(8+9)-II-4	2466	7.47	32.00	4.3	1.81	20.00	11	V	4.3
0	(8+9)-VII-3	-3239	-9.81	32.00	3.3	-2.37	20.00	8.4	V	3.3
0	(8+9)-VI-1	-2003	-6.07	32.00	5.3	-1.47	20.00	14	V	5.3
0	(8+9)-VI-3	-3584	-10.86	32.00	2.9	-2.63	20.00	7.6	V	2.9
0	(8+9)-III-2	2426	7.35	32.00	4.4	1.78	20.00	11	V	4.4
0	(8+9)-I-3	-2432	-7.37	32.00	4.3	-1.78	20.00	11	V	4.3
0	(8+9)-III-3	-2257	-6.84	32.00	4.7	-1.65	20.00	12	V	4.7
0	(8+9)-II-1	-2297	-6.96	32.00	4.6	-1.68	20.00	12	V	4.6
0	(8+9)-V-3	-3414	-10.34	32.00	3.1	-2.50	20.00	8.0	V	3.1
0	(8+9)-VIII-1	-1419	-4.30	32.00	7.4	-1.04	20.00	19	V	7.4
0	(8+9)-IV-1	-1713	-5.19	32.00	6.2	-1.26	20.00	16	V	6.2
0	(8+9)-VIII-3	-3000	-9.09	32.00	3.5	-2.20	20.00	9.1	V	3.5
0	(8+9)-VI-4	2172	6.58	32.00	4.9	1.59	20.00	13	V	4.9
0	(8+9)-VI-2	3753	11.37	32.00	2.8	2.75	20.00	7.3	V	2.8
0	(8+9)-I-2	2601	7.88	32.00	4.1	1.91	20.00	10	V	4.1
0	(8+9)-IV-3	-2705	-8.20	32.00	3.9	-1.98	20.00	10	V	3.9
0	(8+9)-IV-4	1882	5.70	32.00	5.6	1.38	20.00	14	V	5.6
1935	1	123	0.37	19.20	51	0.09	12.00	>100	V	51
1935	2	237	0.72	28.80	40	0.17	18.00	>100	V	40
1935	3	237	0.72	28.80	40	0.17	18.00	>100	V	40
1935	4	123	0.37	25.60	69	0.09	16.00	>100	V	69
1935	5	123	0.37	25.60	69	0.09	16.00	>100	V	69
1935	6	123	0.37	25.60	69	0.09	16.00	>100	V	69
1935	7	123	0.37	25.60	69	0.09	16.00	>100	V	69
1935	(8+9)-VII-1	2052	6.22	32.00	5.1	1.50	20.00	13	V	5.1
1935	(8+9)-I-1	889	2.69	32.00	12	0.65	20.00	31	V	12

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
1935	(8+9)-VII-2	3408	10.33	32.00	3.1	2.50	20.00	8.0	V	3.1
1935	(8+9)-I-4	-717	-2.17	32.00	15	-0.53	20.00	38	V	15
1935	(8+9)-VII-4	-1880	-5.69	32.00	5.6	-1.38	20.00	15	V	5.6
1935	(8+9)-III-1	1062	3.22	32.00	9.9	0.78	20.00	26	V	9.9
1935	(8+9)-V-4	-1707	-5.17	32.00	6.2	-1.25	20.00	16	V	6.2
1935	(8+9)-III-4	-890	-2.69	32.00	12	-0.65	20.00	31	V	12
1935	(8+9)-V-1	1879	5.69	32.00	5.6	1.38	20.00	15	V	5.6

Setto 30: origine (1164.4,2725.3,328.5), direzione (0.927376,-0.374131,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	(8+9)-III-2	1516	29	883	1.78	1.27	5.33	132.00	192.00	192.00	21
0	(8+9)-I-2	1621	31	943	1.91	1.37	5.69	132.00	192.00	192.00	20
0	(8+9)-VIII-4	940	17	554	1.11	0.74	3.34	132.00	192.00	192.00	34
0	(8+9)-V-1	1209	19	709	1.42	0.86	4.28	132.00	192.00	192.00	27
0	(8+9)-VII-2	2148	41	1250	2.53	1.82	7.55	132.00	192.00	192.00	15
0	(8+9)-IV-4	1129	20	664	1.33	0.90	4.01	132.00	192.00	192.00	28
0	(8+9)-VI-4	1289	24	753	1.52	1.07	4.54	132.00	192.00	192.00	25
0	(8+9)-IV-2	1757	35	1024	2.07	1.53	6.18	132.00	192.00	192.00	18
0	(8+9)-V-2	2252	43	1310	2.65	1.92	7.91	132.00	192.00	192.00	14
0	(8+9)-II-2	2106	42	1223	2.48	1.87	7.38	132.00	192.00	192.00	15
0	(8+9)-VI-2	2295	46	1333	2.70	2.03	8.05	132.00	192.00	192.00	14
0	(8+9)-I-1	578	7	342	0.68	0.32	2.07	132.00	192.00	192.00	57
0	(8+9)-VII-1	1314	22	769	1.55	0.96	4.64	132.00	192.00	192.00	24
0	(8+9)-VIII-2	1946	38	1134	2.29	1.70	6.85	132.00	192.00	192.00	16
0	(8+9)-II-4	1478	28	863	1.74	1.23	5.21	132.00	192.00	192.00	21
0	(8+9)-III-1	682	9	402	0.80	0.42	2.43	132.00	192.00	192.00	48
1200	1	-81	13	-57	-0.10	0.57	-0.35	79.20	115.20	115.20	>100
1200	2	-167	27	-116	-0.20	1.18	-0.70	118.80	172.80	172.80	92
1200	3	-167	27	-116	-0.20	1.18	-0.70	118.80	172.80	172.80	92
1200	4	-81	13	-57	-0.10	0.57	-0.35	105.60	153.60	153.60	>100
1200	5	-81	13	-57	-0.10	0.57	-0.35	105.60	153.60	153.60	>100
1200	6	-81	13	-57	-0.10	0.57	-0.35	105.60	153.60	153.60	>100
1200	7	-81	13	-57	-0.10	0.57	-0.35	105.60	153.60	153.60	>100
1200	(8+9)-IV-1	1811	22	839	2.13	0.96	5.07	132.00	192.00	192.00	21
1200	(8+9)-III-3	2485	28	1186	2.93	1.26	7.16	132.00	192.00	192.00	15
1200	(8+9)-II-1	2411	25	1160	2.84	1.11	7.00	132.00	192.00	192.00	16
1200	(8+9)-I-3	2665	29	1282	3.14	1.30	7.74	132.00	192.00	192.00	14
1200	(8+9)-II-3	3502	34	1689	4.12	1.49	10.20	132.00	192.00	192.00	11
1200	(8+9)-V-4	1952	25	933	2.30	1.09	5.63	132.00	192.00	192.00	19
1200	(8+9)-VII-3	3579	36	1715	4.21	1.59	10.36	132.00	192.00	192.00	11
1200	(8+9)-I-4	858	17	404	1.01	0.76	2.44	132.00	192.00	192.00	41
1200	(8+9)-VII-4	2132	26	1029	2.51	1.14	6.21	132.00	192.00	192.00	17
1200	(8+9)-VI-1	2083	23	1001	2.45	1.01	6.04	132.00	192.00	192.00	18
1200	(8+9)-VI-3	3830	36	1848	4.51	1.59	11.16	132.00	192.00	192.00	9.9
1200	(8+9)-V-3	3759	37	1811	4.43	1.64	10.94	132.00	192.00	192.00	10
1200	(8+9)-VIII-1	1482	19	680	1.75	0.86	4.11	132.00	192.00	192.00	26
1200	(8+9)-III-4	1038	18	500	1.22	0.80	3.02	132.00	192.00	192.00	34
1200	(8+9)-VIII-3	3229	33	1527	3.80	1.44	9.22	132.00	192.00	192.00	12
1200	(8+9)-IV-3	2901	30	1369	3.42	1.34	8.26	132.00	192.00	192.00	13
Verifiche nella direzione secondaria											
0	(8+9)-VIII-4	-688	-13	2595	-1.18	-1.25	22.34	132.00	192.00	192.00	8.1
0	(8+9)-VII-2	-1181	-0	6205	-2.03	-0.04	53.42	132.00	192.00	192.00	3.6
0	(8+9)-III-3	-231	4	-4323	-0.40	0.41	-37.22	132.00	192.00	192.00	5.1
0	(8+9)-IV-2	-931	-12	5019	-1.60	-1.15	43.20	132.00	192.00	192.00	4.3
0	(8+9)-III-4	-370	-4	-1875	-0.64	-0.38	-16.14	132.00	192.00	192.00	12
0	(8+9)-VIII-2	-990	-11	5579	-1.71	-1.12	48.03	132.00	192.00	192.00	3.9
0	(8+9)-IV-1	-468	15	-3142	-0.81	1.48	-27.05	132.00	192.00	192.00	6.7
0	(8+9)-VII-4	-173	-5	-3744	-0.30	-0.49	-32.23	132.00	192.00	192.00	5.9
0	(8+9)-I-1	-841	7	1578	-1.45	0.68	13.59	132.00	192.00	192.00	13
0	(8+9)-IV-3	-284	14	-5006	-0.49	1.41	-43.09	132.00	192.00	192.00	4.3
0	(8+9)-I-3	-226	5	-4632	-0.39	0.46	-39.88	132.00	192.00	192.00	4.8

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-IV-4	-747	-12	3155	-1.29	-1.22	27.16	132.00	192.00	192.00	6.8
0	(8+9)-II-1	-454	17	-4173	-0.78	1.63	-35.93	132.00	192.00	192.00	5.1
0	(8+9)-V-1	-1038	8	3447	-1.79	0.79	29.68	132.00	192.00	192.00	6.3
0	(8+9)-II-3	-269	16	-6037	-0.46	1.57	-51.97	132.00	192.00	192.00	3.6
0	(8+9)-V-2	-1185	-1	6514	-2.04	-0.09	56.08	132.00	192.00	192.00	3.4
0	(8+9)-III-1	-846	6	1888	-1.46	0.64	16.25	132.00	192.00	192.00	11
0	(8+9)-V-3	-30	4	-6501	-0.05	0.35	-55.97	132.00	192.00	192.00	3.4
0	(8+9)-VIII-3	-225	14	-5566	-0.39	1.38	-47.92	132.00	192.00	192.00	3.9
0	(8+9)-V-4	-178	-5	-3434	-0.31	-0.54	-29.57	132.00	192.00	192.00	6.4
0	(8+9)-VII-3	-34	3	-6192	-0.06	0.30	-53.31	132.00	192.00	192.00	3.6
0	(8+9)-VI-1	-513	17	-3613	-0.88	1.67	-31.10	132.00	192.00	192.00	5.9
0	(8+9)-I-4	-374	-4	-1565	-0.64	-0.43	-13.48	132.00	192.00	192.00	14
0	(8+9)-VI-2	-1005	-13	6610	-1.73	-1.28	56.91	132.00	192.00	192.00	3.3
0	(8+9)-II-4	-762	-14	4186	-1.31	-1.38	36.04	132.00	192.00	192.00	5.1
0	(8+9)-VIII-1	-527	15	-2582	-0.91	1.51	-22.23	132.00	192.00	192.00	8.1
0	(8+9)-I-2	-989	-2	4645	-1.70	-0.20	39.99	132.00	192.00	192.00	4.8
0	(8+9)-II-2	-946	-13	6050	-1.63	-1.31	52.08	132.00	192.00	192.00	3.6
0	(8+9)-III-2	-985	-2	4336	-1.70	-0.15	37.33	132.00	192.00	192.00	5.1
0	(8+9)-VI-3	-210	16	-6597	-0.36	1.53	-56.80	132.00	192.00	192.00	3.3
0	(8+9)-VI-4	-703	-14	3626	-1.21	-1.41	31.21	132.00	192.00	192.00	5.9
0	(8+9)-VII-1	-1042	8	3757	-1.79	0.74	32.34	132.00	192.00	192.00	5.8
585	1	-718	1	245	-1.24	0.12	2.11	79.20	115.20	115.20	51
585	2	-1472	3	509	-2.53	0.28	4.38	118.80	172.80	172.80	37
585	3	-1472	3	509	-2.53	0.28	4.38	118.80	172.80	172.80	37
585	4	-718	1	245	-1.24	0.12	2.11	105.60	153.60	153.60	69
585	5	-718	1	245	-1.24	0.12	2.11	105.60	153.60	153.60	69
585	6	-718	1	245	-1.24	0.12	2.11	105.60	153.60	153.60	69
585	7	-718	1	245	-1.24	0.12	2.11	105.60	153.60	153.60	69

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Ty kg	τ_d kg/cmq	fvd kg/cmq	RS	Cs
0	(8+9)-VI-4	-28	0.02	6.40	Si	>100
0	(8+9)-IV-4	-23	0.02	6.40	Si	>100
0	(8+9)-VIII-1	41	0.04	6.40	Si	>100
0	(8+9)-VIII-4	-18	0.02	6.40	Si	>100
600	2	36	0.03	5.76	Si	>100
600	3	36	0.03	5.76	Si	>100
600	(8+9)-VII-4	51	0.04	6.40	Si	>100
600	(8+9)-III-3	59	0.05	6.40	Si	>100
600	(8+9)-IV-3	67	0.06	6.40	Si	>100
600	(8+9)-I-1	-6	0.01	6.40	Si	>100
600	(8+9)-VIII-3	72	0.06	6.40	Si	>100
600	(8+9)-I-3	62	0.05	6.40	Si	>100
600	(8+9)-V-1	-25	0.02	6.40	Si	>100
600	(8+9)-II-1	57	0.05	6.40	Si	>100
600	(8+9)-V-2	-58	0.05	6.40	Si	>100
600	(8+9)-II-3	77	0.07	6.40	Si	97
600	(8+9)-V-3	81	0.07	6.40	Si	92
600	(8+9)-III-1	-9	0.01	6.40	Si	>100
600	(8+9)-V-4	48	0.04	6.40	Si	>100
600	(8+9)-VIII-2	-49	0.04	6.40	Si	>100
600	(8+9)-VI-1	51	0.04	6.40	Si	>100
600	(8+9)-IV-1	46	0.04	6.40	Si	>100
600	(8+9)-VI-2	-59	0.05	6.40	Si	>100
600	(8+9)-I-2	-39	0.03	6.40	Si	>100
600	(8+9)-VI-3	83	0.07	6.40	Si	90
600	(8+9)-II-2	-54	0.05	6.40	Si	>100
600	(8+9)-III-2	-36	0.03	6.40	Si	>100
600	(8+9)-IV-2	-43	0.04	6.40	Si	>100
600	(8+9)-I-4	29	0.03	6.40	Si	>100
600	(8+9)-II-4	-33	0.03	6.40	Si	>100
600	(8+9)-III-4	32	0.03	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
600	(8+9)-VII-1	-28	0.02	6.40	Si	>100
600	(8+9)-VII-2	-55	0.05	6.40	Si	>100
600	(8+9)-VII-3	78	0.07	6.40	Si	96
1200	1	17	0.01	3.84	Si	>100
1200	4	17	0.01	5.12	Si	>100
1200	5	17	0.01	5.12	Si	>100
1200	6	17	0.01	5.12	Si	>100
1200	7	17	0.01	5.12	Si	>100
Verifiche nella direzione secondaria						
0	(8+9)-IV-2	12	0.02	6.40	Si	>100
0	(8+9)-I-2	17	0.03	6.40	Si	>100
0	(8+9)-II-1	-17	0.03	6.40	Si	>100
0	(8+9)-VIII-2	18	0.03	6.40	Si	>100
0	(8+9)-II-2	27	0.04	6.40	Si	>100
0	(8+9)-VII-2	35	0.05	6.40	Si	>100
0	(8+9)-II-3	-22	0.04	6.40	Si	>100
0	(8+9)-VI-4	15	0.02	6.40	Si	>100
0	(8+9)-II-4	21	0.03	6.40	Si	>100
0	(8+9)-I-1	4	0.01	6.40	Si	>100
0	(8+9)-III-1	8	0.01	6.40	Si	>100
0	(8+9)-VI-2	33	0.05	6.40	Si	>100
0	(8+9)-III-2	13	0.02	6.40	Si	>100
0	(8+9)-VI-3	-29	0.05	6.40	Si	>100
0	(8+9)-VII-4	-26	0.04	6.40	Si	>100
0	(8+9)-V-3	-35	0.06	6.40	Si	>100
0	(8+9)-VII-1	30	0.05	6.40	Si	>100
0	(8+9)-V-2	39	0.06	6.40	Si	>100
0	(8+9)-V-1	26	0.04	6.40	Si	>100
0	(8+9)-IV-4	7	0.01	6.40	Si	>100
585	(8+9)-VIII-4	4	0.01	6.40	Si	>100
1170	1	7	0.01	3.84	Si	>100
1170	2	14	0.02	5.76	Si	>100
1170	3	14	0.02	5.76	Si	>100
1170	4	7	0.01	5.12	Si	>100
1170	5	7	0.01	5.12	Si	>100
1170	6	7	0.01	5.12	Si	>100
1170	7	7	0.01	5.12	Si	>100
1170	(8+9)-IV-3	19	0.03	6.40	Si	>100
1170	(8+9)-VII-3	30	0.05	6.40	Si	>100
1170	(8+9)-VI-1	11	0.02	6.40	Si	>100
1170	(8+9)-III-4	14	0.02	6.40	Si	>100
1170	(8+9)-III-3	21	0.03	6.40	Si	>100
1170	(8+9)-I-3	21	0.03	6.40	Si	>100
1170	(8+9)-I-4	14	0.02	6.40	Si	>100
1170	(8+9)-VIII-1	8	0.01	6.40	Si	>100
1170	(8+9)-IV-1	11	0.02	6.40	Si	>100
1170	(8+9)-VIII-3	22	0.03	6.40	Si	>100
1170	(8+9)-V-4	24	0.04	6.40	Si	>100

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	(8+9)-I-4	-1234	-2.18	32.00	15	-0.53	20.00	38	V	15
0	(8+9)-V-4	-2737	-4.83	32.00	6.6	-1.17	20.00	17	V	6.6
0	(8+9)-VII-4	-2987	-5.27	32.00	6.1	-1.28	20.00	16	V	6.1
0	(8+9)-VI-1	-2926	-5.17	32.00	6.2	-1.25	20.00	16	V	6.2
0	(8+9)-VIII-1	-2093	-3.70	32.00	8.7	-0.89	20.00	22	V	8.7
0	(8+9)-IV-1	-2544	-4.49	32.00	7.1	-1.09	20.00	18	V	7.1
0	(8+9)-III-4	-1484	-2.62	32.00	12	-0.63	20.00	32	V	12
0	(8+9)-II-1	-3377	-5.96	32.00	5.4	-1.44	20.00	14	V	5.4
1200	1	429	0.76	19.20	25	0.18	12.00	65	V	25
1200	2	847	1.50	28.80	19	0.36	18.00	50	V	19
1200	3	847	1.50	28.80	19	0.36	18.00	50	V	19

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
1200	4	429	0.76	25.60	34	0.18	16.00	87	V	34
1200	5	429	0.76	25.60	34	0.18	16.00	87	V	34
1200	6	429	0.76	25.60	34	0.18	16.00	87	V	34
1200	7	429	0.76	25.60	34	0.18	16.00	87	V	34
1200	(8+9)-VIII-4	2557	4.52	32.00	7.1	1.09	20.00	18	V	7.1
1200	(8+9)-V-2	5965	10.53	32.00	3.0	2.55	20.00	7.8	V	3.0
1200	(8+9)-I-3	-3732	-6.59	32.00	4.9	-1.59	20.00	13	V	4.9
1200	(8+9)-VI-2	6047	10.68	32.00	3.0	2.58	20.00	7.7	V	3.0
1200	(8+9)-III-3	-3465	-6.12	32.00	5.2	-1.48	20.00	14	V	5.2
1200	(8+9)-VI-3	-5449	-9.62	32.00	3.3	-2.33	20.00	8.6	V	3.3
1200	(8+9)-III-1	1928	3.41	32.00	9.4	0.82	20.00	24	V	9.4
1200	(8+9)-VI-4	3448	6.09	32.00	5.3	1.47	20.00	14	V	5.3
1200	(8+9)-IV-3	-4068	-7.18	32.00	4.5	-1.74	20.00	12	V	4.5
1200	(8+9)-VII-1	3563	6.29	32.00	5.1	1.52	20.00	13	V	5.1
1200	(8+9)-V-1	3296	5.82	32.00	5.5	1.41	20.00	14	V	5.5
1200	(8+9)-VII-2	5698	10.06	32.00	3.2	2.43	20.00	8.2	V	3.2
1200	(8+9)-V-3	-5367	-9.48	32.00	3.4	-2.29	20.00	8.7	V	3.4
1200	(8+9)-VII-3	-5100	-9.01	32.00	3.6	-2.18	20.00	9.2	V	3.6
1200	(8+9)-II-2	5556	9.81	32.00	3.3	2.37	20.00	8.4	V	3.3
1200	(8+9)-I-1	1661	2.93	32.00	11	0.71	20.00	28	V	11
1200	(8+9)-II-4	3938	6.95	32.00	4.6	1.68	20.00	12	V	4.6
1200	(8+9)-II-3	-4958	-8.76	32.00	3.7	-2.12	20.00	9.4	V	3.7
1200	(8+9)-III-2	4063	7.17	32.00	4.5	1.74	20.00	12	V	4.5
1200	(8+9)-IV-4	3048	5.38	32.00	5.9	1.30	20.00	15	V	5.9
1200	(8+9)-I-2	4330	7.65	32.00	4.2	1.85	20.00	11	V	4.2
1200	(8+9)-VIII-2	5156	9.11	32.00	3.5	2.20	20.00	9.1	V	3.5
1200	(8+9)-VIII-3	-4558	-8.05	32.00	4.0	-1.95	20.00	10	V	4.0
1200	(8+9)-IV-2	4666	8.24	32.00	3.9	1.99	20.00	10	V	3.9
Verifiche nella direzione secondaria										
0	1	223	0.38	19.20	50	0.09	12.00	>100	V	50
0	2	447	0.77	28.80	37	0.19	18.00	97	V	37
0	3	447	0.77	28.80	37	0.19	18.00	97	V	37
0	4	223	0.38	25.60	67	0.09	16.00	>100	V	67
0	5	223	0.38	25.60	67	0.09	16.00	>100	V	67
0	6	223	0.38	25.60	67	0.09	16.00	>100	V	67
0	7	223	0.38	25.60	67	0.09	16.00	>100	V	67
1170	(8+9)-VIII-4	2527	4.35	32.00	7.4	1.05	20.00	19	V	7.4
1170	(8+9)-IV-2	4727	8.14	32.00	3.9	1.97	20.00	10	V	3.9
1170	(8+9)-V-1	3230	5.56	32.00	5.8	1.35	20.00	15	V	5.8
1170	(8+9)-I-2	4352	7.49	32.00	4.3	1.81	20.00	11	V	4.3
1170	(8+9)-V-2	6048	10.41	32.00	3.1	2.52	20.00	7.9	V	3.1
1170	(8+9)-I-4	-1286	-2.21	32.00	14	-0.54	20.00	37	V	14
1170	(8+9)-V-3	-5799	-9.99	32.00	3.2	-2.42	20.00	8.3	V	3.2
1170	(8+9)-II-2	5667	9.76	32.00	3.3	2.36	20.00	8.5	V	3.3
1170	(8+9)-V-4	-2982	-5.13	32.00	6.2	-1.24	20.00	16	V	6.2
1170	(8+9)-II-4	3975	6.84	32.00	4.7	1.66	20.00	12	V	4.7
1170	(8+9)-VI-1	-3218	-5.54	32.00	5.8	-1.34	20.00	15	V	5.8
1170	(8+9)-III-2	4071	7.01	32.00	4.6	1.70	20.00	12	V	4.6
1170	(8+9)-VI-2	6175	10.63	32.00	3.0	2.57	20.00	7.8	V	3.0
1170	(8+9)-III-4	-1568	-2.70	32.00	12	-0.65	20.00	31	V	12
1170	(8+9)-VI-3	-5927	-10.20	32.00	3.1	-2.47	20.00	8.1	V	3.1
1170	(8+9)-I-1	1534	2.64	32.00	12	0.64	20.00	31	V	12
1170	(8+9)-VI-4	3466	5.97	32.00	5.4	1.44	20.00	14	V	5.4
1170	(8+9)-IV-4	3036	5.23	32.00	6.1	1.26	20.00	16	V	6.1
1170	(8+9)-VII-1	3512	6.05	32.00	5.3	1.46	20.00	14	V	5.3
1170	(8+9)-II-1	-3727	-6.42	32.00	5.0	-1.55	20.00	13	V	5.0
1170	(8+9)-VII-2	5766	9.93	32.00	3.2	2.40	20.00	8.3	V	3.2
1170	(8+9)-III-1	1816	3.13	32.00	10	0.76	20.00	26	V	10
1170	(8+9)-VII-3	-5518	-9.50	32.00	3.4	-2.30	20.00	8.7	V	3.4
1170	(8+9)-IV-1	-2787	-4.80	32.00	6.7	-1.16	20.00	17	V	6.7
1170	(8+9)-VII-4	-3263	-5.62	32.00	5.7	-1.36	20.00	15	V	5.7
1170	(8+9)-III-3	-3822	-6.58	32.00	4.9	-1.59	20.00	13	V	4.9
1170	(8+9)-IV-3	-4479	-7.71	32.00	4.1	-1.87	20.00	11	V	4.1
1170	(8+9)-II-3	-5418	-9.33	32.00	3.4	-2.26	20.00	8.9	V	3.4

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
1170	(8+9)-VIII-1	-2278	-3.92	32.00	8.2	-0.95	20.00	21	V	8.2
1170	(8+9)-VIII-2	5236	9.01	32.00	3.5	2.18	20.00	9.2	V	3.5
1170	(8+9)-VIII-3	-4987	-8.59	32.00	3.7	-2.08	20.00	9.6	V	3.7
1170	(8+9)-I-3	-4104	-7.07	32.00	4.5	-1.71	20.00	12	V	4.5

Verifiche a instabilità

Setto(X)	Comb.	krit _c	krit _m	λ_{relc}	λ_{relm}	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
(cm)						kg/cm ^q	kg/cm ^q	kg/cm ^q	kg/cm ^q	kg/cm ^q	kg/cm ^q	
28(50.0)	(8+9)-VI-2	--	--	--	--	0.40	0.54	-2.39	132.00	192.00	192.00	55
29(0.0)	(8+9)-VI-3	--	--	--	--	0.70	0.56	-4.01	132.00	192.00	192.00	34
30(120.0)	(8+9)-VI-3	--	--	--	--	4.51	1.59	11.16	132.00	192.00	192.00	9.9

Parete Xlam 6 - Nodi: [15-16-6-7-17-18-108-107] - **Crit.Prog.** Criterio di verifica XLAM 0 - **Verificato:**
[Cs=1.269,Comb=(8+9)-VIII-3]

Geometria setti

Setto	Crit.	X mm	L cm	S cm	X90 mm	L90 cm	S90 cm
28	Criterio di verifica XLAM 0	0	387.0	12.1	0	50.0	12.1
		250	387.0	12.1	1935	50.0	12.1
		500	387.0	12.1	3870	50.0	12.1
29	Criterio di verifica XLAM 0	0	387.0	12.1	0	68.2	12.1
		341	387.0	12.1	1935	68.2	12.1
		682	387.0	12.1	3870	68.2	12.1
30	Criterio di verifica XLAM 0	0	117.0	12.1	0	120.0	12.1
		600	117.0	12.1	585	120.0	12.1
		1200	117.0	12.1	1170	120.0	12.1

Setto 28: origine (1118.0,2744.0,193.5), direzione (0.927376,-0.374131,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X mm	Comb.	N kg	Mx kg*m	My kg*m	σ_n kg/cm ^q	σ_{mx} kg/cm ^q	σ_{my} kg/cm ^q	ftd kg/cm ^q	fcd kg/cm ^q	fmd kg/cm ^q	Cs
0	1	-23	-14	239	-0.01	-0.19	0.13	79.20	115.20	115.20	>100
0	2	-67	-31	498	-0.02	-0.41	0.27	118.80	172.80	172.80	>100
0	3	-67	-31	498	-0.02	-0.41	0.27	118.80	172.80	172.80	>100
0	4	-23	-14	239	-0.01	-0.19	0.13	105.60	153.60	153.60	>100
0	5	-23	-14	239	-0.01	-0.19	0.13	105.60	153.60	153.60	>100
0	6	-23	-14	239	-0.01	-0.19	0.13	105.60	153.60	153.60	>100
0	7	-23	-14	239	-0.01	-0.19	0.13	105.60	153.60	153.60	>100
0	(8+9)-VIII-4	537	29	1514	0.19	0.39	0.84	132.00	192.00	192.00	>100
0	(8+9)-IV-1	-779	-56	-1265	-0.28	-0.75	-0.70	132.00	192.00	192.00	>100
0	(8+9)-VIII-1	-567	-48	-1184	-0.20	-0.65	-0.65	132.00	192.00	192.00	>100
0	(8+9)-IV-4	749	37	1594	0.27	0.49	0.88	132.00	192.00	192.00	>100
500	(8+9)-V-1	544	17	-2269	0.19	0.23	-1.25	132.00	192.00	192.00	>100
500	(8+9)-I-2	766	27	-3085	0.27	0.36	-1.70	132.00	192.00	192.00	78
500	(8+9)-V-3	-1022	-48	3965	-0.36	-0.64	2.19	132.00	192.00	192.00	68
500	(8+9)-II-2	1023	37	-3995	0.36	0.49	-2.20	132.00	192.00	192.00	59
500	(8+9)-V-4	-507	-27	2003	-0.18	-0.35	1.11	132.00	192.00	192.00	>100
500	(8+9)-II-4	729	24	-2813	0.26	0.32	-1.55	132.00	192.00	192.00	85
500	(8+9)-VI-1	-605	-30	2202	-0.22	-0.40	1.22	132.00	192.00	192.00	>100
500	(8+9)-III-2	712	26	-2833	0.25	0.34	-1.56	132.00	192.00	192.00	84
500	(8+9)-VI-2	1111	40	-4339	0.40	0.54	-2.39	132.00	192.00	192.00	55
500	(8+9)-III-4	-268	-17	1109	-0.10	-0.23	0.61	132.00	192.00	192.00	>100
500	(8+9)-VI-3	-1074	-50	4073	-0.38	-0.66	2.25	132.00	192.00	192.00	66
500	(8+9)-IV-2	843	32	-3153	0.30	0.42	-1.74	132.00	192.00	192.00	74
500	(8+9)-VI-4	642	21	-2469	0.23	0.28	-1.36	132.00	192.00	192.00	97
500	(8+9)-II-1	-692	-33	2546	-0.25	-0.45	1.41	132.00	192.00	192.00	>100

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
500	(8+9)-VII-1	598	19	-2522	0.21	0.25	-1.39	132.00	192.00	192.00	98
500	(8+9)-V-2	1059	38	-4232	0.38	0.51	-2.34	132.00	192.00	192.00	57
500	(8+9)-VII-2	1005	37	-3979	0.36	0.49	-2.20	132.00	192.00	192.00	60
500	(8+9)-III-1	305	8	-1375	0.11	0.10	-0.76	132.00	192.00	192.00	>100
500	(8+9)-VII-3	-968	-46	3713	-0.34	-0.62	2.05	132.00	192.00	192.00	72
500	(8+9)-I-1	251	6	-1123	0.09	0.08	-0.62	132.00	192.00	192.00	>100
500	(8+9)-VII-4	-561	-28	2255	-0.20	-0.38	1.24	132.00	192.00	192.00	>100
500	(8+9)-III-3	-675	-35	2566	-0.24	-0.47	1.42	132.00	192.00	192.00	>100
500	(8+9)-IV-3	-806	-41	2887	-0.29	-0.55	1.59	132.00	192.00	192.00	90
500	(8+9)-II-3	-986	-46	3729	-0.35	-0.62	2.06	132.00	192.00	192.00	72
500	(8+9)-I-3	-729	-37	2819	-0.26	-0.49	1.56	132.00	192.00	192.00	94
500	(8+9)-VIII-2	931	35	-3497	0.33	0.47	-1.93	132.00	192.00	192.00	67
500	(8+9)-VIII-3	-894	-44	3231	-0.32	-0.59	1.78	132.00	192.00	192.00	81
500	(8+9)-I-4	-214	-16	856	-0.08	-0.21	0.47	132.00	192.00	192.00	>100
Verifiche nella direzione secondaria											
0	1	-1371	-3	62	-5.66	-0.70	3.06	79.20	115.20	115.20	29
0	2	-2754	-7	115	-11.38	-1.73	5.71	118.80	172.80	172.80	21
0	3	-2754	-7	115	-11.38	-1.73	5.71	118.80	172.80	172.80	21
0	4	-1371	-3	62	-5.66	-0.70	3.06	105.60	153.60	153.60	39
0	5	-1371	-3	62	-5.66	-0.70	3.06	105.60	153.60	153.60	39
0	6	-1371	-3	62	-5.66	-0.70	3.06	105.60	153.60	153.60	39
0	7	-1371	-3	62	-5.66	-0.70	3.06	105.60	153.60	153.60	39
0	(8+9)-VIII-4	-1464	233	884	-6.05	55.14	43.83	132.00	192.00	192.00	1.9
0	(8+9)-IV-2	-4988	240	1366	-20.61	56.69	67.76	132.00	192.00	192.00	1.5
0	(8+9)-V-1	-6899	6	567	-28.51	1.50	28.11	132.00	192.00	192.00	5.7
0	(8+9)-I-2	-6750	12	1129	-27.89	2.74	55.96	132.00	192.00	192.00	3.1
0	(8+9)-V-2	-9221	21	1575	-38.10	4.87	78.08	132.00	192.00	192.00	2.1
0	(8+9)-I-4	2525	-1	-34	10.43	-0.30	-1.70	132.00	192.00	192.00	11
0	(8+9)-V-3	7317	-24	-1488	30.24	-5.79	-73.78	132.00	192.00	192.00	1.6
0	(8+9)-II-2	-6212	24	1897	-25.67	5.60	94.07	132.00	192.00	192.00	1.9
0	(8+9)-V-4	4996	-10	-480	20.64	-2.43	-23.81	132.00	192.00	192.00	3.4
0	(8+9)-II-4	-3430	20	1548	-14.17	4.69	76.77	132.00	192.00	192.00	2.3
0	(8+9)-VI-1	785	-21	-1328	3.24	-4.97	-65.84	132.00	192.00	192.00	2.5
0	(8+9)-III-2	-6383	76	969	-26.38	18.06	48.07	132.00	192.00	192.00	2.8
0	(8+9)-VI-2	-6954	26	2031	-28.73	6.24	100.70	132.00	192.00	192.00	1.7
0	(8+9)-III-4	2893	64	-193	11.95	15.03	-9.59	132.00	192.00	192.00	4.6
0	(8+9)-VI-3	5050	-30	-1944	20.87	-7.16	-96.41	132.00	192.00	192.00	1.4
0	(8+9)-VI-4	-2689	17	1414	-11.11	4.05	70.14	132.00	192.00	192.00	2.6
0	(8+9)-IV-4	-2205	236	1018	-9.11	55.78	50.46	132.00	192.00	192.00	1.8
0	(8+9)-VII-1	-7267	-58	726	-30.03	-13.82	36.01	132.00	192.00	192.00	3.5
0	(8+9)-II-1	1526	-24	-1462	6.31	-5.61	-72.47	132.00	192.00	192.00	2.2
0	(8+9)-VII-2	-8853	85	1415	-36.58	20.19	70.18	132.00	192.00	192.00	2.0
0	(8+9)-III-1	-4796	-67	280	-19.82	-15.95	13.89	132.00	192.00	192.00	6.0
0	(8+9)-VII-3	6950	-89	-1329	28.72	-21.11	-65.88	132.00	192.00	192.00	1.5
0	(8+9)-IV-1	302	-240	-931	1.25	-56.70	-46.16	132.00	192.00	192.00	1.8
0	(8+9)-VII-4	5363	55	-639	22.16	12.90	-31.71	132.00	192.00	192.00	2.5
0	(8+9)-I-3	4847	-15	-1042	20.03	-3.66	-51.66	132.00	192.00	192.00	2.3
0	(8+9)-III-3	4479	-80	-883	18.51	-18.99	-43.77	132.00	192.00	192.00	2.1
0	(8+9)-IV-3	3084	-244	-1280	12.74	-57.61	-63.46	132.00	192.00	192.00	1.4
0	(8+9)-II-3	4309	-28	-1810	17.80	-6.52	-89.77	132.00	192.00	192.00	1.6
0	(8+9)-VIII-1	-440	-237	-797	-1.82	-56.06	-39.53	132.00	192.00	192.00	2.0
0	(8+9)-VIII-2	-5729	242	1500	-23.67	57.32	74.39	132.00	192.00	192.00	1.4
0	(8+9)-VIII-3	3825	-246	-1414	15.81	-58.25	-70.10	132.00	192.00	192.00	1.3
1935	(8+9)-I-1	-470	1	-207	-1.94	0.27	-10.24	132.00	192.00	192.00	18

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Ty kg	τ_d kg/cmq	fvd kg/cmq	RS	Cs
0	(8+9)-VIII-4	-51	0.01	6.40	Si	>100
0	(8+9)-IV-1	111	0.03	6.40	Si	>100
0	(8+9)-VI-3	168	0.04	6.40	Si	>100
0	(8+9)-II-2	-88	0.02	6.40	Si	>100
0	(8+9)-IV-2	-128	0.03	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
0	(8+9)-III-3	108	0.03	6.40	Si	>100
0	(8+9)-VIII-2	-168	0.04	6.40	Si	>100
0	(8+9)-VII-2	-221	0.06	6.40	Si	>100
0	(8+9)-VII-4	170	0.04	6.40	Si	>100
0	(8+9)-VII-1	-149	0.04	6.40	Si	>100
0	(8+9)-I-2	-82	0.02	6.40	Si	>100
0	(8+9)-I-4	42	0.01	6.40	Si	>100
0	(8+9)-IV-3	148	0.04	6.40	Si	>100
0	(8+9)-II-2	-108	0.03	6.40	Si	>100
0	(8+9)-IV-4	-91	0.02	6.40	Si	>100
0	(8+9)-II-4	-71	0.02	6.40	Si	>100
0	(8+9)-V-1	-155	0.04	6.40	Si	>100
0	(8+9)-VIII-3	188	0.05	6.40	Si	>100
0	(8+9)-V-2	-215	0.06	6.40	Si	>100
0	(8+9)-I-1	-22	0.01	6.40	Si	>100
0	(8+9)-V-3	235	0.06	6.40	Si	>100
0	(8+9)-VII-3	241	0.06	6.40	Si	>100
0	(8+9)-VI-2	-148	0.04	6.40	Si	>100
0	(8+9)-VIII-1	71	0.02	6.40	Si	>100
0	(8+9)-I-3	102	0.03	6.40	Si	>100
0	(8+9)-II-3	128	0.03	6.40	Si	>100
0	(8+9)-V-4	176	0.05	6.40	Si	>100
250	(8+9)-III-1	-20	0.01	6.40	Si	>100
250	(8+9)-VI-4	-61	0.02	6.40	Si	>100
500	1	19	0.00	3.84	Si	>100
500	2	41	0.01	5.76	Si	>100
500	3	41	0.01	5.76	Si	>100
500	4	19	0.00	5.12	Si	>100
500	5	19	0.00	5.12	Si	>100
500	6	19	0.00	5.12	Si	>100
500	7	19	0.00	5.12	Si	>100
500	(8+9)-II-1	92	0.02	6.40	Si	>100
500	(8+9)-III-4	45	0.01	6.40	Si	>100
500	(8+9)-VI-1	83	0.02	6.40	Si	>100
Verifiche nella direzione secondaria						
0	(8+9)-VIII-4	-24	0.09	6.40	Si	70
0	(8+9)-III-3	44	0.17	6.40	Si	38
0	(8+9)-IV-2	-44	0.17	6.40	Si	38
0	(8+9)-III-4	19	0.07	6.40	Si	87
0	(8+9)-VIII-2	-48	0.18	6.40	Si	35
0	(8+9)-IV-1	39	0.15	6.40	Si	43
0	(8+9)-VII-4	33	0.13	6.40	Si	50
0	(8+9)-V-3	62	0.24	6.40	Si	27
0	(8+9)-VI-2	-60	0.23	6.40	Si	28
0	(8+9)-VIII-3	59	0.23	6.40	Si	28
0	(8+9)-I-3	48	0.18	6.40	Si	35
0	(8+9)-VIII-1	35	0.13	6.40	Si	48
0	(8+9)-II-1	51	0.20	6.40	Si	33
0	(8+9)-VII-3	58	0.22	6.40	Si	29
0	(8+9)-II-3	67	0.26	6.40	Si	25
0	(8+9)-V-4	30	0.11	6.40	Si	56
0	(8+9)-VI-3	71	0.27	6.40	Si	24
0	(8+9)-I-4	16	0.06	6.40	Si	>100
0	(8+9)-II-2	-56	0.21	6.40	Si	30
0	(8+9)-II-4	-40	0.15	6.40	Si	42
0	(8+9)-VI-4	-36	0.14	6.40	Si	47
0	(8+9)-IV-3	55	0.21	6.40	Si	31
0	(8+9)-IV-4	-28	0.11	6.40	Si	60
0	(8+9)-VI-1	47	0.18	6.40	Si	36
1935	(8+9)-VII-2	54	0.21	6.40	Si	31
1935	(8+9)-I-1	24	0.09	6.40	Si	71
1935	(8+9)-V-2	54	0.21	6.40	Si	31
1935	(8+9)-V-1	40	0.15	6.40	Si	42
1935	(8+9)-III-2	38	0.14	6.40	Si	45

X	Comb.	Ty	τ_d	fvd	RS	Cs
1935	(8+9)-III-1	24	0.09	6.40	Si	69
1935	(8+9)-I-2	38	0.15	6.40	Si	44
1935	(8+9)-VII-1	41	0.15	6.40	Si	41
3870	1	14	0.06	3.84	Si	70
3870	2	30	0.11	5.76	Si	51
3870	3	30	0.11	5.76	Si	51
3870	4	14	0.06	5.12	Si	93
3870	5	14	0.06	5.12	Si	93
3870	6	14	0.06	5.12	Si	93
3870	7	14	0.06	5.12	Si	93

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	(8+9)-VII-1	7320	3.91	32.00	8.2	0.95	20.00	21	V	8.2
0	(8+9)-VII-4	-6489	-3.46	32.00	9.2	-0.84	20.00	24	V	9.2
250	(8+9)-VIII-4	6896	3.68	32.00	8.7	0.89	20.00	22	V	8.7
250	(8+9)-IV-1	-6696	-3.57	32.00	9.0	-0.87	20.00	23	V	9.0
250	(8+9)-VII-2	12209	6.52	32.00	4.9	1.58	20.00	13	V	4.9
250	(8+9)-III-4	-3125	-1.67	32.00	19	-0.40	20.00	50	V	19
250	(8+9)-IV-3	-10505	-5.61	32.00	5.7	-1.36	20.00	15	V	5.7
250	(8+9)-VIII-1	-5905	-3.15	32.00	10	-0.76	20.00	26	V	10
250	(8+9)-VIII-2	12287	6.56	32.00	4.9	1.59	20.00	13	V	4.9
250	(8+9)-IV-2	11496	6.14	32.00	5.2	1.49	20.00	13	V	5.2
250	(8+9)-I-2	9484	5.06	32.00	6.3	1.23	20.00	16	V	6.3
250	(8+9)-I-4	-3215	-1.72	32.00	19	-0.42	20.00	48	V	19
250	(8+9)-IV-4	7687	4.10	32.00	7.8	0.99	20.00	20	V	7.8
250	(8+9)-II-2	11197	5.98	32.00	5.4	1.45	20.00	14	V	5.4
250	(8+9)-V-1	6841	3.65	32.00	8.8	0.88	20.00	23	V	8.8
250	(8+9)-II-4	7388	3.94	32.00	8.1	0.95	20.00	21	V	8.1
250	(8+9)-V-2	12119	6.47	32.00	4.9	1.57	20.00	13	V	4.9
250	(8+9)-III-2	9574	5.11	32.00	6.3	1.24	20.00	16	V	6.3
250	(8+9)-V-3	-11128	-5.94	32.00	5.4	-1.44	20.00	14	V	5.4
250	(8+9)-VIII-3	-11296	-6.03	32.00	5.3	-1.46	20.00	14	V	5.3
250	(8+9)-V-4	-5850	-3.12	32.00	10	-0.76	20.00	26	V	10
250	(8+9)-I-3	-8493	-4.53	32.00	7.1	-1.10	20.00	18	V	7.1
250	(8+9)-VI-1	-5606	-2.99	32.00	11	-0.72	20.00	28	V	11
250	(8+9)-II-3	-10206	-5.45	32.00	5.9	-1.32	20.00	15	V	5.9
250	(8+9)-VI-2	11988	6.40	32.00	5.0	1.55	20.00	13	V	5.0
250	(8+9)-III-3	-8583	-4.58	32.00	7.0	-1.11	20.00	18	V	7.0
250	(8+9)-II-1	-6397	-3.42	32.00	9.4	-0.83	20.00	24	V	9.4
250	(8+9)-III-1	4116	2.20	32.00	15	0.53	20.00	38	V	15
250	(8+9)-I-1	4206	2.25	32.00	14	0.54	20.00	37	V	14
250	(8+9)-VI-3	-10997	-5.87	32.00	5.5	-1.42	20.00	14	V	5.5
250	(8+9)-VI-4	6597	3.52	32.00	9.1	0.85	20.00	23	V	9.1
250	(8+9)-VII-3	-11218	-5.99	32.00	5.3	-1.45	20.00	14	V	5.3
500	1	793	0.42	19.20	45	0.10	12.00	>100	V	45
500	2	1582	0.84	28.80	34	0.20	18.00	88	V	34
500	3	1582	0.84	28.80	34	0.20	18.00	88	V	34
500	4	793	0.42	25.60	60	0.10	16.00	>100	V	60
500	5	793	0.42	25.60	60	0.10	16.00	>100	V	60
500	6	793	0.42	25.60	60	0.10	16.00	>100	V	60
500	7	793	0.42	25.60	60	0.10	16.00	>100	V	60
Verifiche nella direzione secondaria										
1935	1	128	0.53	19.20	36	0.13	12.00	94	V	36
1935	2	260	1.08	28.80	27	0.26	18.00	69	V	27
1935	3	260	1.08	28.80	27	0.26	18.00	69	V	27
1935	4	128	0.53	25.60	49	0.13	16.00	>100	V	49
1935	5	128	0.53	25.60	49	0.13	16.00	>100	V	49
1935	6	128	0.53	25.60	49	0.13	16.00	>100	V	49
1935	7	128	0.53	25.60	49	0.13	16.00	>100	V	49
1935	(8+9)-VIII-4	954	3.94	32.00	8.1	0.95	20.00	21	V	8.1
1935	(8+9)-IV-2	1807	7.47	32.00	4.3	1.81	20.00	11	V	4.3

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
1935	(8+9)-V-1	1324	5.47	32.00	5.8	1.32	20.00	15	V	5.8
1935	(8+9)-I-2	1695	7.01	32.00	4.6	1.70	20.00	12	V	4.6
1935	(8+9)-V-2	2364	9.77	32.00	3.3	2.36	20.00	8.5	V	3.3
1935	(8+9)-I-4	-479	-1.98	32.00	16	-0.48	20.00	42	V	16
1935	(8+9)-V-3	-2187	-9.04	32.00	3.5	-2.19	20.00	9.1	V	3.5
1935	(8+9)-II-2	2147	8.87	32.00	3.6	2.15	20.00	9.3	V	3.6
1935	(8+9)-V-4	-1147	-4.74	32.00	6.7	-1.15	20.00	17	V	6.7
1935	(8+9)-II-4	1495	6.18	32.00	5.2	1.50	20.00	13	V	5.2
1935	(8+9)-VI-1	-1118	-4.62	32.00	6.9	-1.12	20.00	18	V	6.9
1935	(8+9)-III-2	1593	6.58	32.00	4.9	1.59	20.00	13	V	4.9
1935	(8+9)-VI-2	2348	9.70	32.00	3.3	2.35	20.00	8.5	V	3.3
1935	(8+9)-III-4	-581	-2.40	32.00	13	-0.58	20.00	34	V	13
1935	(8+9)-VI-3	-2171	-8.97	32.00	3.6	-2.17	20.00	9.2	V	3.6
1935	(8+9)-I-1	656	2.71	32.00	12	0.66	20.00	31	V	12
1935	(8+9)-VI-4	1295	5.35	32.00	6.0	1.29	20.00	15	V	6.0
1935	(8+9)-IV-4	1155	4.77	32.00	6.7	1.15	20.00	17	V	6.7
1935	(8+9)-VII-1	1426	5.89	32.00	5.4	1.43	20.00	14	V	5.4
1935	(8+9)-II-1	-1319	-5.45	32.00	5.9	-1.32	20.00	15	V	5.9
1935	(8+9)-VII-2	2262	9.35	32.00	3.4	2.26	20.00	8.8	V	3.4
1935	(8+9)-III-1	758	3.13	32.00	10	0.76	20.00	26	V	10
1935	(8+9)-VII-3	-2085	-8.62	32.00	3.7	-2.09	20.00	9.6	V	3.7
1935	(8+9)-IV-1	-978	-4.04	32.00	7.9	-0.98	20.00	20	V	7.9
1935	(8+9)-VII-4	-1250	-5.16	32.00	6.2	-1.25	20.00	16	V	6.2
1935	(8+9)-III-3	-1417	-5.85	32.00	5.5	-1.42	20.00	14	V	5.5
1935	(8+9)-IV-3	-1631	-6.74	32.00	4.7	-1.63	20.00	12	V	4.7
1935	(8+9)-II-3	-1971	-8.14	32.00	3.9	-1.97	20.00	10	V	3.9
1935	(8+9)-VIII-1	-778	-3.21	32.00	10.0	-0.78	20.00	26	V	10.0
1935	(8+9)-VIII-2	2008	8.30	32.00	3.9	2.01	20.00	10.0	V	3.9
1935	(8+9)-VIII-3	-1831	-7.57	32.00	4.2	-1.83	20.00	11	V	4.2
1935	(8+9)-I-3	-1519	-6.28	32.00	5.1	-1.52	20.00	13	V	5.1

Setto 29: origine (1275.7,2680.4,193.5), direzione (0.927376,-0.374131,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	(8+9)-VIII-4	-820	-7	3376	-0.29	-0.09	1.86	132.00	192.00	192.00	98
0	(8+9)-IV-1	1042	26	-3662	0.37	0.35	-2.02	132.00	192.00	192.00	66
0	(8+9)-VII-2	-1861	-16	6978	-0.66	-0.22	3.85	132.00	192.00	192.00	47
0	(8+9)-III-3	1325	26	-4620	0.47	0.34	-2.55	132.00	192.00	192.00	54
0	(8+9)-IV-2	-1543	-16	5987	-0.55	-0.21	3.30	132.00	192.00	192.00	55
0	(8+9)-III-4	549	13	-1726	0.20	0.18	-0.95	132.00	192.00	192.00	>100
0	(8+9)-VIII-2	-1718	-18	6597	-0.61	-0.24	3.64	132.00	192.00	192.00	49
0	(8+9)-VII-3	1908	33	-6654	0.68	0.44	-3.67	132.00	192.00	192.00	38
0	(8+9)-VII-4	1133	21	-3759	0.40	0.28	-2.07	132.00	192.00	192.00	65
0	(8+9)-I-2	-1334	-11	5242	-0.47	-0.15	2.89	132.00	192.00	192.00	63
0	(8+9)-IV-3	1590	33	-5663	0.57	0.43	-3.12	132.00	192.00	192.00	44
0	(8+9)-I-4	493	11	-1428	0.18	0.15	-0.79	132.00	192.00	192.00	>100
0	(8+9)-IV-4	-995	-9	3986	-0.35	-0.12	2.20	132.00	192.00	192.00	83
0	(8+9)-II-2	-1731	-23	6979	-0.62	-0.30	3.85	132.00	192.00	192.00	46
0	(8+9)-V-1	-1029	-2	3786	-0.37	-0.02	2.09	132.00	192.00	192.00	91
0	(8+9)-II-4	-1183	-16	4978	-0.42	-0.21	2.75	132.00	192.00	192.00	65
0	(8+9)-V-2	-1918	-18	7275	-0.68	-0.25	4.01	132.00	192.00	192.00	45
0	(8+9)-III-2	-1278	-9	4944	-0.45	-0.12	2.73	132.00	192.00	192.00	67
0	(8+9)-V-3	1965	35	-6952	0.70	0.47	-3.84	132.00	192.00	192.00	36
0	(8+9)-VIII-1	867	24	-3052	0.31	0.32	-1.68	132.00	192.00	192.00	78
0	(8+9)-V-4	1076	19	-3462	0.38	0.25	-1.91	132.00	192.00	192.00	71
0	(8+9)-I-3	1381	28	-4918	0.49	0.37	-2.71	132.00	192.00	192.00	51
0	(8+9)-VI-1	1055	31	-4044	0.38	0.41	-2.23	132.00	192.00	192.00	60
0	(8+9)-II-3	1778	39	-6655	0.63	0.53	-3.67	132.00	192.00	192.00	38
0	(8+9)-VI-2	-1906	-25	7589	-0.68	-0.33	4.19	132.00	192.00	192.00	42
0	(8+9)-VIII-3	1765	35	-6273	0.63	0.46	-3.46	132.00	192.00	192.00	40
0	(8+9)-II-1	1230	33	-4654	0.44	0.44	-2.57	132.00	192.00	192.00	53
0	(8+9)-III-1	-502	4	2049	-0.18	0.05	1.13	132.00	192.00	192.00	>100

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-I-1	-446	6	1752	-0.16	0.08	0.97	132.00	192.00	192.00	>100
0	(8+9)-VI-3	1953	42	-7265	0.70	0.56	-4.01	132.00	192.00	192.00	34
0	(8+9)-VI-4	-1008	-14	4367	-0.36	-0.18	2.41	132.00	192.00	192.00	74
0	(8+9)-VII-1	-1086	-4	4083	-0.39	-0.05	2.25	132.00	192.00	192.00	83
682	1	27	28	-85	0.01	0.38	-0.05	79.20	115.20	115.20	>100
682	2	50	58	-164	0.02	0.77	-0.09	118.80	172.80	172.80	>100
682	3	50	58	-164	0.02	0.77	-0.09	118.80	172.80	172.80	>100
682	4	27	28	-85	0.01	0.38	-0.05	105.60	153.60	153.60	>100
682	5	27	28	-85	0.01	0.38	-0.05	105.60	153.60	153.60	>100
682	6	27	28	-85	0.01	0.38	-0.05	105.60	153.60	153.60	>100
682	7	27	28	-85	0.01	0.38	-0.05	105.60	153.60	153.60	>100
Verifiche nella direzione secondaria											
0	1	-371	4	56	-1.12	0.77	1.50	79.20	115.20	115.20	51
0	2	-739	7	119	-2.24	1.25	3.17	118.80	172.80	172.80	39
0	3	-739	7	119	-2.24	1.25	3.17	118.80	172.80	172.80	39
0	4	-371	4	56	-1.12	0.77	1.50	105.60	153.60	153.60	68
0	5	-371	4	56	-1.12	0.77	1.50	105.60	153.60	153.60	68
0	6	-371	4	56	-1.12	0.77	1.50	105.60	153.60	153.60	68
0	7	-371	4	56	-1.12	0.77	1.50	105.60	153.60	153.60	68
0	(8+9)-VIII-4	5942	44	634	18.00	7.66	16.89	132.00	192.00	192.00	3.8
0	(8+9)-IV-2	9020	61	1813	27.33	10.63	48.31	132.00	192.00	192.00	1.9
0	(8+9)-V-1	3212	17	1872	9.73	2.87	49.90	132.00	192.00	192.00	2.9
0	(8+9)-I-2	6528	47	2135	19.78	8.12	56.89	132.00	192.00	192.00	2.0
0	(8+9)-V-2	9090	50	2924	27.54	8.72	77.94	132.00	192.00	192.00	1.5
0	(8+9)-I-4	-1169	-7	-1006	-3.54	-1.16	-26.81	132.00	192.00	192.00	6.8
0	(8+9)-V-3	-9609	-44	-2847	-29.11	-7.61	-75.89	132.00	192.00	192.00	2.2
0	(8+9)-II-2	10692	68	2263	32.39	11.70	60.31	132.00	192.00	192.00	1.6
0	(8+9)-V-4	-3731	-10	-1795	-11.30	-1.76	-47.85	132.00	192.00	192.00	3.8
0	(8+9)-II-4	8383	51	1321	25.40	8.92	35.20	132.00	192.00	192.00	2.4
0	(8+9)-VI-1	-8133	-44	-1007	-24.64	-7.63	-26.83	132.00	192.00	192.00	5.1
0	(8+9)-III-2	6026	45	2000	18.26	7.80	53.29	132.00	192.00	192.00	2.2
0	(8+9)-VI-2	11461	69	2500	34.72	11.88	66.62	132.00	192.00	192.00	1.5
0	(8+9)-III-4	-1670	-9	-1141	-5.06	-1.48	-30.40	132.00	192.00	192.00	6.0
0	(8+9)-VI-3	-11979	-62	-2423	-36.29	-10.77	-64.57	132.00	192.00	192.00	2.3
0	(8+9)-I-1	650	13	1083	1.97	2.27	28.86	132.00	192.00	192.00	5.6
0	(8+9)-VI-4	7614	50	1084	23.07	8.74	28.88	132.00	192.00	192.00	2.7
0	(8+9)-IV-4	6711	45	870	20.33	7.84	23.20	132.00	192.00	192.00	3.2
0	(8+9)-VII-1	3714	18	2007	11.25	3.19	53.50	132.00	192.00	192.00	2.6
0	(8+9)-II-1	-8902	-45	-1244	-26.97	-7.81	-33.15	132.00	192.00	192.00	4.3
0	(8+9)-VII-2	8589	48	2789	26.02	8.40	74.34	132.00	192.00	192.00	1.6
0	(8+9)-III-1	1152	15	1218	3.49	2.59	32.46	132.00	192.00	192.00	4.8
0	(8+9)-VII-3	-9107	-42	-2712	-27.59	-7.29	-72.29	132.00	192.00	192.00	2.3
0	(8+9)-IV-1	-7230	-39	-793	-21.90	-6.74	-21.15	132.00	192.00	192.00	6.3
0	(8+9)-VII-4	-4233	-12	-1930	-12.82	-2.08	-51.45	132.00	192.00	192.00	3.5
0	(8+9)-III-3	-6545	-39	-1923	-19.83	-6.69	-51.24	132.00	192.00	192.00	3.2
0	(8+9)-IV-3	-9538	-55	-1736	-28.90	-9.52	-46.26	132.00	192.00	192.00	3.2
0	(8+9)-II-3	-11211	-61	-2186	-33.96	-10.59	-58.26	132.00	192.00	192.00	2.6
0	(8+9)-VIII-1	-6461	-38	-557	-19.57	-6.56	-14.84	132.00	192.00	192.00	8.2
0	(8+9)-VIII-2	9788	62	2049	29.65	10.81	54.62	132.00	192.00	192.00	1.8
0	(8+9)-VIII-3	-10307	-56	-1972	-31.23	-9.70	-52.57	132.00	192.00	192.00	2.9
0	(8+9)-I-3	-7047	-40	-2058	-21.35	-7.01	-54.84	132.00	192.00	192.00	3.0

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
0	(8+9)-II-4	-42	0.01	6.40	Si	>100
0	(8+9)-VI-4	-36	0.01	6.40	Si	>100
0	(8+9)-VI-3	94	0.02	6.40	Si	>100
0	(8+9)-II-3	88	0.02	6.40	Si	>100
0	(8+9)-II-2	-56	0.01	6.40	Si	>100
0	(8+9)-II-1	74	0.02	6.40	Si	>100
0	(8+9)-VI-1	68	0.02	6.40	Si	>100
0	(8+9)-VI-2	-62	0.02	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
341	1	25	0.01	3.84	Si	>100
341	2	51	0.01	5.76	Si	>100
341	3	51	0.01	5.76	Si	>100
341	4	25	0.01	5.12	Si	>100
341	5	25	0.01	5.12	Si	>100
341	6	25	0.01	5.12	Si	>100
341	7	25	0.01	5.12	Si	>100
341	(8+9)-IV-1	43	0.01	6.40	Si	>100
341	(8+9)-IV-3	64	0.02	6.40	Si	>100
341	(8+9)-VIII-3	72	0.02	6.40	Si	>100
341	(8+9)-VIII-2	-38	0.01	6.40	Si	>100
341	(8+9)-VIII-1	35	0.01	6.40	Si	>100
341	(8+9)-IV-2	-30	0.01	6.40	Si	>100
682	(8+9)-VIII-4	52	0.01	6.40	Si	>100
682	(8+9)-I-4	91	0.02	6.40	Si	>100
682	(8+9)-III-2	-63	0.02	6.40	Si	>100
682	(8+9)-VII-1	-94	0.02	6.40	Si	>100
682	(8+9)-V-1	-87	0.02	6.40	Si	>100
682	(8+9)-VII-2	-93	0.02	6.40	Si	>100
682	(8+9)-V-3	134	0.03	6.40	Si	>100
682	(8+9)-VII-3	127	0.03	6.40	Si	>100
682	(8+9)-IV-4	43	0.01	6.40	Si	>100
682	(8+9)-VII-4	129	0.03	6.40	Si	>100
682	(8+9)-V-2	-100	0.03	6.40	Si	>100
682	(8+9)-V-4	122	0.03	6.40	Si	>100
682	(8+9)-I-3	104	0.03	6.40	Si	>100
682	(8+9)-I-1	-57	0.01	6.40	Si	>100
682	(8+9)-III-1	-64	0.02	6.40	Si	>100
682	(8+9)-III-4	98	0.03	6.40	Si	>100
682	(8+9)-III-3	97	0.03	6.40	Si	>100
682	(8+9)-I-2	-69	0.02	6.40	Si	>100
Verifiche nella direzione secondaria						
0	1	-9	0.02	3.84	Si	>100
0	2	-15	0.04	5.76	Si	>100
0	3	-15	0.04	5.76	Si	>100
0	4	-9	0.02	5.12	Si	>100
0	5	-9	0.02	5.12	Si	>100
0	6	-9	0.02	5.12	Si	>100
0	7	-9	0.02	5.12	Si	>100
0	(8+9)-VIII-4	-77	0.22	6.40	Si	30
0	(8+9)-IV-2	-111	0.31	6.40	Si	21
0	(8+9)-V-1	-37	0.10	6.40	Si	62
0	(8+9)-I-2	-87	0.24	6.40	Si	26
0	(8+9)-V-2	-103	0.29	6.40	Si	22
0	(8+9)-V-3	90	0.25	6.40	Si	25
0	(8+9)-II-2	-130	0.36	6.40	Si	18
0	(8+9)-VIII-3	103	0.29	6.40	Si	22
0	(8+9)-II-4	-101	0.28	6.40	Si	23
0	(8+9)-VI-1	84	0.24	6.40	Si	27
0	(8+9)-III-2	-81	0.23	6.40	Si	28
0	(8+9)-VI-2	-135	0.38	6.40	Si	17
0	(8+9)-III-4	14	0.04	6.40	Si	>100
0	(8+9)-VI-3	122	0.34	6.40	Si	19
0	(8+9)-I-1	-21	0.06	6.40	Si	>100
0	(8+9)-VI-4	-97	0.27	6.40	Si	24
0	(8+9)-IV-4	-82	0.23	6.40	Si	28
0	(8+9)-VII-1	-43	0.12	6.40	Si	54
0	(8+9)-II-1	89	0.25	6.40	Si	26
0	(8+9)-VII-2	-97	0.27	6.40	Si	24
0	(8+9)-III-1	-27	0.08	6.40	Si	85
0	(8+9)-VII-3	84	0.24	6.40	Si	27
0	(8+9)-IV-1	70	0.19	6.40	Si	33
0	(8+9)-I-3	74	0.21	6.40	Si	31
0	(8+9)-II-3	117	0.33	6.40	Si	19

X	Comb.	Ty	τ_d	fvd	RS	Cs
0	(8+9)-III-3	69	0.19	6.40	Si	33
0	(8+9)-IV-3	98	0.27	6.40	Si	23
0	(8+9)-VII-4	30	0.08	6.40	Si	76
0	(8+9)-VIII-1	65	0.18	6.40	Si	35
0	(8+9)-VIII-2	-115	0.32	6.40	Si	20
3870	(8+9)-I-4	15	0.04	6.40	Si	>100
3870	(8+9)-V-4	29	0.08	6.40	Si	80

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	(8+9)-VIII-4	6900	3.68	32.00	8.7	0.89	20.00	22	V	8.7
0	(8+9)-IV-1	-7692	-4.11	32.00	7.8	-0.99	20.00	20	V	7.8
0	(8+9)-IV-3	-11934	-6.37	32.00	5.0	-1.54	20.00	13	V	5.0
0	(8+9)-II-1	-8692	-4.64	32.00	6.9	-1.12	20.00	18	V	6.9
0	(8+9)-IV-2	12334	6.58	32.00	4.9	1.59	20.00	13	V	4.9
0	(8+9)-VIII-2	13527	7.22	32.00	4.4	1.75	20.00	11	V	4.4
0	(8+9)-V-4	-7541	-4.03	32.00	7.9	-0.97	20.00	21	V	7.9
0	(8+9)-VII-4	-7841	-4.19	32.00	7.6	-1.01	20.00	20	V	7.6
0	(8+9)-IV-4	8093	4.32	32.00	7.4	1.05	20.00	19	V	7.4
0	(8+9)-VII-3	-13849	-7.39	32.00	4.3	-1.79	20.00	11	V	4.3
0	(8+9)-VII-2	14250	7.61	32.00	4.2	1.84	20.00	11	V	4.2
0	(8+9)-VI-3	-14126	-7.54	32.00	4.2	-1.83	20.00	11	V	4.2
0	(8+9)-VIII-1	-6499	-3.47	32.00	9.2	-0.84	20.00	24	V	9.2
0	(8+9)-VII-1	8242	4.40	32.00	7.3	1.06	20.00	19	V	7.3
0	(8+9)-VIII-3	-13127	-7.01	32.00	4.6	-1.70	20.00	12	V	4.6
0	(8+9)-V-3	-14149	-7.55	32.00	4.2	-1.83	20.00	11	V	4.2
0	(8+9)-V-2	14550	7.77	32.00	4.1	1.88	20.00	11	V	4.1
0	(8+9)-V-1	7942	4.24	32.00	7.5	1.03	20.00	19	V	7.5
341	(8+9)-VI-2	14595	7.79	32.00	4.1	1.89	20.00	11	V	4.1
341	(8+9)-II-4	9217	4.92	32.00	6.5	1.19	20.00	17	V	6.5
682	1	622	0.33	19.20	58	0.08	12.00	>100	V	58
682	2	1127	0.60	28.80	48	0.15	18.00	>100	V	48
682	3	1127	0.60	28.80	48	0.15	18.00	>100	V	48
682	4	622	0.33	25.60	77	0.08	16.00	>100	V	77
682	5	622	0.33	25.60	77	0.08	16.00	>100	V	77
682	6	622	0.33	25.60	77	0.08	16.00	>100	V	77
682	7	622	0.33	25.60	77	0.08	16.00	>100	V	77
682	(8+9)-VI-4	8997	4.80	32.00	6.7	1.16	20.00	17	V	6.7
682	(8+9)-I-3	-13404	-7.16	32.00	4.5	-1.73	20.00	12	V	4.5
682	(8+9)-III-3	-12135	-6.48	32.00	4.9	-1.57	20.00	13	V	4.9
682	(8+9)-VI-1	-8116	-4.33	32.00	7.4	-1.05	20.00	19	V	7.4
682	(8+9)-II-2	14869	7.94	32.00	4.0	1.92	20.00	10	V	4.0
682	(8+9)-I-2	14285	7.63	32.00	4.2	1.85	20.00	11	V	4.2
682	(8+9)-I-1	7510	4.01	32.00	8.0	0.97	20.00	21	V	8.0
682	(8+9)-III-4	-7898	-4.22	32.00	7.6	-1.02	20.00	20	V	7.6
682	(8+9)-II-3	-13989	-7.47	32.00	4.3	-1.81	20.00	11	V	4.3
682	(8+9)-III-1	8779	4.69	32.00	6.8	1.13	20.00	18	V	6.8
682	(8+9)-III-2	13016	6.95	32.00	4.6	1.68	20.00	12	V	4.6
682	(8+9)-I-4	-6629	-3.54	32.00	9.0	-0.86	20.00	23	V	9.0
Verifiche nella direzione secondaria										
0	(8+9)-VIII-4	1588	4.81	32.00	6.7	1.16	20.00	17	V	6.7
0	(8+9)-V-2	3583	10.85	32.00	2.9	2.63	20.00	7.6	V	2.9
0	(8+9)-II-2	3458	10.48	32.00	3.1	2.54	20.00	7.9	V	3.1
0	(8+9)-IV-2	2874	8.71	32.00	3.7	2.11	20.00	9.5	V	3.7
0	(8+9)-II-3	-3289	-9.96	32.00	3.2	-2.41	20.00	8.3	V	3.2
0	(8+9)-VIII-2	3169	9.60	32.00	3.3	2.32	20.00	8.6	V	3.3
0	(8+9)-II-4	2466	7.47	32.00	4.3	1.81	20.00	11	V	4.3
0	(8+9)-VII-3	-3239	-9.81	32.00	3.3	-2.37	20.00	8.4	V	3.3
0	(8+9)-VI-1	-2003	-6.07	32.00	5.3	-1.47	20.00	14	V	5.3
0	(8+9)-VI-3	-3584	-10.86	32.00	2.9	-2.63	20.00	7.6	V	2.9
0	(8+9)-III-2	2426	7.35	32.00	4.4	1.78	20.00	11	V	4.4
0	(8+9)-I-3	-2432	-7.37	32.00	4.3	-1.78	20.00	11	V	4.3

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
0	(8+9)-III-3	-2257	-6.84	32.00	4.7	-1.65	20.00	12	V	4.7
0	(8+9)-II-1	-2297	-6.96	32.00	4.6	-1.68	20.00	12	V	4.6
0	(8+9)-V-3	-3414	-10.34	32.00	3.1	-2.50	20.00	8.0	V	3.1
0	(8+9)-VIII-1	-1419	-4.30	32.00	7.4	-1.04	20.00	19	V	7.4
0	(8+9)-IV-1	-1713	-5.19	32.00	6.2	-1.26	20.00	16	V	6.2
0	(8+9)-VIII-3	-3000	-9.09	32.00	3.5	-2.20	20.00	9.1	V	3.5
0	(8+9)-VI-4	2172	6.58	32.00	4.9	1.59	20.00	13	V	4.9
0	(8+9)-VI-2	3753	11.37	32.00	2.8	2.75	20.00	7.3	V	2.8
0	(8+9)-I-2	2601	7.88	32.00	4.1	1.91	20.00	10	V	4.1
0	(8+9)-IV-3	-2705	-8.20	32.00	3.9	-1.98	20.00	10	V	3.9
0	(8+9)-IV-4	1882	5.70	32.00	5.6	1.38	20.00	14	V	5.6
1935	1	123	0.37	19.20	51	0.09	12.00	>100	V	51
1935	2	237	0.72	28.80	40	0.17	18.00	>100	V	40
1935	3	237	0.72	28.80	40	0.17	18.00	>100	V	40
1935	4	123	0.37	25.60	69	0.09	16.00	>100	V	69
1935	5	123	0.37	25.60	69	0.09	16.00	>100	V	69
1935	6	123	0.37	25.60	69	0.09	16.00	>100	V	69
1935	7	123	0.37	25.60	69	0.09	16.00	>100	V	69
1935	(8+9)-VII-1	2052	6.22	32.00	5.1	1.50	20.00	13	V	5.1
1935	(8+9)-I-1	889	2.69	32.00	12	0.65	20.00	31	V	12
1935	(8+9)-VII-2	3408	10.33	32.00	3.1	2.50	20.00	8.0	V	3.1
1935	(8+9)-I-4	-717	-2.17	32.00	15	-0.53	20.00	38	V	15
1935	(8+9)-VII-4	-1880	-5.69	32.00	5.6	-1.38	20.00	15	V	5.6
1935	(8+9)-III-1	1062	3.22	32.00	9.9	0.78	20.00	26	V	9.9
1935	(8+9)-V-4	-1707	-5.17	32.00	6.2	-1.25	20.00	16	V	6.2
1935	(8+9)-III-4	-890	-2.69	32.00	12	-0.65	20.00	31	V	12
1935	(8+9)-V-1	1879	5.69	32.00	5.6	1.38	20.00	15	V	5.6

Setto 30: origine (1164.4,2725.3,328.5), direzione (0.927376,-0.374131,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	(8+9)-III-2	1516	29	883	1.78	1.27	5.33	132.00	192.00	192.00	21
0	(8+9)-I-2	1621	31	943	1.91	1.37	5.69	132.00	192.00	192.00	20
0	(8+9)-VIII-4	940	17	554	1.11	0.74	3.34	132.00	192.00	192.00	34
0	(8+9)-V-1	1209	19	709	1.42	0.86	4.28	132.00	192.00	192.00	27
0	(8+9)-VII-2	2148	41	1250	2.53	1.82	7.55	132.00	192.00	192.00	15
0	(8+9)-IV-4	1129	20	664	1.33	0.90	4.01	132.00	192.00	192.00	28
0	(8+9)-VI-4	1289	24	753	1.52	1.07	4.54	132.00	192.00	192.00	25
0	(8+9)-IV-2	1757	35	1024	2.07	1.53	6.18	132.00	192.00	192.00	18
0	(8+9)-V-2	2252	43	1310	2.65	1.92	7.91	132.00	192.00	192.00	14
0	(8+9)-II-2	2106	42	1223	2.48	1.87	7.38	132.00	192.00	192.00	15
0	(8+9)-VI-2	2295	46	1333	2.70	2.03	8.05	132.00	192.00	192.00	14
0	(8+9)-I-1	578	7	342	0.68	0.32	2.07	132.00	192.00	192.00	57
0	(8+9)-VII-1	1314	22	769	1.55	0.96	4.64	132.00	192.00	192.00	24
0	(8+9)-VIII-2	1946	38	1134	2.29	1.70	6.85	132.00	192.00	192.00	16
0	(8+9)-II-4	1478	28	863	1.74	1.23	5.21	132.00	192.00	192.00	21
0	(8+9)-III-1	682	9	402	0.80	0.42	2.43	132.00	192.00	192.00	48
1200	1	-81	13	-57	-0.10	0.57	-0.35	79.20	115.20	115.20	>100
1200	2	-167	27	-116	-0.20	1.18	-0.70	118.80	172.80	172.80	92
1200	3	-167	27	-116	-0.20	1.18	-0.70	118.80	172.80	172.80	92
1200	4	-81	13	-57	-0.10	0.57	-0.35	105.60	153.60	153.60	>100
1200	5	-81	13	-57	-0.10	0.57	-0.35	105.60	153.60	153.60	>100
1200	6	-81	13	-57	-0.10	0.57	-0.35	105.60	153.60	153.60	>100
1200	7	-81	13	-57	-0.10	0.57	-0.35	105.60	153.60	153.60	>100
1200	(8+9)-IV-1	1811	22	839	2.13	0.96	5.07	132.00	192.00	192.00	21
1200	(8+9)-III-3	2485	28	1186	2.93	1.26	7.16	132.00	192.00	192.00	15
1200	(8+9)-II-1	2411	25	1160	2.84	1.11	7.00	132.00	192.00	192.00	16
1200	(8+9)-I-3	2665	29	1282	3.14	1.30	7.74	132.00	192.00	192.00	14
1200	(8+9)-II-3	3502	34	1689	4.12	1.49	10.20	132.00	192.00	192.00	11
1200	(8+9)-V-4	1952	25	933	2.30	1.09	5.63	132.00	192.00	192.00	19
1200	(8+9)-VII-3	3579	36	1715	4.21	1.59	10.36	132.00	192.00	192.00	11
1200	(8+9)-I-4	858	17	404	1.01	0.76	2.44	132.00	192.00	192.00	41

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
1200	(8+9)-VII-4	2132	26	1029	2.51	1.14	6.21	132.00	192.00	192.00	17
1200	(8+9)-VI-1	2083	23	1001	2.45	1.01	6.04	132.00	192.00	192.00	18
1200	(8+9)-VI-3	3830	36	1848	4.51	1.59	11.16	132.00	192.00	192.00	9.9
1200	(8+9)-V-3	3759	37	1811	4.43	1.64	10.94	132.00	192.00	192.00	10
1200	(8+9)-VIII-1	1482	19	680	1.75	0.86	4.11	132.00	192.00	192.00	26
1200	(8+9)-III-4	1038	18	500	1.22	0.80	3.02	132.00	192.00	192.00	34
1200	(8+9)-VIII-3	3229	33	1527	3.80	1.44	9.22	132.00	192.00	192.00	12
1200	(8+9)-IV-3	2901	30	1369	3.42	1.34	8.26	132.00	192.00	192.00	13
Verifiche nella direzione secondaria											
0	(8+9)-VIII-4	-688	-13	2595	-1.18	-1.25	22.34	132.00	192.00	192.00	8.1
0	(8+9)-VII-2	-1181	-0	6205	-2.03	-0.04	53.42	132.00	192.00	192.00	3.6
0	(8+9)-III-3	-231	4	-4323	-0.40	0.41	-37.22	132.00	192.00	192.00	5.1
0	(8+9)-IV-2	-931	-12	5019	-1.60	-1.15	43.20	132.00	192.00	192.00	4.3
0	(8+9)-III-4	-370	-4	-1875	-0.64	-0.38	-16.14	132.00	192.00	192.00	12
0	(8+9)-VIII-2	-990	-11	5579	-1.71	-1.12	48.03	132.00	192.00	192.00	3.9
0	(8+9)-IV-1	-468	15	-3142	-0.81	1.48	-27.05	132.00	192.00	192.00	6.7
0	(8+9)-VII-4	-173	-5	-3744	-0.30	-0.49	-32.23	132.00	192.00	192.00	5.9
0	(8+9)-I-1	-841	7	1578	-1.45	0.68	13.59	132.00	192.00	192.00	13
0	(8+9)-IV-3	-284	14	-5006	-0.49	1.41	-43.09	132.00	192.00	192.00	4.3
0	(8+9)-I-3	-226	5	-4632	-0.39	0.46	-39.88	132.00	192.00	192.00	4.8
0	(8+9)-IV-4	-747	-12	3155	-1.29	-1.22	27.16	132.00	192.00	192.00	6.8
0	(8+9)-II-1	-454	17	-4173	-0.78	1.63	-35.93	132.00	192.00	192.00	5.1
0	(8+9)-V-1	-1038	8	3447	-1.79	0.79	29.68	132.00	192.00	192.00	6.3
0	(8+9)-II-3	-269	16	-6037	-0.46	1.57	-51.97	132.00	192.00	192.00	3.6
0	(8+9)-V-2	-1185	-1	6514	-2.04	-0.09	56.08	132.00	192.00	192.00	3.4
0	(8+9)-III-1	-846	6	1888	-1.46	0.64	16.25	132.00	192.00	192.00	11
0	(8+9)-V-3	-30	4	-6501	-0.05	0.35	-55.97	132.00	192.00	192.00	3.4
0	(8+9)-VIII-3	-225	14	-5566	-0.39	1.38	-47.92	132.00	192.00	192.00	3.9
0	(8+9)-V-4	-178	-5	-3434	-0.31	-0.54	-29.57	132.00	192.00	192.00	6.4
0	(8+9)-VII-3	-34	3	-6192	-0.06	0.30	-53.31	132.00	192.00	192.00	3.6
0	(8+9)-VI-1	-513	17	-3613	-0.88	1.67	-31.10	132.00	192.00	192.00	5.9
0	(8+9)-I-4	-374	-4	-1565	-0.64	-0.43	-13.48	132.00	192.00	192.00	14
0	(8+9)-VI-2	-1005	-13	6610	-1.73	-1.28	56.91	132.00	192.00	192.00	3.3
0	(8+9)-II-4	-762	-14	4186	-1.31	-1.38	36.04	132.00	192.00	192.00	5.1
0	(8+9)-VIII-1	-527	15	-2582	-0.91	1.51	-22.23	132.00	192.00	192.00	8.1
0	(8+9)-I-2	-989	-2	4645	-1.70	-0.20	39.99	132.00	192.00	192.00	4.8
0	(8+9)-II-2	-946	-13	6050	-1.63	-1.31	52.08	132.00	192.00	192.00	3.6
0	(8+9)-III-2	-985	-2	4336	-1.70	-0.15	37.33	132.00	192.00	192.00	5.1
0	(8+9)-VI-3	-210	16	-6597	-0.36	1.53	-56.80	132.00	192.00	192.00	3.3
0	(8+9)-VI-4	-703	-14	3626	-1.21	-1.41	31.21	132.00	192.00	192.00	5.9
0	(8+9)-VII-1	-1042	8	3757	-1.79	0.74	32.34	132.00	192.00	192.00	5.8
585	1	-718	1	245	-1.24	0.12	2.11	79.20	115.20	115.20	51
585	2	-1472	3	509	-2.53	0.28	4.38	118.80	172.80	172.80	37
585	3	-1472	3	509	-2.53	0.28	4.38	118.80	172.80	172.80	37
585	4	-718	1	245	-1.24	0.12	2.11	105.60	153.60	153.60	69
585	5	-718	1	245	-1.24	0.12	2.11	105.60	153.60	153.60	69
585	6	-718	1	245	-1.24	0.12	2.11	105.60	153.60	153.60	69
585	7	-718	1	245	-1.24	0.12	2.11	105.60	153.60	153.60	69

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
0	(8+9)-VI-4	-28	0.02	6.40	Si	>100
0	(8+9)-IV-4	-23	0.02	6.40	Si	>100
0	(8+9)-VIII-1	41	0.04	6.40	Si	>100
0	(8+9)-VIII-4	-18	0.02	6.40	Si	>100
600	2	36	0.03	5.76	Si	>100
600	3	36	0.03	5.76	Si	>100
600	(8+9)-VII-4	51	0.04	6.40	Si	>100
600	(8+9)-III-3	59	0.05	6.40	Si	>100
600	(8+9)-IV-3	67	0.06	6.40	Si	>100
600	(8+9)-I-1	-6	0.01	6.40	Si	>100
600	(8+9)-VIII-3	72	0.06	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
600	(8+9)-I-3	62	0.05	6.40	Si	>100
600	(8+9)-V-1	-25	0.02	6.40	Si	>100
600	(8+9)-II-1	57	0.05	6.40	Si	>100
600	(8+9)-V-2	-58	0.05	6.40	Si	>100
600	(8+9)-II-3	77	0.07	6.40	Si	97
600	(8+9)-V-3	81	0.07	6.40	Si	92
600	(8+9)-III-1	-9	0.01	6.40	Si	>100
600	(8+9)-V-4	48	0.04	6.40	Si	>100
600	(8+9)-VIII-2	-49	0.04	6.40	Si	>100
600	(8+9)-VI-1	51	0.04	6.40	Si	>100
600	(8+9)-IV-1	46	0.04	6.40	Si	>100
600	(8+9)-VI-2	-59	0.05	6.40	Si	>100
600	(8+9)-I-2	-39	0.03	6.40	Si	>100
600	(8+9)-VI-3	83	0.07	6.40	Si	90
600	(8+9)-II-2	-54	0.05	6.40	Si	>100
600	(8+9)-III-2	-36	0.03	6.40	Si	>100
600	(8+9)-IV-2	-43	0.04	6.40	Si	>100
600	(8+9)-I-4	29	0.03	6.40	Si	>100
600	(8+9)-II-4	-33	0.03	6.40	Si	>100
600	(8+9)-III-4	32	0.03	6.40	Si	>100
600	(8+9)-VII-1	-28	0.02	6.40	Si	>100
600	(8+9)-VII-2	-55	0.05	6.40	Si	>100
600	(8+9)-VII-3	78	0.07	6.40	Si	96
1200	1	17	0.01	3.84	Si	>100
1200	4	17	0.01	5.12	Si	>100
1200	5	17	0.01	5.12	Si	>100
1200	6	17	0.01	5.12	Si	>100
1200	7	17	0.01	5.12	Si	>100
Verifiche nella direzione secondaria						
0	(8+9)-IV-2	12	0.02	6.40	Si	>100
0	(8+9)-I-2	17	0.03	6.40	Si	>100
0	(8+9)-II-1	-17	0.03	6.40	Si	>100
0	(8+9)-VIII-2	18	0.03	6.40	Si	>100
0	(8+9)-II-2	27	0.04	6.40	Si	>100
0	(8+9)-VII-2	35	0.05	6.40	Si	>100
0	(8+9)-II-3	-22	0.04	6.40	Si	>100
0	(8+9)-VI-4	15	0.02	6.40	Si	>100
0	(8+9)-II-4	21	0.03	6.40	Si	>100
0	(8+9)-I-1	4	0.01	6.40	Si	>100
0	(8+9)-III-1	8	0.01	6.40	Si	>100
0	(8+9)-VI-2	33	0.05	6.40	Si	>100
0	(8+9)-III-2	13	0.02	6.40	Si	>100
0	(8+9)-VI-3	-29	0.05	6.40	Si	>100
0	(8+9)-VII-4	-26	0.04	6.40	Si	>100
0	(8+9)-V-3	-35	0.06	6.40	Si	>100
0	(8+9)-VII-1	30	0.05	6.40	Si	>100
0	(8+9)-V-2	39	0.06	6.40	Si	>100
0	(8+9)-V-1	26	0.04	6.40	Si	>100
0	(8+9)-IV-4	7	0.01	6.40	Si	>100
585	(8+9)-VIII-4	4	0.01	6.40	Si	>100
1170	1	7	0.01	3.84	Si	>100
1170	2	14	0.02	5.76	Si	>100
1170	3	14	0.02	5.76	Si	>100
1170	4	7	0.01	5.12	Si	>100
1170	5	7	0.01	5.12	Si	>100
1170	6	7	0.01	5.12	Si	>100
1170	7	7	0.01	5.12	Si	>100
1170	(8+9)-IV-3	19	0.03	6.40	Si	>100
1170	(8+9)-VII-3	30	0.05	6.40	Si	>100
1170	(8+9)-VI-1	11	0.02	6.40	Si	>100
1170	(8+9)-III-4	14	0.02	6.40	Si	>100
1170	(8+9)-III-3	21	0.03	6.40	Si	>100
1170	(8+9)-I-3	21	0.03	6.40	Si	>100
1170	(8+9)-I-4	14	0.02	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
1170	(8+9)-VIII-1	8	0.01	6.40	Si	>100
1170	(8+9)-IV-1	11	0.02	6.40	Si	>100
1170	(8+9)-VIII-3	22	0.03	6.40	Si	>100
1170	(8+9)-V-4	24	0.04	6.40	Si	>100

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	(8+9)-I-4	-1234	-2.18	32.00	15	-0.53	20.00	38	V	15
0	(8+9)-V-4	-2737	-4.83	32.00	6.6	-1.17	20.00	17	V	6.6
0	(8+9)-VII-4	-2987	-5.27	32.00	6.1	-1.28	20.00	16	V	6.1
0	(8+9)-VI-1	-2926	-5.17	32.00	6.2	-1.25	20.00	16	V	6.2
0	(8+9)-VIII-1	-2093	-3.70	32.00	8.7	-0.89	20.00	22	V	8.7
0	(8+9)-IV-1	-2544	-4.49	32.00	7.1	-1.09	20.00	18	V	7.1
0	(8+9)-III-4	-1484	-2.62	32.00	12	-0.63	20.00	32	V	12
0	(8+9)-II-1	-3377	-5.96	32.00	5.4	-1.44	20.00	14	V	5.4
1200	1	429	0.76	19.20	25	0.18	12.00	65	V	25
1200	2	847	1.50	28.80	19	0.36	18.00	50	V	19
1200	3	847	1.50	28.80	19	0.36	18.00	50	V	19
1200	4	429	0.76	25.60	34	0.18	16.00	87	V	34
1200	5	429	0.76	25.60	34	0.18	16.00	87	V	34
1200	6	429	0.76	25.60	34	0.18	16.00	87	V	34
1200	7	429	0.76	25.60	34	0.18	16.00	87	V	34
1200	(8+9)-VIII-4	2557	4.52	32.00	7.1	1.09	20.00	18	V	7.1
1200	(8+9)-V-2	5965	10.53	32.00	3.0	2.55	20.00	7.8	V	3.0
1200	(8+9)-I-3	-3732	-6.59	32.00	4.9	-1.59	20.00	13	V	4.9
1200	(8+9)-VI-2	6047	10.68	32.00	3.0	2.58	20.00	7.7	V	3.0
1200	(8+9)-III-3	-3465	-6.12	32.00	5.2	-1.48	20.00	14	V	5.2
1200	(8+9)-VI-3	-5449	-9.62	32.00	3.3	-2.33	20.00	8.6	V	3.3
1200	(8+9)-III-1	1928	3.41	32.00	9.4	0.82	20.00	24	V	9.4
1200	(8+9)-VI-4	3448	6.09	32.00	5.3	1.47	20.00	14	V	5.3
1200	(8+9)-IV-3	-4068	-7.18	32.00	4.5	-1.74	20.00	12	V	4.5
1200	(8+9)-VII-1	3563	6.29	32.00	5.1	1.52	20.00	13	V	5.1
1200	(8+9)-V-1	3296	5.82	32.00	5.5	1.41	20.00	14	V	5.5
1200	(8+9)-VII-2	5698	10.06	32.00	3.2	2.43	20.00	8.2	V	3.2
1200	(8+9)-V-3	-5367	-9.48	32.00	3.4	-2.29	20.00	8.7	V	3.4
1200	(8+9)-VII-3	-5100	-9.01	32.00	3.6	-2.18	20.00	9.2	V	3.6
1200	(8+9)-II-2	5556	9.81	32.00	3.3	2.37	20.00	8.4	V	3.3
1200	(8+9)-I-1	1661	2.93	32.00	11	0.71	20.00	28	V	11
1200	(8+9)-II-4	3938	6.95	32.00	4.6	1.68	20.00	12	V	4.6
1200	(8+9)-II-3	-4958	-8.76	32.00	3.7	-2.12	20.00	9.4	V	3.7
1200	(8+9)-III-2	4063	7.17	32.00	4.5	1.74	20.00	12	V	4.5
1200	(8+9)-IV-4	3048	5.38	32.00	5.9	1.30	20.00	15	V	5.9
1200	(8+9)-I-2	4330	7.65	32.00	4.2	1.85	20.00	11	V	4.2
1200	(8+9)-VIII-2	5156	9.11	32.00	3.5	2.20	20.00	9.1	V	3.5
1200	(8+9)-VIII-3	-4558	-8.05	32.00	4.0	-1.95	20.00	10	V	4.0
1200	(8+9)-IV-2	4666	8.24	32.00	3.9	1.99	20.00	10	V	3.9
Verifiche nella direzione secondaria										
0	1	223	0.38	19.20	50	0.09	12.00	>100	V	50
0	2	447	0.77	28.80	37	0.19	18.00	97	V	37
0	3	447	0.77	28.80	37	0.19	18.00	97	V	37
0	4	223	0.38	25.60	67	0.09	16.00	>100	V	67
0	5	223	0.38	25.60	67	0.09	16.00	>100	V	67
0	6	223	0.38	25.60	67	0.09	16.00	>100	V	67
0	7	223	0.38	25.60	67	0.09	16.00	>100	V	67
1170	(8+9)-VIII-4	2527	4.35	32.00	7.4	1.05	20.00	19	V	7.4
1170	(8+9)-IV-2	4727	8.14	32.00	3.9	1.97	20.00	10	V	3.9
1170	(8+9)-V-1	3230	5.56	32.00	5.8	1.35	20.00	15	V	5.8
1170	(8+9)-I-2	4352	7.49	32.00	4.3	1.81	20.00	11	V	4.3
1170	(8+9)-V-2	6048	10.41	32.00	3.1	2.52	20.00	7.9	V	3.1
1170	(8+9)-I-4	-1286	-2.21	32.00	14	-0.54	20.00	37	V	14
1170	(8+9)-V-3	-5799	-9.99	32.00	3.2	-2.42	20.00	8.3	V	3.2
1170	(8+9)-II-2	5667	9.76	32.00	3.3	2.36	20.00	8.5	V	3.3

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
1170	(8+9)-V-4	-2982	-5.13	32.00	6.2	-1.24	20.00	16	V	6.2
1170	(8+9)-II-4	3975	6.84	32.00	4.7	1.66	20.00	12	V	4.7
1170	(8+9)-VI-1	-3218	-5.54	32.00	5.8	-1.34	20.00	15	V	5.8
1170	(8+9)-III-2	4071	7.01	32.00	4.6	1.70	20.00	12	V	4.6
1170	(8+9)-VI-2	6175	10.63	32.00	3.0	2.57	20.00	7.8	V	3.0
1170	(8+9)-III-4	-1568	-2.70	32.00	12	-0.65	20.00	31	V	12
1170	(8+9)-VI-3	-5927	-10.20	32.00	3.1	-2.47	20.00	8.1	V	3.1
1170	(8+9)-I-1	1534	2.64	32.00	12	0.64	20.00	31	V	12
1170	(8+9)-VI-4	3466	5.97	32.00	5.4	1.44	20.00	14	V	5.4
1170	(8+9)-IV-4	3036	5.23	32.00	6.1	1.26	20.00	16	V	6.1
1170	(8+9)-VII-1	3512	6.05	32.00	5.3	1.46	20.00	14	V	5.3
1170	(8+9)-II-1	-3727	-6.42	32.00	5.0	-1.55	20.00	13	V	5.0
1170	(8+9)-VII-2	5766	9.93	32.00	3.2	2.40	20.00	8.3	V	3.2
1170	(8+9)-III-1	1816	3.13	32.00	10	0.76	20.00	26	V	10
1170	(8+9)-VII-3	-5518	-9.50	32.00	3.4	-2.30	20.00	8.7	V	3.4
1170	(8+9)-IV-1	-2787	-4.80	32.00	6.7	-1.16	20.00	17	V	6.7
1170	(8+9)-VII-4	-3263	-5.62	32.00	5.7	-1.36	20.00	15	V	5.7
1170	(8+9)-III-3	-3822	-6.58	32.00	4.9	-1.59	20.00	13	V	4.9
1170	(8+9)-IV-3	-4479	-7.71	32.00	4.1	-1.87	20.00	11	V	4.1
1170	(8+9)-II-3	-5418	-9.33	32.00	3.4	-2.26	20.00	8.9	V	3.4
1170	(8+9)-VIII-1	-2278	-3.92	32.00	8.2	-0.95	20.00	21	V	8.2
1170	(8+9)-VIII-2	5236	9.01	32.00	3.5	2.18	20.00	9.2	V	3.5
1170	(8+9)-VIII-3	-4987	-8.59	32.00	3.7	-2.08	20.00	9.6	V	3.7
1170	(8+9)-I-3	-4104	-7.07	32.00	4.5	-1.71	20.00	12	V	4.5

Verifiche a instabilità

Setto(X)	Comb.	k _{critc}	k _{critm}	λ_{relc}	λ_{relm}	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
(cm)						kg/cm ² q	kg/cm ² q	kg/cm ² q	kg/cm ² q	kg/cm ² q	kg/cm ² q	
28(50.0)	(8+9)-VI-2	--	--	--	--	0.40	0.54	-2.39	132.00	192.00	192.00	55
29(0.0)	(8+9)-VI-3	--	--	--	--	0.70	0.56	-4.01	132.00	192.00	192.00	34
30(120.0)	(8+9)-VI-3	--	--	--	--	4.51	1.59	11.16	132.00	192.00	192.00	9.9

Parete Xlam 3 - Nodi: [14-19-10-11-20-8-110-18-17-16-15-103] - **Crit.Prog.** Criterio di verifica XLAM 0 - **Verificato:** [Cs=2.272,Comb=3]

Geometria setti

Setto	Crit.	X	L	S	X90	L90	S90
		mm	cm	cm	mm	cm	cm
31	Criterio di verifica XLAM 0	0	387.0	12.1	0	420.0	12.1
		2100	387.0	12.1	1935	420.0	12.1
		4200	387.0	12.1	3870	420.0	12.1
32	Criterio di verifica XLAM 0	0	387.0	12.1	0	364.3	12.1
		1822	387.0	12.1	1935	364.3	12.1
		3643	387.0	12.1	3870	364.3	12.1
33	Criterio di verifica XLAM 0	0	167.0	12.1	0	180.0	12.1
		900	167.0	12.1	835	180.0	12.1
		1800	167.0	12.1	1670	180.0	12.1

Setto 31: origine (742.0,828.0,193.5), direzione (0.930183,0.367096,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cm ² q	kg/cm ² q	kg/cm ² q	kg/cm ² q	kg/cm ² q	kg/cm ² q	
0	(8+9)-VIII-3	385	352	532	0.14	4.71	0.29	132.00	192.00	192.00	37
0	(8+9)-IV-1	611	188	1518	0.22	2.52	0.84	132.00	192.00	192.00	52
0	(8+9)-VI-4	-318	253	-1809	-0.11	3.38	-1.00	132.00	192.00	192.00	44
0	(8+9)-III-2	117	-522	1728	0.04	-6.98	0.95	132.00	192.00	192.00	24
0	(8+9)-IV-2	-605	-454	-9	-0.22	-6.07	-0.01	132.00	192.00	192.00	32

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-III-3	-366	507	-1250	-0.13	6.78	-0.69	132.00	192.00	192.00	26
0	(8+9)-VIII-1	582	275	1473	0.21	3.68	0.81	132.00	192.00	192.00	40
0	(8+9)-III-4	-730	314	-1708	-0.26	4.20	-0.94	132.00	192.00	192.00	37
0	(8+9)-VII-3	-271	218	-1100	-0.10	2.91	-0.61	132.00	192.00	192.00	55
0	(8+9)-VII-2	22	-232	1578	0.01	-3.11	0.87	132.00	192.00	192.00	48
0	(8+9)-I-2	271	-359	1484	0.10	-4.80	0.82	132.00	192.00	192.00	33
0	(8+9)-I-4	-577	477	-1952	-0.21	6.38	-1.08	132.00	192.00	192.00	26
0	(8+9)-IV-3	357	439	487	0.13	5.87	0.27	132.00	192.00	192.00	30
0	(8+9)-II-2	-92	89	-823	-0.03	1.18	-0.45	132.00	192.00	192.00	>100
0	(8+9)-IV-4	-860	-203	-1040	-0.31	-2.72	-0.57	132.00	192.00	192.00	58
0	(8+9)-II-4	-347	340	-1854	-0.12	4.54	-1.02	132.00	192.00	192.00	35
0	(8+9)-V-1	233	-203	2280	0.08	-2.71	1.26	132.00	192.00	192.00	47
0	(8+9)-VIII-2	-634	-367	-54	-0.23	-4.91	-0.03	132.00	192.00	192.00	39
0	(8+9)-V-2	176	-70	1333	0.06	-0.93	0.74	132.00	192.00	192.00	>100
0	(8+9)-I-1	328	-492	2430	0.12	-6.58	1.34	132.00	192.00	192.00	24
0	(8+9)-V-3	-425	55	-856	-0.15	0.73	-0.47	132.00	192.00	192.00	>100
0	(8+9)-II-1	98	-355	2331	0.03	-4.74	1.29	132.00	192.00	192.00	32
0	(8+9)-V-4	-482	188	-1802	-0.17	2.51	-0.99	132.00	192.00	192.00	55
0	(8+9)-III-1	482	-329	2186	0.17	-4.40	1.21	132.00	192.00	192.00	33
0	(8+9)-I-3	-520	344	-1006	-0.18	4.60	-0.56	132.00	192.00	192.00	37
0	(8+9)-II-3	-156	-104	1301	-0.06	-1.38	0.72	132.00	192.00	192.00	91
0	(8+9)-VIII-4	-831	-290	-995	-0.30	-3.88	-0.55	132.00	192.00	192.00	43
0	(8+9)-VI-1	69	-268	2286	0.02	-3.58	1.26	132.00	192.00	192.00	39
0	(8+9)-VI-2	-121	176	-868	-0.04	2.35	-0.48	132.00	192.00	192.00	68
0	(8+9)-VI-3	-128	-190	1346	-0.05	-2.55	0.74	132.00	192.00	192.00	58
2100	1	281	-20	-1336	0.10	-0.26	-0.74	79.20	115.20	115.20	>100
2100	2	467	-39	-2621	0.17	-0.52	-1.45	118.80	172.80	172.80	78
2100	3	467	-39	-2621	0.17	-0.52	-1.45	118.80	172.80	172.80	78
2100	4	281	-20	-1336	0.10	-0.26	-0.74	105.60	153.60	153.60	>100
2100	5	281	-20	-1336	0.10	-0.26	-0.74	105.60	153.60	153.60	>100
2100	6	281	-20	-1336	0.10	-0.26	-0.74	105.60	153.60	153.60	>100
2100	7	281	-20	-1336	0.10	-0.26	-0.74	105.60	153.60	153.60	>100
4200	(8+9)-VII-1	2363	-5	-2378	0.84	-0.06	-1.31	132.00	192.00	192.00	74
4200	(8+9)-VII-4	-2087	-1	2157	-0.74	-0.01	1.19	132.00	192.00	192.00	>100
Verifiche nella direzione secondaria											
0	(8+9)-V-1	-13614	-26	19421	-6.70	-0.74	13.65	132.00	192.00	192.00	13
0	(8+9)-II-1	-13541	-64	19423	-6.66	-1.81	13.65	132.00	192.00	192.00	12
0	(8+9)-VI-1	-13411	-75	18785	-6.60	-2.10	13.20	132.00	192.00	192.00	12
0	(8+9)-VIII-3	-12134	-117	7030	-5.97	-3.30	4.94	132.00	192.00	192.00	23
0	(8+9)-II-3	-12591	-72	11641	-6.19	-2.03	8.18	132.00	192.00	192.00	18
0	(8+9)-VII-4	-10975	88	-6656	-5.40	2.47	-4.68	132.00	192.00	192.00	26
0	(8+9)-II-4	-10873	109	-8232	-5.35	3.08	-5.79	132.00	192.00	192.00	21
0	(8+9)-VII-1	-13438	-43	17847	-6.61	-1.21	12.54	132.00	192.00	192.00	14
0	(8+9)-III-1	-13870	-9	19972	-6.82	-0.25	14.04	132.00	192.00	192.00	13
0	(8+9)-I-1	-14046	8	21547	-6.91	0.22	15.14	132.00	192.00	192.00	12
0	(8+9)-III-2	-13707	79	17160	-6.74	2.22	12.06	132.00	192.00	192.00	13
0	(8+9)-VI-3	-12721	-62	12278	-6.26	-1.74	8.63	132.00	192.00	192.00	18
0	(8+9)-V-4	-10799	71	-8230	-5.31	2.00	-5.78	132.00	192.00	192.00	24
0	(8+9)-III-4	-10543	54	-8782	-5.19	1.51	-6.17	132.00	192.00	192.00	25
0	(8+9)-VII-2	-13275	45	15034	-6.53	1.26	10.57	132.00	192.00	192.00	16
0	(8+9)-I-2	-13531	62	15585	-6.66	1.75	10.95	132.00	192.00	192.00	15
0	(8+9)-I-4	-10367	37	-10356	-5.10	1.04	-7.28	132.00	192.00	192.00	23
0	(8+9)-VIII-1	-12824	-130	13537	-6.31	-3.66	9.51	132.00	192.00	192.00	14
0	(8+9)-VI-4	-11003	120	-7594	-5.41	3.37	-5.34	132.00	192.00	192.00	22
0	(8+9)-IV-1	-12953	-120	14175	-6.37	-3.37	9.96	132.00	192.00	192.00	14
0	(8+9)-V-2	-13099	28	13459	-6.44	0.79	9.46	132.00	192.00	192.00	18
0	(8+9)-IV-3	-12004	-127	6392	-5.91	-3.59	4.49	132.00	192.00	192.00	23
1935	1	-17283	-18	9233	-8.50	-0.51	6.49	79.20	115.20	115.20	15
1935	2	-32397	-45	17459	-15.94	-1.28	12.27	118.80	172.80	172.80	12
1935	3	-32397	-45	17459	-15.94	-1.28	12.27	118.80	172.80	172.80	12
1935	4	-17283	-18	9233	-8.50	-0.51	6.49	105.60	153.60	153.60	21
1935	5	-17283	-18	9233	-8.50	-0.51	6.49	105.60	153.60	153.60	21
1935	6	-17283	-18	9233	-8.50	-0.51	6.49	105.60	153.60	153.60	21
1935	7	-17283	-18	9233	-8.50	-0.51	6.49	105.60	153.60	153.60	21

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
3870	(8+9)-VIII-4	-10922	-133	7880	-5.37	-3.74	5.54	132.00	192.00	192.00	20
3870	(8+9)-IV-4	-10847	-135	7821	-5.34	-3.79	5.50	132.00	192.00	192.00	20
3870	(8+9)-III-3	-9419	67	5589	-4.63	1.88	3.93	132.00	192.00	192.00	32
3870	(8+9)-II-2	-10675	-57	8426	-5.25	-1.61	5.92	132.00	192.00	192.00	25
3870	(8+9)-VII-3	-9669	73	5785	-4.76	2.05	4.07	132.00	192.00	192.00	31
3870	(8+9)-VI-2	-10599	-59	8367	-5.21	-1.66	5.88	132.00	192.00	192.00	25
3870	(8+9)-V-3	-9755	47	5616	-4.80	1.33	3.95	132.00	192.00	192.00	36
3870	(8+9)-VIII-2	-10886	-144	7803	-5.36	-4.06	5.48	132.00	192.00	192.00	20
3870	(8+9)-IV-2	-10961	-143	7861	-5.39	-4.01	5.52	132.00	192.00	192.00	20
3870	(8+9)-I-3	-9505	41	5420	-4.68	1.16	3.81	132.00	192.00	192.00	38

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Ty kg	τ_d kg/cmq	fvd kg/cmq	RS	Cs
0	(8+9)-VI-4	-99	0.03	6.40	Si	>100
0	(8+9)-III-1	142	0.04	6.40	Si	>100
0	(8+9)-V-3	-111	0.03	6.40	Si	>100
0	(8+9)-III-2	349	0.09	6.40	Si	71
0	(8+9)-VIII-3	-386	0.10	6.40	Si	64
0	(8+9)-III-3	-354	0.09	6.40	Si	70
0	(8+9)-VIII-1	-311	0.08	6.40	Si	80
0	(8+9)-III-4	-147	0.04	6.40	Si	>100
0	(8+9)-VII-3	-232	0.06	6.40	Si	>100
0	(8+9)-IV-1	-274	0.07	6.40	Si	90
0	(8+9)-I-2	228	0.06	6.40	Si	>100
0	(8+9)-IV-2	418	0.11	6.40	Si	59
0	(8+9)-I-4	-268	0.07	6.40	Si	92
0	(8+9)-IV-3	-423	0.11	6.40	Si	58
0	(8+9)-VII-2	227	0.06	6.40	Si	>100
0	(8+9)-IV-4	269	0.07	6.40	Si	92
0	(8+9)-II-4	-135	0.04	6.40	Si	>100
0	(8+9)-V-1	141	0.04	6.40	Si	>100
0	(8+9)-VIII-2	381	0.10	6.40	Si	65
0	(8+9)-V-2	105	0.03	6.40	Si	>100
0	(8+9)-I-1	263	0.07	6.40	Si	94
0	(8+9)-II-1	130	0.03	6.40	Si	>100
0	(8+9)-V-4	-146	0.04	6.40	Si	>100
0	(8+9)-VIII-4	306	0.08	6.40	Si	81
0	(8+9)-I-3	-233	0.06	6.40	Si	>100
0	(8+9)-VII-1	19	0.00	6.40	Si	>100
0	(8+9)-VII-4	-24	0.01	6.40	Si	>100
0	(8+9)-VI-1	94	0.02	6.40	Si	>100
2100	(8+9)-II-3	27	0.01	6.40	Si	>100
2100	(8+9)-VI-3	25	0.01	6.40	Si	>100
4200	1	-22	0.01	3.84	Si	>100
4200	2	-43	0.01	5.76	Si	>100
4200	3	-43	0.01	5.76	Si	>100
4200	4	-22	0.01	5.12	Si	>100
4200	5	-22	0.01	5.12	Si	>100
4200	6	-22	0.01	5.12	Si	>100
4200	7	-22	0.01	5.12	Si	>100
4200	(8+9)-VI-2	-53	0.01	6.40	Si	>100
4200	(8+9)-II-2	-53	0.01	6.40	Si	>100
Verifiche nella direzione secondaria						
0	(8+9)-II-2	-77	0.04	6.40	Si	>100
0	(8+9)-VI-4	-82	0.04	6.40	Si	>100
0	(8+9)-VII-4	-41	0.02	6.40	Si	>100
0	(8+9)-II-4	-77	0.03	6.40	Si	>100
0	(8+9)-VI-3	37	0.02	6.40	Si	>100
0	(8+9)-V-4	-54	0.02	6.40	Si	>100
0	(8+9)-I-4	-34	0.02	6.40	Si	>100
0	(8+9)-VI-2	-71	0.03	6.40	Si	>100
0	(8+9)-II-3	43	0.02	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
1935	(8+9)-III-1	-19	0.01	6.40	Si	>100
1935	(8+9)-I-3	-8	0.00	6.40	Si	>100
3870	1	-40	0.02	3.84	Si	>100
3870	2	-102	0.05	5.76	Si	>100
3870	3	-102	0.05	5.76	Si	>100
3870	4	-40	0.02	5.12	Si	>100
3870	5	-40	0.02	5.12	Si	>100
3870	6	-40	0.02	5.12	Si	>100
3870	7	-40	0.02	5.12	Si	>100
3870	(8+9)-VIII-4	-157	0.07	6.40	Si	90
3870	(8+9)-V-3	22	0.01	6.40	Si	>100
3870	(8+9)-II-1	-44	0.02	6.40	Si	>100
3870	(8+9)-III-2	-96	0.04	6.40	Si	>100
3870	(8+9)-IV-2	-180	0.08	6.40	Si	78
3870	(8+9)-I-1	-55	0.02	6.40	Si	>100
3870	(8+9)-IV-4	-166	0.08	6.40	Si	85
3870	(8+9)-VII-1	-35	0.02	6.40	Si	>100
3870	(8+9)-V-2	-76	0.03	6.40	Si	>100
3870	(8+9)-VII-2	-123	0.06	6.40	Si	>100
3870	(8+9)-III-4	-46	0.02	6.40	Si	>100
3870	(8+9)-VII-3	69	0.03	6.40	Si	>100
3870	(8+9)-III-3	41	0.02	6.40	Si	>100
3870	(8+9)-I-2	-49	0.02	6.40	Si	>100
3870	(8+9)-VI-1	-52	0.02	6.40	Si	>100
3870	(8+9)-IV-3	126	0.06	6.40	Si	>100
3870	(8+9)-IV-1	111	0.05	6.40	Si	>100
3870	(8+9)-VIII-1	103	0.05	6.40	Si	>100
3870	(8+9)-VIII-2	-189	0.09	6.40	Si	75
3870	(8+9)-VIII-3	134	0.06	6.40	Si	>100
3870	(8+9)-V-1	-82	0.04	6.40	Si	>100

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	1	286	0.15	19.20	>100	0.04	12.00	>100	V	>100
0	4	286	0.15	25.60	>100	0.04	16.00	>100	V	>100
0	5	286	0.15	25.60	>100	0.04	16.00	>100	V	>100
0	6	286	0.15	25.60	>100	0.04	16.00	>100	V	>100
0	7	286	0.15	25.60	>100	0.04	16.00	>100	V	>100
2100	2	-180	-0.10	28.80	>100	-0.02	18.00	>100	V	>100
2100	3	-180	-0.10	28.80	>100	-0.02	18.00	>100	V	>100
2100	(8+9)-VIII-4	-6917	-3.69	32.00	8.7	-0.89	20.00	22	V	8.7
2100	(8+9)-IV-1	7320	3.91	32.00	8.2	0.95	20.00	21	V	8.2
2100	(8+9)-V-1	8215	4.39	32.00	7.3	1.06	20.00	19	V	7.3
2100	(8+9)-I-2	5659	3.02	32.00	11	0.73	20.00	27	V	11
2100	(8+9)-V-2	4637	2.48	32.00	13	0.60	20.00	33	V	13
2100	(8+9)-I-4	-9140	-4.88	32.00	6.6	-1.18	20.00	17	V	6.6
2100	(8+9)-V-3	-4541	-2.42	32.00	13	-0.59	20.00	34	V	13
2100	(8+9)-II-2	-3694	-1.97	32.00	16	-0.48	20.00	42	V	16
2100	(8+9)-V-4	-8119	-4.33	32.00	7.4	-1.05	20.00	19	V	7.4
2100	(8+9)-II-4	-8134	-4.34	32.00	7.4	-1.05	20.00	19	V	7.4
2100	(8+9)-VI-1	7924	4.23	32.00	7.6	1.02	20.00	20	V	7.6
2100	(8+9)-III-2	5932	3.17	32.00	10	0.77	20.00	26	V	10
2100	(8+9)-VI-2	-4001	-2.14	32.00	15	-0.52	20.00	39	V	15
2100	(8+9)-III-4	-8867	-4.73	32.00	6.8	-1.15	20.00	17	V	6.8
2100	(8+9)-VI-3	4097	2.19	32.00	15	0.53	20.00	38	V	15
2100	(8+9)-IV-2	-2784	-1.49	32.00	22	-0.36	20.00	56	V	22
2100	(8+9)-VI-4	-7828	-4.18	32.00	7.7	-1.01	20.00	20	V	7.7
2100	(8+9)-IV-4	-7224	-3.86	32.00	8.3	-0.93	20.00	21	V	8.3
2100	(8+9)-VII-1	7941	4.24	32.00	7.5	1.03	20.00	19	V	7.5
2100	(8+9)-II-1	8230	4.39	32.00	7.3	1.06	20.00	19	V	7.3
2100	(8+9)-VII-2	4910	2.62	32.00	12	0.63	20.00	32	V	12
2100	(8+9)-III-1	8963	4.79	32.00	6.7	1.16	20.00	17	V	6.7

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
2100	(8+9)-VII-3	-4814	-2.57	32.00	12	-0.62	20.00	32	V	12
2100	(8+9)-I-1	9236	4.93	32.00	6.5	1.19	20.00	17	V	6.5
2100	(8+9)-VII-4	-7845	-4.19	32.00	7.6	-1.01	20.00	20	V	7.6
2100	(8+9)-III-3	-5836	-3.12	32.00	10	-0.75	20.00	27	V	10
2100	(8+9)-IV-3	2880	1.54	32.00	21	0.37	20.00	54	V	21
2100	(8+9)-II-3	3791	2.02	32.00	16	0.49	20.00	41	V	16
2100	(8+9)-VIII-1	7013	3.74	32.00	8.5	0.91	20.00	22	V	8.5
2100	(8+9)-VIII-2	-3090	-1.65	32.00	19	-0.40	20.00	50	V	19
2100	(8+9)-VIII-3	3186	1.70	32.00	19	0.41	20.00	49	V	19
2100	(8+9)-I-3	-5563	-2.97	32.00	11	-0.72	20.00	28	V	11
Verifiche nella direzione secondaria										
1935	(8+9)-VIII-4	-8916	-4.39	32.00	7.3	-1.06	20.00	19	V	7.3
1935	(8+9)-VII-2	5388	2.65	32.00	12	0.64	20.00	31	V	12
1935	(8+9)-III-3	-7735	-3.81	32.00	8.4	-0.92	20.00	22	V	8.4
1935	(8+9)-IV-2	-3884	-1.91	32.00	17	-0.46	20.00	43	V	17
1935	(8+9)-III-4	-11388	-5.60	32.00	5.7	-1.36	20.00	15	V	5.7
1935	(8+9)-VIII-2	-4281	-2.11	32.00	15	-0.51	20.00	39	V	15
1935	(8+9)-IV-1	8293	4.08	32.00	7.8	0.99	20.00	20	V	7.8
1935	(8+9)-VII-4	-10062	-4.95	32.00	6.5	-1.20	20.00	17	V	6.5
1935	(8+9)-I-1	10700	5.26	32.00	6.1	1.27	20.00	16	V	6.1
1935	(8+9)-IV-3	2862	1.41	32.00	23	0.34	20.00	59	V	23
1935	(8+9)-I-3	-7402	-3.64	32.00	8.8	-0.88	20.00	23	V	8.8
1935	(8+9)-IV-4	-9314	-4.58	32.00	7.0	-1.11	20.00	18	V	7.0
1935	(8+9)-II-1	9403	4.63	32.00	6.9	1.12	20.00	18	V	6.9
1935	(8+9)-V-1	9374	4.61	32.00	6.9	1.12	20.00	18	V	6.9
1935	(8+9)-II-3	3972	1.95	32.00	16	0.47	20.00	42	V	16
1935	(8+9)-V-2	5055	2.49	32.00	13	0.60	20.00	33	V	13
1935	(8+9)-III-1	10367	5.10	32.00	6.3	1.23	20.00	16	V	6.3
1935	(8+9)-V-3	-6077	-2.99	32.00	11	-0.72	20.00	28	V	11
1935	(8+9)-VIII-3	3260	1.60	32.00	20	0.39	20.00	52	V	20
1935	(8+9)-V-4	-10395	-5.11	32.00	6.3	-1.24	20.00	16	V	6.3
1935	(8+9)-VII-3	-6410	-3.15	32.00	10	-0.76	20.00	26	V	10
1935	(8+9)-VI-1	9005	4.43	32.00	7.2	1.07	20.00	19	V	7.2
1935	(8+9)-I-4	-11721	-5.77	32.00	5.5	-1.40	20.00	14	V	5.5
1935	(8+9)-VI-2	-5391	-2.65	32.00	12	-0.64	20.00	31	V	12
1935	(8+9)-II-4	-10424	-5.13	32.00	6.2	-1.24	20.00	16	V	6.2
1935	(8+9)-VIII-1	7895	3.88	32.00	8.2	0.94	20.00	21	V	8.2
1935	(8+9)-I-2	6381	3.14	32.00	10	0.76	20.00	26	V	10
1935	(8+9)-II-2	-4994	-2.46	32.00	13	-0.59	20.00	34	V	13
1935	(8+9)-III-2	6714	3.30	32.00	9.7	0.80	20.00	25	V	9.7
1935	(8+9)-VI-3	4370	2.15	32.00	15	0.52	20.00	38	V	15
1935	(8+9)-VI-4	-10026	-4.93	32.00	6.5	-1.19	20.00	17	V	6.5
1935	(8+9)-VII-1	9041	4.45	32.00	7.2	1.08	20.00	19	V	7.2
3870	1	-1538	-0.76	19.20	25	-0.18	12.00	66	V	25
3870	2	-3266	-1.61	28.80	18	-0.39	18.00	46	V	18
3870	3	-3266	-1.61	28.80	18	-0.39	18.00	46	V	18
3870	4	-1538	-0.76	25.60	34	-0.18	16.00	87	V	34
3870	5	-1538	-0.76	25.60	34	-0.18	16.00	87	V	34
3870	6	-1538	-0.76	25.60	34	-0.18	16.00	87	V	34
3870	7	-1538	-0.76	25.60	34	-0.18	16.00	87	V	34

Setto 32: origine (1300.1,1048.3,193.5), direzione (0.930183,0.367096,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
1822	(8+9)-IV-3	-921	154	1022	-0.33	2.05	0.56	132.00	192.00	192.00	73
1822	(8+9)-VIII-3	-995	162	1118	-0.35	2.17	0.62	132.00	192.00	192.00	69
3643	1	2683	-106	-4632	0.96	-1.41	-2.56	79.20	115.20	115.20	22
3643	2	5595	-224	-9703	1.99	-3.00	-5.35	118.80	172.80	172.80	15
3643	3	5595	-224	-9703	1.99	-3.00	-5.35	118.80	172.80	172.80	15
3643	4	2683	-106	-4632	0.96	-1.41	-2.56	105.60	153.60	153.60	29
3643	5	2683	-106	-4632	0.96	-1.41	-2.56	105.60	153.60	153.60	29
3643	6	2683	-106	-4632	0.96	-1.41	-2.56	105.60	153.60	153.60	29

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
3643	7	2683	-106	-4632	0.96	-1.41	-2.56	105.60	153.60	153.60	29
3643	(8+9)-VIII-4	2405	-549	-3344	0.86	-7.35	-1.85	132.00	192.00	192.00	18
3643	(8+9)-IV-1	1189	412	-2991	0.42	5.50	-1.65	132.00	192.00	192.00	25
3643	(8+9)-V-2	2835	462	-5601	1.01	6.18	-3.09	132.00	192.00	192.00	18
3643	(8+9)-I-4	1556	-663	-872	0.55	-8.87	-0.48	132.00	192.00	192.00	19
3643	(8+9)-V-3	867	-608	-781	0.31	-8.12	-0.43	132.00	192.00	192.00	21
3643	(8+9)-II-2	2542	49	-3769	0.90	0.66	-2.08	132.00	192.00	192.00	47
3643	(8+9)-V-4	1199	-638	-716	0.43	-8.53	-0.40	132.00	192.00	192.00	20
3643	(8+9)-II-4	2265	-296	-2397	0.81	-3.96	-1.32	132.00	192.00	192.00	30
3643	(8+9)-VI-1	1543	143	-4031	0.55	1.92	-2.22	132.00	192.00	192.00	39
3643	(8+9)-III-2	2552	409	-5743	0.91	5.47	-3.17	132.00	192.00	192.00	19
3643	(8+9)-VI-2	2649	42	-3816	0.94	0.56	-2.11	132.00	192.00	192.00	48
3643	(8+9)-III-4	1630	-741	-1170	0.58	-9.91	-0.65	132.00	192.00	192.00	17
3643	(8+9)-VI-3	1053	-187	-2566	0.37	-2.50	-1.42	132.00	192.00	192.00	43
3643	(8+9)-IV-2	2789	-212	-4763	0.99	-2.83	-2.63	132.00	192.00	192.00	28
3643	(8+9)-VI-4	2158	-288	-2350	0.77	-3.86	-1.30	132.00	192.00	192.00	31
3643	(8+9)-IV-4	2512	-557	-3391	0.89	-7.45	-1.87	132.00	192.00	192.00	18
3643	(8+9)-VII-1	2429	571	-5368	0.86	7.64	-2.96	132.00	192.00	192.00	16
3643	(8+9)-II-1	1436	151	-3985	0.51	2.02	-2.20	132.00	192.00	192.00	39
3643	(8+9)-VII-2	2909	384	-5899	1.04	5.14	-3.26	132.00	192.00	192.00	19
3643	(8+9)-III-1	2072	596	-5212	0.74	7.97	-2.88	132.00	192.00	192.00	16
3643	(8+9)-VII-3	793	-529	-483	0.28	-7.08	-0.27	132.00	192.00	192.00	25
3643	(8+9)-I-3	1224	-633	-937	0.44	-8.46	-0.52	132.00	192.00	192.00	20
3643	(8+9)-VII-4	1273	-716	-1014	0.45	-9.58	-0.56	132.00	192.00	192.00	18
3643	(8+9)-III-3	1150	-554	-639	0.41	-7.41	-0.35	132.00	192.00	192.00	23
3643	(8+9)-I-2	2478	487	-5445	0.88	6.52	-3.00	132.00	192.00	192.00	18
3643	(8+9)-II-3	1160	-194	-2613	0.41	-2.60	-1.44	132.00	192.00	192.00	41
3643	(8+9)-VIII-1	1296	404	-3038	0.46	5.40	-1.68	132.00	192.00	192.00	25
3643	(8+9)-VIII-2	2896	-219	-4809	1.03	-2.93	-2.65	132.00	192.00	192.00	27
3643	(8+9)-I-1	2146	518	-5510	0.76	6.92	-3.04	132.00	192.00	192.00	17
3643	(8+9)-V-1	2503	493	-5666	0.89	6.59	-3.13	132.00	192.00	192.00	17
Verifiche nella direzione secondaria											
0	(8+9)-VIII-4	-10391	239	-13324	-5.89	7.76	-12.45	132.00	192.00	192.00	9.4
0	(8+9)-III-3	-10707	-21	-12002	-6.07	-0.68	-11.21	132.00	192.00	192.00	16
0	(8+9)-I-3	-10697	-8	-11499	-6.07	-0.25	-10.74	132.00	192.00	192.00	17
0	(8+9)-IV-2	-9795	247	-8056	-5.55	8.03	-7.53	132.00	192.00	192.00	12
0	(8+9)-I-4	-10912	77	-16336	-6.19	2.51	-15.26	132.00	192.00	192.00	11
0	(8+9)-VII-4	-10838	104	-14551	-6.15	3.36	-13.59	132.00	192.00	192.00	11
0	(8+9)-IV-4	-10410	235	-13709	-5.90	7.64	-12.81	132.00	192.00	192.00	9.3
0	(8+9)-VI-4	-10427	194	-15001	-5.91	6.31	-14.01	132.00	192.00	192.00	9.4
0	(8+9)-II-2	-9831	203	-9733	-5.58	6.58	-9.09	132.00	192.00	192.00	12
0	(8+9)-VIII-2	-9813	244	-8441	-5.57	7.90	-7.88	132.00	192.00	192.00	12
0	(8+9)-VII-3	-10645	-8	-10720	-6.04	-0.26	-10.01	132.00	192.00	192.00	18
0	(8+9)-VI-2	-9849	199	-10117	-5.59	6.45	-9.45	132.00	192.00	192.00	12
0	(8+9)-V-3	-10634	5	-10217	-6.03	0.17	-9.54	132.00	192.00	192.00	19
0	(8+9)-V-4	-10849	90	-15054	-6.15	2.93	-14.06	132.00	192.00	192.00	11
0	(8+9)-II-4	-10446	191	-15385	-5.92	6.18	-14.37	132.00	192.00	192.00	9.3
0	(8+9)-III-4	-10901	91	-15833	-6.18	2.94	-14.79	132.00	192.00	192.00	11
3870	1	-10860	-427	-1168	-6.16	-13.87	-1.09	79.20	115.20	115.20	7.5
3870	2	-21933	-904	-1604	-12.44	-29.34	-1.50	118.80	172.80	172.80	5.4
3870	3	-21933	-904	-1604	-12.44	-29.34	-1.50	118.80	172.80	172.80	5.4
3870	4	-10860	-427	-1168	-6.16	-13.87	-1.09	105.60	153.60	153.60	10
3870	5	-10860	-427	-1168	-6.16	-13.87	-1.09	105.60	153.60	153.60	10
3870	6	-10860	-427	-1168	-6.16	-13.87	-1.09	105.60	153.60	153.60	10
3870	7	-10860	-427	-1168	-6.16	-13.87	-1.09	105.60	153.60	153.60	10
3870	(8+9)-III-2	-8196	-327	-1988	-4.65	-10.60	-1.86	132.00	192.00	192.00	15
3870	(8+9)-VII-1	-8093	-298	-1987	-4.59	-9.67	-1.86	132.00	192.00	192.00	16
3870	(8+9)-V-1	-8150	-283	-2038	-4.62	-9.19	-1.90	132.00	192.00	192.00	17
3870	(8+9)-VII-2	-7982	-311	-1509	-4.53	-10.09	-1.41	132.00	192.00	192.00	17
3870	(8+9)-I-2	-8138	-342	-1937	-4.62	-11.08	-1.81	132.00	192.00	192.00	15
3870	(8+9)-II-3	-7624	-215	-1324	-4.32	-6.98	-1.24	132.00	192.00	192.00	23
3870	(8+9)-VI-1	-8023	-226	-2043	-4.55	-7.33	-1.91	132.00	192.00	192.00	21
3870	(8+9)-IV-1	-7896	-281	-2015	-4.48	-9.11	-1.88	132.00	192.00	192.00	17
3870	(8+9)-V-2	-7925	-326	-1458	-4.49	-10.58	-1.36	132.00	192.00	192.00	16

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
3870	(8+9)-I-1	-8364	-299	-2517	-4.74	-9.69	-2.35	132.00	192.00	192.00	16
3870	(8+9)-II-1	-8087	-231	-2187	-4.59	-7.49	-2.04	132.00	192.00	192.00	20
3870	(8+9)-IV-3	-7433	-265	-1152	-4.22	-8.60	-1.08	132.00	192.00	192.00	20
3870	(8+9)-VIII-1	-7832	-276	-1871	-4.44	-8.95	-1.75	132.00	192.00	192.00	18
3870	(8+9)-III-1	-8306	-314	-2465	-4.71	-10.18	-2.30	132.00	192.00	192.00	15
3870	(8+9)-VIII-3	-7498	-270	-1295	-4.25	-8.76	-1.21	132.00	192.00	192.00	19
3870	(8+9)-VI-3	-7688	-220	-1467	-4.36	-7.14	-1.37	132.00	192.00	192.00	22

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
1822	(8+9)-II-3	-107	0.03	6.40	Si	>100
1822	(8+9)-VI-1	-105	0.03	6.40	Si	>100
1822	(8+9)-VIII-1	-199	0.05	6.40	Si	>100
1822	(8+9)-VII-1	-106	0.03	6.40	Si	>100
1822	(8+9)-VI-3	-112	0.03	6.40	Si	>100
1822	(8+9)-VIII-2	43	0.01	6.40	Si	>100
1822	(8+9)-V-2	-61	0.02	6.40	Si	>100
1822	(8+9)-IV-2	37	0.01	6.40	Si	>100
1822	(8+9)-IV-1	-205	0.05	6.40	Si	>100
3643	1	-179	0.05	3.84	Si	83
3643	2	-374	0.10	5.76	Si	60
3643	3	-374	0.10	5.76	Si	60
3643	4	-179	0.05	5.12	Si	>100
3643	5	-179	0.05	5.12	Si	>100
3643	6	-179	0.05	5.12	Si	>100
3643	7	-179	0.05	5.12	Si	>100
3643	(8+9)-VIII-4	-143	0.04	6.40	Si	>100
3643	(8+9)-I-4	-582	0.15	6.40	Si	42
3643	(8+9)-VI-2	-232	0.06	6.40	Si	>100
3643	(8+9)-III-3	-544	0.14	6.40	Si	45
3643	(8+9)-II-4	-412	0.11	6.40	Si	60
3643	(8+9)-I-2	236	0.06	6.40	Si	>100
3643	(8+9)-VI-4	-346	0.09	6.40	Si	71
3643	(8+9)-IV-3	-283	0.07	6.40	Si	87
3643	(8+9)-I-3	-483	0.12	6.40	Si	51
3643	(8+9)-V-1	117	0.03	6.40	Si	>100
3643	(8+9)-VII-2	78	0.02	6.40	Si	>100
3643	(8+9)-V-3	-264	0.07	6.40	Si	94
3643	(8+9)-VII-3	-325	0.08	6.40	Si	76
3643	(8+9)-III-1	275	0.07	6.40	Si	90
3643	(8+9)-VII-4	-302	0.08	6.40	Si	82
3643	(8+9)-III-2	297	0.08	6.40	Si	83
3643	(8+9)-V-4	-363	0.09	6.40	Si	68
3643	(8+9)-III-4	-521	0.13	6.40	Si	47
3643	(8+9)-IV-4	-209	0.05	6.40	Si	>100
3643	(8+9)-II-2	-166	0.04	6.40	Si	>100
3643	(8+9)-II-1	165	0.04	6.40	Si	>100
3643	(8+9)-VIII-3	-218	0.06	6.40	Si	>100
3643	(8+9)-I-1	336	0.09	6.40	Si	74
Verifiche nella direzione secondaria						
1935	(8+9)-VIII-4	-321	0.17	6.40	Si	38
1935	(8+9)-IV-2	-333	0.17	6.40	Si	37
1935	(8+9)-VIII-2	-330	0.17	6.40	Si	37
1935	(8+9)-VII-2	-152	0.08	6.40	Si	81
1935	(8+9)-IV-4	-317	0.17	6.40	Si	39
3870	1	-464	0.24	3.84	Si	16
3870	2	-971	0.51	5.76	Si	11
3870	3	-971	0.51	5.76	Si	11
3870	4	-464	0.24	5.12	Si	21
3870	5	-464	0.24	5.12	Si	21
3870	6	-464	0.24	5.12	Si	21
3870	7	-464	0.24	5.12	Si	21

X	Comb.	Ty	τ_d	fvd	RS	Cs
3870	(8+9)-V-2	-293	0.15	6.40	Si	42
3870	(8+9)-I-4	-325	0.17	6.40	Si	38
3870	(8+9)-V-4	-370	0.19	6.40	Si	33
3870	(8+9)-II-3	-277	0.15	6.40	Si	44
3870	(8+9)-VI-1	-268	0.14	6.40	Si	46
3870	(8+9)-III-1	-466	0.24	6.40	Si	26
3870	(8+9)-VI-2	-348	0.18	6.40	Si	35
3870	(8+9)-III-3	-452	0.24	6.40	Si	27
3870	(8+9)-VI-3	-291	0.15	6.40	Si	42
3870	(8+9)-IV-1	-788	0.41	6.40	Si	16
3870	(8+9)-VI-4	-371	0.19	6.40	Si	33
3870	(8+9)-IV-3	-783	0.41	6.40	Si	16
3870	(8+9)-VII-1	-421	0.22	6.40	Si	29
3870	(8+9)-V-1	-269	0.14	6.40	Si	45
3870	(8+9)-I-2	-339	0.18	6.40	Si	36
3870	(8+9)-V-3	-346	0.18	6.40	Si	35
3870	(8+9)-VII-3	-498	0.26	6.40	Si	25
3870	(8+9)-III-2	-187	0.10	6.40	Si	65
3870	(8+9)-VII-4	-218	0.11	6.40	Si	56
3870	(8+9)-II-1	-281	0.15	6.40	Si	43
3870	(8+9)-II-4	-358	0.19	6.40	Si	34
3870	(8+9)-III-4	-173	0.09	6.40	Si	71
3870	(8+9)-I-3	-301	0.16	6.40	Si	41
3870	(8+9)-VIII-1	-774	0.41	6.40	Si	16
3870	(8+9)-I-1	-314	0.16	6.40	Si	39
3870	(8+9)-VIII-3	-797	0.42	6.40	Si	15
3870	(8+9)-II-2	-362	0.19	6.40	Si	34

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	1	3677	1.96	19.20	9.8	0.48	12.00	25	V	9.8
0	2	7057	3.77	28.80	7.6	0.91	18.00	20	V	7.6
0	3	7057	3.77	28.80	7.6	0.91	18.00	20	V	7.6
0	4	3677	1.96	25.60	13	0.48	16.00	34	V	13
0	5	3677	1.96	25.60	13	0.48	16.00	34	V	13
0	6	3677	1.96	25.60	13	0.48	16.00	34	V	13
0	7	3677	1.96	25.60	13	0.48	16.00	34	V	13
0	(8+9)-IV-3	3770	2.01	32.00	16	0.49	20.00	41	V	16
0	(8+9)-VII-2	6278	3.35	32.00	9.5	0.81	20.00	25	V	9.5
0	(8+9)-II-3	5797	3.09	32.00	10	0.75	20.00	27	V	10
0	(8+9)-VI-3	6037	3.22	32.00	9.9	0.78	20.00	26	V	9.9
0	(8+9)-II-1	9048	4.83	32.00	6.6	1.17	20.00	17	V	6.6
0	(8+9)-VI-1	8808	4.70	32.00	6.8	1.14	20.00	18	V	6.8
0	(8+9)-VIII-3	4010	2.14	32.00	15	0.52	20.00	39	V	15
0	(8+9)-V-2	5670	3.03	32.00	11	0.73	20.00	27	V	11
0	(8+9)-V-1	8610	4.60	32.00	7.0	1.11	20.00	18	V	7.0
0	(8+9)-III-2	7079	3.78	32.00	8.5	0.91	20.00	22	V	8.5
0	(8+9)-I-2	6471	3.45	32.00	9.3	0.84	20.00	24	V	9.3
1822	(8+9)-VIII-4	-5680	-3.03	32.00	11	-0.73	20.00	27	V	11
1822	(8+9)-IV-1	7554	4.03	32.00	7.9	0.98	20.00	20	V	7.9
1822	(8+9)-I-4	-7905	-4.22	32.00	7.6	-1.02	20.00	20	V	7.6
1822	(8+9)-III-4	-7665	-4.09	32.00	7.8	-0.99	20.00	20	V	7.8
1822	(8+9)-VI-4	-6479	-3.46	32.00	9.3	-0.84	20.00	24	V	9.3
1822	(8+9)-VII-1	8208	4.38	32.00	7.3	1.06	20.00	19	V	7.3
1822	(8+9)-III-1	9231	4.93	32.00	6.5	1.19	20.00	17	V	6.5
1822	(8+9)-VIII-2	-2063	-1.10	32.00	29	-0.27	20.00	75	V	29
1822	(8+9)-II-4	-6786	-3.62	32.00	8.8	-0.88	20.00	23	V	8.8
1822	(8+9)-VIII-1	7247	3.87	32.00	8.3	0.94	20.00	21	V	8.3
1822	(8+9)-V-4	-6881	-3.67	32.00	8.7	-0.89	20.00	22	V	8.7
1822	(8+9)-IV-2	-1756	-0.94	32.00	34	-0.23	20.00	88	V	34
1822	(8+9)-IV-4	-5987	-3.20	32.00	10	-0.77	20.00	26	V	10
1822	(8+9)-VI-2	-2862	-1.53	32.00	21	-0.37	20.00	54	V	21

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
1822	(8+9)-II-2	-2555	-1.36	32.00	23	-0.33	20.00	61	V	23
1822	(8+9)-I-1	9471	5.06	32.00	6.3	1.22	20.00	16	V	6.3
1822	(8+9)-VII-4	-6642	-3.55	32.00	9.0	-0.86	20.00	23	V	9.0
3643	(8+9)-III-3	-5495	-2.93	32.00	11	-0.71	20.00	28	V	11
3643	(8+9)-I-3	-4802	-2.56	32.00	12	-0.62	20.00	32	V	12
3643	(8+9)-VII-3	-4697	-2.51	32.00	13	-0.61	20.00	33	V	13
3643	(8+9)-V-3	-4004	-2.14	32.00	15	-0.52	20.00	39	V	15
Verifiche nella direzione secondaria										
0	(8+9)-VIII-4	-6234	-3.54	32.00	9.1	-0.86	20.00	23	V	9.1
0	(8+9)-IV-2	-2169	-1.23	32.00	26	-0.30	20.00	67	V	26
0	(8+9)-VIII-3	3663	2.08	32.00	15	0.50	20.00	40	V	15
0	(8+9)-VIII-2	-2484	-1.41	32.00	23	-0.34	20.00	59	V	23
0	(8+9)-VIII-1	7414	4.20	32.00	7.6	1.02	20.00	20	V	7.6
0	(8+9)-IV-4	-6550	-3.71	32.00	8.6	-0.90	20.00	22	V	8.6
0	(8+9)-IV-3	3348	1.90	32.00	17	0.46	20.00	44	V	17
0	(8+9)-IV-1	7729	4.38	32.00	7.3	1.06	20.00	19	V	7.3
1935	(8+9)-VII-2	5719	3.24	32.00	9.9	0.78	20.00	25	V	9.9
1935	(8+9)-III-3	-5562	-3.15	32.00	10	-0.76	20.00	26	V	10
1935	(8+9)-VII-3	-4497	-2.55	32.00	13	-0.62	20.00	32	V	13
1935	(8+9)-I-3	-5164	-2.93	32.00	11	-0.71	20.00	28	V	11
1935	(8+9)-VII-4	-7207	-4.09	32.00	7.8	-0.99	20.00	20	V	7.8
1935	(8+9)-II-1	8712	4.94	32.00	6.5	1.20	20.00	17	V	6.5
1935	(8+9)-V-1	8827	5.01	32.00	6.4	1.21	20.00	17	V	6.4
1935	(8+9)-II-3	4195	2.38	32.00	13	0.58	20.00	35	V	13
1935	(8+9)-V-2	5322	3.02	32.00	11	0.73	20.00	27	V	11
1935	(8+9)-III-1	9495	5.38	32.00	5.9	1.30	20.00	15	V	5.9
1935	(8+9)-V-3	-4099	-2.32	32.00	14	-0.56	20.00	36	V	14
1935	(8+9)-I-2	6387	3.62	32.00	8.8	0.88	20.00	23	V	8.8
1935	(8+9)-V-4	-7605	-4.31	32.00	7.4	-1.04	20.00	19	V	7.4
1935	(8+9)-I-1	9892	5.61	32.00	5.7	1.36	20.00	15	V	5.7
1935	(8+9)-VI-1	8392	4.76	32.00	6.7	1.15	20.00	17	V	6.7
1935	(8+9)-I-4	-8670	-4.92	32.00	6.5	-1.19	20.00	17	V	6.5
1935	(8+9)-VI-2	-3292	-1.87	32.00	17	-0.45	20.00	44	V	17
1935	(8+9)-III-4	-8272	-4.69	32.00	6.8	-1.14	20.00	18	V	6.8
1935	(8+9)-II-4	-7489	-4.25	32.00	7.5	-1.03	20.00	19	V	7.5
1935	(8+9)-II-2	-2973	-1.69	32.00	19	-0.41	20.00	49	V	19
1935	(8+9)-III-2	6784	3.85	32.00	8.3	0.93	20.00	21	V	8.3
1935	(8+9)-VI-3	4514	2.56	32.00	12	0.62	20.00	32	V	12
1935	(8+9)-VI-4	-7170	-4.07	32.00	7.9	-0.98	20.00	20	V	7.9
1935	(8+9)-VII-1	8430	4.78	32.00	6.7	1.16	20.00	17	V	6.7
3870	1	2235	1.27	19.20	15	0.31	12.00	39	V	15
3870	2	4396	2.49	28.80	12	0.60	18.00	30	V	12
3870	3	4396	2.49	28.80	12	0.60	18.00	30	V	12
3870	4	2235	1.27	25.60	20	0.31	16.00	52	V	20
3870	5	2235	1.27	25.60	20	0.31	16.00	52	V	20
3870	6	2235	1.27	25.60	20	0.31	16.00	52	V	20
3870	7	2235	1.27	25.60	20	0.31	16.00	52	V	20

Setto 33: origine (1132.7,982.2,303.5), direzione (0.930183,0.367096,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	(8+9)-II-1	2834	12	1817	2.34	0.36	5.38	132.00	192.00	192.00	21
0	(8+9)-V-1	2892	-4	1820	2.39	-0.11	5.39	132.00	192.00	192.00	21
0	(8+9)-VII-1	2834	-6	1773	2.34	-0.18	5.25	132.00	192.00	192.00	22
0	(8+9)-VI-1	2711	6	1746	2.24	0.19	5.17	132.00	192.00	192.00	22
0	(8+9)-VIII-1	2515	-1	1589	2.07	-0.04	4.71	132.00	192.00	192.00	25
0	(8+9)-IV-1	2639	4	1660	2.18	0.13	4.92	132.00	192.00	192.00	23
0	(8+9)-III-1	3245	13	2009	2.68	0.40	5.95	132.00	192.00	192.00	19
0	(8+9)-I-1	3304	15	2056	2.72	0.47	6.09	132.00	192.00	192.00	18
1800	1	3017	2	-1359	2.49	0.06	-4.03	79.20	115.20	115.20	15
1800	2	5769	9	-2595	4.76	0.29	-7.69	118.80	172.80	172.80	12
1800	3	5769	9	-2595	4.76	0.29	-7.69	118.80	172.80	172.80	12

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
1800	4	3017	2	-1359	2.49	0.06	-4.03	105.60	153.60	153.60	20
1800	5	3017	2	-1359	2.49	0.06	-4.03	105.60	153.60	153.60	20
1800	6	3017	2	-1359	2.49	0.06	-4.03	105.60	153.60	153.60	20
1800	7	3017	2	-1359	2.49	0.06	-4.03	105.60	153.60	153.60	20
1800	(8+9)-VIII-4	3987	4	446	3.29	0.13	1.32	132.00	192.00	192.00	31
1800	(8+9)-V-2	970	-10	-1936	0.80	-0.32	-5.74	132.00	192.00	192.00	27
1800	(8+9)-I-3	3539	13	270	2.92	0.41	0.80	132.00	192.00	192.00	35
1800	(8+9)-VI-2	3361	-4	-92	2.77	-0.11	-0.27	132.00	192.00	192.00	43
1800	(8+9)-III-3	3646	13	357	3.01	0.40	1.06	132.00	192.00	192.00	33
1800	(8+9)-VI-3	788	6	-1772	0.65	0.20	-5.25	132.00	192.00	192.00	30
1800	(8+9)-III-2	503	-10	-2221	0.42	-0.32	-6.58	132.00	192.00	192.00	26
1800	(8+9)-VI-4	4344	3	735	3.58	0.10	2.18	132.00	192.00	192.00	26
1800	(8+9)-IV-3	1254	5	-1424	1.03	0.16	-4.22	132.00	192.00	192.00	33
1800	(8+9)-I-2	611	-11	-2135	0.50	-0.33	-6.33	132.00	192.00	192.00	26
1800	(8+9)-II-4	4452	3	795	3.67	0.10	2.36	132.00	192.00	192.00	25
1800	(8+9)-VII-2	863	-10	-2023	0.71	-0.31	-5.99	132.00	192.00	192.00	26
1800	(8+9)-V-3	3179	13	71	2.62	0.40	0.21	132.00	192.00	192.00	43
1800	(8+9)-VII-3	3287	13	158	2.71	0.39	0.47	132.00	192.00	192.00	40
1800	(8+9)-II-2	3253	-4	-152	2.68	-0.11	-0.45	132.00	192.00	192.00	43
1800	(8+9)-VII-4	4139	12	737	3.41	0.39	2.18	132.00	192.00	192.00	25
1800	(8+9)-II-3	896	6	-1713	0.74	0.20	-5.08	132.00	192.00	192.00	30
1800	(8+9)-V-4	4246	12	824	3.50	0.37	2.44	132.00	192.00	192.00	24
1800	(8+9)-III-4	4499	13	936	3.71	0.40	2.77	132.00	192.00	192.00	22
1800	(8+9)-IV-4	4094	4	506	3.38	0.14	1.50	132.00	192.00	192.00	29
1800	(8+9)-I-4	4606	12	1022	3.80	0.38	3.03	132.00	192.00	192.00	21
1800	(8+9)-VIII-2	3004	-2	-381	2.48	-0.07	-1.13	132.00	192.00	192.00	40
1800	(8+9)-VIII-3	1146	5	-1483	0.95	0.16	-4.40	132.00	192.00	192.00	32
1800	(8+9)-IV-2	2896	-2	-441	2.39	-0.08	-1.31	132.00	192.00	192.00	40
Verifiche nella direzione secondaria											
0	(8+9)-VIII-4	-5894	-37	-3389	-6.76	-2.40	-12.97	132.00	192.00	192.00	12
0	(8+9)-IV-4	-5851	-37	-3500	-6.72	-2.41	-13.39	132.00	192.00	192.00	12
0	(8+9)-III-4	-5630	-19	-3856	-6.46	-1.23	-14.75	132.00	192.00	192.00	12
0	(8+9)-II-4	-6038	-30	-3798	-6.93	-1.97	-14.53	132.00	192.00	192.00	11
0	(8+9)-VII-4	-5773	-19	-3487	-6.63	-1.22	-13.34	132.00	192.00	192.00	13
0	(8+9)-V-4	-5829	-17	-3577	-6.69	-1.09	-13.68	132.00	192.00	192.00	13
0	(8+9)-VI-4	-6081	-30	-3687	-6.98	-1.97	-14.11	132.00	192.00	192.00	12
0	(8+9)-I-4	-5686	-17	-3946	-6.53	-1.10	-15.10	132.00	192.00	192.00	12
835	(8+9)-VI-1	-5419	-9	3582	-6.22	-0.61	13.71	132.00	192.00	192.00	13
835	(8+9)-IV-2	-6467	-103	1656	-7.42	-6.77	6.34	132.00	192.00	192.00	14
835	(8+9)-III-2	-5997	-58	3406	-6.88	-3.83	13.03	132.00	192.00	192.00	11
835	(8+9)-I-2	-5835	-38	3181	-6.70	-2.50	12.17	132.00	192.00	192.00	13
835	(8+9)-V-2	-5752	-29	2892	-6.60	-1.90	11.07	132.00	192.00	192.00	15
835	(8+9)-II-1	-5444	-12	3669	-6.25	-0.79	14.04	132.00	192.00	192.00	13
835	(8+9)-VIII-2	-6442	-100	1569	-7.39	-6.59	6.00	132.00	192.00	192.00	15
835	(8+9)-III-1	-5529	-11	3785	-6.35	-0.71	14.48	132.00	192.00	192.00	12
835	(8+9)-I-1	-5691	-31	4009	-6.53	-2.04	15.34	132.00	192.00	192.00	11
835	(8+9)-VII-1	-5445	-2	3496	-6.25	-0.11	13.38	132.00	192.00	192.00	14
835	(8+9)-VIII-1	-4880	58	2833	-5.60	3.83	10.84	132.00	192.00	192.00	13
835	(8+9)-IV-1	-4905	56	2920	-5.63	3.65	11.17	132.00	192.00	192.00	13
835	(8+9)-VII-2	-5914	-49	3117	-6.79	-3.24	11.93	132.00	192.00	192.00	12
835	(8+9)-V-1	-5607	-22	3721	-6.44	-1.45	14.24	132.00	192.00	192.00	12
1670	1	-8475	38	3686	-9.73	2.47	14.10	79.20	115.20	115.20	6.6
1670	2	-16235	51	7068	-18.64	3.33	27.04	118.80	172.80	172.80	5.3
1670	3	-16235	51	7068	-18.64	3.33	27.04	118.80	172.80	172.80	5.3
1670	4	-8475	38	3686	-9.73	2.47	14.10	105.60	153.60	153.60	8.9
1670	5	-8475	38	3686	-9.73	2.47	14.10	105.60	153.60	153.60	8.9
1670	6	-8475	38	3686	-9.73	2.47	14.10	105.60	153.60	153.60	8.9
1670	7	-8475	38	3686	-9.73	2.47	14.10	105.60	153.60	153.60	8.9
1670	(8+9)-IV-3	-5214	70	2020	-5.99	4.58	7.73	132.00	192.00	192.00	15
1670	(8+9)-II-3	-4974	65	1801	-5.71	4.25	6.89	132.00	192.00	192.00	17
1670	(8+9)-VI-2	-6617	-6	3241	-7.59	-0.36	12.40	132.00	192.00	192.00	15
1670	(8+9)-II-2	-6671	-13	3260	-7.66	-0.88	12.47	132.00	192.00	192.00	14
1670	(8+9)-VII-3	-5833	38	2851	-6.70	2.47	10.91	132.00	192.00	192.00	14
1670	(8+9)-I-3	-5579	63	2722	-6.40	4.11	10.41	132.00	192.00	192.00	13

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
1670	(8+9)-V-3	-5761	36	2785	-6.61	2.38	10.66	132.00	192.00	192.00	14
1670	(8+9)-III-3	-5652	64	2788	-6.49	4.20	10.67	132.00	192.00	192.00	13
1670	(8+9)-VIII-3	-5269	62	2039	-6.05	4.06	7.80	132.00	192.00	192.00	16
1670	(8+9)-VI-3	-5029	57	1820	-5.77	3.73	6.96	132.00	192.00	192.00	18

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
0	(8+9)-III-2	-20	0.01	6.40	Si	>100
0	(8+9)-I-2	-19	0.01	6.40	Si	>100
1800	1	41	0.02	3.84	Si	>100
1800	2	73	0.04	5.76	Si	>100
1800	3	73	0.04	5.76	Si	>100
1800	4	41	0.02	5.12	Si	>100
1800	5	41	0.02	5.12	Si	>100
1800	6	41	0.02	5.12	Si	>100
1800	7	41	0.02	5.12	Si	>100
1800	(8+9)-IV-4	35	0.02	6.40	Si	>100
1800	(8+9)-VI-1	29	0.02	6.40	Si	>100
1800	(8+9)-I-4	38	0.02	6.40	Si	>100
1800	(8+9)-VI-2	25	0.01	6.40	Si	>100
1800	(8+9)-II-2	23	0.01	6.40	Si	>100
1800	(8+9)-VI-3	32	0.02	6.40	Si	>100
1800	(8+9)-II-4	29	0.02	6.40	Si	>100
1800	(8+9)-VI-4	27	0.02	6.40	Si	>100
1800	(8+9)-I-3	39	0.02	6.40	Si	>100
1800	(8+9)-VII-1	23	0.01	6.40	Si	>100
1800	(8+9)-III-4	40	0.02	6.40	Si	>100
1800	(8+9)-VII-2	25	0.02	6.40	Si	>100
1800	(8+9)-IV-2	29	0.02	6.40	Si	>100
1800	(8+9)-VII-3	31	0.02	6.40	Si	>100
1800	(8+9)-I-1	19	0.01	6.40	Si	>100
1800	(8+9)-VII-4	34	0.02	6.40	Si	>100
1800	(8+9)-V-2	23	0.01	6.40	Si	>100
1800	(8+9)-VIII-1	23	0.01	6.40	Si	>100
1800	(8+9)-V-4	32	0.02	6.40	Si	>100
1800	(8+9)-VIII-2	31	0.02	6.40	Si	>100
1800	(8+9)-II-3	34	0.02	6.40	Si	>100
1800	(8+9)-VIII-3	26	0.02	6.40	Si	>100
1800	(8+9)-III-3	38	0.02	6.40	Si	>100
1800	(8+9)-VIII-4	33	0.02	6.40	Si	>100
1800	(8+9)-IV-3	28	0.02	6.40	Si	>100
1800	(8+9)-V-3	33	0.02	6.40	Si	>100
1800	(8+9)-II-1	28	0.02	6.40	Si	>100
1800	(8+9)-III-1	17	0.01	6.40	Si	>100
1800	(8+9)-IV-1	22	0.01	6.40	Si	>100
1800	(8+9)-V-1	25	0.01	6.40	Si	>100
Verifiche nella direzione secondaria						
0	(8+9)-II-2	-52	0.06	6.40	Si	>100
0	(8+9)-VI-4	-48	0.05	6.40	Si	>100
0	(8+9)-VI-2	-52	0.06	6.40	Si	>100
0	(8+9)-II-4	-48	0.05	6.40	Si	>100
1670	1	66	0.07	3.84	Si	55
1670	2	121	0.13	5.76	Si	45
1670	3	121	0.13	5.76	Si	45
1670	4	66	0.07	5.12	Si	73
1670	5	66	0.07	5.12	Si	73
1670	6	66	0.07	5.12	Si	73
1670	7	66	0.07	5.12	Si	73
1670	(8+9)-VIII-4	47	0.05	6.40	Si	>100
1670	(8+9)-IV-4	47	0.05	6.40	Si	>100
1670	(8+9)-V-3	47	0.05	6.40	Si	>100
1670	(8+9)-II-1	62	0.07	6.40	Si	98

X	Comb.	Ty	τ_d	fvd	RS	Cs
1670	(8+9)-V-4	38	0.04	6.40	Si	>100
1670	(8+9)-I-4	37	0.04	6.40	Si	>100
1670	(8+9)-VI-1	61	0.06	6.40	Si	99
1670	(8+9)-III-2	49	0.05	6.40	Si	>100
1670	(8+9)-I-2	44	0.05	6.40	Si	>100
1670	(8+9)-III-4	43	0.05	6.40	Si	>100
1670	(8+9)-VI-3	60	0.06	6.40	Si	>100
1670	(8+9)-IV-2	49	0.05	6.40	Si	>100
1670	(8+9)-I-1	53	0.06	6.40	Si	>100
1670	(8+9)-I-3	46	0.05	6.40	Si	>100
1670	(8+9)-VII-1	47	0.05	6.40	Si	>100
1670	(8+9)-V-2	43	0.05	6.40	Si	>100
1670	(8+9)-VII-2	48	0.05	6.40	Si	>100
1670	(8+9)-III-1	48	0.05	6.40	Si	>100
1670	(8+9)-VII-3	42	0.04	6.40	Si	>100
1670	(8+9)-IV-1	44	0.05	6.40	Si	>100
1670	(8+9)-VII-4	44	0.05	6.40	Si	>100
1670	(8+9)-III-3	41	0.04	6.40	Si	>100
1670	(8+9)-IV-3	42	0.04	6.40	Si	>100
1670	(8+9)-II-3	60	0.06	6.40	Si	>100
1670	(8+9)-VIII-1	44	0.05	6.40	Si	>100
1670	(8+9)-VIII-2	48	0.05	6.40	Si	>100
1670	(8+9)-VIII-3	42	0.04	6.40	Si	>100
1670	(8+9)-V-1	52	0.06	6.40	Si	>100

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	(8+9)-III-3	-4272	-5.29	32.00	6.1	-1.28	20.00	16	V	6.1
0	(8+9)-IV-4	-4725	-5.85	32.00	5.5	-1.41	20.00	14	V	5.5
0	(8+9)-VIII-4	-4562	-5.64	32.00	5.7	-1.37	20.00	15	V	5.7
0	(8+9)-I-3	-4093	-5.06	32.00	6.3	-1.23	20.00	16	V	6.3
0	(8+9)-VII-4	-5109	-6.32	32.00	5.1	-1.53	20.00	13	V	5.1
0	(8+9)-I-4	-5832	-7.21	32.00	4.4	-1.75	20.00	11	V	4.4
0	(8+9)-VI-4	-5158	-6.38	32.00	5.0	-1.54	20.00	13	V	5.0
0	(8+9)-V-4	-5288	-6.54	32.00	4.9	-1.58	20.00	13	V	4.9
0	(8+9)-VIII-2	-2711	-3.35	32.00	9.5	-0.81	20.00	25	V	9.5
0	(8+9)-VII-3	-3728	-4.61	32.00	6.9	-1.12	20.00	18	V	6.9
0	(8+9)-VI-2	-3307	-4.09	32.00	7.8	-0.99	20.00	20	V	7.8
0	(8+9)-V-3	-3550	-4.39	32.00	7.3	-1.06	20.00	19	V	7.3
0	(8+9)-II-2	-3144	-3.89	32.00	8.2	-0.94	20.00	21	V	8.2
0	(8+9)-III-4	-5653	-6.99	32.00	4.6	-1.69	20.00	12	V	4.6
0	(8+9)-II-4	-5321	-6.58	32.00	4.9	-1.59	20.00	13	V	4.9
1800	1	5386	6.66	19.20	2.9	1.61	12.00	7.4	V	2.9
1800	2	10248	12.68	28.80	2.3	3.07	18.00	5.9	V	2.3
1800	3	10248	12.68	28.80	2.3	3.07	18.00	5.9	V	2.3
1800	4	5386	6.66	25.60	3.8	1.61	16.00	9.9	V	3.8
1800	5	5386	6.66	25.60	3.8	1.61	16.00	9.9	V	3.8
1800	6	5386	6.66	25.60	3.8	1.61	16.00	9.9	V	3.8
1800	7	5386	6.66	25.60	3.8	1.61	16.00	9.9	V	3.8
1800	(8+9)-IV-1	6929	8.57	32.00	3.7	2.07	20.00	9.6	V	3.7
1800	(8+9)-VI-1	7688	9.51	32.00	3.4	2.30	20.00	8.7	V	3.4
1800	(8+9)-III-2	6674	8.26	32.00	3.9	2.00	20.00	10	V	3.9
1800	(8+9)-VII-1	7385	9.14	32.00	3.5	2.21	20.00	9.0	V	3.5
1800	(8+9)-V-2	5821	7.20	32.00	4.4	1.74	20.00	11	V	4.4
1800	(8+9)-VII-2	6101	7.55	32.00	4.2	1.83	20.00	11	V	4.2
1800	(8+9)-V-1	7664	9.48	32.00	3.4	2.29	20.00	8.7	V	3.4
1800	(8+9)-II-1	7860	9.72	32.00	3.3	2.35	20.00	8.5	V	3.3
1800	(8+9)-IV-3	4762	5.89	32.00	5.4	1.43	20.00	14	V	5.4
1800	(8+9)-II-3	5694	7.04	32.00	4.5	1.70	20.00	12	V	4.5
1800	(8+9)-I-2	6395	7.91	32.00	4.0	1.91	20.00	10	V	4.0
1800	(8+9)-VI-3	5865	7.26	32.00	4.4	1.76	20.00	11	V	4.4
1800	(8+9)-I-1	8237	10.19	32.00	3.1	2.47	20.00	8.1	V	3.1

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
1800	(8+9)-VIII-1	6757	8.36	32.00	3.8	2.02	20.00	9.9	V	3.8
1800	(8+9)-III-1	7958	9.85	32.00	3.3	2.38	20.00	8.4	V	3.3
1800	(8+9)-VIII-3	4934	6.10	32.00	5.2	1.48	20.00	14	V	5.2
1800	(8+9)-IV-2	2649	3.28	32.00	9.8	0.79	20.00	25	V	9.8
Verifiche nella direzione secondaria										
0	1	225	0.26	19.20	74	0.06	12.00	>100	V	74
0	2	433	0.50	28.80	58	0.12	18.00	>100	V	58
0	3	433	0.50	28.80	58	0.12	18.00	>100	V	58
0	4	225	0.26	25.60	99	0.06	16.00	>100	V	99
0	5	225	0.26	25.60	99	0.06	16.00	>100	V	99
0	6	225	0.26	25.60	99	0.06	16.00	>100	V	99
0	7	225	0.26	25.60	99	0.06	16.00	>100	V	99
835	(8+9)-VIII-4	-4559	-5.23	32.00	6.1	-1.27	20.00	16	V	6.1
835	(8+9)-IV-2	-1786	-2.05	32.00	16	-0.50	20.00	40	V	16
835	(8+9)-V-1	5492	6.30	32.00	5.1	1.53	20.00	13	V	5.1
835	(8+9)-I-2	3904	4.48	32.00	7.1	1.08	20.00	18	V	7.1
835	(8+9)-V-2	3136	3.60	32.00	8.9	0.87	20.00	23	V	8.9
835	(8+9)-VII-1	5323	6.11	32.00	5.2	1.48	20.00	14	V	5.2
835	(8+9)-IV-3	1936	2.22	32.00	14	0.54	20.00	37	V	14
835	(8+9)-I-4	-6110	-7.01	32.00	4.6	-1.70	20.00	12	V	4.6
835	(8+9)-IV-4	-4790	-5.50	32.00	5.8	-1.33	20.00	15	V	5.8
835	(8+9)-VIII-3	2167	2.49	32.00	13	0.60	20.00	33	V	13
835	(8+9)-VIII-1	4710	5.41	32.00	5.9	1.31	20.00	15	V	5.9
835	(8+9)-III-2	4073	4.68	32.00	6.8	1.13	20.00	18	V	6.8
835	(8+9)-II-1	5504	6.32	32.00	5.1	1.53	20.00	13	V	5.1
835	(8+9)-III-4	-5941	-6.82	32.00	4.7	-1.65	20.00	12	V	4.7
835	(8+9)-I-1	6260	7.19	32.00	4.5	1.74	20.00	12	V	4.5
835	(8+9)-VII-4	-5172	-5.94	32.00	5.4	-1.44	20.00	14	V	5.4
835	(8+9)-III-1	6091	6.99	32.00	4.6	1.69	20.00	12	V	4.6
835	(8+9)-IV-1	4940	5.67	32.00	5.6	1.37	20.00	15	V	5.6
835	(8+9)-II-3	2499	2.87	32.00	11	0.69	20.00	29	V	11
835	(8+9)-VIII-2	-2016	-2.31	32.00	14	-0.56	20.00	36	V	14
835	(8+9)-VI-1	5273	6.05	32.00	5.3	1.46	20.00	14	V	5.3
835	(8+9)-VII-2	3305	3.79	32.00	8.4	0.92	20.00	22	V	8.4
835	(8+9)-VI-3	2730	3.13	32.00	10	0.76	20.00	26	V	10
1670	(8+9)-V-3	-3064	-3.52	32.00	9.1	-0.85	20.00	23	V	9.1
1670	(8+9)-VI-4	-5166	-5.93	32.00	5.4	-1.44	20.00	14	V	5.4
1670	(8+9)-VI-2	-2689	-3.09	32.00	10	-0.75	20.00	27	V	10
1670	(8+9)-VII-3	-3272	-3.76	32.00	8.5	-0.91	20.00	22	V	8.5
1670	(8+9)-V-4	-5368	-6.16	32.00	5.2	-1.49	20.00	13	V	5.2
1670	(8+9)-I-3	-3778	-4.34	32.00	7.4	-1.05	20.00	19	V	7.4
1670	(8+9)-III-3	-3985	-4.57	32.00	7.0	-1.11	20.00	18	V	7.0
1670	(8+9)-II-4	-5380	-6.18	32.00	5.2	-1.49	20.00	13	V	5.2
1670	(8+9)-II-2	-2475	-2.84	32.00	11	-0.69	20.00	29	V	11

Verifiche a instabilità

Setto(X)	Comb.	krit _c	krit _m	λ_{relc}	λ_{relm}	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
(cm)						kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	
31(0.0)	(8+9)-I-1	--	--	--	--	0.12	-6.58	1.34	132.00	192.00	192.00	24
32(364.3)	3	--	--	--	--	1.99	-3.00	-5.35	118.80	172.80	172.80	15
33(180.0)	3	--	--	--	--	4.76	0.29	-7.69	118.80	172.80	172.80	12

Parete Xlam 3 - Nodi: [14-19-10-11-20-8-110-18-17-16-15-103] - **Crit.Prog.** Criterio di verifica XLAM 0 - **Verificato:** [Cs=2.272,Comb=3]

Geometria setti

Setto	Crit.	X	L	S	X90	L90	S90
		mm	cm	cm	mm	cm	cm

Setto	Crit.	X	L	S	X90	L90	S90
31	Criterio di verifica XLAM 0	0	387.0	12.1	0	420.0	12.1
		2100	387.0	12.1	1935	420.0	12.1
		4200	387.0	12.1	3870	420.0	12.1
32	Criterio di verifica XLAM 0	0	387.0	12.1	0	364.3	12.1
		1822	387.0	12.1	1935	364.3	12.1
		3643	387.0	12.1	3870	364.3	12.1
33	Criterio di verifica XLAM 0	0	167.0	12.1	0	180.0	12.1
		900	167.0	12.1	835	180.0	12.1
		1800	167.0	12.1	1670	180.0	12.1

Setto 31: origine (742.0,828.0,193.5), direzione (0.930183,0.367096,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	(8+9)-VIII-3	385	352	532	0.14	4.71	0.29	132.00	192.00	192.00	37
0	(8+9)-IV-1	611	188	1518	0.22	2.52	0.84	132.00	192.00	192.00	52
0	(8+9)-VI-4	-318	253	-1809	-0.11	3.38	-1.00	132.00	192.00	192.00	44
0	(8+9)-III-2	117	-522	1728	0.04	-6.98	0.95	132.00	192.00	192.00	24
0	(8+9)-IV-2	-605	-454	-9	-0.22	-6.07	-0.01	132.00	192.00	192.00	32
0	(8+9)-III-3	-366	507	-1250	-0.13	6.78	-0.69	132.00	192.00	192.00	26
0	(8+9)-VIII-1	582	275	1473	0.21	3.68	0.81	132.00	192.00	192.00	40
0	(8+9)-III-4	-730	314	-1708	-0.26	4.20	-0.94	132.00	192.00	192.00	37
0	(8+9)-VII-3	-271	218	-1100	-0.10	2.91	-0.61	132.00	192.00	192.00	55
0	(8+9)-VII-2	22	-232	1578	0.01	-3.11	0.87	132.00	192.00	192.00	48
0	(8+9)-I-2	271	-359	1484	0.10	-4.80	0.82	132.00	192.00	192.00	33
0	(8+9)-I-4	-577	477	-1952	-0.21	6.38	-1.08	132.00	192.00	192.00	26
0	(8+9)-IV-3	357	439	487	0.13	5.87	0.27	132.00	192.00	192.00	30
0	(8+9)-II-2	-92	89	-823	-0.03	1.18	-0.45	132.00	192.00	192.00	>100
0	(8+9)-IV-4	-860	-203	-1040	-0.31	-2.72	-0.57	132.00	192.00	192.00	58
0	(8+9)-II-4	-347	340	-1854	-0.12	4.54	-1.02	132.00	192.00	192.00	35
0	(8+9)-V-1	233	-203	2280	0.08	-2.71	1.26	132.00	192.00	192.00	47
0	(8+9)-VIII-2	-634	-367	-54	-0.23	-4.91	-0.03	132.00	192.00	192.00	39
0	(8+9)-V-2	176	-70	1333	0.06	-0.93	0.74	132.00	192.00	192.00	>100
0	(8+9)-I-1	328	-492	2430	0.12	-6.58	1.34	132.00	192.00	192.00	24
0	(8+9)-V-3	-425	55	-856	-0.15	0.73	-0.47	132.00	192.00	192.00	>100
0	(8+9)-II-1	98	-355	2331	0.03	-4.74	1.29	132.00	192.00	192.00	32
0	(8+9)-V-4	-482	188	-1802	-0.17	2.51	-0.99	132.00	192.00	192.00	55
0	(8+9)-III-1	482	-329	2186	0.17	-4.40	1.21	132.00	192.00	192.00	33
0	(8+9)-I-3	-520	344	-1006	-0.18	4.60	-0.56	132.00	192.00	192.00	37
0	(8+9)-II-3	-156	-104	1301	-0.06	-1.38	0.72	132.00	192.00	192.00	91
0	(8+9)-VIII-4	-831	-290	-995	-0.30	-3.88	-0.55	132.00	192.00	192.00	43
0	(8+9)-VI-1	69	-268	2286	0.02	-3.58	1.26	132.00	192.00	192.00	39
0	(8+9)-VI-2	-121	176	-868	-0.04	2.35	-0.48	132.00	192.00	192.00	68
0	(8+9)-VI-3	-128	-190	1346	-0.05	-2.55	0.74	132.00	192.00	192.00	58
2100	1	281	-20	-1336	0.10	-0.26	-0.74	79.20	115.20	115.20	>100
2100	2	467	-39	-2621	0.17	-0.52	-1.45	118.80	172.80	172.80	78
2100	3	467	-39	-2621	0.17	-0.52	-1.45	118.80	172.80	172.80	78
2100	4	281	-20	-1336	0.10	-0.26	-0.74	105.60	153.60	153.60	>100
2100	5	281	-20	-1336	0.10	-0.26	-0.74	105.60	153.60	153.60	>100
2100	6	281	-20	-1336	0.10	-0.26	-0.74	105.60	153.60	153.60	>100
2100	7	281	-20	-1336	0.10	-0.26	-0.74	105.60	153.60	153.60	>100
4200	(8+9)-VII-1	2363	-5	-2378	0.84	-0.06	-1.31	132.00	192.00	192.00	74
4200	(8+9)-VII-4	-2087	-1	2157	-0.74	-0.01	1.19	132.00	192.00	192.00	>100
Verifiche nella direzione secondaria											
0	(8+9)-V-1	-13614	-26	19421	-6.70	-0.74	13.65	132.00	192.00	192.00	13
0	(8+9)-II-1	-13541	-64	19423	-6.66	-1.81	13.65	132.00	192.00	192.00	12
0	(8+9)-VI-1	-13411	-75	18785	-6.60	-2.10	13.20	132.00	192.00	192.00	12
0	(8+9)-VIII-3	-12134	-117	7030	-5.97	-3.30	4.94	132.00	192.00	192.00	23
0	(8+9)-II-3	-12591	-72	11641	-6.19	-2.03	8.18	132.00	192.00	192.00	18
0	(8+9)-VII-4	-10975	88	-6656	-5.40	2.47	-4.68	132.00	192.00	192.00	26
0	(8+9)-II-4	-10873	109	-8232	-5.35	3.08	-5.79	132.00	192.00	192.00	21
0	(8+9)-VII-1	-13438	-43	17847	-6.61	-1.21	12.54	132.00	192.00	192.00	14
0	(8+9)-III-1	-13870	-9	19972	-6.82	-0.25	14.04	132.00	192.00	192.00	13

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-I-1	-14046	8	21547	-6.91	0.22	15.14	132.00	192.00	192.00	12
0	(8+9)-III-2	-13707	79	17160	-6.74	2.22	12.06	132.00	192.00	192.00	13
0	(8+9)-VI-3	-12721	-62	12278	-6.26	-1.74	8.63	132.00	192.00	192.00	18
0	(8+9)-V-4	-10799	71	-8230	-5.31	2.00	-5.78	132.00	192.00	192.00	24
0	(8+9)-III-4	-10543	54	-8782	-5.19	1.51	-6.17	132.00	192.00	192.00	25
0	(8+9)-VII-2	-13275	45	15034	-6.53	1.26	10.57	132.00	192.00	192.00	16
0	(8+9)-I-2	-13531	62	15585	-6.66	1.75	10.95	132.00	192.00	192.00	15
0	(8+9)-I-4	-10367	37	-10356	-5.10	1.04	-7.28	132.00	192.00	192.00	23
0	(8+9)-VIII-1	-12824	-130	13537	-6.31	-3.66	9.51	132.00	192.00	192.00	14
0	(8+9)-VI-4	-11003	120	-7594	-5.41	3.37	-5.34	132.00	192.00	192.00	22
0	(8+9)-IV-1	-12953	-120	14175	-6.37	-3.37	9.96	132.00	192.00	192.00	14
0	(8+9)-V-2	-13099	28	13459	-6.44	0.79	9.46	132.00	192.00	192.00	18
0	(8+9)-IV-3	-12004	-127	6392	-5.91	-3.59	4.49	132.00	192.00	192.00	23
1935	1	-17283	-18	9233	-8.50	-0.51	6.49	79.20	115.20	115.20	15
1935	2	-32397	-45	17459	-15.94	-1.28	12.27	118.80	172.80	172.80	12
1935	3	-32397	-45	17459	-15.94	-1.28	12.27	118.80	172.80	172.80	12
1935	4	-17283	-18	9233	-8.50	-0.51	6.49	105.60	153.60	153.60	21
1935	5	-17283	-18	9233	-8.50	-0.51	6.49	105.60	153.60	153.60	21
1935	6	-17283	-18	9233	-8.50	-0.51	6.49	105.60	153.60	153.60	21
1935	7	-17283	-18	9233	-8.50	-0.51	6.49	105.60	153.60	153.60	21
3870	(8+9)-VIII-4	-10922	-133	7880	-5.37	-3.74	5.54	132.00	192.00	192.00	20
3870	(8+9)-IV-4	-10847	-135	7821	-5.34	-3.79	5.50	132.00	192.00	192.00	20
3870	(8+9)-III-3	-9419	67	5589	-4.63	1.88	3.93	132.00	192.00	192.00	32
3870	(8+9)-II-2	-10675	-57	8426	-5.25	-1.61	5.92	132.00	192.00	192.00	25
3870	(8+9)-VII-3	-9669	73	5785	-4.76	2.05	4.07	132.00	192.00	192.00	31
3870	(8+9)-VI-2	-10599	-59	8367	-5.21	-1.66	5.88	132.00	192.00	192.00	25
3870	(8+9)-V-3	-9755	47	5616	-4.80	1.33	3.95	132.00	192.00	192.00	36
3870	(8+9)-VIII-2	-10886	-144	7803	-5.36	-4.06	5.48	132.00	192.00	192.00	20
3870	(8+9)-IV-2	-10961	-143	7861	-5.39	-4.01	5.52	132.00	192.00	192.00	20
3870	(8+9)-I-3	-9505	41	5420	-4.68	1.16	3.81	132.00	192.00	192.00	38

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
0	(8+9)-VI-4	-99	0.03	6.40	Si	>100
0	(8+9)-III-1	142	0.04	6.40	Si	>100
0	(8+9)-V-3	-111	0.03	6.40	Si	>100
0	(8+9)-III-2	349	0.09	6.40	Si	71
0	(8+9)-VIII-3	-386	0.10	6.40	Si	64
0	(8+9)-III-3	-354	0.09	6.40	Si	70
0	(8+9)-VIII-1	-311	0.08	6.40	Si	80
0	(8+9)-III-4	-147	0.04	6.40	Si	>100
0	(8+9)-VII-3	-232	0.06	6.40	Si	>100
0	(8+9)-IV-1	-274	0.07	6.40	Si	90
0	(8+9)-I-2	228	0.06	6.40	Si	>100
0	(8+9)-IV-2	418	0.11	6.40	Si	59
0	(8+9)-I-4	-268	0.07	6.40	Si	92
0	(8+9)-IV-3	-423	0.11	6.40	Si	58
0	(8+9)-VII-2	227	0.06	6.40	Si	>100
0	(8+9)-IV-4	269	0.07	6.40	Si	92
0	(8+9)-II-4	-135	0.04	6.40	Si	>100
0	(8+9)-V-1	141	0.04	6.40	Si	>100
0	(8+9)-VIII-2	381	0.10	6.40	Si	65
0	(8+9)-V-2	105	0.03	6.40	Si	>100
0	(8+9)-I-1	263	0.07	6.40	Si	94
0	(8+9)-II-1	130	0.03	6.40	Si	>100
0	(8+9)-V-4	-146	0.04	6.40	Si	>100
0	(8+9)-VIII-4	306	0.08	6.40	Si	81
0	(8+9)-I-3	-233	0.06	6.40	Si	>100
0	(8+9)-VII-1	19	0.00	6.40	Si	>100
0	(8+9)-VII-4	-24	0.01	6.40	Si	>100
0	(8+9)-VI-1	94	0.02	6.40	Si	>100
2100	(8+9)-II-3	27	0.01	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
2100	(8+9)-VI-3	25	0.01	6.40	Si	>100
4200	1	-22	0.01	3.84	Si	>100
4200	2	-43	0.01	5.76	Si	>100
4200	3	-43	0.01	5.76	Si	>100
4200	4	-22	0.01	5.12	Si	>100
4200	5	-22	0.01	5.12	Si	>100
4200	6	-22	0.01	5.12	Si	>100
4200	7	-22	0.01	5.12	Si	>100
4200	(8+9)-VI-2	-53	0.01	6.40	Si	>100
4200	(8+9)-II-2	-53	0.01	6.40	Si	>100
Verifiche nella direzione secondaria						
0	(8+9)-II-2	-77	0.04	6.40	Si	>100
0	(8+9)-VI-4	-82	0.04	6.40	Si	>100
0	(8+9)-VII-4	-41	0.02	6.40	Si	>100
0	(8+9)-II-4	-77	0.03	6.40	Si	>100
0	(8+9)-VI-3	37	0.02	6.40	Si	>100
0	(8+9)-V-4	-54	0.02	6.40	Si	>100
0	(8+9)-I-4	-34	0.02	6.40	Si	>100
0	(8+9)-VI-2	-71	0.03	6.40	Si	>100
0	(8+9)-II-3	43	0.02	6.40	Si	>100
1935	(8+9)-III-1	-19	0.01	6.40	Si	>100
1935	(8+9)-I-3	-8	0.00	6.40	Si	>100
3870	1	-40	0.02	3.84	Si	>100
3870	2	-102	0.05	5.76	Si	>100
3870	3	-102	0.05	5.76	Si	>100
3870	4	-40	0.02	5.12	Si	>100
3870	5	-40	0.02	5.12	Si	>100
3870	6	-40	0.02	5.12	Si	>100
3870	7	-40	0.02	5.12	Si	>100
3870	(8+9)-VIII-4	-157	0.07	6.40	Si	90
3870	(8+9)-V-3	22	0.01	6.40	Si	>100
3870	(8+9)-II-1	-44	0.02	6.40	Si	>100
3870	(8+9)-III-2	-96	0.04	6.40	Si	>100
3870	(8+9)-IV-2	-180	0.08	6.40	Si	78
3870	(8+9)-I-1	-55	0.02	6.40	Si	>100
3870	(8+9)-IV-4	-166	0.08	6.40	Si	85
3870	(8+9)-VII-1	-35	0.02	6.40	Si	>100
3870	(8+9)-V-2	-76	0.03	6.40	Si	>100
3870	(8+9)-VII-2	-123	0.06	6.40	Si	>100
3870	(8+9)-III-4	-46	0.02	6.40	Si	>100
3870	(8+9)-VII-3	69	0.03	6.40	Si	>100
3870	(8+9)-III-3	41	0.02	6.40	Si	>100
3870	(8+9)-I-2	-49	0.02	6.40	Si	>100
3870	(8+9)-VI-1	-52	0.02	6.40	Si	>100
3870	(8+9)-IV-3	126	0.06	6.40	Si	>100
3870	(8+9)-IV-1	111	0.05	6.40	Si	>100
3870	(8+9)-VIII-1	103	0.05	6.40	Si	>100
3870	(8+9)-VIII-2	-189	0.09	6.40	Si	75
3870	(8+9)-VIII-3	134	0.06	6.40	Si	>100
3870	(8+9)-V-1	-82	0.04	6.40	Si	>100

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	1	286	0.15	19.20	>100	0.04	12.00	>100	V	>100
0	4	286	0.15	25.60	>100	0.04	16.00	>100	V	>100
0	5	286	0.15	25.60	>100	0.04	16.00	>100	V	>100
0	6	286	0.15	25.60	>100	0.04	16.00	>100	V	>100
0	7	286	0.15	25.60	>100	0.04	16.00	>100	V	>100
2100	2	-180	-0.10	28.80	>100	-0.02	18.00	>100	V	>100
2100	3	-180	-0.10	28.80	>100	-0.02	18.00	>100	V	>100
2100	(8+9)-VIII-4	-6917	-3.69	32.00	8.7	-0.89	20.00	22	V	8.7
2100	(8+9)-IV-1	7320	3.91	32.00	8.2	0.95	20.00	21	V	8.2

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
2100	(8+9)-V-1	8215	4.39	32.00	7.3	1.06	20.00	19	V	7.3
2100	(8+9)-I-2	5659	3.02	32.00	11	0.73	20.00	27	V	11
2100	(8+9)-V-2	4637	2.48	32.00	13	0.60	20.00	33	V	13
2100	(8+9)-I-4	-9140	-4.88	32.00	6.6	-1.18	20.00	17	V	6.6
2100	(8+9)-V-3	-4541	-2.42	32.00	13	-0.59	20.00	34	V	13
2100	(8+9)-II-2	-3694	-1.97	32.00	16	-0.48	20.00	42	V	16
2100	(8+9)-V-4	-8119	-4.33	32.00	7.4	-1.05	20.00	19	V	7.4
2100	(8+9)-II-4	-8134	-4.34	32.00	7.4	-1.05	20.00	19	V	7.4
2100	(8+9)-VI-1	7924	4.23	32.00	7.6	1.02	20.00	20	V	7.6
2100	(8+9)-III-2	5932	3.17	32.00	10	0.77	20.00	26	V	10
2100	(8+9)-VI-2	-4001	-2.14	32.00	15	-0.52	20.00	39	V	15
2100	(8+9)-III-4	-8867	-4.73	32.00	6.8	-1.15	20.00	17	V	6.8
2100	(8+9)-VI-3	4097	2.19	32.00	15	0.53	20.00	38	V	15
2100	(8+9)-IV-2	-2784	-1.49	32.00	22	-0.36	20.00	56	V	22
2100	(8+9)-VI-4	-7828	-4.18	32.00	7.7	-1.01	20.00	20	V	7.7
2100	(8+9)-IV-4	-7224	-3.86	32.00	8.3	-0.93	20.00	21	V	8.3
2100	(8+9)-VII-1	7941	4.24	32.00	7.5	1.03	20.00	19	V	7.5
2100	(8+9)-II-1	8230	4.39	32.00	7.3	1.06	20.00	19	V	7.3
2100	(8+9)-VII-2	4910	2.62	32.00	12	0.63	20.00	32	V	12
2100	(8+9)-III-1	8963	4.79	32.00	6.7	1.16	20.00	17	V	6.7
2100	(8+9)-VII-3	-4814	-2.57	32.00	12	-0.62	20.00	32	V	12
2100	(8+9)-I-1	9236	4.93	32.00	6.5	1.19	20.00	17	V	6.5
2100	(8+9)-VII-4	-7845	-4.19	32.00	7.6	-1.01	20.00	20	V	7.6
2100	(8+9)-III-3	-5836	-3.12	32.00	10	-0.75	20.00	27	V	10
2100	(8+9)-IV-3	2880	1.54	32.00	21	0.37	20.00	54	V	21
2100	(8+9)-II-3	3791	2.02	32.00	16	0.49	20.00	41	V	16
2100	(8+9)-VIII-1	7013	3.74	32.00	8.5	0.91	20.00	22	V	8.5
2100	(8+9)-VIII-2	-3090	-1.65	32.00	19	-0.40	20.00	50	V	19
2100	(8+9)-VIII-3	3186	1.70	32.00	19	0.41	20.00	49	V	19
2100	(8+9)-I-3	-5563	-2.97	32.00	11	-0.72	20.00	28	V	11
Verifiche nella direzione secondaria										
1935	(8+9)-VIII-4	-8916	-4.39	32.00	7.3	-1.06	20.00	19	V	7.3
1935	(8+9)-VII-2	5388	2.65	32.00	12	0.64	20.00	31	V	12
1935	(8+9)-III-3	-7735	-3.81	32.00	8.4	-0.92	20.00	22	V	8.4
1935	(8+9)-IV-2	-3884	-1.91	32.00	17	-0.46	20.00	43	V	17
1935	(8+9)-III-4	-11388	-5.60	32.00	5.7	-1.36	20.00	15	V	5.7
1935	(8+9)-VIII-2	-4281	-2.11	32.00	15	-0.51	20.00	39	V	15
1935	(8+9)-IV-1	8293	4.08	32.00	7.8	0.99	20.00	20	V	7.8
1935	(8+9)-VII-4	-10062	-4.95	32.00	6.5	-1.20	20.00	17	V	6.5
1935	(8+9)-I-1	10700	5.26	32.00	6.1	1.27	20.00	16	V	6.1
1935	(8+9)-IV-3	2862	1.41	32.00	23	0.34	20.00	59	V	23
1935	(8+9)-I-3	-7402	-3.64	32.00	8.8	-0.88	20.00	23	V	8.8
1935	(8+9)-IV-4	-9314	-4.58	32.00	7.0	-1.11	20.00	18	V	7.0
1935	(8+9)-II-1	9403	4.63	32.00	6.9	1.12	20.00	18	V	6.9
1935	(8+9)-V-1	9374	4.61	32.00	6.9	1.12	20.00	18	V	6.9
1935	(8+9)-II-3	3972	1.95	32.00	16	0.47	20.00	42	V	16
1935	(8+9)-V-2	5055	2.49	32.00	13	0.60	20.00	33	V	13
1935	(8+9)-III-1	10367	5.10	32.00	6.3	1.23	20.00	16	V	6.3
1935	(8+9)-V-3	-6077	-2.99	32.00	11	-0.72	20.00	28	V	11
1935	(8+9)-VIII-3	3260	1.60	32.00	20	0.39	20.00	52	V	20
1935	(8+9)-V-4	-10395	-5.11	32.00	6.3	-1.24	20.00	16	V	6.3
1935	(8+9)-VII-3	-6410	-3.15	32.00	10	-0.76	20.00	26	V	10
1935	(8+9)-VI-1	9005	4.43	32.00	7.2	1.07	20.00	19	V	7.2
1935	(8+9)-I-4	-11721	-5.77	32.00	5.5	-1.40	20.00	14	V	5.5
1935	(8+9)-VI-2	-5391	-2.65	32.00	12	-0.64	20.00	31	V	12
1935	(8+9)-II-4	-10424	-5.13	32.00	6.2	-1.24	20.00	16	V	6.2
1935	(8+9)-VIII-1	7895	3.88	32.00	8.2	0.94	20.00	21	V	8.2
1935	(8+9)-I-2	6381	3.14	32.00	10	0.76	20.00	26	V	10
1935	(8+9)-II-2	-4994	-2.46	32.00	13	-0.59	20.00	34	V	13
1935	(8+9)-III-2	6714	3.30	32.00	9.7	0.80	20.00	25	V	9.7
1935	(8+9)-VI-3	4370	2.15	32.00	15	0.52	20.00	38	V	15
1935	(8+9)-VI-4	-10026	-4.93	32.00	6.5	-1.19	20.00	17	V	6.5
1935	(8+9)-VII-1	9041	4.45	32.00	7.2	1.08	20.00	19	V	7.2
3870	1	-1538	-0.76	19.20	25	-0.18	12.00	66	V	25

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
3870	2	-3266	-1.61	28.80	18	-0.39	18.00	46	V	18
3870	3	-3266	-1.61	28.80	18	-0.39	18.00	46	V	18
3870	4	-1538	-0.76	25.60	34	-0.18	16.00	87	V	34
3870	5	-1538	-0.76	25.60	34	-0.18	16.00	87	V	34
3870	6	-1538	-0.76	25.60	34	-0.18	16.00	87	V	34
3870	7	-1538	-0.76	25.60	34	-0.18	16.00	87	V	34

Setto 32: origine (1300.1,1048.3,193.5), direzione (0.930183,0.367096,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
1822	(8+9)-IV-3	-921	154	1022	-0.33	2.05	0.56	132.00	192.00	192.00	73
1822	(8+9)-VIII-3	-995	162	1118	-0.35	2.17	0.62	132.00	192.00	192.00	69
3643	1	2683	-106	-4632	0.96	-1.41	-2.56	79.20	115.20	115.20	22
3643	2	5595	-224	-9703	1.99	-3.00	-5.35	118.80	172.80	172.80	15
3643	3	5595	-224	-9703	1.99	-3.00	-5.35	118.80	172.80	172.80	15
3643	4	2683	-106	-4632	0.96	-1.41	-2.56	105.60	153.60	153.60	29
3643	5	2683	-106	-4632	0.96	-1.41	-2.56	105.60	153.60	153.60	29
3643	6	2683	-106	-4632	0.96	-1.41	-2.56	105.60	153.60	153.60	29
3643	7	2683	-106	-4632	0.96	-1.41	-2.56	105.60	153.60	153.60	29
3643	(8+9)-VIII-4	2405	-549	-3344	0.86	-7.35	-1.85	132.00	192.00	192.00	18
3643	(8+9)-IV-1	1189	412	-2991	0.42	5.50	-1.65	132.00	192.00	192.00	25
3643	(8+9)-V-2	2835	462	-5601	1.01	6.18	-3.09	132.00	192.00	192.00	18
3643	(8+9)-I-4	1556	-663	-872	0.55	-8.87	-0.48	132.00	192.00	192.00	19
3643	(8+9)-V-3	867	-608	-781	0.31	-8.12	-0.43	132.00	192.00	192.00	21
3643	(8+9)-II-2	2542	49	-3769	0.90	0.66	-2.08	132.00	192.00	192.00	47
3643	(8+9)-V-4	1199	-638	-716	0.43	-8.53	-0.40	132.00	192.00	192.00	20
3643	(8+9)-II-4	2265	-296	-2397	0.81	-3.96	-1.32	132.00	192.00	192.00	30
3643	(8+9)-VI-1	1543	143	-4031	0.55	1.92	-2.22	132.00	192.00	192.00	39
3643	(8+9)-III-2	2552	409	-5743	0.91	5.47	-3.17	132.00	192.00	192.00	19
3643	(8+9)-VI-2	2649	42	-3816	0.94	0.56	-2.11	132.00	192.00	192.00	48
3643	(8+9)-III-4	1630	-741	-1170	0.58	-9.91	-0.65	132.00	192.00	192.00	17
3643	(8+9)-VI-3	1053	-187	-2566	0.37	-2.50	-1.42	132.00	192.00	192.00	43
3643	(8+9)-IV-2	2789	-212	-4763	0.99	-2.83	-2.63	132.00	192.00	192.00	28
3643	(8+9)-VI-4	2158	-288	-2350	0.77	-3.86	-1.30	132.00	192.00	192.00	31
3643	(8+9)-IV-4	2512	-557	-3391	0.89	-7.45	-1.87	132.00	192.00	192.00	18
3643	(8+9)-VII-1	2429	571	-5368	0.86	7.64	-2.96	132.00	192.00	192.00	16
3643	(8+9)-II-1	1436	151	-3985	0.51	2.02	-2.20	132.00	192.00	192.00	39
3643	(8+9)-VII-2	2909	384	-5899	1.04	5.14	-3.26	132.00	192.00	192.00	19
3643	(8+9)-III-1	2072	596	-5212	0.74	7.97	-2.88	132.00	192.00	192.00	16
3643	(8+9)-VII-3	793	-529	-483	0.28	-7.08	-0.27	132.00	192.00	192.00	25
3643	(8+9)-I-3	1224	-633	-937	0.44	-8.46	-0.52	132.00	192.00	192.00	20
3643	(8+9)-VII-4	1273	-716	-1014	0.45	-9.58	-0.56	132.00	192.00	192.00	18
3643	(8+9)-III-3	1150	-554	-639	0.41	-7.41	-0.35	132.00	192.00	192.00	23
3643	(8+9)-I-2	2478	487	-5445	0.88	6.52	-3.00	132.00	192.00	192.00	18
3643	(8+9)-II-3	1160	-194	-2613	0.41	-2.60	-1.44	132.00	192.00	192.00	41
3643	(8+9)-VIII-1	1296	404	-3038	0.46	5.40	-1.68	132.00	192.00	192.00	25
3643	(8+9)-VIII-2	2896	-219	-4809	1.03	-2.93	-2.65	132.00	192.00	192.00	27
3643	(8+9)-I-1	2146	518	-5510	0.76	6.92	-3.04	132.00	192.00	192.00	17
3643	(8+9)-V-1	2503	493	-5666	0.89	6.59	-3.13	132.00	192.00	192.00	17
Verifiche nella direzione secondaria											
0	(8+9)-VIII-4	-10391	239	-13324	-5.89	7.76	-12.45	132.00	192.00	192.00	9.4
0	(8+9)-III-3	-10707	-21	-12002	-6.07	-0.68	-11.21	132.00	192.00	192.00	16
0	(8+9)-I-3	-10697	-8	-11499	-6.07	-0.25	-10.74	132.00	192.00	192.00	17
0	(8+9)-IV-2	-9795	247	-8056	-5.55	8.03	-7.53	132.00	192.00	192.00	12
0	(8+9)-I-4	-10912	77	-16336	-6.19	2.51	-15.26	132.00	192.00	192.00	11
0	(8+9)-VII-4	-10838	104	-14551	-6.15	3.36	-13.59	132.00	192.00	192.00	11
0	(8+9)-IV-4	-10410	235	-13709	-5.90	7.64	-12.81	132.00	192.00	192.00	9.3
0	(8+9)-VI-4	-10427	194	-15001	-5.91	6.31	-14.01	132.00	192.00	192.00	9.4
0	(8+9)-II-2	-9831	203	-9733	-5.58	6.58	-9.09	132.00	192.00	192.00	12
0	(8+9)-VIII-2	-9813	244	-8441	-5.57	7.90	-7.88	132.00	192.00	192.00	12
0	(8+9)-VII-3	-10645	-8	-10720	-6.04	-0.26	-10.01	132.00	192.00	192.00	18
0	(8+9)-VI-2	-9849	199	-10117	-5.59	6.45	-9.45	132.00	192.00	192.00	12

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-V-3	-10634	5	-10217	-6.03	0.17	-9.54	132.00	192.00	192.00	19
0	(8+9)-V-4	-10849	90	-15054	-6.15	2.93	-14.06	132.00	192.00	192.00	11
0	(8+9)-II-4	-10446	191	-15385	-5.92	6.18	-14.37	132.00	192.00	192.00	9.3
0	(8+9)-III-4	-10901	91	-15833	-6.18	2.94	-14.79	132.00	192.00	192.00	11
3870	1	-10860	-427	-1168	-6.16	-13.87	-1.09	79.20	115.20	115.20	7.5
3870	2	-21933	-904	-1604	-12.44	-29.34	-1.50	118.80	172.80	172.80	5.4
3870	3	-21933	-904	-1604	-12.44	-29.34	-1.50	118.80	172.80	172.80	5.4
3870	4	-10860	-427	-1168	-6.16	-13.87	-1.09	105.60	153.60	153.60	10
3870	5	-10860	-427	-1168	-6.16	-13.87	-1.09	105.60	153.60	153.60	10
3870	6	-10860	-427	-1168	-6.16	-13.87	-1.09	105.60	153.60	153.60	10
3870	7	-10860	-427	-1168	-6.16	-13.87	-1.09	105.60	153.60	153.60	10
3870	(8+9)-III-2	-8196	-327	-1988	-4.65	-10.60	-1.86	132.00	192.00	192.00	15
3870	(8+9)-VII-1	-8093	-298	-1987	-4.59	-9.67	-1.86	132.00	192.00	192.00	16
3870	(8+9)-V-1	-8150	-283	-2038	-4.62	-9.19	-1.90	132.00	192.00	192.00	17
3870	(8+9)-VII-2	-7982	-311	-1509	-4.53	-10.09	-1.41	132.00	192.00	192.00	17
3870	(8+9)-I-2	-8138	-342	-1937	-4.62	-11.08	-1.81	132.00	192.00	192.00	15
3870	(8+9)-II-3	-7624	-215	-1324	-4.32	-6.98	-1.24	132.00	192.00	192.00	23
3870	(8+9)-VI-1	-8023	-226	-2043	-4.55	-7.33	-1.91	132.00	192.00	192.00	21
3870	(8+9)-IV-1	-7896	-281	-2015	-4.48	-9.11	-1.88	132.00	192.00	192.00	17
3870	(8+9)-V-2	-7925	-326	-1458	-4.49	-10.58	-1.36	132.00	192.00	192.00	16
3870	(8+9)-I-1	-8364	-299	-2517	-4.74	-9.69	-2.35	132.00	192.00	192.00	16
3870	(8+9)-II-1	-8087	-231	-2187	-4.59	-7.49	-2.04	132.00	192.00	192.00	20
3870	(8+9)-IV-3	-7433	-265	-1152	-4.22	-8.60	-1.08	132.00	192.00	192.00	20
3870	(8+9)-VIII-1	-7832	-276	-1871	-4.44	-8.95	-1.75	132.00	192.00	192.00	18
3870	(8+9)-III-1	-8306	-314	-2465	-4.71	-10.18	-2.30	132.00	192.00	192.00	15
3870	(8+9)-VIII-3	-7498	-270	-1295	-4.25	-8.76	-1.21	132.00	192.00	192.00	19
3870	(8+9)-VI-3	-7688	-220	-1467	-4.36	-7.14	-1.37	132.00	192.00	192.00	22

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Ty kg	τ_d kg/cm ²	fvd kg/cm ²	RS	Cs
1822	(8+9)-II-3	-107	0.03	6.40	Si	>100
1822	(8+9)-VI-1	-105	0.03	6.40	Si	>100
1822	(8+9)-VIII-1	-199	0.05	6.40	Si	>100
1822	(8+9)-VII-1	-106	0.03	6.40	Si	>100
1822	(8+9)-VI-3	-112	0.03	6.40	Si	>100
1822	(8+9)-VIII-2	43	0.01	6.40	Si	>100
1822	(8+9)-V-2	-61	0.02	6.40	Si	>100
1822	(8+9)-IV-2	37	0.01	6.40	Si	>100
1822	(8+9)-IV-1	-205	0.05	6.40	Si	>100
3643	1	-179	0.05	3.84	Si	83
3643	2	-374	0.10	5.76	Si	60
3643	3	-374	0.10	5.76	Si	60
3643	4	-179	0.05	5.12	Si	>100
3643	5	-179	0.05	5.12	Si	>100
3643	6	-179	0.05	5.12	Si	>100
3643	7	-179	0.05	5.12	Si	>100
3643	(8+9)-VIII-4	-143	0.04	6.40	Si	>100
3643	(8+9)-I-4	-582	0.15	6.40	Si	42
3643	(8+9)-VI-2	-232	0.06	6.40	Si	>100
3643	(8+9)-III-3	-544	0.14	6.40	Si	45
3643	(8+9)-II-4	-412	0.11	6.40	Si	60
3643	(8+9)-I-2	236	0.06	6.40	Si	>100
3643	(8+9)-VI-4	-346	0.09	6.40	Si	71
3643	(8+9)-IV-3	-283	0.07	6.40	Si	87
3643	(8+9)-I-3	-483	0.12	6.40	Si	51
3643	(8+9)-V-1	117	0.03	6.40	Si	>100
3643	(8+9)-VII-2	78	0.02	6.40	Si	>100
3643	(8+9)-V-3	-264	0.07	6.40	Si	94
3643	(8+9)-VII-3	-325	0.08	6.40	Si	76
3643	(8+9)-III-1	275	0.07	6.40	Si	90
3643	(8+9)-VII-4	-302	0.08	6.40	Si	82
3643	(8+9)-III-2	297	0.08	6.40	Si	83

X	Comb.	Ty	τ_d	fvd	RS	Cs
3643	(8+9)-V-4	-363	0.09	6.40	Si	68
3643	(8+9)-III-4	-521	0.13	6.40	Si	47
3643	(8+9)-IV-4	-209	0.05	6.40	Si	>100
3643	(8+9)-II-2	-166	0.04	6.40	Si	>100
3643	(8+9)-II-1	165	0.04	6.40	Si	>100
3643	(8+9)-VIII-3	-218	0.06	6.40	Si	>100
3643	(8+9)-I-1	336	0.09	6.40	Si	74
Verifiche nella direzione secondaria						
1935	(8+9)-VIII-4	-321	0.17	6.40	Si	38
1935	(8+9)-IV-2	-333	0.17	6.40	Si	37
1935	(8+9)-VIII-2	-330	0.17	6.40	Si	37
1935	(8+9)-VII-2	-152	0.08	6.40	Si	81
1935	(8+9)-IV-4	-317	0.17	6.40	Si	39
3870	1	-464	0.24	3.84	Si	16
3870	2	-971	0.51	5.76	Si	11
3870	3	-971	0.51	5.76	Si	11
3870	4	-464	0.24	5.12	Si	21
3870	5	-464	0.24	5.12	Si	21
3870	6	-464	0.24	5.12	Si	21
3870	7	-464	0.24	5.12	Si	21
3870	(8+9)-V-2	-293	0.15	6.40	Si	42
3870	(8+9)-I-4	-325	0.17	6.40	Si	38
3870	(8+9)-V-4	-370	0.19	6.40	Si	33
3870	(8+9)-II-3	-277	0.15	6.40	Si	44
3870	(8+9)-VI-1	-268	0.14	6.40	Si	46
3870	(8+9)-III-1	-466	0.24	6.40	Si	26
3870	(8+9)-VI-2	-348	0.18	6.40	Si	35
3870	(8+9)-III-3	-452	0.24	6.40	Si	27
3870	(8+9)-VI-3	-291	0.15	6.40	Si	42
3870	(8+9)-IV-1	-788	0.41	6.40	Si	16
3870	(8+9)-VI-4	-371	0.19	6.40	Si	33
3870	(8+9)-IV-3	-783	0.41	6.40	Si	16
3870	(8+9)-VII-1	-421	0.22	6.40	Si	29
3870	(8+9)-V-1	-269	0.14	6.40	Si	45
3870	(8+9)-I-2	-339	0.18	6.40	Si	36
3870	(8+9)-V-3	-346	0.18	6.40	Si	35
3870	(8+9)-VII-3	-498	0.26	6.40	Si	25
3870	(8+9)-III-2	-187	0.10	6.40	Si	65
3870	(8+9)-VII-4	-218	0.11	6.40	Si	56
3870	(8+9)-II-1	-281	0.15	6.40	Si	43
3870	(8+9)-II-4	-358	0.19	6.40	Si	34
3870	(8+9)-III-4	-173	0.09	6.40	Si	71
3870	(8+9)-I-3	-301	0.16	6.40	Si	41
3870	(8+9)-VIII-1	-774	0.41	6.40	Si	16
3870	(8+9)-I-1	-314	0.16	6.40	Si	39
3870	(8+9)-VIII-3	-797	0.42	6.40	Si	15
3870	(8+9)-II-2	-362	0.19	6.40	Si	34

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	1	3677	1.96	19.20	9.8	0.48	12.00	25	V	9.8
0	2	7057	3.77	28.80	7.6	0.91	18.00	20	V	7.6
0	3	7057	3.77	28.80	7.6	0.91	18.00	20	V	7.6
0	4	3677	1.96	25.60	13	0.48	16.00	34	V	13
0	5	3677	1.96	25.60	13	0.48	16.00	34	V	13
0	6	3677	1.96	25.60	13	0.48	16.00	34	V	13
0	7	3677	1.96	25.60	13	0.48	16.00	34	V	13
0	(8+9)-IV-3	3770	2.01	32.00	16	0.49	20.00	41	V	16
0	(8+9)-VII-2	6278	3.35	32.00	9.5	0.81	20.00	25	V	9.5
0	(8+9)-II-3	5797	3.09	32.00	10	0.75	20.00	27	V	10
0	(8+9)-VI-3	6037	3.22	32.00	9.9	0.78	20.00	26	V	9.9
0	(8+9)-II-1	9048	4.83	32.00	6.6	1.17	20.00	17	V	6.6

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
0	(8+9)-VI-1	8808	4.70	32.00	6.8	1.14	20.00	18	V	6.8
0	(8+9)-VIII-3	4010	2.14	32.00	15	0.52	20.00	39	V	15
0	(8+9)-V-2	5670	3.03	32.00	11	0.73	20.00	27	V	11
0	(8+9)-V-1	8610	4.60	32.00	7.0	1.11	20.00	18	V	7.0
0	(8+9)-III-2	7079	3.78	32.00	8.5	0.91	20.00	22	V	8.5
0	(8+9)-I-2	6471	3.45	32.00	9.3	0.84	20.00	24	V	9.3
1822	(8+9)-VIII-4	-5680	-3.03	32.00	11	-0.73	20.00	27	V	11
1822	(8+9)-IV-1	7554	4.03	32.00	7.9	0.98	20.00	20	V	7.9
1822	(8+9)-I-4	-7905	-4.22	32.00	7.6	-1.02	20.00	20	V	7.6
1822	(8+9)-III-4	-7665	-4.09	32.00	7.8	-0.99	20.00	20	V	7.8
1822	(8+9)-VI-4	-6479	-3.46	32.00	9.3	-0.84	20.00	24	V	9.3
1822	(8+9)-VII-1	8208	4.38	32.00	7.3	1.06	20.00	19	V	7.3
1822	(8+9)-III-1	9231	4.93	32.00	6.5	1.19	20.00	17	V	6.5
1822	(8+9)-VIII-2	-2063	-1.10	32.00	29	-0.27	20.00	75	V	29
1822	(8+9)-II-4	-6786	-3.62	32.00	8.8	-0.88	20.00	23	V	8.8
1822	(8+9)-VIII-1	7247	3.87	32.00	8.3	0.94	20.00	21	V	8.3
1822	(8+9)-V-4	-6881	-3.67	32.00	8.7	-0.89	20.00	22	V	8.7
1822	(8+9)-IV-2	-1756	-0.94	32.00	34	-0.23	20.00	88	V	34
1822	(8+9)-IV-4	-5987	-3.20	32.00	10	-0.77	20.00	26	V	10
1822	(8+9)-VI-2	-2862	-1.53	32.00	21	-0.37	20.00	54	V	21
1822	(8+9)-II-2	-2555	-1.36	32.00	23	-0.33	20.00	61	V	23
1822	(8+9)-I-1	9471	5.06	32.00	6.3	1.22	20.00	16	V	6.3
1822	(8+9)-VII-4	-6642	-3.55	32.00	9.0	-0.86	20.00	23	V	9.0
3643	(8+9)-III-3	-5495	-2.93	32.00	11	-0.71	20.00	28	V	11
3643	(8+9)-I-3	-4802	-2.56	32.00	12	-0.62	20.00	32	V	12
3643	(8+9)-VII-3	-4697	-2.51	32.00	13	-0.61	20.00	33	V	13
3643	(8+9)-V-3	-4004	-2.14	32.00	15	-0.52	20.00	39	V	15
Verifiche nella direzione secondaria										
0	(8+9)-VIII-4	-6234	-3.54	32.00	9.1	-0.86	20.00	23	V	9.1
0	(8+9)-IV-2	-2169	-1.23	32.00	26	-0.30	20.00	67	V	26
0	(8+9)-VIII-3	3663	2.08	32.00	15	0.50	20.00	40	V	15
0	(8+9)-VIII-2	-2484	-1.41	32.00	23	-0.34	20.00	59	V	23
0	(8+9)-VIII-1	7414	4.20	32.00	7.6	1.02	20.00	20	V	7.6
0	(8+9)-IV-4	-6550	-3.71	32.00	8.6	-0.90	20.00	22	V	8.6
0	(8+9)-IV-3	3348	1.90	32.00	17	0.46	20.00	44	V	17
0	(8+9)-IV-1	7729	4.38	32.00	7.3	1.06	20.00	19	V	7.3
1935	(8+9)-VII-2	5719	3.24	32.00	9.9	0.78	20.00	25	V	9.9
1935	(8+9)-III-3	-5562	-3.15	32.00	10	-0.76	20.00	26	V	10
1935	(8+9)-VII-3	-4497	-2.55	32.00	13	-0.62	20.00	32	V	13
1935	(8+9)-I-3	-5164	-2.93	32.00	11	-0.71	20.00	28	V	11
1935	(8+9)-VII-4	-7207	-4.09	32.00	7.8	-0.99	20.00	20	V	7.8
1935	(8+9)-II-1	8712	4.94	32.00	6.5	1.20	20.00	17	V	6.5
1935	(8+9)-V-1	8827	5.01	32.00	6.4	1.21	20.00	17	V	6.4
1935	(8+9)-II-3	4195	2.38	32.00	13	0.58	20.00	35	V	13
1935	(8+9)-V-2	5322	3.02	32.00	11	0.73	20.00	27	V	11
1935	(8+9)-III-1	9495	5.38	32.00	5.9	1.30	20.00	15	V	5.9
1935	(8+9)-V-3	-4099	-2.32	32.00	14	-0.56	20.00	36	V	14
1935	(8+9)-I-2	6387	3.62	32.00	8.8	0.88	20.00	23	V	8.8
1935	(8+9)-V-4	-7605	-4.31	32.00	7.4	-1.04	20.00	19	V	7.4
1935	(8+9)-I-1	9892	5.61	32.00	5.7	1.36	20.00	15	V	5.7
1935	(8+9)-VI-1	8392	4.76	32.00	6.7	1.15	20.00	17	V	6.7
1935	(8+9)-I-4	-8670	-4.92	32.00	6.5	-1.19	20.00	17	V	6.5
1935	(8+9)-VI-2	-3292	-1.87	32.00	17	-0.45	20.00	44	V	17
1935	(8+9)-III-4	-8272	-4.69	32.00	6.8	-1.14	20.00	18	V	6.8
1935	(8+9)-II-4	-7489	-4.25	32.00	7.5	-1.03	20.00	19	V	7.5
1935	(8+9)-II-2	-2973	-1.69	32.00	19	-0.41	20.00	49	V	19
1935	(8+9)-III-2	6784	3.85	32.00	8.3	0.93	20.00	21	V	8.3
1935	(8+9)-VI-3	4514	2.56	32.00	12	0.62	20.00	32	V	12
1935	(8+9)-VI-4	-7170	-4.07	32.00	7.9	-0.98	20.00	20	V	7.9
1935	(8+9)-VII-1	8430	4.78	32.00	6.7	1.16	20.00	17	V	6.7
3870	1	2235	1.27	19.20	15	0.31	12.00	39	V	15
3870	2	4396	2.49	28.80	12	0.60	18.00	30	V	12
3870	3	4396	2.49	28.80	12	0.60	18.00	30	V	12
3870	4	2235	1.27	25.60	20	0.31	16.00	52	V	20

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
3870	5	2235	1.27	25.60	20	0.31	16.00	52	V	20
3870	6	2235	1.27	25.60	20	0.31	16.00	52	V	20
3870	7	2235	1.27	25.60	20	0.31	16.00	52	V	20

Setto 33: origine (1132.7,982.2,303.5), direzione (0.930183,0.367096,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	(8+9)-II-1	2834	12	1817	2.34	0.36	5.38	132.00	192.00	192.00	21
0	(8+9)-V-1	2892	-4	1820	2.39	-0.11	5.39	132.00	192.00	192.00	21
0	(8+9)-VII-1	2834	-6	1773	2.34	-0.18	5.25	132.00	192.00	192.00	22
0	(8+9)-VI-1	2711	6	1746	2.24	0.19	5.17	132.00	192.00	192.00	22
0	(8+9)-VIII-1	2515	-1	1589	2.07	-0.04	4.71	132.00	192.00	192.00	25
0	(8+9)-IV-1	2639	4	1660	2.18	0.13	4.92	132.00	192.00	192.00	23
0	(8+9)-III-1	3245	13	2009	2.68	0.40	5.95	132.00	192.00	192.00	19
0	(8+9)-I-1	3304	15	2056	2.72	0.47	6.09	132.00	192.00	192.00	18
1800	1	3017	2	-1359	2.49	0.06	-4.03	79.20	115.20	115.20	15
1800	2	5769	9	-2595	4.76	0.29	-7.69	118.80	172.80	172.80	12
1800	3	5769	9	-2595	4.76	0.29	-7.69	118.80	172.80	172.80	12
1800	4	3017	2	-1359	2.49	0.06	-4.03	105.60	153.60	153.60	20
1800	5	3017	2	-1359	2.49	0.06	-4.03	105.60	153.60	153.60	20
1800	6	3017	2	-1359	2.49	0.06	-4.03	105.60	153.60	153.60	20
1800	7	3017	2	-1359	2.49	0.06	-4.03	105.60	153.60	153.60	20
1800	(8+9)-VIII-4	3987	4	446	3.29	0.13	1.32	132.00	192.00	192.00	31
1800	(8+9)-V-2	970	-10	-1936	0.80	-0.32	-5.74	132.00	192.00	192.00	27
1800	(8+9)-I-3	3539	13	270	2.92	0.41	0.80	132.00	192.00	192.00	35
1800	(8+9)-VI-2	3361	-4	-92	2.77	-0.11	-0.27	132.00	192.00	192.00	43
1800	(8+9)-III-3	3646	13	357	3.01	0.40	1.06	132.00	192.00	192.00	33
1800	(8+9)-VI-3	788	6	-1772	0.65	0.20	-5.25	132.00	192.00	192.00	30
1800	(8+9)-III-2	503	-10	-2221	0.42	-0.32	-6.58	132.00	192.00	192.00	26
1800	(8+9)-VI-4	4344	3	735	3.58	0.10	2.18	132.00	192.00	192.00	26
1800	(8+9)-IV-3	1254	5	-1424	1.03	0.16	-4.22	132.00	192.00	192.00	33
1800	(8+9)-I-2	611	-11	-2135	0.50	-0.33	-6.33	132.00	192.00	192.00	26
1800	(8+9)-II-4	4452	3	795	3.67	0.10	2.36	132.00	192.00	192.00	25
1800	(8+9)-VII-2	863	-10	-2023	0.71	-0.31	-5.99	132.00	192.00	192.00	26
1800	(8+9)-V-3	3179	13	71	2.62	0.40	0.21	132.00	192.00	192.00	43
1800	(8+9)-VII-3	3287	13	158	2.71	0.39	0.47	132.00	192.00	192.00	40
1800	(8+9)-II-2	3253	-4	-152	2.68	-0.11	-0.45	132.00	192.00	192.00	43
1800	(8+9)-VII-4	4139	12	737	3.41	0.39	2.18	132.00	192.00	192.00	25
1800	(8+9)-II-3	896	6	-1713	0.74	0.20	-5.08	132.00	192.00	192.00	30
1800	(8+9)-V-4	4246	12	824	3.50	0.37	2.44	132.00	192.00	192.00	24
1800	(8+9)-III-4	4499	13	936	3.71	0.40	2.77	132.00	192.00	192.00	22
1800	(8+9)-IV-4	4094	4	506	3.38	0.14	1.50	132.00	192.00	192.00	29
1800	(8+9)-I-4	4606	12	1022	3.80	0.38	3.03	132.00	192.00	192.00	21
1800	(8+9)-VIII-2	3004	-2	-381	2.48	-0.07	-1.13	132.00	192.00	192.00	40
1800	(8+9)-VIII-3	1146	5	-1483	0.95	0.16	-4.40	132.00	192.00	192.00	32
1800	(8+9)-IV-2	2896	-2	-441	2.39	-0.08	-1.31	132.00	192.00	192.00	40
Verifiche nella direzione secondaria											
0	(8+9)-VIII-4	-5894	-37	-3389	-6.76	-2.40	-12.97	132.00	192.00	192.00	12
0	(8+9)-IV-4	-5851	-37	-3500	-6.72	-2.41	-13.39	132.00	192.00	192.00	12
0	(8+9)-III-4	-5630	-19	-3856	-6.46	-1.23	-14.75	132.00	192.00	192.00	12
0	(8+9)-II-4	-6038	-30	-3798	-6.93	-1.97	-14.53	132.00	192.00	192.00	11
0	(8+9)-VII-4	-5773	-19	-3487	-6.63	-1.22	-13.34	132.00	192.00	192.00	13
0	(8+9)-V-4	-5829	-17	-3577	-6.69	-1.09	-13.68	132.00	192.00	192.00	13
0	(8+9)-VI-4	-6081	-30	-3687	-6.98	-1.97	-14.11	132.00	192.00	192.00	12
0	(8+9)-I-4	-5686	-17	-3946	-6.53	-1.10	-15.10	132.00	192.00	192.00	12
835	(8+9)-VI-1	-5419	-9	3582	-6.22	-0.61	13.71	132.00	192.00	192.00	13
835	(8+9)-IV-2	-6467	-103	1656	-7.42	-6.77	6.34	132.00	192.00	192.00	14
835	(8+9)-III-2	-5997	-58	3406	-6.88	-3.83	13.03	132.00	192.00	192.00	11
835	(8+9)-I-2	-5835	-38	3181	-6.70	-2.50	12.17	132.00	192.00	192.00	13
835	(8+9)-V-2	-5752	-29	2892	-6.60	-1.90	11.07	132.00	192.00	192.00	15
835	(8+9)-II-1	-5444	-12	3669	-6.25	-0.79	14.04	132.00	192.00	192.00	13
835	(8+9)-VIII-2	-6442	-100	1569	-7.39	-6.59	6.00	132.00	192.00	192.00	15

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
835	(8+9)-III-1	-5529	-11	3785	-6.35	-0.71	14.48	132.00	192.00	192.00	12
835	(8+9)-I-1	-5691	-31	4009	-6.53	-2.04	15.34	132.00	192.00	192.00	11
835	(8+9)-VII-1	-5445	-2	3496	-6.25	-0.11	13.38	132.00	192.00	192.00	14
835	(8+9)-VIII-1	-4880	58	2833	-5.60	3.83	10.84	132.00	192.00	192.00	13
835	(8+9)-IV-1	-4905	56	2920	-5.63	3.65	11.17	132.00	192.00	192.00	13
835	(8+9)-VII-2	-5914	-49	3117	-6.79	-3.24	11.93	132.00	192.00	192.00	12
835	(8+9)-V-1	-5607	-22	3721	-6.44	-1.45	14.24	132.00	192.00	192.00	12
1670	1	-8475	38	3686	-9.73	2.47	14.10	79.20	115.20	115.20	6.6
1670	2	-16235	51	7068	-18.64	3.33	27.04	118.80	172.80	172.80	5.3
1670	3	-16235	51	7068	-18.64	3.33	27.04	118.80	172.80	172.80	5.3
1670	4	-8475	38	3686	-9.73	2.47	14.10	105.60	153.60	153.60	8.9
1670	5	-8475	38	3686	-9.73	2.47	14.10	105.60	153.60	153.60	8.9
1670	6	-8475	38	3686	-9.73	2.47	14.10	105.60	153.60	153.60	8.9
1670	7	-8475	38	3686	-9.73	2.47	14.10	105.60	153.60	153.60	8.9
1670	(8+9)-IV-3	-5214	70	2020	-5.99	4.58	7.73	132.00	192.00	192.00	15
1670	(8+9)-II-3	-4974	65	1801	-5.71	4.25	6.89	132.00	192.00	192.00	17
1670	(8+9)-VI-2	-6617	-6	3241	-7.59	-0.36	12.40	132.00	192.00	192.00	15
1670	(8+9)-II-2	-6671	-13	3260	-7.66	-0.88	12.47	132.00	192.00	192.00	14
1670	(8+9)-VII-3	-5833	38	2851	-6.70	2.47	10.91	132.00	192.00	192.00	14
1670	(8+9)-I-3	-5579	63	2722	-6.40	4.11	10.41	132.00	192.00	192.00	13
1670	(8+9)-V-3	-5761	36	2785	-6.61	2.38	10.66	132.00	192.00	192.00	14
1670	(8+9)-III-3	-5652	64	2788	-6.49	4.20	10.67	132.00	192.00	192.00	13
1670	(8+9)-VIII-3	-5269	62	2039	-6.05	4.06	7.80	132.00	192.00	192.00	16
1670	(8+9)-VI-3	-5029	57	1820	-5.77	3.73	6.96	132.00	192.00	192.00	18

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
0	(8+9)-III-2	-20	0.01	6.40	Si	>100
0	(8+9)-I-2	-19	0.01	6.40	Si	>100
1800	1	41	0.02	3.84	Si	>100
1800	2	73	0.04	5.76	Si	>100
1800	3	73	0.04	5.76	Si	>100
1800	4	41	0.02	5.12	Si	>100
1800	5	41	0.02	5.12	Si	>100
1800	6	41	0.02	5.12	Si	>100
1800	7	41	0.02	5.12	Si	>100
1800	(8+9)-IV-4	35	0.02	6.40	Si	>100
1800	(8+9)-VI-1	29	0.02	6.40	Si	>100
1800	(8+9)-I-4	38	0.02	6.40	Si	>100
1800	(8+9)-VI-2	25	0.01	6.40	Si	>100
1800	(8+9)-II-2	23	0.01	6.40	Si	>100
1800	(8+9)-VI-3	32	0.02	6.40	Si	>100
1800	(8+9)-II-4	29	0.02	6.40	Si	>100
1800	(8+9)-VI-4	27	0.02	6.40	Si	>100
1800	(8+9)-I-3	39	0.02	6.40	Si	>100
1800	(8+9)-VII-1	23	0.01	6.40	Si	>100
1800	(8+9)-III-4	40	0.02	6.40	Si	>100
1800	(8+9)-VII-2	25	0.02	6.40	Si	>100
1800	(8+9)-IV-2	29	0.02	6.40	Si	>100
1800	(8+9)-VII-3	31	0.02	6.40	Si	>100
1800	(8+9)-I-1	19	0.01	6.40	Si	>100
1800	(8+9)-VII-4	34	0.02	6.40	Si	>100
1800	(8+9)-V-2	23	0.01	6.40	Si	>100
1800	(8+9)-VIII-1	23	0.01	6.40	Si	>100
1800	(8+9)-V-4	32	0.02	6.40	Si	>100
1800	(8+9)-VIII-2	31	0.02	6.40	Si	>100
1800	(8+9)-II-3	34	0.02	6.40	Si	>100
1800	(8+9)-VIII-3	26	0.02	6.40	Si	>100
1800	(8+9)-III-3	38	0.02	6.40	Si	>100
1800	(8+9)-VIII-4	33	0.02	6.40	Si	>100
1800	(8+9)-IV-3	28	0.02	6.40	Si	>100
1800	(8+9)-V-3	33	0.02	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
1800	(8+9)-II-1	28	0.02	6.40	Si	>100
1800	(8+9)-III-1	17	0.01	6.40	Si	>100
1800	(8+9)-IV-1	22	0.01	6.40	Si	>100
1800	(8+9)-V-1	25	0.01	6.40	Si	>100
Verifiche nella direzione secondaria						
0	(8+9)-II-2	-52	0.06	6.40	Si	>100
0	(8+9)-VI-4	-48	0.05	6.40	Si	>100
0	(8+9)-VI-2	-52	0.06	6.40	Si	>100
0	(8+9)-II-4	-48	0.05	6.40	Si	>100
1670	1	66	0.07	3.84	Si	55
1670	2	121	0.13	5.76	Si	45
1670	3	121	0.13	5.76	Si	45
1670	4	66	0.07	5.12	Si	73
1670	5	66	0.07	5.12	Si	73
1670	6	66	0.07	5.12	Si	73
1670	7	66	0.07	5.12	Si	73
1670	(8+9)-VIII-4	47	0.05	6.40	Si	>100
1670	(8+9)-IV-4	47	0.05	6.40	Si	>100
1670	(8+9)-V-3	47	0.05	6.40	Si	>100
1670	(8+9)-II-1	62	0.07	6.40	Si	98
1670	(8+9)-V-4	38	0.04	6.40	Si	>100
1670	(8+9)-I-4	37	0.04	6.40	Si	>100
1670	(8+9)-VI-1	61	0.06	6.40	Si	99
1670	(8+9)-III-2	49	0.05	6.40	Si	>100
1670	(8+9)-I-2	44	0.05	6.40	Si	>100
1670	(8+9)-III-4	43	0.05	6.40	Si	>100
1670	(8+9)-VI-3	60	0.06	6.40	Si	>100
1670	(8+9)-IV-2	49	0.05	6.40	Si	>100
1670	(8+9)-I-1	53	0.06	6.40	Si	>100
1670	(8+9)-I-3	46	0.05	6.40	Si	>100
1670	(8+9)-VII-1	47	0.05	6.40	Si	>100
1670	(8+9)-V-2	43	0.05	6.40	Si	>100
1670	(8+9)-VII-2	48	0.05	6.40	Si	>100
1670	(8+9)-III-1	48	0.05	6.40	Si	>100
1670	(8+9)-VII-3	42	0.04	6.40	Si	>100
1670	(8+9)-IV-1	44	0.05	6.40	Si	>100
1670	(8+9)-VII-4	44	0.05	6.40	Si	>100
1670	(8+9)-III-3	41	0.04	6.40	Si	>100
1670	(8+9)-IV-3	42	0.04	6.40	Si	>100
1670	(8+9)-II-3	60	0.06	6.40	Si	>100
1670	(8+9)-VIII-1	44	0.05	6.40	Si	>100
1670	(8+9)-VIII-2	48	0.05	6.40	Si	>100
1670	(8+9)-VIII-3	42	0.04	6.40	Si	>100
1670	(8+9)-V-1	52	0.06	6.40	Si	>100

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	(8+9)-III-3	-4272	-5.29	32.00	6.1	-1.28	20.00	16	V	6.1
0	(8+9)-IV-4	-4725	-5.85	32.00	5.5	-1.41	20.00	14	V	5.5
0	(8+9)-VIII-4	-4562	-5.64	32.00	5.7	-1.37	20.00	15	V	5.7
0	(8+9)-I-3	-4093	-5.06	32.00	6.3	-1.23	20.00	16	V	6.3
0	(8+9)-VII-4	-5109	-6.32	32.00	5.1	-1.53	20.00	13	V	5.1
0	(8+9)-I-4	-5832	-7.21	32.00	4.4	-1.75	20.00	11	V	4.4
0	(8+9)-VI-4	-5158	-6.38	32.00	5.0	-1.54	20.00	13	V	5.0
0	(8+9)-V-4	-5288	-6.54	32.00	4.9	-1.58	20.00	13	V	4.9
0	(8+9)-VIII-2	-2711	-3.35	32.00	9.5	-0.81	20.00	25	V	9.5
0	(8+9)-VII-3	-3728	-4.61	32.00	6.9	-1.12	20.00	18	V	6.9
0	(8+9)-VI-2	-3307	-4.09	32.00	7.8	-0.99	20.00	20	V	7.8
0	(8+9)-V-3	-3550	-4.39	32.00	7.3	-1.06	20.00	19	V	7.3
0	(8+9)-II-2	-3144	-3.89	32.00	8.2	-0.94	20.00	21	V	8.2
0	(8+9)-III-4	-5653	-6.99	32.00	4.6	-1.69	20.00	12	V	4.6
0	(8+9)-II-4	-5321	-6.58	32.00	4.9	-1.59	20.00	13	V	4.9

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
1800	1	5386	6.66	19.20	2.9	1.61	12.00	7.4	V	2.9
1800	2	10248	12.68	28.80	2.3	3.07	18.00	5.9	V	2.3
1800	3	10248	12.68	28.80	2.3	3.07	18.00	5.9	V	2.3
1800	4	5386	6.66	25.60	3.8	1.61	16.00	9.9	V	3.8
1800	5	5386	6.66	25.60	3.8	1.61	16.00	9.9	V	3.8
1800	6	5386	6.66	25.60	3.8	1.61	16.00	9.9	V	3.8
1800	7	5386	6.66	25.60	3.8	1.61	16.00	9.9	V	3.8
1800	(8+9)-IV-1	6929	8.57	32.00	3.7	2.07	20.00	9.6	V	3.7
1800	(8+9)-VI-1	7688	9.51	32.00	3.4	2.30	20.00	8.7	V	3.4
1800	(8+9)-III-2	6674	8.26	32.00	3.9	2.00	20.00	10	V	3.9
1800	(8+9)-VII-1	7385	9.14	32.00	3.5	2.21	20.00	9.0	V	3.5
1800	(8+9)-V-2	5821	7.20	32.00	4.4	1.74	20.00	11	V	4.4
1800	(8+9)-VII-2	6101	7.55	32.00	4.2	1.83	20.00	11	V	4.2
1800	(8+9)-V-1	7664	9.48	32.00	3.4	2.29	20.00	8.7	V	3.4
1800	(8+9)-II-1	7860	9.72	32.00	3.3	2.35	20.00	8.5	V	3.3
1800	(8+9)-IV-3	4762	5.89	32.00	5.4	1.43	20.00	14	V	5.4
1800	(8+9)-II-3	5694	7.04	32.00	4.5	1.70	20.00	12	V	4.5
1800	(8+9)-I-2	6395	7.91	32.00	4.0	1.91	20.00	10	V	4.0
1800	(8+9)-VI-3	5865	7.26	32.00	4.4	1.76	20.00	11	V	4.4
1800	(8+9)-I-1	8237	10.19	32.00	3.1	2.47	20.00	8.1	V	3.1
1800	(8+9)-VIII-1	6757	8.36	32.00	3.8	2.02	20.00	9.9	V	3.8
1800	(8+9)-III-1	7958	9.85	32.00	3.3	2.38	20.00	8.4	V	3.3
1800	(8+9)-VIII-3	4934	6.10	32.00	5.2	1.48	20.00	14	V	5.2
1800	(8+9)-IV-2	2649	3.28	32.00	9.8	0.79	20.00	25	V	9.8
Verifiche nella direzione secondaria										
0	1	225	0.26	19.20	74	0.06	12.00	>100	V	74
0	2	433	0.50	28.80	58	0.12	18.00	>100	V	58
0	3	433	0.50	28.80	58	0.12	18.00	>100	V	58
0	4	225	0.26	25.60	99	0.06	16.00	>100	V	99
0	5	225	0.26	25.60	99	0.06	16.00	>100	V	99
0	6	225	0.26	25.60	99	0.06	16.00	>100	V	99
0	7	225	0.26	25.60	99	0.06	16.00	>100	V	99
835	(8+9)-VIII-4	-4559	-5.23	32.00	6.1	-1.27	20.00	16	V	6.1
835	(8+9)-IV-2	-1786	-2.05	32.00	16	-0.50	20.00	40	V	16
835	(8+9)-V-1	5492	6.30	32.00	5.1	1.53	20.00	13	V	5.1
835	(8+9)-I-2	3904	4.48	32.00	7.1	1.08	20.00	18	V	7.1
835	(8+9)-V-2	3136	3.60	32.00	8.9	0.87	20.00	23	V	8.9
835	(8+9)-VII-1	5323	6.11	32.00	5.2	1.48	20.00	14	V	5.2
835	(8+9)-IV-3	1936	2.22	32.00	14	0.54	20.00	37	V	14
835	(8+9)-I-4	-6110	-7.01	32.00	4.6	-1.70	20.00	12	V	4.6
835	(8+9)-IV-4	-4790	-5.50	32.00	5.8	-1.33	20.00	15	V	5.8
835	(8+9)-VIII-3	2167	2.49	32.00	13	0.60	20.00	33	V	13
835	(8+9)-VIII-1	4710	5.41	32.00	5.9	1.31	20.00	15	V	5.9
835	(8+9)-III-2	4073	4.68	32.00	6.8	1.13	20.00	18	V	6.8
835	(8+9)-II-1	5504	6.32	32.00	5.1	1.53	20.00	13	V	5.1
835	(8+9)-III-4	-5941	-6.82	32.00	4.7	-1.65	20.00	12	V	4.7
835	(8+9)-I-1	6260	7.19	32.00	4.5	1.74	20.00	12	V	4.5
835	(8+9)-VII-4	-5172	-5.94	32.00	5.4	-1.44	20.00	14	V	5.4
835	(8+9)-III-1	6091	6.99	32.00	4.6	1.69	20.00	12	V	4.6
835	(8+9)-IV-1	4940	5.67	32.00	5.6	1.37	20.00	15	V	5.6
835	(8+9)-II-3	2499	2.87	32.00	11	0.69	20.00	29	V	11
835	(8+9)-VIII-2	-2016	-2.31	32.00	14	-0.56	20.00	36	V	14
835	(8+9)-VI-1	5273	6.05	32.00	5.3	1.46	20.00	14	V	5.3
835	(8+9)-VII-2	3305	3.79	32.00	8.4	0.92	20.00	22	V	8.4
835	(8+9)-VI-3	2730	3.13	32.00	10	0.76	20.00	26	V	10
1670	(8+9)-V-3	-3064	-3.52	32.00	9.1	-0.85	20.00	23	V	9.1
1670	(8+9)-VI-4	-5166	-5.93	32.00	5.4	-1.44	20.00	14	V	5.4
1670	(8+9)-VI-2	-2689	-3.09	32.00	10	-0.75	20.00	27	V	10
1670	(8+9)-VII-3	-3272	-3.76	32.00	8.5	-0.91	20.00	22	V	8.5
1670	(8+9)-V-4	-5368	-6.16	32.00	5.2	-1.49	20.00	13	V	5.2
1670	(8+9)-I-3	-3778	-4.34	32.00	7.4	-1.05	20.00	19	V	7.4
1670	(8+9)-III-3	-3985	-4.57	32.00	7.0	-1.11	20.00	18	V	7.0
1670	(8+9)-II-4	-5380	-6.18	32.00	5.2	-1.49	20.00	13	V	5.2
1670	(8+9)-II-2	-2475	-2.84	32.00	11	-0.69	20.00	29	V	11

Verifiche a instabilità

Setto(X)	Comb.	k _{critc}	k _{critm}	λ _{relc}	λ _{relm}	σ _n	σ _{mx}	σ _{my}	ftd	fcd	fmd	Cs
(cm)						kg/cm q	kg/cm q	kg/cm q	kg/cm q	kg/cm q	kg/cm q	
31(0.0)	(8+9)-I-1	--	--	--	--	0.12	-6.58	1.34	132.00	192.00	192.00	24
32(364.3)	3	--	--	--	--	1.99	-3.00	-5.35	118.80	172.80	172.80	15
33(180.0)	3	--	--	--	--	4.76	0.29	-7.69	118.80	172.80	172.80	12

Parete Xlam 4 - Nodi: [6-21-109-13-12-11-10-9-8-104] - **Crit.Prog.** Criterio di verifica XLAM 0 - **Verificato:** [Cs=5.443,Comb=(8+9)-VII-4]

Geometria setti

Setto	Crit.	X	L	S	X90	L90	S90
		mm	cm	cm	mm	cm	cm
34	Criterio di verifica XLAM 0	0	387.0	12.1	0	1324.7	12.1
		6624	387.0	12.1	1935	1324.7	12.1
		13247	387.0	12.1	3870	1324.7	12.1

Setto 34: origine (366.0,1315.0,193.5), direzione (0.825849,0.563892,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	M _x	M _y	σ _n	σ _{mx}	σ _{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	
13247	1	531	-198	-796	0.19	-2.65	-0.44	79.20	115.20	115.20	34
13247	2	1087	-416	-1704	0.39	-5.56	-0.94	118.80	172.80	172.80	24
13247	3	1087	-416	-1704	0.39	-5.56	-0.94	118.80	172.80	172.80	24
13247	4	531	-198	-796	0.19	-2.65	-0.44	105.60	153.60	153.60	46
13247	5	531	-198	-796	0.19	-2.65	-0.44	105.60	153.60	153.60	46
13247	6	531	-198	-796	0.19	-2.65	-0.44	105.60	153.60	153.60	46
13247	7	531	-198	-796	0.19	-2.65	-0.44	105.60	153.60	153.60	46
13247	(8+9)-VIII-4	479	-83	923	0.17	-1.11	0.51	132.00	192.00	192.00	>100
13247	(8+9)-IV-1	255	-196	-1941	0.09	-2.62	-1.07	132.00	192.00	192.00	50
13247	(8+9)-V-1	-42	-105	-2576	-0.01	-1.40	-1.42	132.00	192.00	192.00	68
13247	(8+9)-I-2	-136	-72	-1805	-0.05	-0.97	-1.00	132.00	192.00	192.00	98
13247	(8+9)-V-2	-134	-54	-2046	-0.05	-0.72	-1.13	132.00	192.00	192.00	>100
13247	(8+9)-I-4	777	-150	1244	0.28	-2.01	0.69	132.00	192.00	192.00	62
13247	(8+9)-V-3	868	-219	955	0.31	-2.93	0.53	132.00	192.00	192.00	49
13247	(8+9)-II-2	75	-40	-119	0.03	-0.54	-0.07	132.00	192.00	192.00	>100
13247	(8+9)-V-4	775	-168	1485	0.28	-2.25	0.82	132.00	192.00	192.00	55
13247	(8+9)-II-4	349	-64	795	0.12	-0.85	0.44	132.00	192.00	192.00	>100
13247	(8+9)-VI-1	385	-204	-1959	0.14	-2.73	-1.08	132.00	192.00	192.00	48
13247	(8+9)-III-2	-97	-77	-1788	-0.03	-1.02	-0.99	132.00	192.00	192.00	96
13247	(8+9)-VI-2	76	-35	-191	0.03	-0.47	-0.11	132.00	192.00	192.00	>100
13247	(8+9)-III-4	816	-154	1260	0.29	-2.06	0.70	132.00	192.00	192.00	60
13247	(8+9)-VI-3	658	-238	-900	0.23	-3.18	-0.50	132.00	192.00	192.00	48
13247	(8+9)-IV-2	205	-54	-64	0.07	-0.72	-0.04	132.00	192.00	192.00	>100
13247	(8+9)-VI-4	349	-69	868	0.12	-0.92	0.48	132.00	192.00	192.00	>100
13247	(8+9)-IV-4	479	-78	850	0.17	-1.04	0.47	132.00	192.00	192.00	>100
13247	(8+9)-VII-1	-81	-101	-2592	-0.03	-1.35	-1.43	132.00	192.00	192.00	69
13247	(8+9)-II-1	385	-209	-1886	0.14	-2.80	-1.04	132.00	192.00	192.00	48
13247	(8+9)-VII-2	-95	-58	-2029	-0.03	-0.78	-1.12	132.00	192.00	192.00	>100
13247	(8+9)-III-1	-82	-119	-2351	-0.03	-1.59	-1.30	132.00	192.00	192.00	66
13247	(8+9)-VII-3	829	-215	938	0.30	-2.87	0.52	132.00	192.00	192.00	50
13247	(8+9)-I-1	-43	-123	-2335	-0.02	-1.65	-1.29	132.00	192.00	192.00	65
13247	(8+9)-VII-4	814	-172	1501	0.29	-2.30	0.83	132.00	192.00	192.00	54
13247	(8+9)-III-3	831	-197	697	0.30	-2.63	0.38	132.00	192.00	192.00	56
13247	(8+9)-IV-3	529	-219	-1027	0.19	-2.93	-0.57	132.00	192.00	192.00	51
13247	(8+9)-II-3	659	-233	-972	0.23	-3.11	-0.54	132.00	192.00	192.00	48
13247	(8+9)-VIII-1	255	-190	-2014	0.09	-2.54	-1.11	132.00	192.00	192.00	51

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
13247	(8+9)-VIII-2	206	-49	-136	0.07	-0.65	-0.08	132.00	192.00	192.00	>100
13247	(8+9)-VIII-3	528	-224	-955	0.19	-3.00	-0.53	132.00	192.00	192.00	51
13247	(8+9)-I-3	870	-201	714	0.31	-2.68	0.39	132.00	192.00	192.00	54
Verifiche nella direzione secondaria											
0	(8+9)-VIII-4	-49908	244	-47000	-7.78	2.17	-3.32	132.00	192.00	192.00	33
0	(8+9)-VI-4	-48915	176	-41573	-7.63	1.57	-2.94	132.00	192.00	192.00	40
0	(8+9)-III-2	-49762	298	28727	-7.76	2.66	2.03	132.00	192.00	192.00	38
0	(8+9)-IV-2	-50247	358	-24104	-7.84	3.19	-1.70	132.00	192.00	192.00	37
0	(8+9)-III-3	-48229	-142	-19335	-7.52	-1.26	-1.37	132.00	192.00	192.00	66
0	(8+9)-VIII-2	-50328	382	-22749	-7.85	3.41	-1.61	132.00	192.00	192.00	36
0	(8+9)-III-4	-48903	-1	-43077	-7.63	-0.01	-3.04	132.00	192.00	192.00	57
0	(8+9)-VII-4	-48632	-82	-47594	-7.59	-0.73	-3.36	132.00	192.00	192.00	44
0	(8+9)-IV-1	-48001	-112	55037	-7.49	-1.00	3.89	132.00	192.00	192.00	37
0	(8+9)-I-1	-49386	177	50841	-7.70	1.58	3.59	132.00	192.00	192.00	35
0	(8+9)-I-3	-48527	-122	-20963	-7.57	-1.08	-1.48	132.00	192.00	192.00	67
0	(8+9)-IV-3	-47743	-201	33495	-7.45	-1.80	2.37	132.00	192.00	192.00	43
0	(8+9)-II-1	-48994	-44	49610	-7.64	-0.40	3.50	132.00	192.00	192.00	46
0	(8+9)-IV-4	-49990	268	-45645	-7.80	2.39	-3.22	132.00	192.00	192.00	32
0	(8+9)-II-3	-48736	-134	28069	-7.60	-1.20	1.98	132.00	192.00	192.00	55
0	(8+9)-V-1	-49656	259	55358	-7.74	2.31	3.91	132.00	192.00	192.00	29
0	(8+9)-III-1	-49088	157	52469	-7.66	1.40	3.71	132.00	192.00	192.00	35
0	(8+9)-V-2	-49734	359	34872	-7.76	3.21	2.46	132.00	192.00	192.00	32
0	(8+9)-VIII-1	-48082	-87	56392	-7.50	-0.78	3.98	132.00	192.00	192.00	38
0	(8+9)-V-3	-48256	-203	-25480	-7.53	-1.81	-1.80	132.00	192.00	192.00	49
0	(8+9)-I-2	-49464	278	30355	-7.71	2.48	2.14	132.00	192.00	192.00	39
0	(8+9)-V-4	-48334	-102	-45966	-7.54	-0.91	-3.25	132.00	192.00	192.00	43
0	(8+9)-VII-2	-50032	379	33244	-7.80	3.39	2.35	132.00	192.00	192.00	32
0	(8+9)-VIII-3	-47662	-226	32140	-7.43	-2.01	2.27	132.00	192.00	192.00	42
0	(8+9)-VII-3	-47958	-223	-23852	-7.48	-1.99	-1.68	132.00	192.00	192.00	48
0	(8+9)-I-4	-48605	-21	-41449	-7.58	-0.19	-2.93	132.00	192.00	192.00	56
0	(8+9)-II-4	-48997	201	-40218	-7.64	1.79	-2.84	132.00	192.00	192.00	39
0	(8+9)-VI-1	-49075	-20	50965	-7.65	-0.18	3.60	132.00	192.00	192.00	47
0	(8+9)-VII-1	-49358	239	56986	-7.70	2.13	4.03	132.00	192.00	192.00	30
0	(8+9)-VI-3	-48655	-158	26714	-7.59	-1.41	1.89	132.00	192.00	192.00	53
3870	1	-69470	-409	14257	-10.84	-3.65	1.01	79.20	115.20	115.20	20
3870	2	-145932	-847	28625	-22.76	-7.56	2.02	118.80	172.80	172.80	14
3870	3	-145932	-847	28625	-22.76	-7.56	2.02	118.80	172.80	172.80	14
3870	4	-69470	-409	14257	-10.84	-3.65	1.01	105.60	153.60	153.60	28
3870	5	-69470	-409	14257	-10.84	-3.65	1.01	105.60	153.60	153.60	28
3870	6	-69470	-409	14257	-10.84	-3.65	1.01	105.60	153.60	153.60	28
3870	7	-69470	-409	14257	-10.84	-3.65	1.01	105.60	153.60	153.60	28
3870	(8+9)-VI-2	-47858	-374	11154	-7.46	-3.34	0.79	132.00	192.00	192.00	43
3870	(8+9)-II-2	-47714	-363	10905	-7.44	-3.24	0.77	132.00	192.00	192.00	45

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Ty kg	τ_d kg/cmq	fvd kg/cmq	RS	Cs
0	(8+9)-VIII-4	709	0.18	6.40	Si	35
0	(8+9)-IV-1	-643	0.17	6.40	Si	38
0	(8+9)-III-4	228	0.06	6.40	Si	>100
0	(8+9)-V-2	102	0.03	6.40	Si	>100
0	(8+9)-IV-2	716	0.19	6.40	Si	35
0	(8+9)-IV-4	710	0.18	6.40	Si	35
0	(8+9)-VIII-2	717	0.19	6.40	Si	34
0	(8+9)-IV-3	-649	0.17	6.40	Si	38
0	(8+9)-VII-4	224	0.06	6.40	Si	>100
0	(8+9)-I-2	98	0.03	6.40	Si	>100
0	(8+9)-VIII-3	-650	0.17	6.40	Si	38
0	(8+9)-VIII-1	-642	0.17	6.40	Si	39
0	(8+9)-VII-2	250	0.06	6.40	Si	99
0	(8+9)-V-4	76	0.02	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
0	(8+9)-II-4	215	0.06	6.40	Si	>100
0	(8+9)-III-1	-161	0.04	6.40	Si	>100
0	(8+9)-III-2	247	0.06	6.40	Si	>100
13247	1	-208	0.05	3.84	Si	71
13247	2	-436	0.11	5.76	Si	51
13247	3	-436	0.11	5.76	Si	51
13247	4	-208	0.05	5.12	Si	95
13247	5	-208	0.05	5.12	Si	95
13247	6	-208	0.05	5.12	Si	95
13247	7	-208	0.05	5.12	Si	95
13247	(8+9)-VI-2	224	0.06	6.40	Si	>100
13247	(8+9)-III-3	-355	0.09	6.40	Si	70
13247	(8+9)-I-1	-156	0.04	6.40	Si	>100
13247	(8+9)-V-3	-215	0.06	6.40	Si	>100
13247	(8+9)-VII-3	-213	0.06	6.40	Si	>100
13247	(8+9)-VI-1	-534	0.14	6.40	Si	46
13247	(8+9)-V-1	-298	0.08	6.40	Si	83
13247	(8+9)-VII-1	-296	0.08	6.40	Si	84
13247	(8+9)-I-3	-357	0.09	6.40	Si	69
13247	(8+9)-I-4	-129	0.03	6.40	Si	>100
13247	(8+9)-VI-4	249	0.06	6.40	Si	99
13247	(8+9)-II-1	-492	0.13	6.40	Si	50
13247	(8+9)-II-2	266	0.07	6.40	Si	93
13247	(8+9)-II-3	-552	0.14	6.40	Si	45
13247	(8+9)-VI-3	-509	0.13	6.40	Si	49
Verifiche nella direzione secondaria						
3870	1	-330	0.05	3.84	Si	81
3870	2	-685	0.10	5.76	Si	58
3870	3	-685	0.10	5.76	Si	58
3870	4	-330	0.05	5.12	Si	>100
3870	5	-330	0.05	5.12	Si	>100
3870	6	-330	0.05	5.12	Si	>100
3870	7	-330	0.05	5.12	Si	>100
3870	(8+9)-VIII-4	-192	0.03	6.40	Si	>100
3870	(8+9)-IV-2	-248	0.04	6.40	Si	>100
3870	(8+9)-V-1	-336	0.05	6.40	Si	>100
3870	(8+9)-I-2	-302	0.04	6.40	Si	>100
3870	(8+9)-V-2	-321	0.05	6.40	Si	>100
3870	(8+9)-I-4	-136	0.02	6.40	Si	>100
3870	(8+9)-V-3	-132	0.02	6.40	Si	>100
3870	(8+9)-II-2	-226	0.03	6.40	Si	>100
3870	(8+9)-V-4	-117	0.02	6.40	Si	>100
3870	(8+9)-II-4	-176	0.03	6.40	Si	>100
3870	(8+9)-VI-1	-283	0.04	6.40	Si	>100
3870	(8+9)-III-2	-308	0.04	6.40	Si	>100
3870	(8+9)-VI-2	-231	0.03	6.40	Si	>100
3870	(8+9)-III-4	-143	0.02	6.40	Si	>100
3870	(8+9)-VI-3	-222	0.03	6.40	Si	>100
3870	(8+9)-I-1	-317	0.05	6.40	Si	>100
3870	(8+9)-VI-4	-170	0.02	6.40	Si	>100
3870	(8+9)-IV-4	-198	0.03	6.40	Si	>100
3870	(8+9)-VII-1	-330	0.05	6.40	Si	>100
3870	(8+9)-II-1	-277	0.04	6.40	Si	>100
3870	(8+9)-VII-2	-328	0.05	6.40	Si	>100
3870	(8+9)-III-1	-311	0.04	6.40	Si	>100
3870	(8+9)-VII-3	-126	0.02	6.40	Si	>100
3870	(8+9)-IV-1	-255	0.04	6.40	Si	>100
3870	(8+9)-VII-4	-123	0.02	6.40	Si	>100
3870	(8+9)-III-3	-145	0.02	6.40	Si	>100
3870	(8+9)-IV-3	-205	0.03	6.40	Si	>100
3870	(8+9)-II-3	-228	0.03	6.40	Si	>100
3870	(8+9)-VIII-1	-261	0.04	6.40	Si	>100
3870	(8+9)-VIII-2	-254	0.04	6.40	Si	>100
3870	(8+9)-VIII-3	-200	0.03	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
3870	(8+9)-I-3	-152	0.02	6.40	Si	>100

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
6624	(8+9)-VIII-4	-9669	-5.16	32.00	6.2	-1.25	20.00	16	V	6.2
6624	(8+9)-IV-1	9572	5.11	32.00	6.3	1.24	20.00	16	V	6.3
6624	(8+9)-VII-1	10783	5.76	32.00	5.6	1.39	20.00	14	V	5.6
6624	(8+9)-III-3	-5631	-3.01	32.00	11	-0.73	20.00	27	V	11
6624	(8+9)-IV-2	-4744	-2.53	32.00	13	-0.61	20.00	33	V	13
6624	(8+9)-III-4	-9926	-5.30	32.00	6.0	-1.28	20.00	16	V	6.0
6624	(8+9)-VIII-2	-4524	-2.42	32.00	13	-0.58	20.00	34	V	13
6624	(8+9)-VII-3	-6365	-3.40	32.00	9.4	-0.82	20.00	24	V	9.4
6624	(8+9)-VII-4	-10660	-5.69	32.00	5.6	-1.38	20.00	15	V	5.6
6624	(8+9)-I-2	5858	3.13	32.00	10	0.76	20.00	26	V	10
6624	(8+9)-IV-3	4868	2.60	32.00	12	0.63	20.00	32	V	12
6624	(8+9)-I-4	-9823	-5.24	32.00	6.1	-1.27	20.00	16	V	6.1
6624	(8+9)-IV-4	-9449	-5.04	32.00	6.3	-1.22	20.00	16	V	6.3
6624	(8+9)-II-2	-4399	-2.35	32.00	14	-0.57	20.00	35	V	14
6624	(8+9)-V-1	10679	5.70	32.00	5.6	1.38	20.00	14	V	5.6
6624	(8+9)-II-4	-9103	-4.86	32.00	6.6	-1.18	20.00	17	V	6.6
6624	(8+9)-V-2	6592	3.52	32.00	9.1	0.85	20.00	23	V	9.1
6624	(8+9)-III-2	5755	3.07	32.00	10	0.74	20.00	27	V	10
6624	(8+9)-V-3	-6468	-3.45	32.00	9.3	-0.84	20.00	24	V	9.3
6624	(8+9)-VIII-1	9792	5.23	32.00	6.1	1.27	20.00	16	V	6.1
6624	(8+9)-V-4	-10556	-5.64	32.00	5.7	-1.36	20.00	15	V	5.7
6624	(8+9)-I-3	-5735	-3.06	32.00	10	-0.74	20.00	27	V	10
6624	(8+9)-VI-1	9446	5.04	32.00	6.3	1.22	20.00	16	V	6.3
6624	(8+9)-II-3	4522	2.41	32.00	13	0.58	20.00	34	V	13
6624	(8+9)-VIII-3	4648	2.48	32.00	13	0.60	20.00	33	V	13
6624	(8+9)-I-1	9946	5.31	32.00	6.0	1.28	20.00	16	V	6.0
6624	(8+9)-II-1	9226	4.93	32.00	6.5	1.19	20.00	17	V	6.5
6624	(8+9)-III-1	10050	5.37	32.00	6.0	1.30	20.00	15	V	6.0
6624	(8+9)-VI-2	-4179	-2.23	32.00	14	-0.54	20.00	37	V	14
6624	(8+9)-VII-2	6488	3.46	32.00	9.2	0.84	20.00	24	V	9.2
6624	(8+9)-VI-4	-9323	-4.98	32.00	6.4	-1.20	20.00	17	V	6.4
13247	1	1490	0.80	19.20	24	0.19	12.00	62	V	24
13247	2	3293	1.76	28.80	16	0.43	18.00	42	V	16
13247	3	3293	1.76	28.80	16	0.43	18.00	42	V	16
13247	4	1490	0.80	25.60	32	0.19	16.00	83	V	32
13247	5	1490	0.80	25.60	32	0.19	16.00	83	V	32
13247	6	1490	0.80	25.60	32	0.19	16.00	83	V	32
13247	7	1490	0.80	25.60	32	0.19	16.00	83	V	32
13247	(8+9)-VI-3	4336	2.31	32.00	14	0.56	20.00	36	V	14
Verifiche nella direzione secondaria										
1935	(8+9)-VIII-4	-33914	-5.29	32.00	6.0	-1.28	20.00	16	V	6.0
1935	(8+9)-IV-1	33161	5.17	32.00	6.2	1.25	20.00	16	V	6.2
1935	(8+9)-VI-1	32853	5.12	32.00	6.2	1.24	20.00	16	V	6.2
1935	(8+9)-IV-2	-16673	-2.60	32.00	12	-0.63	20.00	32	V	12
1935	(8+9)-II-1	32096	5.01	32.00	6.4	1.21	20.00	17	V	6.4
1935	(8+9)-VIII-2	-15916	-2.48	32.00	13	-0.60	20.00	33	V	13
1935	(8+9)-V-2	22843	3.56	32.00	9.0	0.86	20.00	23	V	9.0
1935	(8+9)-VII-2	22524	3.51	32.00	9.1	0.85	20.00	24	V	9.1
1935	(8+9)-II-3	15612	2.43	32.00	13	0.59	20.00	34	V	13
1935	(8+9)-I-1	34631	5.40	32.00	5.9	1.31	20.00	15	V	5.9
1935	(8+9)-V-1	37154	5.79	32.00	5.5	1.40	20.00	14	V	5.5
1935	(8+9)-VI-3	14855	2.32	32.00	14	0.56	20.00	36	V	14
1935	(8+9)-III-1	34950	5.45	32.00	5.9	1.32	20.00	15	V	5.9
1935	(8+9)-I-2	20320	3.17	32.00	10	0.77	20.00	26	V	10
1935	(8+9)-VIII-3	15920	2.48	32.00	13	0.60	20.00	33	V	13
1935	(8+9)-VII-1	37474	5.84	32.00	5.5	1.41	20.00	14	V	5.5
1935	(8+9)-III-2	20000	3.12	32.00	10	0.75	20.00	26	V	10
1935	(8+9)-IV-4	-33157	-5.17	32.00	6.2	-1.25	20.00	16	V	6.2

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
1935	(8+9)-IV-3	16677	2.60	32.00	12	0.63	20.00	32	V	12
1935	(8+9)-VIII-1	33918	5.29	32.00	6.0	1.28	20.00	16	V	6.0
3870	1	-474	-0.07	19.20	>100	-0.02	12.00	>100	V	>100
3870	2	-951	-0.15	28.80	>100	-0.04	18.00	>100	V	>100
3870	3	-951	-0.15	28.80	>100	-0.04	18.00	>100	V	>100
3870	4	-474	-0.07	25.60	>100	-0.02	16.00	>100	V	>100
3870	5	-474	-0.07	25.60	>100	-0.02	16.00	>100	V	>100
3870	6	-474	-0.07	25.60	>100	-0.02	16.00	>100	V	>100
3870	7	-474	-0.07	25.60	>100	-0.02	16.00	>100	V	>100
3870	(8+9)-VI-4	-32938	-5.14	32.00	6.2	-1.24	20.00	16	V	6.2
3870	(8+9)-III-4	-35108	-5.48	32.00	5.8	-1.33	20.00	15	V	5.8
3870	(8+9)-VII-3	-23007	-3.59	32.00	8.9	-0.87	20.00	23	V	8.9
3870	(8+9)-VI-2	-14927	-2.33	32.00	14	-0.56	20.00	35	V	14
3870	(8+9)-VII-4	-37692	-5.88	32.00	5.4	-1.42	20.00	14	V	5.4
3870	(8+9)-V-3	-23269	-3.63	32.00	8.8	-0.88	20.00	23	V	8.8
3870	(8+9)-I-3	-20685	-3.23	32.00	9.9	-0.78	20.00	26	V	9.9
3870	(8+9)-V-4	-37430	-5.84	32.00	5.5	-1.41	20.00	14	V	5.5
3870	(8+9)-II-2	-15702	-2.45	32.00	13	-0.59	20.00	34	V	13
3870	(8+9)-II-4	-32163	-5.02	32.00	6.4	-1.21	20.00	16	V	6.4
3870	(8+9)-III-3	-20423	-3.19	32.00	10	-0.77	20.00	26	V	10
3870	(8+9)-I-4	-34846	-5.43	32.00	5.9	-1.32	20.00	15	V	5.9

Verifiche a instabilità

Setto(X)	Comb.	kcrit _c	kcrit _m	λ_{relc}	λ_{relm}	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
(cm)						kg/cm ² q	kg/cm ² q	kg/cm ² q	kg/cm ² q	kg/cm ² q	kg/cm ² q	
34(132 4.7)	3	--	--	--	--	0.39	-5.56	-0.94	118.80	172.80	172.80	24

Parete Xlam 4 - Nodi: [6-21-109-13-12-11-10-9-8-104] - **Crit.Prog.** Criterio di verifica XLAM 0 - **Verificato:** [Cs=5.443,Comb=(8+9)-VII-4]

Geometria setti

Setto	Crit.	X	L	S	X90	L90	S90
		mm	cm	cm	mm	cm	cm
34	Criterio di verifica XLAM 0	0	387.0	12.1	0	1324.7	12.1
		6624	387.0	12.1	1935	1324.7	12.1
		13247	387.0	12.1	3870	1324.7	12.1

Setto 34: origine (366.0,1315.0,193.5), direzione (0.825849,0.563892,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	
13247	1	531	-198	-796	0.19	-2.65	-0.44	79.20	115.20	115.20	34
13247	2	1087	-416	-1704	0.39	-5.56	-0.94	118.80	172.80	172.80	24
13247	3	1087	-416	-1704	0.39	-5.56	-0.94	118.80	172.80	172.80	24
13247	4	531	-198	-796	0.19	-2.65	-0.44	105.60	153.60	153.60	46
13247	5	531	-198	-796	0.19	-2.65	-0.44	105.60	153.60	153.60	46
13247	6	531	-198	-796	0.19	-2.65	-0.44	105.60	153.60	153.60	46
13247	7	531	-198	-796	0.19	-2.65	-0.44	105.60	153.60	153.60	46
13247	(8+9)-VIII-4	479	-83	923	0.17	-1.11	0.51	132.00	192.00	192.00	>100
13247	(8+9)-IV-1	255	-196	-1941	0.09	-2.62	-1.07	132.00	192.00	192.00	50
13247	(8+9)-V-1	-42	-105	-2576	-0.01	-1.40	-1.42	132.00	192.00	192.00	68
13247	(8+9)-I-2	-136	-72	-1805	-0.05	-0.97	-1.00	132.00	192.00	192.00	98
13247	(8+9)-V-2	-134	-54	-2046	-0.05	-0.72	-1.13	132.00	192.00	192.00	>100
13247	(8+9)-I-4	777	-150	1244	0.28	-2.01	0.69	132.00	192.00	192.00	62
13247	(8+9)-V-3	868	-219	955	0.31	-2.93	0.53	132.00	192.00	192.00	49
13247	(8+9)-II-2	75	-40	-119	0.03	-0.54	-0.07	132.00	192.00	192.00	>100
13247	(8+9)-V-4	775	-168	1485	0.28	-2.25	0.82	132.00	192.00	192.00	55
13247	(8+9)-II-4	349	-64	795	0.12	-0.85	0.44	132.00	192.00	192.00	>100
13247	(8+9)-VI-1	385	-204	-1959	0.14	-2.73	-1.08	132.00	192.00	192.00	48

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
13247	(8+9)-III-2	-97	-77	-1788	-0.03	-1.02	-0.99	132.00	192.00	192.00	96
13247	(8+9)-VI-2	76	-35	-191	0.03	-0.47	-0.11	132.00	192.00	192.00	>100
13247	(8+9)-III-4	816	-154	1260	0.29	-2.06	0.70	132.00	192.00	192.00	60
13247	(8+9)-VI-3	658	-238	-900	0.23	-3.18	-0.50	132.00	192.00	192.00	48
13247	(8+9)-IV-2	205	-54	-64	0.07	-0.72	-0.04	132.00	192.00	192.00	>100
13247	(8+9)-VI-4	349	-69	868	0.12	-0.92	0.48	132.00	192.00	192.00	>100
13247	(8+9)-IV-4	479	-78	850	0.17	-1.04	0.47	132.00	192.00	192.00	>100
13247	(8+9)-VII-1	-81	-101	-2592	-0.03	-1.35	-1.43	132.00	192.00	192.00	69
13247	(8+9)-II-1	385	-209	-1886	0.14	-2.80	-1.04	132.00	192.00	192.00	48
13247	(8+9)-VII-2	-95	-58	-2029	-0.03	-0.78	-1.12	132.00	192.00	192.00	>100
13247	(8+9)-III-1	-82	-119	-2351	-0.03	-1.59	-1.30	132.00	192.00	192.00	66
13247	(8+9)-VII-3	829	-215	938	0.30	-2.87	0.52	132.00	192.00	192.00	50
13247	(8+9)-I-1	-43	-123	-2335	-0.02	-1.65	-1.29	132.00	192.00	192.00	65
13247	(8+9)-VII-4	814	-172	1501	0.29	-2.30	0.83	132.00	192.00	192.00	54
13247	(8+9)-III-3	831	-197	697	0.30	-2.63	0.38	132.00	192.00	192.00	56
13247	(8+9)-IV-3	529	-219	-1027	0.19	-2.93	-0.57	132.00	192.00	192.00	51
13247	(8+9)-II-3	659	-233	-972	0.23	-3.11	-0.54	132.00	192.00	192.00	48
13247	(8+9)-VIII-1	255	-190	-2014	0.09	-2.54	-1.11	132.00	192.00	192.00	51
13247	(8+9)-VIII-2	206	-49	-136	0.07	-0.65	-0.08	132.00	192.00	192.00	>100
13247	(8+9)-VIII-3	528	-224	-955	0.19	-3.00	-0.53	132.00	192.00	192.00	51
13247	(8+9)-I-3	870	-201	714	0.31	-2.68	0.39	132.00	192.00	192.00	54
Verifiche nella direzione secondaria											
0	(8+9)-VIII-4	-49908	244	-47000	-7.78	2.17	-3.32	132.00	192.00	192.00	33
0	(8+9)-VI-4	-48915	176	-41573	-7.63	1.57	-2.94	132.00	192.00	192.00	40
0	(8+9)-III-2	-49762	298	28727	-7.76	2.66	2.03	132.00	192.00	192.00	38
0	(8+9)-IV-2	-50247	358	-24104	-7.84	3.19	-1.70	132.00	192.00	192.00	37
0	(8+9)-III-3	-48229	-142	-19335	-7.52	-1.26	-1.37	132.00	192.00	192.00	66
0	(8+9)-VIII-2	-50328	382	-22749	-7.85	3.41	-1.61	132.00	192.00	192.00	36
0	(8+9)-III-4	-48903	-1	-43077	-7.63	-0.01	-3.04	132.00	192.00	192.00	57
0	(8+9)-VII-4	-48632	-82	-47594	-7.59	-0.73	-3.36	132.00	192.00	192.00	44
0	(8+9)-IV-1	-48001	-112	55037	-7.49	-1.00	3.89	132.00	192.00	192.00	37
0	(8+9)-I-1	-49386	177	50841	-7.70	1.58	3.59	132.00	192.00	192.00	35
0	(8+9)-I-3	-48527	-122	-20963	-7.57	-1.08	-1.48	132.00	192.00	192.00	67
0	(8+9)-IV-3	-47743	-201	33495	-7.45	-1.80	2.37	132.00	192.00	192.00	43
0	(8+9)-II-1	-48994	-44	49610	-7.64	-0.40	3.50	132.00	192.00	192.00	46
0	(8+9)-IV-4	-49990	268	-45645	-7.80	2.39	-3.22	132.00	192.00	192.00	32
0	(8+9)-II-3	-48736	-134	28069	-7.60	-1.20	1.98	132.00	192.00	192.00	55
0	(8+9)-V-1	-49656	259	55358	-7.74	2.31	3.91	132.00	192.00	192.00	29
0	(8+9)-III-1	-49088	157	52469	-7.66	1.40	3.71	132.00	192.00	192.00	35
0	(8+9)-V-2	-49734	359	34872	-7.76	3.21	2.46	132.00	192.00	192.00	32
0	(8+9)-VIII-1	-48082	-87	56392	-7.50	-0.78	3.98	132.00	192.00	192.00	38
0	(8+9)-V-3	-48256	-203	-25480	-7.53	-1.81	-1.80	132.00	192.00	192.00	49
0	(8+9)-I-2	-49464	278	30355	-7.71	2.48	2.14	132.00	192.00	192.00	39
0	(8+9)-V-4	-48334	-102	-45966	-7.54	-0.91	-3.25	132.00	192.00	192.00	43
0	(8+9)-VII-2	-50032	379	33244	-7.80	3.39	2.35	132.00	192.00	192.00	32
0	(8+9)-VIII-3	-47662	-226	32140	-7.43	-2.01	2.27	132.00	192.00	192.00	42
0	(8+9)-VII-3	-47958	-223	-23852	-7.48	-1.99	-1.68	132.00	192.00	192.00	48
0	(8+9)-I-4	-48605	-21	-41449	-7.58	-0.19	-2.93	132.00	192.00	192.00	56
0	(8+9)-II-4	-48997	201	-40218	-7.64	1.79	-2.84	132.00	192.00	192.00	39
0	(8+9)-VI-1	-49075	-20	50965	-7.65	-0.18	3.60	132.00	192.00	192.00	47
0	(8+9)-VII-1	-49358	239	56986	-7.70	2.13	4.03	132.00	192.00	192.00	30
0	(8+9)-VI-3	-48655	-158	26714	-7.59	-1.41	1.89	132.00	192.00	192.00	53
3870	1	-69470	-409	14257	-10.84	-3.65	1.01	79.20	115.20	115.20	20
3870	2	-	-847	28625	-22.76	-7.56	2.02	118.80	172.80	172.80	14
3870	3	-	-847	28625	-22.76	-7.56	2.02	118.80	172.80	172.80	14
3870	4	-69470	-409	14257	-10.84	-3.65	1.01	105.60	153.60	153.60	28
3870	5	-69470	-409	14257	-10.84	-3.65	1.01	105.60	153.60	153.60	28
3870	6	-69470	-409	14257	-10.84	-3.65	1.01	105.60	153.60	153.60	28
3870	7	-69470	-409	14257	-10.84	-3.65	1.01	105.60	153.60	153.60	28
3870	(8+9)-VI-2	-47858	-374	11154	-7.46	-3.34	0.79	132.00	192.00	192.00	43
3870	(8+9)-II-2	-47714	-363	10905	-7.44	-3.24	0.77	132.00	192.00	192.00	45

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Ty kg	τ_d kg/cmq	fvd kg/cmq	RS	Cs
0	(8+9)-VIII-4	709	0.18	6.40	Si	35
0	(8+9)-IV-1	-643	0.17	6.40	Si	38
0	(8+9)-III-4	228	0.06	6.40	Si	>100
0	(8+9)-V-2	102	0.03	6.40	Si	>100
0	(8+9)-IV-2	716	0.19	6.40	Si	35
0	(8+9)-IV-4	710	0.18	6.40	Si	35
0	(8+9)-VIII-2	717	0.19	6.40	Si	34
0	(8+9)-IV-3	-649	0.17	6.40	Si	38
0	(8+9)-VII-4	224	0.06	6.40	Si	>100
0	(8+9)-I-2	98	0.03	6.40	Si	>100
0	(8+9)-VIII-3	-650	0.17	6.40	Si	38
0	(8+9)-VIII-1	-642	0.17	6.40	Si	39
0	(8+9)-VII-2	250	0.06	6.40	Si	99
0	(8+9)-V-4	76	0.02	6.40	Si	>100
0	(8+9)-II-4	215	0.06	6.40	Si	>100
0	(8+9)-III-1	-161	0.04	6.40	Si	>100
0	(8+9)-III-2	247	0.06	6.40	Si	>100
13247	1	-208	0.05	3.84	Si	71
13247	2	-436	0.11	5.76	Si	51
13247	3	-436	0.11	5.76	Si	51
13247	4	-208	0.05	5.12	Si	95
13247	5	-208	0.05	5.12	Si	95
13247	6	-208	0.05	5.12	Si	95
13247	7	-208	0.05	5.12	Si	95
13247	(8+9)-VI-2	224	0.06	6.40	Si	>100
13247	(8+9)-III-3	-355	0.09	6.40	Si	70
13247	(8+9)-I-1	-156	0.04	6.40	Si	>100
13247	(8+9)-V-3	-215	0.06	6.40	Si	>100
13247	(8+9)-VII-3	-213	0.06	6.40	Si	>100
13247	(8+9)-VI-1	-534	0.14	6.40	Si	46
13247	(8+9)-V-1	-298	0.08	6.40	Si	83
13247	(8+9)-VII-1	-296	0.08	6.40	Si	84
13247	(8+9)-I-3	-357	0.09	6.40	Si	69
13247	(8+9)-I-4	-129	0.03	6.40	Si	>100
13247	(8+9)-VI-4	249	0.06	6.40	Si	99
13247	(8+9)-II-1	-492	0.13	6.40	Si	50
13247	(8+9)-II-2	266	0.07	6.40	Si	93
13247	(8+9)-II-3	-552	0.14	6.40	Si	45
13247	(8+9)-VI-3	-509	0.13	6.40	Si	49
Verifiche nella direzione secondaria						
3870	1	-330	0.05	3.84	Si	81
3870	2	-685	0.10	5.76	Si	58
3870	3	-685	0.10	5.76	Si	58
3870	4	-330	0.05	5.12	Si	>100
3870	5	-330	0.05	5.12	Si	>100
3870	6	-330	0.05	5.12	Si	>100
3870	7	-330	0.05	5.12	Si	>100
3870	(8+9)-VIII-4	-192	0.03	6.40	Si	>100
3870	(8+9)-IV-2	-248	0.04	6.40	Si	>100
3870	(8+9)-V-1	-336	0.05	6.40	Si	>100
3870	(8+9)-I-2	-302	0.04	6.40	Si	>100
3870	(8+9)-V-2	-321	0.05	6.40	Si	>100
3870	(8+9)-I-4	-136	0.02	6.40	Si	>100
3870	(8+9)-V-3	-132	0.02	6.40	Si	>100
3870	(8+9)-II-2	-226	0.03	6.40	Si	>100
3870	(8+9)-V-4	-117	0.02	6.40	Si	>100
3870	(8+9)-II-4	-176	0.03	6.40	Si	>100
3870	(8+9)-VI-1	-283	0.04	6.40	Si	>100
3870	(8+9)-III-2	-308	0.04	6.40	Si	>100
3870	(8+9)-VI-2	-231	0.03	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
3870	(8+9)-III-4	-143	0.02	6.40	Si	>100
3870	(8+9)-VI-3	-222	0.03	6.40	Si	>100
3870	(8+9)-I-1	-317	0.05	6.40	Si	>100
3870	(8+9)-VI-4	-170	0.02	6.40	Si	>100
3870	(8+9)-IV-4	-198	0.03	6.40	Si	>100
3870	(8+9)-VII-1	-330	0.05	6.40	Si	>100
3870	(8+9)-II-1	-277	0.04	6.40	Si	>100
3870	(8+9)-VII-2	-328	0.05	6.40	Si	>100
3870	(8+9)-III-1	-311	0.04	6.40	Si	>100
3870	(8+9)-VII-3	-126	0.02	6.40	Si	>100
3870	(8+9)-IV-1	-255	0.04	6.40	Si	>100
3870	(8+9)-VII-4	-123	0.02	6.40	Si	>100
3870	(8+9)-III-3	-145	0.02	6.40	Si	>100
3870	(8+9)-IV-3	-205	0.03	6.40	Si	>100
3870	(8+9)-II-3	-228	0.03	6.40	Si	>100
3870	(8+9)-VIII-1	-261	0.04	6.40	Si	>100
3870	(8+9)-VIII-2	-254	0.04	6.40	Si	>100
3870	(8+9)-VIII-3	-200	0.03	6.40	Si	>100
3870	(8+9)-I-3	-152	0.02	6.40	Si	>100

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
6624	(8+9)-VIII-4	-9669	-5.16	32.00	6.2	-1.25	20.00	16	V	6.2
6624	(8+9)-IV-1	9572	5.11	32.00	6.3	1.24	20.00	16	V	6.3
6624	(8+9)-VII-1	10783	5.76	32.00	5.6	1.39	20.00	14	V	5.6
6624	(8+9)-III-3	-5631	-3.01	32.00	11	-0.73	20.00	27	V	11
6624	(8+9)-IV-2	-4744	-2.53	32.00	13	-0.61	20.00	33	V	13
6624	(8+9)-III-4	-9926	-5.30	32.00	6.0	-1.28	20.00	16	V	6.0
6624	(8+9)-VIII-2	-4524	-2.42	32.00	13	-0.58	20.00	34	V	13
6624	(8+9)-VII-3	-6365	-3.40	32.00	9.4	-0.82	20.00	24	V	9.4
6624	(8+9)-VII-4	-10660	-5.69	32.00	5.6	-1.38	20.00	15	V	5.6
6624	(8+9)-I-2	5858	3.13	32.00	10	0.76	20.00	26	V	10
6624	(8+9)-IV-3	4868	2.60	32.00	12	0.63	20.00	32	V	12
6624	(8+9)-I-4	-9823	-5.24	32.00	6.1	-1.27	20.00	16	V	6.1
6624	(8+9)-IV-4	-9449	-5.04	32.00	6.3	-1.22	20.00	16	V	6.3
6624	(8+9)-II-2	-4399	-2.35	32.00	14	-0.57	20.00	35	V	14
6624	(8+9)-V-1	10679	5.70	32.00	5.6	1.38	20.00	14	V	5.6
6624	(8+9)-II-4	-9103	-4.86	32.00	6.6	-1.18	20.00	17	V	6.6
6624	(8+9)-V-2	6592	3.52	32.00	9.1	0.85	20.00	23	V	9.1
6624	(8+9)-III-2	5755	3.07	32.00	10	0.74	20.00	27	V	10
6624	(8+9)-V-3	-6468	-3.45	32.00	9.3	-0.84	20.00	24	V	9.3
6624	(8+9)-VIII-1	9792	5.23	32.00	6.1	1.27	20.00	16	V	6.1
6624	(8+9)-V-4	-10556	-5.64	32.00	5.7	-1.36	20.00	15	V	5.7
6624	(8+9)-I-3	-5735	-3.06	32.00	10	-0.74	20.00	27	V	10
6624	(8+9)-VI-1	9446	5.04	32.00	6.3	1.22	20.00	16	V	6.3
6624	(8+9)-II-3	4522	2.41	32.00	13	0.58	20.00	34	V	13
6624	(8+9)-VIII-3	4648	2.48	32.00	13	0.60	20.00	33	V	13
6624	(8+9)-I-1	9946	5.31	32.00	6.0	1.28	20.00	16	V	6.0
6624	(8+9)-II-1	9226	4.93	32.00	6.5	1.19	20.00	17	V	6.5
6624	(8+9)-III-1	10050	5.37	32.00	6.0	1.30	20.00	15	V	6.0
6624	(8+9)-VI-2	-4179	-2.23	32.00	14	-0.54	20.00	37	V	14
6624	(8+9)-VII-2	6488	3.46	32.00	9.2	0.84	20.00	24	V	9.2
6624	(8+9)-VI-4	-9323	-4.98	32.00	6.4	-1.20	20.00	17	V	6.4
13247	1	1490	0.80	19.20	24	0.19	12.00	62	V	24
13247	2	3293	1.76	28.80	16	0.43	18.00	42	V	16
13247	3	3293	1.76	28.80	16	0.43	18.00	42	V	16
13247	4	1490	0.80	25.60	32	0.19	16.00	83	V	32
13247	5	1490	0.80	25.60	32	0.19	16.00	83	V	32
13247	6	1490	0.80	25.60	32	0.19	16.00	83	V	32
13247	7	1490	0.80	25.60	32	0.19	16.00	83	V	32
13247	(8+9)-VI-3	4336	2.31	32.00	14	0.56	20.00	36	V	14

Verifiche nella direzione secondaria

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
1935	(8+9)-VIII-4	-33914	-5.29	32.00	6.0	-1.28	20.00	16	V	6.0
1935	(8+9)-IV-1	33161	5.17	32.00	6.2	1.25	20.00	16	V	6.2
1935	(8+9)-VI-1	32853	5.12	32.00	6.2	1.24	20.00	16	V	6.2
1935	(8+9)-IV-2	-16673	-2.60	32.00	12	-0.63	20.00	32	V	12
1935	(8+9)-II-1	32096	5.01	32.00	6.4	1.21	20.00	17	V	6.4
1935	(8+9)-VIII-2	-15916	-2.48	32.00	13	-0.60	20.00	33	V	13
1935	(8+9)-V-2	22843	3.56	32.00	9.0	0.86	20.00	23	V	9.0
1935	(8+9)-VII-2	22524	3.51	32.00	9.1	0.85	20.00	24	V	9.1
1935	(8+9)-II-3	15612	2.43	32.00	13	0.59	20.00	34	V	13
1935	(8+9)-I-1	34631	5.40	32.00	5.9	1.31	20.00	15	V	5.9
1935	(8+9)-V-1	37154	5.79	32.00	5.5	1.40	20.00	14	V	5.5
1935	(8+9)-VI-3	14855	2.32	32.00	14	0.56	20.00	36	V	14
1935	(8+9)-III-1	34950	5.45	32.00	5.9	1.32	20.00	15	V	5.9
1935	(8+9)-I-2	20320	3.17	32.00	10	0.77	20.00	26	V	10
1935	(8+9)-VIII-3	15920	2.48	32.00	13	0.60	20.00	33	V	13
1935	(8+9)-VII-1	37474	5.84	32.00	5.5	1.41	20.00	14	V	5.5
1935	(8+9)-III-2	20000	3.12	32.00	10	0.75	20.00	26	V	10
1935	(8+9)-IV-4	-33157	-5.17	32.00	6.2	-1.25	20.00	16	V	6.2
1935	(8+9)-IV-3	16677	2.60	32.00	12	0.63	20.00	32	V	12
1935	(8+9)-VIII-1	33918	5.29	32.00	6.0	1.28	20.00	16	V	6.0
3870	1	-474	-0.07	19.20	>100	-0.02	12.00	>100	V	>100
3870	2	-951	-0.15	28.80	>100	-0.04	18.00	>100	V	>100
3870	3	-951	-0.15	28.80	>100	-0.04	18.00	>100	V	>100
3870	4	-474	-0.07	25.60	>100	-0.02	16.00	>100	V	>100
3870	5	-474	-0.07	25.60	>100	-0.02	16.00	>100	V	>100
3870	6	-474	-0.07	25.60	>100	-0.02	16.00	>100	V	>100
3870	7	-474	-0.07	25.60	>100	-0.02	16.00	>100	V	>100
3870	(8+9)-VI-4	-32938	-5.14	32.00	6.2	-1.24	20.00	16	V	6.2
3870	(8+9)-III-4	-35108	-5.48	32.00	5.8	-1.33	20.00	15	V	5.8
3870	(8+9)-VII-3	-23007	-3.59	32.00	8.9	-0.87	20.00	23	V	8.9
3870	(8+9)-VI-2	-14927	-2.33	32.00	14	-0.56	20.00	35	V	14
3870	(8+9)-VII-4	-37692	-5.88	32.00	5.4	-1.42	20.00	14	V	5.4
3870	(8+9)-V-3	-23269	-3.63	32.00	8.8	-0.88	20.00	23	V	8.8
3870	(8+9)-I-3	-20685	-3.23	32.00	9.9	-0.78	20.00	26	V	9.9
3870	(8+9)-V-4	-37430	-5.84	32.00	5.5	-1.41	20.00	14	V	5.5
3870	(8+9)-II-2	-15702	-2.45	32.00	13	-0.59	20.00	34	V	13
3870	(8+9)-II-4	-32163	-5.02	32.00	6.4	-1.21	20.00	16	V	6.4
3870	(8+9)-III-3	-20423	-3.19	32.00	10	-0.77	20.00	26	V	10
3870	(8+9)-I-4	-34846	-5.43	32.00	5.9	-1.32	20.00	15	V	5.9

Verifiche a instabilità

Setto(X)	Comb.	kcrit _c	kcrit _m	$\lambda_{rel,c}$	$\lambda_{rel,m}$	σ_n	σ_{mx}	σ_{my}	f _{td}	f _{cd}	f _{md}	Cs
(cm)						kg/cm ² q	kg/cm ² q	kg/cm ² q	kg/cm ² q	kg/cm ² q	kg/cm ² q	
34(132 4.7)	3	--	--	--	--	0.39	-5.56	-0.94	118.80	172.80	172.80	24

Parete Xlam 15 - Nodi: [18-22-14-15-23-24-18-19-25-21-109-25-108] - **Crit.Prog.** Criterio di verifica XLAM 0 - **Verificato:** [Cs=1.387,Comb=(8+9)-V-2]

Geometria setti

Setto	Crit.	X	L	S	X90	L90	S90
		mm	cm	cm	mm	cm	cm
35	Criterio di verifica XLAM 0	0	387.0	12.1	0	229.3	12.1
		1147	387.0	12.1	1935	229.3	12.1
		2293	387.0	12.1	3870	229.3	12.1
36	Criterio di verifica XLAM 0	0	387.0	12.1	0	100.7	12.1
		504	387.0	12.1	1935	100.7	12.1
		1007	387.0	12.1	3870	100.7	12.1
37	Criterio di verifica XLAM 0	0	387.0	12.1	0	55.2	12.1
		276	387.0	12.1	1935	55.2	12.1
		552	387.0	12.1	3870	55.2	12.1

Setto	Crit.	X	L	S	X90	L90	S90
38	Criterio di verifica XLAM 0	0	167.0	12.1	0	120.0	12.1
		600	167.0	12.1	835	120.0	12.1
		1200	167.0	12.1	1670	120.0	12.1
39	Criterio di verifica XLAM 0	0	167.0	12.1	0	100.0	12.1
		500	167.0	12.1	835	100.0	12.1
		1000	167.0	12.1	1670	100.0	12.1

Setto 35: origine (1384.8,2430.3,193.5), direzione (-0.200098,0.979776,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	
0	(8+9)-VIII-4	4263	-20	-4041	1.52	-0.27	-2.23	132.00	192.00	192.00	41
0	(8+9)-IV-1	-4751	12	4665	-1.69	0.16	2.57	132.00	192.00	192.00	70
0	(8+9)-VII-2	7275	-45	-6931	2.59	-0.61	-3.82	132.00	192.00	192.00	23
0	(8+9)-III-3	-5707	22	5562	-2.03	0.29	3.07	132.00	192.00	192.00	57
0	(8+9)-IV-2	7092	-36	-6761	2.52	-0.48	-3.73	132.00	192.00	192.00	24
0	(8+9)-III-4	-2154	8	2134	-0.77	0.10	1.18	132.00	192.00	192.00	>100
0	(8+9)-VIII-2	7566	-40	-7220	2.69	-0.53	-3.98	132.00	192.00	192.00	23
0	(8+9)-VII-3	-7289	34	7095	-2.59	0.45	3.92	132.00	192.00	192.00	44
0	(8+9)-VII-4	-3736	19	3667	-1.33	0.26	2.02	132.00	192.00	192.00	84
0	(8+9)-I-2	6036	-35	-5730	2.15	-0.47	-3.16	132.00	192.00	192.00	28
0	(8+9)-IV-3	-7105	24	6925	-2.53	0.32	3.82	132.00	192.00	192.00	46
0	(8+9)-I-4	-1810	6	1803	-0.64	0.08	0.99	132.00	192.00	192.00	>100
0	(8+9)-IV-4	4738	-24	-4501	1.69	-0.32	-2.48	132.00	192.00	192.00	37
0	(8+9)-II-2	8237	-42	-7866	2.93	-0.56	-4.34	132.00	192.00	192.00	21
0	(8+9)-V-1	3378	-29	-3172	1.20	-0.39	-1.75	132.00	192.00	192.00	49
0	(8+9)-II-4	5883	-29	-5606	2.09	-0.39	-3.09	132.00	192.00	192.00	29
0	(8+9)-V-2	7618	-47	-7263	2.71	-0.63	-4.01	132.00	192.00	192.00	22
0	(8+9)-III-2	5693	-34	-5398	2.03	-0.45	-2.98	132.00	192.00	192.00	30
0	(8+9)-V-3	-7632	35	7427	-2.72	0.47	4.10	132.00	192.00	192.00	42
0	(8+9)-VIII-1	-4277	8	4205	-1.52	0.11	2.32	132.00	192.00	192.00	79
0	(8+9)-V-4	-3392	18	3336	-1.21	0.24	1.84	132.00	192.00	192.00	92
0	(8+9)-I-3	-6050	24	5894	-2.15	0.32	3.25	132.00	192.00	192.00	53
0	(8+9)-VI-1	-5422	14	5310	-1.93	0.19	2.93	132.00	192.00	192.00	61
0	(8+9)-II-3	-8251	30	8030	-2.94	0.40	4.43	132.00	192.00	192.00	39
0	(8+9)-VI-2	8711	-45	-8326	3.10	-0.60	-4.59	132.00	192.00	192.00	20
0	(8+9)-VIII-3	-7580	28	7384	-2.70	0.37	4.07	132.00	192.00	192.00	43
0	(8+9)-II-1	-5897	17	5770	-2.10	0.23	3.18	132.00	192.00	192.00	56
0	(8+9)-III-1	2140	-19	-1970	0.76	-0.26	-1.09	132.00	192.00	192.00	78
0	(8+9)-I-1	1796	-18	-1639	0.64	-0.24	-0.90	132.00	192.00	192.00	93
0	(8+9)-VI-3	-8725	33	8490	-3.11	0.45	4.68	132.00	192.00	192.00	37
0	(8+9)-VI-4	5408	-26	-5146	1.92	-0.34	-2.84	132.00	192.00	192.00	32
0	(8+9)-VII-1	3722	-31	-3503	1.32	-0.42	-1.93	132.00	192.00	192.00	45
2293	1	91	-29	74	0.03	-0.38	0.04	79.20	115.20	115.20	>100
2293	2	175	-59	107	0.06	-0.79	0.06	118.80	172.80	172.80	>100
2293	3	175	-59	107	0.06	-0.79	0.06	118.80	172.80	172.80	>100
2293	4	91	-29	74	0.03	-0.38	0.04	105.60	153.60	153.60	>100
2293	5	91	-29	74	0.03	-0.38	0.04	105.60	153.60	153.60	>100
2293	6	91	-29	74	0.03	-0.38	0.04	105.60	153.60	153.60	>100
2293	7	91	-29	74	0.03	-0.38	0.04	105.60	153.60	153.60	>100
Verifiche nella direzione secondaria											
0	(8+9)-VIII-4	-2081	-71	8625	-1.87	-3.67	20.34	132.00	192.00	192.00	8.0
0	(8+9)-VII-2	-12792	-200	6792	-11.53	-10.32	16.01	132.00	192.00	192.00	7.1
0	(8+9)-III-3	6207	92	-5152	5.59	4.76	-12.15	132.00	192.00	192.00	7.7
0	(8+9)-IV-2	-7198	-142	10475	-6.49	-7.33	24.70	132.00	192.00	192.00	6.0
0	(8+9)-III-4	4264	36	625	3.84	1.86	1.47	132.00	192.00	192.00	22
0	(8+9)-VIII-2	-8071	-161	10890	-7.27	-8.30	25.68	132.00	192.00	192.00	5.6
0	(8+9)-IV-1	-721	45	-8780	-0.65	2.33	-20.70	132.00	192.00	192.00	8.3
0	(8+9)-VII-4	7174	99	-756	6.46	5.10	-1.78	132.00	192.00	192.00	12
0	(8+9)-I-1	-6633	-70	108	-5.98	-3.62	0.25	132.00	192.00	192.00	47
0	(8+9)-IV-3	3523	97	-10216	3.17	5.01	-24.09	132.00	192.00	192.00	5.7
0	(8+9)-I-3	7514	103	-4678	6.77	5.32	-11.03	132.00	192.00	192.00	7.3
0	(8+9)-IV-4	-2954	-90	9040	-2.66	-4.65	21.31	132.00	192.00	192.00	7.4

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-II-1	3634	82	-7201	3.27	4.21	-16.98	132.00	192.00	192.00	7.4
0	(8+9)-V-1	-9543	-133	1489	-8.60	-6.86	3.51	132.00	192.00	192.00	18
0	(8+9)-II-3	7878	134	-8637	7.10	6.89	-20.36	132.00	192.00	192.00	5.1
0	(8+9)-V-2	-14099	-211	6318	-12.70	-10.88	14.90	132.00	192.00	192.00	7.2
0	(8+9)-III-1	-7939	-81	-366	-7.15	-4.18	-0.86	132.00	192.00	192.00	36
0	(8+9)-V-3	10424	166	-6059	9.39	8.56	-14.29	132.00	192.00	192.00	5.3
0	(8+9)-VIII-3	4396	116	-10630	3.96	5.98	-25.06	132.00	192.00	192.00	5.2
0	(8+9)-V-4	5868	88	-1230	5.29	4.53	-2.90	132.00	192.00	192.00	13
0	(8+9)-VII-3	9117	155	-6533	8.22	8.00	-15.40	132.00	192.00	192.00	5.4
0	(8+9)-VI-1	2761	63	-6787	2.49	3.24	-16.00	132.00	192.00	192.00	8.4
0	(8+9)-I-4	2958	25	151	2.67	1.30	0.36	132.00	192.00	192.00	35
0	(8+9)-VI-2	-12426	-198	9310	-11.20	-10.18	21.95	132.00	192.00	192.00	5.9
0	(8+9)-II-4	-7309	-127	7460	-6.59	-6.53	17.59	132.00	192.00	192.00	7.9
0	(8+9)-VIII-1	-1594	26	-8366	-1.44	1.35	-19.72	132.00	192.00	192.00	9.1
0	(8+9)-I-2	-11189	-148	4937	-10.08	-7.64	11.64	132.00	192.00	192.00	9.7
0	(8+9)-II-2	-11553	-179	8896	-10.41	-9.21	20.97	132.00	192.00	192.00	6.2
0	(8+9)-III-2	-9882	-137	5411	-8.90	-7.08	12.76	132.00	192.00	192.00	9.5
0	(8+9)-VI-3	8751	153	-9051	7.89	7.86	-21.34	132.00	192.00	192.00	4.7
0	(8+9)-VI-4	-6436	-108	7046	-5.80	-5.56	16.61	132.00	192.00	192.00	8.6
0	(8+9)-VII-1	-10849	-144	1015	-9.78	-7.42	2.39	132.00	192.00	192.00	19
1935	1	-2069	25	545	-1.86	1.29	1.28	79.20	115.20	115.20	44
1935	2	-4071	52	1063	-3.67	2.66	2.51	118.80	172.80	172.80	33
1935	3	-4071	52	1063	-3.67	2.66	2.51	118.80	172.80	172.80	33
1935	4	-2069	25	545	-1.86	1.29	1.28	105.60	153.60	153.60	59
1935	5	-2069	25	545	-1.86	1.29	1.28	105.60	153.60	153.60	59
1935	6	-2069	25	545	-1.86	1.29	1.28	105.60	153.60	153.60	59
1935	7	-2069	25	545	-1.86	1.29	1.28	105.60	153.60	153.60	59

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Ty kg	τ_d kg/cmq	fvd kg/cmq	RS	Cs
0	1	-32	0.01	3.84	Si	>100
0	2	-66	0.02	5.76	Si	>100
0	3	-66	0.02	5.76	Si	>100
0	4	-32	0.01	5.12	Si	>100
0	5	-32	0.01	5.12	Si	>100
0	6	-32	0.01	5.12	Si	>100
0	7	-32	0.01	5.12	Si	>100
2293	(8+9)-VIII-4	45	0.01	6.40	Si	>100
2293	(8+9)-IV-1	-42	0.01	6.40	Si	>100
2293	(8+9)-V-1	91	0.02	6.40	Si	>100
2293	(8+9)-I-2	165	0.04	6.40	Si	>100
2293	(8+9)-V-2	153	0.04	6.40	Si	>100
2293	(8+9)-I-4	-102	0.03	6.40	Si	>100
2293	(8+9)-V-3	-153	0.04	6.40	Si	>100
2293	(8+9)-II-2	145	0.04	6.40	Si	>100
2293	(8+9)-V-4	-90	0.02	6.40	Si	>100
2293	(8+9)-II-4	64	0.02	6.40	Si	>100
2293	(8+9)-VI-1	-67	0.02	6.40	Si	>100
2293	(8+9)-III-2	158	0.04	6.40	Si	>100
2293	(8+9)-VI-2	141	0.04	6.40	Si	>100
2293	(8+9)-III-4	-109	0.03	6.40	Si	>100
2293	(8+9)-VI-3	-141	0.04	6.40	Si	>100
2293	(8+9)-IV-2	122	0.03	6.40	Si	>100
2293	(8+9)-VI-4	68	0.02	6.40	Si	>100
2293	(8+9)-IV-4	42	0.01	6.40	Si	>100
2293	(8+9)-VII-1	98	0.03	6.40	Si	>100
2293	(8+9)-II-1	-64	0.02	6.40	Si	>100
2293	(8+9)-VII-2	147	0.04	6.40	Si	>100
2293	(8+9)-III-1	109	0.03	6.40	Si	>100
2293	(8+9)-VII-3	-146	0.04	6.40	Si	>100
2293	(8+9)-I-1	102	0.03	6.40	Si	>100
2293	(8+9)-VII-4	-97	0.03	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
2293	(8+9)-III-3	-158	0.04	6.40	Si	>100
2293	(8+9)-IV-3	-122	0.03	6.40	Si	>100
2293	(8+9)-II-3	-144	0.04	6.40	Si	>100
2293	(8+9)-VIII-1	-45	0.01	6.40	Si	>100
2293	(8+9)-VIII-2	119	0.03	6.40	Si	>100
2293	(8+9)-VIII-3	-118	0.03	6.40	Si	>100
2293	(8+9)-I-3	-165	0.04	6.40	Si	>100
Verifiche nella direzione secondaria						
0	1	33	0.03	3.84	Si	>100
0	2	70	0.06	5.76	Si	98
0	3	70	0.06	5.76	Si	98
0	4	33	0.03	5.12	Si	>100
0	5	33	0.03	5.12	Si	>100
0	6	33	0.03	5.12	Si	>100
0	7	33	0.03	5.12	Si	>100
0	(8+9)-VII-4	-83	0.07	6.40	Si	93
0	(8+9)-VII-1	128	0.11	6.40	Si	60
0	(8+9)-V-4	-72	0.06	6.40	Si	>100
0	(8+9)-V-1	117	0.10	6.40	Si	66
1935	(8+9)-VIII-4	88	0.07	6.40	Si	87
1935	(8+9)-IV-2	150	0.13	6.40	Si	51
1935	(8+9)-V-3	-151	0.13	6.40	Si	51
1935	(8+9)-II-2	182	0.15	6.40	Si	42
1935	(8+9)-I-3	-95	0.08	6.40	Si	81
1935	(8+9)-II-4	137	0.11	6.40	Si	56
1935	(8+9)-VI-1	-77	0.06	6.40	Si	>100
1935	(8+9)-III-2	130	0.11	6.40	Si	59
1935	(8+9)-VI-2	199	0.17	6.40	Si	39
1935	(8+9)-III-4	-22	0.02	6.40	Si	>100
1935	(8+9)-VI-3	-155	0.13	6.40	Si	49
1935	(8+9)-II-1	-93	0.08	6.40	Si	83
1935	(8+9)-VI-4	120	0.10	6.40	Si	64
1935	(8+9)-IV-4	105	0.09	6.40	Si	73
1935	(8+9)-I-2	139	0.12	6.40	Si	55
1935	(8+9)-V-2	195	0.16	6.40	Si	39
1935	(8+9)-VII-2	185	0.15	6.40	Si	42
1935	(8+9)-III-1	66	0.05	6.40	Si	>100
1935	(8+9)-VII-3	-141	0.12	6.40	Si	54
1935	(8+9)-IV-1	-61	0.05	6.40	Si	>100
1935	(8+9)-I-1	56	0.05	6.40	Si	>100
1935	(8+9)-III-3	-86	0.07	6.40	Si	90
1935	(8+9)-IV-3	-107	0.09	6.40	Si	72
1935	(8+9)-II-3	-139	0.12	6.40	Si	55
1935	(8+9)-VIII-1	-44	0.04	6.40	Si	>100
1935	(8+9)-VIII-2	167	0.14	6.40	Si	46
1935	(8+9)-VIII-3	-123	0.10	6.40	Si	62
1935	(8+9)-I-4	-13	0.01	6.40	Si	>100

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	1	478	0.25	19.20	75	0.06	12.00	>100	V	75
0	2	1126	0.60	28.80	48	0.15	18.00	>100	V	48
0	3	1126	0.60	28.80	48	0.15	18.00	>100	V	48
0	4	478	0.25	25.60	>100	0.06	16.00	>100	V	>100
0	5	478	0.25	25.60	>100	0.06	16.00	>100	V	>100
0	6	478	0.25	25.60	>100	0.06	16.00	>100	V	>100
0	7	478	0.25	25.60	>100	0.06	16.00	>100	V	>100
1147	(8+9)-IV-2	-13744	-7.34	32.00	4.4	-1.78	20.00	11	V	4.4
1147	(8+9)-V-2	-14663	-7.83	32.00	4.1	-1.89	20.00	11	V	4.1
1147	(8+9)-I-2	-11378	-6.07	32.00	5.3	-1.47	20.00	14	V	5.3
1147	(8+9)-V-3	14913	7.96	32.00	4.0	1.93	20.00	10	V	4.0
1147	(8+9)-I-4	3566	1.90	32.00	17	0.46	20.00	43	V	17

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
1147	(8+9)-V-4	6852	3.66	32.00	8.7	0.89	20.00	23	V	8.7
1147	(8+9)-II-2	-15552	-8.30	32.00	3.9	-2.01	20.00	10.0	V	3.9
1147	(8+9)-VI-1	10333	5.52	32.00	5.8	1.33	20.00	15	V	5.8
1147	(8+9)-II-4	-11069	-5.91	32.00	5.4	-1.43	20.00	14	V	5.4
1147	(8+9)-VI-2	-16537	-8.83	32.00	3.6	-2.14	20.00	9.4	V	3.6
1147	(8+9)-III-2	-10835	-5.78	32.00	5.5	-1.40	20.00	14	V	5.5
1147	(8+9)-VI-3	16787	8.96	32.00	3.6	2.17	20.00	9.2	V	3.6
1147	(8+9)-III-4	4109	2.19	32.00	15	0.53	20.00	38	V	15
1147	(8+9)-VI-4	-10083	-5.38	32.00	5.9	-1.30	20.00	15	V	5.9
1147	(8+9)-I-1	-3317	-1.77	32.00	18	-0.43	20.00	47	V	18
1147	(8+9)-VII-1	-7144	-3.81	32.00	8.4	-0.92	20.00	22	V	8.4
1147	(8+9)-IV-4	-9261	-4.94	32.00	6.5	-1.20	20.00	17	V	6.5
1147	(8+9)-VII-2	-14121	-7.54	32.00	4.2	-1.82	20.00	11	V	4.2
1147	(8+9)-I-3	11627	6.21	32.00	5.2	1.50	20.00	13	V	5.2
1147	(8+9)-VII-3	14371	7.67	32.00	4.2	1.86	20.00	11	V	4.2
1147	(8+9)-II-3	15801	8.44	32.00	3.8	2.04	20.00	9.8	V	3.8
1147	(8+9)-VII-4	7394	3.95	32.00	8.1	0.96	20.00	21	V	8.1
1147	(8+9)-III-3	11085	5.92	32.00	5.4	1.43	20.00	14	V	5.4
1147	(8+9)-VIII-1	8525	4.55	32.00	7.0	1.10	20.00	18	V	7.0
1147	(8+9)-IV-3	13994	7.47	32.00	4.3	1.81	20.00	11	V	4.3
1147	(8+9)-VIII-2	-14730	-7.86	32.00	4.1	-1.90	20.00	11	V	4.1
1147	(8+9)-II-1	11318	6.04	32.00	5.3	1.46	20.00	14	V	5.3
1147	(8+9)-IV-1	9511	5.08	32.00	6.3	1.23	20.00	16	V	6.3
1147	(8+9)-V-1	-6602	-3.52	32.00	9.1	-0.85	20.00	23	V	9.1
1147	(8+9)-III-1	-3859	-2.06	32.00	16	-0.50	20.00	40	V	16
1147	(8+9)-VIII-3	14979	8.00	32.00	4.0	1.94	20.00	10	V	4.0
1147	(8+9)-VIII-4	-8275	-4.42	32.00	7.2	-1.07	20.00	19	V	7.2
Verifiche nella direzione secondaria										
0	(8+9)-VII-4	-5942	-5.35	32.00	6.0	-1.30	20.00	15	V	6.0
1935	(8+9)-VIII-4	6363	5.73	32.00	5.6	1.39	20.00	14	V	5.6
1935	(8+9)-VII-2	11296	10.18	32.00	3.1	2.46	20.00	8.1	V	3.1
1935	(8+9)-III-3	-8654	-7.80	32.00	4.1	-1.89	20.00	11	V	4.1
1935	(8+9)-IV-2	10736	9.67	32.00	3.3	2.34	20.00	8.5	V	3.3
1935	(8+9)-III-4	-3279	-2.95	32.00	11	-0.72	20.00	28	V	11
1935	(8+9)-VIII-2	11534	10.39	32.00	3.1	2.52	20.00	8.0	V	3.1
1935	(8+9)-IV-1	-7182	-6.47	32.00	4.9	-1.57	20.00	13	V	4.9
1935	(8+9)-VII-3	-11317	-10.20	32.00	3.1	-2.47	20.00	8.1	V	3.1
1935	(8+9)-I-2	9179	8.27	32.00	3.9	2.00	20.00	10.0	V	3.9
1935	(8+9)-IV-3	-10756	-9.69	32.00	3.3	-2.35	20.00	8.5	V	3.3
1935	(8+9)-I-4	-2734	-2.46	32.00	13	-0.60	20.00	34	V	13
1935	(8+9)-IV-4	7162	6.45	32.00	5.0	1.56	20.00	13	V	5.0
1935	(8+9)-II-2	12553	11.31	32.00	2.8	2.74	20.00	7.3	V	2.8
1935	(8+9)-V-1	5376	4.84	32.00	6.6	1.17	20.00	17	V	6.6
1935	(8+9)-II-4	8979	8.09	32.00	4.0	1.96	20.00	10	V	4.0
1935	(8+9)-V-2	11842	10.67	32.00	3.0	2.58	20.00	7.7	V	3.0
1935	(8+9)-III-2	8634	7.78	32.00	4.1	1.88	20.00	11	V	4.1
1935	(8+9)-V-3	-11862	-10.69	32.00	3.0	-2.59	20.00	7.7	V	3.0
1935	(8+9)-VIII-1	-6383	-5.75	32.00	5.6	-1.39	20.00	14	V	5.6
1935	(8+9)-V-4	-5396	-4.86	32.00	6.6	-1.18	20.00	17	V	6.6
1935	(8+9)-I-3	-9200	-8.29	32.00	3.9	-2.01	20.00	10.0	V	3.9
1935	(8+9)-VI-1	-8201	-7.39	32.00	4.3	-1.79	20.00	11	V	4.3
1935	(8+9)-II-3	-12574	-11.33	32.00	2.8	-2.74	20.00	7.3	V	2.8
1935	(8+9)-VI-2	13352	12.03	32.00	2.7	2.91	20.00	6.9	V	2.7
1935	(8+9)-VIII-3	-11555	-10.41	32.00	3.1	-2.52	20.00	7.9	V	3.1
1935	(8+9)-II-1	-9000	-8.11	32.00	3.9	-1.96	20.00	10	V	3.9
1935	(8+9)-III-1	3259	2.94	32.00	11	0.71	20.00	28	V	11
1935	(8+9)-I-1	2713	2.44	32.00	13	0.59	20.00	34	V	13
1935	(8+9)-VI-3	-13372	-12.05	32.00	2.7	-2.92	20.00	6.9	V	2.7
1935	(8+9)-VI-4	8181	7.37	32.00	4.3	1.78	20.00	11	V	4.3
1935	(8+9)-VII-1	5921	5.34	32.00	6.0	1.29	20.00	15	V	6.0
3870	1	-111	-0.10	19.20	>100	-0.02	12.00	>100	V	>100
3870	2	-309	-0.28	28.80	>100	-0.07	18.00	>100	V	>100
3870	3	-309	-0.28	28.80	>100	-0.07	18.00	>100	V	>100
3870	4	-111	-0.10	25.60	>100	-0.02	16.00	>100	V	>100

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
3870	5	-111	-0.10	25.60	>100	-0.02	16.00	>100	V	>100
3870	6	-111	-0.10	25.60	>100	-0.02	16.00	>100	V	>100
3870	7	-111	-0.10	25.60	>100	-0.02	16.00	>100	V	>100

Setto 36: origine (1429.0,2214.1,193.5), direzione (-0.200098,0.979776,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	1	2993	130	-4535	1.07	1.74	-2.50	79.20	115.20	115.20	20
0	2	6191	270	-9363	2.20	3.61	-5.17	118.80	172.80	172.80	14
0	3	6191	270	-9363	2.20	3.61	-5.17	118.80	172.80	172.80	14
0	4	2993	130	-4535	1.07	1.74	-2.50	105.60	153.60	153.60	27
0	5	2993	130	-4535	1.07	1.74	-2.50	105.60	153.60	153.60	27
0	6	2993	130	-4535	1.07	1.74	-2.50	105.60	153.60	153.60	27
0	7	2993	130	-4535	1.07	1.74	-2.50	105.60	153.60	153.60	27
0	(8+9)-VIII-4	5105	93	-6677	1.82	1.24	-3.68	132.00	192.00	192.00	25
0	(8+9)-IV-1	-1342	92	892	-0.48	1.22	0.49	132.00	192.00	192.00	>100
0	(8+9)-V-1	4628	79	-6204	1.65	1.06	-3.42	132.00	192.00	192.00	28
0	(8+9)-I-2	6469	95	-8208	2.30	1.26	-4.53	132.00	192.00	192.00	21
0	(8+9)-V-2	7722	79	-9825	2.75	1.06	-5.42	132.00	192.00	192.00	18
0	(8+9)-I-4	763	85	-1683	0.27	1.14	-0.93	132.00	192.00	192.00	78
0	(8+9)-V-3	-3583	101	3555	-1.28	1.34	1.96	132.00	192.00	192.00	58
0	(8+9)-II-2	8081	91	-10149	2.88	1.22	-5.60	132.00	192.00	192.00	17
0	(8+9)-V-4	-490	101	-66	-0.17	1.34	-0.04	132.00	192.00	192.00	>100
0	(8+9)-II-4	6369	89	-8192	2.27	1.18	-4.52	132.00	192.00	192.00	21
0	(8+9)-VI-1	-1855	87	1437	-0.66	1.16	0.79	132.00	192.00	192.00	98
0	(8+9)-III-2	6203	94	-7899	2.21	1.26	-4.36	132.00	192.00	192.00	22
0	(8+9)-VI-2	8457	87	-10634	3.01	1.16	-5.87	132.00	192.00	192.00	17
0	(8+9)-III-4	496	85	-1374	0.18	1.14	-0.76	132.00	192.00	192.00	89
0	(8+9)-VI-3	-4318	93	4365	-1.54	1.24	2.41	132.00	192.00	192.00	52
0	(8+9)-IV-2	7193	91	-9119	2.56	1.22	-5.03	132.00	192.00	192.00	19
0	(8+9)-VI-4	5993	93	-7707	2.13	1.25	-4.25	132.00	192.00	192.00	22
0	(8+9)-IV-4	5481	88	-7162	1.95	1.18	-3.95	132.00	192.00	192.00	24
0	(8+9)-VII-1	4895	79	-6512	1.74	1.06	-3.59	132.00	192.00	192.00	27
0	(8+9)-II-1	-2231	91	1922	-0.79	1.22	1.06	132.00	192.00	192.00	84
0	(8+9)-VII-2	7455	79	-9516	2.65	1.06	-5.25	132.00	192.00	192.00	19
0	(8+9)-III-1	3642	95	-4896	1.30	1.26	-2.70	132.00	192.00	192.00	33
0	(8+9)-VII-3	-3317	101	3246	-1.18	1.34	1.79	132.00	192.00	192.00	61
0	(8+9)-I-1	3376	95	-4587	1.20	1.26	-2.53	132.00	192.00	192.00	35
0	(8+9)-VII-4	-756	100	243	-0.27	1.34	0.13	132.00	192.00	192.00	>100
0	(8+9)-III-3	-2064	85	1629	-0.73	1.14	0.90	132.00	192.00	192.00	94
0	(8+9)-IV-3	-3054	89	2850	-1.09	1.19	1.57	132.00	192.00	192.00	69
0	(8+9)-II-3	-3943	89	3880	-1.40	1.18	2.14	132.00	192.00	192.00	58
0	(8+9)-VIII-1	-967	87	407	-0.34	1.16	0.22	132.00	192.00	192.00	>100
0	(8+9)-VIII-2	7568	87	-9604	2.69	1.16	-5.30	132.00	192.00	192.00	19
0	(8+9)-VIII-3	-3430	93	3335	-1.22	1.25	1.84	132.00	192.00	192.00	62
0	(8+9)-I-3	-2331	85	1938	-0.83	1.14	1.07	132.00	192.00	192.00	87
Verifiche nella direzione secondaria											
0	(8+9)-VIII-4	-2318	-27	3217	-4.76	-3.12	39.32	132.00	192.00	192.00	4.5
0	(8+9)-VI-2	-2649	-79	6700	-5.43	-9.33	81.90	132.00	192.00	192.00	2.1
0	(8+9)-VI-4	-2447	-36	4104	-5.02	-4.26	50.17	132.00	192.00	192.00	3.5
0	(8+9)-IV-2	-2438	-63	5440	-5.00	-7.40	66.51	132.00	192.00	192.00	2.6
0	(8+9)-III-2	-2421	-81	4342	-4.97	-9.45	53.09	132.00	192.00	192.00	3.1
0	(8+9)-VIII-2	-2520	-70	5813	-5.17	-8.19	71.06	132.00	192.00	192.00	2.4
0	(8+9)-III-3	-2244	34	-4622	-4.60	3.95	-56.51	132.00	192.00	192.00	3.2
0	(8+9)-VII-4	-2022	41	-3071	-4.15	4.82	-37.54	132.00	192.00	192.00	4.5
0	(8+9)-VI-3	-2016	33	-6980	-4.14	3.83	-85.33	132.00	192.00	192.00	2.2
0	(8+9)-VII-2	-2695	-103	5583	-5.53	-12.07	68.26	132.00	192.00	192.00	2.4
0	(8+9)-IV-1	-2265	-14	-3869	-4.65	-1.60	-47.30	132.00	192.00	192.00	3.9
0	(8+9)-I-3	-2205	37	-4889	-4.52	4.29	-59.76	132.00	192.00	192.00	3.0
0	(8+9)-II-1	-2136	-4	-4756	-4.38	-0.46	-58.14	132.00	192.00	192.00	3.3
0	(8+9)-IV-3	-2227	16	-5721	-4.57	1.90	-69.93	132.00	192.00	192.00	2.7
0	(8+9)-II-3	-2098	26	-6608	-4.30	3.04	-80.78	132.00	192.00	192.00	2.3

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-IV-4	-2400	-33	3589	-4.92	-3.91	43.87	132.00	192.00	192.00	4.0
0	(8+9)-VIII-3	-2145	23	-6093	-4.40	2.69	-74.48	132.00	192.00	192.00	2.5
0	(8+9)-V-1	-2605	-85	2524	-5.34	-9.99	30.86	132.00	192.00	192.00	4.7
0	(8+9)-VII-3	-1970	56	-5863	-4.04	6.57	-71.68	132.00	192.00	192.00	2.5
0	(8+9)-V-2	-2734	-106	5849	-5.61	-12.41	71.51	132.00	192.00	192.00	2.3
0	(8+9)-VII-1	-2643	-88	2791	-5.42	-10.33	34.11	132.00	192.00	192.00	4.3
0	(8+9)-II-4	-2529	-43	4476	-5.19	-5.05	54.72	132.00	192.00	192.00	3.2
0	(8+9)-VIII-1	-2347	-20	-3497	-4.82	-2.38	-42.75	132.00	192.00	192.00	4.2
0	(8+9)-I-2	-2460	-83	4609	-5.05	-9.79	56.34	132.00	192.00	192.00	2.9
0	(8+9)-II-2	-2567	-73	6327	-5.27	-8.55	77.35	132.00	192.00	192.00	2.2
0	(8+9)-V-3	-1931	59	-6129	-3.96	6.91	-74.93	132.00	192.00	192.00	2.3
0	(8+9)-V-4	-2060	38	-2804	-4.23	4.48	-34.28	132.00	192.00	192.00	4.9
0	(8+9)-VI-1	-2218	-11	-4384	-4.55	-1.24	-53.59	132.00	192.00	192.00	3.5
3870	1	-3947	215	1825	-8.10	25.23	22.31	79.20	115.20	115.20	2.4
3870	2	-8155	446	3793	-16.73	52.41	46.37	118.80	172.80	172.80	1.7
3870	3	-8155	446	3793	-16.73	52.41	46.37	118.80	172.80	172.80	1.7
3870	4	-3947	215	1825	-8.10	25.23	22.31	105.60	153.60	153.60	3.2
3870	5	-3947	215	1825	-8.10	25.23	22.31	105.60	153.60	153.60	3.2
3870	6	-3947	215	1825	-8.10	25.23	22.31	105.60	153.60	153.60	3.2
3870	7	-3947	215	1825	-8.10	25.23	22.31	105.60	153.60	153.60	3.2
3870	(8+9)-I-1	-3426	153	1192	-7.03	17.98	14.57	132.00	192.00	192.00	5.9
3870	(8+9)-I-4	-2024	143	1325	-4.15	16.82	16.20	132.00	192.00	192.00	5.8
3870	(8+9)-III-1	-3448	154	1140	-7.07	18.05	13.94	132.00	192.00	192.00	6.0
3870	(8+9)-III-4	-2002	143	1377	-4.11	16.74	16.83	132.00	192.00	192.00	5.7

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
0	(8+9)-V-1	-167	0.04	6.40	Si	>100
0	(8+9)-VIII-2	-124	0.03	6.40	Si	>100
0	(8+9)-VII-3	53	0.01	6.40	Si	>100
0	(8+9)-V-2	-187	0.05	6.40	Si	>100
0	(8+9)-V-3	56	0.01	6.40	Si	>100
0	(8+9)-VI-2	-132	0.03	6.40	Si	>100
0	(8+9)-VII-1	-169	0.04	6.40	Si	>100
0	(8+9)-VII-2	-184	0.05	6.40	Si	>100
504	1	-130	0.03	3.84	Si	>100
504	2	-269	0.07	5.76	Si	83
504	3	-269	0.07	5.76	Si	83
504	4	-130	0.03	5.12	Si	>100
504	5	-130	0.03	5.12	Si	>100
504	6	-130	0.03	5.12	Si	>100
504	7	-130	0.03	5.12	Si	>100
504	(8+9)-IV-4	-106	0.03	6.40	Si	>100
504	(8+9)-VI-4	-110	0.03	6.40	Si	>100
504	(8+9)-III-2	-113	0.03	6.40	Si	>100
504	(8+9)-I-4	-82	0.02	6.40	Si	>100
504	(8+9)-III-4	-79	0.02	6.40	Si	>100
504	(8+9)-I-3	-63	0.02	6.40	Si	>100
504	(8+9)-IV-2	-116	0.03	6.40	Si	>100
504	(8+9)-I-2	-115	0.03	6.40	Si	>100
504	(8+9)-III-1	-100	0.03	6.40	Si	>100
504	(8+9)-VII-4	-64	0.02	6.40	Si	>100
504	(8+9)-II-3	-54	0.01	6.40	Si	>100
504	(8+9)-VIII-1	-77	0.02	6.40	Si	>100
504	(8+9)-V-4	-67	0.02	6.40	Si	>100
504	(8+9)-I-1	-97	0.03	6.40	Si	>100
504	(8+9)-II-1	-64	0.02	6.40	Si	>100
504	(8+9)-VIII-3	-58	0.02	6.40	Si	>100
504	(8+9)-III-3	-66	0.02	6.40	Si	>100
504	(8+9)-VIII-4	-102	0.03	6.40	Si	>100
504	(8+9)-IV-3	-63	0.02	6.40	Si	>100
504	(8+9)-II-2	-125	0.03	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
504	(8+9)-VI-1	-69	0.02	6.40	Si	>100
504	(8+9)-VI-3	-49	0.01	6.40	Si	>100
504	(8+9)-IV-1	-73	0.02	6.40	Si	>100
504	(8+9)-II-4	-115	0.03	6.40	Si	>100
Verifiche nella direzione secondaria						
0	(8+9)-V-3	-9	0.02	6.40	Si	>100
0	(8+9)-VII-3	-8	0.01	6.40	Si	>100
1935	(8+9)-VII-4	3	0.01	6.40	Si	>100
1935	(8+9)-V-4	4	0.01	6.40	Si	>100
3870	1	169	0.32	3.84	Si	12
3870	2	352	0.67	5.76	Si	8.7
3870	3	352	0.67	5.76	Si	8.7
3870	4	169	0.32	5.12	Si	16
3870	5	169	0.32	5.12	Si	16
3870	6	169	0.32	5.12	Si	16
3870	7	169	0.32	5.12	Si	16
3870	(8+9)-VIII-4	76	0.14	6.40	Si	44
3870	(8+9)-IV-4	112	0.21	6.40	Si	30
3870	(8+9)-I-4	120	0.23	6.40	Si	28
3870	(8+9)-II-2	110	0.21	6.40	Si	31
3870	(8+9)-I-3	123	0.23	6.40	Si	27
3870	(8+9)-II-4	113	0.21	6.40	Si	30
3870	(8+9)-VI-1	157	0.30	6.40	Si	22
3870	(8+9)-III-2	110	0.21	6.40	Si	31
3870	(8+9)-VI-2	146	0.28	6.40	Si	23
3870	(8+9)-III-4	120	0.23	6.40	Si	28
3870	(8+9)-VI-3	87	0.17	6.40	Si	39
3870	(8+9)-IV-2	109	0.21	6.40	Si	31
3870	(8+9)-VI-4	77	0.15	6.40	Si	44
3870	(8+9)-II-1	120	0.23	6.40	Si	28
3870	(8+9)-VII-1	234	0.44	6.40	Si	14
3870	(8+9)-V-2	230	0.44	6.40	Si	15
3870	(8+9)-VII-2	230	0.44	6.40	Si	15
3870	(8+9)-III-1	113	0.21	6.40	Si	30
3870	(8+9)-I-2	110	0.21	6.40	Si	31
3870	(8+9)-IV-1	121	0.23	6.40	Si	28
3870	(8+9)-I-1	113	0.21	6.40	Si	30
3870	(8+9)-III-3	123	0.23	6.40	Si	27
3870	(8+9)-IV-3	124	0.23	6.40	Si	27
3870	(8+9)-II-3	124	0.23	6.40	Si	27
3870	(8+9)-VIII-1	157	0.30	6.40	Si	22
3870	(8+9)-VIII-2	146	0.28	6.40	Si	23
3870	(8+9)-VIII-3	88	0.17	6.40	Si	38
3870	(8+9)-V-1	234	0.44	6.40	Si	14

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	(8+9)-IV-2	-9900	-5.29	32.00	6.1	-1.28	20.00	16	V	6.1
0	(8+9)-VIII-2	-10833	-5.78	32.00	5.5	-1.40	20.00	14	V	5.5
0	(8+9)-VII-1	-5816	-3.10	32.00	10	-0.75	20.00	27	V	10
0	(8+9)-I-1	-2223	-1.19	32.00	27	-0.29	20.00	70	V	27
0	(8+9)-III-2	-8010	-4.28	32.00	7.5	-1.03	20.00	19	V	7.5
0	(8+9)-III-1	-2707	-1.45	32.00	22	-0.35	20.00	57	V	22
0	(8+9)-V-2	-11603	-6.19	32.00	5.2	-1.50	20.00	13	V	5.2
0	(8+9)-V-1	-5332	-2.85	32.00	11	-0.69	20.00	29	V	11
0	(8+9)-I-2	-8494	-4.53	32.00	7.1	-1.10	20.00	18	V	7.1
0	(8+9)-VI-2	-12447	-6.65	32.00	4.8	-1.61	20.00	12	V	4.8
0	(8+9)-VII-2	-11119	-5.94	32.00	5.4	-1.44	20.00	14	V	5.4
504	1	2408	1.29	19.20	15	0.31	12.00	39	V	15
504	2	5036	2.69	28.80	11	0.65	18.00	28	V	11
504	3	5036	2.69	28.80	11	0.65	18.00	28	V	11
504	4	2408	1.29	25.60	20	0.31	16.00	51	V	20

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
504	5	2408	1.29	25.60	20	0.31	16.00	51	V	20
504	6	2408	1.29	25.60	20	0.31	16.00	51	V	20
504	7	2408	1.29	25.60	20	0.31	16.00	51	V	20
504	(8+9)-V-4	7150	3.82	32.00	8.4	0.92	20.00	22	V	8.4
504	(8+9)-VIII-1	8154	4.35	32.00	7.4	1.05	20.00	19	V	7.4
504	(8+9)-IV-1	8988	4.80	32.00	6.7	1.16	20.00	17	V	6.7
504	(8+9)-I-3	10850	5.79	32.00	5.5	1.40	20.00	14	V	5.5
504	(8+9)-IV-3	12558	6.70	32.00	4.8	1.62	20.00	12	V	4.8
504	(8+9)-VIII-3	13393	7.15	32.00	4.5	1.73	20.00	12	V	4.5
504	(8+9)-III-3	10343	5.52	32.00	5.8	1.34	20.00	15	V	5.8
504	(8+9)-VII-4	7656	4.09	32.00	7.8	0.99	20.00	20	V	7.8
504	(8+9)-III-4	4875	2.60	32.00	12	0.63	20.00	32	V	12
504	(8+9)-VI-1	9842	5.25	32.00	6.1	1.27	20.00	16	V	6.1
504	(8+9)-V-3	13631	7.28	32.00	4.4	1.76	20.00	11	V	4.4
504	(8+9)-VI-3	15081	8.05	32.00	4.0	1.95	20.00	10	V	4.0
504	(8+9)-II-3	14246	7.61	32.00	4.2	1.84	20.00	11	V	4.2
504	(8+9)-II-1	10677	5.70	32.00	5.6	1.38	20.00	14	V	5.6
504	(8+9)-I-4	4369	2.33	32.00	14	0.56	20.00	35	V	14
504	(8+9)-VII-3	13125	7.01	32.00	4.6	1.70	20.00	12	V	4.6
1007	(8+9)-VIII-4	-5531	-2.95	32.00	11	-0.71	20.00	28	V	11
1007	(8+9)-VI-4	-7221	-3.86	32.00	8.3	-0.93	20.00	21	V	8.3
1007	(8+9)-IV-4	-6238	-3.33	32.00	9.6	-0.81	20.00	25	V	9.6
1007	(8+9)-II-4	-7927	-4.23	32.00	7.6	-1.02	20.00	20	V	7.6
1007	(8+9)-II-2	-11552	-6.17	32.00	5.2	-1.49	20.00	13	V	5.2
Verifiche nella direzione secondaria										
0	(8+9)-V-1	1900	3.90	32.00	8.2	0.94	20.00	21	V	8.2
0	(8+9)-VII-3	-4682	-9.61	32.00	3.3	-2.32	20.00	8.6	V	3.3
0	(8+9)-VI-3	-5518	-11.32	32.00	2.8	-2.74	20.00	7.3	V	2.8
0	(8+9)-VIII-3	-4828	-9.91	32.00	3.2	-2.40	20.00	8.3	V	3.2
0	(8+9)-VI-2	5105	10.47	32.00	3.1	2.53	20.00	7.9	V	3.1
0	(8+9)-VII-2	4269	8.76	32.00	3.7	2.12	20.00	9.4	V	3.7
0	(8+9)-VII-1	2107	4.32	32.00	7.4	1.05	20.00	19	V	7.4
0	(8+9)-VIII-2	4415	9.06	32.00	3.5	2.19	20.00	9.1	V	3.5
0	(8+9)-VII-4	-2520	-5.17	32.00	6.2	-1.25	20.00	16	V	6.2
0	(8+9)-V-4	-2313	-4.75	32.00	6.7	-1.15	20.00	17	V	6.7
0	(8+9)-V-3	-4889	-10.03	32.00	3.2	-2.43	20.00	8.2	V	3.2
0	(8+9)-V-2	4475	9.18	32.00	3.5	2.22	20.00	9.0	V	3.5
1935	(8+9)-VIII-4	2402	4.93	32.00	6.5	1.19	20.00	17	V	6.5
1935	(8+9)-I-3	-3885	-7.97	32.00	4.0	-1.93	20.00	10	V	4.0
1935	(8+9)-II-3	-5222	-10.71	32.00	3.0	-2.59	20.00	7.7	V	3.0
1935	(8+9)-VI-1	-3502	-7.19	32.00	4.5	-1.74	20.00	12	V	4.5
1935	(8+9)-III-1	1098	2.25	32.00	14	0.55	20.00	37	V	14
1935	(8+9)-I-2	3472	7.12	32.00	4.5	1.72	20.00	12	V	4.5
1935	(8+9)-III-3	-3679	-7.55	32.00	4.2	-1.83	20.00	11	V	4.2
1935	(8+9)-I-1	892	1.83	32.00	17	0.44	20.00	45	V	17
1935	(8+9)-IV-1	-3102	-6.36	32.00	5.0	-1.54	20.00	13	V	5.0
1935	(8+9)-VI-4	3089	6.34	32.00	5.0	1.53	20.00	13	V	5.0
1935	(8+9)-IV-3	-4535	-9.30	32.00	3.4	-2.25	20.00	8.9	V	3.4
1935	(8+9)-II-2	4808	9.87	32.00	3.2	2.39	20.00	8.4	V	3.2
1935	(8+9)-II-1	-3788	-7.77	32.00	4.1	-1.88	20.00	11	V	4.1
1935	(8+9)-VIII-1	-2815	-5.78	32.00	5.5	-1.40	20.00	14	V	5.5
1935	(8+9)-II-4	3375	6.93	32.00	4.6	1.68	20.00	12	V	4.6
1935	(8+9)-III-2	3266	6.70	32.00	4.8	1.62	20.00	12	V	4.8
1935	(8+9)-IV-4	2689	5.52	32.00	5.8	1.34	20.00	15	V	5.8
1935	(8+9)-IV-2	4122	8.46	32.00	3.8	2.05	20.00	9.8	V	3.8
3870	1	-783	-1.61	19.20	12	-0.39	12.00	31	V	12
3870	2	-1688	-3.46	28.80	8.3	-0.84	18.00	21	V	8.3
3870	3	-1688	-3.46	28.80	8.3	-0.84	18.00	21	V	8.3
3870	4	-783	-1.61	25.60	16	-0.39	16.00	41	V	16
3870	5	-783	-1.61	25.60	16	-0.39	16.00	41	V	16
3870	6	-783	-1.61	25.60	16	-0.39	16.00	41	V	16
3870	7	-783	-1.61	25.60	16	-0.39	16.00	41	V	16
3870	(8+9)-III-4	-1626	-3.34	32.00	9.6	-0.81	20.00	25	V	9.6
3870	(8+9)-I-4	-1471	-3.02	32.00	11	-0.73	20.00	27	V	11

Setto 37: origine (1460.0,2062.0,193.5), direzione (-0.200098,0.979776,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	1	262	-218	-458	0.09	-2.92	-0.25	79.20	115.20	115.20	35
0	2	611	-454	-941	0.22	-6.06	-0.52	118.80	172.80	172.80	25
0	3	611	-454	-941	0.22	-6.06	-0.52	118.80	172.80	172.80	25
0	4	262	-218	-458	0.09	-2.92	-0.25	105.60	153.60	153.60	46
0	5	262	-218	-458	0.09	-2.92	-0.25	105.60	153.60	153.60	46
0	6	262	-218	-458	0.09	-2.92	-0.25	105.60	153.60	153.60	46
0	7	262	-218	-458	0.09	-2.92	-0.25	105.60	153.60	153.60	46
0	(8+9)-VIII-4	1520	-81	-2373	0.54	-1.08	-1.31	132.00	192.00	192.00	61
0	(8+9)-IV-1	-1601	-226	2794	-0.57	-3.02	1.54	132.00	192.00	192.00	42
0	(8+9)-V-1	2763	-130	-5863	0.98	-1.74	-3.24	132.00	192.00	192.00	30
0	(8+9)-I-2	3057	-89	-5379	1.09	-1.19	-2.97	132.00	192.00	192.00	33
0	(8+9)-V-2	4536	-70	-8923	1.61	-0.93	-4.92	132.00	192.00	192.00	23
0	(8+9)-I-4	-921	-151	1677	-0.33	-2.02	0.93	132.00	192.00	192.00	65
0	(8+9)-V-3	-4174	-231	8281	-1.49	-3.09	4.57	132.00	192.00	192.00	25
0	(8+9)-II-2	3734	-41	-6479	1.33	-0.54	-3.58	132.00	192.00	192.00	32
0	(8+9)-V-4	-2400	-171	5221	-0.85	-2.28	2.88	132.00	192.00	192.00	37
0	(8+9)-II-4	2540	-59	-4362	0.90	-0.79	-2.41	132.00	192.00	192.00	43
0	(8+9)-VI-1	-1734	-236	2657	-0.62	-3.15	1.47	132.00	192.00	192.00	42
0	(8+9)-III-2	2884	-94	-5101	1.03	-1.26	-2.81	132.00	192.00	192.00	35
0	(8+9)-VI-2	4177	-35	-7542	1.49	-0.47	-4.16	132.00	192.00	192.00	28
0	(8+9)-III-4	-1094	-156	1955	-0.39	-2.09	1.08	132.00	192.00	192.00	61
0	(8+9)-VI-3	-3815	-266	6900	-1.36	-3.56	3.81	132.00	192.00	192.00	26
0	(8+9)-IV-2	3157	-56	-5553	1.12	-0.75	-3.06	132.00	192.00	192.00	35
0	(8+9)-VI-4	2096	-65	-3299	0.75	-0.87	-1.82	132.00	192.00	192.00	51
0	(8+9)-IV-4	1964	-75	-3436	0.70	-1.00	-1.90	132.00	192.00	192.00	49
0	(8+9)-VII-1	2936	-126	-6141	1.04	-1.68	-3.39	132.00	192.00	192.00	29
0	(8+9)-II-1	-2178	-242	3720	-0.78	-3.23	2.05	132.00	192.00	192.00	36
0	(8+9)-VII-2	4363	-75	-8645	1.55	-1.00	-4.77	132.00	192.00	192.00	24
0	(8+9)-III-1	1456	-145	-2597	0.52	-1.94	-1.43	132.00	192.00	192.00	47
0	(8+9)-VII-3	-4001	-226	8003	-1.42	-3.03	4.42	132.00	192.00	192.00	26
0	(8+9)-I-1	1284	-150	-2319	0.46	-2.00	-1.28	132.00	192.00	192.00	49
0	(8+9)-VII-4	-2573	-175	5499	-0.92	-2.35	3.03	132.00	192.00	192.00	36
0	(8+9)-III-3	-2522	-207	4459	-0.90	-2.77	2.46	132.00	192.00	192.00	37
0	(8+9)-IV-3	-2795	-245	4911	-0.99	-3.27	2.71	132.00	192.00	192.00	32
0	(8+9)-II-3	-3371	-260	5837	-1.20	-3.48	3.22	132.00	192.00	192.00	29
0	(8+9)-VIII-1	-1158	-220	1731	-0.41	-2.95	0.95	132.00	192.00	192.00	49
0	(8+9)-VIII-2	3601	-50	-6616	1.28	-0.67	-3.65	132.00	192.00	192.00	31
0	(8+9)-VIII-3	-3239	-251	5974	-1.15	-3.35	3.30	132.00	192.00	192.00	29
0	(8+9)-I-3	-2695	-212	4737	-0.96	-2.83	2.61	132.00	192.00	192.00	35
Verifiche nella direzione secondaria											
0	(8+9)-VIII-4	5676	37	390	21.25	7.84	15.87	132.00	192.00	192.00	3.5
0	(8+9)-VII-2	2541	-221	1776	9.51	-47.41	72.24	132.00	192.00	192.00	1.4
0	(8+9)-III-3	-3748	76	-1981	-14.03	16.20	-80.61	132.00	192.00	192.00	2.0
0	(8+9)-IV-2	6307	-48	1358	23.61	-10.30	55.26	132.00	192.00	192.00	1.9
0	(8+9)-III-4	440	61	-1451	1.65	13.08	-59.05	132.00	192.00	192.00	2.6
0	(8+9)-VIII-2	6484	-90	1315	24.27	-19.34	53.50	132.00	192.00	192.00	1.8
0	(8+9)-VII-4	-152	202	-1307	-0.57	43.19	-53.17	132.00	192.00	192.00	2.0
0	(8+9)-VII-1	-1647	-207	1246	-6.17	-44.29	50.68	132.00	192.00	192.00	2.0
0	(8+9)-VII-3	-4340	216	-1837	-16.24	46.31	-74.73	132.00	192.00	192.00	1.6
0	(8+9)-I-1	-2551	-62	1332	-9.55	-13.35	54.17	132.00	192.00	192.00	2.8
0	(8+9)-I-3	-4060	80	-2040	-15.20	17.03	-83.00	132.00	192.00	192.00	1.9
0	(8+9)-IV-3	-8106	43	-1420	-30.34	9.21	-57.75	132.00	192.00	192.00	2.7
0	(8+9)-II-1	-8694	13	-604	-32.54	2.85	-24.55	132.00	192.00	192.00	5.8
0	(8+9)-IV-4	5854	-6	347	21.91	-1.19	14.11	132.00	192.00	192.00	4.1
0	(8+9)-II-3	-9147	56	-1615	-34.24	11.97	-65.70	132.00	192.00	192.00	2.3
0	(8+9)-V-1	-1959	-203	1187	-7.33	-43.46	48.30	132.00	192.00	192.00	2.1
0	(8+9)-III-1	-2239	-66	1390	-8.38	-14.18	56.56	132.00	192.00	192.00	2.7
0	(8+9)-V-2	2853	-225	1834	10.68	-48.23	74.63	132.00	192.00	192.00	1.4
0	(8+9)-VIII-3	-8283	85	-1376	-31.00	18.24	-55.99	132.00	192.00	192.00	2.4

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-V-3	-4652	220	-1896	-17.41	47.14	-77.12	132.00	192.00	192.00	1.5
0	(8+9)-I-2	2261	-85	1979	8.46	-18.12	80.50	132.00	192.00	192.00	1.7
0	(8+9)-V-4	160	198	-1248	0.60	42.37	-50.79	132.00	192.00	192.00	2.0
0	(8+9)-II-2	7348	-61	1554	27.50	-13.06	63.21	132.00	192.00	192.00	1.7
0	(8+9)-VI-1	-8517	-29	-647	-31.88	-6.18	-26.32	132.00	192.00	192.00	5.1
0	(8+9)-III-2	1949	-81	1920	7.29	-17.30	78.12	132.00	192.00	192.00	1.8
0	(8+9)-I-4	752	57	-1393	2.82	12.26	-56.67	132.00	192.00	192.00	2.6
0	(8+9)-II-4	6895	-18	542	25.81	-3.94	22.06	132.00	192.00	192.00	3.0
0	(8+9)-VIII-1	-7475	-42	-451	-27.98	-8.94	-18.37	132.00	192.00	192.00	6.1
0	(8+9)-VI-2	7525	-103	1510	28.17	-22.09	61.45	132.00	192.00	192.00	1.5
0	(8+9)-VI-3	-9324	98	-1572	-34.90	21.00	-63.94	132.00	192.00	192.00	2.1
0	(8+9)-VI-4	6717	24	586	25.14	5.09	23.82	132.00	192.00	192.00	2.9
1935	(8+9)-IV-1	2590	-11	134	9.69	-2.42	5.43	132.00	192.00	192.00	8.7
3870	1	-167	54	-34	-0.62	11.50	-1.40	79.20	115.20	115.20	8.9
3870	2	-362	112	-69	-1.36	24.04	-2.82	118.80	172.80	172.80	6.4
3870	3	-362	112	-69	-1.36	24.04	-2.82	118.80	172.80	172.80	6.4
3870	4	-167	54	-34	-0.62	11.50	-1.40	105.60	153.60	153.60	12
3870	5	-167	54	-34	-0.62	11.50	-1.40	105.60	153.60	153.60	12
3870	6	-167	54	-34	-0.62	11.50	-1.40	105.60	153.60	153.60	12
3870	7	-167	54	-34	-0.62	11.50	-1.40	105.60	153.60	153.60	12

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
0	(8+9)-V-1	567	0.15	6.40	Si	44
0	(8+9)-II-2	129	0.03	6.40	Si	>100
0	(8+9)-VI-1	390	0.10	6.40	Si	63
0	(8+9)-I-3	365	0.09	6.40	Si	68
0	(8+9)-VII-1	565	0.15	6.40	Si	44
0	(8+9)-I-4	326	0.08	6.40	Si	76
0	(8+9)-V-2	528	0.14	6.40	Si	47
0	(8+9)-VII-2	531	0.14	6.40	Si	47
0	(8+9)-III-4	328	0.08	6.40	Si	75
0	(8+9)-III-3	362	0.09	6.40	Si	68
0	(8+9)-IV-2	138	0.04	6.40	Si	>100
0	(8+9)-VIII-2	268	0.07	6.40	Si	92
0	(8+9)-IV-4	207	0.05	6.40	Si	>100
0	(8+9)-VIII-1	381	0.10	6.40	Si	65
0	(8+9)-II-4	198	0.05	6.40	Si	>100
0	(8+9)-VI-2	259	0.07	6.40	Si	95
276	1	332	0.09	3.84	Si	45
276	2	690	0.18	5.76	Si	32
276	3	690	0.18	5.76	Si	32
276	4	332	0.09	5.12	Si	60
276	5	332	0.09	5.12	Si	60
276	6	332	0.09	5.12	Si	60
276	7	332	0.09	5.12	Si	60
276	(8+9)-IV-1	304	0.08	6.40	Si	81
276	(8+9)-II-3	338	0.09	6.40	Si	73
276	(8+9)-IV-3	325	0.08	6.40	Si	76
276	(8+9)-II-1	317	0.08	6.40	Si	78
276	(8+9)-III-2	168	0.04	6.40	Si	>100
276	(8+9)-III-1	219	0.06	6.40	Si	>100
276	(8+9)-I-1	223	0.06	6.40	Si	>100
276	(8+9)-I-2	164	0.04	6.40	Si	>100
552	(8+9)-VIII-4	159	0.04	6.40	Si	>100
552	(8+9)-V-3	313	0.08	6.40	Si	79
552	(8+9)-VII-3	308	0.08	6.40	Si	80
552	(8+9)-VII-4	261	0.07	6.40	Si	95
552	(8+9)-VI-4	142	0.04	6.40	Si	>100
552	(8+9)-VI-3	331	0.09	6.40	Si	75
552	(8+9)-VIII-3	314	0.08	6.40	Si	79
552	(8+9)-V-4	256	0.07	6.40	Si	96

X	Comb.	Ty	τ_d	fvd	RS	Cs
Verifiche nella direzione secondaria						
0	(8+9)-VIII-4	64	0.22	6.40	Si	29
0	(8+9)-V-2	169	0.58	6.40	Si	11
0	(8+9)-II-3	-131	0.45	6.40	Si	14
0	(8+9)-IV-2	123	0.42	6.40	Si	15
0	(8+9)-II-4	104	0.36	6.40	Si	18
0	(8+9)-VIII-2	139	0.48	6.40	Si	13
0	(8+9)-VI-3	-147	0.51	6.40	Si	13
0	(8+9)-VII-3	-145	0.50	6.40	Si	13
0	(8+9)-III-2	108	0.37	6.40	Si	17
0	(8+9)-VI-4	88	0.30	6.40	Si	21
0	(8+9)-III-3	-92	0.32	6.40	Si	20
0	(8+9)-I-3	-99	0.34	6.40	Si	19
0	(8+9)-III-4	-36	0.12	6.40	Si	52
0	(8+9)-II-1	-88	0.30	6.40	Si	21
0	(8+9)-VI-2	163	0.56	6.40	Si	11
0	(8+9)-VIII-3	-123	0.42	6.40	Si	15
0	(8+9)-VII-2	161	0.56	6.40	Si	11
0	(8+9)-I-4	-28	0.10	6.40	Si	65
0	(8+9)-II-2	147	0.51	6.40	Si	13
0	(8+9)-VII-4	-89	0.31	6.40	Si	21
0	(8+9)-I-2	115	0.40	6.40	Si	16
0	(8+9)-IV-3	-107	0.37	6.40	Si	17
0	(8+9)-IV-4	80	0.28	6.40	Si	23
0	(8+9)-V-3	-152	0.53	6.40	Si	12
3870	1	62	0.21	3.84	Si	18
3870	2	131	0.45	5.76	Si	13
3870	3	131	0.45	5.76	Si	13
3870	4	62	0.21	5.12	Si	24
3870	5	62	0.21	5.12	Si	24
3870	6	62	0.21	5.12	Si	24
3870	7	62	0.21	5.12	Si	24
3870	(8+9)-VII-1	172	0.60	6.40	Si	11
3870	(8+9)-I-1	68	0.23	6.40	Si	27
3870	(8+9)-III-1	69	0.24	6.40	Si	27
3870	(8+9)-IV-1	70	0.24	6.40	Si	26
3870	(8+9)-VIII-1	101	0.35	6.40	Si	18
3870	(8+9)-VI-1	96	0.33	6.40	Si	19
3870	(8+9)-V-4	-85	0.30	6.40	Si	22
3870	(8+9)-V-1	171	0.59	6.40	Si	11

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	(8+9)-IV-1	8456	4.51	32.00	7.1	1.09	20.00	18	V	7.1
0	(8+9)-VI-4	-10101	-5.39	32.00	5.9	-1.31	20.00	15	V	5.9
0	(8+9)-VIII-4	-8450	-4.51	32.00	7.1	-1.09	20.00	18	V	7.1
0	(8+9)-II-1	10107	5.40	32.00	5.9	1.31	20.00	15	V	5.9
0	(8+9)-IV-4	-8610	-4.60	32.00	7.0	-1.11	20.00	18	V	7.0
0	(8+9)-VI-1	9947	5.31	32.00	6.0	1.29	20.00	16	V	6.0
0	(8+9)-II-4	-10260	-5.48	32.00	5.8	-1.33	20.00	15	V	5.8
0	(8+9)-VIII-1	8297	4.43	32.00	7.2	1.07	20.00	19	V	7.2
276	(8+9)-II-2	-12849	-6.86	32.00	4.7	-1.66	20.00	12	V	4.7
276	(8+9)-IV-2	-11195	-5.98	32.00	5.4	-1.45	20.00	14	V	5.4
276	(8+9)-VI-2	-12126	-6.47	32.00	4.9	-1.57	20.00	13	V	4.9
276	(8+9)-VIII-2	-10472	-5.59	32.00	5.7	-1.35	20.00	15	V	5.7
552	1	156	0.08	19.20	>100	0.02	12.00	>100	V	>100
552	2	439	0.23	28.80	>100	0.06	18.00	>100	V	>100
552	3	439	0.23	28.80	>100	0.06	18.00	>100	V	>100
552	4	156	0.08	25.60	>100	0.02	16.00	>100	V	>100
552	5	156	0.08	25.60	>100	0.02	16.00	>100	V	>100
552	6	156	0.08	25.60	>100	0.02	16.00	>100	V	>100
552	7	156	0.08	25.60	>100	0.02	16.00	>100	V	>100

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
552	(8+9)-VI-3	12296	6.56	32.00	4.9	1.59	20.00	13	V	4.9
552	(8+9)-I-1	-4083	-2.18	32.00	15	-0.53	20.00	38	V	15
552	(8+9)-II-3	12871	6.87	32.00	4.7	1.66	20.00	12	V	4.7
552	(8+9)-III-4	4777	2.55	32.00	13	0.62	20.00	32	V	13
552	(8+9)-I-4	4284	2.29	32.00	14	0.55	20.00	36	V	14
552	(8+9)-III-3	10131	5.41	32.00	5.9	1.31	20.00	15	V	5.9
552	(8+9)-VII-1	-2660	-1.42	32.00	23	-0.34	20.00	58	V	23
552	(8+9)-V-2	-8507	-4.54	32.00	7.0	-1.10	20.00	18	V	7.0
552	(8+9)-VII-2	-8014	-4.28	32.00	7.5	-1.04	20.00	19	V	7.5
552	(8+9)-V-4	2369	1.26	32.00	25	0.31	20.00	65	V	25
552	(8+9)-VII-3	8215	4.39	32.00	7.3	1.06	20.00	19	V	7.3
552	(8+9)-III-1	-4576	-2.44	32.00	13	-0.59	20.00	34	V	13
552	(8+9)-VII-4	2861	1.53	32.00	21	0.37	20.00	54	V	21
552	(8+9)-III-2	-9930	-5.30	32.00	6.0	-1.28	20.00	16	V	6.0
552	(8+9)-IV-3	11230	6.00	32.00	5.3	1.45	20.00	14	V	5.3
552	(8+9)-V-3	8707	4.65	32.00	6.9	1.12	20.00	18	V	6.9
552	(8+9)-I-3	10623	5.67	32.00	5.6	1.37	20.00	15	V	5.6
552	(8+9)-I-2	-10422	-5.56	32.00	5.8	-1.35	20.00	15	V	5.8
552	(8+9)-VIII-3	10655	5.69	32.00	5.6	1.38	20.00	15	V	5.6
552	(8+9)-V-1	-2168	-1.16	32.00	28	-0.28	20.00	71	V	28
Verifiche nella direzione secondaria										
0	(8+9)-III-4	-866	-3.24	32.00	9.9	-0.78	20.00	26	V	9.9
0	(8+9)-I-4	-751	-2.81	32.00	11	-0.68	20.00	29	V	11
0	(8+9)-VIII-3	-2623	-9.82	32.00	3.3	-2.38	20.00	8.4	V	3.3
0	(8+9)-V-3	-2710	-10.14	32.00	3.2	-2.45	20.00	8.1	V	3.2
0	(8+9)-VII-3	-2595	-9.71	32.00	3.3	-2.35	20.00	8.5	V	3.3
0	(8+9)-V-2	2647	9.91	32.00	3.2	2.40	20.00	8.3	V	3.2
0	(8+9)-VII-1	1331	4.98	32.00	6.4	1.21	20.00	17	V	6.4
0	(8+9)-II-3	-2847	-10.66	32.00	3.0	-2.58	20.00	7.8	V	3.0
0	(8+9)-I-1	688	2.57	32.00	12	0.62	20.00	32	V	12
0	(8+9)-V-1	1216	4.55	32.00	7.0	1.10	20.00	18	V	7.0
0	(8+9)-I-3	-2182	-8.17	32.00	3.9	-1.98	20.00	10	V	3.9
0	(8+9)-VII-2	2532	9.48	32.00	3.4	2.29	20.00	8.7	V	3.4
0	(8+9)-VI-3	-3006	-11.25	32.00	2.8	-2.72	20.00	7.3	V	2.8
0	(8+9)-V-4	-1279	-4.79	32.00	6.7	-1.16	20.00	17	V	6.7
0	(8+9)-VII-4	-1394	-5.22	32.00	6.1	-1.26	20.00	16	V	6.1
0	(8+9)-III-1	802	3.00	32.00	11	0.73	20.00	28	V	11
0	(8+9)-IV-3	-2465	-9.23	32.00	3.5	-2.23	20.00	9.0	V	3.5
0	(8+9)-III-3	-2067	-7.74	32.00	4.1	-1.87	20.00	11	V	4.1
1935	(8+9)-VIII-4	1527	5.72	32.00	5.6	1.38	20.00	14	V	5.6
1935	(8+9)-VIII-1	-1461	-5.47	32.00	5.9	-1.32	20.00	15	V	5.9
1935	(8+9)-I-2	2126	7.96	32.00	4.0	1.93	20.00	10	V	4.0
1935	(8+9)-IV-1	-1616	-6.05	32.00	5.3	-1.46	20.00	14	V	5.3
1935	(8+9)-VI-1	-1840	-6.89	32.00	4.6	-1.67	20.00	12	V	4.6
1935	(8+9)-III-2	2012	7.53	32.00	4.2	1.82	20.00	11	V	4.2
1935	(8+9)-VI-2	3032	11.35	32.00	2.8	2.75	20.00	7.3	V	2.8
1935	(8+9)-II-1	-1995	-7.47	32.00	4.3	-1.81	20.00	11	V	4.3
1935	(8+9)-IV-2	2499	9.35	32.00	3.4	2.26	20.00	8.8	V	3.4
1935	(8+9)-IV-4	1682	6.30	32.00	5.1	1.52	20.00	13	V	5.1
1935	(8+9)-II-2	2877	10.77	32.00	3.0	2.61	20.00	7.7	V	3.0
1935	(8+9)-II-4	2060	7.71	32.00	4.1	1.87	20.00	11	V	4.1
1935	(8+9)-VI-4	1905	7.13	32.00	4.5	1.73	20.00	12	V	4.5
1935	(8+9)-VIII-2	2654	9.93	32.00	3.2	2.40	20.00	8.3	V	3.2
3870	1	92	0.35	19.20	56	0.08	12.00	>100	V	56
3870	2	156	0.58	28.80	49	0.14	18.00	>100	V	49
3870	3	156	0.58	28.80	49	0.14	18.00	>100	V	49
3870	4	92	0.35	25.60	74	0.08	16.00	>100	V	74
3870	5	92	0.35	25.60	74	0.08	16.00	>100	V	74
3870	6	92	0.35	25.60	74	0.08	16.00	>100	V	74
3870	7	92	0.35	25.60	74	0.08	16.00	>100	V	74

Setto 38: origine (1408.8,2312.7,303.5), direzione (-0.200098,0.979776,0)
 Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	1	273	49	177	0.23	1.51	0.52	79.20	115.20	115.20	49
0	2	543	101	379	0.45	3.13	1.12	118.80	172.80	172.80	35
0	3	543	101	379	0.45	3.13	1.12	118.80	172.80	172.80	35
0	4	273	49	177	0.23	1.51	0.52	105.60	153.60	153.60	65
0	5	273	49	177	0.23	1.51	0.52	105.60	153.60	153.60	65
0	6	273	49	177	0.23	1.51	0.52	105.60	153.60	153.60	65
0	7	273	49	177	0.23	1.51	0.52	105.60	153.60	153.60	65
1200	(8+9)-VIII-4	4771	-20	2278	3.94	-0.62	6.75	132.00	192.00	192.00	15
1200	(8+9)-IV-1	-5415	12	-2640	-4.47	0.38	-7.82	132.00	192.00	192.00	23
1200	(8+9)-V-1	3778	-29	1810	3.12	-0.91	5.36	132.00	192.00	192.00	18
1200	(8+9)-I-2	6777	-35	3250	5.59	-1.09	9.63	132.00	192.00	192.00	10
1200	(8+9)-V-2	8571	-47	4128	7.07	-1.45	12.23	132.00	192.00	192.00	8.0
1200	(8+9)-I-4	-2090	6	-1032	-1.72	0.19	-3.06	132.00	192.00	192.00	59
1200	(8+9)-V-3	-8676	35	-4227	-7.16	1.10	-12.53	132.00	192.00	192.00	14
1200	(8+9)-II-2	9265	-41	4455	7.64	-1.27	13.20	132.00	192.00	192.00	7.5
1200	(8+9)-V-4	-3884	18	-1910	-3.20	0.56	-5.66	132.00	192.00	192.00	31
1200	(8+9)-II-4	6605	-29	3170	5.45	-0.89	9.39	132.00	192.00	192.00	11
1200	(8+9)-VI-1	-6172	14	-3006	-5.09	0.43	-8.91	132.00	192.00	192.00	20
1200	(8+9)-III-2	6388	-34	3061	5.27	-1.04	9.07	132.00	192.00	192.00	11
1200	(8+9)-VI-2	9803	-45	4718	8.09	-1.38	13.98	132.00	192.00	192.00	7.1
1200	(8+9)-III-4	-2479	8	-1221	-2.04	0.24	-3.62	132.00	192.00	192.00	49
1200	(8+9)-VI-3	-9909	33	-4818	-8.17	1.03	-14.28	132.00	192.00	192.00	12
1200	(8+9)-IV-2	7969	-36	3825	6.57	-1.12	11.34	132.00	192.00	192.00	8.7
1200	(8+9)-VI-4	6067	-25	2907	5.00	-0.78	8.61	132.00	192.00	192.00	12
1200	(8+9)-IV-4	5309	-24	2541	4.38	-0.73	7.53	132.00	192.00	192.00	13
1200	(8+9)-VII-1	4167	-31	1999	3.44	-0.96	5.92	132.00	192.00	192.00	16
1200	(8+9)-II-1	-6711	17	-3270	-5.53	0.54	-9.69	132.00	192.00	192.00	18
1200	(8+9)-VII-2	8182	-45	3939	6.75	-1.40	11.67	132.00	192.00	192.00	8.4
1200	(8+9)-III-1	2373	-19	1122	1.96	-0.59	3.32	132.00	192.00	192.00	28
1200	(8+9)-VII-3	-8288	34	-4038	-6.84	1.05	-11.97	132.00	192.00	192.00	14
1200	(8+9)-I-1	1984	-18	933	1.64	-0.55	2.76	132.00	192.00	192.00	34
1200	(8+9)-VII-4	-4272	19	-2099	-3.52	0.60	-6.22	132.00	192.00	192.00	28
1200	(8+9)-III-3	-6494	22	-3161	-5.36	0.69	-9.37	132.00	192.00	192.00	19
1200	(8+9)-IV-3	-8075	25	-3925	-6.66	0.77	-11.63	132.00	192.00	192.00	15
1200	(8+9)-II-3	-9371	30	-4554	-7.73	0.92	-13.50	132.00	192.00	192.00	13
1200	(8+9)-VIII-1	-4877	9	-2377	-4.02	0.27	-7.04	132.00	192.00	192.00	26
1200	(8+9)-VIII-2	8508	-40	4089	7.02	-1.23	12.12	132.00	192.00	192.00	8.2
1200	(8+9)-VIII-3	-8613	28	-4188	-7.10	0.87	-12.41	132.00	192.00	192.00	14
1200	(8+9)-I-3	-6882	24	-3349	-5.68	0.74	-9.93	132.00	192.00	192.00	18
Verifiche nella direzione secondaria											
0	1	-1441	26	241	-2.48	2.55	2.08	79.20	115.20	115.20	25
0	4	-1441	26	241	-2.48	2.55	2.08	105.60	153.60	153.60	33
0	5	-1441	26	241	-2.48	2.55	2.08	105.60	153.60	153.60	33
0	6	-1441	26	241	-2.48	2.55	2.08	105.60	153.60	153.60	33
0	7	-1441	26	241	-2.48	2.55	2.08	105.60	153.60	153.60	33
0	(8+9)-VIII-4	-1542	22	3614	-2.65	2.18	31.11	132.00	192.00	192.00	5.8
0	(8+9)-IV-2	-1938	26	5914	-3.34	2.53	50.91	132.00	192.00	192.00	3.6
0	(8+9)-V-1	-1514	23	2951	-2.61	2.24	25.40	132.00	192.00	192.00	6.9
0	(8+9)-I-1	-1233	20	1627	-2.12	1.94	14.01	132.00	192.00	192.00	12
0	(8+9)-V-2	-2102	28	6385	-3.62	2.74	54.96	132.00	192.00	192.00	3.3
0	(8+9)-I-3	-193	11	-4716	-0.33	1.09	-40.60	132.00	192.00	192.00	4.6
0	(8+9)-V-3	87	8	-6039	0.15	0.79	-51.99	132.00	192.00	192.00	3.6
0	(8+9)-II-1	-183	11	-4599	-0.32	1.07	-39.59	132.00	192.00	192.00	4.7
0	(8+9)-V-4	-501	13	-2605	-0.86	1.28	-22.43	132.00	192.00	192.00	8.1
0	(8+9)-II-3	129	8	-6502	0.22	0.81	-55.97	132.00	192.00	192.00	3.4
0	(8+9)-VI-1	-267	12	-4202	-0.46	1.15	-36.17	132.00	192.00	192.00	5.1
0	(8+9)-III-1	-1295	20	1908	-2.23	2.00	16.42	132.00	192.00	192.00	10
0	(8+9)-VI-2	-2227	28	7244	-3.84	2.80	62.37	132.00	192.00	192.00	2.9
0	(8+9)-III-3	-255	12	-4436	-0.44	1.14	-38.19	132.00	192.00	192.00	4.9
0	(8+9)-VI-3	213	7	-6899	0.37	0.72	-59.39	132.00	192.00	192.00	3.2
0	(8+9)-IV-1	-388	13	-3665	-0.67	1.25	-31.55	132.00	192.00	192.00	5.9
0	(8+9)-VI-4	-1747	24	4548	-3.01	2.37	39.15	132.00	192.00	192.00	4.6
0	(8+9)-IV-3	-77	10	-5568	-0.13	0.99	-47.93	132.00	192.00	192.00	3.9

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-VII-1	-1575	23	3231	-2.71	2.30	27.81	132.00	192.00	192.00	6.4
0	(8+9)-I-2	-1821	25	5061	-3.14	2.44	43.57	132.00	192.00	192.00	4.2
0	(8+9)-VII-2	-2040	27	6104	-3.51	2.68	52.55	132.00	192.00	192.00	3.5
0	(8+9)-II-2	-2143	28	6848	-3.69	2.71	58.95	132.00	192.00	192.00	3.1
0	(8+9)-VII-3	26	9	-5759	0.04	0.84	-49.58	132.00	192.00	192.00	3.8
0	(8+9)-III-2	-1759	24	4781	-3.03	2.38	41.16	132.00	192.00	192.00	4.4
0	(8+9)-VIII-3	8	9	-5965	0.01	0.90	-51.35	132.00	192.00	192.00	3.7
0	(8+9)-III-4	-720	15	-1562	-1.24	1.53	-13.45	132.00	192.00	192.00	13
0	(8+9)-I-4	-781	16	-1282	-1.35	1.58	-11.04	132.00	192.00	192.00	15
0	(8+9)-II-4	-1831	25	4945	-3.15	2.46	42.57	132.00	192.00	192.00	4.3
0	(8+9)-IV-4	-1626	23	4011	-2.80	2.27	34.53	132.00	192.00	192.00	5.2
0	(8+9)-VII-4	-439	12	-2885	-0.76	1.23	-24.84	132.00	192.00	192.00	7.4
0	(8+9)-VIII-1	-473	14	-3268	-0.81	1.34	-28.13	132.00	192.00	192.00	6.5
0	(8+9)-VIII-2	-2022	27	6311	-3.48	2.62	54.33	132.00	192.00	192.00	3.4
835	2	-1072	87	-84	-1.85	8.60	-0.72	118.80	172.80	172.80	19
835	3	-1072	87	-84	-1.85	8.60	-0.72	118.80	172.80	172.80	19

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Ty kg	τ_d kg/cmq	fvd kg/cmq	RS	Cs
0	1	-66	0.04	3.84	Si	97
0	2	-137	0.08	5.76	Si	70
0	3	-137	0.08	5.76	Si	70
0	4	-66	0.04	5.12	Si	>100
0	5	-66	0.04	5.12	Si	>100
0	6	-66	0.04	5.12	Si	>100
0	7	-66	0.04	5.12	Si	>100
0	(8+9)-VIII-4	-50	0.03	6.40	Si	>100
0	(8+9)-IV-1	-39	0.02	6.40	Si	>100
0	(8+9)-V-1	-54	0.03	6.40	Si	>100
0	(8+9)-I-2	-55	0.03	6.40	Si	>100
0	(8+9)-V-2	-61	0.04	6.40	Si	>100
0	(8+9)-I-4	-43	0.03	6.40	Si	>100
0	(8+9)-V-3	-30	0.02	6.40	Si	>100
0	(8+9)-II-2	-59	0.04	6.40	Si	>100
0	(8+9)-V-4	-37	0.02	6.40	Si	>100
0	(8+9)-II-4	-55	0.03	6.40	Si	>100
0	(8+9)-VI-1	-38	0.02	6.40	Si	>100
0	(8+9)-III-2	-54	0.03	6.40	Si	>100
0	(8+9)-VI-2	-61	0.04	6.40	Si	>100
0	(8+9)-III-4	-42	0.03	6.40	Si	>100
0	(8+9)-VI-3	-30	0.02	6.40	Si	>100
0	(8+9)-IV-2	-56	0.03	6.40	Si	>100
0	(8+9)-VI-4	-53	0.03	6.40	Si	>100
0	(8+9)-IV-4	-52	0.03	6.40	Si	>100
0	(8+9)-VII-1	-55	0.03	6.40	Si	>100
0	(8+9)-II-1	-36	0.02	6.40	Si	>100
0	(8+9)-VII-2	-60	0.04	6.40	Si	>100
0	(8+9)-III-1	-49	0.03	6.40	Si	>100
0	(8+9)-VII-3	-31	0.02	6.40	Si	>100
0	(8+9)-I-1	-48	0.03	6.40	Si	>100
0	(8+9)-VII-4	-36	0.02	6.40	Si	>100
0	(8+9)-III-3	-37	0.02	6.40	Si	>100
0	(8+9)-IV-3	-35	0.02	6.40	Si	>100
0	(8+9)-II-3	-32	0.02	6.40	Si	>100
0	(8+9)-VIII-1	-41	0.02	6.40	Si	>100
0	(8+9)-VIII-2	-57	0.03	6.40	Si	>100
0	(8+9)-VIII-3	-34	0.02	6.40	Si	>100
0	(8+9)-I-3	-36	0.02	6.40	Si	>100
Verifiche nella direzione secondaria						
0	1	41	0.07	3.84	Si	59
0	2	85	0.14	5.76	Si	42
0	3	85	0.14	5.76	Si	42

X	Comb.	Ty	τ_d	fvd	RS	Cs
0	4	41	0.07	5.12	Si	79
0	5	41	0.07	5.12	Si	79
0	6	41	0.07	5.12	Si	79
0	7	41	0.07	5.12	Si	79
0	(8+9)-IV-2	41	0.06	6.40	Si	99
0	(8+9)-V-1	65	0.10	6.40	Si	62
0	(8+9)-I-2	40	0.06	6.40	Si	>100
0	(8+9)-V-2	74	0.12	6.40	Si	54
0	(8+9)-I-4	26	0.04	6.40	Si	>100
0	(8+9)-VI-1	25	0.04	6.40	Si	>100
0	(8+9)-VII-2	73	0.12	6.40	Si	55
0	(8+9)-II-2	46	0.07	6.40	Si	88
0	(8+9)-I-1	31	0.05	6.40	Si	>100
0	(8+9)-II-4	42	0.07	6.40	Si	97
0	(8+9)-VII-1	66	0.11	6.40	Si	61
0	(8+9)-III-2	38	0.06	6.40	Si	>100
0	(8+9)-IV-4	37	0.06	6.40	Si	>100
0	(8+9)-III-1	32	0.05	6.40	Si	>100
0	(8+9)-VIII-1	30	0.05	6.40	Si	>100
0	(8+9)-VIII-2	51	0.08	6.40	Si	79
0	(8+9)-VI-4	31	0.05	6.40	Si	>100
0	(8+9)-VI-2	56	0.09	6.40	Si	72
0	(8+9)-III-4	24	0.04	6.40	Si	>100
1670	(8+9)-VIII-4	-29	0.05	6.40	Si	>100
1670	(8+9)-V-3	-19	0.03	6.40	Si	>100
1670	(8+9)-VII-3	-19	0.03	6.40	Si	>100
1670	(8+9)-V-4	-22	0.04	6.40	Si	>100
1670	(8+9)-VII-4	-22	0.03	6.40	Si	>100
1670	(8+9)-IV-3	-21	0.03	6.40	Si	>100
1670	(8+9)-IV-1	-22	0.04	6.40	Si	>100
1670	(8+9)-II-1	-21	0.03	6.40	Si	>100
1670	(8+9)-I-3	-21	0.03	6.40	Si	>100
1670	(8+9)-III-3	-22	0.03	6.40	Si	>100
1670	(8+9)-II-3	-19	0.03	6.40	Si	>100
1670	(8+9)-VIII-3	-20	0.03	6.40	Si	>100
1670	(8+9)-VI-3	-18	0.03	6.40	Si	>100

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Tx kg	τ_{vd} kg/cmq	fvd kg/cmq	Csv	τ_M kg/cmq	fTd kg/cmq	Csm	Mecc.	Cs
0	(8+9)-III-2	-4438	-5.49	32.00	5.8	-1.33	20.00	15	V	5.8
0	(8+9)-I-2	-4720	-5.84	32.00	5.5	-1.41	20.00	14	V	5.5
0	(8+9)-VIII-4	-3359	-4.16	32.00	7.7	-1.01	20.00	20	V	7.7
0	(8+9)-V-1	-2553	-3.16	32.00	10	-0.76	20.00	26	V	10
0	(8+9)-VII-2	-5762	-7.13	32.00	4.5	-1.73	20.00	12	V	4.5
0	(8+9)-IV-4	-3756	-4.65	32.00	6.9	-1.12	20.00	18	V	6.9
0	(8+9)-VI-4	-4297	-5.32	32.00	6.0	-1.29	20.00	16	V	6.0
0	(8+9)-IV-2	-5647	-6.99	32.00	4.6	-1.69	20.00	12	V	4.6
0	(8+9)-V-2	-6044	-7.48	32.00	4.3	-1.81	20.00	11	V	4.3
0	(8+9)-II-2	-6586	-8.15	32.00	3.9	-1.97	20.00	10	V	3.9
0	(8+9)-VI-2	-6983	-8.64	32.00	3.7	-2.09	20.00	9.6	V	3.7
0	(8+9)-I-1	-1229	-1.52	32.00	21	-0.37	20.00	54	V	21
0	(8+9)-VII-1	-2834	-3.51	32.00	9.1	-0.85	20.00	24	V	9.1
0	(8+9)-VIII-2	-6045	-7.48	32.00	4.3	-1.81	20.00	11	V	4.3
0	(8+9)-II-4	-4694	-5.81	32.00	5.5	-1.41	20.00	14	V	5.5
0	(8+9)-III-1	-1510	-1.87	32.00	17	-0.45	20.00	44	V	17
1200	1	681	0.84	19.20	23	0.20	12.00	59	V	23
1200	2	1430	1.77	28.80	16	0.43	18.00	42	V	16
1200	3	1430	1.77	28.80	16	0.43	18.00	42	V	16
1200	4	681	0.84	25.60	30	0.20	16.00	79	V	30
1200	5	681	0.84	25.60	30	0.20	16.00	79	V	30
1200	6	681	0.84	25.60	30	0.20	16.00	79	V	30
1200	7	681	0.84	25.60	30	0.20	16.00	79	V	30

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
1200	(8+9)-IV-1	4474	5.53	32.00	5.8	1.34	20.00	15	V	5.8
1200	(8+9)-III-3	5267	6.52	32.00	4.9	1.58	20.00	13	V	4.9
1200	(8+9)-II-1	5433	6.72	32.00	4.8	1.63	20.00	12	V	4.8
1200	(8+9)-I-3	5555	6.87	32.00	4.7	1.66	20.00	12	V	4.7
1200	(8+9)-II-3	7412	9.17	32.00	3.5	2.22	20.00	9.0	V	3.5
1200	(8+9)-V-4	3339	4.13	32.00	7.7	1.00	20.00	20	V	7.7
1200	(8+9)-VII-3	6623	8.19	32.00	3.9	1.98	20.00	10	V	3.9
1200	(8+9)-I-4	1983	2.45	32.00	13	0.59	20.00	34	V	13
1200	(8+9)-VII-4	3626	4.49	32.00	7.1	1.09	20.00	18	V	7.1
1200	(8+9)-VI-1	5026	6.22	32.00	5.1	1.50	20.00	13	V	5.1
1200	(8+9)-VI-3	7819	9.67	32.00	3.3	2.34	20.00	8.5	V	3.3
1200	(8+9)-V-3	6910	8.55	32.00	3.7	2.07	20.00	9.7	V	3.7
1200	(8+9)-VIII-1	4067	5.03	32.00	6.4	1.22	20.00	16	V	6.4
1200	(8+9)-III-4	2271	2.81	32.00	11	0.68	20.00	29	V	11
1200	(8+9)-VIII-3	6860	8.49	32.00	3.8	2.05	20.00	9.7	V	3.8
1200	(8+9)-IV-3	6454	7.98	32.00	4.0	1.93	20.00	10	V	4.0
Verifiche nella direzione secondaria										
0	(8+9)-VIII-4	3348	5.76	32.00	5.6	1.39	20.00	14	V	5.6
0	(8+9)-VII-2	5698	9.81	32.00	3.3	2.37	20.00	8.4	V	3.3
0	(8+9)-III-3	-4890	-8.42	32.00	3.8	-2.04	20.00	9.8	V	3.8
0	(8+9)-IV-2	5646	9.72	32.00	3.3	2.35	20.00	8.5	V	3.3
0	(8+9)-III-4	-1963	-3.38	32.00	9.5	-0.82	20.00	24	V	9.5
0	(8+9)-VIII-2	6008	10.35	32.00	3.1	2.50	20.00	8.0	V	3.1
0	(8+9)-IV-1	-4109	-7.07	32.00	4.5	-1.71	20.00	12	V	4.5
0	(8+9)-VII-4	-3170	-5.46	32.00	5.9	-1.32	20.00	15	V	5.9
0	(8+9)-I-1	1281	2.21	32.00	15	0.53	20.00	37	V	15
0	(8+9)-IV-3	-6045	-10.41	32.00	3.1	-2.52	20.00	7.9	V	3.1
0	(8+9)-I-3	-5173	-8.91	32.00	3.6	-2.16	20.00	9.3	V	3.6
0	(8+9)-IV-4	3710	6.39	32.00	5.0	1.55	20.00	13	V	5.0
0	(8+9)-II-1	-5054	-8.70	32.00	3.7	-2.11	20.00	9.5	V	3.7
0	(8+9)-V-1	2488	4.28	32.00	7.5	1.04	20.00	19	V	7.5
0	(8+9)-II-3	-6990	-12.03	32.00	2.7	-2.91	20.00	6.9	V	2.7
0	(8+9)-V-2	5981	10.30	32.00	3.1	2.49	20.00	8.0	V	3.1
0	(8+9)-III-1	1564	2.69	32.00	12	0.65	20.00	31	V	12
0	(8+9)-V-3	-6380	-10.99	32.00	2.9	-2.66	20.00	7.5	V	2.9
0	(8+9)-VIII-3	-6407	-11.03	32.00	2.9	-2.67	20.00	7.5	V	2.9
0	(8+9)-V-4	-2887	-4.97	32.00	6.4	-1.20	20.00	17	V	6.4
0	(8+9)-VII-3	-6097	-10.50	32.00	3.0	-2.54	20.00	7.9	V	3.0
0	(8+9)-VI-1	-4692	-8.08	32.00	4.0	-1.95	20.00	10	V	4.0
0	(8+9)-I-4	-1680	-2.89	32.00	11	-0.70	20.00	29	V	11
0	(8+9)-VI-2	6953	11.97	32.00	2.7	2.90	20.00	6.9	V	2.7
0	(8+9)-II-4	4655	8.01	32.00	4.0	1.94	20.00	10	V	4.0
0	(8+9)-VIII-1	-3747	-6.45	32.00	5.0	-1.56	20.00	13	V	5.0
0	(8+9)-I-2	4774	8.22	32.00	3.9	1.99	20.00	10	V	3.9
0	(8+9)-II-2	6591	11.35	32.00	2.8	2.75	20.00	7.3	V	2.8
0	(8+9)-III-2	4491	7.73	32.00	4.1	1.87	20.00	11	V	4.1
0	(8+9)-VI-3	-7352	-12.66	32.00	2.5	-3.06	20.00	6.5	V	2.5
0	(8+9)-VI-4	4293	7.39	32.00	4.3	1.79	20.00	11	V	4.3
0	(8+9)-VII-1	2771	4.77	32.00	6.7	1.15	20.00	17	V	6.7
1670	1	-558	-0.96	19.20	20	-0.23	12.00	52	V	20
1670	2	-1222	-2.10	28.80	14	-0.51	18.00	35	V	14
1670	3	-1222	-2.10	28.80	14	-0.51	18.00	35	V	14
1670	4	-558	-0.96	25.60	27	-0.23	16.00	69	V	27
1670	5	-558	-0.96	25.60	27	-0.23	16.00	69	V	27
1670	6	-558	-0.96	25.60	27	-0.23	16.00	69	V	27
1670	7	-558	-0.96	25.60	27	-0.23	16.00	69	V	27

Setto 39: origine (1449.0,2116.1,303.5), direzione (-0.200098,0.979776,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
500	(8+9)-V-1	2144	89	1471	1.77	2.75	4.36	132.00	192.00	192.00	20
1000	1	2928	131	-1364	2.42	4.05	-4.04	79.20	115.20	115.20	9.9

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
1000	2	6048	271	-2841	4.99	8.40	-8.42	118.80	172.80	172.80	7.2
1000	3	6048	271	-2841	4.99	8.40	-8.42	118.80	172.80	172.80	7.2
1000	4	2928	131	-1364	2.42	4.05	-4.04	105.60	153.60	153.60	13
1000	5	2928	131	-1364	2.42	4.05	-4.04	105.60	153.60	153.60	13
1000	6	2928	131	-1364	2.42	4.05	-4.04	105.60	153.60	153.60	13
1000	7	2928	131	-1364	2.42	4.05	-4.04	105.60	153.60	153.60	13
1000	(8+9)-VII-1	5388	79	499	4.44	2.46	1.48	132.00	192.00	192.00	18
1000	(8+9)-VIII-1	-1633	87	-2741	-1.35	2.68	-8.12	132.00	192.00	192.00	18
1000	(8+9)-I-3	-3255	86	-3430	-2.68	2.66	-10.17	132.00	192.00	192.00	15
1000	(8+9)-VIII-2	8625	87	2166	7.11	2.71	6.42	132.00	192.00	192.00	9.9
1000	(8+9)-II-1	-3123	92	-3374	-2.58	2.85	-10.00	132.00	192.00	192.00	15
1000	(8+9)-VIII-3	-4574	93	-4045	-3.77	2.88	-11.99	132.00	192.00	192.00	13
1000	(8+9)-II-3	-5179	89	-4343	-4.27	2.77	-12.87	132.00	192.00	192.00	12
1000	(8+9)-VIII-4	5684	94	862	4.69	2.91	2.55	132.00	192.00	192.00	16
1000	(8+9)-III-1	3914	94	-60	3.23	2.92	-0.18	132.00	192.00	192.00	25
1000	(8+9)-III-2	6991	95	1412	5.77	2.93	4.18	132.00	192.00	192.00	12
1000	(8+9)-VI-2	9673	86	2631	7.98	2.68	7.80	132.00	192.00	192.00	8.7
1000	(8+9)-III-3	-2940	86	-3291	-2.43	2.65	-9.75	132.00	192.00	192.00	15
1000	(8+9)-VI-3	-5621	94	-4510	-4.64	2.91	-13.37	132.00	192.00	192.00	12
1000	(8+9)-IV-1	-2075	91	-2908	-1.71	2.82	-8.62	132.00	192.00	192.00	17
1000	(8+9)-VI-4	6732	93	1327	5.55	2.87	3.93	132.00	192.00	192.00	13
1000	(8+9)-IV-3	-4132	88	-3877	-3.41	2.74	-11.49	132.00	192.00	192.00	13
1000	(8+9)-I-1	3600	95	-200	2.97	2.93	-0.59	132.00	192.00	192.00	24
1000	(8+9)-I-2	7306	94	1551	6.03	2.92	4.60	132.00	192.00	192.00	12
1000	(8+9)-VII-2	8466	80	1971	6.98	2.46	5.84	132.00	192.00	192.00	10
1000	(8+9)-V-3	-4729	101	-3989	-3.90	3.13	-11.82	132.00	192.00	192.00	13
1000	(8+9)-VII-3	-4415	101	-3850	-3.64	3.12	-11.41	132.00	192.00	192.00	13
1000	(8+9)-VI-1	-2681	88	-3206	-2.21	2.71	-9.50	132.00	192.00	192.00	16
1000	(8+9)-VII-4	-1337	101	-2378	-1.10	3.13	-7.05	132.00	192.00	192.00	19
1000	(8+9)-V-2	8780	79	2110	7.24	2.45	6.25	132.00	192.00	192.00	10.0
1000	(8+9)-V-4	-1023	101	-2238	-0.84	3.12	-6.63	132.00	192.00	192.00	20
1000	(8+9)-III-4	137	86	-1819	0.11	2.66	-5.39	132.00	192.00	192.00	23
1000	(8+9)-IV-4	6126	89	1029	5.05	2.77	3.05	132.00	192.00	192.00	15
1000	(8+9)-I-4	451	86	-1679	0.37	2.65	-4.98	132.00	192.00	192.00	24
1000	(8+9)-II-2	9230	91	2464	7.61	2.82	7.30	132.00	192.00	192.00	9.1
1000	(8+9)-II-4	7174	88	1495	5.92	2.73	4.43	132.00	192.00	192.00	12
1000	(8+9)-IV-2	8183	92	1999	6.75	2.85	5.92	132.00	192.00	192.00	10
Verifiche nella direzione secondaria											
0	(8+9)-IV-4	-2199	12	3285	-4.54	1.39	40.73	132.00	192.00	192.00	4.5
0	(8+9)-II-2	-3047	25	5656	-6.30	2.99	70.11	132.00	192.00	192.00	2.6
0	(8+9)-VIII-3	503	-16	-4900	1.04	-1.84	-60.75	132.00	192.00	192.00	3.0
0	(8+9)-II-3	633	-16	-5292	1.31	-1.95	-65.61	132.00	192.00	192.00	2.8
0	(8+9)-VII-4	-114	-16	-2535	-0.23	-1.90	-31.42	132.00	192.00	192.00	5.8
0	(8+9)-II-4	-2494	15	4033	-5.15	1.74	50.00	132.00	192.00	192.00	3.7
0	(8+9)-VII-2	-3062	32	5247	-6.33	3.84	65.05	132.00	192.00	192.00	2.8
0	(8+9)-VI-1	-86	-4	-3314	-0.18	-0.47	-41.08	132.00	192.00	192.00	4.6
0	(8+9)-VI-3	798	-18	-5648	1.65	-2.19	-70.02	132.00	192.00	192.00	2.6
0	(8+9)-III-2	-2510	26	4061	-5.19	3.05	50.34	132.00	192.00	192.00	3.6
0	(8+9)-I-3	184	-18	-3922	0.38	-2.12	-48.62	132.00	192.00	192.00	3.7
0	(8+9)-III-3	95	-17	-3697	0.20	-2.01	-45.83	132.00	192.00	192.00	4.0
0	(8+9)-II-1	79	-6	-3669	0.16	-0.70	-45.49	132.00	192.00	192.00	4.1
0	(8+9)-V-3	736	-25	-5108	1.52	-2.90	-63.32	132.00	192.00	192.00	2.8
0	(8+9)-VII-3	647	-24	-4884	1.34	-2.80	-60.54	132.00	192.00	192.00	2.9
0	(8+9)-I-2	-2598	27	4285	-5.37	3.15	53.12	132.00	192.00	192.00	3.4
0	(8+9)-VI-2	-3213	27	6012	-6.64	3.22	74.53	132.00	192.00	192.00	2.5
0	(8+9)-VIII-2	-2918	24	5264	-6.03	2.88	65.26	132.00	192.00	192.00	2.8
0	(8+9)-VI-4	-2328	13	3677	-4.81	1.50	45.59	132.00	192.00	192.00	4.1
0	(8+9)-V-2	-3150	33	5472	-6.51	3.94	67.83	132.00	192.00	192.00	2.7
0	(8+9)-IV-2	-2752	22	4908	-5.69	2.64	60.85	132.00	192.00	192.00	3.0
0	(8+9)-IV-3	337	-14	-4545	0.70	-1.61	-56.34	132.00	192.00	192.00	3.3
1670	1	-3054	344	-1442	-6.31	40.61	-17.88	79.20	115.20	115.20	2.0
1670	2	-6348	714	-2965	-13.12	84.39	-36.76	118.80	172.80	172.80	1.4
1670	3	-6348	714	-2965	-13.12	84.39	-36.76	118.80	172.80	172.80	1.4
1670	4	-3054	344	-1442	-6.31	40.61	-17.88	105.60	153.60	153.60	2.6

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
1670	5	-3054	344	-1442	-6.31	40.61	-17.88	105.60	153.60	153.60	2.6
1670	6	-3054	344	-1442	-6.31	40.61	-17.88	105.60	153.60	153.60	2.6
1670	7	-3054	344	-1442	-6.31	40.61	-17.88	105.60	153.60	153.60	2.6
1670	(8+9)-VIII-4	-1886	235	-988	-3.90	27.73	-12.25	132.00	192.00	192.00	4.8
1670	(8+9)-VII-1	-2759	261	-1505	-5.70	30.85	-18.66	132.00	192.00	192.00	3.9
1670	(8+9)-I-1	-2207	251	-1110	-4.56	29.69	-13.77	132.00	192.00	192.00	4.4
1670	(8+9)-I-4	-2004	223	-883	-4.14	26.32	-10.94	132.00	192.00	192.00	5.1
1670	(8+9)-III-1	-2209	252	-1120	-4.56	29.75	-13.88	132.00	192.00	192.00	4.4
1670	(8+9)-V-4	-1454	213	-497	-3.00	25.22	-6.16	132.00	192.00	192.00	6.1
1670	(8+9)-VIII-1	-2325	239	-1005	-4.80	28.28	-12.46	132.00	192.00	192.00	4.7
1670	(8+9)-III-4	-2003	222	-874	-4.14	26.26	-10.83	132.00	192.00	192.00	5.2
1670	(8+9)-IV-1	-2160	236	-889	-4.46	27.95	-11.03	132.00	192.00	192.00	4.9
1670	(8+9)-V-1	-2758	260	-1496	-5.70	30.79	-18.55	132.00	192.00	192.00	3.9

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
0	1	315	0.19	3.84	Si	20
0	2	654	0.39	5.76	Si	15
0	3	654	0.39	5.76	Si	15
0	4	315	0.19	5.12	Si	27
0	5	315	0.19	5.12	Si	27
0	6	315	0.19	5.12	Si	27
0	7	315	0.19	5.12	Si	27
0	(8+9)-VIII-4	189	0.11	6.40	Si	56
0	(8+9)-IV-1	246	0.15	6.40	Si	43
0	(8+9)-I-2	209	0.13	6.40	Si	51
0	(8+9)-VIII-1	245	0.15	6.40	Si	44
0	(8+9)-I-3	225	0.13	6.40	Si	47
0	(8+9)-I-4	206	0.12	6.40	Si	52
0	(8+9)-II-2	186	0.11	6.40	Si	57
0	(8+9)-V-3	228	0.14	6.40	Si	47
0	(8+9)-II-4	185	0.11	6.40	Si	58
0	(8+9)-V-4	208	0.13	6.40	Si	51
0	(8+9)-III-2	211	0.13	6.40	Si	51
0	(8+9)-VI-1	249	0.15	6.40	Si	43
0	(8+9)-III-4	207	0.12	6.40	Si	52
0	(8+9)-VI-2	185	0.11	6.40	Si	58
0	(8+9)-IV-2	190	0.11	6.40	Si	56
0	(8+9)-VI-3	249	0.15	6.40	Si	43
0	(8+9)-IV-4	189	0.11	6.40	Si	57
0	(8+9)-VI-4	185	0.11	6.40	Si	58
0	(8+9)-II-3	248	0.15	6.40	Si	43
0	(8+9)-VIII-3	245	0.15	6.40	Si	43
0	(8+9)-III-3	224	0.13	6.40	Si	48
0	(8+9)-IV-3	244	0.15	6.40	Si	44
0	(8+9)-II-1	249	0.15	6.40	Si	43
0	(8+9)-III-1	227	0.14	6.40	Si	47
0	(8+9)-I-1	228	0.14	6.40	Si	47
0	(8+9)-VIII-2	189	0.11	6.40	Si	56
0	(8+9)-VII-3	226	0.14	6.40	Si	47
0	(8+9)-VII-4	210	0.13	6.40	Si	51
500	(8+9)-V-1	264	0.16	6.40	Si	40
500	(8+9)-VII-2	240	0.14	6.40	Si	44
500	(8+9)-VII-1	262	0.16	6.40	Si	41
500	(8+9)-V-2	238	0.14	6.40	Si	45
Verifiche nella direzione secondaria						
1670	1	406	0.77	3.84	Si	5.0
1670	2	843	1.61	5.76	Si	3.6
1670	3	843	1.61	5.76	Si	3.6
1670	4	406	0.77	5.12	Si	6.6
1670	5	406	0.77	5.12	Si	6.6
1670	6	406	0.77	5.12	Si	6.6

X	Comb.	Ty	τ_d	fvd	RS	Cs
1670	7	406	0.77	5.12	Si	6.6
1670	(8+9)-VIII-4	281	0.54	6.40	Si	12
1670	(8+9)-IV-2	286	0.55	6.40	Si	12
1670	(8+9)-V-1	292	0.56	6.40	Si	11
1670	(8+9)-I-2	286	0.55	6.40	Si	12
1670	(8+9)-V-2	296	0.56	6.40	Si	11
1670	(8+9)-I-4	277	0.53	6.40	Si	12
1670	(8+9)-V-3	264	0.50	6.40	Si	13
1670	(8+9)-II-2	287	0.55	6.40	Si	12
1670	(8+9)-V-4	267	0.51	6.40	Si	13
1670	(8+9)-II-4	284	0.54	6.40	Si	12
1670	(8+9)-VI-1	278	0.53	6.40	Si	12
1670	(8+9)-III-2	286	0.55	6.40	Si	12
1670	(8+9)-VI-2	290	0.55	6.40	Si	12
1670	(8+9)-III-4	277	0.53	6.40	Si	12
1670	(8+9)-VI-3	270	0.51	6.40	Si	12
1670	(8+9)-I-1	283	0.54	6.40	Si	12
1670	(8+9)-VI-4	281	0.54	6.40	Si	12
1670	(8+9)-IV-4	283	0.54	6.40	Si	12
1670	(8+9)-VII-1	293	0.56	6.40	Si	11
1670	(8+9)-II-1	275	0.53	6.40	Si	12
1670	(8+9)-VII-2	296	0.56	6.40	Si	11
1670	(8+9)-III-1	283	0.54	6.40	Si	12
1670	(8+9)-VII-3	264	0.50	6.40	Si	13
1670	(8+9)-IV-1	276	0.53	6.40	Si	12
1670	(8+9)-VII-4	267	0.51	6.40	Si	13
1670	(8+9)-III-3	274	0.52	6.40	Si	12
1670	(8+9)-IV-3	273	0.52	6.40	Si	12
1670	(8+9)-II-3	273	0.52	6.40	Si	12
1670	(8+9)-VIII-1	279	0.53	6.40	Si	12
1670	(8+9)-VIII-2	289	0.55	6.40	Si	12
1670	(8+9)-VIII-3	270	0.52	6.40	Si	12
1670	(8+9)-I-3	273	0.52	6.40	Si	12

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	(8+9)-VIII-4	-4094	-5.07	32.00	6.3	-1.23	20.00	16	V	6.3
0	(8+9)-VIII-2	-6366	-7.88	32.00	4.1	-1.91	20.00	10	V	4.1
0	(8+9)-II-4	-5226	-6.47	32.00	4.9	-1.56	20.00	13	V	4.9
0	(8+9)-II-2	-7001	-8.66	32.00	3.7	-2.10	20.00	9.5	V	3.7
0	(8+9)-VI-4	-4978	-6.16	32.00	5.2	-1.49	20.00	13	V	5.2
0	(8+9)-VI-2	-7250	-8.97	32.00	3.6	-2.17	20.00	9.2	V	3.6
0	(8+9)-IV-2	-6118	-7.57	32.00	4.2	-1.83	20.00	11	V	4.2
0	(8+9)-IV-4	-4343	-5.37	32.00	6.0	-1.30	20.00	15	V	6.0
500	(8+9)-III-2	-5081	-6.29	32.00	5.1	-1.52	20.00	13	V	5.1
500	(8+9)-V-1	-3067	-3.79	32.00	8.4	-0.92	20.00	22	V	8.4
500	(8+9)-I-1	-2082	-2.58	32.00	12	-0.62	20.00	32	V	12
500	(8+9)-V-2	-6318	-7.82	32.00	4.1	-1.89	20.00	11	V	4.1
500	(8+9)-VII-1	-3319	-4.11	32.00	7.8	-0.99	20.00	20	V	7.8
500	(8+9)-I-2	-5333	-6.60	32.00	4.8	-1.60	20.00	13	V	4.8
500	(8+9)-VII-2	-6066	-7.51	32.00	4.3	-1.82	20.00	11	V	4.3
500	(8+9)-III-1	-2334	-2.89	32.00	11	-0.70	20.00	29	V	11
1000	1	1862	2.30	19.20	8.3	0.56	12.00	22	V	8.3
1000	2	3891	4.81	28.80	6.0	1.17	18.00	15	V	6.0
1000	3	3891	4.81	28.80	6.0	1.17	18.00	15	V	6.0
1000	4	1862	2.30	25.60	11	0.56	16.00	29	V	11
1000	5	1862	2.30	25.60	11	0.56	16.00	29	V	11
1000	6	1862	2.30	25.60	11	0.56	16.00	29	V	11
1000	7	1862	2.30	25.60	11	0.56	16.00	29	V	11
1000	(8+9)-IV-1	5153	6.38	32.00	5.0	1.54	20.00	13	V	5.0
1000	(8+9)-III-3	5938	7.35	32.00	4.4	1.78	20.00	11	V	4.4
1000	(8+9)-II-1	5993	7.41	32.00	4.3	1.79	20.00	11	V	4.3

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
1000	(8+9)-I-3	6190	7.66	32.00	4.2	1.85	20.00	11	V	4.2
1000	(8+9)-II-3	7916	9.79	32.00	3.3	2.37	20.00	8.4	V	3.3
1000	(8+9)-V-4	3914	4.84	32.00	6.6	1.17	20.00	17	V	6.6
1000	(8+9)-VII-3	7065	8.74	32.00	3.7	2.12	20.00	9.5	V	3.7
1000	(8+9)-I-4	2788	3.45	32.00	9.3	0.83	20.00	24	V	9.3
1000	(8+9)-VII-4	4166	5.15	32.00	6.2	1.25	20.00	16	V	6.2
1000	(8+9)-VI-1	5655	7.00	32.00	4.6	1.69	20.00	12	V	4.6
1000	(8+9)-VI-3	8254	10.21	32.00	3.1	2.47	20.00	8.1	V	3.1
1000	(8+9)-V-3	7317	9.05	32.00	3.5	2.19	20.00	9.1	V	3.5
1000	(8+9)-VIII-1	4815	5.96	32.00	5.4	1.44	20.00	14	V	5.4
1000	(8+9)-III-4	3040	3.76	32.00	8.5	0.91	20.00	22	V	8.5
1000	(8+9)-VIII-3	7414	9.17	32.00	3.5	2.22	20.00	9.0	V	3.5
1000	(8+9)-IV-3	7076	8.75	32.00	3.7	2.12	20.00	9.4	V	3.7
Verifiche nella direzione secondaria										
0	(8+9)-VIII-4	3615	7.47	32.00	4.3	1.81	20.00	11	V	4.3
0	(8+9)-VII-2	5584	11.54	32.00	2.8	2.79	20.00	7.2	V	2.8
0	(8+9)-III-3	-4186	-8.65	32.00	3.7	-2.09	20.00	9.6	V	3.7
0	(8+9)-IV-2	5693	11.76	32.00	2.7	2.85	20.00	7.0	V	2.7
0	(8+9)-III-4	-1344	-2.78	32.00	12	-0.67	20.00	30	V	12
0	(8+9)-VIII-2	6055	12.51	32.00	2.6	3.03	20.00	6.6	V	2.6
0	(8+9)-IV-1	-3782	-7.81	32.00	4.1	-1.89	20.00	11	V	4.1
0	(8+9)-VII-4	-2547	-5.26	32.00	6.1	-1.27	20.00	16	V	6.1
0	(8+9)-I-1	1276	2.64	32.00	12	0.64	20.00	31	V	12
0	(8+9)-IV-3	-5499	-11.36	32.00	2.8	-2.75	20.00	7.3	V	2.8
0	(8+9)-I-3	-4448	-9.19	32.00	3.5	-2.22	20.00	9.0	V	3.5
0	(8+9)-IV-4	3976	8.22	32.00	3.9	1.99	20.00	10	V	3.9
0	(8+9)-II-1	-4656	-9.62	32.00	3.3	-2.33	20.00	8.6	V	3.3
0	(8+9)-V-1	2479	5.12	32.00	6.2	1.24	20.00	16	V	6.2
0	(8+9)-II-3	-6373	-13.17	32.00	2.4	-3.19	20.00	6.3	V	2.4
0	(8+9)-V-2	5846	12.08	32.00	2.6	2.92	20.00	6.8	V	2.6
0	(8+9)-III-1	1538	3.18	32.00	10	0.77	20.00	26	V	10
0	(8+9)-V-3	-5652	-11.68	32.00	2.7	-2.83	20.00	7.1	V	2.7
0	(8+9)-VIII-3	-5860	-12.11	32.00	2.6	-2.93	20.00	6.8	V	2.6
0	(8+9)-V-4	-2285	-4.72	32.00	6.8	-1.14	20.00	18	V	6.8
0	(8+9)-VII-3	-5390	-11.14	32.00	2.9	-2.69	20.00	7.4	V	2.9
0	(8+9)-VI-1	-4295	-8.87	32.00	3.6	-2.15	20.00	9.3	V	3.6
0	(8+9)-I-4	-1081	-2.23	32.00	14	-0.54	20.00	37	V	14
0	(8+9)-VI-2	6929	14.32	32.00	2.2	3.46	20.00	5.8	V	2.2
0	(8+9)-II-4	4850	10.02	32.00	3.2	2.43	20.00	8.2	V	3.2
0	(8+9)-VIII-1	-3420	-7.07	32.00	4.5	-1.71	20.00	12	V	4.5
0	(8+9)-I-2	4643	9.59	32.00	3.3	2.32	20.00	8.6	V	3.3
0	(8+9)-II-2	6568	13.57	32.00	2.4	3.28	20.00	6.1	V	2.4
0	(8+9)-III-2	4381	9.05	32.00	3.5	2.19	20.00	9.1	V	3.5
0	(8+9)-VI-3	-6734	-13.91	32.00	2.3	-3.37	20.00	5.9	V	2.3
0	(8+9)-VI-4	4489	9.28	32.00	3.4	2.24	20.00	8.9	V	3.4
0	(8+9)-VII-1	2742	5.66	32.00	5.6	1.37	20.00	15	V	5.6
1670	1	340	0.70	19.20	27	0.17	12.00	71	V	27
1670	2	631	1.30	28.80	22	0.32	18.00	57	V	22
1670	3	631	1.30	28.80	22	0.32	18.00	57	V	22
1670	4	340	0.70	25.60	36	0.17	16.00	94	V	36
1670	5	340	0.70	25.60	36	0.17	16.00	94	V	36
1670	6	340	0.70	25.60	36	0.17	16.00	94	V	36
1670	7	340	0.70	25.60	36	0.17	16.00	94	V	36

Verifiche a instabilità

Setto(X)	Comb.	k _{critc}	k _{critm}	λ_{relc}	λ_{relm}	σ_n	σ_{mx}	σ_{my}	f _{td}	f _{cd}	f _{md}	Cs
(cm)						kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	
35(0.0)	(8+9)-VI-2	--	--	--	--	3.10	-0.60	-4.59	132.00	192.00	192.00	20
36(0.0)	3	--	--	--	--	2.20	3.61	-5.17	118.80	172.80	172.80	14

Setto(X)	Comb.	kcrit _c	kcrit _m	λ _{relc}	λ _{relm}	σ _n	σ _{mx}	σ _{my}	ftd	fcd	fmd	Cs
37(0.0)	(8+9)-V-3	1.00	--	0.20	--	-1.49	-3.09	4.57	132.00	192.00	192.00	21
38(120.0)	(8+9)-VI-2	--	--	--	--	8.09	-1.38	13.98	132.00	192.00	192.00	7.1
39(100.0)	3	--	--	--	--	4.99	8.40	-8.42	118.80	172.80	172.80	7.2

Parete Xlam 15 - Nodi: [18-22-14-15-23-24-18-19-25-21-109-25-108] - **Crit.Prog.** Criterio di verifica XLAM 0 - **Verificato:** [Cs=1.387,Comb=(8+9)-V-2]

Geometria setti

Setto	Crit.	X mm	L cm	S cm	X90 mm	L90 cm	S90 cm
35	Criterio di verifica XLAM 0	0	387.0	12.1	0	229.3	12.1
		1147	387.0	12.1	1935	229.3	12.1
		2293	387.0	12.1	3870	229.3	12.1
36	Criterio di verifica XLAM 0	0	387.0	12.1	0	100.7	12.1
		504	387.0	12.1	1935	100.7	12.1
		1007	387.0	12.1	3870	100.7	12.1
37	Criterio di verifica XLAM 0	0	387.0	12.1	0	55.2	12.1
		276	387.0	12.1	1935	55.2	12.1
		552	387.0	12.1	3870	55.2	12.1
38	Criterio di verifica XLAM 0	0	167.0	12.1	0	120.0	12.1
		600	167.0	12.1	835	120.0	12.1
		1200	167.0	12.1	1670	120.0	12.1
39	Criterio di verifica XLAM 0	0	167.0	12.1	0	100.0	12.1
		500	167.0	12.1	835	100.0	12.1
		1000	167.0	12.1	1670	100.0	12.1

Setto 35: origine (1384.8,2430.3,193.5), direzione (-0.200098,0.979776,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X mm	Comb.	N kg	M _x kg*m	M _y kg*m	σ _n kg/cmq	σ _{mx} kg/cmq	σ _{my} kg/cmq	ftd kg/cmq	fcd kg/cmq	fmd kg/cmq	Cs
0	(8+9)-VIII-4	4263	-20	-4041	1.52	-0.27	-2.23	132.00	192.00	192.00	41
0	(8+9)-IV-1	-4751	12	4665	-1.69	0.16	2.57	132.00	192.00	192.00	70
0	(8+9)-VII-2	7275	-45	-6931	2.59	-0.61	-3.82	132.00	192.00	192.00	23
0	(8+9)-III-3	-5707	22	5562	-2.03	0.29	3.07	132.00	192.00	192.00	57
0	(8+9)-IV-2	7092	-36	-6761	2.52	-0.48	-3.73	132.00	192.00	192.00	24
0	(8+9)-III-4	-2154	8	2134	-0.77	0.10	1.18	132.00	192.00	192.00	>100
0	(8+9)-VIII-2	7566	-40	-7220	2.69	-0.53	-3.98	132.00	192.00	192.00	23
0	(8+9)-VII-3	-7289	34	7095	-2.59	0.45	3.92	132.00	192.00	192.00	44
0	(8+9)-VII-4	-3736	19	3667	-1.33	0.26	2.02	132.00	192.00	192.00	84
0	(8+9)-I-2	6036	-35	-5730	2.15	-0.47	-3.16	132.00	192.00	192.00	28
0	(8+9)-IV-3	-7105	24	6925	-2.53	0.32	3.82	132.00	192.00	192.00	46
0	(8+9)-I-4	-1810	6	1803	-0.64	0.08	0.99	132.00	192.00	192.00	>100
0	(8+9)-IV-4	4738	-24	-4501	1.69	-0.32	-2.48	132.00	192.00	192.00	37
0	(8+9)-II-2	8237	-42	-7866	2.93	-0.56	-4.34	132.00	192.00	192.00	21
0	(8+9)-V-1	3378	-29	-3172	1.20	-0.39	-1.75	132.00	192.00	192.00	49
0	(8+9)-II-4	5883	-29	-5606	2.09	-0.39	-3.09	132.00	192.00	192.00	29
0	(8+9)-V-2	7618	-47	-7263	2.71	-0.63	-4.01	132.00	192.00	192.00	22
0	(8+9)-III-2	5693	-34	-5398	2.03	-0.45	-2.98	132.00	192.00	192.00	30
0	(8+9)-V-3	-7632	35	7427	-2.72	0.47	4.10	132.00	192.00	192.00	42
0	(8+9)-VIII-1	-4277	8	4205	-1.52	0.11	2.32	132.00	192.00	192.00	79
0	(8+9)-V-4	-3392	18	3336	-1.21	0.24	1.84	132.00	192.00	192.00	92
0	(8+9)-I-3	-6050	24	5894	-2.15	0.32	3.25	132.00	192.00	192.00	53
0	(8+9)-VI-1	-5422	14	5310	-1.93	0.19	2.93	132.00	192.00	192.00	61
0	(8+9)-II-3	-8251	30	8030	-2.94	0.40	4.43	132.00	192.00	192.00	39
0	(8+9)-VI-2	8711	-45	-8326	3.10	-0.60	-4.59	132.00	192.00	192.00	20
0	(8+9)-VIII-3	-7580	28	7384	-2.70	0.37	4.07	132.00	192.00	192.00	43
0	(8+9)-II-1	-5897	17	5770	-2.10	0.23	3.18	132.00	192.00	192.00	56
0	(8+9)-III-1	2140	-19	-1970	0.76	-0.26	-1.09	132.00	192.00	192.00	78
0	(8+9)-I-1	1796	-18	-1639	0.64	-0.24	-0.90	132.00	192.00	192.00	93

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-VI-3	-8725	33	8490	-3.11	0.45	4.68	132.00	192.00	192.00	37
0	(8+9)-VI-4	5408	-26	-5146	1.92	-0.34	-2.84	132.00	192.00	192.00	32
0	(8+9)-VII-1	3722	-31	-3503	1.32	-0.42	-1.93	132.00	192.00	192.00	45
2293	1	91	-29	74	0.03	-0.38	0.04	79.20	115.20	115.20	>100
2293	2	175	-59	107	0.06	-0.79	0.06	118.80	172.80	172.80	>100
2293	3	175	-59	107	0.06	-0.79	0.06	118.80	172.80	172.80	>100
2293	4	91	-29	74	0.03	-0.38	0.04	105.60	153.60	153.60	>100
2293	5	91	-29	74	0.03	-0.38	0.04	105.60	153.60	153.60	>100
2293	6	91	-29	74	0.03	-0.38	0.04	105.60	153.60	153.60	>100
2293	7	91	-29	74	0.03	-0.38	0.04	105.60	153.60	153.60	>100
Verifiche nella direzione secondaria											
0	(8+9)-VIII-4	-2081	-71	8625	-1.87	-3.67	20.34	132.00	192.00	192.00	8.0
0	(8+9)-VII-2	-12792	-200	6792	-11.53	-10.32	16.01	132.00	192.00	192.00	7.1
0	(8+9)-III-3	6207	92	-5152	5.59	4.76	-12.15	132.00	192.00	192.00	7.7
0	(8+9)-IV-2	-7198	-142	10475	-6.49	-7.33	24.70	132.00	192.00	192.00	6.0
0	(8+9)-III-4	4264	36	625	3.84	1.86	1.47	132.00	192.00	192.00	22
0	(8+9)-VIII-2	-8071	-161	10890	-7.27	-8.30	25.68	132.00	192.00	192.00	5.6
0	(8+9)-IV-1	-721	45	-8780	-0.65	2.33	-20.70	132.00	192.00	192.00	8.3
0	(8+9)-VII-4	7174	99	-756	6.46	5.10	-1.78	132.00	192.00	192.00	12
0	(8+9)-I-1	-6633	-70	108	-5.98	-3.62	0.25	132.00	192.00	192.00	47
0	(8+9)-IV-3	3523	97	-10216	3.17	5.01	-24.09	132.00	192.00	192.00	5.7
0	(8+9)-I-3	7514	103	-4678	6.77	5.32	-11.03	132.00	192.00	192.00	7.3
0	(8+9)-IV-4	-2954	-90	9040	-2.66	-4.65	21.31	132.00	192.00	192.00	7.4
0	(8+9)-II-1	3634	82	-7201	3.27	4.21	-16.98	132.00	192.00	192.00	7.4
0	(8+9)-V-1	-9543	-133	1489	-8.60	-6.86	3.51	132.00	192.00	192.00	18
0	(8+9)-II-3	7878	134	-8637	7.10	6.89	-20.36	132.00	192.00	192.00	5.1
0	(8+9)-V-2	-14099	-211	6318	-12.70	-10.88	14.90	132.00	192.00	192.00	7.2
0	(8+9)-III-1	-7939	-81	-366	-7.15	-4.18	-0.86	132.00	192.00	192.00	36
0	(8+9)-V-3	10424	166	-6059	9.39	8.56	-14.29	132.00	192.00	192.00	5.3
0	(8+9)-VIII-3	4396	116	-10630	3.96	5.98	-25.06	132.00	192.00	192.00	5.2
0	(8+9)-V-4	5868	88	-1230	5.29	4.53	-2.90	132.00	192.00	192.00	13
0	(8+9)-VII-3	9117	155	-6533	8.22	8.00	-15.40	132.00	192.00	192.00	5.4
0	(8+9)-VI-1	2761	63	-6787	2.49	3.24	-16.00	132.00	192.00	192.00	8.4
0	(8+9)-I-4	2958	25	151	2.67	1.30	0.36	132.00	192.00	192.00	35
0	(8+9)-VI-2	-12426	-198	9310	-11.20	-10.18	21.95	132.00	192.00	192.00	5.9
0	(8+9)-II-4	-7309	-127	7460	-6.59	-6.53	17.59	132.00	192.00	192.00	7.9
0	(8+9)-VIII-1	-1594	26	-8366	-1.44	1.35	-19.72	132.00	192.00	192.00	9.1
0	(8+9)-I-2	-11189	-148	4937	-10.08	-7.64	11.64	132.00	192.00	192.00	9.7
0	(8+9)-II-2	-11553	-179	8896	-10.41	-9.21	20.97	132.00	192.00	192.00	6.2
0	(8+9)-III-2	-9882	-137	5411	-8.90	-7.08	12.76	132.00	192.00	192.00	9.5
0	(8+9)-VI-3	8751	153	-9051	7.89	7.86	-21.34	132.00	192.00	192.00	4.7
0	(8+9)-VI-4	-6436	-108	7046	-5.80	-5.56	16.61	132.00	192.00	192.00	8.6
0	(8+9)-VII-1	-10849	-144	1015	-9.78	-7.42	2.39	132.00	192.00	192.00	19
1935	1	-2069	25	545	-1.86	1.29	1.28	79.20	115.20	115.20	44
1935	2	-4071	52	1063	-3.67	2.66	2.51	118.80	172.80	172.80	33
1935	3	-4071	52	1063	-3.67	2.66	2.51	118.80	172.80	172.80	33
1935	4	-2069	25	545	-1.86	1.29	1.28	105.60	153.60	153.60	59
1935	5	-2069	25	545	-1.86	1.29	1.28	105.60	153.60	153.60	59
1935	6	-2069	25	545	-1.86	1.29	1.28	105.60	153.60	153.60	59
1935	7	-2069	25	545	-1.86	1.29	1.28	105.60	153.60	153.60	59

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
0	1	-32	0.01	3.84	Si	>100
0	2	-66	0.02	5.76	Si	>100
0	3	-66	0.02	5.76	Si	>100
0	4	-32	0.01	5.12	Si	>100
0	5	-32	0.01	5.12	Si	>100
0	6	-32	0.01	5.12	Si	>100
0	7	-32	0.01	5.12	Si	>100
2293	(8+9)-VIII-4	45	0.01	6.40	Si	>100
2293	(8+9)-IV-1	-42	0.01	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
2293	(8+9)-V-1	91	0.02	6.40	Si	>100
2293	(8+9)-I-2	165	0.04	6.40	Si	>100
2293	(8+9)-V-2	153	0.04	6.40	Si	>100
2293	(8+9)-I-4	-102	0.03	6.40	Si	>100
2293	(8+9)-V-3	-153	0.04	6.40	Si	>100
2293	(8+9)-II-2	145	0.04	6.40	Si	>100
2293	(8+9)-V-4	-90	0.02	6.40	Si	>100
2293	(8+9)-II-4	64	0.02	6.40	Si	>100
2293	(8+9)-VI-1	-67	0.02	6.40	Si	>100
2293	(8+9)-III-2	158	0.04	6.40	Si	>100
2293	(8+9)-VI-2	141	0.04	6.40	Si	>100
2293	(8+9)-III-4	-109	0.03	6.40	Si	>100
2293	(8+9)-VI-3	-141	0.04	6.40	Si	>100
2293	(8+9)-IV-2	122	0.03	6.40	Si	>100
2293	(8+9)-VI-4	68	0.02	6.40	Si	>100
2293	(8+9)-IV-4	42	0.01	6.40	Si	>100
2293	(8+9)-VII-1	98	0.03	6.40	Si	>100
2293	(8+9)-II-1	-64	0.02	6.40	Si	>100
2293	(8+9)-VII-2	147	0.04	6.40	Si	>100
2293	(8+9)-III-1	109	0.03	6.40	Si	>100
2293	(8+9)-VII-3	-146	0.04	6.40	Si	>100
2293	(8+9)-I-1	102	0.03	6.40	Si	>100
2293	(8+9)-VII-4	-97	0.03	6.40	Si	>100
2293	(8+9)-III-3	-158	0.04	6.40	Si	>100
2293	(8+9)-IV-3	-122	0.03	6.40	Si	>100
2293	(8+9)-II-3	-144	0.04	6.40	Si	>100
2293	(8+9)-VIII-1	-45	0.01	6.40	Si	>100
2293	(8+9)-VIII-2	119	0.03	6.40	Si	>100
2293	(8+9)-VIII-3	-118	0.03	6.40	Si	>100
2293	(8+9)-I-3	-165	0.04	6.40	Si	>100
Verifiche nella direzione secondaria						
0	1	33	0.03	3.84	Si	>100
0	2	70	0.06	5.76	Si	98
0	3	70	0.06	5.76	Si	98
0	4	33	0.03	5.12	Si	>100
0	5	33	0.03	5.12	Si	>100
0	6	33	0.03	5.12	Si	>100
0	7	33	0.03	5.12	Si	>100
0	(8+9)-VII-4	-83	0.07	6.40	Si	93
0	(8+9)-VII-1	128	0.11	6.40	Si	60
0	(8+9)-V-4	-72	0.06	6.40	Si	>100
0	(8+9)-V-1	117	0.10	6.40	Si	66
1935	(8+9)-VIII-4	88	0.07	6.40	Si	87
1935	(8+9)-IV-2	150	0.13	6.40	Si	51
1935	(8+9)-V-3	-151	0.13	6.40	Si	51
1935	(8+9)-II-2	182	0.15	6.40	Si	42
1935	(8+9)-I-3	-95	0.08	6.40	Si	81
1935	(8+9)-II-4	137	0.11	6.40	Si	56
1935	(8+9)-VI-1	-77	0.06	6.40	Si	>100
1935	(8+9)-III-2	130	0.11	6.40	Si	59
1935	(8+9)-VI-2	199	0.17	6.40	Si	39
1935	(8+9)-III-4	-22	0.02	6.40	Si	>100
1935	(8+9)-VI-3	-155	0.13	6.40	Si	49
1935	(8+9)-II-1	-93	0.08	6.40	Si	83
1935	(8+9)-VI-4	120	0.10	6.40	Si	64
1935	(8+9)-IV-4	105	0.09	6.40	Si	73
1935	(8+9)-I-2	139	0.12	6.40	Si	55
1935	(8+9)-V-2	195	0.16	6.40	Si	39
1935	(8+9)-VII-2	185	0.15	6.40	Si	42
1935	(8+9)-III-1	66	0.05	6.40	Si	>100
1935	(8+9)-VII-3	-141	0.12	6.40	Si	54
1935	(8+9)-IV-1	-61	0.05	6.40	Si	>100
1935	(8+9)-I-1	56	0.05	6.40	Si	>100
1935	(8+9)-III-3	-86	0.07	6.40	Si	90

X	Comb.	Ty	τ_d	fvd	RS	Cs
1935	(8+9)-IV-3	-107	0.09	6.40	Si	72
1935	(8+9)-II-3	-139	0.12	6.40	Si	55
1935	(8+9)-VIII-1	-44	0.04	6.40	Si	>100
1935	(8+9)-VIII-2	167	0.14	6.40	Si	46
1935	(8+9)-VIII-3	-123	0.10	6.40	Si	62
1935	(8+9)-I-4	-13	0.01	6.40	Si	>100

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	1	478	0.25	19.20	75	0.06	12.00	>100	V	75
0	2	1126	0.60	28.80	48	0.15	18.00	>100	V	48
0	3	1126	0.60	28.80	48	0.15	18.00	>100	V	48
0	4	478	0.25	25.60	>100	0.06	16.00	>100	V	>100
0	5	478	0.25	25.60	>100	0.06	16.00	>100	V	>100
0	6	478	0.25	25.60	>100	0.06	16.00	>100	V	>100
0	7	478	0.25	25.60	>100	0.06	16.00	>100	V	>100
1147	(8+9)-IV-2	-13744	-7.34	32.00	4.4	-1.78	20.00	11	V	4.4
1147	(8+9)-V-2	-14663	-7.83	32.00	4.1	-1.89	20.00	11	V	4.1
1147	(8+9)-I-2	-11378	-6.07	32.00	5.3	-1.47	20.00	14	V	5.3
1147	(8+9)-V-3	14913	7.96	32.00	4.0	1.93	20.00	10	V	4.0
1147	(8+9)-I-4	3566	1.90	32.00	17	0.46	20.00	43	V	17
1147	(8+9)-V-4	6852	3.66	32.00	8.7	0.89	20.00	23	V	8.7
1147	(8+9)-II-2	-15552	-8.30	32.00	3.9	-2.01	20.00	10.0	V	3.9
1147	(8+9)-VI-1	10333	5.52	32.00	5.8	1.33	20.00	15	V	5.8
1147	(8+9)-II-4	-11069	-5.91	32.00	5.4	-1.43	20.00	14	V	5.4
1147	(8+9)-VI-2	-16537	-8.83	32.00	3.6	-2.14	20.00	9.4	V	3.6
1147	(8+9)-III-2	-10835	-5.78	32.00	5.5	-1.40	20.00	14	V	5.5
1147	(8+9)-VI-3	16787	8.96	32.00	3.6	2.17	20.00	9.2	V	3.6
1147	(8+9)-III-4	4109	2.19	32.00	15	0.53	20.00	38	V	15
1147	(8+9)-VI-4	-10083	-5.38	32.00	5.9	-1.30	20.00	15	V	5.9
1147	(8+9)-I-1	-3317	-1.77	32.00	18	-0.43	20.00	47	V	18
1147	(8+9)-VII-1	-7144	-3.81	32.00	8.4	-0.92	20.00	22	V	8.4
1147	(8+9)-IV-4	-9261	-4.94	32.00	6.5	-1.20	20.00	17	V	6.5
1147	(8+9)-VII-2	-14121	-7.54	32.00	4.2	-1.82	20.00	11	V	4.2
1147	(8+9)-I-3	11627	6.21	32.00	5.2	1.50	20.00	13	V	5.2
1147	(8+9)-VII-3	14371	7.67	32.00	4.2	1.86	20.00	11	V	4.2
1147	(8+9)-II-3	15801	8.44	32.00	3.8	2.04	20.00	9.8	V	3.8
1147	(8+9)-VII-4	7394	3.95	32.00	8.1	0.96	20.00	21	V	8.1
1147	(8+9)-III-3	11085	5.92	32.00	5.4	1.43	20.00	14	V	5.4
1147	(8+9)-VIII-1	8525	4.55	32.00	7.0	1.10	20.00	18	V	7.0
1147	(8+9)-IV-3	13994	7.47	32.00	4.3	1.81	20.00	11	V	4.3
1147	(8+9)-VIII-2	-14730	-7.86	32.00	4.1	-1.90	20.00	11	V	4.1
1147	(8+9)-II-1	11318	6.04	32.00	5.3	1.46	20.00	14	V	5.3
1147	(8+9)-IV-1	9511	5.08	32.00	6.3	1.23	20.00	16	V	6.3
1147	(8+9)-V-1	-6602	-3.52	32.00	9.1	-0.85	20.00	23	V	9.1
1147	(8+9)-III-1	-3859	-2.06	32.00	16	-0.50	20.00	40	V	16
1147	(8+9)-VIII-3	14979	8.00	32.00	4.0	1.94	20.00	10	V	4.0
1147	(8+9)-VIII-4	-8275	-4.42	32.00	7.2	-1.07	20.00	19	V	7.2
Verifiche nella direzione secondaria										
0	(8+9)-VII-4	-5942	-5.35	32.00	6.0	-1.30	20.00	15	V	6.0
1935	(8+9)-VIII-4	6363	5.73	32.00	5.6	1.39	20.00	14	V	5.6
1935	(8+9)-VII-2	11296	10.18	32.00	3.1	2.46	20.00	8.1	V	3.1
1935	(8+9)-III-3	-8654	-7.80	32.00	4.1	-1.89	20.00	11	V	4.1
1935	(8+9)-IV-2	10736	9.67	32.00	3.3	2.34	20.00	8.5	V	3.3
1935	(8+9)-III-4	-3279	-2.95	32.00	11	-0.72	20.00	28	V	11
1935	(8+9)-VIII-2	11534	10.39	32.00	3.1	2.52	20.00	8.0	V	3.1
1935	(8+9)-IV-1	-7182	-6.47	32.00	4.9	-1.57	20.00	13	V	4.9
1935	(8+9)-VII-3	-11317	-10.20	32.00	3.1	-2.47	20.00	8.1	V	3.1
1935	(8+9)-I-2	9179	8.27	32.00	3.9	2.00	20.00	10.0	V	3.9
1935	(8+9)-IV-3	-10756	-9.69	32.00	3.3	-2.35	20.00	8.5	V	3.3
1935	(8+9)-I-4	-2734	-2.46	32.00	13	-0.60	20.00	34	V	13
1935	(8+9)-IV-4	7162	6.45	32.00	5.0	1.56	20.00	13	V	5.0

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
1935	(8+9)-II-2	12553	11.31	32.00	2.8	2.74	20.00	7.3	V	2.8
1935	(8+9)-V-1	5376	4.84	32.00	6.6	1.17	20.00	17	V	6.6
1935	(8+9)-II-4	8979	8.09	32.00	4.0	1.96	20.00	10	V	4.0
1935	(8+9)-V-2	11842	10.67	32.00	3.0	2.58	20.00	7.7	V	3.0
1935	(8+9)-III-2	8634	7.78	32.00	4.1	1.88	20.00	11	V	4.1
1935	(8+9)-V-3	-11862	-10.69	32.00	3.0	-2.59	20.00	7.7	V	3.0
1935	(8+9)-VIII-1	-6383	-5.75	32.00	5.6	-1.39	20.00	14	V	5.6
1935	(8+9)-V-4	-5396	-4.86	32.00	6.6	-1.18	20.00	17	V	6.6
1935	(8+9)-I-3	-9200	-8.29	32.00	3.9	-2.01	20.00	10.0	V	3.9
1935	(8+9)-VI-1	-8201	-7.39	32.00	4.3	-1.79	20.00	11	V	4.3
1935	(8+9)-II-3	-12574	-11.33	32.00	2.8	-2.74	20.00	7.3	V	2.8
1935	(8+9)-VI-2	13352	12.03	32.00	2.7	2.91	20.00	6.9	V	2.7
1935	(8+9)-VIII-3	-11555	-10.41	32.00	3.1	-2.52	20.00	7.9	V	3.1
1935	(8+9)-II-1	-9000	-8.11	32.00	3.9	-1.96	20.00	10	V	3.9
1935	(8+9)-III-1	3259	2.94	32.00	11	0.71	20.00	28	V	11
1935	(8+9)-I-1	2713	2.44	32.00	13	0.59	20.00	34	V	13
1935	(8+9)-VI-3	-13372	-12.05	32.00	2.7	-2.92	20.00	6.9	V	2.7
1935	(8+9)-VI-4	8181	7.37	32.00	4.3	1.78	20.00	11	V	4.3
1935	(8+9)-VII-1	5921	5.34	32.00	6.0	1.29	20.00	15	V	6.0
3870	1	-111	-0.10	19.20	>100	-0.02	12.00	>100	V	>100
3870	2	-309	-0.28	28.80	>100	-0.07	18.00	>100	V	>100
3870	3	-309	-0.28	28.80	>100	-0.07	18.00	>100	V	>100
3870	4	-111	-0.10	25.60	>100	-0.02	16.00	>100	V	>100
3870	5	-111	-0.10	25.60	>100	-0.02	16.00	>100	V	>100
3870	6	-111	-0.10	25.60	>100	-0.02	16.00	>100	V	>100
3870	7	-111	-0.10	25.60	>100	-0.02	16.00	>100	V	>100

Setto 36: origine (1429.0,2214.1,193.5), direzione (-0.200098,0.979776,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	
0	1	2993	130	-4535	1.07	1.74	-2.50	79.20	115.20	115.20	20
0	2	6191	270	-9363	2.20	3.61	-5.17	118.80	172.80	172.80	14
0	3	6191	270	-9363	2.20	3.61	-5.17	118.80	172.80	172.80	14
0	4	2993	130	-4535	1.07	1.74	-2.50	105.60	153.60	153.60	27
0	5	2993	130	-4535	1.07	1.74	-2.50	105.60	153.60	153.60	27
0	6	2993	130	-4535	1.07	1.74	-2.50	105.60	153.60	153.60	27
0	7	2993	130	-4535	1.07	1.74	-2.50	105.60	153.60	153.60	27
0	(8+9)-VIII-4	5105	93	-6677	1.82	1.24	-3.68	132.00	192.00	192.00	25
0	(8+9)-IV-1	-1342	92	892	-0.48	1.22	0.49	132.00	192.00	192.00	>100
0	(8+9)-V-1	4628	79	-6204	1.65	1.06	-3.42	132.00	192.00	192.00	28
0	(8+9)-I-2	6469	95	-8208	2.30	1.26	-4.53	132.00	192.00	192.00	21
0	(8+9)-V-2	7722	79	-9825	2.75	1.06	-5.42	132.00	192.00	192.00	18
0	(8+9)-I-4	763	85	-1683	0.27	1.14	-0.93	132.00	192.00	192.00	78
0	(8+9)-V-3	-3583	101	3555	-1.28	1.34	1.96	132.00	192.00	192.00	58
0	(8+9)-II-2	8081	91	-10149	2.88	1.22	-5.60	132.00	192.00	192.00	17
0	(8+9)-V-4	-490	101	-66	-0.17	1.34	-0.04	132.00	192.00	192.00	>100
0	(8+9)-II-4	6369	89	-8192	2.27	1.18	-4.52	132.00	192.00	192.00	21
0	(8+9)-VI-1	-1855	87	1437	-0.66	1.16	0.79	132.00	192.00	192.00	98
0	(8+9)-III-2	6203	94	-7899	2.21	1.26	-4.36	132.00	192.00	192.00	22
0	(8+9)-VI-2	8457	87	-10634	3.01	1.16	-5.87	132.00	192.00	192.00	17
0	(8+9)-III-4	496	85	-1374	0.18	1.14	-0.76	132.00	192.00	192.00	89
0	(8+9)-VI-3	-4318	93	4365	-1.54	1.24	2.41	132.00	192.00	192.00	52
0	(8+9)-IV-2	7193	91	-9119	2.56	1.22	-5.03	132.00	192.00	192.00	19
0	(8+9)-VI-4	5993	93	-7707	2.13	1.25	-4.25	132.00	192.00	192.00	22
0	(8+9)-IV-4	5481	88	-7162	1.95	1.18	-3.95	132.00	192.00	192.00	24
0	(8+9)-VII-1	4895	79	-6512	1.74	1.06	-3.59	132.00	192.00	192.00	27
0	(8+9)-II-1	-2231	91	1922	-0.79	1.22	1.06	132.00	192.00	192.00	84
0	(8+9)-VII-2	7455	79	-9516	2.65	1.06	-5.25	132.00	192.00	192.00	19
0	(8+9)-III-1	3642	95	-4896	1.30	1.26	-2.70	132.00	192.00	192.00	33
0	(8+9)-VII-3	-3317	101	3246	-1.18	1.34	1.79	132.00	192.00	192.00	61
0	(8+9)-I-1	3376	95	-4587	1.20	1.26	-2.53	132.00	192.00	192.00	35
0	(8+9)-VII-4	-756	100	243	-0.27	1.34	0.13	132.00	192.00	192.00	>100

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-III-3	-2064	85	1629	-0.73	1.14	0.90	132.00	192.00	192.00	94
0	(8+9)-IV-3	-3054	89	2850	-1.09	1.19	1.57	132.00	192.00	192.00	69
0	(8+9)-II-3	-3943	89	3880	-1.40	1.18	2.14	132.00	192.00	192.00	58
0	(8+9)-VIII-1	-967	87	407	-0.34	1.16	0.22	132.00	192.00	192.00	>100
0	(8+9)-VIII-2	7568	87	-9604	2.69	1.16	-5.30	132.00	192.00	192.00	19
0	(8+9)-VIII-3	-3430	93	3335	-1.22	1.25	1.84	132.00	192.00	192.00	62
0	(8+9)-I-3	-2331	85	1938	-0.83	1.14	1.07	132.00	192.00	192.00	87
Verifiche nella direzione secondaria											
0	(8+9)-VIII-4	-2318	-27	3217	-4.76	-3.12	39.32	132.00	192.00	192.00	4.5
0	(8+9)-VI-2	-2649	-79	6700	-5.43	-9.33	81.90	132.00	192.00	192.00	2.1
0	(8+9)-VI-4	-2447	-36	4104	-5.02	-4.26	50.17	132.00	192.00	192.00	3.5
0	(8+9)-IV-2	-2438	-63	5440	-5.00	-7.40	66.51	132.00	192.00	192.00	2.6
0	(8+9)-III-2	-2421	-81	4342	-4.97	-9.45	53.09	132.00	192.00	192.00	3.1
0	(8+9)-VIII-2	-2520	-70	5813	-5.17	-8.19	71.06	132.00	192.00	192.00	2.4
0	(8+9)-III-3	-2244	34	-4622	-4.60	3.95	-56.51	132.00	192.00	192.00	3.2
0	(8+9)-VII-4	-2022	41	-3071	-4.15	4.82	-37.54	132.00	192.00	192.00	4.5
0	(8+9)-VI-3	-2016	33	-6980	-4.14	3.83	-85.33	132.00	192.00	192.00	2.2
0	(8+9)-VII-2	-2695	-103	5583	-5.53	-12.07	68.26	132.00	192.00	192.00	2.4
0	(8+9)-IV-1	-2265	-14	-3869	-4.65	-1.60	-47.30	132.00	192.00	192.00	3.9
0	(8+9)-I-3	-2205	37	-4889	-4.52	4.29	-59.76	132.00	192.00	192.00	3.0
0	(8+9)-II-1	-2136	-4	-4756	-4.38	-0.46	-58.14	132.00	192.00	192.00	3.3
0	(8+9)-IV-3	-2227	16	-5721	-4.57	1.90	-69.93	132.00	192.00	192.00	2.7
0	(8+9)-II-3	-2098	26	-6608	-4.30	3.04	-80.78	132.00	192.00	192.00	2.3
0	(8+9)-IV-4	-2400	-33	3589	-4.92	-3.91	43.87	132.00	192.00	192.00	4.0
0	(8+9)-VIII-3	-2145	23	-6093	-4.40	2.69	-74.48	132.00	192.00	192.00	2.5
0	(8+9)-V-1	-2605	-85	2524	-5.34	-9.99	30.86	132.00	192.00	192.00	4.7
0	(8+9)-VII-3	-1970	56	-5863	-4.04	6.57	-71.68	132.00	192.00	192.00	2.5
0	(8+9)-V-2	-2734	-106	5849	-5.61	-12.41	71.51	132.00	192.00	192.00	2.3
0	(8+9)-VII-1	-2643	-88	2791	-5.42	-10.33	34.11	132.00	192.00	192.00	4.3
0	(8+9)-II-4	-2529	-43	4476	-5.19	-5.05	54.72	132.00	192.00	192.00	3.2
0	(8+9)-VIII-1	-2347	-20	-3497	-4.82	-2.38	-42.75	132.00	192.00	192.00	4.2
0	(8+9)-I-2	-2460	-83	4609	-5.05	-9.79	56.34	132.00	192.00	192.00	2.9
0	(8+9)-II-2	-2567	-73	6327	-5.27	-8.55	77.35	132.00	192.00	192.00	2.2
0	(8+9)-V-3	-1931	59	-6129	-3.96	6.91	-74.93	132.00	192.00	192.00	2.3
0	(8+9)-V-4	-2060	38	-2804	-4.23	4.48	-34.28	132.00	192.00	192.00	4.9
0	(8+9)-VI-1	-2218	-11	-4384	-4.55	-1.24	-53.59	132.00	192.00	192.00	3.5
3870	1	-3947	215	1825	-8.10	25.23	22.31	79.20	115.20	115.20	2.4
3870	2	-8155	446	3793	-16.73	52.41	46.37	118.80	172.80	172.80	1.7
3870	3	-8155	446	3793	-16.73	52.41	46.37	118.80	172.80	172.80	1.7
3870	4	-3947	215	1825	-8.10	25.23	22.31	105.60	153.60	153.60	3.2
3870	5	-3947	215	1825	-8.10	25.23	22.31	105.60	153.60	153.60	3.2
3870	6	-3947	215	1825	-8.10	25.23	22.31	105.60	153.60	153.60	3.2
3870	7	-3947	215	1825	-8.10	25.23	22.31	105.60	153.60	153.60	3.2
3870	(8+9)-I-1	-3426	153	1192	-7.03	17.98	14.57	132.00	192.00	192.00	5.9
3870	(8+9)-I-4	-2024	143	1325	-4.15	16.82	16.20	132.00	192.00	192.00	5.8
3870	(8+9)-III-1	-3448	154	1140	-7.07	18.05	13.94	132.00	192.00	192.00	6.0
3870	(8+9)-III-4	-2002	143	1377	-4.11	16.74	16.83	132.00	192.00	192.00	5.7

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Ty kg	τ_d kg/cmq	fvd kg/cmq	RS	Cs
0	(8+9)-V-1	-167	0.04	6.40	Si	>100
0	(8+9)-VIII-2	-124	0.03	6.40	Si	>100
0	(8+9)-VII-3	53	0.01	6.40	Si	>100
0	(8+9)-V-2	-187	0.05	6.40	Si	>100
0	(8+9)-V-3	56	0.01	6.40	Si	>100
0	(8+9)-VI-2	-132	0.03	6.40	Si	>100
0	(8+9)-VII-1	-169	0.04	6.40	Si	>100
0	(8+9)-VII-2	-184	0.05	6.40	Si	>100
504	1	-130	0.03	3.84	Si	>100
504	2	-269	0.07	5.76	Si	83
504	3	-269	0.07	5.76	Si	83
504	4	-130	0.03	5.12	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
504	5	-130	0.03	5.12	Si	>100
504	6	-130	0.03	5.12	Si	>100
504	7	-130	0.03	5.12	Si	>100
504	(8+9)-IV-4	-106	0.03	6.40	Si	>100
504	(8+9)-VI-4	-110	0.03	6.40	Si	>100
504	(8+9)-III-2	-113	0.03	6.40	Si	>100
504	(8+9)-I-4	-82	0.02	6.40	Si	>100
504	(8+9)-III-4	-79	0.02	6.40	Si	>100
504	(8+9)-I-3	-63	0.02	6.40	Si	>100
504	(8+9)-IV-2	-116	0.03	6.40	Si	>100
504	(8+9)-I-2	-115	0.03	6.40	Si	>100
504	(8+9)-III-1	-100	0.03	6.40	Si	>100
504	(8+9)-VII-4	-64	0.02	6.40	Si	>100
504	(8+9)-II-3	-54	0.01	6.40	Si	>100
504	(8+9)-VIII-1	-77	0.02	6.40	Si	>100
504	(8+9)-V-4	-67	0.02	6.40	Si	>100
504	(8+9)-I-1	-97	0.03	6.40	Si	>100
504	(8+9)-II-1	-64	0.02	6.40	Si	>100
504	(8+9)-VIII-3	-58	0.02	6.40	Si	>100
504	(8+9)-III-3	-66	0.02	6.40	Si	>100
504	(8+9)-VIII-4	-102	0.03	6.40	Si	>100
504	(8+9)-IV-3	-63	0.02	6.40	Si	>100
504	(8+9)-II-2	-125	0.03	6.40	Si	>100
504	(8+9)-VI-1	-69	0.02	6.40	Si	>100
504	(8+9)-VI-3	-49	0.01	6.40	Si	>100
504	(8+9)-IV-1	-73	0.02	6.40	Si	>100
504	(8+9)-II-4	-115	0.03	6.40	Si	>100
Verifiche nella direzione secondaria						
0	(8+9)-V-3	-9	0.02	6.40	Si	>100
0	(8+9)-VII-3	-8	0.01	6.40	Si	>100
1935	(8+9)-VII-4	3	0.01	6.40	Si	>100
1935	(8+9)-V-4	4	0.01	6.40	Si	>100
3870	1	169	0.32	3.84	Si	12
3870	2	352	0.67	5.76	Si	8.7
3870	3	352	0.67	5.76	Si	8.7
3870	4	169	0.32	5.12	Si	16
3870	5	169	0.32	5.12	Si	16
3870	6	169	0.32	5.12	Si	16
3870	7	169	0.32	5.12	Si	16
3870	(8+9)-VIII-4	76	0.14	6.40	Si	44
3870	(8+9)-IV-4	112	0.21	6.40	Si	30
3870	(8+9)-I-4	120	0.23	6.40	Si	28
3870	(8+9)-II-2	110	0.21	6.40	Si	31
3870	(8+9)-I-3	123	0.23	6.40	Si	27
3870	(8+9)-II-4	113	0.21	6.40	Si	30
3870	(8+9)-VI-1	157	0.30	6.40	Si	22
3870	(8+9)-III-2	110	0.21	6.40	Si	31
3870	(8+9)-VI-2	146	0.28	6.40	Si	23
3870	(8+9)-III-4	120	0.23	6.40	Si	28
3870	(8+9)-VI-3	87	0.17	6.40	Si	39
3870	(8+9)-IV-2	109	0.21	6.40	Si	31
3870	(8+9)-VI-4	77	0.15	6.40	Si	44
3870	(8+9)-II-1	120	0.23	6.40	Si	28
3870	(8+9)-VII-1	234	0.44	6.40	Si	14
3870	(8+9)-V-2	230	0.44	6.40	Si	15
3870	(8+9)-VII-2	230	0.44	6.40	Si	15
3870	(8+9)-III-1	113	0.21	6.40	Si	30
3870	(8+9)-I-2	110	0.21	6.40	Si	31
3870	(8+9)-IV-1	121	0.23	6.40	Si	28
3870	(8+9)-I-1	113	0.21	6.40	Si	30
3870	(8+9)-III-3	123	0.23	6.40	Si	27
3870	(8+9)-IV-3	124	0.23	6.40	Si	27
3870	(8+9)-II-3	124	0.23	6.40	Si	27
3870	(8+9)-VIII-1	157	0.30	6.40	Si	22

X	Comb.	Ty	τ_d	fvd	RS	Cs
3870	(8+9)-VIII-2	146	0.28	6.40	Si	23
3870	(8+9)-VIII-3	88	0.17	6.40	Si	38
3870	(8+9)-V-1	234	0.44	6.40	Si	14

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	(8+9)-IV-2	-9900	-5.29	32.00	6.1	-1.28	20.00	16	V	6.1
0	(8+9)-VIII-2	-10833	-5.78	32.00	5.5	-1.40	20.00	14	V	5.5
0	(8+9)-VII-1	-5816	-3.10	32.00	10	-0.75	20.00	27	V	10
0	(8+9)-I-1	-2223	-1.19	32.00	27	-0.29	20.00	70	V	27
0	(8+9)-III-2	-8010	-4.28	32.00	7.5	-1.03	20.00	19	V	7.5
0	(8+9)-III-1	-2707	-1.45	32.00	22	-0.35	20.00	57	V	22
0	(8+9)-V-2	-11603	-6.19	32.00	5.2	-1.50	20.00	13	V	5.2
0	(8+9)-V-1	-5332	-2.85	32.00	11	-0.69	20.00	29	V	11
0	(8+9)-I-2	-8494	-4.53	32.00	7.1	-1.10	20.00	18	V	7.1
0	(8+9)-VI-2	-12447	-6.65	32.00	4.8	-1.61	20.00	12	V	4.8
0	(8+9)-VII-2	-11119	-5.94	32.00	5.4	-1.44	20.00	14	V	5.4
504	1	2408	1.29	19.20	15	0.31	12.00	39	V	15
504	2	5036	2.69	28.80	11	0.65	18.00	28	V	11
504	3	5036	2.69	28.80	11	0.65	18.00	28	V	11
504	4	2408	1.29	25.60	20	0.31	16.00	51	V	20
504	5	2408	1.29	25.60	20	0.31	16.00	51	V	20
504	6	2408	1.29	25.60	20	0.31	16.00	51	V	20
504	7	2408	1.29	25.60	20	0.31	16.00	51	V	20
504	(8+9)-V-4	7150	3.82	32.00	8.4	0.92	20.00	22	V	8.4
504	(8+9)-VIII-1	8154	4.35	32.00	7.4	1.05	20.00	19	V	7.4
504	(8+9)-IV-1	8988	4.80	32.00	6.7	1.16	20.00	17	V	6.7
504	(8+9)-I-3	10850	5.79	32.00	5.5	1.40	20.00	14	V	5.5
504	(8+9)-IV-3	12558	6.70	32.00	4.8	1.62	20.00	12	V	4.8
504	(8+9)-VIII-3	13393	7.15	32.00	4.5	1.73	20.00	12	V	4.5
504	(8+9)-III-3	10343	5.52	32.00	5.8	1.34	20.00	15	V	5.8
504	(8+9)-VII-4	7656	4.09	32.00	7.8	0.99	20.00	20	V	7.8
504	(8+9)-III-4	4875	2.60	32.00	12	0.63	20.00	32	V	12
504	(8+9)-VI-1	9842	5.25	32.00	6.1	1.27	20.00	16	V	6.1
504	(8+9)-V-3	13631	7.28	32.00	4.4	1.76	20.00	11	V	4.4
504	(8+9)-VI-3	15081	8.05	32.00	4.0	1.95	20.00	10	V	4.0
504	(8+9)-II-3	14246	7.61	32.00	4.2	1.84	20.00	11	V	4.2
504	(8+9)-II-1	10677	5.70	32.00	5.6	1.38	20.00	14	V	5.6
504	(8+9)-I-4	4369	2.33	32.00	14	0.56	20.00	35	V	14
504	(8+9)-VII-3	13125	7.01	32.00	4.6	1.70	20.00	12	V	4.6
1007	(8+9)-VIII-4	-5531	-2.95	32.00	11	-0.71	20.00	28	V	11
1007	(8+9)-VI-4	-7221	-3.86	32.00	8.3	-0.93	20.00	21	V	8.3
1007	(8+9)-IV-4	-6238	-3.33	32.00	9.6	-0.81	20.00	25	V	9.6
1007	(8+9)-II-4	-7927	-4.23	32.00	7.6	-1.02	20.00	20	V	7.6
1007	(8+9)-II-2	-11552	-6.17	32.00	5.2	-1.49	20.00	13	V	5.2
Verifiche nella direzione secondaria										
0	(8+9)-V-1	1900	3.90	32.00	8.2	0.94	20.00	21	V	8.2
0	(8+9)-VII-3	-4682	-9.61	32.00	3.3	-2.32	20.00	8.6	V	3.3
0	(8+9)-VI-3	-5518	-11.32	32.00	2.8	-2.74	20.00	7.3	V	2.8
0	(8+9)-VIII-3	-4828	-9.91	32.00	3.2	-2.40	20.00	8.3	V	3.2
0	(8+9)-VI-2	5105	10.47	32.00	3.1	2.53	20.00	7.9	V	3.1
0	(8+9)-VII-2	4269	8.76	32.00	3.7	2.12	20.00	9.4	V	3.7
0	(8+9)-VII-1	2107	4.32	32.00	7.4	1.05	20.00	19	V	7.4
0	(8+9)-VIII-2	4415	9.06	32.00	3.5	2.19	20.00	9.1	V	3.5
0	(8+9)-VII-4	-2520	-5.17	32.00	6.2	-1.25	20.00	16	V	6.2
0	(8+9)-V-4	-2313	-4.75	32.00	6.7	-1.15	20.00	17	V	6.7
0	(8+9)-V-3	-4889	-10.03	32.00	3.2	-2.43	20.00	8.2	V	3.2
0	(8+9)-V-2	4475	9.18	32.00	3.5	2.22	20.00	9.0	V	3.5
1935	(8+9)-VIII-4	2402	4.93	32.00	6.5	1.19	20.00	17	V	6.5
1935	(8+9)-I-3	-3885	-7.97	32.00	4.0	-1.93	20.00	10	V	4.0
1935	(8+9)-II-3	-5222	-10.71	32.00	3.0	-2.59	20.00	7.7	V	3.0
1935	(8+9)-VI-1	-3502	-7.19	32.00	4.5	-1.74	20.00	12	V	4.5

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
1935	(8+9)-III-1	1098	2.25	32.00	14	0.55	20.00	37	V	14
1935	(8+9)-I-2	3472	7.12	32.00	4.5	1.72	20.00	12	V	4.5
1935	(8+9)-III-3	-3679	-7.55	32.00	4.2	-1.83	20.00	11	V	4.2
1935	(8+9)-I-1	892	1.83	32.00	17	0.44	20.00	45	V	17
1935	(8+9)-IV-1	-3102	-6.36	32.00	5.0	-1.54	20.00	13	V	5.0
1935	(8+9)-VI-4	3089	6.34	32.00	5.0	1.53	20.00	13	V	5.0
1935	(8+9)-IV-3	-4535	-9.30	32.00	3.4	-2.25	20.00	8.9	V	3.4
1935	(8+9)-II-2	4808	9.87	32.00	3.2	2.39	20.00	8.4	V	3.2
1935	(8+9)-II-1	-3788	-7.77	32.00	4.1	-1.88	20.00	11	V	4.1
1935	(8+9)-VIII-1	-2815	-5.78	32.00	5.5	-1.40	20.00	14	V	5.5
1935	(8+9)-II-4	3375	6.93	32.00	4.6	1.68	20.00	12	V	4.6
1935	(8+9)-III-2	3266	6.70	32.00	4.8	1.62	20.00	12	V	4.8
1935	(8+9)-IV-4	2689	5.52	32.00	5.8	1.34	20.00	15	V	5.8
1935	(8+9)-IV-2	4122	8.46	32.00	3.8	2.05	20.00	9.8	V	3.8
3870	1	-783	-1.61	19.20	12	-0.39	12.00	31	V	12
3870	2	-1688	-3.46	28.80	8.3	-0.84	18.00	21	V	8.3
3870	3	-1688	-3.46	28.80	8.3	-0.84	18.00	21	V	8.3
3870	4	-783	-1.61	25.60	16	-0.39	16.00	41	V	16
3870	5	-783	-1.61	25.60	16	-0.39	16.00	41	V	16
3870	6	-783	-1.61	25.60	16	-0.39	16.00	41	V	16
3870	7	-783	-1.61	25.60	16	-0.39	16.00	41	V	16
3870	(8+9)-III-4	-1626	-3.34	32.00	9.6	-0.81	20.00	25	V	9.6
3870	(8+9)-I-4	-1471	-3.02	32.00	11	-0.73	20.00	27	V	11

Setto 37: origine (1460.0,2062.0,193.5), direzione (-0.200098,0.979776,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_N	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	1	262	-218	-458	0.09	-2.92	-0.25	79.20	115.20	115.20	35
0	2	611	-454	-941	0.22	-6.06	-0.52	118.80	172.80	172.80	25
0	3	611	-454	-941	0.22	-6.06	-0.52	118.80	172.80	172.80	25
0	4	262	-218	-458	0.09	-2.92	-0.25	105.60	153.60	153.60	46
0	5	262	-218	-458	0.09	-2.92	-0.25	105.60	153.60	153.60	46
0	6	262	-218	-458	0.09	-2.92	-0.25	105.60	153.60	153.60	46
0	7	262	-218	-458	0.09	-2.92	-0.25	105.60	153.60	153.60	46
0	(8+9)-VIII-4	1520	-81	-2373	0.54	-1.08	-1.31	132.00	192.00	192.00	61
0	(8+9)-IV-1	-1601	-226	2794	-0.57	-3.02	1.54	132.00	192.00	192.00	42
0	(8+9)-V-1	2763	-130	-5863	0.98	-1.74	-3.24	132.00	192.00	192.00	30
0	(8+9)-I-2	3057	-89	-5379	1.09	-1.19	-2.97	132.00	192.00	192.00	33
0	(8+9)-V-2	4536	-70	-8923	1.61	-0.93	-4.92	132.00	192.00	192.00	23
0	(8+9)-I-4	-921	-151	1677	-0.33	-2.02	0.93	132.00	192.00	192.00	65
0	(8+9)-V-3	-4174	-231	8281	-1.49	-3.09	4.57	132.00	192.00	192.00	25
0	(8+9)-II-2	3734	-41	-6479	1.33	-0.54	-3.58	132.00	192.00	192.00	32
0	(8+9)-V-4	-2400	-171	5221	-0.85	-2.28	2.88	132.00	192.00	192.00	37
0	(8+9)-II-4	2540	-59	-4362	0.90	-0.79	-2.41	132.00	192.00	192.00	43
0	(8+9)-VI-1	-1734	-236	2657	-0.62	-3.15	1.47	132.00	192.00	192.00	42
0	(8+9)-III-2	2884	-94	-5101	1.03	-1.26	-2.81	132.00	192.00	192.00	35
0	(8+9)-VI-2	4177	-35	-7542	1.49	-0.47	-4.16	132.00	192.00	192.00	28
0	(8+9)-III-4	-1094	-156	1955	-0.39	-2.09	1.08	132.00	192.00	192.00	61
0	(8+9)-VI-3	-3815	-266	6900	-1.36	-3.56	3.81	132.00	192.00	192.00	26
0	(8+9)-IV-2	3157	-56	-5553	1.12	-0.75	-3.06	132.00	192.00	192.00	35
0	(8+9)-VI-4	2096	-65	-3299	0.75	-0.87	-1.82	132.00	192.00	192.00	51
0	(8+9)-IV-4	1964	-75	-3436	0.70	-1.00	-1.90	132.00	192.00	192.00	49
0	(8+9)-VII-1	2936	-126	-6141	1.04	-1.68	-3.39	132.00	192.00	192.00	29
0	(8+9)-II-1	-2178	-242	3720	-0.78	-3.23	2.05	132.00	192.00	192.00	36
0	(8+9)-VII-2	4363	-75	-8645	1.55	-1.00	-4.77	132.00	192.00	192.00	24
0	(8+9)-III-1	1456	-145	-2597	0.52	-1.94	-1.43	132.00	192.00	192.00	47
0	(8+9)-VII-3	-4001	-226	8003	-1.42	-3.03	4.42	132.00	192.00	192.00	26
0	(8+9)-I-1	1284	-150	-2319	0.46	-2.00	-1.28	132.00	192.00	192.00	49
0	(8+9)-VII-4	-2573	-175	5499	-0.92	-2.35	3.03	132.00	192.00	192.00	36
0	(8+9)-III-3	-2522	-207	4459	-0.90	-2.77	2.46	132.00	192.00	192.00	37
0	(8+9)-IV-3	-2795	-245	4911	-0.99	-3.27	2.71	132.00	192.00	192.00	32
0	(8+9)-II-3	-3371	-260	5837	-1.20	-3.48	3.22	132.00	192.00	192.00	29

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-VIII-1	-1158	-220	1731	-0.41	-2.95	0.95	132.00	192.00	192.00	49
0	(8+9)-VIII-2	3601	-50	-6616	1.28	-0.67	-3.65	132.00	192.00	192.00	31
0	(8+9)-VIII-3	-3239	-251	5974	-1.15	-3.35	3.30	132.00	192.00	192.00	29
0	(8+9)-I-3	-2695	-212	4737	-0.96	-2.83	2.61	132.00	192.00	192.00	35
Verifiche nella direzione secondaria											
0	(8+9)-VIII-4	5676	37	390	21.25	7.84	15.87	132.00	192.00	192.00	3.5
0	(8+9)-VII-2	2541	-221	1776	9.51	-47.41	72.24	132.00	192.00	192.00	1.4
0	(8+9)-III-3	-3748	76	-1981	-14.03	16.20	-80.61	132.00	192.00	192.00	2.0
0	(8+9)-IV-2	6307	-48	1358	23.61	-10.30	55.26	132.00	192.00	192.00	1.9
0	(8+9)-III-4	440	61	-1451	1.65	13.08	-59.05	132.00	192.00	192.00	2.6
0	(8+9)-VIII-2	6484	-90	1315	24.27	-19.34	53.50	132.00	192.00	192.00	1.8
0	(8+9)-VII-4	-152	202	-1307	-0.57	43.19	-53.17	132.00	192.00	192.00	2.0
0	(8+9)-VII-1	-1647	-207	1246	-6.17	-44.29	50.68	132.00	192.00	192.00	2.0
0	(8+9)-VII-3	-4340	216	-1837	-16.24	46.31	-74.73	132.00	192.00	192.00	1.6
0	(8+9)-I-1	-2551	-62	1332	-9.55	-13.35	54.17	132.00	192.00	192.00	2.8
0	(8+9)-I-3	-4060	80	-2040	-15.20	17.03	-83.00	132.00	192.00	192.00	1.9
0	(8+9)-IV-3	-8106	43	-1420	-30.34	9.21	-57.75	132.00	192.00	192.00	2.7
0	(8+9)-II-1	-8694	13	-604	-32.54	2.85	-24.55	132.00	192.00	192.00	5.8
0	(8+9)-IV-4	5854	-6	347	21.91	-1.19	14.11	132.00	192.00	192.00	4.1
0	(8+9)-II-3	-9147	56	-1615	-34.24	11.97	-65.70	132.00	192.00	192.00	2.3
0	(8+9)-V-1	-1959	-203	1187	-7.33	-43.46	48.30	132.00	192.00	192.00	2.1
0	(8+9)-III-1	-2239	-66	1390	-8.38	-14.18	56.56	132.00	192.00	192.00	2.7
0	(8+9)-V-2	2853	-225	1834	10.68	-48.23	74.63	132.00	192.00	192.00	1.4
0	(8+9)-VIII-3	-8283	85	-1376	-31.00	18.24	-55.99	132.00	192.00	192.00	2.4
0	(8+9)-V-3	-4652	220	-1896	-17.41	47.14	-77.12	132.00	192.00	192.00	1.5
0	(8+9)-I-2	2261	-85	1979	8.46	-18.12	80.50	132.00	192.00	192.00	1.7
0	(8+9)-V-4	160	198	-1248	0.60	42.37	-50.79	132.00	192.00	192.00	2.0
0	(8+9)-II-2	7348	-61	1554	27.50	-13.06	63.21	132.00	192.00	192.00	1.7
0	(8+9)-VI-1	-8517	-29	-647	-31.88	-6.18	-26.32	132.00	192.00	192.00	5.1
0	(8+9)-III-2	1949	-81	1920	7.29	-17.30	78.12	132.00	192.00	192.00	1.8
0	(8+9)-I-4	752	57	-1393	2.82	12.26	-56.67	132.00	192.00	192.00	2.6
0	(8+9)-II-4	6895	-18	542	25.81	-3.94	22.06	132.00	192.00	192.00	3.0
0	(8+9)-VIII-1	-7475	-42	-451	-27.98	-8.94	-18.37	132.00	192.00	192.00	6.1
0	(8+9)-VI-2	7525	-103	1510	28.17	-22.09	61.45	132.00	192.00	192.00	1.5
0	(8+9)-VI-3	-9324	98	-1572	-34.90	21.00	-63.94	132.00	192.00	192.00	2.1
0	(8+9)-VI-4	6717	24	586	25.14	5.09	23.82	132.00	192.00	192.00	2.9
1935	(8+9)-IV-1	2590	-11	134	9.69	-2.42	5.43	132.00	192.00	192.00	8.7
3870	1	-167	54	-34	-0.62	11.50	-1.40	79.20	115.20	115.20	8.9
3870	2	-362	112	-69	-1.36	24.04	-2.82	118.80	172.80	172.80	6.4
3870	3	-362	112	-69	-1.36	24.04	-2.82	118.80	172.80	172.80	6.4
3870	4	-167	54	-34	-0.62	11.50	-1.40	105.60	153.60	153.60	12
3870	5	-167	54	-34	-0.62	11.50	-1.40	105.60	153.60	153.60	12
3870	6	-167	54	-34	-0.62	11.50	-1.40	105.60	153.60	153.60	12
3870	7	-167	54	-34	-0.62	11.50	-1.40	105.60	153.60	153.60	12

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Ty kg	τ_d kg/cm ²	fvd kg/cm ²	RS	Cs
0	(8+9)-V-1	567	0.15	6.40	Si	44
0	(8+9)-II-2	129	0.03	6.40	Si	>100
0	(8+9)-VI-1	390	0.10	6.40	Si	63
0	(8+9)-I-3	365	0.09	6.40	Si	68
0	(8+9)-VII-1	565	0.15	6.40	Si	44
0	(8+9)-I-4	326	0.08	6.40	Si	76
0	(8+9)-V-2	528	0.14	6.40	Si	47
0	(8+9)-VII-2	531	0.14	6.40	Si	47
0	(8+9)-III-4	328	0.08	6.40	Si	75
0	(8+9)-III-3	362	0.09	6.40	Si	68
0	(8+9)-IV-2	138	0.04	6.40	Si	>100
0	(8+9)-VIII-2	268	0.07	6.40	Si	92
0	(8+9)-IV-4	207	0.05	6.40	Si	>100
0	(8+9)-VIII-1	381	0.10	6.40	Si	65
0	(8+9)-II-4	198	0.05	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
0	(8+9)-VI-2	259	0.07	6.40	Si	95
276	1	332	0.09	3.84	Si	45
276	2	690	0.18	5.76	Si	32
276	3	690	0.18	5.76	Si	32
276	4	332	0.09	5.12	Si	60
276	5	332	0.09	5.12	Si	60
276	6	332	0.09	5.12	Si	60
276	7	332	0.09	5.12	Si	60
276	(8+9)-IV-1	304	0.08	6.40	Si	81
276	(8+9)-II-3	338	0.09	6.40	Si	73
276	(8+9)-IV-3	325	0.08	6.40	Si	76
276	(8+9)-II-1	317	0.08	6.40	Si	78
276	(8+9)-III-2	168	0.04	6.40	Si	>100
276	(8+9)-III-1	219	0.06	6.40	Si	>100
276	(8+9)-I-1	223	0.06	6.40	Si	>100
276	(8+9)-I-2	164	0.04	6.40	Si	>100
552	(8+9)-VIII-4	159	0.04	6.40	Si	>100
552	(8+9)-V-3	313	0.08	6.40	Si	79
552	(8+9)-VII-3	308	0.08	6.40	Si	80
552	(8+9)-VII-4	261	0.07	6.40	Si	95
552	(8+9)-VI-4	142	0.04	6.40	Si	>100
552	(8+9)-VI-3	331	0.09	6.40	Si	75
552	(8+9)-VIII-3	314	0.08	6.40	Si	79
552	(8+9)-V-4	256	0.07	6.40	Si	96
Verifiche nella direzione secondaria						
0	(8+9)-VIII-4	64	0.22	6.40	Si	29
0	(8+9)-V-2	169	0.58	6.40	Si	11
0	(8+9)-II-3	-131	0.45	6.40	Si	14
0	(8+9)-IV-2	123	0.42	6.40	Si	15
0	(8+9)-II-4	104	0.36	6.40	Si	18
0	(8+9)-VIII-2	139	0.48	6.40	Si	13
0	(8+9)-VI-3	-147	0.51	6.40	Si	13
0	(8+9)-VII-3	-145	0.50	6.40	Si	13
0	(8+9)-III-2	108	0.37	6.40	Si	17
0	(8+9)-VI-4	88	0.30	6.40	Si	21
0	(8+9)-III-3	-92	0.32	6.40	Si	20
0	(8+9)-I-3	-99	0.34	6.40	Si	19
0	(8+9)-III-4	-36	0.12	6.40	Si	52
0	(8+9)-II-1	-88	0.30	6.40	Si	21
0	(8+9)-VI-2	163	0.56	6.40	Si	11
0	(8+9)-VIII-3	-123	0.42	6.40	Si	15
0	(8+9)-VII-2	161	0.56	6.40	Si	11
0	(8+9)-I-4	-28	0.10	6.40	Si	65
0	(8+9)-II-2	147	0.51	6.40	Si	13
0	(8+9)-VII-4	-89	0.31	6.40	Si	21
0	(8+9)-I-2	115	0.40	6.40	Si	16
0	(8+9)-IV-3	-107	0.37	6.40	Si	17
0	(8+9)-IV-4	80	0.28	6.40	Si	23
0	(8+9)-V-3	-152	0.53	6.40	Si	12
3870	1	62	0.21	3.84	Si	18
3870	2	131	0.45	5.76	Si	13
3870	3	131	0.45	5.76	Si	13
3870	4	62	0.21	5.12	Si	24
3870	5	62	0.21	5.12	Si	24
3870	6	62	0.21	5.12	Si	24
3870	7	62	0.21	5.12	Si	24
3870	(8+9)-VII-1	172	0.60	6.40	Si	11
3870	(8+9)-I-1	68	0.23	6.40	Si	27
3870	(8+9)-III-1	69	0.24	6.40	Si	27
3870	(8+9)-IV-1	70	0.24	6.40	Si	26
3870	(8+9)-VIII-1	101	0.35	6.40	Si	18
3870	(8+9)-VI-1	96	0.33	6.40	Si	19
3870	(8+9)-V-4	-85	0.30	6.40	Si	22
3870	(8+9)-V-1	171	0.59	6.40	Si	11

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Tx kg	τ_{vd} kg/cmq	fvd kg/cmq	Csv	τ_M kg/cmq	fTd kg/cmq	Csm	Mecc.	Cs
0	(8+9)-IV-1	8456	4.51	32.00	7.1	1.09	20.00	18	V	7.1
0	(8+9)-VI-4	-10101	-5.39	32.00	5.9	-1.31	20.00	15	V	5.9
0	(8+9)-VIII-4	-8450	-4.51	32.00	7.1	-1.09	20.00	18	V	7.1
0	(8+9)-II-1	10107	5.40	32.00	5.9	1.31	20.00	15	V	5.9
0	(8+9)-IV-4	-8610	-4.60	32.00	7.0	-1.11	20.00	18	V	7.0
0	(8+9)-VI-1	9947	5.31	32.00	6.0	1.29	20.00	16	V	6.0
0	(8+9)-II-4	-10260	-5.48	32.00	5.8	-1.33	20.00	15	V	5.8
0	(8+9)-VIII-1	8297	4.43	32.00	7.2	1.07	20.00	19	V	7.2
276	(8+9)-II-2	-12849	-6.86	32.00	4.7	-1.66	20.00	12	V	4.7
276	(8+9)-IV-2	-11195	-5.98	32.00	5.4	-1.45	20.00	14	V	5.4
276	(8+9)-VI-2	-12126	-6.47	32.00	4.9	-1.57	20.00	13	V	4.9
276	(8+9)-VIII-2	-10472	-5.59	32.00	5.7	-1.35	20.00	15	V	5.7
552	1	156	0.08	19.20	>100	0.02	12.00	>100	V	>100
552	2	439	0.23	28.80	>100	0.06	18.00	>100	V	>100
552	3	439	0.23	28.80	>100	0.06	18.00	>100	V	>100
552	4	156	0.08	25.60	>100	0.02	16.00	>100	V	>100
552	5	156	0.08	25.60	>100	0.02	16.00	>100	V	>100
552	6	156	0.08	25.60	>100	0.02	16.00	>100	V	>100
552	7	156	0.08	25.60	>100	0.02	16.00	>100	V	>100
552	(8+9)-VI-3	12296	6.56	32.00	4.9	1.59	20.00	13	V	4.9
552	(8+9)-I-1	-4083	-2.18	32.00	15	-0.53	20.00	38	V	15
552	(8+9)-II-3	12871	6.87	32.00	4.7	1.66	20.00	12	V	4.7
552	(8+9)-III-4	4777	2.55	32.00	13	0.62	20.00	32	V	13
552	(8+9)-I-4	4284	2.29	32.00	14	0.55	20.00	36	V	14
552	(8+9)-III-3	10131	5.41	32.00	5.9	1.31	20.00	15	V	5.9
552	(8+9)-VII-1	-2660	-1.42	32.00	23	-0.34	20.00	58	V	23
552	(8+9)-V-2	-8507	-4.54	32.00	7.0	-1.10	20.00	18	V	7.0
552	(8+9)-VII-2	-8014	-4.28	32.00	7.5	-1.04	20.00	19	V	7.5
552	(8+9)-V-4	2369	1.26	32.00	25	0.31	20.00	65	V	25
552	(8+9)-VII-3	8215	4.39	32.00	7.3	1.06	20.00	19	V	7.3
552	(8+9)-III-1	-4576	-2.44	32.00	13	-0.59	20.00	34	V	13
552	(8+9)-VII-4	2861	1.53	32.00	21	0.37	20.00	54	V	21
552	(8+9)-III-2	-9930	-5.30	32.00	6.0	-1.28	20.00	16	V	6.0
552	(8+9)-IV-3	11230	6.00	32.00	5.3	1.45	20.00	14	V	5.3
552	(8+9)-V-3	8707	4.65	32.00	6.9	1.12	20.00	18	V	6.9
552	(8+9)-I-3	10623	5.67	32.00	5.6	1.37	20.00	15	V	5.6
552	(8+9)-I-2	-10422	-5.56	32.00	5.8	-1.35	20.00	15	V	5.8
552	(8+9)-VIII-3	10655	5.69	32.00	5.6	1.38	20.00	15	V	5.6
552	(8+9)-V-1	-2168	-1.16	32.00	28	-0.28	20.00	71	V	28
Verifiche nella direzione secondaria										
0	(8+9)-III-4	-866	-3.24	32.00	9.9	-0.78	20.00	26	V	9.9
0	(8+9)-I-4	-751	-2.81	32.00	11	-0.68	20.00	29	V	11
0	(8+9)-VIII-3	-2623	-9.82	32.00	3.3	-2.38	20.00	8.4	V	3.3
0	(8+9)-V-3	-2710	-10.14	32.00	3.2	-2.45	20.00	8.1	V	3.2
0	(8+9)-VII-3	-2595	-9.71	32.00	3.3	-2.35	20.00	8.5	V	3.3
0	(8+9)-V-2	2647	9.91	32.00	3.2	2.40	20.00	8.3	V	3.2
0	(8+9)-VII-1	1331	4.98	32.00	6.4	1.21	20.00	17	V	6.4
0	(8+9)-II-3	-2847	-10.66	32.00	3.0	-2.58	20.00	7.8	V	3.0
0	(8+9)-I-1	688	2.57	32.00	12	0.62	20.00	32	V	12
0	(8+9)-V-1	1216	4.55	32.00	7.0	1.10	20.00	18	V	7.0
0	(8+9)-I-3	-2182	-8.17	32.00	3.9	-1.98	20.00	10	V	3.9
0	(8+9)-VII-2	2532	9.48	32.00	3.4	2.29	20.00	8.7	V	3.4
0	(8+9)-VI-3	-3006	-11.25	32.00	2.8	-2.72	20.00	7.3	V	2.8
0	(8+9)-V-4	-1279	-4.79	32.00	6.7	-1.16	20.00	17	V	6.7
0	(8+9)-VII-4	-1394	-5.22	32.00	6.1	-1.26	20.00	16	V	6.1
0	(8+9)-III-1	802	3.00	32.00	11	0.73	20.00	28	V	11
0	(8+9)-IV-3	-2465	-9.23	32.00	3.5	-2.23	20.00	9.0	V	3.5
0	(8+9)-III-3	-2067	-7.74	32.00	4.1	-1.87	20.00	11	V	4.1
1935	(8+9)-VIII-4	1527	5.72	32.00	5.6	1.38	20.00	14	V	5.6
1935	(8+9)-VIII-1	-1461	-5.47	32.00	5.9	-1.32	20.00	15	V	5.9

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
1935	(8+9)-I-2	2126	7.96	32.00	4.0	1.93	20.00	10	V	4.0
1935	(8+9)-IV-1	-1616	-6.05	32.00	5.3	-1.46	20.00	14	V	5.3
1935	(8+9)-VI-1	-1840	-6.89	32.00	4.6	-1.67	20.00	12	V	4.6
1935	(8+9)-III-2	2012	7.53	32.00	4.2	1.82	20.00	11	V	4.2
1935	(8+9)-VI-2	3032	11.35	32.00	2.8	2.75	20.00	7.3	V	2.8
1935	(8+9)-II-1	-1995	-7.47	32.00	4.3	-1.81	20.00	11	V	4.3
1935	(8+9)-IV-2	2499	9.35	32.00	3.4	2.26	20.00	8.8	V	3.4
1935	(8+9)-IV-4	1682	6.30	32.00	5.1	1.52	20.00	13	V	5.1
1935	(8+9)-II-2	2877	10.77	32.00	3.0	2.61	20.00	7.7	V	3.0
1935	(8+9)-II-4	2060	7.71	32.00	4.1	1.87	20.00	11	V	4.1
1935	(8+9)-VI-4	1905	7.13	32.00	4.5	1.73	20.00	12	V	4.5
1935	(8+9)-VIII-2	2654	9.93	32.00	3.2	2.40	20.00	8.3	V	3.2
3870	1	92	0.35	19.20	56	0.08	12.00	>100	V	56
3870	2	156	0.58	28.80	49	0.14	18.00	>100	V	49
3870	3	156	0.58	28.80	49	0.14	18.00	>100	V	49
3870	4	92	0.35	25.60	74	0.08	16.00	>100	V	74
3870	5	92	0.35	25.60	74	0.08	16.00	>100	V	74
3870	6	92	0.35	25.60	74	0.08	16.00	>100	V	74
3870	7	92	0.35	25.60	74	0.08	16.00	>100	V	74

Setto 38: origine (1408.8,2312.7,303.5), direzione (-0.200098,0.979776,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	1	273	49	177	0.23	1.51	0.52	79.20	115.20	115.20	49
0	2	543	101	379	0.45	3.13	1.12	118.80	172.80	172.80	35
0	3	543	101	379	0.45	3.13	1.12	118.80	172.80	172.80	35
0	4	273	49	177	0.23	1.51	0.52	105.60	153.60	153.60	65
0	5	273	49	177	0.23	1.51	0.52	105.60	153.60	153.60	65
0	6	273	49	177	0.23	1.51	0.52	105.60	153.60	153.60	65
0	7	273	49	177	0.23	1.51	0.52	105.60	153.60	153.60	65
1200	(8+9)-VIII-4	4771	-20	2278	3.94	-0.62	6.75	132.00	192.00	192.00	15
1200	(8+9)-IV-1	-5415	12	-2640	-4.47	0.38	-7.82	132.00	192.00	192.00	23
1200	(8+9)-V-1	3778	-29	1810	3.12	-0.91	5.36	132.00	192.00	192.00	18
1200	(8+9)-I-2	6777	-35	3250	5.59	-1.09	9.63	132.00	192.00	192.00	10
1200	(8+9)-V-2	8571	-47	4128	7.07	-1.45	12.23	132.00	192.00	192.00	8.0
1200	(8+9)-I-4	-2090	6	-1032	-1.72	0.19	-3.06	132.00	192.00	192.00	59
1200	(8+9)-V-3	-8676	35	-4227	-7.16	1.10	-12.53	132.00	192.00	192.00	14
1200	(8+9)-II-2	9265	-41	4455	7.64	-1.27	13.20	132.00	192.00	192.00	7.5
1200	(8+9)-V-4	-3884	18	-1910	-3.20	0.56	-5.66	132.00	192.00	192.00	31
1200	(8+9)-II-4	6605	-29	3170	5.45	-0.89	9.39	132.00	192.00	192.00	11
1200	(8+9)-VI-1	-6172	14	-3006	-5.09	0.43	-8.91	132.00	192.00	192.00	20
1200	(8+9)-III-2	6388	-34	3061	5.27	-1.04	9.07	132.00	192.00	192.00	11
1200	(8+9)-VI-2	9803	-45	4718	8.09	-1.38	13.98	132.00	192.00	192.00	7.1
1200	(8+9)-III-4	-2479	8	-1221	-2.04	0.24	-3.62	132.00	192.00	192.00	49
1200	(8+9)-VI-3	-9909	33	-4818	-8.17	1.03	-14.28	132.00	192.00	192.00	12
1200	(8+9)-IV-2	7969	-36	3825	6.57	-1.12	11.34	132.00	192.00	192.00	8.7
1200	(8+9)-VI-4	6067	-25	2907	5.00	-0.78	8.61	132.00	192.00	192.00	12
1200	(8+9)-IV-4	5309	-24	2541	4.38	-0.73	7.53	132.00	192.00	192.00	13
1200	(8+9)-VII-1	4167	-31	1999	3.44	-0.96	5.92	132.00	192.00	192.00	16
1200	(8+9)-II-1	-6711	17	-3270	-5.53	0.54	-9.69	132.00	192.00	192.00	18
1200	(8+9)-VII-2	8182	-45	3939	6.75	-1.40	11.67	132.00	192.00	192.00	8.4
1200	(8+9)-III-1	2373	-19	1122	1.96	-0.59	3.32	132.00	192.00	192.00	28
1200	(8+9)-VII-3	-8288	34	-4038	-6.84	1.05	-11.97	132.00	192.00	192.00	14
1200	(8+9)-I-1	1984	-18	933	1.64	-0.55	2.76	132.00	192.00	192.00	34
1200	(8+9)-VII-4	-4272	19	-2099	-3.52	0.60	-6.22	132.00	192.00	192.00	28
1200	(8+9)-III-3	-6494	22	-3161	-5.36	0.69	-9.37	132.00	192.00	192.00	19
1200	(8+9)-IV-3	-8075	25	-3925	-6.66	0.77	-11.63	132.00	192.00	192.00	15
1200	(8+9)-II-3	-9371	30	-4554	-7.73	0.92	-13.50	132.00	192.00	192.00	13
1200	(8+9)-VIII-1	-4877	9	-2377	-4.02	0.27	-7.04	132.00	192.00	192.00	26
1200	(8+9)-VIII-2	8508	-40	4089	7.02	-1.23	12.12	132.00	192.00	192.00	8.2
1200	(8+9)-VIII-3	-8613	28	-4188	-7.10	0.87	-12.41	132.00	192.00	192.00	14
1200	(8+9)-I-3	-6882	24	-3349	-5.68	0.74	-9.93	132.00	192.00	192.00	18

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
Verifiche nella direzione secondaria											
0	1	-1441	26	241	-2.48	2.55	2.08	79.20	115.20	115.20	25
0	4	-1441	26	241	-2.48	2.55	2.08	105.60	153.60	153.60	33
0	5	-1441	26	241	-2.48	2.55	2.08	105.60	153.60	153.60	33
0	6	-1441	26	241	-2.48	2.55	2.08	105.60	153.60	153.60	33
0	7	-1441	26	241	-2.48	2.55	2.08	105.60	153.60	153.60	33
0	(8+9)-VIII-4	-1542	22	3614	-2.65	2.18	31.11	132.00	192.00	192.00	5.8
0	(8+9)-IV-2	-1938	26	5914	-3.34	2.53	50.91	132.00	192.00	192.00	3.6
0	(8+9)-V-1	-1514	23	2951	-2.61	2.24	25.40	132.00	192.00	192.00	6.9
0	(8+9)-I-1	-1233	20	1627	-2.12	1.94	14.01	132.00	192.00	192.00	12
0	(8+9)-V-2	-2102	28	6385	-3.62	2.74	54.96	132.00	192.00	192.00	3.3
0	(8+9)-I-3	-193	11	-4716	-0.33	1.09	-40.60	132.00	192.00	192.00	4.6
0	(8+9)-V-3	87	8	-6039	0.15	0.79	-51.99	132.00	192.00	192.00	3.6
0	(8+9)-II-1	-183	11	-4599	-0.32	1.07	-39.59	132.00	192.00	192.00	4.7
0	(8+9)-V-4	-501	13	-2605	-0.86	1.28	-22.43	132.00	192.00	192.00	8.1
0	(8+9)-II-3	129	8	-6502	0.22	0.81	-55.97	132.00	192.00	192.00	3.4
0	(8+9)-VI-1	-267	12	-4202	-0.46	1.15	-36.17	132.00	192.00	192.00	5.1
0	(8+9)-III-1	-1295	20	1908	-2.23	2.00	16.42	132.00	192.00	192.00	10
0	(8+9)-VI-2	-2227	28	7244	-3.84	2.80	62.37	132.00	192.00	192.00	2.9
0	(8+9)-III-3	-255	12	-4436	-0.44	1.14	-38.19	132.00	192.00	192.00	4.9
0	(8+9)-VI-3	213	7	-6899	0.37	0.72	-59.39	132.00	192.00	192.00	3.2
0	(8+9)-IV-1	-388	13	-3665	-0.67	1.25	-31.55	132.00	192.00	192.00	5.9
0	(8+9)-VI-4	-1747	24	4548	-3.01	2.37	39.15	132.00	192.00	192.00	4.6
0	(8+9)-IV-3	-77	10	-5568	-0.13	0.99	-47.93	132.00	192.00	192.00	3.9
0	(8+9)-VII-1	-1575	23	3231	-2.71	2.30	27.81	132.00	192.00	192.00	6.4
0	(8+9)-I-2	-1821	25	5061	-3.14	2.44	43.57	132.00	192.00	192.00	4.2
0	(8+9)-VII-2	-2040	27	6104	-3.51	2.68	52.55	132.00	192.00	192.00	3.5
0	(8+9)-II-2	-2143	28	6848	-3.69	2.71	58.95	132.00	192.00	192.00	3.1
0	(8+9)-VII-3	26	9	-5759	0.04	0.84	-49.58	132.00	192.00	192.00	3.8
0	(8+9)-III-2	-1759	24	4781	-3.03	2.38	41.16	132.00	192.00	192.00	4.4
0	(8+9)-VIII-3	8	9	-5965	0.01	0.90	-51.35	132.00	192.00	192.00	3.7
0	(8+9)-III-4	-720	15	-1562	-1.24	1.53	-13.45	132.00	192.00	192.00	13
0	(8+9)-I-4	-781	16	-1282	-1.35	1.58	-11.04	132.00	192.00	192.00	15
0	(8+9)-II-4	-1831	25	4945	-3.15	2.46	42.57	132.00	192.00	192.00	4.3
0	(8+9)-IV-4	-1626	23	4011	-2.80	2.27	34.53	132.00	192.00	192.00	5.2
0	(8+9)-VII-4	-439	12	-2885	-0.76	1.23	-24.84	132.00	192.00	192.00	7.4
0	(8+9)-VIII-1	-473	14	-3268	-0.81	1.34	-28.13	132.00	192.00	192.00	6.5
0	(8+9)-VIII-2	-2022	27	6311	-3.48	2.62	54.33	132.00	192.00	192.00	3.4
835	2	-1072	87	-84	-1.85	8.60	-0.72	118.80	172.80	172.80	19
835	3	-1072	87	-84	-1.85	8.60	-0.72	118.80	172.80	172.80	19

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
0	1	-66	0.04	3.84	Si	97
0	2	-137	0.08	5.76	Si	70
0	3	-137	0.08	5.76	Si	70
0	4	-66	0.04	5.12	Si	>100
0	5	-66	0.04	5.12	Si	>100
0	6	-66	0.04	5.12	Si	>100
0	7	-66	0.04	5.12	Si	>100
0	(8+9)-VIII-4	-50	0.03	6.40	Si	>100
0	(8+9)-IV-1	-39	0.02	6.40	Si	>100
0	(8+9)-V-1	-54	0.03	6.40	Si	>100
0	(8+9)-I-2	-55	0.03	6.40	Si	>100
0	(8+9)-V-2	-61	0.04	6.40	Si	>100
0	(8+9)-I-4	-43	0.03	6.40	Si	>100
0	(8+9)-V-3	-30	0.02	6.40	Si	>100
0	(8+9)-II-2	-59	0.04	6.40	Si	>100
0	(8+9)-V-4	-37	0.02	6.40	Si	>100
0	(8+9)-II-4	-55	0.03	6.40	Si	>100
0	(8+9)-VI-1	-38	0.02	6.40	Si	>100
0	(8+9)-III-2	-54	0.03	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
0	(8+9)-VI-2	-61	0.04	6.40	Si	>100
0	(8+9)-III-4	-42	0.03	6.40	Si	>100
0	(8+9)-VI-3	-30	0.02	6.40	Si	>100
0	(8+9)-IV-2	-56	0.03	6.40	Si	>100
0	(8+9)-VI-4	-53	0.03	6.40	Si	>100
0	(8+9)-IV-4	-52	0.03	6.40	Si	>100
0	(8+9)-VII-1	-55	0.03	6.40	Si	>100
0	(8+9)-II-1	-36	0.02	6.40	Si	>100
0	(8+9)-VII-2	-60	0.04	6.40	Si	>100
0	(8+9)-III-1	-49	0.03	6.40	Si	>100
0	(8+9)-VII-3	-31	0.02	6.40	Si	>100
0	(8+9)-I-1	-48	0.03	6.40	Si	>100
0	(8+9)-VII-4	-36	0.02	6.40	Si	>100
0	(8+9)-III-3	-37	0.02	6.40	Si	>100
0	(8+9)-IV-3	-35	0.02	6.40	Si	>100
0	(8+9)-II-3	-32	0.02	6.40	Si	>100
0	(8+9)-VIII-1	-41	0.02	6.40	Si	>100
0	(8+9)-VIII-2	-57	0.03	6.40	Si	>100
0	(8+9)-VIII-3	-34	0.02	6.40	Si	>100
0	(8+9)-I-3	-36	0.02	6.40	Si	>100
Verifiche nella direzione secondaria						
0	1	41	0.07	3.84	Si	59
0	2	85	0.14	5.76	Si	42
0	3	85	0.14	5.76	Si	42
0	4	41	0.07	5.12	Si	79
0	5	41	0.07	5.12	Si	79
0	6	41	0.07	5.12	Si	79
0	7	41	0.07	5.12	Si	79
0	(8+9)-IV-2	41	0.06	6.40	Si	99
0	(8+9)-V-1	65	0.10	6.40	Si	62
0	(8+9)-I-2	40	0.06	6.40	Si	>100
0	(8+9)-V-2	74	0.12	6.40	Si	54
0	(8+9)-I-4	26	0.04	6.40	Si	>100
0	(8+9)-VI-1	25	0.04	6.40	Si	>100
0	(8+9)-VII-2	73	0.12	6.40	Si	55
0	(8+9)-II-2	46	0.07	6.40	Si	88
0	(8+9)-I-1	31	0.05	6.40	Si	>100
0	(8+9)-II-4	42	0.07	6.40	Si	97
0	(8+9)-VII-1	66	0.11	6.40	Si	61
0	(8+9)-III-2	38	0.06	6.40	Si	>100
0	(8+9)-IV-4	37	0.06	6.40	Si	>100
0	(8+9)-III-1	32	0.05	6.40	Si	>100
0	(8+9)-VIII-1	30	0.05	6.40	Si	>100
0	(8+9)-VIII-2	51	0.08	6.40	Si	79
0	(8+9)-VI-4	31	0.05	6.40	Si	>100
0	(8+9)-VI-2	56	0.09	6.40	Si	72
0	(8+9)-III-4	24	0.04	6.40	Si	>100
1670	(8+9)-VIII-4	-29	0.05	6.40	Si	>100
1670	(8+9)-V-3	-19	0.03	6.40	Si	>100
1670	(8+9)-VII-3	-19	0.03	6.40	Si	>100
1670	(8+9)-V-4	-22	0.04	6.40	Si	>100
1670	(8+9)-VII-4	-22	0.03	6.40	Si	>100
1670	(8+9)-IV-3	-21	0.03	6.40	Si	>100
1670	(8+9)-IV-1	-22	0.04	6.40	Si	>100
1670	(8+9)-II-1	-21	0.03	6.40	Si	>100
1670	(8+9)-I-3	-21	0.03	6.40	Si	>100
1670	(8+9)-III-3	-22	0.03	6.40	Si	>100
1670	(8+9)-II-3	-19	0.03	6.40	Si	>100
1670	(8+9)-VIII-3	-20	0.03	6.40	Si	>100
1670	(8+9)-VI-3	-18	0.03	6.40	Si	>100

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	(8+9)-III-2	-4438	-5.49	32.00	5.8	-1.33	20.00	15	V	5.8
0	(8+9)-I-2	-4720	-5.84	32.00	5.5	-1.41	20.00	14	V	5.5
0	(8+9)-VIII-4	-3359	-4.16	32.00	7.7	-1.01	20.00	20	V	7.7
0	(8+9)-V-1	-2553	-3.16	32.00	10	-0.76	20.00	26	V	10
0	(8+9)-VII-2	-5762	-7.13	32.00	4.5	-1.73	20.00	12	V	4.5
0	(8+9)-IV-4	-3756	-4.65	32.00	6.9	-1.12	20.00	18	V	6.9
0	(8+9)-VI-4	-4297	-5.32	32.00	6.0	-1.29	20.00	16	V	6.0
0	(8+9)-IV-2	-5647	-6.99	32.00	4.6	-1.69	20.00	12	V	4.6
0	(8+9)-V-2	-6044	-7.48	32.00	4.3	-1.81	20.00	11	V	4.3
0	(8+9)-II-2	-6586	-8.15	32.00	3.9	-1.97	20.00	10	V	3.9
0	(8+9)-VI-2	-6983	-8.64	32.00	3.7	-2.09	20.00	9.6	V	3.7
0	(8+9)-I-1	-1229	-1.52	32.00	21	-0.37	20.00	54	V	21
0	(8+9)-VII-1	-2834	-3.51	32.00	9.1	-0.85	20.00	24	V	9.1
0	(8+9)-VIII-2	-6045	-7.48	32.00	4.3	-1.81	20.00	11	V	4.3
0	(8+9)-II-4	-4694	-5.81	32.00	5.5	-1.41	20.00	14	V	5.5
0	(8+9)-III-1	-1510	-1.87	32.00	17	-0.45	20.00	44	V	17
1200	1	681	0.84	19.20	23	0.20	12.00	59	V	23
1200	2	1430	1.77	28.80	16	0.43	18.00	42	V	16
1200	3	1430	1.77	28.80	16	0.43	18.00	42	V	16
1200	4	681	0.84	25.60	30	0.20	16.00	79	V	30
1200	5	681	0.84	25.60	30	0.20	16.00	79	V	30
1200	6	681	0.84	25.60	30	0.20	16.00	79	V	30
1200	7	681	0.84	25.60	30	0.20	16.00	79	V	30
1200	(8+9)-IV-1	4474	5.53	32.00	5.8	1.34	20.00	15	V	5.8
1200	(8+9)-III-3	5267	6.52	32.00	4.9	1.58	20.00	13	V	4.9
1200	(8+9)-II-1	5433	6.72	32.00	4.8	1.63	20.00	12	V	4.8
1200	(8+9)-I-3	5555	6.87	32.00	4.7	1.66	20.00	12	V	4.7
1200	(8+9)-II-3	7412	9.17	32.00	3.5	2.22	20.00	9.0	V	3.5
1200	(8+9)-V-4	3339	4.13	32.00	7.7	1.00	20.00	20	V	7.7
1200	(8+9)-VII-3	6623	8.19	32.00	3.9	1.98	20.00	10	V	3.9
1200	(8+9)-I-4	1983	2.45	32.00	13	0.59	20.00	34	V	13
1200	(8+9)-VII-4	3626	4.49	32.00	7.1	1.09	20.00	18	V	7.1
1200	(8+9)-VI-1	5026	6.22	32.00	5.1	1.50	20.00	13	V	5.1
1200	(8+9)-VI-3	7819	9.67	32.00	3.3	2.34	20.00	8.5	V	3.3
1200	(8+9)-V-3	6910	8.55	32.00	3.7	2.07	20.00	9.7	V	3.7
1200	(8+9)-VIII-1	4067	5.03	32.00	6.4	1.22	20.00	16	V	6.4
1200	(8+9)-III-4	2271	2.81	32.00	11	0.68	20.00	29	V	11
1200	(8+9)-VIII-3	6860	8.49	32.00	3.8	2.05	20.00	9.7	V	3.8
1200	(8+9)-IV-3	6454	7.98	32.00	4.0	1.93	20.00	10	V	4.0
Verifiche nella direzione secondaria										
0	(8+9)-VIII-4	3348	5.76	32.00	5.6	1.39	20.00	14	V	5.6
0	(8+9)-VII-2	5698	9.81	32.00	3.3	2.37	20.00	8.4	V	3.3
0	(8+9)-III-3	-4890	-8.42	32.00	3.8	-2.04	20.00	9.8	V	3.8
0	(8+9)-IV-2	5646	9.72	32.00	3.3	2.35	20.00	8.5	V	3.3
0	(8+9)-III-4	-1963	-3.38	32.00	9.5	-0.82	20.00	24	V	9.5
0	(8+9)-VIII-2	6008	10.35	32.00	3.1	2.50	20.00	8.0	V	3.1
0	(8+9)-IV-1	-4109	-7.07	32.00	4.5	-1.71	20.00	12	V	4.5
0	(8+9)-VII-4	-3170	-5.46	32.00	5.9	-1.32	20.00	15	V	5.9
0	(8+9)-I-1	1281	2.21	32.00	15	0.53	20.00	37	V	15
0	(8+9)-IV-3	-6045	-10.41	32.00	3.1	-2.52	20.00	7.9	V	3.1
0	(8+9)-I-3	-5173	-8.91	32.00	3.6	-2.16	20.00	9.3	V	3.6
0	(8+9)-IV-4	3710	6.39	32.00	5.0	1.55	20.00	13	V	5.0
0	(8+9)-II-1	-5054	-8.70	32.00	3.7	-2.11	20.00	9.5	V	3.7
0	(8+9)-V-1	2488	4.28	32.00	7.5	1.04	20.00	19	V	7.5
0	(8+9)-II-3	-6990	-12.03	32.00	2.7	-2.91	20.00	6.9	V	2.7
0	(8+9)-V-2	5981	10.30	32.00	3.1	2.49	20.00	8.0	V	3.1
0	(8+9)-III-1	1564	2.69	32.00	12	0.65	20.00	31	V	12
0	(8+9)-V-3	-6380	-10.99	32.00	2.9	-2.66	20.00	7.5	V	2.9
0	(8+9)-VIII-3	-6407	-11.03	32.00	2.9	-2.67	20.00	7.5	V	2.9
0	(8+9)-V-4	-2887	-4.97	32.00	6.4	-1.20	20.00	17	V	6.4
0	(8+9)-VII-3	-6097	-10.50	32.00	3.0	-2.54	20.00	7.9	V	3.0
0	(8+9)-VI-1	-4692	-8.08	32.00	4.0	-1.95	20.00	10	V	4.0
0	(8+9)-I-4	-1680	-2.89	32.00	11	-0.70	20.00	29	V	11

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
0	(8+9)-VI-2	6953	11.97	32.00	2.7	2.90	20.00	6.9	V	2.7
0	(8+9)-II-4	4655	8.01	32.00	4.0	1.94	20.00	10	V	4.0
0	(8+9)-VIII-1	-3747	-6.45	32.00	5.0	-1.56	20.00	13	V	5.0
0	(8+9)-I-2	4774	8.22	32.00	3.9	1.99	20.00	10	V	3.9
0	(8+9)-II-2	6591	11.35	32.00	2.8	2.75	20.00	7.3	V	2.8
0	(8+9)-III-2	4491	7.73	32.00	4.1	1.87	20.00	11	V	4.1
0	(8+9)-VI-3	-7352	-12.66	32.00	2.5	-3.06	20.00	6.5	V	2.5
0	(8+9)-VI-4	4293	7.39	32.00	4.3	1.79	20.00	11	V	4.3
0	(8+9)-VII-1	2771	4.77	32.00	6.7	1.15	20.00	17	V	6.7
1670	1	-558	-0.96	19.20	20	-0.23	12.00	52	V	20
1670	2	-1222	-2.10	28.80	14	-0.51	18.00	35	V	14
1670	3	-1222	-2.10	28.80	14	-0.51	18.00	35	V	14
1670	4	-558	-0.96	25.60	27	-0.23	16.00	69	V	27
1670	5	-558	-0.96	25.60	27	-0.23	16.00	69	V	27
1670	6	-558	-0.96	25.60	27	-0.23	16.00	69	V	27
1670	7	-558	-0.96	25.60	27	-0.23	16.00	69	V	27

Setto 39: origine (1449.0,2116.1,303.5), direzione (-0.200098,0.979776,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
500	(8+9)-V-1	2144	89	1471	1.77	2.75	4.36	132.00	192.00	192.00	20
1000	1	2928	131	-1364	2.42	4.05	-4.04	79.20	115.20	115.20	9.9
1000	2	6048	271	-2841	4.99	8.40	-8.42	118.80	172.80	172.80	7.2
1000	3	6048	271	-2841	4.99	8.40	-8.42	118.80	172.80	172.80	7.2
1000	4	2928	131	-1364	2.42	4.05	-4.04	105.60	153.60	153.60	13
1000	5	2928	131	-1364	2.42	4.05	-4.04	105.60	153.60	153.60	13
1000	6	2928	131	-1364	2.42	4.05	-4.04	105.60	153.60	153.60	13
1000	7	2928	131	-1364	2.42	4.05	-4.04	105.60	153.60	153.60	13
1000	(8+9)-VII-1	5388	79	499	4.44	2.46	1.48	132.00	192.00	192.00	18
1000	(8+9)-VIII-1	-1633	87	-2741	-1.35	2.68	-8.12	132.00	192.00	192.00	18
1000	(8+9)-I-3	-3255	86	-3430	-2.68	2.66	-10.17	132.00	192.00	192.00	15
1000	(8+9)-VIII-2	8625	87	2166	7.11	2.71	6.42	132.00	192.00	192.00	9.9
1000	(8+9)-II-1	-3123	92	-3374	-2.58	2.85	-10.00	132.00	192.00	192.00	15
1000	(8+9)-VIII-3	-4574	93	-4045	-3.77	2.88	-11.99	132.00	192.00	192.00	13
1000	(8+9)-II-3	-5179	89	-4343	-4.27	2.77	-12.87	132.00	192.00	192.00	12
1000	(8+9)-VIII-4	5684	94	862	4.69	2.91	2.55	132.00	192.00	192.00	16
1000	(8+9)-III-1	3914	94	-60	3.23	2.92	-0.18	132.00	192.00	192.00	25
1000	(8+9)-III-2	6991	95	1412	5.77	2.93	4.18	132.00	192.00	192.00	12
1000	(8+9)-VI-2	9673	86	2631	7.98	2.68	7.80	132.00	192.00	192.00	8.7
1000	(8+9)-III-3	-2940	86	-3291	-2.43	2.65	-9.75	132.00	192.00	192.00	15
1000	(8+9)-VI-3	-5621	94	-4510	-4.64	2.91	-13.37	132.00	192.00	192.00	12
1000	(8+9)-IV-1	-2075	91	-2908	-1.71	2.82	-8.62	132.00	192.00	192.00	17
1000	(8+9)-VI-4	6732	93	1327	5.55	2.87	3.93	132.00	192.00	192.00	13
1000	(8+9)-IV-3	-4132	88	-3877	-3.41	2.74	-11.49	132.00	192.00	192.00	13
1000	(8+9)-I-1	3600	95	-200	2.97	2.93	-0.59	132.00	192.00	192.00	24
1000	(8+9)-I-2	7306	94	1551	6.03	2.92	4.60	132.00	192.00	192.00	12
1000	(8+9)-VII-2	8466	80	1971	6.98	2.46	5.84	132.00	192.00	192.00	10
1000	(8+9)-V-3	-4729	101	-3989	-3.90	3.13	-11.82	132.00	192.00	192.00	13
1000	(8+9)-VII-3	-4415	101	-3850	-3.64	3.12	-11.41	132.00	192.00	192.00	13
1000	(8+9)-VI-1	-2681	88	-3206	-2.21	2.71	-9.50	132.00	192.00	192.00	16
1000	(8+9)-VII-4	-1337	101	-2378	-1.10	3.13	-7.05	132.00	192.00	192.00	19
1000	(8+9)-V-2	8780	79	2110	7.24	2.45	6.25	132.00	192.00	192.00	10.0
1000	(8+9)-V-4	-1023	101	-2238	-0.84	3.12	-6.63	132.00	192.00	192.00	20
1000	(8+9)-III-4	137	86	-1819	0.11	2.66	-5.39	132.00	192.00	192.00	23
1000	(8+9)-IV-4	6126	89	1029	5.05	2.77	3.05	132.00	192.00	192.00	15
1000	(8+9)-I-4	451	86	-1679	0.37	2.65	-4.98	132.00	192.00	192.00	24
1000	(8+9)-II-2	9230	91	2464	7.61	2.82	7.30	132.00	192.00	192.00	9.1
1000	(8+9)-II-4	7174	88	1495	5.92	2.73	4.43	132.00	192.00	192.00	12
1000	(8+9)-IV-2	8183	92	1999	6.75	2.85	5.92	132.00	192.00	192.00	10
Verifiche nella direzione secondaria											
0	(8+9)-IV-4	-2199	12	3285	-4.54	1.39	40.73	132.00	192.00	192.00	4.5
0	(8+9)-II-2	-3047	25	5656	-6.30	2.99	70.11	132.00	192.00	192.00	2.6

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-VIII-3	503	-16	-4900	1.04	-1.84	-60.75	132.00	192.00	192.00	3.0
0	(8+9)-II-3	633	-16	-5292	1.31	-1.95	-65.61	132.00	192.00	192.00	2.8
0	(8+9)-VII-4	-114	-16	-2535	-0.23	-1.90	-31.42	132.00	192.00	192.00	5.8
0	(8+9)-II-4	-2494	15	4033	-5.15	1.74	50.00	132.00	192.00	192.00	3.7
0	(8+9)-VII-2	-3062	32	5247	-6.33	3.84	65.05	132.00	192.00	192.00	2.8
0	(8+9)-VI-1	-86	-4	-3314	-0.18	-0.47	-41.08	132.00	192.00	192.00	4.6
0	(8+9)-VI-3	798	-18	-5648	1.65	-2.19	-70.02	132.00	192.00	192.00	2.6
0	(8+9)-III-2	-2510	26	4061	-5.19	3.05	50.34	132.00	192.00	192.00	3.6
0	(8+9)-I-3	184	-18	-3922	0.38	-2.12	-48.62	132.00	192.00	192.00	3.7
0	(8+9)-III-3	95	-17	-3697	0.20	-2.01	-45.83	132.00	192.00	192.00	4.0
0	(8+9)-II-1	79	-6	-3669	0.16	-0.70	-45.49	132.00	192.00	192.00	4.1
0	(8+9)-V-3	736	-25	-5108	1.52	-2.90	-63.32	132.00	192.00	192.00	2.8
0	(8+9)-VII-3	647	-24	-4884	1.34	-2.80	-60.54	132.00	192.00	192.00	2.9
0	(8+9)-I-2	-2598	27	4285	-5.37	3.15	53.12	132.00	192.00	192.00	3.4
0	(8+9)-VI-2	-3213	27	6012	-6.64	3.22	74.53	132.00	192.00	192.00	2.5
0	(8+9)-VIII-2	-2918	24	5264	-6.03	2.88	65.26	132.00	192.00	192.00	2.8
0	(8+9)-VI-4	-2328	13	3677	-4.81	1.50	45.59	132.00	192.00	192.00	4.1
0	(8+9)-V-2	-3150	33	5472	-6.51	3.94	67.83	132.00	192.00	192.00	2.7
0	(8+9)-IV-2	-2752	22	4908	-5.69	2.64	60.85	132.00	192.00	192.00	3.0
0	(8+9)-IV-3	337	-14	-4545	0.70	-1.61	-56.34	132.00	192.00	192.00	3.3
1670	1	-3054	344	-1442	-6.31	40.61	-17.88	79.20	115.20	115.20	2.0
1670	2	-6348	714	-2965	-13.12	84.39	-36.76	118.80	172.80	172.80	1.4
1670	3	-6348	714	-2965	-13.12	84.39	-36.76	118.80	172.80	172.80	1.4
1670	4	-3054	344	-1442	-6.31	40.61	-17.88	105.60	153.60	153.60	2.6
1670	5	-3054	344	-1442	-6.31	40.61	-17.88	105.60	153.60	153.60	2.6
1670	6	-3054	344	-1442	-6.31	40.61	-17.88	105.60	153.60	153.60	2.6
1670	7	-3054	344	-1442	-6.31	40.61	-17.88	105.60	153.60	153.60	2.6
1670	(8+9)-VIII-4	-1886	235	-988	-3.90	27.73	-12.25	132.00	192.00	192.00	4.8
1670	(8+9)-VII-1	-2759	261	-1505	-5.70	30.85	-18.66	132.00	192.00	192.00	3.9
1670	(8+9)-I-1	-2207	251	-1110	-4.56	29.69	-13.77	132.00	192.00	192.00	4.4
1670	(8+9)-I-4	-2004	223	-883	-4.14	26.32	-10.94	132.00	192.00	192.00	5.1
1670	(8+9)-III-1	-2209	252	-1120	-4.56	29.75	-13.88	132.00	192.00	192.00	4.4
1670	(8+9)-V-4	-1454	213	-497	-3.00	25.22	-6.16	132.00	192.00	192.00	6.1
1670	(8+9)-VIII-1	-2325	239	-1005	-4.80	28.28	-12.46	132.00	192.00	192.00	4.7
1670	(8+9)-III-4	-2003	222	-874	-4.14	26.26	-10.83	132.00	192.00	192.00	5.2
1670	(8+9)-IV-1	-2160	236	-889	-4.46	27.95	-11.03	132.00	192.00	192.00	4.9
1670	(8+9)-V-1	-2758	260	-1496	-5.70	30.79	-18.55	132.00	192.00	192.00	3.9

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Ty kg	τ_d kg/cmq	fvd kg/cmq	RS	Cs
0	1	315	0.19	3.84	Si	20
0	2	654	0.39	5.76	Si	15
0	3	654	0.39	5.76	Si	15
0	4	315	0.19	5.12	Si	27
0	5	315	0.19	5.12	Si	27
0	6	315	0.19	5.12	Si	27
0	7	315	0.19	5.12	Si	27
0	(8+9)-VIII-4	189	0.11	6.40	Si	56
0	(8+9)-IV-1	246	0.15	6.40	Si	43
0	(8+9)-I-2	209	0.13	6.40	Si	51
0	(8+9)-VIII-1	245	0.15	6.40	Si	44
0	(8+9)-I-3	225	0.13	6.40	Si	47
0	(8+9)-I-4	206	0.12	6.40	Si	52
0	(8+9)-II-2	186	0.11	6.40	Si	57
0	(8+9)-V-3	228	0.14	6.40	Si	47
0	(8+9)-II-4	185	0.11	6.40	Si	58
0	(8+9)-V-4	208	0.13	6.40	Si	51
0	(8+9)-III-2	211	0.13	6.40	Si	51
0	(8+9)-VI-1	249	0.15	6.40	Si	43
0	(8+9)-III-4	207	0.12	6.40	Si	52
0	(8+9)-VI-2	185	0.11	6.40	Si	58
0	(8+9)-IV-2	190	0.11	6.40	Si	56

X	Comb.	Ty	τ_d	fvd	RS	Cs
0	(8+9)-VI-3	249	0.15	6.40	Si	43
0	(8+9)-IV-4	189	0.11	6.40	Si	57
0	(8+9)-VI-4	185	0.11	6.40	Si	58
0	(8+9)-II-3	248	0.15	6.40	Si	43
0	(8+9)-VIII-3	245	0.15	6.40	Si	43
0	(8+9)-III-3	224	0.13	6.40	Si	48
0	(8+9)-IV-3	244	0.15	6.40	Si	44
0	(8+9)-II-1	249	0.15	6.40	Si	43
0	(8+9)-III-1	227	0.14	6.40	Si	47
0	(8+9)-I-1	228	0.14	6.40	Si	47
0	(8+9)-VIII-2	189	0.11	6.40	Si	56
0	(8+9)-VII-3	226	0.14	6.40	Si	47
0	(8+9)-VII-4	210	0.13	6.40	Si	51
500	(8+9)-V-1	264	0.16	6.40	Si	40
500	(8+9)-VII-2	240	0.14	6.40	Si	44
500	(8+9)-VII-1	262	0.16	6.40	Si	41
500	(8+9)-V-2	238	0.14	6.40	Si	45
Verifiche nella direzione secondaria						
1670	1	406	0.77	3.84	Si	5.0
1670	2	843	1.61	5.76	Si	3.6
1670	3	843	1.61	5.76	Si	3.6
1670	4	406	0.77	5.12	Si	6.6
1670	5	406	0.77	5.12	Si	6.6
1670	6	406	0.77	5.12	Si	6.6
1670	7	406	0.77	5.12	Si	6.6
1670	(8+9)-VIII-4	281	0.54	6.40	Si	12
1670	(8+9)-IV-2	286	0.55	6.40	Si	12
1670	(8+9)-V-1	292	0.56	6.40	Si	11
1670	(8+9)-I-2	286	0.55	6.40	Si	12
1670	(8+9)-V-2	296	0.56	6.40	Si	11
1670	(8+9)-I-4	277	0.53	6.40	Si	12
1670	(8+9)-V-3	264	0.50	6.40	Si	13
1670	(8+9)-II-2	287	0.55	6.40	Si	12
1670	(8+9)-V-4	267	0.51	6.40	Si	13
1670	(8+9)-II-4	284	0.54	6.40	Si	12
1670	(8+9)-VI-1	278	0.53	6.40	Si	12
1670	(8+9)-III-2	286	0.55	6.40	Si	12
1670	(8+9)-VI-2	290	0.55	6.40	Si	12
1670	(8+9)-III-4	277	0.53	6.40	Si	12
1670	(8+9)-VI-3	270	0.51	6.40	Si	12
1670	(8+9)-I-1	283	0.54	6.40	Si	12
1670	(8+9)-VI-4	281	0.54	6.40	Si	12
1670	(8+9)-IV-4	283	0.54	6.40	Si	12
1670	(8+9)-VII-1	293	0.56	6.40	Si	11
1670	(8+9)-II-1	275	0.53	6.40	Si	12
1670	(8+9)-VII-2	296	0.56	6.40	Si	11
1670	(8+9)-III-1	283	0.54	6.40	Si	12
1670	(8+9)-VII-3	264	0.50	6.40	Si	13
1670	(8+9)-IV-1	276	0.53	6.40	Si	12
1670	(8+9)-VII-4	267	0.51	6.40	Si	13
1670	(8+9)-III-3	274	0.52	6.40	Si	12
1670	(8+9)-IV-3	273	0.52	6.40	Si	12
1670	(8+9)-II-3	273	0.52	6.40	Si	12
1670	(8+9)-VIII-1	279	0.53	6.40	Si	12
1670	(8+9)-VIII-2	289	0.55	6.40	Si	12
1670	(8+9)-VIII-3	270	0.52	6.40	Si	12
1670	(8+9)-I-3	273	0.52	6.40	Si	12

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	(8+9)-VIII-4	-4094	-5.07	32.00	6.3	-1.23	20.00	16	V	6.3
0	(8+9)-VIII-2	-6366	-7.88	32.00	4.1	-1.91	20.00	10	V	4.1

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
0	(8+9)-II-4	-5226	-6.47	32.00	4.9	-1.56	20.00	13	V	4.9
0	(8+9)-II-2	-7001	-8.66	32.00	3.7	-2.10	20.00	9.5	V	3.7
0	(8+9)-VI-4	-4978	-6.16	32.00	5.2	-1.49	20.00	13	V	5.2
0	(8+9)-VI-2	-7250	-8.97	32.00	3.6	-2.17	20.00	9.2	V	3.6
0	(8+9)-IV-2	-6118	-7.57	32.00	4.2	-1.83	20.00	11	V	4.2
0	(8+9)-IV-4	-4343	-5.37	32.00	6.0	-1.30	20.00	15	V	6.0
500	(8+9)-III-2	-5081	-6.29	32.00	5.1	-1.52	20.00	13	V	5.1
500	(8+9)-V-1	-3067	-3.79	32.00	8.4	-0.92	20.00	22	V	8.4
500	(8+9)-I-1	-2082	-2.58	32.00	12	-0.62	20.00	32	V	12
500	(8+9)-V-2	-6318	-7.82	32.00	4.1	-1.89	20.00	11	V	4.1
500	(8+9)-VII-1	-3319	-4.11	32.00	7.8	-0.99	20.00	20	V	7.8
500	(8+9)-I-2	-5333	-6.60	32.00	4.8	-1.60	20.00	13	V	4.8
500	(8+9)-VII-2	-6066	-7.51	32.00	4.3	-1.82	20.00	11	V	4.3
500	(8+9)-III-1	-2334	-2.89	32.00	11	-0.70	20.00	29	V	11
1000	1	1862	2.30	19.20	8.3	0.56	12.00	22	V	8.3
1000	2	3891	4.81	28.80	6.0	1.17	18.00	15	V	6.0
1000	3	3891	4.81	28.80	6.0	1.17	18.00	15	V	6.0
1000	4	1862	2.30	25.60	11	0.56	16.00	29	V	11
1000	5	1862	2.30	25.60	11	0.56	16.00	29	V	11
1000	6	1862	2.30	25.60	11	0.56	16.00	29	V	11
1000	7	1862	2.30	25.60	11	0.56	16.00	29	V	11
1000	(8+9)-IV-1	5153	6.38	32.00	5.0	1.54	20.00	13	V	5.0
1000	(8+9)-III-3	5938	7.35	32.00	4.4	1.78	20.00	11	V	4.4
1000	(8+9)-II-1	5993	7.41	32.00	4.3	1.79	20.00	11	V	4.3
1000	(8+9)-I-3	6190	7.66	32.00	4.2	1.85	20.00	11	V	4.2
1000	(8+9)-II-3	7916	9.79	32.00	3.3	2.37	20.00	8.4	V	3.3
1000	(8+9)-V-4	3914	4.84	32.00	6.6	1.17	20.00	17	V	6.6
1000	(8+9)-VII-3	7065	8.74	32.00	3.7	2.12	20.00	9.5	V	3.7
1000	(8+9)-I-4	2788	3.45	32.00	9.3	0.83	20.00	24	V	9.3
1000	(8+9)-VII-4	4166	5.15	32.00	6.2	1.25	20.00	16	V	6.2
1000	(8+9)-VI-1	5655	7.00	32.00	4.6	1.69	20.00	12	V	4.6
1000	(8+9)-VI-3	8254	10.21	32.00	3.1	2.47	20.00	8.1	V	3.1
1000	(8+9)-V-3	7317	9.05	32.00	3.5	2.19	20.00	9.1	V	3.5
1000	(8+9)-VIII-1	4815	5.96	32.00	5.4	1.44	20.00	14	V	5.4
1000	(8+9)-III-4	3040	3.76	32.00	8.5	0.91	20.00	22	V	8.5
1000	(8+9)-VIII-3	7414	9.17	32.00	3.5	2.22	20.00	9.0	V	3.5
1000	(8+9)-IV-3	7076	8.75	32.00	3.7	2.12	20.00	9.4	V	3.7
Verifiche nella direzione secondaria										
0	(8+9)-VIII-4	3615	7.47	32.00	4.3	1.81	20.00	11	V	4.3
0	(8+9)-VII-2	5584	11.54	32.00	2.8	2.79	20.00	7.2	V	2.8
0	(8+9)-III-3	-4186	-8.65	32.00	3.7	-2.09	20.00	9.6	V	3.7
0	(8+9)-IV-2	5693	11.76	32.00	2.7	2.85	20.00	7.0	V	2.7
0	(8+9)-III-4	-1344	-2.78	32.00	12	-0.67	20.00	30	V	12
0	(8+9)-VIII-2	6055	12.51	32.00	2.6	3.03	20.00	6.6	V	2.6
0	(8+9)-IV-1	-3782	-7.81	32.00	4.1	-1.89	20.00	11	V	4.1
0	(8+9)-VII-4	-2547	-5.26	32.00	6.1	-1.27	20.00	16	V	6.1
0	(8+9)-I-1	1276	2.64	32.00	12	0.64	20.00	31	V	12
0	(8+9)-IV-3	-5499	-11.36	32.00	2.8	-2.75	20.00	7.3	V	2.8
0	(8+9)-I-3	-4448	-9.19	32.00	3.5	-2.22	20.00	9.0	V	3.5
0	(8+9)-IV-4	3976	8.22	32.00	3.9	1.99	20.00	10	V	3.9
0	(8+9)-II-1	-4656	-9.62	32.00	3.3	-2.33	20.00	8.6	V	3.3
0	(8+9)-V-1	2479	5.12	32.00	6.2	1.24	20.00	16	V	6.2
0	(8+9)-II-3	-6373	-13.17	32.00	2.4	-3.19	20.00	6.3	V	2.4
0	(8+9)-V-2	5846	12.08	32.00	2.6	2.92	20.00	6.8	V	2.6
0	(8+9)-III-1	1538	3.18	32.00	10	0.77	20.00	26	V	10
0	(8+9)-V-3	-5652	-11.68	32.00	2.7	-2.83	20.00	7.1	V	2.7
0	(8+9)-VIII-3	-5860	-12.11	32.00	2.6	-2.93	20.00	6.8	V	2.6
0	(8+9)-V-4	-2285	-4.72	32.00	6.8	-1.14	20.00	18	V	6.8
0	(8+9)-VII-3	-5390	-11.14	32.00	2.9	-2.69	20.00	7.4	V	2.9
0	(8+9)-VI-1	-4295	-8.87	32.00	3.6	-2.15	20.00	9.3	V	3.6
0	(8+9)-I-4	-1081	-2.23	32.00	14	-0.54	20.00	37	V	14
0	(8+9)-VI-2	6929	14.32	32.00	2.2	3.46	20.00	5.8	V	2.2
0	(8+9)-II-4	4850	10.02	32.00	3.2	2.43	20.00	8.2	V	3.2
0	(8+9)-VIII-1	-3420	-7.07	32.00	4.5	-1.71	20.00	12	V	4.5

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
0	(8+9)-I-2	4643	9.59	32.00	3.3	2.32	20.00	8.6	V	3.3
0	(8+9)-II-2	6568	13.57	32.00	2.4	3.28	20.00	6.1	V	2.4
0	(8+9)-III-2	4381	9.05	32.00	3.5	2.19	20.00	9.1	V	3.5
0	(8+9)-VI-3	-6734	-13.91	32.00	2.3	-3.37	20.00	5.9	V	2.3
0	(8+9)-VI-4	4489	9.28	32.00	3.4	2.24	20.00	8.9	V	3.4
0	(8+9)-VII-1	2742	5.66	32.00	5.6	1.37	20.00	15	V	5.6
1670	1	340	0.70	19.20	27	0.17	12.00	71	V	27
1670	2	631	1.30	28.80	22	0.32	18.00	57	V	22
1670	3	631	1.30	28.80	22	0.32	18.00	57	V	22
1670	4	340	0.70	25.60	36	0.17	16.00	94	V	36
1670	5	340	0.70	25.60	36	0.17	16.00	94	V	36
1670	6	340	0.70	25.60	36	0.17	16.00	94	V	36
1670	7	340	0.70	25.60	36	0.17	16.00	94	V	36

Verifiche a instabilità

Setto(X)	Comb.	k _{critc}	k _{critm}	λ_{relc}	λ_{relm}	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
(cm)						kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	
35(0.0)	(8+9)-VI-2	--	--	--	--	3.10	-0.60	-4.59	132.00	192.00	192.00	20
36(0.0)	3	--	--	--	--	2.20	3.61	-5.17	118.80	172.80	172.80	14
37(0.0)	(8+9)-V-3	1.00	--	0.20	--	-1.49	-3.09	4.57	132.00	192.00	192.00	21
38(120.0)	(8+9)-VI-2	--	--	--	--	8.09	-1.38	13.98	132.00	192.00	192.00	7.1
39(100.0)	3	--	--	--	--	4.99	8.40	-8.42	118.80	172.80	172.80	7.2

Parete Xlam 13 - Nodi: [21-26-22-23-27-28-26-27-29-30-30-31-31-8-110-26-109] - **Crit.Prog.** Criterio di verifica XLAM 0 - **Verificato:** [Cs=1.570,Comb=(8+9)-VI-3]

Geometria setti

Setto	Crit.	X	L	S	X90	L90	S90
		mm	cm	cm	mm	cm	cm
40	Criterio di verifica XLAM 0	0	387.0	12.1	0	80.0	12.1
		400	387.0	12.1	1935	80.0	12.1
		800	387.0	12.1	3870	80.0	12.1
41	Criterio di verifica XLAM 0	0	387.0	12.1	0	30.0	12.1
		150	387.0	12.1	1935	30.0	12.1
		300	387.0	12.1	3870	30.0	12.1
42	Criterio di verifica XLAM 0	0	387.0	12.1	0	30.0	12.1
		150	387.0	12.1	1935	30.0	12.1
		300	387.0	12.1	3870	30.0	12.1
43	Criterio di verifica XLAM 0	0	387.0	12.1	0	58.0	12.1
		290	387.0	12.1	1935	58.0	12.1
		580	387.0	12.1	3870	58.0	12.1
44	Criterio di verifica XLAM 0	0	167.0	12.1	0	220.0	12.1
		1100	167.0	12.1	835	220.0	12.1
		2200	167.0	12.1	1670	220.0	12.1
45	Criterio di verifica XLAM 0	0	167.0	12.1	0	240.0	12.1
		1200	167.0	12.1	835	240.0	12.1
		2400	167.0	12.1	1670	240.0	12.1
46	Criterio di verifica XLAM 0	0	167.0	12.1	0	240.0	12.1
		1200	167.0	12.1	835	240.0	12.1
		2400	167.0	12.1	1670	240.0	12.1

Setto 40: origine (1475.9,1983.6,193.5), direzione (-0.199392,0.97992,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-VIII-4	4355	-5	-3921	1.55	-0.07	-2.16	132.00	192.00	192.00	43
0	(8+9)-IV-1	-4925	-7	3983	-1.75	-0.09	2.20	132.00	192.00	192.00	83
0	(8+9)-VII-2	7180	-7	-6381	2.56	-0.10	-3.52	132.00	192.00	192.00	26
0	(8+9)-III-3	-5980	-2	5257	-2.13	-0.03	2.90	132.00	192.00	192.00	65
0	(8+9)-IV-2	7211	-7	-6471	2.57	-0.09	-3.57	132.00	192.00	192.00	26
0	(8+9)-III-4	-2340	-2	2121	-0.83	-0.03	1.17	132.00	192.00	192.00	>100
0	(8+9)-VIII-2	7619	-6	-6745	2.71	-0.08	-3.72	132.00	192.00	192.00	25
0	(8+9)-VII-3	-7341	-4	6169	-2.61	-0.06	3.40	132.00	192.00	192.00	55
0	(8+9)-VII-4	-3701	-4	3033	-1.32	-0.06	1.67	132.00	192.00	192.00	>100
0	(8+9)-I-2	6200	-9	-5798	2.21	-0.12	-3.20	132.00	192.00	192.00	29
0	(8+9)-IV-3	-7373	-5	6260	-2.62	-0.07	3.45	132.00	192.00	192.00	54
0	(8+9)-I-4	-1959	-2	1791	-0.70	-0.02	0.99	132.00	192.00	192.00	>100
0	(8+9)-IV-4	4764	-5	-4195	1.70	-0.06	-2.31	132.00	192.00	192.00	40
0	(8+9)-II-2	8480	-5	-7569	3.02	-0.07	-4.18	132.00	192.00	192.00	22
0	(8+9)-V-1	3158	-8	-2915	1.12	-0.10	-1.61	132.00	192.00	192.00	57
0	(8+9)-II-4	6033	-3	-5293	2.15	-0.04	-2.92	132.00	192.00	192.00	32
0	(8+9)-V-2	7561	-7	-6710	2.69	-0.09	-3.70	132.00	192.00	192.00	25
0	(8+9)-III-2	5819	-9	-5468	2.07	-0.12	-3.02	132.00	192.00	192.00	31
0	(8+9)-V-3	-7722	-5	6499	-2.75	-0.07	3.59	132.00	192.00	192.00	52
0	(8+9)-VIII-1	-4517	-6	3709	-1.61	-0.09	2.05	132.00	192.00	192.00	89
0	(8+9)-V-4	-3320	-4	2703	-1.18	-0.05	1.49	132.00	192.00	192.00	>100
0	(8+9)-I-3	-6361	-3	5586	-2.26	-0.04	3.08	132.00	192.00	192.00	61
0	(8+9)-VI-1	-5786	-8	4807	-2.06	-0.11	2.65	132.00	192.00	192.00	69
0	(8+9)-II-3	-8642	-7	7358	-3.08	-0.09	4.06	132.00	192.00	192.00	46
0	(8+9)-VI-2	8889	-4	-7843	3.16	-0.06	-4.33	132.00	192.00	192.00	21
0	(8+9)-VIII-3	-7781	-6	6533	-2.77	-0.08	3.61	132.00	192.00	192.00	52
0	(8+9)-II-1	-6194	-9	5081	-2.20	-0.12	2.80	132.00	192.00	192.00	65
0	(8+9)-III-1	2178	-9	-2332	0.78	-0.12	-1.29	132.00	192.00	192.00	76
0	(8+9)-I-1	1797	-10	-2003	0.64	-0.13	-1.11	132.00	192.00	192.00	89
0	(8+9)-VI-3	-9050	-7	7632	-3.22	-0.10	4.21	132.00	192.00	192.00	44
0	(8+9)-VI-4	5625	-4	-5019	2.00	-0.05	-2.77	132.00	192.00	192.00	34
0	(8+9)-VII-1	3539	-7	-3245	1.26	-0.10	-1.79	132.00	192.00	192.00	52
800	1	-233	-17	53	-0.08	-0.23	0.03	79.20	115.20	115.20	>100
800	2	-443	-32	111	-0.16	-0.43	0.06	118.80	172.80	172.80	>100
800	3	-443	-32	111	-0.16	-0.43	0.06	118.80	172.80	172.80	>100
800	4	-233	-17	53	-0.08	-0.23	0.03	105.60	153.60	153.60	>100
800	5	-233	-17	53	-0.08	-0.23	0.03	105.60	153.60	153.60	>100
800	6	-233	-17	53	-0.08	-0.23	0.03	105.60	153.60	153.60	>100
800	7	-233	-17	53	-0.08	-0.23	0.03	105.60	153.60	153.60	>100
Verifiche nella direzione secondaria											
0	(8+9)-VIII-4	-6681	-21	1311	-17.25	-3.15	25.39	132.00	192.00	192.00	6.4
0	(8+9)-VII-2	-12258	-73	2140	-31.66	-10.75	41.46	132.00	192.00	192.00	3.3
0	(8+9)-III-3	7803	42	-1607	20.15	6.27	-31.12	132.00	192.00	192.00	2.9
0	(8+9)-IV-2	-11184	-50	2114	-28.89	-7.35	40.95	132.00	192.00	192.00	3.6
0	(8+9)-III-4	2755	22	-537	7.11	3.24	-10.41	132.00	192.00	192.00	8.0
0	(8+9)-VIII-2	-11973	-56	2269	-30.92	-8.28	43.95	132.00	192.00	192.00	3.4
0	(8+9)-IV-1	5642	18	-1450	14.57	2.72	-28.09	132.00	192.00	192.00	3.7
0	(8+9)-VII-4	5382	43	-1055	13.90	6.36	-20.44	132.00	192.00	192.00	4.1
0	(8+9)-I-1	-4120	-29	438	-10.64	-4.23	8.49	132.00	192.00	192.00	14
0	(8+9)-IV-3	9357	40	-2098	24.17	5.98	-40.64	132.00	192.00	192.00	2.3
0	(8+9)-I-3	8265	45	-1721	21.35	6.65	-33.34	132.00	192.00	192.00	2.7
0	(8+9)-IV-4	-7469	-28	1466	-19.29	-4.09	28.40	132.00	192.00	192.00	5.6
0	(8+9)-II-1	7184	27	-1832	18.55	4.00	-35.49	132.00	192.00	192.00	2.9
0	(8+9)-V-1	-6747	-50	956	-17.43	-7.34	18.52	132.00	192.00	192.00	7.0
0	(8+9)-II-3	10900	49	-2480	28.15	7.27	-48.04	132.00	192.00	192.00	2.0
0	(8+9)-V-2	-12720	-75	2255	-32.85	-11.13	43.68	132.00	192.00	192.00	3.2
0	(8+9)-III-1	-4582	-31	553	-11.83	-4.61	10.71	132.00	192.00	192.00	12
0	(8+9)-V-3	10893	66	-2239	28.13	9.77	-43.37	132.00	192.00	192.00	2.0
0	(8+9)-VIII-3	10145	47	-2253	26.20	6.92	-43.65	132.00	192.00	192.00	2.2
0	(8+9)-V-4	4920	40	-941	12.71	5.97	-18.22	132.00	192.00	192.00	4.5
0	(8+9)-VII-3	10430	63	-2124	26.94	9.38	-41.15	132.00	192.00	192.00	2.1
0	(8+9)-VI-1	6396	21	-1677	16.52	3.07	-32.48	132.00	192.00	192.00	3.2
0	(8+9)-I-4	2292	19	-423	5.92	2.86	-8.19	132.00	192.00	192.00	9.8
0	(8+9)-VI-2	-13515	-65	2652	-34.91	-9.57	51.36	132.00	192.00	192.00	2.9

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-II-4	-9012	-36	1848	-23.27	-5.37	35.80	132.00	192.00	192.00	4.4
0	(8+9)-VIII-1	4853	12	-1295	12.53	1.78	-25.08	132.00	192.00	192.00	4.3
0	(8+9)-I-2	-10093	-54	1737	-26.07	-8.02	33.65	132.00	192.00	192.00	4.2
0	(8+9)-II-2	-12727	-58	2496	-32.87	-8.63	48.35	132.00	192.00	192.00	3.1
0	(8+9)-III-2	-9630	-52	1622	-24.87	-7.63	31.42	132.00	192.00	192.00	4.5
0	(8+9)-VI-3	11688	55	-2636	30.19	8.20	-51.05	132.00	192.00	192.00	1.9
0	(8+9)-VI-4	-8223	-30	1693	-21.24	-4.43	32.79	132.00	192.00	192.00	4.9
0	(8+9)-VII-1	-7210	-52	1071	-18.62	-7.73	20.75	132.00	192.00	192.00	6.3
3870	1	-220	13	76	-0.57	1.88	1.46	79.20	115.20	115.20	34
3870	2	-476	27	157	-1.23	3.99	3.03	118.80	172.80	172.80	25
3870	3	-476	27	157	-1.23	3.99	3.03	118.80	172.80	172.80	25
3870	4	-220	13	76	-0.57	1.88	1.46	105.60	153.60	153.60	46
3870	5	-220	13	76	-0.57	1.88	1.46	105.60	153.60	153.60	46
3870	6	-220	13	76	-0.57	1.88	1.46	105.60	153.60	153.60	46
3870	7	-220	13	76	-0.57	1.88	1.46	105.60	153.60	153.60	46

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
0	(8+9)-II-2	-20	0.01	6.40	Si	>100
0	(8+9)-IV-2	-18	0.00	6.40	Si	>100
400	(8+9)-VI-2	-42	0.01	6.40	Si	>100
400	(8+9)-VI-3	30	0.01	6.40	Si	>100
400	(8+9)-VIII-2	-47	0.01	6.40	Si	>100
400	(8+9)-VIII-3	34	0.01	6.40	Si	>100
800	1	-10	0.00	3.84	Si	>100
800	2	-17	0.00	5.76	Si	>100
800	3	-17	0.00	5.76	Si	>100
800	4	-10	0.00	5.12	Si	>100
800	5	-10	0.00	5.12	Si	>100
800	6	-10	0.00	5.12	Si	>100
800	7	-10	0.00	5.12	Si	>100
800	(8+9)-VIII-4	-88	0.02	6.40	Si	>100
800	(8+9)-IV-1	71	0.02	6.40	Si	>100
800	(8+9)-V-4	-180	0.05	6.40	Si	>100
800	(8+9)-II-4	-85	0.02	6.40	Si	>100
800	(8+9)-VI-1	75	0.02	6.40	Si	>100
800	(8+9)-III-2	135	0.04	6.40	Si	>100
800	(8+9)-I-4	-169	0.04	6.40	Si	>100
800	(8+9)-III-4	-169	0.04	6.40	Si	>100
800	(8+9)-I-3	-149	0.04	6.40	Si	>100
800	(8+9)-II-1	71	0.02	6.40	Si	>100
800	(8+9)-VI-4	-89	0.02	6.40	Si	>100
800	(8+9)-IV-4	-85	0.02	6.40	Si	>100
800	(8+9)-VII-1	166	0.04	6.40	Si	>100
800	(8+9)-V-2	146	0.04	6.40	Si	>100
800	(8+9)-VII-2	146	0.04	6.40	Si	>100
800	(8+9)-III-1	155	0.04	6.40	Si	>100
800	(8+9)-VII-3	-160	0.04	6.40	Si	>100
800	(8+9)-II-3	-20	0.01	6.40	Si	>100
800	(8+9)-VII-4	-180	0.05	6.40	Si	>100
800	(8+9)-III-3	-149	0.04	6.40	Si	>100
800	(8+9)-IV-3	-20	0.01	6.40	Si	>100
800	(8+9)-V-3	-160	0.04	6.40	Si	>100
800	(8+9)-VIII-1	74	0.02	6.40	Si	>100
800	(8+9)-I-2	135	0.04	6.40	Si	>100
800	(8+9)-I-1	155	0.04	6.40	Si	>100
800	(8+9)-V-1	166	0.04	6.40	Si	>100
Verifiche nella direzione secondaria						
0	(8+9)-VIII-4	37	0.09	6.40	Si	72
0	(8+9)-VI-2	103	0.24	6.40	Si	26
0	(8+9)-VI-4	53	0.13	6.40	Si	51
0	(8+9)-IV-2	75	0.18	6.40	Si	36

X	Comb.	Ty	τ_d	fvd	RS	Cs
0	(8+9)-III-2	69	0.17	6.40	Si	39
0	(8+9)-VIII-2	87	0.21	6.40	Si	31
0	(8+9)-III-3	-47	0.11	6.40	Si	57
0	(8+9)-VII-3	-88	0.21	6.40	Si	31
0	(8+9)-VII-1	79	0.19	6.40	Si	34
0	(8+9)-VI-3	-80	0.19	6.40	Si	33
0	(8+9)-I-3	-52	0.12	6.40	Si	52
0	(8+9)-VI-1	-30	0.07	6.40	Si	89
0	(8+9)-I-4	-12	0.03	6.40	Si	>100
0	(8+9)-II-1	-42	0.10	6.40	Si	63
0	(8+9)-II-3	-68	0.16	6.40	Si	39
0	(8+9)-IV-3	-53	0.13	6.40	Si	51
0	(8+9)-VIII-3	-65	0.15	6.40	Si	41
0	(8+9)-IV-4	49	0.12	6.40	Si	54
0	(8+9)-VII-2	110	0.26	6.40	Si	24
0	(8+9)-V-1	75	0.18	6.40	Si	36
0	(8+9)-II-2	91	0.22	6.40	Si	30
0	(8+9)-VII-4	-57	0.14	6.40	Si	47
0	(8+9)-I-2	74	0.18	6.40	Si	36
0	(8+9)-II-4	65	0.15	6.40	Si	41
0	(8+9)-V-2	115	0.27	6.40	Si	23
0	(8+9)-V-3	-92	0.22	6.40	Si	29
0	(8+9)-V-4	-52	0.12	6.40	Si	51
1935	(8+9)-III-4	-26	0.06	6.40	Si	>100
3870	1	31	0.07	3.84	Si	51
3870	2	67	0.16	5.76	Si	36
3870	3	67	0.16	5.76	Si	36
3870	4	31	0.07	5.12	Si	69
3870	5	31	0.07	5.12	Si	69
3870	6	31	0.07	5.12	Si	69
3870	7	31	0.07	5.12	Si	69
3870	(8+9)-VIII-1	29	0.07	6.40	Si	93
3870	(8+9)-I-1	53	0.13	6.40	Si	51
3870	(8+9)-III-1	53	0.13	6.40	Si	51
3870	(8+9)-IV-1	27	0.06	6.40	Si	99

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
400	(8+9)-I-4	2398	1.28	32.00	25	0.31	20.00	65	V	25
400	(8+9)-III-4	2839	1.52	32.00	21	0.37	20.00	55	V	21
800	1	-356	-0.19	19.20	>100	-0.05	12.00	>100	V	>100
800	2	-750	-0.40	28.80	72	-0.10	18.00	>100	V	72
800	3	-750	-0.40	28.80	72	-0.10	18.00	>100	V	72
800	4	-356	-0.19	25.60	>100	-0.05	16.00	>100	V	>100
800	5	-356	-0.19	25.60	>100	-0.05	16.00	>100	V	>100
800	6	-356	-0.19	25.60	>100	-0.05	16.00	>100	V	>100
800	7	-356	-0.19	25.60	>100	-0.05	16.00	>100	V	>100
800	(8+9)-VIII-4	-8636	-4.61	32.00	6.9	-1.12	20.00	18	V	6.9
800	(8+9)-IV-1	9103	4.86	32.00	6.6	1.18	20.00	17	V	6.6
800	(8+9)-V-2	-13775	-7.35	32.00	4.4	-1.78	20.00	11	V	4.4
800	(8+9)-I-3	10110	5.40	32.00	5.9	1.31	20.00	15	V	5.9
800	(8+9)-V-3	13289	7.09	32.00	4.5	1.72	20.00	12	V	4.5
800	(8+9)-II-2	-15223	-8.13	32.00	3.9	-1.97	20.00	10	V	3.9
800	(8+9)-V-4	5460	2.91	32.00	11	0.71	20.00	28	V	11
800	(8+9)-II-4	-11360	-6.06	32.00	5.3	-1.47	20.00	14	V	5.3
800	(8+9)-VI-1	9920	5.30	32.00	6.0	1.28	20.00	16	V	6.0
800	(8+9)-III-2	-10065	-5.37	32.00	6.0	-1.30	20.00	15	V	6.0
800	(8+9)-VI-2	-16177	-8.64	32.00	3.7	-2.09	20.00	9.6	V	3.7
800	(8+9)-I-2	-10596	-5.66	32.00	5.7	-1.37	20.00	15	V	5.7
800	(8+9)-VI-3	15691	8.38	32.00	3.8	2.03	20.00	9.9	V	3.8
800	(8+9)-IV-2	-13453	-7.18	32.00	4.5	-1.74	20.00	12	V	4.5
800	(8+9)-VI-4	-10406	-5.56	32.00	5.8	-1.34	20.00	15	V	5.8

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
800	(8+9)-IV-4	-9589	-5.12	32.00	6.3	-1.24	20.00	16	V	6.3
800	(8+9)-VII-1	-6477	-3.46	32.00	9.3	-0.84	20.00	24	V	9.3
800	(8+9)-II-1	10874	5.81	32.00	5.5	1.40	20.00	14	V	5.5
800	(8+9)-VII-2	-13244	-7.07	32.00	4.5	-1.71	20.00	12	V	4.5
800	(8+9)-III-1	-3298	-1.76	32.00	18	-0.43	20.00	47	V	18
800	(8+9)-VII-3	12758	6.81	32.00	4.7	1.65	20.00	12	V	4.7
800	(8+9)-I-1	-2767	-1.48	32.00	22	-0.36	20.00	56	V	22
800	(8+9)-VII-4	5991	3.20	32.00	10	0.77	20.00	26	V	10
800	(8+9)-III-3	9579	5.11	32.00	6.3	1.24	20.00	16	V	6.3
800	(8+9)-IV-3	12967	6.92	32.00	4.6	1.68	20.00	12	V	4.6
800	(8+9)-II-3	14737	7.87	32.00	4.1	1.90	20.00	11	V	4.1
800	(8+9)-VIII-1	8150	4.35	32.00	7.4	1.05	20.00	19	V	7.4
800	(8+9)-VIII-2	-14406	-7.69	32.00	4.2	-1.86	20.00	11	V	4.2
800	(8+9)-VIII-3	13920	7.43	32.00	4.3	1.80	20.00	11	V	4.3
800	(8+9)-V-1	-5946	-3.17	32.00	10	-0.77	20.00	26	V	10
Verifiche nella direzione secondaria										
0	1	64	0.16	19.20	>100	0.04	12.00	>100	V	>100
0	2	99	0.26	28.80	>100	0.06	18.00	>100	V	>100
0	3	99	0.26	28.80	>100	0.06	18.00	>100	V	>100
0	4	64	0.16	25.60	>100	0.04	16.00	>100	V	>100
0	5	64	0.16	25.60	>100	0.04	16.00	>100	V	>100
0	6	64	0.16	25.60	>100	0.04	16.00	>100	V	>100
0	7	64	0.16	25.60	>100	0.04	16.00	>100	V	>100
1935	(8+9)-VIII-4	2420	6.25	32.00	5.1	1.51	20.00	13	V	5.1
1935	(8+9)-IV-2	4108	10.61	32.00	3.0	2.57	20.00	7.8	V	3.0
1935	(8+9)-V-1	2038	5.26	32.00	6.1	1.27	20.00	16	V	6.1
1935	(8+9)-I-2	3539	9.14	32.00	3.5	2.21	20.00	9.0	V	3.5
1935	(8+9)-V-2	4488	11.59	32.00	2.8	2.80	20.00	7.1	V	2.8
1935	(8+9)-I-4	-1139	-2.94	32.00	11	-0.71	20.00	28	V	11
1935	(8+9)-V-3	-4537	-11.72	32.00	2.7	-2.84	20.00	7.1	V	2.7
1935	(8+9)-II-2	4760	12.29	32.00	2.6	2.98	20.00	6.7	V	2.6
1935	(8+9)-V-4	-2087	-5.39	32.00	5.9	-1.30	20.00	15	V	5.9
1935	(8+9)-II-4	3357	8.67	32.00	3.7	2.10	20.00	9.5	V	3.7
1935	(8+9)-VI-1	-3121	-8.06	32.00	4.0	-1.95	20.00	10	V	4.0
1935	(8+9)-III-2	3344	8.64	32.00	3.7	2.09	20.00	9.6	V	3.7
1935	(8+9)-VI-2	5045	13.03	32.00	2.5	3.15	20.00	6.3	V	2.5
1935	(8+9)-III-4	-1334	-3.45	32.00	9.3	-0.83	20.00	24	V	9.3
1935	(8+9)-VI-3	-5094	-13.16	32.00	2.4	-3.18	20.00	6.3	V	2.4
1935	(8+9)-I-1	1090	2.81	32.00	11	0.68	20.00	29	V	11
1935	(8+9)-VI-4	3072	7.93	32.00	4.0	1.92	20.00	10	V	4.0
1935	(8+9)-IV-4	2705	6.98	32.00	4.6	1.69	20.00	12	V	4.6
1935	(8+9)-VII-1	2234	5.77	32.00	5.5	1.40	20.00	14	V	5.5
1935	(8+9)-II-1	-3406	-8.80	32.00	3.6	-2.13	20.00	9.4	V	3.6
1935	(8+9)-VII-2	4292	11.09	32.00	2.9	2.68	20.00	7.5	V	2.9
1935	(8+9)-III-1	1285	3.32	32.00	9.6	0.80	20.00	25	V	9.6
1935	(8+9)-VII-3	-4341	-11.21	32.00	2.9	-2.71	20.00	7.4	V	2.9
1935	(8+9)-IV-1	-2754	-7.11	32.00	4.5	-1.72	20.00	12	V	4.5
1935	(8+9)-VII-4	-2283	-5.90	32.00	5.4	-1.43	20.00	14	V	5.4
1935	(8+9)-III-3	-3393	-8.76	32.00	3.7	-2.12	20.00	9.4	V	3.7
1935	(8+9)-IV-3	-4157	-10.74	32.00	3.0	-2.60	20.00	7.7	V	3.0
1935	(8+9)-II-3	-4809	-12.42	32.00	2.6	-3.01	20.00	6.7	V	2.6
1935	(8+9)-VIII-1	-2469	-6.38	32.00	5.0	-1.54	20.00	13	V	5.0
1935	(8+9)-VIII-2	4392	11.34	32.00	2.8	2.75	20.00	7.3	V	2.8
1935	(8+9)-VIII-3	-4442	-11.47	32.00	2.8	-2.78	20.00	7.2	V	2.8
1935	(8+9)-I-3	-3588	-9.27	32.00	3.5	-2.24	20.00	8.9	V	3.5

Setto 41: origine (1525.8,1738.6,193.5), direzione (-0.199392,0.97992,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	1	-461	-16	411	-0.16	-0.22	0.23	79.20	115.20	115.20	>100
0	2	-950	-34	862	-0.34	-0.46	0.48	118.80	172.80	172.80	>100
0	3	-950	-34	862	-0.34	-0.46	0.48	118.80	172.80	172.80	>100

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	4	-461	-16	411	-0.16	-0.22	0.23	105.60	153.60	153.60	>100
0	5	-461	-16	411	-0.16	-0.22	0.23	105.60	153.60	153.60	>100
0	6	-461	-16	411	-0.16	-0.22	0.23	105.60	153.60	153.60	>100
0	7	-461	-16	411	-0.16	-0.22	0.23	105.60	153.60	153.60	>100
0	(8+9)-VIII-4	1076	-25	-1119	0.38	-0.34	-0.62	132.00	192.00	192.00	>100
0	(8+9)-IV-1	-1828	4	1841	-0.65	0.06	1.02	132.00	192.00	192.00	>100
0	(8+9)-V-1	577	9	-933	0.21	0.13	-0.51	132.00	192.00	192.00	>100
0	(8+9)-I-2	1541	9	-1844	0.55	0.12	-1.02	132.00	192.00	192.00	99
0	(8+9)-V-2	1992	6	-2422	0.71	0.08	-1.34	132.00	192.00	192.00	79
0	(8+9)-I-4	-742	-35	903	-0.26	-0.46	0.50	132.00	192.00	192.00	>100
0	(8+9)-V-3	-2608	-28	2970	-0.93	-0.37	1.64	132.00	192.00	192.00	95
0	(8+9)-II-2	2393	-11	-2619	0.85	-0.14	-1.45	132.00	192.00	192.00	68
0	(8+9)-V-4	-1193	-31	1482	-0.42	-0.42	0.82	132.00	192.00	192.00	>100
0	(8+9)-II-4	1708	-24	-1795	0.61	-0.32	-0.99	132.00	192.00	192.00	88
0	(8+9)-VI-1	-2189	1	2170	-0.78	0.01	1.20	132.00	192.00	192.00	>100
0	(8+9)-III-2	1392	8	-1693	0.50	0.11	-0.93	132.00	192.00	192.00	>100
0	(8+9)-VI-2	2528	-12	-2793	0.90	-0.16	-1.54	132.00	192.00	192.00	64
0	(8+9)-III-4	-891	-35	1054	-0.32	-0.47	0.58	132.00	192.00	192.00	>100
0	(8+9)-VI-3	-3145	-10	3341	-1.12	-0.14	1.84	132.00	192.00	192.00	96
0	(8+9)-IV-2	1897	-13	-2117	0.68	-0.18	-1.17	132.00	192.00	192.00	82
0	(8+9)-VI-4	1573	-23	-1622	0.56	-0.30	-0.89	132.00	192.00	192.00	95
0	(8+9)-IV-4	1212	-26	-1293	0.43	-0.35	-0.71	132.00	192.00	192.00	>100
0	(8+9)-VII-1	726	10	-1084	0.26	0.14	-0.60	132.00	192.00	192.00	>100
0	(8+9)-II-1	-2324	2	2344	-0.83	0.02	1.29	132.00	192.00	192.00	>100
0	(8+9)-VII-2	1843	5	-2271	0.66	0.07	-1.25	132.00	192.00	192.00	84
0	(8+9)-III-1	275	13	-506	0.10	0.18	-0.28	132.00	192.00	192.00	>100
0	(8+9)-VII-3	-2459	-27	2820	-0.88	-0.36	1.56	132.00	192.00	192.00	100
0	(8+9)-I-1	126	12	-355	0.04	0.17	-0.20	132.00	192.00	192.00	>100
0	(8+9)-VII-4	-1342	-32	1632	-0.48	-0.43	0.90	132.00	192.00	192.00	>100
0	(8+9)-III-3	-2009	-30	2241	-0.71	-0.40	1.24	132.00	192.00	192.00	>100
0	(8+9)-IV-3	-2513	-9	2665	-0.89	-0.12	1.47	132.00	192.00	192.00	>100
0	(8+9)-II-3	-3009	-11	3168	-1.07	-0.15	1.75	132.00	192.00	192.00	>100
0	(8+9)-VIII-1	-1693	3	1668	-0.60	0.04	0.92	132.00	192.00	192.00	>100
0	(8+9)-VIII-2	2032	-14	-2290	0.72	-0.19	-1.26	132.00	192.00	192.00	77
0	(8+9)-VIII-3	-2648	-8	2839	-0.94	-0.11	1.57	132.00	192.00	192.00	>100
0	(8+9)-I-3	-2157	-31	2392	-0.77	-0.41	1.32	132.00	192.00	192.00	>100
Verifiche nella direzione secondaria											
0	1	-926	5	13	-6.38	1.98	1.72	79.20	115.20	115.20	28
0	4	-926	5	13	-6.38	1.98	1.72	105.60	153.60	153.60	39
0	5	-926	5	13	-6.38	1.98	1.72	105.60	153.60	153.60	39
0	6	-926	5	13	-6.38	1.98	1.72	105.60	153.60	153.60	39
0	7	-926	5	13	-6.38	1.98	1.72	105.60	153.60	153.60	39
0	(8+9)-VIII-4	-960	5	406	-6.61	2.00	55.91	132.00	192.00	192.00	3.3
0	(8+9)-IV-2	-1231	-5	692	-8.47	-2.01	95.29	132.00	192.00	192.00	2.0
0	(8+9)-V-1	-1055	-7	362	-7.26	-2.80	49.88	132.00	192.00	192.00	3.6
0	(8+9)-I-1	-827	-18	205	-5.69	-7.21	28.22	132.00	192.00	192.00	5.4
0	(8+9)-V-2	-1396	-9	767	-9.62	-3.49	105.60	132.00	192.00	192.00	1.8
0	(8+9)-I-3	-154	27	-591	-1.06	10.57	-81.41	132.00	192.00	192.00	2.1
0	(8+9)-V-3	74	16	-748	0.51	6.16	-103.08	132.00	192.00	192.00	1.7
0	(8+9)-II-1	-193	-0	-546	-1.33	-0.18	-75.16	132.00	192.00	192.00	2.5
0	(8+9)-V-4	-267	14	-344	-1.84	5.48	-47.35	132.00	192.00	192.00	3.6
0	(8+9)-II-3	9	13	-784	0.06	5.15	-108.05	132.00	192.00	192.00	1.7
0	(8+9)-VI-1	-261	3	-499	-1.80	1.14	-68.66	132.00	192.00	192.00	2.7
0	(8+9)-III-1	-857	-19	238	-5.90	-7.35	32.80	132.00	192.00	192.00	4.8
0	(8+9)-VI-2	-1399	-3	850	-9.64	-1.15	117.08	132.00	192.00	192.00	1.6
0	(8+9)-III-3	-184	26	-558	-1.27	10.43	-76.83	132.00	192.00	192.00	2.2
0	(8+9)-VI-3	77	10	-832	0.53	3.83	-114.55	132.00	192.00	192.00	1.6
0	(8+9)-IV-1	-293	-2	-435	-2.02	-0.65	-59.88	132.00	192.00	192.00	3.2
0	(8+9)-VI-4	-1061	4	517	-7.31	1.54	71.19	132.00	192.00	192.00	2.6
0	(8+9)-IV-3	-91	12	-674	-0.63	4.69	-92.77	132.00	192.00	192.00	2.0
0	(8+9)-VII-1	-1085	-7	395	-7.47	-2.94	54.46	132.00	192.00	192.00	3.3
0	(8+9)-I-2	-1168	-20	609	-8.04	-7.89	83.94	132.00	192.00	192.00	2.1
0	(8+9)-VII-2	-1366	-9	733	-9.41	-3.35	101.02	132.00	192.00	192.00	1.8
0	(8+9)-II-2	-1331	-6	803	-9.17	-2.47	110.58	132.00	192.00	192.00	1.7

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-VII-3	44	15	-715	0.30	6.03	-98.49	132.00	192.00	192.00	1.8
0	(8+9)-III-2	-1138	-20	576	-7.84	-7.76	79.35	132.00	192.00	192.00	2.2
0	(8+9)-VIII-3	-23	9	-721	-0.16	3.37	-99.27	132.00	192.00	192.00	1.9
0	(8+9)-III-4	-465	25	-220	-3.20	10.02	-30.28	132.00	192.00	192.00	4.8
0	(8+9)-I-4	-495	25	-187	-3.41	9.88	-25.69	132.00	192.00	192.00	5.4
0	(8+9)-II-4	-1129	7	564	-7.78	2.86	77.69	132.00	192.00	192.00	2.4
0	(8+9)-IV-4	-1029	8	453	-7.08	3.32	62.41	132.00	192.00	192.00	2.9
0	(8+9)-VII-4	-237	14	-377	-1.63	5.62	-51.94	132.00	192.00	192.00	3.3
0	(8+9)-VIII-1	-362	2	-388	-2.49	0.68	-53.38	132.00	192.00	192.00	3.5
0	(8+9)-VIII-2	-1299	-2	739	-8.95	-0.69	101.79	132.00	192.00	192.00	1.9
3870	2	-48	-14	-20	-0.33	-5.46	-2.79	118.80	172.80	172.80	21
3870	3	-48	-14	-20	-0.33	-5.46	-2.79	118.80	172.80	172.80	21

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
0	(8+9)-IV-1	17	0.00	6.40	Si	>100
0	(8+9)-VIII-1	15	0.00	6.40	Si	>100
0	(8+9)-VI-1	18	0.00	6.40	Si	>100
0	(8+9)-II-1	20	0.01	6.40	Si	>100
150	(8+9)-VIII-4	14	0.00	6.40	Si	>100
150	(8+9)-VII-2	-28	0.01	6.40	Si	>100
150	(8+9)-VII-4	45	0.01	6.40	Si	>100
150	(8+9)-IV-4	10	0.00	6.40	Si	>100
150	(8+9)-IV-2	-4	0.00	6.40	Si	>100
150	(8+9)-I-1	-10	0.00	6.40	Si	>100
150	(8+9)-IV-3	26	0.01	6.40	Si	>100
150	(8+9)-I-3	38	0.01	6.40	Si	>100
150	(8+9)-VIII-2	-8	0.00	6.40	Si	>100
150	(8+9)-V-1	-23	0.01	6.40	Si	>100
150	(8+9)-II-3	29	0.01	6.40	Si	>100
150	(8+9)-V-2	-29	0.01	6.40	Si	>100
150	(8+9)-III-1	-11	0.00	6.40	Si	>100
150	(8+9)-V-3	51	0.01	6.40	Si	>100
150	(8+9)-III-3	37	0.01	6.40	Si	>100
150	(8+9)-V-4	44	0.01	6.40	Si	>100
150	(8+9)-VIII-3	29	0.01	6.40	Si	>100
150	(8+9)-VII-3	50	0.01	6.40	Si	>100
150	(8+9)-I-4	31	0.01	6.40	Si	>100
150	(8+9)-VI-2	-12	0.00	6.40	Si	>100
150	(8+9)-II-4	7	0.00	6.40	Si	>100
150	(8+9)-III-4	32	0.01	6.40	Si	>100
150	(8+9)-I-2	-17	0.00	6.40	Si	>100
150	(8+9)-II-2	-8	0.00	6.40	Si	>100
150	(8+9)-III-2	-16	0.00	6.40	Si	>100
150	(8+9)-VI-3	33	0.01	6.40	Si	>100
150	(8+9)-VI-4	10	0.00	6.40	Si	>100
150	(8+9)-VII-1	-24	0.01	6.40	Si	>100
300	1	16	0.00	3.84	Si	>100
300	2	34	0.01	5.76	Si	>100
300	3	34	0.01	5.76	Si	>100
300	4	16	0.00	5.12	Si	>100
300	5	16	0.00	5.12	Si	>100
300	6	16	0.00	5.12	Si	>100
300	7	16	0.00	5.12	Si	>100
Verifiche nella direzione secondaria						
0	1	-8	0.05	3.84	Si	77
0	2	-16	0.10	5.76	Si	55
0	3	-16	0.10	5.76	Si	55
0	4	-8	0.05	5.12	Si	>100
0	5	-8	0.05	5.12	Si	>100
0	6	-8	0.05	5.12	Si	>100
0	7	-8	0.05	5.12	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
0	(8+9)-V-3	-11	0.07	6.40	Si	88
0	(8+9)-II-3	-13	0.08	6.40	Si	78
0	(8+9)-III-3	-10	0.07	6.40	Si	98
0	(8+9)-VIII-1	-10	0.06	6.40	Si	>100
0	(8+9)-III-4	-7	0.04	6.40	Si	>100
0	(8+9)-I-4	-7	0.04	6.40	Si	>100
0	(8+9)-IV-1	-10	0.06	6.40	Si	>100
0	(8+9)-II-2	2	0.01	6.40	Si	>100
0	(8+9)-VII-4	-8	0.05	6.40	Si	>100
0	(8+9)-IV-3	-12	0.08	6.40	Si	84
0	(8+9)-VI-3	-13	0.08	6.40	Si	77
0	(8+9)-II-1	-11	0.07	6.40	Si	92
0	(8+9)-VIII-3	-12	0.08	6.40	Si	83
0	(8+9)-VII-3	-11	0.07	6.40	Si	90
0	(8+9)-I-3	-11	0.07	6.40	Si	95
0	(8+9)-VI-2	2	0.01	6.40	Si	>100
0	(8+9)-VI-1	-11	0.07	6.40	Si	94
0	(8+9)-V-4	-8	0.05	6.40	Si	>100
1935	(8+9)-VIII-4	-1	0.01	6.40	Si	>100
1935	(8+9)-VII-1	-3	0.02	6.40	Si	>100
1935	(8+9)-V-1	-4	0.02	6.40	Si	>100
1935	(8+9)-I-1	-4	0.03	6.40	Si	>100
1935	(8+9)-III-1	-4	0.03	6.40	Si	>100
3870	(8+9)-IV-2	2	0.01	6.40	Si	>100
3870	(8+9)-VII-2	3	0.02	6.40	Si	>100
3870	(8+9)-VI-4	1	0.01	6.40	Si	>100
3870	(8+9)-III-2	2	0.01	6.40	Si	>100
3870	(8+9)-II-4	1	0.01	6.40	Si	>100
3870	(8+9)-I-2	2	0.01	6.40	Si	>100
3870	(8+9)-VIII-2	2	0.01	6.40	Si	>100
3870	(8+9)-IV-4	1	0.01	6.40	Si	>100
3870	(8+9)-V-2	3	0.02	6.40	Si	>100

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	1	-178	-0.09	19.20	>100	-0.02	12.00	>100	V	>100
0	2	-287	-0.15	28.80	>100	-0.04	18.00	>100	V	>100
0	3	-287	-0.15	28.80	>100	-0.04	18.00	>100	V	>100
0	4	-178	-0.09	25.60	>100	-0.02	16.00	>100	V	>100
0	5	-178	-0.09	25.60	>100	-0.02	16.00	>100	V	>100
0	6	-178	-0.09	25.60	>100	-0.02	16.00	>100	V	>100
0	7	-178	-0.09	25.60	>100	-0.02	16.00	>100	V	>100
0	(8+9)-IV-3	6352	3.39	32.00	9.4	0.82	20.00	24	V	9.4
0	(8+9)-VIII-1	3948	2.11	32.00	15	0.51	20.00	39	V	15
0	(8+9)-I-1	-2083	-1.11	32.00	29	-0.27	20.00	74	V	29
0	(8+9)-I-2	-5881	-3.14	32.00	10	-0.76	20.00	26	V	10
0	(8+9)-IV-4	-4295	-2.29	32.00	14	-0.55	20.00	36	V	14
0	(8+9)-I-4	1827	0.98	32.00	33	0.24	20.00	85	V	33
0	(8+9)-II-2	-7614	-4.06	32.00	7.9	-0.98	20.00	20	V	7.9
0	(8+9)-VI-2	-7705	-4.11	32.00	7.8	-1.00	20.00	20	V	7.8
0	(8+9)-I-3	5625	3.00	32.00	11	0.73	20.00	28	V	11
0	(8+9)-II-4	-5301	-2.83	32.00	11	-0.68	20.00	29	V	11
0	(8+9)-II-1	5046	2.69	32.00	12	0.65	20.00	31	V	12
0	(8+9)-III-2	-5579	-2.98	32.00	11	-0.72	20.00	28	V	11
0	(8+9)-II-3	7358	3.93	32.00	8.1	0.95	20.00	21	V	8.1
0	(8+9)-III-4	2129	1.14	32.00	28	0.28	20.00	73	V	28
0	(8+9)-IV-2	-6608	-3.53	32.00	9.1	-0.85	20.00	23	V	9.1
0	(8+9)-III-3	5323	2.84	32.00	11	0.69	20.00	29	V	11
0	(8+9)-IV-1	4040	2.16	32.00	15	0.52	20.00	38	V	15
0	(8+9)-III-1	-2385	-1.27	32.00	25	-0.31	20.00	65	V	25
0	(8+9)-VI-4	-5210	-2.78	32.00	12	-0.67	20.00	30	V	12
0	(8+9)-VIII-4	-4204	-2.24	32.00	14	-0.54	20.00	37	V	14

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
0	(8+9)-VI-1	4954	2.65	32.00	12	0.64	20.00	31	V	12
150	(8+9)-V-1	-4086	-2.18	32.00	15	-0.53	20.00	38	V	15
150	(8+9)-VIII-2	-6720	-3.59	32.00	8.9	-0.87	20.00	23	V	8.9
150	(8+9)-V-2	-7600	-4.06	32.00	7.9	-0.98	20.00	20	V	7.9
150	(8+9)-VII-1	-4371	-2.33	32.00	14	-0.56	20.00	35	V	14
150	(8+9)-VII-2	-7315	-3.91	32.00	8.2	-0.95	20.00	21	V	8.2
300	(8+9)-V-3	7434	3.97	32.00	8.1	0.96	20.00	21	V	8.1
300	(8+9)-VII-4	4212	2.25	32.00	14	0.54	20.00	37	V	14
300	(8+9)-VII-3	7149	3.82	32.00	8.4	0.92	20.00	22	V	8.4
300	(8+9)-VI-3	7505	4.01	32.00	8.0	0.97	20.00	21	V	8.0
300	(8+9)-VIII-3	6556	3.50	32.00	9.1	0.85	20.00	24	V	9.1
300	(8+9)-V-4	3927	2.10	32.00	15	0.51	20.00	39	V	15
Verifiche nella direzione secondaria										
0	2	11	0.07	28.80	>100	0.02	18.00	>100	V	>100
0	3	11	0.07	28.80	>100	0.02	18.00	>100	V	>100
3870	1	8	0.05	19.20	>100	0.01	12.00	>100	V	>100
3870	4	8	0.05	25.60	>100	0.01	16.00	>100	V	>100
3870	5	8	0.05	25.60	>100	0.01	16.00	>100	V	>100
3870	6	8	0.05	25.60	>100	0.01	16.00	>100	V	>100
3870	7	8	0.05	25.60	>100	0.01	16.00	>100	V	>100
3870	(8+9)-VIII-4	847	5.83	32.00	5.5	1.41	20.00	14	V	5.5
3870	(8+9)-IV-3	-1412	-9.73	32.00	3.3	-2.35	20.00	8.5	V	3.3
3870	(8+9)-V-1	716	4.93	32.00	6.5	1.19	20.00	17	V	6.5
3870	(8+9)-I-2	1212	8.35	32.00	3.8	2.02	20.00	9.9	V	3.8
3870	(8+9)-V-2	1557	10.72	32.00	3.0	2.59	20.00	7.7	V	3.0
3870	(8+9)-I-4	-361	-2.49	32.00	13	-0.60	20.00	33	V	13
3870	(8+9)-V-3	-1547	-10.65	32.00	3.0	-2.58	20.00	7.8	V	3.0
3870	(8+9)-II-2	1642	11.31	32.00	2.8	2.74	20.00	7.3	V	2.8
3870	(8+9)-V-4	-706	-4.86	32.00	6.6	-1.18	20.00	17	V	6.6
3870	(8+9)-II-4	1170	8.06	32.00	4.0	1.95	20.00	10	V	4.0
3870	(8+9)-VI-1	-1057	-7.28	32.00	4.4	-1.76	20.00	11	V	4.4
3870	(8+9)-III-2	1146	7.89	32.00	4.1	1.91	20.00	10	V	4.1
3870	(8+9)-VI-2	1745	12.02	32.00	2.7	2.91	20.00	6.9	V	2.7
3870	(8+9)-III-4	-427	-2.94	32.00	11	-0.71	20.00	28	V	11
3870	(8+9)-VI-3	-1735	-11.95	32.00	2.7	-2.89	20.00	6.9	V	2.7
3870	(8+9)-IV-2	1422	9.79	32.00	3.3	2.37	20.00	8.4	V	3.3
3870	(8+9)-VI-4	1067	7.35	32.00	4.4	1.78	20.00	11	V	4.4
3870	(8+9)-IV-4	950	6.54	32.00	4.9	1.58	20.00	13	V	4.9
3870	(8+9)-VII-1	782	5.39	32.00	5.9	1.30	20.00	15	V	5.9
3870	(8+9)-II-1	-1160	-7.99	32.00	4.0	-1.93	20.00	10	V	4.0
3870	(8+9)-VII-2	1491	10.27	32.00	3.1	2.48	20.00	8.0	V	3.1
3870	(8+9)-III-1	437	3.01	32.00	11	0.73	20.00	27	V	11
3870	(8+9)-VII-3	-1481	-10.20	32.00	3.1	-2.47	20.00	8.1	V	3.1
3870	(8+9)-IV-1	-940	-6.47	32.00	4.9	-1.57	20.00	13	V	4.9
3870	(8+9)-VII-4	-772	-5.32	32.00	6.0	-1.29	20.00	16	V	6.0
3870	(8+9)-III-3	-1136	-7.82	32.00	4.1	-1.89	20.00	11	V	4.1
3870	(8+9)-I-1	371	2.56	32.00	13	0.62	20.00	32	V	13
3870	(8+9)-II-3	-1632	-11.24	32.00	2.8	-2.72	20.00	7.4	V	2.8
3870	(8+9)-VIII-1	-837	-5.76	32.00	5.6	-1.39	20.00	14	V	5.6
3870	(8+9)-VIII-2	1526	10.51	32.00	3.0	2.54	20.00	7.9	V	3.0
3870	(8+9)-VIII-3	-1516	-10.44	32.00	3.1	-2.53	20.00	7.9	V	3.1
3870	(8+9)-I-3	-1202	-8.28	32.00	3.9	-2.00	20.00	10.0	V	3.9

Setto 42: origine (1579.6,1474.1,193.5), direzione (-0.199392,0.97992,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	1	181	-2	-316	0.06	-0.02	-0.17	79.20	115.20	115.20	>100
0	2	478	-3	-721	0.17	-0.04	-0.40	118.80	172.80	172.80	>100
0	3	478	-3	-721	0.17	-0.04	-0.40	118.80	172.80	172.80	>100
0	4	181	-2	-316	0.06	-0.02	-0.17	105.60	153.60	153.60	>100
0	5	181	-2	-316	0.06	-0.02	-0.17	105.60	153.60	153.60	>100
0	6	181	-2	-316	0.06	-0.02	-0.17	105.60	153.60	153.60	>100

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	7	181	-2	-316	0.06	-0.02	-0.17	105.60	153.60	153.60	>100
0	(8+9)-IV-1	3470	-0	-2689	1.24	-0.01	-1.48	132.00	192.00	192.00	58
0	(8+9)-VI-1	3711	3	-2791	1.32	0.04	-1.54	132.00	192.00	192.00	55
0	(8+9)-III-4	1634	24	-1304	0.58	0.32	-0.72	132.00	192.00	192.00	>100
0	(8+9)-V-1	-2461	-29	1754	-0.88	-0.38	0.97	132.00	192.00	192.00	>100
0	(8+9)-I-4	1446	23	-1182	0.51	0.30	-0.65	132.00	192.00	192.00	>100
0	(8+9)-VII-3	5408	33	-4165	1.92	0.45	-2.30	132.00	192.00	192.00	35
0	(8+9)-VIII-3	5504	17	-4195	1.96	0.23	-2.31	132.00	192.00	192.00	36
0	(8+9)-IV-3	5122	16	-3888	1.82	0.22	-2.15	132.00	192.00	192.00	38
0	(8+9)-VIII-1	3087	-2	-2382	1.10	-0.02	-1.31	132.00	192.00	192.00	65
0	(8+9)-VII-1	-2648	-30	1877	-0.94	-0.40	1.04	132.00	192.00	192.00	>100
0	(8+9)-VII-4	2909	28	-2327	1.04	0.37	-1.28	132.00	192.00	192.00	61
0	(8+9)-I-3	4320	31	-3265	1.54	0.41	-1.80	132.00	192.00	192.00	43
0	(8+9)-II-1	4094	4	-3098	1.46	0.06	-1.71	132.00	192.00	192.00	49
0	(8+9)-II-3	5745	21	-4297	2.04	0.28	-2.37	132.00	192.00	192.00	34
0	(8+9)-V-4	2722	27	-2205	0.97	0.35	-1.22	132.00	192.00	192.00	64
0	(8+9)-III-3	4133	30	-3142	1.47	0.40	-1.73	132.00	192.00	192.00	45
0	(8+9)-V-3	5595	35	-4288	1.99	0.46	-2.37	132.00	192.00	192.00	34
0	(8+9)-VI-3	6128	22	-4603	2.18	0.30	-2.54	132.00	192.00	192.00	32
150	(8+9)-I-1	-1090	-25	769	-0.39	-0.33	0.42	132.00	192.00	192.00	>100
150	(8+9)-III-1	-1238	-26	870	-0.44	-0.35	0.48	132.00	192.00	192.00	>100
300	(8+9)-VIII-4	-2386	-7	2269	-0.85	-0.10	1.25	132.00	192.00	192.00	>100
300	(8+9)-I-2	-3345	-28	3134	-1.19	-0.38	1.73	132.00	192.00	192.00	91
300	(8+9)-IV-2	-4058	-22	3854	-1.44	-0.29	2.13	132.00	192.00	192.00	79
300	(8+9)-VI-2	-4874	-27	4620	-1.73	-0.36	2.55	132.00	192.00	192.00	66
300	(8+9)-III-2	-3201	-27	2993	-1.14	-0.36	1.65	132.00	192.00	192.00	95
300	(8+9)-VII-2	-4320	-32	3986	-1.54	-0.43	2.20	132.00	192.00	192.00	73
300	(8+9)-V-2	-4464	-33	4126	-1.59	-0.44	2.28	132.00	192.00	192.00	70
300	(8+9)-IV-4	-2722	-9	2567	-0.97	-0.12	1.42	132.00	192.00	192.00	>100
300	(8+9)-II-4	-3202	-13	3035	-1.14	-0.17	1.67	132.00	192.00	192.00	>100
300	(8+9)-VIII-2	-4394	-23	4152	-1.56	-0.31	2.29	132.00	192.00	192.00	73
300	(8+9)-II-2	-4538	-26	4322	-1.62	-0.34	2.39	132.00	192.00	192.00	70
300	(8+9)-VI-4	-2866	-11	2737	-1.02	-0.15	1.51	132.00	192.00	192.00	>100
Verifiche nella direzione secondaria											
0	(8+9)-VIII-4	-642	-18	374	-4.42	-6.93	51.51	132.00	192.00	192.00	3.3
0	(8+9)-VII-2	-397	18	743	-2.73	7.02	102.32	132.00	192.00	192.00	1.8
0	(8+9)-III-3	-1689	15	-556	-11.63	5.81	-76.61	132.00	192.00	192.00	2.3
0	(8+9)-IV-2	-366	-15	662	-2.52	-5.84	91.23	132.00	192.00	192.00	2.0
0	(8+9)-III-4	-1319	9	-218	-9.09	3.38	-30.09	132.00	192.00	192.00	5.7
0	(8+9)-VIII-2	-330	-5	726	-2.27	-1.80	100.01	132.00	192.00	192.00	1.9
0	(8+9)-IV-1	-1598	6	-463	-11.01	2.27	-63.84	132.00	192.00	192.00	2.9
0	(8+9)-VII-4	-1438	-26	-431	-9.91	-10.08	-59.35	132.00	192.00	192.00	2.7
0	(8+9)-I-1	-933	-13	159	-6.43	-5.09	21.96	132.00	192.00	192.00	7.0
0	(8+9)-IV-3	-1839	13	-688	-12.67	5.21	-94.78	132.00	192.00	192.00	1.9
0	(8+9)-I-3	-1737	12	-589	-11.96	4.73	-81.18	132.00	192.00	192.00	2.2
0	(8+9)-IV-4	-607	-7	438	-4.18	-2.89	60.29	132.00	192.00	192.00	3.0
0	(8+9)-II-1	-1758	-3	-574	-12.10	-1.34	-79.09	132.00	192.00	192.00	2.4
0	(8+9)-V-1	-814	21	372	-5.61	8.37	51.23	132.00	192.00	192.00	3.2
0	(8+9)-II-3	-1999	4	-799	-13.77	1.61	-110.04	132.00	192.00	192.00	1.7
0	(8+9)-V-2	-349	21	776	-2.40	8.11	106.90	132.00	192.00	192.00	1.7
0	(8+9)-III-1	-885	-10	193	-6.10	-4.01	26.54	132.00	192.00	192.00	6.2
0	(8+9)-V-3	-1856	-22	-802	-12.78	-8.73	-110.45	132.00	192.00	192.00	1.6
0	(8+9)-VIII-3	-1875	3	-752	-12.91	1.18	-103.56	132.00	192.00	192.00	1.8
0	(8+9)-V-4	-1390	-23	-398	-9.58	-9.00	-54.77	132.00	192.00	192.00	3.0
0	(8+9)-VII-3	-1808	-19	-769	-12.45	-7.65	-105.87	132.00	192.00	192.00	1.7
0	(8+9)-VI-1	-1722	7	-510	-11.86	2.70	-70.31	132.00	192.00	192.00	2.6
0	(8+9)-I-4	-1272	11	-185	-8.76	4.46	-25.51	132.00	192.00	192.00	6.3
0	(8+9)-VI-2	-170	5	837	-1.17	1.81	115.27	132.00	192.00	192.00	1.6
0	(8+9)-II-4	-447	2	548	-3.08	0.72	75.54	132.00	192.00	192.00	2.5
0	(8+9)-VIII-1	-1562	16	-400	-10.76	6.31	-55.06	132.00	192.00	192.00	3.1
0	(8+9)-I-2	-468	-14	564	-3.22	-5.36	77.63	132.00	192.00	192.00	2.3
0	(8+9)-II-2	-206	-6	773	-1.42	-2.23	106.49	132.00	192.00	192.00	1.8
0	(8+9)-III-2	-516	-16	530	-3.55	-6.44	73.06	132.00	192.00	192.00	2.4
0	(8+9)-VI-3	-2034	-6	-863	-14.01	-2.43	-118.82	132.00	192.00	192.00	1.6

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-VI-4	-483	-8	485	-3.33	-3.32	66.76	132.00	192.00	192.00	2.7
0	(8+9)-VII-1	-766	24	405	-5.28	9.46	55.80	132.00	192.00	192.00	2.9
3870	1	-414	-1	71	-2.85	-0.53	9.76	79.20	115.20	115.20	11
3870	2	-855	-3	146	-5.89	-1.08	20.16	118.80	172.80	172.80	8.1
3870	3	-855	-3	146	-5.89	-1.08	20.16	118.80	172.80	172.80	8.1
3870	4	-414	-1	71	-2.85	-0.53	9.76	105.60	153.60	153.60	15
3870	5	-414	-1	71	-2.85	-0.53	9.76	105.60	153.60	153.60	15
3870	6	-414	-1	71	-2.85	-0.53	9.76	105.60	153.60	153.60	15
3870	7	-414	-1	71	-2.85	-0.53	9.76	105.60	153.60	153.60	15

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Ty kg	τ_d kg/cmq	fvd kg/cmq	RS	Cs
0	1	2	0.00	3.84	Si	>100
0	2	4	0.00	5.76	Si	>100
0	3	4	0.00	5.76	Si	>100
0	4	2	0.00	5.12	Si	>100
0	5	2	0.00	5.12	Si	>100
0	6	2	0.00	5.12	Si	>100
0	7	2	0.00	5.12	Si	>100
0	(8+9)-VIII-4	-20	0.01	6.40	Si	>100
0	(8+9)-IV-1	20	0.01	6.40	Si	>100
0	(8+9)-V-1	24	0.01	6.40	Si	>100
0	(8+9)-V-2	9	0.00	6.40	Si	>100
0	(8+9)-I-4	-12	0.00	6.40	Si	>100
0	(8+9)-V-3	-7	0.00	6.40	Si	>100
0	(8+9)-II-2	-21	0.01	6.40	Si	>100
0	(8+9)-V-4	-21	0.01	6.40	Si	>100
0	(8+9)-II-4	-24	0.01	6.40	Si	>100
0	(8+9)-VII-2	12	0.00	6.40	Si	>100
0	(8+9)-II-1	27	0.01	6.40	Si	>100
0	(8+9)-VI-1	30	0.01	6.40	Si	>100
0	(8+9)-II-3	23	0.01	6.40	Si	>100
0	(8+9)-VIII-1	22	0.01	6.40	Si	>100
0	(8+9)-III-1	12	0.00	6.40	Si	>100
0	(8+9)-VII-4	-19	0.00	6.40	Si	>100
0	(8+9)-VII-3	-9	0.00	6.40	Si	>100
0	(8+9)-VI-2	-18	0.00	6.40	Si	>100
0	(8+9)-VIII-3	13	0.00	6.40	Si	>100
0	(8+9)-IV-3	16	0.00	6.40	Si	>100
0	(8+9)-I-3	3	0.00	6.40	Si	>100
0	(8+9)-I-1	14	0.00	6.40	Si	>100
0	(8+9)-VI-3	20	0.01	6.40	Si	>100
0	(8+9)-VI-4	-27	0.01	6.40	Si	>100
0	(8+9)-VII-1	22	0.01	6.40	Si	>100
150	(8+9)-I-2	-3	0.00	6.40	Si	>100
150	(8+9)-III-2	-3	0.00	6.40	Si	>100
150	(8+9)-IV-2	-16	0.00	6.40	Si	>100
150	(8+9)-III-3	2	0.00	6.40	Si	>100
300	(8+9)-IV-4	-18	0.00	6.40	Si	>100
300	(8+9)-III-4	-11	0.00	6.40	Si	>100
300	(8+9)-VIII-2	-14	0.00	6.40	Si	>100
Verifiche nella direzione secondaria						
0	1	-8	0.05	3.84	Si	71
0	2	-18	0.11	5.76	Si	51
0	3	-18	0.11	5.76	Si	51
0	4	-8	0.05	5.12	Si	95
0	5	-8	0.05	5.12	Si	95
0	6	-8	0.05	5.12	Si	95
0	7	-8	0.05	5.12	Si	95
0	(8+9)-VIII-4	6	0.04	6.40	Si	>100
0	(8+9)-IV-3	-17	0.11	6.40	Si	59
0	(8+9)-V-2	-8	0.05	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
0	(8+9)-IV-2	5	0.03	6.40	Si	>100
0	(8+9)-I-4	-7	0.04	6.40	Si	>100
0	(8+9)-III-3	-12	0.07	6.40	Si	85
0	(8+9)-VIII-1	-17	0.11	6.40	Si	58
0	(8+9)-VII-1	-13	0.08	6.40	Si	78
0	(8+9)-VIII-3	-15	0.10	6.40	Si	67
0	(8+9)-VIII-2	3	0.02	6.40	Si	>100
0	(8+9)-VII-3	-5	0.03	6.40	Si	>100
0	(8+9)-III-4	-5	0.03	6.40	Si	>100
0	(8+9)-IV-1	-15	0.10	6.40	Si	65
0	(8+9)-IV-4	4	0.02	6.40	Si	>100
1935	(8+9)-V-1	-13	0.08	6.40	Si	75
1935	(8+9)-VI-4	6	0.04	6.40	Si	>100
1935	(8+9)-I-1	-7	0.05	6.40	Si	>100
1935	(8+9)-II-4	4	0.03	6.40	Si	>100
1935	(8+9)-III-1	-7	0.04	6.40	Si	>100
1935	(8+9)-II-2	5	0.03	6.40	Si	>100
1935	(8+9)-V-3	-5	0.03	6.40	Si	>100
1935	(8+9)-VI-2	4	0.02	6.40	Si	>100
1935	(8+9)-VI-3	-15	0.10	6.40	Si	66
1935	(8+9)-I-3	-11	0.07	6.40	Si	94
1935	(8+9)-VI-1	-18	0.11	6.40	Si	57
1935	(8+9)-II-1	-16	0.10	6.40	Si	63
1935	(8+9)-II-3	-17	0.11	6.40	Si	59
3870	(8+9)-VII-2	8	0.05	6.40	Si	>100
3870	(8+9)-I-2	4	0.02	6.40	Si	>100
3870	(8+9)-VII-4	-4	0.03	6.40	Si	>100
3870	(8+9)-III-2	4	0.02	6.40	Si	>100
3870	(8+9)-V-4	-4	0.03	6.40	Si	>100

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	(8+9)-VIII-4	-3729	-1.99	32.00	16	-0.48	20.00	42	V	16
0	(8+9)-III-1	-2176	-1.16	32.00	28	-0.28	20.00	71	V	28
0	(8+9)-I-1	-1875	-1.00	32.00	32	-0.24	20.00	83	V	32
0	(8+9)-VI-4	-4731	-2.53	32.00	13	-0.61	20.00	33	V	13
150	(8+9)-V-4	3872	2.07	32.00	15	0.50	20.00	40	V	15
150	(8+9)-II-3	7699	4.11	32.00	7.8	0.99	20.00	20	V	7.8
150	(8+9)-III-2	-5270	-2.81	32.00	11	-0.68	20.00	29	V	11
150	(8+9)-VII-2	-6883	-3.67	32.00	8.7	-0.89	20.00	22	V	8.7
150	(8+9)-III-3	5728	3.06	32.00	10	0.74	20.00	27	V	10
150	(8+9)-VII-3	7340	3.92	32.00	8.2	0.95	20.00	21	V	8.2
150	(8+9)-III-4	2568	1.37	32.00	23	0.33	20.00	60	V	23
150	(8+9)-I-3	6036	3.22	32.00	9.9	0.78	20.00	26	V	9.9
150	(8+9)-VII-4	4181	2.23	32.00	14	0.54	20.00	37	V	14
150	(8+9)-IV-2	-6213	-3.32	32.00	9.6	-0.80	20.00	25	V	9.6
150	(8+9)-VIII-2	-6697	-3.58	32.00	9.0	-0.87	20.00	23	V	9.0
150	(8+9)-IV-3	6671	3.56	32.00	9.0	0.86	20.00	23	V	9.0
150	(8+9)-VIII-3	7155	3.82	32.00	8.4	0.92	20.00	22	V	8.4
150	(8+9)-VI-2	-7725	-4.12	32.00	7.8	-1.00	20.00	20	V	7.8
150	(8+9)-I-2	-5578	-2.98	32.00	11	-0.72	20.00	28	V	11
150	(8+9)-II-2	-7241	-3.87	32.00	8.3	-0.94	20.00	21	V	8.3
150	(8+9)-VI-3	8183	4.37	32.00	7.3	1.06	20.00	19	V	7.3
150	(8+9)-VII-1	-3723	-1.99	32.00	16	-0.48	20.00	42	V	16
150	(8+9)-I-4	2260	1.21	32.00	27	0.29	20.00	69	V	27
150	(8+9)-V-1	-3414	-1.82	32.00	18	-0.44	20.00	45	V	18
150	(8+9)-V-2	-7191	-3.84	32.00	8.3	-0.93	20.00	22	V	8.3
150	(8+9)-V-3	7649	4.08	32.00	7.8	0.99	20.00	20	V	7.8
300	1	369	0.20	19.20	97	0.05	12.00	>100	V	97
300	2	770	0.41	28.80	70	0.10	18.00	>100	V	70
300	3	770	0.41	28.80	70	0.10	18.00	>100	V	70
300	4	369	0.20	25.60	>100	0.05	16.00	>100	V	>100

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
300	5	369	0.20	25.60	>100	0.05	16.00	>100	V	>100
300	6	369	0.20	25.60	>100	0.05	16.00	>100	V	>100
300	7	369	0.20	25.60	>100	0.05	16.00	>100	V	>100
300	(8+9)-IV-1	4391	2.34	32.00	14	0.57	20.00	35	V	14
300	(8+9)-II-1	5419	2.89	32.00	11	0.70	20.00	29	V	11
300	(8+9)-VIII-1	3926	2.10	32.00	15	0.51	20.00	39	V	15
300	(8+9)-II-4	-4914	-2.62	32.00	12	-0.63	20.00	32	V	12
300	(8+9)-IV-4	-3886	-2.07	32.00	15	-0.50	20.00	40	V	15
300	(8+9)-VI-1	4953	2.64	32.00	12	0.64	20.00	31	V	12
Verifiche nella direzione secondaria										
3870	1	-164	-1.13	19.20	17	-0.27	12.00	44	V	17
3870	2	-350	-2.41	28.80	12	-0.58	18.00	31	V	12
3870	3	-350	-2.41	28.80	12	-0.58	18.00	31	V	12
3870	4	-164	-1.13	25.60	23	-0.27	16.00	58	V	23
3870	5	-164	-1.13	25.60	23	-0.27	16.00	58	V	23
3870	6	-164	-1.13	25.60	23	-0.27	16.00	58	V	23
3870	7	-164	-1.13	25.60	23	-0.27	16.00	58	V	23
3870	(8+9)-VIII-4	914	6.29	32.00	5.1	1.52	20.00	13	V	5.1
3870	(8+9)-IV-2	1544	10.64	32.00	3.0	2.57	20.00	7.8	V	3.0
3870	(8+9)-V-1	631	4.35	32.00	7.4	1.05	20.00	19	V	7.4
3870	(8+9)-I-2	1244	8.57	32.00	3.7	2.07	20.00	9.6	V	3.7
3870	(8+9)-V-2	1627	11.21	32.00	2.9	2.71	20.00	7.4	V	2.9
3870	(8+9)-I-4	-474	-3.26	32.00	9.8	-0.79	20.00	25	V	9.8
3870	(8+9)-V-3	-1853	-12.76	32.00	2.5	-3.09	20.00	6.5	V	2.5
3870	(8+9)-II-2	1805	12.43	32.00	2.6	3.01	20.00	6.6	V	2.6
3870	(8+9)-V-4	-857	-5.90	32.00	5.4	-1.43	20.00	14	V	5.4
3870	(8+9)-II-4	1289	8.88	32.00	3.6	2.15	20.00	9.3	V	3.6
3870	(8+9)-VI-1	-1400	-9.64	32.00	3.3	-2.33	20.00	8.6	V	3.3
3870	(8+9)-III-2	1166	8.03	32.00	4.0	1.94	20.00	10	V	4.0
3870	(8+9)-VI-2	1920	13.22	32.00	2.4	3.20	20.00	6.3	V	2.4
3870	(8+9)-III-4	-552	-3.80	32.00	8.4	-0.92	20.00	22	V	8.4
3870	(8+9)-VI-3	-2145	-14.77	32.00	2.2	-3.58	20.00	5.6	V	2.2
3870	(8+9)-I-1	249	1.71	32.00	19	0.41	20.00	48	V	19
3870	(8+9)-VI-4	1175	8.09	32.00	4.0	1.96	20.00	10	V	4.0
3870	(8+9)-IV-4	1029	7.09	32.00	4.5	1.71	20.00	12	V	4.5
3870	(8+9)-VII-1	709	4.89	32.00	6.5	1.18	20.00	17	V	6.5
3870	(8+9)-II-1	-1515	-10.43	32.00	3.1	-2.52	20.00	7.9	V	3.1
3870	(8+9)-VII-2	1549	10.67	32.00	3.0	2.58	20.00	7.7	V	3.0
3870	(8+9)-III-1	327	2.25	32.00	14	0.54	20.00	37	V	14
3870	(8+9)-VII-3	-1774	-12.22	32.00	2.6	-2.96	20.00	6.8	V	2.6
3870	(8+9)-IV-1	-1254	-8.64	32.00	3.7	-2.09	20.00	9.6	V	3.7
3870	(8+9)-VII-4	-935	-6.44	32.00	5.0	-1.56	20.00	13	V	5.0
3870	(8+9)-III-3	-1392	-9.58	32.00	3.3	-2.32	20.00	8.6	V	3.3
3870	(8+9)-IV-3	-1770	-12.19	32.00	2.6	-2.95	20.00	6.8	V	2.6
3870	(8+9)-II-3	-2030	-13.98	32.00	2.3	-3.38	20.00	5.9	V	2.3
3870	(8+9)-VIII-1	-1139	-7.85	32.00	4.1	-1.90	20.00	11	V	4.1
3870	(8+9)-VIII-2	1659	11.43	32.00	2.8	2.77	20.00	7.2	V	2.8
3870	(8+9)-VIII-3	-1884	-12.98	32.00	2.5	-3.14	20.00	6.4	V	2.5
3870	(8+9)-I-3	-1470	-10.12	32.00	3.2	-2.45	20.00	8.2	V	3.2

Setto 43: origine (1639.0,1182.0,193.5), direzione (-0.199392,0.97992,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	1	5527	-44	-9906	1.97	-0.58	-5.47	79.20	115.20	115.20	13
0	2	11617	-91	-20600	4.13	-1.22	-11.37	118.80	172.80	172.80	9.3
0	3	11617	-91	-20600	4.13	-1.22	-11.37	118.80	172.80	172.80	9.3
0	4	5527	-44	-9906	1.97	-0.58	-5.47	105.60	153.60	153.60	17
0	5	5527	-44	-9906	1.97	-0.58	-5.47	105.60	153.60	153.60	17
0	6	5527	-44	-9906	1.97	-0.58	-5.47	105.60	153.60	153.60	17
0	7	5527	-44	-9906	1.97	-0.58	-5.47	105.60	153.60	153.60	17
0	(8+9)-VIII-4	-2826	359	-3877	-1.01	4.80	-2.14	132.00	192.00	192.00	28
0	(8+9)-IV-1	11272	-427	-10036	4.01	-5.71	-5.54	132.00	192.00	192.00	11

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-V-1	-1497	-407	-5309	-0.53	-5.44	-2.93	132.00	192.00	192.00	23
0	(8+9)-I-2	-5206	-495	-3518	-1.85	-6.61	-1.94	132.00	192.00	192.00	22
0	(8+9)-I-4	6405	374	-7662	2.28	5.00	-4.23	132.00	192.00	192.00	15
0	(8+9)-VII-1	-1953	-517	-5194	-0.70	-6.91	-2.87	132.00	192.00	192.00	20
0	(8+9)-IV-4	-3643	367	-3659	-1.30	4.91	-2.02	132.00	192.00	192.00	28
0	(8+9)-I-3	12836	435	-10178	4.57	5.82	-5.62	132.00	192.00	192.00	11
0	(8+9)-VIII-3	15572	-175	-11496	5.54	-2.33	-6.34	132.00	192.00	192.00	11
0	(8+9)-VII-4	9583	457	-8501	3.41	6.11	-4.69	132.00	192.00	192.00	12
0	(8+9)-IV-3	14756	-166	-11279	5.25	-2.22	-6.22	132.00	192.00	192.00	12
0	(8+9)-III-4	6860	485	-7777	2.44	6.48	-4.29	132.00	192.00	192.00	13
0	(8+9)-I-1	1225	-434	-6033	0.44	-5.80	-3.33	132.00	192.00	192.00	20
0	(8+9)-VIII-1	10456	-419	-9819	3.72	-5.60	-5.42	132.00	192.00	192.00	12
0	(8+9)-VI-3	17092	193	-11879	6.08	2.59	-6.56	132.00	192.00	192.00	11
0	(8+9)-II-3	16275	202	-11662	5.79	2.70	-6.44	132.00	192.00	192.00	11
0	(8+9)-III-1	769	-544	-5918	0.27	-7.28	-3.27	132.00	192.00	192.00	18
0	(8+9)-III-2	-4750	-384	-3632	-1.69	-5.14	-2.00	132.00	192.00	192.00	27
290	(8+9)-V-3	15469	311	-14000	5.51	4.15	-7.73	132.00	192.00	192.00	9.7
290	(8+9)-V-4	9070	347	-9741	3.23	4.64	-5.38	132.00	192.00	192.00	13
290	(8+9)-VI-1	11944	-186	-12163	4.25	-2.48	-6.71	132.00	192.00	192.00	12
290	(8+9)-II-1	12669	-177	-12648	4.51	-2.36	-6.98	132.00	192.00	192.00	12
290	(8+9)-III-3	12608	261	-12071	4.49	3.49	-6.66	132.00	192.00	192.00	12
290	(8+9)-VII-3	15024	292	-13689	5.35	3.90	-7.55	132.00	192.00	192.00	10.0
580	(8+9)-V-2	-10614	-268	9096	-3.78	-3.59	5.02	132.00	192.00	192.00	22
580	(8+9)-VII-2	-10159	-243	8686	-3.62	-3.25	4.79	132.00	192.00	192.00	24
580	(8+9)-VI-4	-6821	89	5356	-2.43	1.19	2.96	132.00	192.00	192.00	46
580	(8+9)-VI-2	-12035	-67	10249	-4.28	-0.89	5.66	132.00	192.00	192.00	29
580	(8+9)-IV-2	-9610	8	7969	-3.42	0.11	4.40	132.00	192.00	192.00	42
580	(8+9)-VIII-2	-10520	17	8881	-3.74	0.22	4.90	132.00	192.00	192.00	37
580	(8+9)-II-4	-7731	97	6268	-2.75	1.30	3.46	132.00	192.00	192.00	40
580	(8+9)-II-2	-11125	-75	9337	-3.96	-1.01	5.15	132.00	192.00	192.00	31
Verifiche nella direzione secondaria											
0	(8+9)-VIII-4	4238	90	383	15.10	18.39	14.11	132.00	192.00	192.00	3.5
0	(8+9)-VII-2	2189	-240	1450	7.80	-49.00	53.45	132.00	192.00	192.00	1.7
0	(8+9)-III-3	-4204	172	-1344	-14.97	35.00	-49.51	132.00	192.00	192.00	2.2
0	(8+9)-IV-2	5043	-39	1070	17.96	-7.85	39.44	132.00	192.00	192.00	2.6
0	(8+9)-III-4	-492	189	-841	-1.75	38.48	-30.98	132.00	192.00	192.00	2.8
0	(8+9)-VIII-2	5291	-53	1146	18.85	-10.84	42.24	132.00	192.00	192.00	2.4
0	(8+9)-IV-1	-7331	-95	-606	-26.12	-19.45	-22.32	132.00	192.00	192.00	4.2
0	(8+9)-VII-4	-1321	238	-1094	-4.70	48.43	-40.32	132.00	192.00	192.00	2.2
0	(8+9)-I-1	-2867	-214	649	-10.21	-43.65	23.93	132.00	192.00	192.00	2.8
0	(8+9)-IV-3	-7887	19	-1217	-28.09	3.81	-44.85	132.00	192.00	192.00	3.6
0	(8+9)-I-3	-4719	166	-1388	-16.81	33.89	-51.16	132.00	192.00	192.00	2.2
0	(8+9)-IV-4	4487	76	459	15.98	15.41	16.91	132.00	192.00	192.00	3.5
0	(8+9)-II-1	-9048	-114	-755	-32.23	-23.18	-27.82	132.00	192.00	192.00	3.4
0	(8+9)-V-1	-2038	-263	903	-7.26	-53.60	33.27	132.00	192.00	192.00	2.2
0	(8+9)-II-3	-9603	0	-1366	-34.21	0.08	-50.35	132.00	192.00	192.00	3.4
0	(8+9)-V-2	2704	-235	1495	9.63	-47.88	55.10	132.00	192.00	192.00	1.6
0	(8+9)-III-1	-2352	-209	694	-8.38	-42.53	25.58	132.00	192.00	192.00	2.8
0	(8+9)-V-3	-5548	215	-1642	-19.76	43.84	-60.50	132.00	192.00	192.00	1.8
0	(8+9)-VIII-3	-8135	33	-1293	-28.98	6.79	-47.65	132.00	192.00	192.00	3.3
0	(8+9)-V-4	-806	243	-1049	-2.87	49.55	-38.67	132.00	192.00	192.00	2.2
0	(8+9)-VII-3	-5033	221	-1597	-17.93	44.95	-58.85	132.00	192.00	192.00	1.8
0	(8+9)-VI-1	-8799	-128	-679	-31.34	-26.16	-25.02	132.00	192.00	192.00	3.4
0	(8+9)-I-4	23	194	-796	0.08	39.60	-29.33	132.00	192.00	192.00	2.8
0	(8+9)-VI-2	7008	-35	1296	24.96	-7.11	47.74	132.00	192.00	192.00	2.1
0	(8+9)-II-4	6204	94	608	22.10	19.13	22.41	132.00	192.00	192.00	2.6
0	(8+9)-VIII-1	-7082	-110	-530	-25.23	-22.44	-19.52	132.00	192.00	192.00	4.2
0	(8+9)-I-2	1875	-186	1242	6.68	-37.93	45.75	132.00	192.00	192.00	2.1
0	(8+9)-II-2	6759	-20	1220	24.08	-4.13	44.94	132.00	192.00	192.00	2.3
0	(8+9)-III-2	1360	-192	1197	4.84	-39.05	44.10	132.00	192.00	192.00	2.1
0	(8+9)-VI-3	-9852	15	-1442	-35.10	3.07	-53.15	132.00	192.00	192.00	3.1
0	(8+9)-VI-4	5955	109	532	21.21	22.12	19.61	132.00	192.00	192.00	2.6
0	(8+9)-VII-1	-1523	-257	948	-5.43	-52.48	34.92	132.00	192.00	192.00	2.2
3870	1	-4819	42	53	-17.17	8.59	1.94	79.20	115.20	115.20	8.8

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
3870	2	-9902	90	100	-35.27	18.30	3.69	118.80	172.80	172.80	5.9
3870	3	-9902	90	100	-35.27	18.30	3.69	118.80	172.80	172.80	5.9
3870	4	-4819	42	53	-17.17	8.59	1.94	105.60	153.60	153.60	12
3870	5	-4819	42	53	-17.17	8.59	1.94	105.60	153.60	153.60	12
3870	6	-4819	42	53	-17.17	8.59	1.94	105.60	153.60	153.60	12
3870	7	-4819	42	53	-17.17	8.59	1.94	105.60	153.60	153.60	12

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
0	(8+9)-III-3	204	0.05	6.40	Si	>100
0	(8+9)-VI-3	150	0.04	6.40	Si	>100
0	(8+9)-I-3	223	0.06	6.40	Si	>100
0	(8+9)-III-4	196	0.05	6.40	Si	>100
0	(8+9)-IV-3	147	0.04	6.40	Si	>100
0	(8+9)-II-3	211	0.05	6.40	Si	>100
0	(8+9)-IV-4	120	0.03	6.40	Si	>100
0	(8+9)-VIII-3	86	0.02	6.40	Si	>100
0	(8+9)-I-4	177	0.05	6.40	Si	>100
290	1	152	0.04	3.84	Si	98
290	2	316	0.08	5.76	Si	70
290	3	316	0.08	5.76	Si	70
290	4	152	0.04	5.12	Si	>100
290	5	152	0.04	5.12	Si	>100
290	6	152	0.04	5.12	Si	>100
290	7	152	0.04	5.12	Si	>100
290	(8+9)-V-3	-238	0.06	6.40	Si	>100
290	(8+9)-VII-3	-282	0.07	6.40	Si	88
290	(8+9)-II-1	242	0.06	6.40	Si	>100
290	(8+9)-III-2	230	0.06	6.40	Si	>100
290	(8+9)-V-4	-300	0.08	6.40	Si	82
290	(8+9)-I-1	248	0.06	6.40	Si	100
290	(8+9)-VI-1	320	0.08	6.40	Si	77
290	(8+9)-VIII-2	259	0.07	6.40	Si	95
290	(8+9)-VI-2	113	0.03	6.40	Si	>100
290	(8+9)-V-1	509	0.13	6.40	Si	49
290	(8+9)-I-2	186	0.05	6.40	Si	>100
290	(8+9)-II-2	35	0.01	6.40	Si	>100
290	(8+9)-V-2	447	0.12	6.40	Si	55
290	(8+9)-IV-2	181	0.05	6.40	Si	>100
290	(8+9)-VIII-1	174	0.05	6.40	Si	>100
290	(8+9)-VII-1	465	0.12	6.40	Si	53
290	(8+9)-VII-2	491	0.13	6.40	Si	50
290	(8+9)-III-1	205	0.05	6.40	Si	>100
580	(8+9)-VII-4	-257	0.07	6.40	Si	96
580	(8+9)-VI-4	-141	0.04	6.40	Si	>100
580	(8+9)-II-4	-98	0.03	6.40	Si	>100
580	(8+9)-IV-1	112	0.03	6.40	Si	>100
580	(8+9)-VIII-4	-99	0.03	6.40	Si	>100
Verifiche nella direzione secondaria						
0	(8+9)-III-3	-76	0.25	6.40	Si	26
0	(8+9)-VI-3	-70	0.23	6.40	Si	28
0	(8+9)-V-3	-82	0.27	6.40	Si	24
0	(8+9)-VIII-3	-82	0.27	6.40	Si	24
0	(8+9)-IV-3	-79	0.26	6.40	Si	25
0	(8+9)-V-4	-51	0.17	6.40	Si	38
0	(8+9)-VII-4	-48	0.16	6.40	Si	41
0	(8+9)-VII-3	-86	0.28	6.40	Si	23
0	(8+9)-IV-1	-44	0.15	6.40	Si	44
0	(8+9)-I-3	-72	0.24	6.40	Si	27
0	(8+9)-I-4	-42	0.14	6.40	Si	47
3870	1	164	0.54	3.84	Si	7.1
3870	2	346	1.14	5.76	Si	5.1

X	Comb.	Ty	τ_d	fvd	RS	Cs
3870	3	346	1.14	5.76	Si	5.1
3870	4	164	0.54	5.12	Si	9.5
3870	5	164	0.54	5.12	Si	9.5
3870	6	164	0.54	5.12	Si	9.5
3870	7	164	0.54	5.12	Si	9.5
3870	(8+9)-VIII-4	173	0.57	6.40	Si	11
3870	(8+9)-II-2	142	0.47	6.40	Si	14
3870	(8+9)-III-2	227	0.75	6.40	Si	8.6
3870	(8+9)-I-2	196	0.65	6.40	Si	9.9
3870	(8+9)-VI-4	70	0.23	6.40	Si	28
3870	(8+9)-I-1	194	0.64	6.40	Si	10
3870	(8+9)-VII-1	239	0.79	6.40	Si	8.1
3870	(8+9)-V-1	270	0.89	6.40	Si	7.2
3870	(8+9)-VII-2	304	1.00	6.40	Si	6.4
3870	(8+9)-III-4	63	0.21	6.40	Si	31
3870	(8+9)-III-1	163	0.54	6.40	Si	12
3870	(8+9)-VI-1	156	0.51	6.40	Si	12
3870	(8+9)-II-4	93	0.31	6.40	Si	21
3870	(8+9)-V-2	273	0.90	6.40	Si	7.1
3870	(8+9)-II-1	133	0.44	6.40	Si	15
3870	(8+9)-VI-2	165	0.54	6.40	Si	12
3870	(8+9)-IV-4	196	0.64	6.40	Si	9.9
3870	(8+9)-VIII-1	53	0.18	6.40	Si	37
3870	(8+9)-VIII-2	268	0.88	6.40	Si	7.3
3870	(8+9)-II-3	84	0.28	6.40	Si	23
3870	(8+9)-IV-2	245	0.81	6.40	Si	7.9

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	1	-1038	-0.55	19.20	35	-0.13	12.00	89	V	35
0	2	-2026	-1.08	28.80	27	-0.26	18.00	69	V	27
0	3	-2026	-1.08	28.80	27	-0.26	18.00	69	V	27
0	4	-1038	-0.55	25.60	46	-0.13	16.00	>100	V	46
0	5	-1038	-0.55	25.60	46	-0.13	16.00	>100	V	46
0	6	-1038	-0.55	25.60	46	-0.13	16.00	>100	V	46
0	7	-1038	-0.55	25.60	46	-0.13	16.00	>100	V	46
0	(8+9)-VIII-4	-8412	-4.49	32.00	7.1	-1.09	20.00	18	V	7.1
0	(8+9)-IV-1	7003	3.74	32.00	8.6	0.90	20.00	22	V	8.6
0	(8+9)-VIII-1	6937	3.70	32.00	8.6	0.90	20.00	22	V	8.6
0	(8+9)-VI-4	-9485	-5.06	32.00	6.3	-1.23	20.00	16	V	6.3
0	(8+9)-II-1	8076	4.31	32.00	7.4	1.04	20.00	19	V	7.4
0	(8+9)-VI-1	8010	4.28	32.00	7.5	1.03	20.00	19	V	7.5
0	(8+9)-IV-4	-8478	-4.53	32.00	7.1	-1.10	20.00	18	V	7.1
0	(8+9)-II-4	-9551	-5.10	32.00	6.3	-1.23	20.00	16	V	6.3
290	(8+9)-V-1	-5681	-3.03	32.00	11	-0.73	20.00	27	V	11
290	(8+9)-I-2	-9129	-4.87	32.00	6.6	-1.18	20.00	17	V	6.6
290	(8+9)-II-2	-11422	-6.10	32.00	5.2	-1.48	20.00	14	V	5.2
290	(8+9)-III-2	-8843	-4.72	32.00	6.8	-1.14	20.00	18	V	6.8
290	(8+9)-VI-2	-12015	-6.41	32.00	5.0	-1.55	20.00	13	V	5.0
290	(8+9)-IV-2	-10469	-5.59	32.00	5.7	-1.35	20.00	15	V	5.7
290	(8+9)-VIII-2	-11062	-5.91	32.00	5.4	-1.43	20.00	14	V	5.4
290	(8+9)-III-1	-3990	-2.13	32.00	15	-0.52	20.00	39	V	15
290	(8+9)-VII-2	-10820	-5.78	32.00	5.5	-1.40	20.00	14	V	5.5
290	(8+9)-V-2	-11106	-5.93	32.00	5.4	-1.43	20.00	14	V	5.4
290	(8+9)-VII-1	-5967	-3.19	32.00	10	-0.77	20.00	26	V	10
290	(8+9)-I-1	-3704	-1.98	32.00	16	-0.48	20.00	42	V	16
580	(8+9)-III-4	4299	2.30	32.00	14	0.56	20.00	36	V	14
580	(8+9)-VI-3	11876	6.34	32.00	5.0	1.53	20.00	13	V	5.0
580	(8+9)-VII-3	11282	6.02	32.00	5.3	1.46	20.00	14	V	5.3
580	(8+9)-III-3	8999	4.80	32.00	6.7	1.16	20.00	17	V	6.7
580	(8+9)-VII-4	6582	3.51	32.00	9.1	0.85	20.00	24	V	9.1
580	(8+9)-II-3	11191	5.97	32.00	5.4	1.45	20.00	14	V	5.4

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
580	(8+9)-V-4	6303	3.36	32.00	9.5	0.81	20.00	25	V	9.5
580	(8+9)-V-3	11561	6.17	32.00	5.2	1.49	20.00	13	V	5.2
580	(8+9)-I-3	9278	4.95	32.00	6.5	1.20	20.00	17	V	6.5
580	(8+9)-IV-3	10262	5.48	32.00	5.8	1.33	20.00	15	V	5.8
580	(8+9)-VIII-3	10946	5.84	32.00	5.5	1.41	20.00	14	V	5.5
580	(8+9)-I-4	4020	2.15	32.00	15	0.52	20.00	39	V	15
Verifiche nella direzione secondaria										
1935	(8+9)-VIII-4	2826	10.07	32.00	3.2	2.44	20.00	8.2	V	3.2
1935	(8+9)-VII-2	4764	16.97	32.00	1.9	4.11	20.00	4.9	V	1.9
1935	(8+9)-III-3	-3565	-12.70	32.00	2.5	-3.07	20.00	6.5	V	2.5
1935	(8+9)-IV-2	4641	16.53	32.00	1.9	4.00	20.00	5.0	V	1.9
1935	(8+9)-III-4	-1286	-4.58	32.00	7.0	-1.11	20.00	18	V	7.0
1935	(8+9)-VIII-2	4947	17.62	32.00	1.8	4.26	20.00	4.7	V	1.8
1935	(8+9)-IV-1	-2954	-10.52	32.00	3.0	-2.55	20.00	7.9	V	3.0
1935	(8+9)-VII-4	-2307	-8.22	32.00	3.9	-1.99	20.00	10	V	3.9
1935	(8+9)-I-1	1240	4.42	32.00	7.2	1.07	20.00	19	V	7.2
1935	(8+9)-IV-3	-4463	-15.90	32.00	2.0	-3.85	20.00	5.2	V	2.0
1935	(8+9)-I-3	-3789	-13.50	32.00	2.4	-3.27	20.00	6.1	V	2.4
1935	(8+9)-IV-4	3132	11.16	32.00	2.9	2.70	20.00	7.4	V	2.9
1935	(8+9)-II-1	-3700	-13.18	32.00	2.4	-3.19	20.00	6.3	V	2.4
1935	(8+9)-V-1	2261	8.06	32.00	4.0	1.95	20.00	10	V	4.0
1935	(8+9)-II-3	-5209	-18.56	32.00	1.7	-4.49	20.00	4.5	V	1.7
1935	(8+9)-V-2	4987	17.77	32.00	1.8	4.30	20.00	4.7	V	1.8
1935	(8+9)-III-1	1464	5.22	32.00	6.1	1.26	20.00	16	V	6.1
1935	(8+9)-V-3	-4810	-17.13	32.00	1.9	-4.15	20.00	4.8	V	1.9
1935	(8+9)-VIII-3	-4769	-16.99	32.00	1.9	-4.11	20.00	4.9	V	1.9
1935	(8+9)-V-4	-2083	-7.42	32.00	4.3	-1.80	20.00	11	V	4.3
1935	(8+9)-VII-3	-4586	-16.34	32.00	2.0	-3.95	20.00	5.1	V	2.0
1935	(8+9)-VI-1	-3394	-12.09	32.00	2.6	-2.93	20.00	6.8	V	2.6
1935	(8+9)-I-4	-1062	-3.78	32.00	8.5	-0.92	20.00	22	V	8.5
1935	(8+9)-VI-2	5693	20.28	32.00	1.6	4.91	20.00	4.1	V	1.6
1935	(8+9)-II-4	3878	13.82	32.00	2.3	3.34	20.00	6.0	V	2.3
1935	(8+9)-VIII-1	-2648	-9.43	32.00	3.4	-2.28	20.00	8.8	V	3.4
1935	(8+9)-I-2	3966	14.13	32.00	2.3	3.42	20.00	5.8	V	2.3
1935	(8+9)-II-2	5387	19.19	32.00	1.7	4.64	20.00	4.3	V	1.7
1935	(8+9)-III-2	3743	13.33	32.00	2.4	3.23	20.00	6.2	V	2.4
1935	(8+9)-VI-3	-5515	-19.65	32.00	1.6	-4.75	20.00	4.2	V	1.6
1935	(8+9)-VI-4	3572	12.72	32.00	2.5	3.08	20.00	6.5	V	2.5
1935	(8+9)-VII-1	2485	8.85	32.00	3.6	2.14	20.00	9.3	V	3.6
3870	1	504	1.80	19.20	11	0.43	12.00	28	V	11
3870	2	1047	3.73	28.80	7.7	0.90	18.00	20	V	7.7
3870	3	1047	3.73	28.80	7.7	0.90	18.00	20	V	7.7
3870	4	504	1.80	25.60	14	0.43	16.00	37	V	14
3870	5	504	1.80	25.60	14	0.43	16.00	37	V	14
3870	6	504	1.80	25.60	14	0.43	16.00	37	V	14
3870	7	504	1.80	25.60	14	0.43	16.00	37	V	14

Setto 44: origine (1519.8,1768.0,303.5), direzione (-0.199392,0.97992,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	1	-488	-12	-116	-0.40	-0.36	-0.34	79.20	115.20	115.20	>100
0	2	-1005	-25	-235	-0.83	-0.76	-0.70	118.80	172.80	172.80	>100
0	3	-1005	-25	-235	-0.83	-0.76	-0.70	118.80	172.80	172.80	>100
0	4	-488	-12	-116	-0.40	-0.36	-0.34	105.60	153.60	153.60	>100
0	5	-488	-12	-116	-0.40	-0.36	-0.34	105.60	153.60	153.60	>100
0	6	-488	-12	-116	-0.40	-0.36	-0.34	105.60	153.60	153.60	>100
0	7	-488	-12	-116	-0.40	-0.36	-0.34	105.60	153.60	153.60	>100
2200	(8+9)-VIII-4	4935	-6	2733	4.07	-0.20	8.10	132.00	192.00	192.00	14
2200	(8+9)-IV-1	-5439	-6	-3098	-4.49	-0.18	-9.18	132.00	192.00	192.00	20
2200	(8+9)-V-1	3661	-7	2243	3.02	-0.21	6.65	132.00	192.00	192.00	17
2200	(8+9)-I-2	7007	-8	3682	5.78	-0.26	10.91	132.00	192.00	192.00	9.8
2200	(8+9)-V-2	8585	-6	4984	7.08	-0.20	14.77	132.00	192.00	192.00	7.6

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
2200	(8+9)-I-4	-2115	-3	-916	-1.74	-0.08	-2.71	132.00	192.00	192.00	68
2200	(8+9)-V-3	-8616	-5	-4959	-7.11	-0.16	-14.69	132.00	192.00	192.00	13
2200	(8+9)-II-2	9558	-6	5271	7.88	-0.19	15.62	132.00	192.00	192.00	7.0
2200	(8+9)-V-4	-3693	-5	-2218	-3.05	-0.15	-6.57	132.00	192.00	192.00	28
2200	(8+9)-II-4	6821	-4	3892	5.63	-0.13	11.53	132.00	192.00	192.00	9.7
2200	(8+9)-VI-1	-6379	-6	-3476	-5.26	-0.20	-10.30	132.00	192.00	192.00	18
2200	(8+9)-III-2	6583	-9	3452	5.43	-0.28	10.23	132.00	192.00	192.00	10
2200	(8+9)-VI-2	10031	-5	5662	8.27	-0.17	16.78	132.00	192.00	192.00	6.6
2200	(8+9)-III-4	-2539	-3	-1146	-2.09	-0.10	-3.40	132.00	192.00	192.00	55
2200	(8+9)-VI-3	-10062	-6	-5636	-8.30	-0.19	-16.70	132.00	192.00	192.00	11
2200	(8+9)-IV-2	8145	-7	4503	6.72	-0.23	13.34	132.00	192.00	192.00	8.2
2200	(8+9)-VI-4	6348	-5	3501	5.24	-0.15	10.37	132.00	192.00	192.00	11
2200	(8+9)-IV-4	5408	-6	3123	4.46	-0.18	9.26	132.00	192.00	192.00	12
2200	(8+9)-VII-1	4085	-6	2474	3.37	-0.19	7.33	132.00	192.00	192.00	15
2200	(8+9)-II-1	-6852	-7	-3866	-5.65	-0.22	-11.46	132.00	192.00	192.00	16
2200	(8+9)-VII-2	8161	-7	4754	6.73	-0.21	14.09	132.00	192.00	192.00	8.0
2200	(8+9)-III-1	2508	-8	1172	2.07	-0.26	3.47	132.00	192.00	192.00	28
2200	(8+9)-VII-3	-8192	-5	-4728	-6.76	-0.14	-14.01	132.00	192.00	192.00	13
2200	(8+9)-I-1	2084	-9	941	1.72	-0.27	2.79	132.00	192.00	192.00	35
2200	(8+9)-VII-4	-4117	-5	-2448	-3.40	-0.16	-7.25	132.00	192.00	192.00	26
2200	(8+9)-III-3	-6615	-3	-3426	-5.46	-0.08	-10.15	132.00	192.00	192.00	18
2200	(8+9)-IV-3	-8176	-4	-4477	-6.74	-0.12	-13.27	132.00	192.00	192.00	14
2200	(8+9)-II-3	-9589	-5	-5246	-7.91	-0.17	-15.54	132.00	192.00	192.00	12
2200	(8+9)-VIII-1	-4966	-5	-2707	-4.10	-0.16	-8.02	132.00	192.00	192.00	23
2200	(8+9)-VIII-2	8618	-7	4893	7.11	-0.21	14.50	132.00	192.00	192.00	7.7
2200	(8+9)-VIII-3	-8649	-5	-4868	-7.13	-0.14	-14.42	132.00	192.00	192.00	13
2200	(8+9)-I-3	-7039	-3	-3657	-5.81	-0.09	-10.84	132.00	192.00	192.00	17
Verifiche nella direzione secondaria											
0	(8+9)-VIII-4	696	0	4468	0.65	0.00	11.44	132.00	192.00	192.00	15
0	(8+9)-VI-4	871	2	5400	0.82	0.10	13.83	132.00	192.00	192.00	13
0	(8+9)-III-2	389	6	4956	0.37	0.34	12.69	132.00	192.00	192.00	14
0	(8+9)-IV-2	700	5	6154	0.66	0.29	15.76	132.00	192.00	192.00	11
0	(8+9)-III-3	-1874	-22	-5025	-1.76	-1.18	-12.87	132.00	192.00	192.00	14
0	(8+9)-VIII-2	243	4	5774	0.23	0.23	14.79	132.00	192.00	192.00	13
0	(8+9)-III-4	-1147	-16	-1932	-1.08	-0.86	-4.95	132.00	192.00	192.00	33
0	(8+9)-VII-4	376	-12	-664	0.35	-0.63	-1.70	132.00	192.00	192.00	67
0	(8+9)-IV-1	-1724	-14	-4157	-1.62	-0.77	-10.65	132.00	192.00	192.00	17
0	(8+9)-I-1	-391	-0	1583	-0.37	-0.01	4.05	132.00	192.00	192.00	47
0	(8+9)-I-3	-1927	-22	-5305	-1.81	-1.21	-13.59	132.00	192.00	192.00	13
0	(8+9)-IV-3	-2185	-21	-6224	-2.05	-1.13	-15.94	132.00	192.00	192.00	11
0	(8+9)-II-1	-1899	-16	-5090	-1.78	-0.87	-13.04	132.00	192.00	192.00	14
0	(8+9)-IV-4	239	-1	4088	0.22	-0.06	10.47	132.00	192.00	192.00	18
0	(8+9)-II-3	-2360	-23	-7156	-2.22	-1.23	-18.33	132.00	192.00	192.00	9.8
0	(8+9)-VII-2	-1134	2	3687	-1.06	0.12	9.44	132.00	192.00	192.00	20
0	(8+9)-III-1	-338	0	1862	-0.32	0.02	4.77	132.00	192.00	192.00	40
0	(8+9)-V-2	-1081	3	3967	-1.02	0.15	10.16	132.00	192.00	192.00	19
0	(8+9)-VIII-1	-2181	-16	-4538	-2.05	-0.84	-11.62	132.00	192.00	192.00	15
0	(8+9)-V-3	-404	-18	-4037	-0.38	-0.98	-10.34	132.00	192.00	192.00	17
0	(8+9)-I-2	442	7	5235	0.41	0.37	13.41	132.00	192.00	192.00	13
0	(8+9)-V-4	429	-11	-384	0.40	-0.60	-0.98	132.00	192.00	192.00	88
0	(8+9)-II-2	875	7	7086	0.82	0.39	18.15	132.00	192.00	192.00	9.7
0	(8+9)-VIII-3	-1728	-20	-5843	-1.62	-1.06	-14.97	132.00	192.00	192.00	12
0	(8+9)-VII-3	-351	-18	-3757	-0.33	-0.95	-9.62	132.00	192.00	192.00	18
0	(8+9)-I-4	-1094	-15	-1652	-1.03	-0.83	-4.23	132.00	192.00	192.00	38
0	(8+9)-II-4	414	1	5020	0.39	0.03	12.86	132.00	192.00	192.00	14
0	(8+9)-VI-1	-2356	-17	-5470	-2.21	-0.94	-14.01	132.00	192.00	192.00	13
0	(8+9)-VI-2	418	6	6706	0.39	0.33	17.18	132.00	192.00	192.00	11
0	(8+9)-VI-3	-1903	-22	-6775	-1.79	-1.16	-17.35	132.00	192.00	192.00	10
835	1	-708	-14	-18	-0.67	-0.75	-0.05	79.20	115.20	115.20	>100
835	2	-1374	-29	-128	-1.29	-1.57	-0.33	118.80	172.80	172.80	91
835	3	-1374	-29	-128	-1.29	-1.57	-0.33	118.80	172.80	172.80	91
835	4	-708	-14	-18	-0.67	-0.75	-0.05	105.60	153.60	153.60	>100
835	5	-708	-14	-18	-0.67	-0.75	-0.05	105.60	153.60	153.60	>100
835	6	-708	-14	-18	-0.67	-0.75	-0.05	105.60	153.60	153.60	>100

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
835	7	-708	-14	-18	-0.67	-0.75	-0.05	105.60	153.60	153.60	>100
1670	(8+9)-VII-1	-392	6	-696	-0.37	0.33	-1.78	132.00	192.00	192.00	91
1670	(8+9)-V-1	-400	6	-654	-0.38	0.32	-1.68	132.00	192.00	192.00	96

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
0	1	13	0.01	3.84	Si	>100
0	2	28	0.02	5.76	Si	>100
0	3	28	0.02	5.76	Si	>100
0	4	13	0.01	5.12	Si	>100
0	5	13	0.01	5.12	Si	>100
0	6	13	0.01	5.12	Si	>100
0	7	13	0.01	5.12	Si	>100
0	(8+9)-VI-1	8	0.00	6.40	Si	>100
0	(8+9)-VI-3	16	0.01	6.40	Si	>100
0	(8+9)-III-4	17	0.01	6.40	Si	>100
0	(8+9)-IV-1	9	0.01	6.40	Si	>100
0	(8+9)-I-4	17	0.01	6.40	Si	>100
0	(8+9)-VII-4	21	0.01	6.40	Si	>100
0	(8+9)-VIII-4	10	0.01	6.40	Si	>100
0	(8+9)-IV-3	15	0.01	6.40	Si	>100
0	(8+9)-II-4	8	0.00	6.40	Si	>100
0	(8+9)-IV-4	8	0.01	6.40	Si	>100
0	(8+9)-VIII-1	8	0.00	6.40	Si	>100
0	(8+9)-VII-3	23	0.01	6.40	Si	>100
0	(8+9)-I-3	19	0.01	6.40	Si	>100
0	(8+9)-II-3	15	0.01	6.40	Si	>100
0	(8+9)-VIII-3	16	0.01	6.40	Si	>100
0	(8+9)-III-3	19	0.01	6.40	Si	>100
0	(8+9)-II-1	9	0.01	6.40	Si	>100
0	(8+9)-VI-4	10	0.01	6.40	Si	>100
0	(8+9)-V-3	23	0.01	6.40	Si	>100
0	(8+9)-V-4	21	0.01	6.40	Si	>100
1100	(8+9)-VII-1	-5	0.00	6.40	Si	>100
1100	(8+9)-I-2	-4	0.00	6.40	Si	>100
1100	(8+9)-II-2	-3	0.00	6.40	Si	>100
1100	(8+9)-IV-2	-3	0.00	6.40	Si	>100
1100	(8+9)-V-2	-7	0.00	6.40	Si	>100
1100	(8+9)-VII-2	-7	0.00	6.40	Si	>100
1100	(8+9)-V-1	-5	0.00	6.40	Si	>100
1100	(8+9)-VI-2	-5	0.00	6.40	Si	>100
1100	(8+9)-III-2	-4	0.00	6.40	Si	>100
1100	(8+9)-VIII-2	-4	0.00	6.40	Si	>100
2200	(8+9)-I-1	-4	0.00	6.40	Si	>100
2200	(8+9)-III-1	-4	0.00	6.40	Si	>100
Verifiche nella direzione secondaria						
0	(8+9)-III-3	-22	0.02	6.40	Si	>100
0	(8+9)-VII-4	-18	0.02	6.40	Si	>100
0	(8+9)-IV-2	6	0.00	6.40	Si	>100
0	(8+9)-VIII-3	-27	0.02	6.40	Si	>100
0	(8+9)-I-3	-23	0.02	6.40	Si	>100
0	(8+9)-VII-3	-26	0.02	6.40	Si	>100
0	(8+9)-IV-1	-20	0.02	6.40	Si	>100
0	(8+9)-IV-3	-25	0.02	6.40	Si	>100
0	(8+9)-V-4	-18	0.02	6.40	Si	>100
0	(8+9)-VI-3	-28	0.02	6.40	Si	>100
0	(8+9)-V-3	-27	0.02	6.40	Si	>100
0	(8+9)-II-1	-22	0.02	6.40	Si	>100
0	(8+9)-II-2	7	0.01	6.40	Si	>100
0	(8+9)-II-3	-27	0.02	6.40	Si	>100
1670	1	20	0.02	3.84	Si	>100
1670	2	41	0.04	5.76	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
1670	3	41	0.04	5.76	Si	>100
1670	4	20	0.02	5.12	Si	>100
1670	5	20	0.02	5.12	Si	>100
1670	6	20	0.02	5.12	Si	>100
1670	7	20	0.02	5.12	Si	>100
1670	(8+9)-VIII-4	-2	0.00	6.40	Si	>100
1670	(8+9)-VI-1	30	0.03	6.40	Si	>100
1670	(8+9)-III-1	9	0.01	6.40	Si	>100
1670	(8+9)-VII-1	45	0.04	6.40	Si	>100
1670	(8+9)-V-1	45	0.04	6.40	Si	>100
1670	(8+9)-VII-2	40	0.04	6.40	Si	>100
1670	(8+9)-IV-4	9	0.01	6.40	Si	>100
1670	(8+9)-III-4	18	0.02	6.40	Si	>100
1670	(8+9)-I-2	5	0.00	6.40	Si	>100
1670	(8+9)-II-4	8	0.01	6.40	Si	>100
1670	(8+9)-V-2	40	0.03	6.40	Si	>100
1670	(8+9)-I-1	10	0.01	6.40	Si	>100
1670	(8+9)-VI-2	15	0.01	6.40	Si	>100
1670	(8+9)-VI-4	-3	0.00	6.40	Si	>100
1670	(8+9)-VIII-1	29	0.03	6.40	Si	>100
1670	(8+9)-VIII-2	15	0.01	6.40	Si	>100
1670	(8+9)-III-2	5	0.00	6.40	Si	>100
1670	(8+9)-I-4	18	0.02	6.40	Si	>100

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	1	-507	-0.63	19.20	31	-0.15	12.00	79	V	31
0	2	-929	-1.15	28.80	25	-0.28	18.00	65	V	25
0	3	-929	-1.15	28.80	25	-0.28	18.00	65	V	25
0	4	-507	-0.63	25.60	41	-0.15	16.00	>100	V	41
0	5	-507	-0.63	25.60	41	-0.15	16.00	>100	V	41
0	6	-507	-0.63	25.60	41	-0.15	16.00	>100	V	41
0	7	-507	-0.63	25.60	41	-0.15	16.00	>100	V	41
0	(8+9)-VIII-4	-2579	-3.19	32.00	10	-0.77	20.00	26	V	10
0	(8+9)-IV-2	-4127	-5.11	32.00	6.3	-1.24	20.00	16	V	6.3
0	(8+9)-II-2	-4727	-5.85	32.00	5.5	-1.42	20.00	14	V	5.5
0	(8+9)-VI-4	-3179	-3.93	32.00	8.1	-0.95	20.00	21	V	8.1
0	(8+9)-VI-2	-5012	-6.20	32.00	5.2	-1.50	20.00	13	V	5.2
0	(8+9)-VIII-2	-4412	-5.46	32.00	5.9	-1.32	20.00	15	V	5.9
0	(8+9)-IV-4	-2864	-3.54	32.00	9.0	-0.86	20.00	23	V	9.0
0	(8+9)-II-4	-3464	-4.29	32.00	7.5	-1.04	20.00	19	V	7.5
2200	(8+9)-V-1	-2761	-3.42	32.00	9.4	-0.83	20.00	24	V	9.4
2200	(8+9)-IV-1	2360	2.92	32.00	11	0.71	20.00	28	V	11
2200	(8+9)-I-2	-3930	-4.86	32.00	6.6	-1.18	20.00	17	V	6.6
2200	(8+9)-II-1	2949	3.65	32.00	8.8	0.88	20.00	23	V	8.8
2200	(8+9)-III-3	3925	4.86	32.00	6.6	1.18	20.00	17	V	6.6
2200	(8+9)-VI-3	5008	6.20	32.00	5.2	1.50	20.00	13	V	5.2
2200	(8+9)-I-1	-1691	-2.09	32.00	15	-0.51	20.00	39	V	15
2200	(8+9)-I-4	1863	2.30	32.00	14	0.56	20.00	36	V	14
2200	(8+9)-IV-3	4098	5.07	32.00	6.3	1.23	20.00	16	V	6.3
2200	(8+9)-VII-1	-2937	-3.63	32.00	8.8	-0.88	20.00	23	V	8.8
2200	(8+9)-II-3	4687	5.80	32.00	5.5	1.40	20.00	14	V	5.5
2200	(8+9)-VII-2	-4823	-5.97	32.00	5.4	-1.44	20.00	14	V	5.4
2200	(8+9)-V-3	5172	6.40	32.00	5.0	1.55	20.00	13	V	5.0
2200	(8+9)-VII-3	4995	6.18	32.00	5.2	1.50	20.00	13	V	5.2
2200	(8+9)-VI-1	2628	3.25	32.00	9.8	0.79	20.00	25	V	9.8
2200	(8+9)-VII-4	3109	3.85	32.00	8.3	0.93	20.00	21	V	8.3
2200	(8+9)-V-2	-5000	-6.19	32.00	5.2	-1.50	20.00	13	V	5.2
2200	(8+9)-V-4	2933	3.63	32.00	8.8	0.88	20.00	23	V	8.8
2200	(8+9)-III-4	2040	2.52	32.00	13	0.61	20.00	33	V	13
2200	(8+9)-III-1	-1868	-2.31	32.00	14	-0.56	20.00	36	V	14
2200	(8+9)-VIII-1	2039	2.52	32.00	13	0.61	20.00	33	V	13

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
2200	(8+9)-I-3	4102	5.08	32.00	6.3	1.23	20.00	16	V	6.3
2200	(8+9)-VIII-3	4419	5.47	32.00	5.9	1.32	20.00	15	V	5.9
2200	(8+9)-III-2	-3754	-4.64	32.00	6.9	-1.12	20.00	18	V	6.9
Verifiche nella direzione secondaria										
835	1	309	0.29	19.20	66	0.07	12.00	>100	V	66
835	2	637	0.60	28.80	48	0.14	18.00	>100	V	48
835	3	637	0.60	28.80	48	0.14	18.00	>100	V	48
835	4	309	0.29	25.60	88	0.07	16.00	>100	V	88
835	5	309	0.29	25.60	88	0.07	16.00	>100	V	88
835	6	309	0.29	25.60	88	0.07	16.00	>100	V	88
835	7	309	0.29	25.60	88	0.07	16.00	>100	V	88
1670	(8+9)-VIII-4	3954	3.71	32.00	8.6	0.90	20.00	22	V	8.6
1670	(8+9)-IV-2	6660	6.25	32.00	5.1	1.51	20.00	13	V	5.1
1670	(8+9)-V-1	3658	3.44	32.00	9.3	0.83	20.00	24	V	9.3
1670	(8+9)-I-2	5708	5.36	32.00	6.0	1.30	20.00	15	V	6.0
1670	(8+9)-V-2	7509	7.05	32.00	4.5	1.71	20.00	12	V	4.5
1670	(8+9)-I-4	-1510	-1.42	32.00	23	-0.34	20.00	58	V	23
1670	(8+9)-V-3	-7161	-6.73	32.00	4.8	-1.63	20.00	12	V	4.8
1670	(8+9)-II-2	7674	7.21	32.00	4.4	1.74	20.00	11	V	4.4
1670	(8+9)-V-4	-3311	-3.11	32.00	10	-0.75	20.00	27	V	10
1670	(8+9)-II-4	5509	5.17	32.00	6.2	1.25	20.00	16	V	6.2
1670	(8+9)-VI-1	-4621	-4.34	32.00	7.4	-1.05	20.00	19	V	7.4
1670	(8+9)-III-2	5403	5.07	32.00	6.3	1.23	20.00	16	V	6.3
1670	(8+9)-VI-2	8214	7.71	32.00	4.1	1.87	20.00	11	V	4.1
1670	(8+9)-III-4	-1814	-1.70	32.00	19	-0.41	20.00	49	V	19
1670	(8+9)-VI-3	-7867	-7.39	32.00	4.3	-1.79	20.00	11	V	4.3
1670	(8+9)-I-1	1857	1.74	32.00	18	0.42	20.00	47	V	18
1670	(8+9)-VI-4	4969	4.67	32.00	6.9	1.13	20.00	18	V	6.9
1670	(8+9)-IV-4	4494	4.22	32.00	7.6	1.02	20.00	20	V	7.6
1670	(8+9)-VII-1	3962	3.72	32.00	8.6	0.90	20.00	22	V	8.6
1670	(8+9)-II-1	-5162	-4.85	32.00	6.6	-1.17	20.00	17	V	6.6
1670	(8+9)-VII-2	7204	6.77	32.00	4.7	1.64	20.00	12	V	4.7
1670	(8+9)-III-1	2161	2.03	32.00	16	0.49	20.00	41	V	16
1670	(8+9)-VII-3	-6857	-6.44	32.00	5.0	-1.56	20.00	13	V	5.0
1670	(8+9)-IV-1	-4147	-3.89	32.00	8.2	-0.94	20.00	21	V	8.2
1670	(8+9)-VII-4	-3615	-3.40	32.00	9.4	-0.82	20.00	24	V	9.4
1670	(8+9)-III-3	-5056	-4.75	32.00	6.7	-1.15	20.00	17	V	6.7
1670	(8+9)-IV-3	-6312	-5.93	32.00	5.4	-1.43	20.00	14	V	5.4
1670	(8+9)-II-3	-7327	-6.88	32.00	4.7	-1.67	20.00	12	V	4.7
1670	(8+9)-VIII-1	-3607	-3.39	32.00	9.4	-0.82	20.00	24	V	9.4
1670	(8+9)-VIII-2	7200	6.76	32.00	4.7	1.64	20.00	12	V	4.7
1670	(8+9)-VIII-3	-6853	-6.44	32.00	5.0	-1.56	20.00	13	V	5.0
1670	(8+9)-I-3	-5361	-5.03	32.00	6.4	-1.22	20.00	16	V	6.4

Setto 45: origine (1573.6,1503.5,303.5), direzione (-0.199392,0.97992,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	(8+9)-V-1	-2268	-23	-901	-1.87	-0.71	-2.67	132.00	192.00	192.00	57
0	(8+9)-VI-1	3205	10	1004	2.64	0.31	2.98	132.00	192.00	192.00	27
0	(8+9)-V-2	-4807	-35	-1787	-3.96	-1.08	-5.30	132.00	192.00	192.00	30
0	(8+9)-II-3	5002	25	1638	4.13	0.77	4.85	132.00	192.00	192.00	17
0	(8+9)-VIII-1	2678	5	788	2.21	0.15	2.33	132.00	192.00	192.00	34
0	(8+9)-V-4	2369	20	705	1.95	0.62	2.09	132.00	192.00	192.00	35
0	(8+9)-VII-3	4750	30	1526	3.92	0.94	4.52	132.00	192.00	192.00	17
0	(8+9)-III-1	-1239	-19	-586	-1.02	-0.58	-1.74	132.00	192.00	192.00	83
0	(8+9)-VII-1	-2426	-24	-966	-2.00	-0.76	-2.86	132.00	192.00	192.00	53
0	(8+9)-III-2	-3461	-28	-1342	-2.85	-0.85	-3.98	132.00	192.00	192.00	39
0	(8+9)-VI-3	5358	27	1752	4.42	0.82	5.19	132.00	192.00	192.00	15
0	(8+9)-III-3	3563	25	1146	2.94	0.76	3.40	132.00	192.00	192.00	23
0	(8+9)-I-4	1182	14	325	0.97	0.45	0.96	132.00	192.00	192.00	68
0	(8+9)-III-4	1340	16	390	1.11	0.50	1.16	132.00	192.00	192.00	59
0	(8+9)-VIII-3	4831	21	1536	3.98	0.66	4.55	132.00	192.00	192.00	17

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-IV-1	3035	7	902	2.50	0.20	2.67	132.00	192.00	192.00	29
0	(8+9)-I-3	3721	26	1211	3.07	0.81	3.59	132.00	192.00	192.00	22
0	(8+9)-II-1	3562	12	1118	2.94	0.37	3.31	132.00	192.00	192.00	24
0	(8+9)-VII-4	2528	22	770	2.08	0.67	2.28	132.00	192.00	192.00	32
0	(8+9)-I-1	-1081	-17	-521	-0.89	-0.53	-1.55	132.00	192.00	192.00	92
0	(8+9)-V-3	4908	32	1591	4.05	0.99	4.71	132.00	192.00	192.00	17
0	(8+9)-IV-3	4475	20	1422	3.69	0.61	4.21	132.00	192.00	192.00	19
0	(8+9)-VII-2	-4649	-33	-1722	-3.83	-1.03	-5.10	132.00	192.00	192.00	31
1200	1	188	-12	-109	0.16	-0.37	-0.32	79.20	115.20	115.20	>100
1200	2	411	-25	-229	0.34	-0.79	-0.68	118.80	172.80	172.80	88
1200	3	411	-25	-229	0.34	-0.79	-0.68	118.80	172.80	172.80	88
1200	4	188	-12	-109	0.16	-0.37	-0.32	105.60	153.60	153.60	>100
1200	5	188	-12	-109	0.16	-0.37	-0.32	105.60	153.60	153.60	>100
1200	6	188	-12	-109	0.16	-0.37	-0.32	105.60	153.60	153.60	>100
1200	7	188	-12	-109	0.16	-0.37	-0.32	105.60	153.60	153.60	>100
2400	(8+9)-VIII-2	2369	-15	1060	1.95	-0.46	3.14	132.00	192.00	192.00	30
2400	(8+9)-IV-4	1333	-27	633	1.10	-0.85	1.87	132.00	192.00	192.00	44
2400	(8+9)-VI-4	1728	-23	775	1.43	-0.71	2.30	132.00	192.00	192.00	38
2400	(8+9)-I-2	1943	9	847	1.60	0.29	2.51	132.00	192.00	192.00	37
2400	(8+9)-VI-2	2918	-11	1269	2.41	-0.35	3.76	132.00	192.00	192.00	25
2400	(8+9)-II-2	2764	-10	1202	2.28	-0.32	3.56	132.00	192.00	192.00	27
2400	(8+9)-II-4	1882	-24	842	1.55	-0.74	2.49	132.00	192.00	192.00	35
2400	(8+9)-IV-2	2216	-14	993	1.83	-0.43	2.94	132.00	192.00	192.00	32
2400	(8+9)-VIII-4	1180	-26	566	0.97	-0.82	1.68	132.00	192.00	192.00	49
Verifiche nella direzione secondaria											
0	(8+9)-II-2	523	-7	2104	0.45	-0.33	4.53	132.00	192.00	192.00	35
0	(8+9)-VII-1	-536	-30	1390	-0.46	-1.49	2.99	132.00	192.00	192.00	43
0	(8+9)-III-2	-41	-23	1694	-0.04	-1.14	3.65	132.00	192.00	192.00	40
0	(8+9)-V-2	294	-21	2036	0.25	-1.04	4.38	132.00	192.00	192.00	33
0	(8+9)-V-1	-616	-29	1342	-0.53	-1.44	2.89	132.00	192.00	192.00	44
0	(8+9)-VI-2	600	-6	2192	0.52	-0.29	4.72	132.00	192.00	192.00	33
0	(8+9)-III-1	-791	-33	1097	-0.68	-1.64	2.36	132.00	192.00	192.00	48
0	(8+9)-I-1	-871	-32	1048	-0.75	-1.59	2.26	132.00	192.00	192.00	50
0	(8+9)-I-2	39	-24	1743	0.03	-1.19	3.75	132.00	192.00	192.00	38
835	(8+9)-VIII-4	-509	-9	1384	-0.44	-0.42	2.98	132.00	192.00	192.00	56
835	(8+9)-IV-2	-727	-7	2145	-0.63	-0.33	4.62	132.00	192.00	192.00	39
835	(8+9)-VI-4	-476	-8	1624	-0.41	-0.38	3.49	132.00	192.00	192.00	50
835	(8+9)-VII-2	-1155	-11	2349	-0.99	-0.52	5.06	132.00	192.00	192.00	34
835	(8+9)-IV-4	-537	-8	1509	-0.46	-0.42	3.25	132.00	192.00	192.00	52
835	(8+9)-II-4	-505	-8	1748	-0.43	-0.38	3.76	132.00	192.00	192.00	46
835	(8+9)-VIII-2	-755	-7	2270	-0.65	-0.33	4.89	132.00	192.00	192.00	37
1670	1	-791	-39	765	-0.68	-1.91	1.65	79.20	115.20	115.20	32
1670	2	-1627	-82	1703	-1.40	-4.05	3.66	118.80	172.80	172.80	22
1670	3	-1627	-82	1703	-1.40	-4.05	3.66	118.80	172.80	172.80	22
1670	4	-791	-39	765	-0.68	-1.91	1.65	105.60	153.60	153.60	43
1670	5	-791	-39	765	-0.68	-1.91	1.65	105.60	153.60	153.60	43
1670	6	-791	-39	765	-0.68	-1.91	1.65	105.60	153.60	153.60	43
1670	7	-791	-39	765	-0.68	-1.91	1.65	105.60	153.60	153.60	43
1670	(8+9)-I-4	-453	-52	1011	-0.39	-2.55	2.18	132.00	192.00	192.00	41
1670	(8+9)-VI-3	-498	-39	2491	-0.43	-1.94	5.36	132.00	192.00	192.00	26
1670	(8+9)-IV-1	-579	-31	1568	-0.50	-1.52	3.37	132.00	192.00	192.00	39
1670	(8+9)-I-3	-450	-53	1941	-0.39	-2.63	4.18	132.00	192.00	192.00	28
1670	(8+9)-V-3	-398	-62	2387	-0.34	-3.05	5.14	132.00	192.00	192.00	23
1670	(8+9)-VII-3	-401	-65	2322	-0.34	-3.18	5.00	132.00	192.00	192.00	23
1670	(8+9)-VI-1	-586	-19	1649	-0.50	-0.93	3.55	132.00	192.00	192.00	43
1670	(8+9)-VII-4	-398	-57	1522	-0.34	-2.83	3.27	132.00	192.00	192.00	31
1670	(8+9)-II-3	-514	-37	2357	-0.44	-1.82	5.07	132.00	192.00	192.00	28
1670	(8+9)-V-4	-400	-60	1457	-0.34	-2.97	3.14	132.00	192.00	192.00	31
1670	(8+9)-III-3	-453	-56	1876	-0.39	-2.77	4.04	132.00	192.00	192.00	28
1670	(8+9)-IV-3	-522	-46	2141	-0.45	-2.28	4.61	132.00	192.00	192.00	28
1670	(8+9)-VIII-1	-594	-28	1434	-0.51	-1.39	3.09	132.00	192.00	192.00	43
1670	(8+9)-II-1	-571	-21	1783	-0.49	-1.05	3.84	132.00	192.00	192.00	39
1670	(8+9)-VIII-3	-506	-49	2275	-0.44	-2.41	4.90	132.00	192.00	192.00	26
1670	(8+9)-III-4	-450	-49	1075	-0.39	-2.41	2.31	132.00	192.00	192.00	41

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Ty kg	τ_d kg/cmq	fvd kg/cmq	RS	Cs
0	(8+9)-V-1	16	0.01	6.40	Si	>100
0	(8+9)-II-4	-15	0.01	6.40	Si	>100
0	(8+9)-V-4	-24	0.01	6.40	Si	>100
0	(8+9)-I-1	12	0.01	6.40	Si	>100
0	(8+9)-III-1	11	0.01	6.40	Si	>100
0	(8+9)-I-2	7	0.00	6.40	Si	>100
0	(8+9)-III-2	9	0.01	6.40	Si	>100
0	(8+9)-VII-2	13	0.01	6.40	Si	>100
0	(8+9)-VI-4	-16	0.01	6.40	Si	>100
0	(8+9)-VII-1	15	0.01	6.40	Si	>100
0	(8+9)-I-4	-19	0.01	6.40	Si	>100
0	(8+9)-V-2	12	0.01	6.40	Si	>100
1200	(8+9)-IV-2	-8	0.00	6.40	Si	>100
1200	(8+9)-II-2	-11	0.01	6.40	Si	>100
1200	(8+9)-VI-2	-9	0.01	6.40	Si	>100
1200	(8+9)-VIII-2	-6	0.00	6.40	Si	>100
1200	(8+9)-VIII-4	-14	0.01	6.40	Si	>100
1200	(8+9)-IV-4	-12	0.01	6.40	Si	>100
2400	1	21	0.01	3.84	Si	>100
2400	2	44	0.03	5.76	Si	>100
2400	3	44	0.03	5.76	Si	>100
2400	4	21	0.01	5.12	Si	>100
2400	5	21	0.01	5.12	Si	>100
2400	6	21	0.01	5.12	Si	>100
2400	7	21	0.01	5.12	Si	>100
2400	(8+9)-IV-1	19	0.01	6.40	Si	>100
2400	(8+9)-III-4	18	0.01	6.40	Si	>100
2400	(8+9)-III-3	22	0.01	6.40	Si	>100
2400	(8+9)-I-3	23	0.01	6.40	Si	>100
2400	(8+9)-VII-3	28	0.02	6.40	Si	>100
2400	(8+9)-V-3	29	0.02	6.40	Si	>100
2400	(8+9)-VII-4	24	0.01	6.40	Si	>100
2400	(8+9)-VI-1	20	0.01	6.40	Si	>100
2400	(8+9)-VI-3	27	0.02	6.40	Si	>100
2400	(8+9)-II-3	25	0.02	6.40	Si	>100
2400	(8+9)-VIII-1	17	0.01	6.40	Si	>100
2400	(8+9)-IV-3	23	0.01	6.40	Si	>100
2400	(8+9)-VIII-3	24	0.01	6.40	Si	>100
2400	(8+9)-II-1	21	0.01	6.40	Si	>100
Verifiche nella direzione secondaria						
0	(8+9)-III-3	68	0.05	6.40	Si	>100
0	(8+9)-VI-2	12	0.01	6.40	Si	>100
0	(8+9)-I-3	67	0.05	6.40	Si	>100
0	(8+9)-VIII-2	9	0.01	6.40	Si	>100
0	(8+9)-I-4	74	0.06	6.40	Si	>100
0	(8+9)-VI-1	-14	0.01	6.40	Si	>100
0	(8+9)-II-1	-40	0.03	6.40	Si	>100
0	(8+9)-IV-2	-18	0.01	6.40	Si	>100
0	(8+9)-II-2	-15	0.01	6.40	Si	>100
0	(8+9)-I-1	-84	0.07	6.40	Si	96
0	(8+9)-III-4	73	0.06	6.40	Si	>100
0	(8+9)-IV-1	-37	0.03	6.40	Si	>100
0	(8+9)-I-2	-76	0.06	6.40	Si	>100
0	(8+9)-IV-4	27	0.02	6.40	Si	>100
0	(8+9)-II-4	31	0.02	6.40	Si	>100
0	(8+9)-III-1	-83	0.07	6.40	Si	97
0	(8+9)-III-2	-77	0.06	6.40	Si	>100
1670	1	-22	0.02	3.84	Si	>100
1670	2	-47	0.04	5.76	Si	>100
1670	3	-47	0.04	5.76	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
1670	4	-22	0.02	5.12	Si	>100
1670	5	-22	0.02	5.12	Si	>100
1670	6	-22	0.02	5.12	Si	>100
1670	7	-22	0.02	5.12	Si	>100
1670	(8+9)-VIII-4	-16	0.01	6.40	Si	>100
1670	(8+9)-II-3	-28	0.02	6.40	Si	>100
1670	(8+9)-VII-2	27	0.02	6.40	Si	>100
1670	(8+9)-V-3	-56	0.04	6.40	Si	>100
1670	(8+9)-VII-3	-57	0.05	6.40	Si	>100
1670	(8+9)-V-2	25	0.02	6.40	Si	>100
1670	(8+9)-VII-4	-51	0.04	6.40	Si	>100
1670	(8+9)-VII-1	20	0.02	6.40	Si	>100
1670	(8+9)-V-4	-52	0.04	6.40	Si	>100
1670	(8+9)-V-1	22	0.02	6.40	Si	>100
1670	(8+9)-VI-4	-21	0.02	6.40	Si	>100
1670	(8+9)-VIII-1	-15	0.01	6.40	Si	>100
1670	(8+9)-IV-3	-33	0.03	6.40	Si	>100
1670	(8+9)-VIII-3	-38	0.03	6.40	Si	>100
1670	(8+9)-VI-3	-32	0.03	6.40	Si	>100

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	1	-494	-0.61	19.20	31	-0.15	12.00	81	V	31
0	2	-889	-1.10	28.80	26	-0.27	18.00	68	V	26
0	3	-889	-1.10	28.80	26	-0.27	18.00	68	V	26
0	4	-494	-0.61	25.60	42	-0.15	16.00	>100	V	42
0	5	-494	-0.61	25.60	42	-0.15	16.00	>100	V	42
0	6	-494	-0.61	25.60	42	-0.15	16.00	>100	V	42
0	7	-494	-0.61	25.60	42	-0.15	16.00	>100	V	42
0	(8+9)-V-1	-1725	-2.13	32.00	15	-0.52	20.00	39	V	15
0	(8+9)-I-1	-1010	-1.25	32.00	26	-0.30	20.00	66	V	26
0	(8+9)-III-2	-2747	-3.40	32.00	9.4	-0.82	20.00	24	V	9.4
0	(8+9)-I-2	-2897	-3.58	32.00	8.9	-0.87	20.00	23	V	8.9
0	(8+9)-VI-4	-2800	-3.46	32.00	9.2	-0.84	20.00	24	V	9.2
0	(8+9)-VIII-2	-3691	-4.57	32.00	7.0	-1.11	20.00	18	V	7.0
0	(8+9)-VI-2	-4191	-5.19	32.00	6.2	-1.25	20.00	16	V	6.2
0	(8+9)-II-2	-3976	-4.92	32.00	6.5	-1.19	20.00	17	V	6.5
0	(8+9)-II-4	-3015	-3.73	32.00	8.6	-0.90	20.00	22	V	8.6
0	(8+9)-VIII-4	-2300	-2.85	32.00	11	-0.69	20.00	29	V	11
0	(8+9)-VII-2	-3463	-4.28	32.00	7.5	-1.04	20.00	19	V	7.5
0	(8+9)-VII-1	-1875	-2.32	32.00	14	-0.56	20.00	36	V	14
0	(8+9)-III-1	-1160	-1.43	32.00	22	-0.35	20.00	58	V	22
0	(8+9)-IV-2	-3477	-4.30	32.00	7.4	-1.04	20.00	19	V	7.4
0	(8+9)-V-2	-3613	-4.47	32.00	7.2	-1.08	20.00	18	V	7.2
0	(8+9)-IV-4	-2515	-3.11	32.00	10	-0.75	20.00	27	V	10
2400	(8+9)-VI-1	2683	3.32	32.00	9.6	0.80	20.00	25	V	9.6
2400	(8+9)-VIII-1	2185	2.70	32.00	12	0.65	20.00	31	V	12
2400	(8+9)-IV-3	3460	4.28	32.00	7.5	1.04	20.00	19	V	7.5
2400	(8+9)-I-4	1042	1.29	32.00	25	0.31	20.00	64	V	25
2400	(8+9)-V-4	1782	2.21	32.00	15	0.53	20.00	37	V	15
2400	(8+9)-VIII-3	3682	4.56	32.00	7.0	1.10	20.00	18	V	7.0
2400	(8+9)-III-4	1191	1.47	32.00	22	0.36	20.00	56	V	22
2400	(8+9)-I-3	2954	3.66	32.00	8.8	0.88	20.00	23	V	8.8
2400	(8+9)-III-3	2805	3.47	32.00	9.2	0.84	20.00	24	V	9.2
2400	(8+9)-II-1	2906	3.59	32.00	8.9	0.87	20.00	23	V	8.9
2400	(8+9)-VII-3	3546	4.39	32.00	7.3	1.06	20.00	19	V	7.3
2400	(8+9)-VII-4	1932	2.39	32.00	13	0.58	20.00	35	V	13
2400	(8+9)-V-3	3695	4.57	32.00	7.0	1.11	20.00	18	V	7.0
2400	(8+9)-IV-1	2407	2.98	32.00	11	0.72	20.00	28	V	11
2400	(8+9)-VI-3	4180	5.17	32.00	6.2	1.25	20.00	16	V	6.2
2400	(8+9)-II-3	3958	4.90	32.00	6.5	1.19	20.00	17	V	6.5

Verifiche nella direzione secondaria

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
835	(8+9)-I-1	1490	1.28	32.00	25	0.31	20.00	64	V	25
835	(8+9)-VII-1	3490	3.00	32.00	11	0.73	20.00	28	V	11
835	(8+9)-V-1	3156	2.72	32.00	12	0.66	20.00	30	V	12
835	(8+9)-III-4	-2338	-2.01	32.00	16	-0.49	20.00	41	V	16
835	(8+9)-III-1	1824	1.57	32.00	20	0.38	20.00	53	V	20
835	(8+9)-I-4	-2004	-1.72	32.00	19	-0.42	20.00	48	V	19
1670	1	-538	-0.46	19.20	41	-0.11	12.00	>100	V	41
1670	2	-1220	-1.05	28.80	27	-0.25	18.00	71	V	27
1670	3	-1220	-1.05	28.80	27	-0.25	18.00	71	V	27
1670	4	-538	-0.46	25.60	55	-0.11	16.00	>100	V	55
1670	5	-538	-0.46	25.60	55	-0.11	16.00	>100	V	55
1670	6	-538	-0.46	25.60	55	-0.11	16.00	>100	V	55
1670	7	-538	-0.46	25.60	55	-0.11	16.00	>100	V	55
1670	(8+9)-VIII-4	4629	3.99	32.00	8.0	0.96	20.00	21	V	8.0
1670	(8+9)-V-4	-3848	-3.31	32.00	9.7	-0.80	20.00	25	V	9.7
1670	(8+9)-II-3	-9484	-8.16	32.00	3.9	-1.98	20.00	10	V	3.9
1670	(8+9)-VI-1	-6537	-5.63	32.00	5.7	-1.36	20.00	15	V	5.7
1670	(8+9)-II-2	8750	7.53	32.00	4.2	1.82	20.00	11	V	4.2
1670	(8+9)-VI-2	9320	8.02	32.00	4.0	1.94	20.00	10	V	4.0
1670	(8+9)-III-3	-6356	-5.47	32.00	5.8	-1.32	20.00	15	V	5.8
1670	(8+9)-VI-3	-10053	-8.65	32.00	3.7	-2.09	20.00	9.5	V	3.7
1670	(8+9)-IV-1	-5932	-5.11	32.00	6.3	-1.24	20.00	16	V	6.3
1670	(8+9)-VI-4	5804	5.00	32.00	6.4	1.21	20.00	17	V	6.4
1670	(8+9)-IV-3	-8309	-7.15	32.00	4.5	-1.73	20.00	12	V	4.5
1670	(8+9)-I-2	5975	5.14	32.00	6.2	1.24	20.00	16	V	6.2
1670	(8+9)-I-3	-6708	-5.78	32.00	5.5	-1.40	20.00	14	V	5.5
1670	(8+9)-VII-2	7519	6.47	32.00	4.9	1.57	20.00	13	V	4.9
1670	(8+9)-V-3	-8605	-7.41	32.00	4.3	-1.79	20.00	11	V	4.3
1670	(8+9)-VII-3	-8253	-7.10	32.00	4.5	-1.72	20.00	12	V	4.5
1670	(8+9)-III-2	5623	4.84	32.00	6.6	1.17	20.00	17	V	6.6
1670	(8+9)-VII-4	-4201	-3.62	32.00	8.8	-0.88	20.00	23	V	8.8
1670	(8+9)-V-2	7872	6.78	32.00	4.7	1.64	20.00	12	V	4.7
1670	(8+9)-II-4	6373	5.49	32.00	5.8	1.33	20.00	15	V	5.8
1670	(8+9)-II-1	-7106	-6.12	32.00	5.2	-1.48	20.00	14	V	5.2
1670	(8+9)-IV-4	5198	4.48	32.00	7.2	1.08	20.00	18	V	7.2
1670	(8+9)-VIII-1	-5362	-4.62	32.00	6.9	-1.12	20.00	18	V	6.9
1670	(8+9)-VIII-2	8145	7.01	32.00	4.6	1.70	20.00	12	V	4.6
1670	(8+9)-VIII-3	-8878	-7.64	32.00	4.2	-1.85	20.00	11	V	4.2
1670	(8+9)-IV-2	7576	6.52	32.00	4.9	1.58	20.00	13	V	4.9

Setto 46: origine (1627.4,1238.9,303.5), direzione (-0.199392,0.97992,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_N	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	1	1955	-26	-459	1.61	-0.80	-1.36	79.20	115.20	115.20	26
0	2	4198	-54	-900	3.46	-1.68	-2.67	118.80	172.80	172.80	18
0	3	4198	-54	-900	3.46	-1.68	-2.67	118.80	172.80	172.80	18
0	4	1955	-26	-459	1.61	-0.80	-1.36	105.60	153.60	153.60	34
0	5	1955	-26	-459	1.61	-0.80	-1.36	105.60	153.60	153.60	34
0	6	1955	-26	-459	1.61	-0.80	-1.36	105.60	153.60	153.60	34
0	7	1955	-26	-459	1.61	-0.80	-1.36	105.60	153.60	153.60	34
0	(8+9)-VIII-4	-5748	179	-3216	-4.74	5.56	-9.53	132.00	192.00	192.00	13
0	(8+9)-IV-1	9403	-223	2932	7.76	-6.91	8.69	132.00	192.00	192.00	7.1
0	(8+9)-V-1	-4496	-283	-2655	-3.71	-8.76	-7.87	132.00	192.00	192.00	11
0	(8+9)-I-2	-8260	-301	-4376	-6.81	-9.32	-12.97	132.00	192.00	192.00	8.5
0	(8+9)-V-2	-11436	-273	-5576	-9.43	-8.47	-16.52	132.00	192.00	192.00	7.5
0	(8+9)-I-4	4022	274	813	3.32	8.50	2.41	132.00	192.00	192.00	12
0	(8+9)-V-3	14139	238	4932	11.66	7.37	14.62	132.00	192.00	192.00	4.9
0	(8+9)-II-2	-12059	-88	-5968	-9.95	-2.74	-17.68	132.00	192.00	192.00	9.2
0	(8+9)-V-4	7198	247	2012	5.94	7.66	5.96	132.00	192.00	192.00	8.6
0	(8+9)-II-4	-8374	84	-4411	-6.91	2.61	-13.07	132.00	192.00	192.00	12
0	(8+9)-VI-1	10124	-111	3408	8.35	-3.45	10.10	132.00	192.00	192.00	7.5
0	(8+9)-III-2	-7758	-270	-4126	-6.40	-8.35	-12.23	132.00	192.00	192.00	9.2

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-VI-2	-13012	-80	-6327	-10.73	-2.49	-18.75	132.00	192.00	192.00	8.8
0	(8+9)-III-4	4524	306	1063	3.73	9.47	3.15	132.00	192.00	192.00	11
0	(8+9)-VI-3	15714	45	5684	12.96	1.38	16.84	132.00	192.00	192.00	5.2
0	(8+9)-IV-2	-10385	15	-5133	-8.57	0.46	-15.21	132.00	192.00	192.00	12
0	(8+9)-VI-4	-7421	76	-4051	-6.12	2.35	-12.00	132.00	192.00	192.00	13
0	(8+9)-IV-4	-6701	188	-3576	-5.53	5.81	-10.60	132.00	192.00	192.00	12
0	(8+9)-VII-1	-4998	-314	-2906	-4.12	-9.72	-8.61	132.00	192.00	192.00	10
0	(8+9)-II-1	11077	-120	3767	9.14	-3.71	11.16	132.00	192.00	192.00	6.8
0	(8+9)-VII-2	-10934	-242	-5325	-9.02	-7.51	-15.78	132.00	192.00	192.00	8.1
0	(8+9)-III-1	-1822	-341	-1707	-1.50	-10.57	-5.06	132.00	192.00	192.00	12
0	(8+9)-VII-3	13637	207	4682	11.25	6.41	13.87	132.00	192.00	192.00	5.2
0	(8+9)-I-1	-1320	-310	-1456	-1.09	-9.61	-4.31	132.00	192.00	192.00	14
0	(8+9)-VII-4	7700	278	2262	6.35	8.62	6.70	132.00	192.00	192.00	7.8
0	(8+9)-III-3	10461	234	3483	8.63	7.25	10.32	132.00	192.00	192.00	6.4
0	(8+9)-IV-3	13088	-51	4489	10.79	-1.57	13.30	132.00	192.00	192.00	6.3
0	(8+9)-II-3	14761	53	5324	12.18	1.64	15.78	132.00	192.00	192.00	5.5
0	(8+9)-VIII-1	8450	-215	2573	6.97	-6.66	7.62	132.00	192.00	192.00	7.9
0	(8+9)-VIII-2	-11338	23	-5492	-9.35	0.72	-16.28	132.00	192.00	192.00	11
0	(8+9)-VIII-3	14041	-59	4849	11.58	-1.82	14.37	132.00	192.00	192.00	5.8
0	(8+9)-I-3	10963	265	3733	9.04	8.21	11.06	132.00	192.00	192.00	5.9
Verifiche nella direzione secondaria											
0	1	-3330	-34	1357	-2.87	-1.66	2.92	79.20	115.20	115.20	25
0	(8+9)-VIII-4	-3677	-9	4560	-3.17	-0.44	9.81	132.00	192.00	192.00	19
0	(8+9)-IV-2	-5010	-31	7521	-4.31	-1.53	16.19	132.00	192.00	192.00	11
0	(8+9)-VII-3	854	18	-6286	0.73	0.88	-13.53	132.00	192.00	192.00	12
0	(8+9)-III-4	-1053	9	-1708	-0.91	0.44	-3.68	132.00	192.00	192.00	47
0	(8+9)-IV-3	366	-16	-5645	0.32	-0.77	-12.15	132.00	192.00	192.00	14
0	(8+9)-IV-1	-776	-35	-3102	-0.67	-1.71	-6.68	132.00	192.00	192.00	23
0	(8+9)-VIII-2	-5201	-34	7938	-4.48	-1.67	17.08	132.00	192.00	192.00	10
0	(8+9)-VII-4	-417	19	-3099	-0.36	0.93	-6.67	132.00	192.00	192.00	25
0	(8+9)-I-1	-3521	-56	3325	-3.03	-2.77	7.16	132.00	192.00	192.00	19
0	(8+9)-I-3	287	7	-5153	0.25	0.35	-11.09	132.00	192.00	192.00	16
0	(8+9)-IV-4	-3868	-12	4977	-3.33	-0.59	10.71	132.00	192.00	192.00	17
0	(8+9)-II-1	-543	-37	-3963	-0.47	-1.81	-8.53	132.00	192.00	192.00	19
0	(8+9)-V-1	-4158	-66	4716	-3.58	-3.26	10.15	132.00	192.00	192.00	14
0	(8+9)-II-3	599	-18	-6506	0.52	-0.87	-14.00	132.00	192.00	192.00	12
0	(8+9)-V-2	-5568	-64	8420	-4.79	-3.15	18.12	132.00	192.00	192.00	9.0
0	(8+9)-III-1	-3591	-56	3583	-3.09	-2.74	7.71	132.00	192.00	192.00	18
0	(8+9)-V-3	923	17	-6544	0.79	0.85	-14.08	132.00	192.00	192.00	12
0	(8+9)-III-3	217	8	-4895	0.19	0.38	-10.53	132.00	192.00	192.00	17
0	(8+9)-V-4	-486	20	-2841	-0.42	0.96	-6.11	132.00	192.00	192.00	27
0	(8+9)-VIII-1	-967	-38	-2684	-0.83	-1.86	-5.78	132.00	192.00	192.00	25
0	(8+9)-VI-1	-734	-40	-3545	-0.63	-1.96	-7.63	132.00	192.00	192.00	20
0	(8+9)-I-4	-1123	9	-1450	-0.97	0.47	-3.12	132.00	192.00	192.00	53
0	(8+9)-VI-2	-5434	-32	8799	-4.68	-1.58	18.94	132.00	192.00	192.00	9.3
0	(8+9)-II-4	-4101	-10	5838	-3.53	-0.49	12.56	132.00	192.00	192.00	15
0	(8+9)-VI-3	790	-15	-6923	0.68	-0.72	-14.90	132.00	192.00	192.00	12
0	(8+9)-VIII-3	557	-13	-6063	0.48	-0.62	-13.05	132.00	192.00	192.00	13
0	(8+9)-II-2	-5243	-29	8381	-4.51	-1.43	18.04	132.00	192.00	192.00	9.8
0	(8+9)-III-2	-4861	-54	6770	-4.18	-2.68	14.57	132.00	192.00	192.00	11
0	(8+9)-I-2	-4931	-54	7028	-4.24	-2.65	15.13	132.00	192.00	192.00	11
0	(8+9)-VI-4	-3910	-7	5421	-3.37	-0.34	11.67	132.00	192.00	192.00	16
0	(8+9)-VII-1	-4227	-66	4975	-3.64	-3.23	10.71	132.00	192.00	192.00	14
0	(8+9)-VII-2	-5498	-65	8161	-4.73	-3.18	17.57	132.00	192.00	192.00	9.2
1670	2	-4281	48	3353	-3.69	2.37	7.22	118.80	172.80	172.80	18
1670	3	-4281	48	3353	-3.69	2.37	7.22	118.80	172.80	172.80	18
1670	4	-2060	23	1626	-1.77	1.12	3.50	105.60	153.60	153.60	33
1670	5	-2060	23	1626	-1.77	1.12	3.50	105.60	153.60	153.60	33
1670	6	-2060	23	1626	-1.77	1.12	3.50	105.60	153.60	153.60	33
1670	7	-2060	23	1626	-1.77	1.12	3.50	105.60	153.60	153.60	33

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
0	1	34	0.02	3.84	Si	>100
0	2	72	0.04	5.76	Si	>100
0	3	72	0.04	5.76	Si	>100
0	4	34	0.02	5.12	Si	>100
0	5	34	0.02	5.12	Si	>100
0	6	34	0.02	5.12	Si	>100
0	7	34	0.02	5.12	Si	>100
0	(8+9)-VI-2	34	0.02	6.40	Si	>100
0	(8+9)-VII-2	217	0.13	6.40	Si	49
0	(8+9)-I-2	170	0.10	6.40	Si	63
0	(8+9)-VII-3	-170	0.10	6.40	Si	63
0	(8+9)-I-4	-151	0.09	6.40	Si	70
0	(8+9)-VII-4	-174	0.10	6.40	Si	61
0	(8+9)-II-2	23	0.01	6.40	Si	>100
0	(8+9)-VIII-1	88	0.05	6.40	Si	>100
0	(8+9)-II-4	-73	0.04	6.40	Si	>100
0	(8+9)-VIII-2	76	0.05	6.40	Si	>100
0	(8+9)-III-2	182	0.11	6.40	Si	59
0	(8+9)-VIII-3	-29	0.02	6.40	Si	>100
0	(8+9)-III-4	-139	0.08	6.40	Si	77
0	(8+9)-VIII-4	-41	0.02	6.40	Si	>100
0	(8+9)-IV-2	66	0.04	6.40	Si	>100
0	(8+9)-IV-3	-19	0.01	6.40	Si	>100
0	(8+9)-VI-4	-83	0.05	6.40	Si	>100
0	(8+9)-IV-4	-30	0.02	6.40	Si	>100
0	(8+9)-VII-1	221	0.13	6.40	Si	48
0	(8+9)-V-2	204	0.12	6.40	Si	52
0	(8+9)-I-3	-122	0.07	6.40	Si	87
0	(8+9)-V-4	-186	0.11	6.40	Si	57
0	(8+9)-II-1	120	0.07	6.40	Si	89
0	(8+9)-I-1	198	0.12	6.40	Si	54
0	(8+9)-V-1	233	0.14	6.40	Si	46
0	(8+9)-VI-1	130	0.08	6.40	Si	82
0	(8+9)-IV-1	78	0.05	6.40	Si	>100
0	(8+9)-V-3	-157	0.09	6.40	Si	68
0	(8+9)-III-1	186	0.11	6.40	Si	57
0	(8+9)-III-3	-135	0.08	6.40	Si	79
1200	(8+9)-VI-3	18	0.01	6.40	Si	>100
1200	(8+9)-II-3	28	0.02	6.40	Si	>100
Verifiche nella direzione secondaria						
0	(8+9)-III-3	-159	0.13	6.40	Si	51
0	(8+9)-I-3	-159	0.13	6.40	Si	51
0	(8+9)-VIII-3	-92	0.07	6.40	Si	87
0	(8+9)-I-4	-138	0.11	6.40	Si	58
0	(8+9)-VII-3	-187	0.15	6.40	Si	43
0	(8+9)-IV-3	-84	0.07	6.40	Si	96
0	(8+9)-VI-2	78	0.06	6.40	Si	>100
0	(8+9)-II-2	69	0.06	6.40	Si	>100
0	(8+9)-IV-4	-17	0.01	6.40	Si	>100
0	(8+9)-II-3	-86	0.07	6.40	Si	94
0	(8+9)-VII-4	-166	0.13	6.40	Si	48
0	(8+9)-V-3	-187	0.15	6.40	Si	43
0	(8+9)-I-2	142	0.11	6.40	Si	57
0	(8+9)-VI-3	-94	0.08	6.40	Si	85
0	(8+9)-IV-2	67	0.05	6.40	Si	>100
0	(8+9)-III-4	-138	0.11	6.40	Si	58
0	(8+9)-III-2	142	0.11	6.40	Si	57
1670	1	54	0.04	3.84	Si	90
1670	2	113	0.09	5.76	Si	64
1670	3	113	0.09	5.76	Si	64
1670	4	54	0.04	5.12	Si	>100
1670	5	54	0.04	5.12	Si	>100
1670	6	54	0.04	5.12	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
1670	7	54	0.04	5.12	Si	>100
1670	(8+9)-VIII-4	-38	0.03	6.40	Si	>100
1670	(8+9)-III-1	140	0.11	6.40	Si	58
1670	(8+9)-VII-2	228	0.18	6.40	Si	35
1670	(8+9)-V-2	222	0.18	6.40	Si	36
1670	(8+9)-II-1	103	0.08	6.40	Si	78
1670	(8+9)-VI-1	132	0.11	6.40	Si	61
1670	(8+9)-II-4	-29	0.02	6.40	Si	>100
1670	(8+9)-VII-1	238	0.19	6.40	Si	34
1670	(8+9)-V-4	-170	0.14	6.40	Si	47
1670	(8+9)-V-1	244	0.19	6.40	Si	33
1670	(8+9)-VI-4	-59	0.05	6.40	Si	>100
1670	(8+9)-VIII-1	112	0.09	6.40	Si	72
1670	(8+9)-VIII-2	79	0.06	6.40	Si	>100
1670	(8+9)-IV-1	83	0.07	6.40	Si	98
1670	(8+9)-I-1	146	0.12	6.40	Si	55

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Tx kg	τ_{vd} kg/cmq	fvd kg/cmq	Csv	τ_M kg/cmq	fTd kg/cmq	Csm	Mecc.	Cs
0	(8+9)-III-2	-3404	-4.21	32.00	7.6	-1.02	20.00	20	V	7.6
0	(8+9)-I-2	-3600	-4.45	32.00	7.2	-1.08	20.00	19	V	7.2
0	(8+9)-VIII-4	-2665	-3.30	32.00	9.7	-0.80	20.00	25	V	9.7
0	(8+9)-V-1	-2132	-2.64	32.00	12	-0.64	20.00	31	V	12
0	(8+9)-VII-2	-4325	-5.35	32.00	6.0	-1.29	20.00	15	V	6.0
0	(8+9)-IV-4	-2942	-3.64	32.00	8.8	-0.88	20.00	23	V	8.8
0	(8+9)-VI-4	-3316	-4.10	32.00	7.8	-0.99	20.00	20	V	7.8
0	(8+9)-IV-2	-4231	-5.23	32.00	6.1	-1.27	20.00	16	V	6.1
0	(8+9)-V-2	-4520	-5.59	32.00	5.7	-1.35	20.00	15	V	5.7
0	(8+9)-II-2	-4882	-6.04	32.00	5.3	-1.46	20.00	14	V	5.3
0	(8+9)-VI-2	-5158	-6.38	32.00	5.0	-1.54	20.00	13	V	5.0
0	(8+9)-I-1	-1212	-1.50	32.00	21	-0.36	20.00	55	V	21
0	(8+9)-VII-1	-2327	-2.88	32.00	11	-0.70	20.00	29	V	11
0	(8+9)-VIII-2	-4507	-5.58	32.00	5.7	-1.35	20.00	15	V	5.7
0	(8+9)-II-4	-3592	-4.44	32.00	7.2	-1.08	20.00	19	V	7.2
0	(8+9)-III-1	-1407	-1.74	32.00	18	-0.42	20.00	47	V	18
2400	1	833	1.03	19.20	19	0.25	12.00	48	V	19
2400	2	1644	2.03	28.80	14	0.49	18.00	37	V	14
2400	3	1644	2.03	28.80	14	0.49	18.00	37	V	14
2400	4	833	1.03	25.60	25	0.25	16.00	64	V	25
2400	5	833	1.03	25.60	25	0.25	16.00	64	V	25
2400	6	833	1.03	25.60	25	0.25	16.00	64	V	25
2400	7	833	1.03	25.60	25	0.25	16.00	64	V	25
2400	(8+9)-IV-1	3144	3.89	32.00	8.2	0.94	20.00	21	V	8.2
2400	(8+9)-III-3	3774	4.67	32.00	6.9	1.13	20.00	18	V	6.9
2400	(8+9)-II-1	3795	4.70	32.00	6.8	1.14	20.00	18	V	6.8
2400	(8+9)-I-3	3970	4.91	32.00	6.5	1.19	20.00	17	V	6.5
2400	(8+9)-II-3	5130	6.35	32.00	5.0	1.54	20.00	13	V	5.0
2400	(8+9)-V-4	2522	3.12	32.00	10	0.76	20.00	26	V	10
2400	(8+9)-VII-3	4657	5.76	32.00	5.6	1.39	20.00	14	V	5.6
2400	(8+9)-I-4	1639	2.03	32.00	16	0.49	20.00	41	V	16
2400	(8+9)-VII-4	2717	3.36	32.00	9.5	0.81	20.00	25	V	9.5
2400	(8+9)-VI-1	3531	4.37	32.00	7.3	1.06	20.00	19	V	7.3
2400	(8+9)-VI-3	5395	6.67	32.00	4.8	1.62	20.00	12	V	4.8
2400	(8+9)-V-3	4852	6.00	32.00	5.3	1.45	20.00	14	V	5.3
2400	(8+9)-VIII-1	2879	3.56	32.00	9.0	0.86	20.00	23	V	9.0
2400	(8+9)-III-4	1835	2.27	32.00	14	0.55	20.00	36	V	14
2400	(8+9)-VIII-3	4744	5.87	32.00	5.5	1.42	20.00	14	V	5.5
2400	(8+9)-IV-3	4479	5.54	32.00	5.8	1.34	20.00	15	V	5.8
Verifiche nella direzione secondaria										
1670	1	-1149	-0.99	19.20	19	-0.24	12.00	50	V	19
1670	2	-2417	-2.08	28.80	14	-0.50	18.00	36	V	14
1670	3	-2417	-2.08	28.80	14	-0.50	18.00	36	V	14

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
1670	4	-1149	-0.99	25.60	26	-0.24	16.00	67	V	26
1670	5	-1149	-0.99	25.60	26	-0.24	16.00	67	V	26
1670	6	-1149	-0.99	25.60	26	-0.24	16.00	67	V	26
1670	7	-1149	-0.99	25.60	26	-0.24	16.00	67	V	26
1670	(8+9)-VIII-4	3885	3.34	32.00	9.6	0.81	20.00	25	V	9.6
1670	(8+9)-IV-2	6963	5.99	32.00	5.3	1.45	20.00	14	V	5.3
1670	(8+9)-V-1	2947	2.54	32.00	13	0.61	20.00	33	V	13
1670	(8+9)-I-2	5737	4.94	32.00	6.5	1.20	20.00	17	V	6.5
1670	(8+9)-V-2	7550	6.50	32.00	4.9	1.57	20.00	13	V	4.9
1670	(8+9)-I-4	-2711	-2.33	32.00	14	-0.56	20.00	35	V	14
1670	(8+9)-V-3	-9127	-7.86	32.00	4.1	-1.90	20.00	11	V	4.1
1670	(8+9)-II-2	8150	7.02	32.00	4.6	1.70	20.00	12	V	4.6
1670	(8+9)-V-4	-4524	-3.89	32.00	8.2	-0.94	20.00	21	V	8.2
1670	(8+9)-II-4	5615	4.83	32.00	6.6	1.17	20.00	17	V	6.6
1670	(8+9)-VI-1	-6648	-5.72	32.00	5.6	-1.39	20.00	14	V	5.6
1670	(8+9)-III-2	5380	4.63	32.00	6.9	1.12	20.00	18	V	6.9
1670	(8+9)-VI-2	8694	7.48	32.00	4.3	1.81	20.00	11	V	4.3
1670	(8+9)-III-4	-3067	-2.64	32.00	12	-0.64	20.00	31	V	12
1670	(8+9)-VI-3	-10271	-8.84	32.00	3.6	-2.14	20.00	9.3	V	3.6
1670	(8+9)-I-1	1134	0.98	32.00	33	0.24	20.00	85	V	33
1670	(8+9)-VI-4	5071	4.37	32.00	7.3	1.06	20.00	19	V	7.3
1670	(8+9)-IV-4	4429	3.81	32.00	8.4	0.92	20.00	22	V	8.4
1670	(8+9)-VII-1	3303	2.84	32.00	11	0.69	20.00	29	V	11
1670	(8+9)-II-1	-7192	-6.19	32.00	5.2	-1.50	20.00	13	V	5.2
1670	(8+9)-VII-2	7194	6.19	32.00	5.2	1.50	20.00	13	V	5.2
1670	(8+9)-III-1	1490	1.28	32.00	25	0.31	20.00	64	V	25
1670	(8+9)-VII-3	-8771	-7.55	32.00	4.2	-1.83	20.00	11	V	4.2
1670	(8+9)-IV-1	-6006	-5.17	32.00	6.2	-1.25	20.00	16	V	6.2
1670	(8+9)-VII-4	-4880	-4.20	32.00	7.6	-1.02	20.00	20	V	7.6
1670	(8+9)-III-3	-6957	-5.99	32.00	5.3	-1.45	20.00	14	V	5.3
1670	(8+9)-IV-3	-8540	-7.35	32.00	4.4	-1.78	20.00	11	V	4.4
1670	(8+9)-II-3	-9727	-8.37	32.00	3.8	-2.03	20.00	9.9	V	3.8
1670	(8+9)-VIII-1	-5462	-4.70	32.00	6.8	-1.14	20.00	18	V	6.8
1670	(8+9)-VIII-2	7507	6.46	32.00	5.0	1.56	20.00	13	V	5.0
1670	(8+9)-VIII-3	-9084	-7.82	32.00	4.1	-1.89	20.00	11	V	4.1
1670	(8+9)-I-3	-7313	-6.30	32.00	5.1	-1.52	20.00	13	V	5.1

Verifiche a instabilità

Setto(X)	Comb.	k _{critc}	k _{critm}	λ_{relc}	λ_{relm}	σ_n	σ_{mx}	σ_{my}	f _{td}	f _{cd}	f _{md}	Cs
(cm)						kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	
40(0.0)	(8+9)-VI-2	--	--	--	--	3.16	-0.06	-4.33	132.00	192.00	192.00	21
41(0.0)	(8+9)-VI-3	1.00	--	0.11	--	-1.12	-0.14	1.84	132.00	192.00	192.00	62
42(0.0)	(8+9)-VI-3	--	--	--	--	2.18	0.30	-2.54	132.00	192.00	192.00	32
43(0.0)	3	--	--	--	--	4.13	-1.22	-11.37	118.80	172.80	172.80	9.3
44(220.0)	(8+9)-VI-2	--	--	--	--	8.27	-0.17	16.78	132.00	192.00	192.00	6.6
45(0.0)	(8+9)-VI-3	--	--	--	--	4.42	0.82	5.19	132.00	192.00	192.00	15
46(0.0)	(8+9)-V-3	--	--	--	--	11.66	7.37	14.62	132.00	192.00	192.00	4.9

Parete Xlam 13 - Nodi: [21-26-22-23-27-28-26-27-29-30-30-31-31-8-110-26-109] - **Crit.Prog.** Criterio di verifica XLAM 0 - **Verificato:** [Cs=1.570,Comb=(8+9)-VI-3]

Geometria setti

Setto	Crit.	X	L	S	X90	L90	S90
		mm	cm	cm	mm	cm	cm

Setto	Crit.	X	L	S	X90	L90	S90
40	Criterio di verifica XLAM 0	0	387.0	12.1	0	80.0	12.1
		400	387.0	12.1	1935	80.0	12.1
		800	387.0	12.1	3870	80.0	12.1
41	Criterio di verifica XLAM 0	0	387.0	12.1	0	30.0	12.1
		150	387.0	12.1	1935	30.0	12.1
		300	387.0	12.1	3870	30.0	12.1
42	Criterio di verifica XLAM 0	0	387.0	12.1	0	30.0	12.1
		150	387.0	12.1	1935	30.0	12.1
		300	387.0	12.1	3870	30.0	12.1
43	Criterio di verifica XLAM 0	0	387.0	12.1	0	58.0	12.1
		290	387.0	12.1	1935	58.0	12.1
		580	387.0	12.1	3870	58.0	12.1
44	Criterio di verifica XLAM 0	0	167.0	12.1	0	220.0	12.1
		1100	167.0	12.1	835	220.0	12.1
		2200	167.0	12.1	1670	220.0	12.1
45	Criterio di verifica XLAM 0	0	167.0	12.1	0	240.0	12.1
		1200	167.0	12.1	835	240.0	12.1
		2400	167.0	12.1	1670	240.0	12.1
46	Criterio di verifica XLAM 0	0	167.0	12.1	0	240.0	12.1
		1200	167.0	12.1	835	240.0	12.1
		2400	167.0	12.1	1670	240.0	12.1

Setto 40: origine (1475.9,1983.6,193.5), direzione (-0.199392,0.97992,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	(8+9)-VIII-4	4355	-5	-3921	1.55	-0.07	-2.16	132.00	192.00	192.00	43
0	(8+9)-IV-1	-4925	-7	3983	-1.75	-0.09	2.20	132.00	192.00	192.00	83
0	(8+9)-VII-2	7180	-7	-6381	2.56	-0.10	-3.52	132.00	192.00	192.00	26
0	(8+9)-III-3	-5980	-2	5257	-2.13	-0.03	2.90	132.00	192.00	192.00	65
0	(8+9)-IV-2	7211	-7	-6471	2.57	-0.09	-3.57	132.00	192.00	192.00	26
0	(8+9)-III-4	-2340	-2	2121	-0.83	-0.03	1.17	132.00	192.00	192.00	>100
0	(8+9)-VIII-2	7619	-6	-6745	2.71	-0.08	-3.72	132.00	192.00	192.00	25
0	(8+9)-VII-3	-7341	-4	6169	-2.61	-0.06	3.40	132.00	192.00	192.00	55
0	(8+9)-VII-4	-3701	-4	3033	-1.32	-0.06	1.67	132.00	192.00	192.00	>100
0	(8+9)-I-2	6200	-9	-5798	2.21	-0.12	-3.20	132.00	192.00	192.00	29
0	(8+9)-IV-3	-7373	-5	6260	-2.62	-0.07	3.45	132.00	192.00	192.00	54
0	(8+9)-I-4	-1959	-2	1791	-0.70	-0.02	0.99	132.00	192.00	192.00	>100
0	(8+9)-IV-4	4764	-5	-4195	1.70	-0.06	-2.31	132.00	192.00	192.00	40
0	(8+9)-II-2	8480	-5	-7569	3.02	-0.07	-4.18	132.00	192.00	192.00	22
0	(8+9)-V-1	3158	-8	-2915	1.12	-0.10	-1.61	132.00	192.00	192.00	57
0	(8+9)-II-4	6033	-3	-5293	2.15	-0.04	-2.92	132.00	192.00	192.00	32
0	(8+9)-V-2	7561	-7	-6710	2.69	-0.09	-3.70	132.00	192.00	192.00	25
0	(8+9)-III-2	5819	-9	-5468	2.07	-0.12	-3.02	132.00	192.00	192.00	31
0	(8+9)-V-3	-7722	-5	6499	-2.75	-0.07	3.59	132.00	192.00	192.00	52
0	(8+9)-VIII-1	-4517	-6	3709	-1.61	-0.09	2.05	132.00	192.00	192.00	89
0	(8+9)-V-4	-3320	-4	2703	-1.18	-0.05	1.49	132.00	192.00	192.00	>100
0	(8+9)-I-3	-6361	-3	5586	-2.26	-0.04	3.08	132.00	192.00	192.00	61
0	(8+9)-VI-1	-5786	-8	4807	-2.06	-0.11	2.65	132.00	192.00	192.00	69
0	(8+9)-II-3	-8642	-7	7358	-3.08	-0.09	4.06	132.00	192.00	192.00	46
0	(8+9)-VI-2	8889	-4	-7843	3.16	-0.06	-4.33	132.00	192.00	192.00	21
0	(8+9)-VIII-3	-7781	-6	6533	-2.77	-0.08	3.61	132.00	192.00	192.00	52
0	(8+9)-II-1	-6194	-9	5081	-2.20	-0.12	2.80	132.00	192.00	192.00	65
0	(8+9)-III-1	2178	-9	-2332	0.78	-0.12	-1.29	132.00	192.00	192.00	76
0	(8+9)-I-1	1797	-10	-2003	0.64	-0.13	-1.11	132.00	192.00	192.00	89
0	(8+9)-VI-3	-9050	-7	7632	-3.22	-0.10	4.21	132.00	192.00	192.00	44
0	(8+9)-VI-4	5625	-4	-5019	2.00	-0.05	-2.77	132.00	192.00	192.00	34
0	(8+9)-VII-1	3539	-7	-3245	1.26	-0.10	-1.79	132.00	192.00	192.00	52
800	1	-233	-17	53	-0.08	-0.23	0.03	79.20	115.20	115.20	>100
800	2	-443	-32	111	-0.16	-0.43	0.06	118.80	172.80	172.80	>100
800	3	-443	-32	111	-0.16	-0.43	0.06	118.80	172.80	172.80	>100
800	4	-233	-17	53	-0.08	-0.23	0.03	105.60	153.60	153.60	>100
800	5	-233	-17	53	-0.08	-0.23	0.03	105.60	153.60	153.60	>100

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
800	6	-233	-17	53	-0.08	-0.23	0.03	105.60	153.60	153.60	>100
800	7	-233	-17	53	-0.08	-0.23	0.03	105.60	153.60	153.60	>100
Verifiche nella direzione secondaria											
0	(8+9)-VIII-4	-6681	-21	1311	-17.25	-3.15	25.39	132.00	192.00	192.00	6.4
0	(8+9)-VII-2	-12258	-73	2140	-31.66	-10.75	41.46	132.00	192.00	192.00	3.3
0	(8+9)-III-3	7803	42	-1607	20.15	6.27	-31.12	132.00	192.00	192.00	2.9
0	(8+9)-IV-2	-11184	-50	2114	-28.89	-7.35	40.95	132.00	192.00	192.00	3.6
0	(8+9)-III-4	2755	22	-537	7.11	3.24	-10.41	132.00	192.00	192.00	8.0
0	(8+9)-VIII-2	-11973	-56	2269	-30.92	-8.28	43.95	132.00	192.00	192.00	3.4
0	(8+9)-IV-1	5642	18	-1450	14.57	2.72	-28.09	132.00	192.00	192.00	3.7
0	(8+9)-VII-4	5382	43	-1055	13.90	6.36	-20.44	132.00	192.00	192.00	4.1
0	(8+9)-I-1	-4120	-29	438	-10.64	-4.23	8.49	132.00	192.00	192.00	14
0	(8+9)-IV-3	9357	40	-2098	24.17	5.98	-40.64	132.00	192.00	192.00	2.3
0	(8+9)-I-3	8265	45	-1721	21.35	6.65	-33.34	132.00	192.00	192.00	2.7
0	(8+9)-IV-4	-7469	-28	1466	-19.29	-4.09	28.40	132.00	192.00	192.00	5.6
0	(8+9)-II-1	7184	27	-1832	18.55	4.00	-35.49	132.00	192.00	192.00	2.9
0	(8+9)-V-1	-6747	-50	956	-17.43	-7.34	18.52	132.00	192.00	192.00	7.0
0	(8+9)-II-3	10900	49	-2480	28.15	7.27	-48.04	132.00	192.00	192.00	2.0
0	(8+9)-V-2	-12720	-75	2255	-32.85	-11.13	43.68	132.00	192.00	192.00	3.2
0	(8+9)-III-1	-4582	-31	553	-11.83	-4.61	10.71	132.00	192.00	192.00	12
0	(8+9)-V-3	10893	66	-2239	28.13	9.77	-43.37	132.00	192.00	192.00	2.0
0	(8+9)-VIII-3	10145	47	-2253	26.20	6.92	-43.65	132.00	192.00	192.00	2.2
0	(8+9)-V-4	4920	40	-941	12.71	5.97	-18.22	132.00	192.00	192.00	4.5
0	(8+9)-VII-3	10430	63	-2124	26.94	9.38	-41.15	132.00	192.00	192.00	2.1
0	(8+9)-VI-1	6396	21	-1677	16.52	3.07	-32.48	132.00	192.00	192.00	3.2
0	(8+9)-I-4	2292	19	-423	5.92	2.86	-8.19	132.00	192.00	192.00	9.8
0	(8+9)-VI-2	-13515	-65	2652	-34.91	-9.57	51.36	132.00	192.00	192.00	2.9
0	(8+9)-II-4	-9012	-36	1848	-23.27	-5.37	35.80	132.00	192.00	192.00	4.4
0	(8+9)-VIII-1	4853	12	-1295	12.53	1.78	-25.08	132.00	192.00	192.00	4.3
0	(8+9)-I-2	-10093	-54	1737	-26.07	-8.02	33.65	132.00	192.00	192.00	4.2
0	(8+9)-II-2	-12727	-58	2496	-32.87	-8.63	48.35	132.00	192.00	192.00	3.1
0	(8+9)-III-2	-9630	-52	1622	-24.87	-7.63	31.42	132.00	192.00	192.00	4.5
0	(8+9)-VI-3	11688	55	-2636	30.19	8.20	-51.05	132.00	192.00	192.00	1.9
0	(8+9)-VI-4	-8223	-30	1693	-21.24	-4.43	32.79	132.00	192.00	192.00	4.9
0	(8+9)-VII-1	-7210	-52	1071	-18.62	-7.73	20.75	132.00	192.00	192.00	6.3
3870	1	-220	13	76	-0.57	1.88	1.46	79.20	115.20	115.20	34
3870	2	-476	27	157	-1.23	3.99	3.03	118.80	172.80	172.80	25
3870	3	-476	27	157	-1.23	3.99	3.03	118.80	172.80	172.80	25
3870	4	-220	13	76	-0.57	1.88	1.46	105.60	153.60	153.60	46
3870	5	-220	13	76	-0.57	1.88	1.46	105.60	153.60	153.60	46
3870	6	-220	13	76	-0.57	1.88	1.46	105.60	153.60	153.60	46
3870	7	-220	13	76	-0.57	1.88	1.46	105.60	153.60	153.60	46

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
0	(8+9)-II-2	-20	0.01	6.40	Si	>100
0	(8+9)-IV-2	-18	0.00	6.40	Si	>100
400	(8+9)-VI-2	-42	0.01	6.40	Si	>100
400	(8+9)-VI-3	30	0.01	6.40	Si	>100
400	(8+9)-VIII-2	-47	0.01	6.40	Si	>100
400	(8+9)-VIII-3	34	0.01	6.40	Si	>100
800	1	-10	0.00	3.84	Si	>100
800	2	-17	0.00	5.76	Si	>100
800	3	-17	0.00	5.76	Si	>100
800	4	-10	0.00	5.12	Si	>100
800	5	-10	0.00	5.12	Si	>100
800	6	-10	0.00	5.12	Si	>100
800	7	-10	0.00	5.12	Si	>100
800	(8+9)-VIII-4	-88	0.02	6.40	Si	>100
800	(8+9)-IV-1	71	0.02	6.40	Si	>100
800	(8+9)-V-4	-180	0.05	6.40	Si	>100
800	(8+9)-II-4	-85	0.02	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
800	(8+9)-VI-1	75	0.02	6.40	Si	>100
800	(8+9)-III-2	135	0.04	6.40	Si	>100
800	(8+9)-I-4	-169	0.04	6.40	Si	>100
800	(8+9)-III-4	-169	0.04	6.40	Si	>100
800	(8+9)-I-3	-149	0.04	6.40	Si	>100
800	(8+9)-II-1	71	0.02	6.40	Si	>100
800	(8+9)-VI-4	-89	0.02	6.40	Si	>100
800	(8+9)-IV-4	-85	0.02	6.40	Si	>100
800	(8+9)-VII-1	166	0.04	6.40	Si	>100
800	(8+9)-V-2	146	0.04	6.40	Si	>100
800	(8+9)-VII-2	146	0.04	6.40	Si	>100
800	(8+9)-III-1	155	0.04	6.40	Si	>100
800	(8+9)-VII-3	-160	0.04	6.40	Si	>100
800	(8+9)-II-3	-20	0.01	6.40	Si	>100
800	(8+9)-VII-4	-180	0.05	6.40	Si	>100
800	(8+9)-III-3	-149	0.04	6.40	Si	>100
800	(8+9)-IV-3	-20	0.01	6.40	Si	>100
800	(8+9)-V-3	-160	0.04	6.40	Si	>100
800	(8+9)-VIII-1	74	0.02	6.40	Si	>100
800	(8+9)-I-2	135	0.04	6.40	Si	>100
800	(8+9)-I-1	155	0.04	6.40	Si	>100
800	(8+9)-V-1	166	0.04	6.40	Si	>100
Verifiche nella direzione secondaria						
0	(8+9)-VIII-4	37	0.09	6.40	Si	72
0	(8+9)-VI-2	103	0.24	6.40	Si	26
0	(8+9)-VI-4	53	0.13	6.40	Si	51
0	(8+9)-IV-2	75	0.18	6.40	Si	36
0	(8+9)-III-2	69	0.17	6.40	Si	39
0	(8+9)-VIII-2	87	0.21	6.40	Si	31
0	(8+9)-III-3	-47	0.11	6.40	Si	57
0	(8+9)-VII-3	-88	0.21	6.40	Si	31
0	(8+9)-VII-1	79	0.19	6.40	Si	34
0	(8+9)-VI-3	-80	0.19	6.40	Si	33
0	(8+9)-I-3	-52	0.12	6.40	Si	52
0	(8+9)-VI-1	-30	0.07	6.40	Si	89
0	(8+9)-I-4	-12	0.03	6.40	Si	>100
0	(8+9)-II-1	-42	0.10	6.40	Si	63
0	(8+9)-II-3	-68	0.16	6.40	Si	39
0	(8+9)-IV-3	-53	0.13	6.40	Si	51
0	(8+9)-VIII-3	-65	0.15	6.40	Si	41
0	(8+9)-IV-4	49	0.12	6.40	Si	54
0	(8+9)-VII-2	110	0.26	6.40	Si	24
0	(8+9)-V-1	75	0.18	6.40	Si	36
0	(8+9)-II-2	91	0.22	6.40	Si	30
0	(8+9)-VII-4	-57	0.14	6.40	Si	47
0	(8+9)-I-2	74	0.18	6.40	Si	36
0	(8+9)-II-4	65	0.15	6.40	Si	41
0	(8+9)-V-2	115	0.27	6.40	Si	23
0	(8+9)-V-3	-92	0.22	6.40	Si	29
0	(8+9)-V-4	-52	0.12	6.40	Si	51
1935	(8+9)-III-4	-26	0.06	6.40	Si	>100
3870	1	31	0.07	3.84	Si	51
3870	2	67	0.16	5.76	Si	36
3870	3	67	0.16	5.76	Si	36
3870	4	31	0.07	5.12	Si	69
3870	5	31	0.07	5.12	Si	69
3870	6	31	0.07	5.12	Si	69
3870	7	31	0.07	5.12	Si	69
3870	(8+9)-VIII-1	29	0.07	6.40	Si	93
3870	(8+9)-I-1	53	0.13	6.40	Si	51
3870	(8+9)-III-1	53	0.13	6.40	Si	51
3870	(8+9)-IV-1	27	0.06	6.40	Si	99

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
400	(8+9)-I-4	2398	1.28	32.00	25	0.31	20.00	65	V	25
400	(8+9)-III-4	2839	1.52	32.00	21	0.37	20.00	55	V	21
800	1	-356	-0.19	19.20	>100	-0.05	12.00	>100	V	>100
800	2	-750	-0.40	28.80	72	-0.10	18.00	>100	V	72
800	3	-750	-0.40	28.80	72	-0.10	18.00	>100	V	72
800	4	-356	-0.19	25.60	>100	-0.05	16.00	>100	V	>100
800	5	-356	-0.19	25.60	>100	-0.05	16.00	>100	V	>100
800	6	-356	-0.19	25.60	>100	-0.05	16.00	>100	V	>100
800	7	-356	-0.19	25.60	>100	-0.05	16.00	>100	V	>100
800	(8+9)-VIII-4	-8636	-4.61	32.00	6.9	-1.12	20.00	18	V	6.9
800	(8+9)-IV-1	9103	4.86	32.00	6.6	1.18	20.00	17	V	6.6
800	(8+9)-V-2	-13775	-7.35	32.00	4.4	-1.78	20.00	11	V	4.4
800	(8+9)-I-3	10110	5.40	32.00	5.9	1.31	20.00	15	V	5.9
800	(8+9)-V-3	13289	7.09	32.00	4.5	1.72	20.00	12	V	4.5
800	(8+9)-II-2	-15223	-8.13	32.00	3.9	-1.97	20.00	10	V	3.9
800	(8+9)-V-4	5460	2.91	32.00	11	0.71	20.00	28	V	11
800	(8+9)-II-4	-11360	-6.06	32.00	5.3	-1.47	20.00	14	V	5.3
800	(8+9)-VI-1	9920	5.30	32.00	6.0	1.28	20.00	16	V	6.0
800	(8+9)-III-2	-10065	-5.37	32.00	6.0	-1.30	20.00	15	V	6.0
800	(8+9)-VI-2	-16177	-8.64	32.00	3.7	-2.09	20.00	9.6	V	3.7
800	(8+9)-I-2	-10596	-5.66	32.00	5.7	-1.37	20.00	15	V	5.7
800	(8+9)-VI-3	15691	8.38	32.00	3.8	2.03	20.00	9.9	V	3.8
800	(8+9)-IV-2	-13453	-7.18	32.00	4.5	-1.74	20.00	12	V	4.5
800	(8+9)-VI-4	-10406	-5.56	32.00	5.8	-1.34	20.00	15	V	5.8
800	(8+9)-IV-4	-9589	-5.12	32.00	6.3	-1.24	20.00	16	V	6.3
800	(8+9)-VII-1	-6477	-3.46	32.00	9.3	-0.84	20.00	24	V	9.3
800	(8+9)-II-1	10874	5.81	32.00	5.5	1.40	20.00	14	V	5.5
800	(8+9)-VII-2	-13244	-7.07	32.00	4.5	-1.71	20.00	12	V	4.5
800	(8+9)-III-1	-3298	-1.76	32.00	18	-0.43	20.00	47	V	18
800	(8+9)-VII-3	12758	6.81	32.00	4.7	1.65	20.00	12	V	4.7
800	(8+9)-I-1	-2767	-1.48	32.00	22	-0.36	20.00	56	V	22
800	(8+9)-VII-4	5991	3.20	32.00	10	0.77	20.00	26	V	10
800	(8+9)-III-3	9579	5.11	32.00	6.3	1.24	20.00	16	V	6.3
800	(8+9)-IV-3	12967	6.92	32.00	4.6	1.68	20.00	12	V	4.6
800	(8+9)-II-3	14737	7.87	32.00	4.1	1.90	20.00	11	V	4.1
800	(8+9)-VIII-1	8150	4.35	32.00	7.4	1.05	20.00	19	V	7.4
800	(8+9)-VIII-2	-14406	-7.69	32.00	4.2	-1.86	20.00	11	V	4.2
800	(8+9)-VIII-3	13920	7.43	32.00	4.3	1.80	20.00	11	V	4.3
800	(8+9)-V-1	-5946	-3.17	32.00	10	-0.77	20.00	26	V	10
Verifiche nella direzione secondaria										
0	1	64	0.16	19.20	>100	0.04	12.00	>100	V	>100
0	2	99	0.26	28.80	>100	0.06	18.00	>100	V	>100
0	3	99	0.26	28.80	>100	0.06	18.00	>100	V	>100
0	4	64	0.16	25.60	>100	0.04	16.00	>100	V	>100
0	5	64	0.16	25.60	>100	0.04	16.00	>100	V	>100
0	6	64	0.16	25.60	>100	0.04	16.00	>100	V	>100
0	7	64	0.16	25.60	>100	0.04	16.00	>100	V	>100
1935	(8+9)-VIII-4	2420	6.25	32.00	5.1	1.51	20.00	13	V	5.1
1935	(8+9)-IV-2	4108	10.61	32.00	3.0	2.57	20.00	7.8	V	3.0
1935	(8+9)-V-1	2038	5.26	32.00	6.1	1.27	20.00	16	V	6.1
1935	(8+9)-I-2	3539	9.14	32.00	3.5	2.21	20.00	9.0	V	3.5
1935	(8+9)-V-2	4488	11.59	32.00	2.8	2.80	20.00	7.1	V	2.8
1935	(8+9)-I-4	-1139	-2.94	32.00	11	-0.71	20.00	28	V	11
1935	(8+9)-V-3	-4537	-11.72	32.00	2.7	-2.84	20.00	7.1	V	2.7
1935	(8+9)-II-2	4760	12.29	32.00	2.6	2.98	20.00	6.7	V	2.6
1935	(8+9)-V-4	-2087	-5.39	32.00	5.9	-1.30	20.00	15	V	5.9
1935	(8+9)-II-4	3357	8.67	32.00	3.7	2.10	20.00	9.5	V	3.7
1935	(8+9)-VI-1	-3121	-8.06	32.00	4.0	-1.95	20.00	10	V	4.0
1935	(8+9)-III-2	3344	8.64	32.00	3.7	2.09	20.00	9.6	V	3.7
1935	(8+9)-VI-2	5045	13.03	32.00	2.5	3.15	20.00	6.3	V	2.5
1935	(8+9)-III-4	-1334	-3.45	32.00	9.3	-0.83	20.00	24	V	9.3
1935	(8+9)-VI-3	-5094	-13.16	32.00	2.4	-3.18	20.00	6.3	V	2.4

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
1935	(8+9)-I-1	1090	2.81	32.00	11	0.68	20.00	29	V	11
1935	(8+9)-VI-4	3072	7.93	32.00	4.0	1.92	20.00	10	V	4.0
1935	(8+9)-IV-4	2705	6.98	32.00	4.6	1.69	20.00	12	V	4.6
1935	(8+9)-VII-1	2234	5.77	32.00	5.5	1.40	20.00	14	V	5.5
1935	(8+9)-II-1	-3406	-8.80	32.00	3.6	-2.13	20.00	9.4	V	3.6
1935	(8+9)-VII-2	4292	11.09	32.00	2.9	2.68	20.00	7.5	V	2.9
1935	(8+9)-III-1	1285	3.32	32.00	9.6	0.80	20.00	25	V	9.6
1935	(8+9)-VII-3	-4341	-11.21	32.00	2.9	-2.71	20.00	7.4	V	2.9
1935	(8+9)-IV-1	-2754	-7.11	32.00	4.5	-1.72	20.00	12	V	4.5
1935	(8+9)-VII-4	-2283	-5.90	32.00	5.4	-1.43	20.00	14	V	5.4
1935	(8+9)-III-3	-3393	-8.76	32.00	3.7	-2.12	20.00	9.4	V	3.7
1935	(8+9)-IV-3	-4157	-10.74	32.00	3.0	-2.60	20.00	7.7	V	3.0
1935	(8+9)-II-3	-4809	-12.42	32.00	2.6	-3.01	20.00	6.7	V	2.6
1935	(8+9)-VIII-1	-2469	-6.38	32.00	5.0	-1.54	20.00	13	V	5.0
1935	(8+9)-VIII-2	4392	11.34	32.00	2.8	2.75	20.00	7.3	V	2.8
1935	(8+9)-VIII-3	-4442	-11.47	32.00	2.8	-2.78	20.00	7.2	V	2.8
1935	(8+9)-I-3	-3588	-9.27	32.00	3.5	-2.24	20.00	8.9	V	3.5

Setto 41: origine (1525.8,1738.6,193.5), direzione (-0.199392,0.97992,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	1	-461	-16	411	-0.16	-0.22	0.23	79.20	115.20	115.20	>100
0	2	-950	-34	862	-0.34	-0.46	0.48	118.80	172.80	172.80	>100
0	3	-950	-34	862	-0.34	-0.46	0.48	118.80	172.80	172.80	>100
0	4	-461	-16	411	-0.16	-0.22	0.23	105.60	153.60	153.60	>100
0	5	-461	-16	411	-0.16	-0.22	0.23	105.60	153.60	153.60	>100
0	6	-461	-16	411	-0.16	-0.22	0.23	105.60	153.60	153.60	>100
0	7	-461	-16	411	-0.16	-0.22	0.23	105.60	153.60	153.60	>100
0	(8+9)-VIII-4	1076	-25	-1119	0.38	-0.34	-0.62	132.00	192.00	192.00	>100
0	(8+9)-IV-1	-1828	4	1841	-0.65	0.06	1.02	132.00	192.00	192.00	>100
0	(8+9)-V-1	577	9	-933	0.21	0.13	-0.51	132.00	192.00	192.00	>100
0	(8+9)-I-2	1541	9	-1844	0.55	0.12	-1.02	132.00	192.00	192.00	99
0	(8+9)-V-2	1992	6	-2422	0.71	0.08	-1.34	132.00	192.00	192.00	79
0	(8+9)-I-4	-742	-35	903	-0.26	-0.46	0.50	132.00	192.00	192.00	>100
0	(8+9)-V-3	-2608	-28	2970	-0.93	-0.37	1.64	132.00	192.00	192.00	95
0	(8+9)-II-2	2393	-11	-2619	0.85	-0.14	-1.45	132.00	192.00	192.00	68
0	(8+9)-V-4	-1193	-31	1482	-0.42	-0.42	0.82	132.00	192.00	192.00	>100
0	(8+9)-II-4	1708	-24	-1795	0.61	-0.32	-0.99	132.00	192.00	192.00	88
0	(8+9)-VI-1	-2189	1	2170	-0.78	0.01	1.20	132.00	192.00	192.00	>100
0	(8+9)-III-2	1392	8	-1693	0.50	0.11	-0.93	132.00	192.00	192.00	>100
0	(8+9)-VI-2	2528	-12	-2793	0.90	-0.16	-1.54	132.00	192.00	192.00	64
0	(8+9)-III-4	-891	-35	1054	-0.32	-0.47	0.58	132.00	192.00	192.00	>100
0	(8+9)-VI-3	-3145	-10	3341	-1.12	-0.14	1.84	132.00	192.00	192.00	96
0	(8+9)-IV-2	1897	-13	-2117	0.68	-0.18	-1.17	132.00	192.00	192.00	82
0	(8+9)-VI-4	1573	-23	-1622	0.56	-0.30	-0.89	132.00	192.00	192.00	95
0	(8+9)-IV-4	1212	-26	-1293	0.43	-0.35	-0.71	132.00	192.00	192.00	>100
0	(8+9)-VII-1	726	10	-1084	0.26	0.14	-0.60	132.00	192.00	192.00	>100
0	(8+9)-II-1	-2324	2	2344	-0.83	0.02	1.29	132.00	192.00	192.00	>100
0	(8+9)-VII-2	1843	5	-2271	0.66	0.07	-1.25	132.00	192.00	192.00	84
0	(8+9)-III-1	275	13	-506	0.10	0.18	-0.28	132.00	192.00	192.00	>100
0	(8+9)-VII-3	-2459	-27	2820	-0.88	-0.36	1.56	132.00	192.00	192.00	100
0	(8+9)-I-1	126	12	-355	0.04	0.17	-0.20	132.00	192.00	192.00	>100
0	(8+9)-VII-4	-1342	-32	1632	-0.48	-0.43	0.90	132.00	192.00	192.00	>100
0	(8+9)-III-3	-2009	-30	2241	-0.71	-0.40	1.24	132.00	192.00	192.00	>100
0	(8+9)-IV-3	-2513	-9	2665	-0.89	-0.12	1.47	132.00	192.00	192.00	>100
0	(8+9)-II-3	-3009	-11	3168	-1.07	-0.15	1.75	132.00	192.00	192.00	>100
0	(8+9)-VIII-1	-1693	3	1668	-0.60	0.04	0.92	132.00	192.00	192.00	>100
0	(8+9)-VIII-2	2032	-14	-2290	0.72	-0.19	-1.26	132.00	192.00	192.00	77
0	(8+9)-VIII-3	-2648	-8	2839	-0.94	-0.11	1.57	132.00	192.00	192.00	>100
0	(8+9)-I-3	-2157	-31	2392	-0.77	-0.41	1.32	132.00	192.00	192.00	>100
Verifiche nella direzione secondaria											
0	1	-926	5	13	-6.38	1.98	1.72	79.20	115.20	115.20	28

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	4	-926	5	13	-6.38	1.98	1.72	105.60	153.60	153.60	39
0	5	-926	5	13	-6.38	1.98	1.72	105.60	153.60	153.60	39
0	6	-926	5	13	-6.38	1.98	1.72	105.60	153.60	153.60	39
0	7	-926	5	13	-6.38	1.98	1.72	105.60	153.60	153.60	39
0	(8+9)-VIII-4	-960	5	406	-6.61	2.00	55.91	132.00	192.00	192.00	3.3
0	(8+9)-IV-2	-1231	-5	692	-8.47	-2.01	95.29	132.00	192.00	192.00	2.0
0	(8+9)-V-1	-1055	-7	362	-7.26	-2.80	49.88	132.00	192.00	192.00	3.6
0	(8+9)-I-1	-827	-18	205	-5.69	-7.21	28.22	132.00	192.00	192.00	5.4
0	(8+9)-V-2	-1396	-9	767	-9.62	-3.49	105.60	132.00	192.00	192.00	1.8
0	(8+9)-I-3	-154	27	-591	-1.06	10.57	-81.41	132.00	192.00	192.00	2.1
0	(8+9)-V-3	74	16	-748	0.51	6.16	-103.08	132.00	192.00	192.00	1.7
0	(8+9)-II-1	-193	-0	-546	-1.33	-0.18	-75.16	132.00	192.00	192.00	2.5
0	(8+9)-V-4	-267	14	-344	-1.84	5.48	-47.35	132.00	192.00	192.00	3.6
0	(8+9)-II-3	9	13	-784	0.06	5.15	-108.05	132.00	192.00	192.00	1.7
0	(8+9)-VI-1	-261	3	-499	-1.80	1.14	-68.66	132.00	192.00	192.00	2.7
0	(8+9)-III-1	-857	-19	238	-5.90	-7.35	32.80	132.00	192.00	192.00	4.8
0	(8+9)-VI-2	-1399	-3	850	-9.64	-1.15	117.08	132.00	192.00	192.00	1.6
0	(8+9)-III-3	-184	26	-558	-1.27	10.43	-76.83	132.00	192.00	192.00	2.2
0	(8+9)-VI-3	77	10	-832	0.53	3.83	-114.55	132.00	192.00	192.00	1.6
0	(8+9)-IV-1	-293	-2	-435	-2.02	-0.65	-59.88	132.00	192.00	192.00	3.2
0	(8+9)-VI-4	-1061	4	517	-7.31	1.54	71.19	132.00	192.00	192.00	2.6
0	(8+9)-IV-3	-91	12	-674	-0.63	4.69	-92.77	132.00	192.00	192.00	2.0
0	(8+9)-VII-1	-1085	-7	395	-7.47	-2.94	54.46	132.00	192.00	192.00	3.3
0	(8+9)-I-2	-1168	-20	609	-8.04	-7.89	83.94	132.00	192.00	192.00	2.1
0	(8+9)-VII-2	-1366	-9	733	-9.41	-3.35	101.02	132.00	192.00	192.00	1.8
0	(8+9)-II-2	-1331	-6	803	-9.17	-2.47	110.58	132.00	192.00	192.00	1.7
0	(8+9)-VII-3	44	15	-715	0.30	6.03	-98.49	132.00	192.00	192.00	1.8
0	(8+9)-III-2	-1138	-20	576	-7.84	-7.76	79.35	132.00	192.00	192.00	2.2
0	(8+9)-VIII-3	-23	9	-721	-0.16	3.37	-99.27	132.00	192.00	192.00	1.9
0	(8+9)-III-4	-465	25	-220	-3.20	10.02	-30.28	132.00	192.00	192.00	4.8
0	(8+9)-I-4	-495	25	-187	-3.41	9.88	-25.69	132.00	192.00	192.00	5.4
0	(8+9)-II-4	-1129	7	564	-7.78	2.86	77.69	132.00	192.00	192.00	2.4
0	(8+9)-IV-4	-1029	8	453	-7.08	3.32	62.41	132.00	192.00	192.00	2.9
0	(8+9)-VII-4	-237	14	-377	-1.63	5.62	-51.94	132.00	192.00	192.00	3.3
0	(8+9)-VIII-1	-362	2	-388	-2.49	0.68	-53.38	132.00	192.00	192.00	3.5
0	(8+9)-VIII-2	-1299	-2	739	-8.95	-0.69	101.79	132.00	192.00	192.00	1.9
3870	2	-48	-14	-20	-0.33	-5.46	-2.79	118.80	172.80	172.80	21
3870	3	-48	-14	-20	-0.33	-5.46	-2.79	118.80	172.80	172.80	21

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Ty kg	τ_d kg/cmq	fvd kg/cmq	RS	Cs
0	(8+9)-IV-1	17	0.00	6.40	Si	>100
0	(8+9)-VIII-1	15	0.00	6.40	Si	>100
0	(8+9)-VI-1	18	0.00	6.40	Si	>100
0	(8+9)-II-1	20	0.01	6.40	Si	>100
150	(8+9)-VIII-4	14	0.00	6.40	Si	>100
150	(8+9)-VII-2	-28	0.01	6.40	Si	>100
150	(8+9)-VII-4	45	0.01	6.40	Si	>100
150	(8+9)-IV-4	10	0.00	6.40	Si	>100
150	(8+9)-IV-2	-4	0.00	6.40	Si	>100
150	(8+9)-I-1	-10	0.00	6.40	Si	>100
150	(8+9)-IV-3	26	0.01	6.40	Si	>100
150	(8+9)-I-3	38	0.01	6.40	Si	>100
150	(8+9)-VIII-2	-8	0.00	6.40	Si	>100
150	(8+9)-V-1	-23	0.01	6.40	Si	>100
150	(8+9)-II-3	29	0.01	6.40	Si	>100
150	(8+9)-V-2	-29	0.01	6.40	Si	>100
150	(8+9)-III-1	-11	0.00	6.40	Si	>100
150	(8+9)-V-3	51	0.01	6.40	Si	>100
150	(8+9)-III-3	37	0.01	6.40	Si	>100
150	(8+9)-V-4	44	0.01	6.40	Si	>100
150	(8+9)-VIII-3	29	0.01	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
150	(8+9)-VII-3	50	0.01	6.40	Si	>100
150	(8+9)-I-4	31	0.01	6.40	Si	>100
150	(8+9)-VI-2	-12	0.00	6.40	Si	>100
150	(8+9)-II-4	7	0.00	6.40	Si	>100
150	(8+9)-III-4	32	0.01	6.40	Si	>100
150	(8+9)-I-2	-17	0.00	6.40	Si	>100
150	(8+9)-II-2	-8	0.00	6.40	Si	>100
150	(8+9)-III-2	-16	0.00	6.40	Si	>100
150	(8+9)-VI-3	33	0.01	6.40	Si	>100
150	(8+9)-VI-4	10	0.00	6.40	Si	>100
150	(8+9)-VII-1	-24	0.01	6.40	Si	>100
300	1	16	0.00	3.84	Si	>100
300	2	34	0.01	5.76	Si	>100
300	3	34	0.01	5.76	Si	>100
300	4	16	0.00	5.12	Si	>100
300	5	16	0.00	5.12	Si	>100
300	6	16	0.00	5.12	Si	>100
300	7	16	0.00	5.12	Si	>100
Verifiche nella direzione secondaria						
0	1	-8	0.05	3.84	Si	77
0	2	-16	0.10	5.76	Si	55
0	3	-16	0.10	5.76	Si	55
0	4	-8	0.05	5.12	Si	>100
0	5	-8	0.05	5.12	Si	>100
0	6	-8	0.05	5.12	Si	>100
0	7	-8	0.05	5.12	Si	>100
0	(8+9)-V-3	-11	0.07	6.40	Si	88
0	(8+9)-II-3	-13	0.08	6.40	Si	78
0	(8+9)-III-3	-10	0.07	6.40	Si	98
0	(8+9)-VIII-1	-10	0.06	6.40	Si	>100
0	(8+9)-III-4	-7	0.04	6.40	Si	>100
0	(8+9)-I-4	-7	0.04	6.40	Si	>100
0	(8+9)-IV-1	-10	0.06	6.40	Si	>100
0	(8+9)-II-2	2	0.01	6.40	Si	>100
0	(8+9)-VII-4	-8	0.05	6.40	Si	>100
0	(8+9)-IV-3	-12	0.08	6.40	Si	84
0	(8+9)-VI-3	-13	0.08	6.40	Si	77
0	(8+9)-II-1	-11	0.07	6.40	Si	92
0	(8+9)-VIII-3	-12	0.08	6.40	Si	83
0	(8+9)-VII-3	-11	0.07	6.40	Si	90
0	(8+9)-I-3	-11	0.07	6.40	Si	95
0	(8+9)-VI-2	2	0.01	6.40	Si	>100
0	(8+9)-VI-1	-11	0.07	6.40	Si	94
0	(8+9)-V-4	-8	0.05	6.40	Si	>100
1935	(8+9)-VIII-4	-1	0.01	6.40	Si	>100
1935	(8+9)-VII-1	-3	0.02	6.40	Si	>100
1935	(8+9)-V-1	-4	0.02	6.40	Si	>100
1935	(8+9)-I-1	-4	0.03	6.40	Si	>100
1935	(8+9)-III-1	-4	0.03	6.40	Si	>100
3870	(8+9)-IV-2	2	0.01	6.40	Si	>100
3870	(8+9)-VII-2	3	0.02	6.40	Si	>100
3870	(8+9)-VI-4	1	0.01	6.40	Si	>100
3870	(8+9)-III-2	2	0.01	6.40	Si	>100
3870	(8+9)-II-4	1	0.01	6.40	Si	>100
3870	(8+9)-I-2	2	0.01	6.40	Si	>100
3870	(8+9)-VIII-2	2	0.01	6.40	Si	>100
3870	(8+9)-IV-4	1	0.01	6.40	Si	>100
3870	(8+9)-V-2	3	0.02	6.40	Si	>100

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	1	-178	-0.09	19.20	>100	-0.02	12.00	>100	V	>100

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
0	2	-287	-0.15	28.80	>100	-0.04	18.00	>100	V	>100
0	3	-287	-0.15	28.80	>100	-0.04	18.00	>100	V	>100
0	4	-178	-0.09	25.60	>100	-0.02	16.00	>100	V	>100
0	5	-178	-0.09	25.60	>100	-0.02	16.00	>100	V	>100
0	6	-178	-0.09	25.60	>100	-0.02	16.00	>100	V	>100
0	7	-178	-0.09	25.60	>100	-0.02	16.00	>100	V	>100
0	(8+9)-IV-3	6352	3.39	32.00	9.4	0.82	20.00	24	V	9.4
0	(8+9)-VIII-1	3948	2.11	32.00	15	0.51	20.00	39	V	15
0	(8+9)-I-1	-2083	-1.11	32.00	29	-0.27	20.00	74	V	29
0	(8+9)-I-2	-5881	-3.14	32.00	10	-0.76	20.00	26	V	10
0	(8+9)-IV-4	-4295	-2.29	32.00	14	-0.55	20.00	36	V	14
0	(8+9)-I-4	1827	0.98	32.00	33	0.24	20.00	85	V	33
0	(8+9)-II-2	-7614	-4.06	32.00	7.9	-0.98	20.00	20	V	7.9
0	(8+9)-VI-2	-7705	-4.11	32.00	7.8	-1.00	20.00	20	V	7.8
0	(8+9)-I-3	5625	3.00	32.00	11	0.73	20.00	28	V	11
0	(8+9)-II-4	-5301	-2.83	32.00	11	-0.68	20.00	29	V	11
0	(8+9)-II-1	5046	2.69	32.00	12	0.65	20.00	31	V	12
0	(8+9)-III-2	-5579	-2.98	32.00	11	-0.72	20.00	28	V	11
0	(8+9)-II-3	7358	3.93	32.00	8.1	0.95	20.00	21	V	8.1
0	(8+9)-III-4	2129	1.14	32.00	28	0.28	20.00	73	V	28
0	(8+9)-IV-2	-6608	-3.53	32.00	9.1	-0.85	20.00	23	V	9.1
0	(8+9)-III-3	5323	2.84	32.00	11	0.69	20.00	29	V	11
0	(8+9)-IV-1	4040	2.16	32.00	15	0.52	20.00	38	V	15
0	(8+9)-III-1	-2385	-1.27	32.00	25	-0.31	20.00	65	V	25
0	(8+9)-VI-4	-5210	-2.78	32.00	12	-0.67	20.00	30	V	12
0	(8+9)-VIII-4	-4204	-2.24	32.00	14	-0.54	20.00	37	V	14
0	(8+9)-VI-1	4954	2.65	32.00	12	0.64	20.00	31	V	12
150	(8+9)-V-1	-4086	-2.18	32.00	15	-0.53	20.00	38	V	15
150	(8+9)-VIII-2	-6720	-3.59	32.00	8.9	-0.87	20.00	23	V	8.9
150	(8+9)-V-2	-7600	-4.06	32.00	7.9	-0.98	20.00	20	V	7.9
150	(8+9)-VII-1	-4371	-2.33	32.00	14	-0.56	20.00	35	V	14
150	(8+9)-VII-2	-7315	-3.91	32.00	8.2	-0.95	20.00	21	V	8.2
300	(8+9)-V-3	7434	3.97	32.00	8.1	0.96	20.00	21	V	8.1
300	(8+9)-VII-4	4212	2.25	32.00	14	0.54	20.00	37	V	14
300	(8+9)-VII-3	7149	3.82	32.00	8.4	0.92	20.00	22	V	8.4
300	(8+9)-VI-3	7505	4.01	32.00	8.0	0.97	20.00	21	V	8.0
300	(8+9)-VIII-3	6556	3.50	32.00	9.1	0.85	20.00	24	V	9.1
300	(8+9)-V-4	3927	2.10	32.00	15	0.51	20.00	39	V	15
Verifiche nella direzione secondaria										
0	2	11	0.07	28.80	>100	0.02	18.00	>100	V	>100
0	3	11	0.07	28.80	>100	0.02	18.00	>100	V	>100
3870	1	8	0.05	19.20	>100	0.01	12.00	>100	V	>100
3870	4	8	0.05	25.60	>100	0.01	16.00	>100	V	>100
3870	5	8	0.05	25.60	>100	0.01	16.00	>100	V	>100
3870	6	8	0.05	25.60	>100	0.01	16.00	>100	V	>100
3870	7	8	0.05	25.60	>100	0.01	16.00	>100	V	>100
3870	(8+9)-VIII-4	847	5.83	32.00	5.5	1.41	20.00	14	V	5.5
3870	(8+9)-IV-3	-1412	-9.73	32.00	3.3	-2.35	20.00	8.5	V	3.3
3870	(8+9)-V-1	716	4.93	32.00	6.5	1.19	20.00	17	V	6.5
3870	(8+9)-I-2	1212	8.35	32.00	3.8	2.02	20.00	9.9	V	3.8
3870	(8+9)-V-2	1557	10.72	32.00	3.0	2.59	20.00	7.7	V	3.0
3870	(8+9)-I-4	-361	-2.49	32.00	13	-0.60	20.00	33	V	13
3870	(8+9)-V-3	-1547	-10.65	32.00	3.0	-2.58	20.00	7.8	V	3.0
3870	(8+9)-II-2	1642	11.31	32.00	2.8	2.74	20.00	7.3	V	2.8
3870	(8+9)-V-4	-706	-4.86	32.00	6.6	-1.18	20.00	17	V	6.6
3870	(8+9)-II-4	1170	8.06	32.00	4.0	1.95	20.00	10	V	4.0
3870	(8+9)-VI-1	-1057	-7.28	32.00	4.4	-1.76	20.00	11	V	4.4
3870	(8+9)-III-2	1146	7.89	32.00	4.1	1.91	20.00	10	V	4.1
3870	(8+9)-VI-2	1745	12.02	32.00	2.7	2.91	20.00	6.9	V	2.7
3870	(8+9)-III-4	-427	-2.94	32.00	11	-0.71	20.00	28	V	11
3870	(8+9)-VI-3	-1735	-11.95	32.00	2.7	-2.89	20.00	6.9	V	2.7
3870	(8+9)-IV-2	1422	9.79	32.00	3.3	2.37	20.00	8.4	V	3.3
3870	(8+9)-VI-4	1067	7.35	32.00	4.4	1.78	20.00	11	V	4.4
3870	(8+9)-IV-4	950	6.54	32.00	4.9	1.58	20.00	13	V	4.9

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
3870	(8+9)-VII-1	782	5.39	32.00	5.9	1.30	20.00	15	V	5.9
3870	(8+9)-II-1	-1160	-7.99	32.00	4.0	-1.93	20.00	10	V	4.0
3870	(8+9)-VII-2	1491	10.27	32.00	3.1	2.48	20.00	8.0	V	3.1
3870	(8+9)-III-1	437	3.01	32.00	11	0.73	20.00	27	V	11
3870	(8+9)-VII-3	-1481	-10.20	32.00	3.1	-2.47	20.00	8.1	V	3.1
3870	(8+9)-IV-1	-940	-6.47	32.00	4.9	-1.57	20.00	13	V	4.9
3870	(8+9)-VII-4	-772	-5.32	32.00	6.0	-1.29	20.00	16	V	6.0
3870	(8+9)-III-3	-1136	-7.82	32.00	4.1	-1.89	20.00	11	V	4.1
3870	(8+9)-I-1	371	2.56	32.00	13	0.62	20.00	32	V	13
3870	(8+9)-II-3	-1632	-11.24	32.00	2.8	-2.72	20.00	7.4	V	2.8
3870	(8+9)-VIII-1	-837	-5.76	32.00	5.6	-1.39	20.00	14	V	5.6
3870	(8+9)-VIII-2	1526	10.51	32.00	3.0	2.54	20.00	7.9	V	3.0
3870	(8+9)-VIII-3	-1516	-10.44	32.00	3.1	-2.53	20.00	7.9	V	3.1
3870	(8+9)-I-3	-1202	-8.28	32.00	3.9	-2.00	20.00	10.0	V	3.9

Setto 42: origine (1579.6,1474.1,193.5), direzione (-0.199392,0.97992,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	1	181	-2	-316	0.06	-0.02	-0.17	79.20	115.20	115.20	>100
0	2	478	-3	-721	0.17	-0.04	-0.40	118.80	172.80	172.80	>100
0	3	478	-3	-721	0.17	-0.04	-0.40	118.80	172.80	172.80	>100
0	4	181	-2	-316	0.06	-0.02	-0.17	105.60	153.60	153.60	>100
0	5	181	-2	-316	0.06	-0.02	-0.17	105.60	153.60	153.60	>100
0	6	181	-2	-316	0.06	-0.02	-0.17	105.60	153.60	153.60	>100
0	7	181	-2	-316	0.06	-0.02	-0.17	105.60	153.60	153.60	>100
0	(8+9)-IV-1	3470	-0	-2689	1.24	-0.01	-1.48	132.00	192.00	192.00	58
0	(8+9)-VI-1	3711	3	-2791	1.32	0.04	-1.54	132.00	192.00	192.00	55
0	(8+9)-III-4	1634	24	-1304	0.58	0.32	-0.72	132.00	192.00	192.00	>100
0	(8+9)-V-1	-2461	-29	1754	-0.88	-0.38	0.97	132.00	192.00	192.00	>100
0	(8+9)-I-4	1446	23	-1182	0.51	0.30	-0.65	132.00	192.00	192.00	>100
0	(8+9)-VII-3	5408	33	-4165	1.92	0.45	-2.30	132.00	192.00	192.00	35
0	(8+9)-VIII-3	5504	17	-4195	1.96	0.23	-2.31	132.00	192.00	192.00	36
0	(8+9)-IV-3	5122	16	-3888	1.82	0.22	-2.15	132.00	192.00	192.00	38
0	(8+9)-VIII-1	3087	-2	-2382	1.10	-0.02	-1.31	132.00	192.00	192.00	65
0	(8+9)-VII-1	-2648	-30	1877	-0.94	-0.40	1.04	132.00	192.00	192.00	>100
0	(8+9)-VII-4	2909	28	-2327	1.04	0.37	-1.28	132.00	192.00	192.00	61
0	(8+9)-I-3	4320	31	-3265	1.54	0.41	-1.80	132.00	192.00	192.00	43
0	(8+9)-II-1	4094	4	-3098	1.46	0.06	-1.71	132.00	192.00	192.00	49
0	(8+9)-II-3	5745	21	-4297	2.04	0.28	-2.37	132.00	192.00	192.00	34
0	(8+9)-V-4	2722	27	-2205	0.97	0.35	-1.22	132.00	192.00	192.00	64
0	(8+9)-III-3	4133	30	-3142	1.47	0.40	-1.73	132.00	192.00	192.00	45
0	(8+9)-V-3	5595	35	-4288	1.99	0.46	-2.37	132.00	192.00	192.00	34
0	(8+9)-VI-3	6128	22	-4603	2.18	0.30	-2.54	132.00	192.00	192.00	32
150	(8+9)-I-1	-1090	-25	769	-0.39	-0.33	0.42	132.00	192.00	192.00	>100
150	(8+9)-III-1	-1238	-26	870	-0.44	-0.35	0.48	132.00	192.00	192.00	>100
300	(8+9)-VIII-4	-2386	-7	2269	-0.85	-0.10	1.25	132.00	192.00	192.00	>100
300	(8+9)-I-2	-3345	-28	3134	-1.19	-0.38	1.73	132.00	192.00	192.00	91
300	(8+9)-IV-2	-4058	-22	3854	-1.44	-0.29	2.13	132.00	192.00	192.00	79
300	(8+9)-VI-2	-4874	-27	4620	-1.73	-0.36	2.55	132.00	192.00	192.00	66
300	(8+9)-III-2	-3201	-27	2993	-1.14	-0.36	1.65	132.00	192.00	192.00	95
300	(8+9)-VII-2	-4320	-32	3986	-1.54	-0.43	2.20	132.00	192.00	192.00	73
300	(8+9)-V-2	-4464	-33	4126	-1.59	-0.44	2.28	132.00	192.00	192.00	70
300	(8+9)-IV-4	-2722	-9	2567	-0.97	-0.12	1.42	132.00	192.00	192.00	>100
300	(8+9)-II-4	-3202	-13	3035	-1.14	-0.17	1.67	132.00	192.00	192.00	>100
300	(8+9)-VIII-2	-4394	-23	4152	-1.56	-0.31	2.29	132.00	192.00	192.00	73
300	(8+9)-II-2	-4538	-26	4322	-1.62	-0.34	2.39	132.00	192.00	192.00	70
300	(8+9)-VI-4	-2866	-11	2737	-1.02	-0.15	1.51	132.00	192.00	192.00	>100
Verifiche nella direzione secondaria											
0	(8+9)-VIII-4	-642	-18	374	-4.42	-6.93	51.51	132.00	192.00	192.00	3.3
0	(8+9)-VII-2	-397	18	743	-2.73	7.02	102.32	132.00	192.00	192.00	1.8
0	(8+9)-III-3	-1689	15	-556	-11.63	5.81	-76.61	132.00	192.00	192.00	2.3
0	(8+9)-IV-2	-366	-15	662	-2.52	-5.84	91.23	132.00	192.00	192.00	2.0

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-III-4	-1319	9	-218	-9.09	3.38	-30.09	132.00	192.00	192.00	5.7
0	(8+9)-VIII-2	-330	-5	726	-2.27	-1.80	100.01	132.00	192.00	192.00	1.9
0	(8+9)-IV-1	-1598	6	-463	-11.01	2.27	-63.84	132.00	192.00	192.00	2.9
0	(8+9)-VII-4	-1438	-26	-431	-9.91	-10.08	-59.35	132.00	192.00	192.00	2.7
0	(8+9)-I-1	-933	-13	159	-6.43	-5.09	21.96	132.00	192.00	192.00	7.0
0	(8+9)-IV-3	-1839	13	-688	-12.67	5.21	-94.78	132.00	192.00	192.00	1.9
0	(8+9)-I-3	-1737	12	-589	-11.96	4.73	-81.18	132.00	192.00	192.00	2.2
0	(8+9)-IV-4	-607	-7	438	-4.18	-2.89	60.29	132.00	192.00	192.00	3.0
0	(8+9)-II-1	-1758	-3	-574	-12.10	-1.34	-79.09	132.00	192.00	192.00	2.4
0	(8+9)-V-1	-814	21	372	-5.61	8.37	51.23	132.00	192.00	192.00	3.2
0	(8+9)-II-3	-1999	4	-799	-13.77	1.61	-110.04	132.00	192.00	192.00	1.7
0	(8+9)-V-2	-349	21	776	-2.40	8.11	106.90	132.00	192.00	192.00	1.7
0	(8+9)-III-1	-885	-10	193	-6.10	-4.01	26.54	132.00	192.00	192.00	6.2
0	(8+9)-V-3	-1856	-22	-802	-12.78	-8.73	-110.45	132.00	192.00	192.00	1.6
0	(8+9)-VIII-3	-1875	3	-752	-12.91	1.18	-103.56	132.00	192.00	192.00	1.8
0	(8+9)-V-4	-1390	-23	-398	-9.58	-9.00	-54.77	132.00	192.00	192.00	3.0
0	(8+9)-VII-3	-1808	-19	-769	-12.45	-7.65	-105.87	132.00	192.00	192.00	1.7
0	(8+9)-VI-1	-1722	7	-510	-11.86	2.70	-70.31	132.00	192.00	192.00	2.6
0	(8+9)-I-4	-1272	11	-185	-8.76	4.46	-25.51	132.00	192.00	192.00	6.3
0	(8+9)-VI-2	-170	5	837	-1.17	1.81	115.27	132.00	192.00	192.00	1.6
0	(8+9)-II-4	-447	2	548	-3.08	0.72	75.54	132.00	192.00	192.00	2.5
0	(8+9)-VIII-1	-1562	16	-400	-10.76	6.31	-55.06	132.00	192.00	192.00	3.1
0	(8+9)-I-2	-468	-14	564	-3.22	-5.36	77.63	132.00	192.00	192.00	2.3
0	(8+9)-II-2	-206	-6	773	-1.42	-2.23	106.49	132.00	192.00	192.00	1.8
0	(8+9)-III-2	-516	-16	530	-3.55	-6.44	73.06	132.00	192.00	192.00	2.4
0	(8+9)-VI-3	-2034	-6	-863	-14.01	-2.43	-118.82	132.00	192.00	192.00	1.6
0	(8+9)-VI-4	-483	-8	485	-3.33	-3.32	66.76	132.00	192.00	192.00	2.7
0	(8+9)-VII-1	-766	24	405	-5.28	9.46	55.80	132.00	192.00	192.00	2.9
3870	1	-414	-1	71	-2.85	-0.53	9.76	79.20	115.20	115.20	11
3870	2	-855	-3	146	-5.89	-1.08	20.16	118.80	172.80	172.80	8.1
3870	3	-855	-3	146	-5.89	-1.08	20.16	118.80	172.80	172.80	8.1
3870	4	-414	-1	71	-2.85	-0.53	9.76	105.60	153.60	153.60	15
3870	5	-414	-1	71	-2.85	-0.53	9.76	105.60	153.60	153.60	15
3870	6	-414	-1	71	-2.85	-0.53	9.76	105.60	153.60	153.60	15
3870	7	-414	-1	71	-2.85	-0.53	9.76	105.60	153.60	153.60	15

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Ty kg	τ_d kg/cmq	fvd kg/cmq	RS	Cs
0	1	2	0.00	3.84	Si	>100
0	2	4	0.00	5.76	Si	>100
0	3	4	0.00	5.76	Si	>100
0	4	2	0.00	5.12	Si	>100
0	5	2	0.00	5.12	Si	>100
0	6	2	0.00	5.12	Si	>100
0	7	2	0.00	5.12	Si	>100
0	(8+9)-VIII-4	-20	0.01	6.40	Si	>100
0	(8+9)-IV-1	20	0.01	6.40	Si	>100
0	(8+9)-V-1	24	0.01	6.40	Si	>100
0	(8+9)-V-2	9	0.00	6.40	Si	>100
0	(8+9)-I-4	-12	0.00	6.40	Si	>100
0	(8+9)-V-3	-7	0.00	6.40	Si	>100
0	(8+9)-II-2	-21	0.01	6.40	Si	>100
0	(8+9)-V-4	-21	0.01	6.40	Si	>100
0	(8+9)-II-4	-24	0.01	6.40	Si	>100
0	(8+9)-VII-2	12	0.00	6.40	Si	>100
0	(8+9)-II-1	27	0.01	6.40	Si	>100
0	(8+9)-VI-1	30	0.01	6.40	Si	>100
0	(8+9)-II-3	23	0.01	6.40	Si	>100
0	(8+9)-VIII-1	22	0.01	6.40	Si	>100
0	(8+9)-III-1	12	0.00	6.40	Si	>100
0	(8+9)-VII-4	-19	0.00	6.40	Si	>100
0	(8+9)-VII-3	-9	0.00	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
0	(8+9)-VI-2	-18	0.00	6.40	Si	>100
0	(8+9)-VIII-3	13	0.00	6.40	Si	>100
0	(8+9)-IV-3	16	0.00	6.40	Si	>100
0	(8+9)-I-3	3	0.00	6.40	Si	>100
0	(8+9)-I-1	14	0.00	6.40	Si	>100
0	(8+9)-VI-3	20	0.01	6.40	Si	>100
0	(8+9)-VI-4	-27	0.01	6.40	Si	>100
0	(8+9)-VII-1	22	0.01	6.40	Si	>100
150	(8+9)-I-2	-3	0.00	6.40	Si	>100
150	(8+9)-III-2	-3	0.00	6.40	Si	>100
150	(8+9)-IV-2	-16	0.00	6.40	Si	>100
150	(8+9)-III-3	2	0.00	6.40	Si	>100
300	(8+9)-IV-4	-18	0.00	6.40	Si	>100
300	(8+9)-III-4	-11	0.00	6.40	Si	>100
300	(8+9)-VIII-2	-14	0.00	6.40	Si	>100
Verifiche nella direzione secondaria						
0	1	-8	0.05	3.84	Si	71
0	2	-18	0.11	5.76	Si	51
0	3	-18	0.11	5.76	Si	51
0	4	-8	0.05	5.12	Si	95
0	5	-8	0.05	5.12	Si	95
0	6	-8	0.05	5.12	Si	95
0	7	-8	0.05	5.12	Si	95
0	(8+9)-VIII-4	6	0.04	6.40	Si	>100
0	(8+9)-IV-3	-17	0.11	6.40	Si	59
0	(8+9)-V-2	-8	0.05	6.40	Si	>100
0	(8+9)-IV-2	5	0.03	6.40	Si	>100
0	(8+9)-I-4	-7	0.04	6.40	Si	>100
0	(8+9)-III-3	-12	0.07	6.40	Si	85
0	(8+9)-VIII-1	-17	0.11	6.40	Si	58
0	(8+9)-VII-1	-13	0.08	6.40	Si	78
0	(8+9)-VIII-3	-15	0.10	6.40	Si	67
0	(8+9)-VIII-2	3	0.02	6.40	Si	>100
0	(8+9)-VII-3	-5	0.03	6.40	Si	>100
0	(8+9)-III-4	-5	0.03	6.40	Si	>100
0	(8+9)-IV-1	-15	0.10	6.40	Si	65
0	(8+9)-IV-4	4	0.02	6.40	Si	>100
1935	(8+9)-V-1	-13	0.08	6.40	Si	75
1935	(8+9)-VI-4	6	0.04	6.40	Si	>100
1935	(8+9)-I-1	-7	0.05	6.40	Si	>100
1935	(8+9)-II-4	4	0.03	6.40	Si	>100
1935	(8+9)-III-1	-7	0.04	6.40	Si	>100
1935	(8+9)-II-2	5	0.03	6.40	Si	>100
1935	(8+9)-V-3	-5	0.03	6.40	Si	>100
1935	(8+9)-VI-2	4	0.02	6.40	Si	>100
1935	(8+9)-VI-3	-15	0.10	6.40	Si	66
1935	(8+9)-I-3	-11	0.07	6.40	Si	94
1935	(8+9)-VI-1	-18	0.11	6.40	Si	57
1935	(8+9)-II-1	-16	0.10	6.40	Si	63
1935	(8+9)-II-3	-17	0.11	6.40	Si	59
3870	(8+9)-VII-2	8	0.05	6.40	Si	>100
3870	(8+9)-I-2	4	0.02	6.40	Si	>100
3870	(8+9)-VII-4	-4	0.03	6.40	Si	>100
3870	(8+9)-III-2	4	0.02	6.40	Si	>100
3870	(8+9)-V-4	-4	0.03	6.40	Si	>100

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Tx kg	τ_{vd} kg/cmq	fvd kg/cmq	Csv	τ_M kg/cmq	fTd kg/cmq	Csm	Mecc.	Cs
0	(8+9)-VIII-4	-3729	-1.99	32.00	16	-0.48	20.00	42	V	16
0	(8+9)-III-1	-2176	-1.16	32.00	28	-0.28	20.00	71	V	28
0	(8+9)-I-1	-1875	-1.00	32.00	32	-0.24	20.00	83	V	32
0	(8+9)-VI-4	-4731	-2.53	32.00	13	-0.61	20.00	33	V	13

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
150	(8+9)-V-4	3872	2.07	32.00	15	0.50	20.00	40	V	15
150	(8+9)-II-3	7699	4.11	32.00	7.8	0.99	20.00	20	V	7.8
150	(8+9)-III-2	-5270	-2.81	32.00	11	-0.68	20.00	29	V	11
150	(8+9)-VII-2	-6883	-3.67	32.00	8.7	-0.89	20.00	22	V	8.7
150	(8+9)-III-3	5728	3.06	32.00	10	0.74	20.00	27	V	10
150	(8+9)-VII-3	7340	3.92	32.00	8.2	0.95	20.00	21	V	8.2
150	(8+9)-III-4	2568	1.37	32.00	23	0.33	20.00	60	V	23
150	(8+9)-I-3	6036	3.22	32.00	9.9	0.78	20.00	26	V	9.9
150	(8+9)-VII-4	4181	2.23	32.00	14	0.54	20.00	37	V	14
150	(8+9)-IV-2	-6213	-3.32	32.00	9.6	-0.80	20.00	25	V	9.6
150	(8+9)-VIII-2	-6697	-3.58	32.00	9.0	-0.87	20.00	23	V	9.0
150	(8+9)-IV-3	6671	3.56	32.00	9.0	0.86	20.00	23	V	9.0
150	(8+9)-VIII-3	7155	3.82	32.00	8.4	0.92	20.00	22	V	8.4
150	(8+9)-VI-2	-7725	-4.12	32.00	7.8	-1.00	20.00	20	V	7.8
150	(8+9)-I-2	-5578	-2.98	32.00	11	-0.72	20.00	28	V	11
150	(8+9)-II-2	-7241	-3.87	32.00	8.3	-0.94	20.00	21	V	8.3
150	(8+9)-VI-3	8183	4.37	32.00	7.3	1.06	20.00	19	V	7.3
150	(8+9)-VII-1	-3723	-1.99	32.00	16	-0.48	20.00	42	V	16
150	(8+9)-I-4	2260	1.21	32.00	27	0.29	20.00	69	V	27
150	(8+9)-V-1	-3414	-1.82	32.00	18	-0.44	20.00	45	V	18
150	(8+9)-V-2	-7191	-3.84	32.00	8.3	-0.93	20.00	22	V	8.3
150	(8+9)-V-3	7649	4.08	32.00	7.8	0.99	20.00	20	V	7.8
300	1	369	0.20	19.20	97	0.05	12.00	>100	V	97
300	2	770	0.41	28.80	70	0.10	18.00	>100	V	70
300	3	770	0.41	28.80	70	0.10	18.00	>100	V	70
300	4	369	0.20	25.60	>100	0.05	16.00	>100	V	>100
300	5	369	0.20	25.60	>100	0.05	16.00	>100	V	>100
300	6	369	0.20	25.60	>100	0.05	16.00	>100	V	>100
300	7	369	0.20	25.60	>100	0.05	16.00	>100	V	>100
300	(8+9)-IV-1	4391	2.34	32.00	14	0.57	20.00	35	V	14
300	(8+9)-II-1	5419	2.89	32.00	11	0.70	20.00	29	V	11
300	(8+9)-VIII-1	3926	2.10	32.00	15	0.51	20.00	39	V	15
300	(8+9)-II-4	-4914	-2.62	32.00	12	-0.63	20.00	32	V	12
300	(8+9)-IV-4	-3886	-2.07	32.00	15	-0.50	20.00	40	V	15
300	(8+9)-VI-1	4953	2.64	32.00	12	0.64	20.00	31	V	12
Verifiche nella direzione secondaria										
3870	1	-164	-1.13	19.20	17	-0.27	12.00	44	V	17
3870	2	-350	-2.41	28.80	12	-0.58	18.00	31	V	12
3870	3	-350	-2.41	28.80	12	-0.58	18.00	31	V	12
3870	4	-164	-1.13	25.60	23	-0.27	16.00	58	V	23
3870	5	-164	-1.13	25.60	23	-0.27	16.00	58	V	23
3870	6	-164	-1.13	25.60	23	-0.27	16.00	58	V	23
3870	7	-164	-1.13	25.60	23	-0.27	16.00	58	V	23
3870	(8+9)-VIII-4	914	6.29	32.00	5.1	1.52	20.00	13	V	5.1
3870	(8+9)-IV-2	1544	10.64	32.00	3.0	2.57	20.00	7.8	V	3.0
3870	(8+9)-V-1	631	4.35	32.00	7.4	1.05	20.00	19	V	7.4
3870	(8+9)-I-2	1244	8.57	32.00	3.7	2.07	20.00	9.6	V	3.7
3870	(8+9)-V-2	1627	11.21	32.00	2.9	2.71	20.00	7.4	V	2.9
3870	(8+9)-I-4	-474	-3.26	32.00	9.8	-0.79	20.00	25	V	9.8
3870	(8+9)-V-3	-1853	-12.76	32.00	2.5	-3.09	20.00	6.5	V	2.5
3870	(8+9)-II-2	1805	12.43	32.00	2.6	3.01	20.00	6.6	V	2.6
3870	(8+9)-V-4	-857	-5.90	32.00	5.4	-1.43	20.00	14	V	5.4
3870	(8+9)-II-4	1289	8.88	32.00	3.6	2.15	20.00	9.3	V	3.6
3870	(8+9)-VI-1	-1400	-9.64	32.00	3.3	-2.33	20.00	8.6	V	3.3
3870	(8+9)-III-2	1166	8.03	32.00	4.0	1.94	20.00	10	V	4.0
3870	(8+9)-VI-2	1920	13.22	32.00	2.4	3.20	20.00	6.3	V	2.4
3870	(8+9)-III-4	-552	-3.80	32.00	8.4	-0.92	20.00	22	V	8.4
3870	(8+9)-VI-3	-2145	-14.77	32.00	2.2	-3.58	20.00	5.6	V	2.2
3870	(8+9)-I-1	249	1.71	32.00	19	0.41	20.00	48	V	19
3870	(8+9)-VI-4	1175	8.09	32.00	4.0	1.96	20.00	10	V	4.0
3870	(8+9)-IV-4	1029	7.09	32.00	4.5	1.71	20.00	12	V	4.5
3870	(8+9)-VII-1	709	4.89	32.00	6.5	1.18	20.00	17	V	6.5
3870	(8+9)-II-1	-1515	-10.43	32.00	3.1	-2.52	20.00	7.9	V	3.1
3870	(8+9)-VII-2	1549	10.67	32.00	3.0	2.58	20.00	7.7	V	3.0

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
3870	(8+9)-III-1	327	2.25	32.00	14	0.54	20.00	37	V	14
3870	(8+9)-VII-3	-1774	-12.22	32.00	2.6	-2.96	20.00	6.8	V	2.6
3870	(8+9)-IV-1	-1254	-8.64	32.00	3.7	-2.09	20.00	9.6	V	3.7
3870	(8+9)-VII-4	-935	-6.44	32.00	5.0	-1.56	20.00	13	V	5.0
3870	(8+9)-III-3	-1392	-9.58	32.00	3.3	-2.32	20.00	8.6	V	3.3
3870	(8+9)-IV-3	-1770	-12.19	32.00	2.6	-2.95	20.00	6.8	V	2.6
3870	(8+9)-II-3	-2030	-13.98	32.00	2.3	-3.38	20.00	5.9	V	2.3
3870	(8+9)-VIII-1	-1139	-7.85	32.00	4.1	-1.90	20.00	11	V	4.1
3870	(8+9)-VIII-2	1659	11.43	32.00	2.8	2.77	20.00	7.2	V	2.8
3870	(8+9)-VIII-3	-1884	-12.98	32.00	2.5	-3.14	20.00	6.4	V	2.5
3870	(8+9)-I-3	-1470	-10.12	32.00	3.2	-2.45	20.00	8.2	V	3.2

Setto 43: origine (1639.0,1182.0,193.5), direzione (-0.199392,0.97992,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_N	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	1	5527	-44	-9906	1.97	-0.58	-5.47	79.20	115.20	115.20	13
0	2	11617	-91	-20600	4.13	-1.22	-11.37	118.80	172.80	172.80	9.3
0	3	11617	-91	-20600	4.13	-1.22	-11.37	118.80	172.80	172.80	9.3
0	4	5527	-44	-9906	1.97	-0.58	-5.47	105.60	153.60	153.60	17
0	5	5527	-44	-9906	1.97	-0.58	-5.47	105.60	153.60	153.60	17
0	6	5527	-44	-9906	1.97	-0.58	-5.47	105.60	153.60	153.60	17
0	7	5527	-44	-9906	1.97	-0.58	-5.47	105.60	153.60	153.60	17
0	(8+9)-VIII-4	-2826	359	-3877	-1.01	4.80	-2.14	132.00	192.00	192.00	28
0	(8+9)-IV-1	11272	-427	-10036	4.01	-5.71	-5.54	132.00	192.00	192.00	11
0	(8+9)-V-1	-1497	-407	-5309	-0.53	-5.44	-2.93	132.00	192.00	192.00	23
0	(8+9)-I-2	-5206	-495	-3518	-1.85	-6.61	-1.94	132.00	192.00	192.00	22
0	(8+9)-I-4	6405	374	-7662	2.28	5.00	-4.23	132.00	192.00	192.00	15
0	(8+9)-VII-1	-1953	-517	-5194	-0.70	-6.91	-2.87	132.00	192.00	192.00	20
0	(8+9)-IV-4	-3643	367	-3659	-1.30	4.91	-2.02	132.00	192.00	192.00	28
0	(8+9)-I-3	12836	435	-10178	4.57	5.82	-5.62	132.00	192.00	192.00	11
0	(8+9)-VIII-3	15572	-175	-11496	5.54	-2.33	-6.34	132.00	192.00	192.00	11
0	(8+9)-VII-4	9583	457	-8501	3.41	6.11	-4.69	132.00	192.00	192.00	12
0	(8+9)-IV-3	14756	-166	-11279	5.25	-2.22	-6.22	132.00	192.00	192.00	12
0	(8+9)-III-4	6860	485	-7777	2.44	6.48	-4.29	132.00	192.00	192.00	13
0	(8+9)-I-1	1225	-434	-6033	0.44	-5.80	-3.33	132.00	192.00	192.00	20
0	(8+9)-VIII-1	10456	-419	-9819	3.72	-5.60	-5.42	132.00	192.00	192.00	12
0	(8+9)-VI-3	17092	193	-11879	6.08	2.59	-6.56	132.00	192.00	192.00	11
0	(8+9)-II-3	16275	202	-11662	5.79	2.70	-6.44	132.00	192.00	192.00	11
0	(8+9)-III-1	769	-544	-5918	0.27	-7.28	-3.27	132.00	192.00	192.00	18
0	(8+9)-III-2	-4750	-384	-3632	-1.69	-5.14	-2.00	132.00	192.00	192.00	27
290	(8+9)-V-3	15469	311	-14000	5.51	4.15	-7.73	132.00	192.00	192.00	9.7
290	(8+9)-V-4	9070	347	-9741	3.23	4.64	-5.38	132.00	192.00	192.00	13
290	(8+9)-VI-1	11944	-186	-12163	4.25	-2.48	-6.71	132.00	192.00	192.00	12
290	(8+9)-II-1	12669	-177	-12648	4.51	-2.36	-6.98	132.00	192.00	192.00	12
290	(8+9)-III-3	12608	261	-12071	4.49	3.49	-6.66	132.00	192.00	192.00	12
290	(8+9)-VII-3	15024	292	-13689	5.35	3.90	-7.55	132.00	192.00	192.00	10.0
580	(8+9)-V-2	-10614	-268	9096	-3.78	-3.59	5.02	132.00	192.00	192.00	22
580	(8+9)-VII-2	-10159	-243	8686	-3.62	-3.25	4.79	132.00	192.00	192.00	24
580	(8+9)-VI-4	-6821	89	5356	-2.43	1.19	2.96	132.00	192.00	192.00	46
580	(8+9)-VI-2	-12035	-67	10249	-4.28	-0.89	5.66	132.00	192.00	192.00	29
580	(8+9)-IV-2	-9610	8	7969	-3.42	0.11	4.40	132.00	192.00	192.00	42
580	(8+9)-VIII-2	-10520	17	8881	-3.74	0.22	4.90	132.00	192.00	192.00	37
580	(8+9)-II-4	-7731	97	6268	-2.75	1.30	3.46	132.00	192.00	192.00	40
580	(8+9)-II-2	-11125	-75	9337	-3.96	-1.01	5.15	132.00	192.00	192.00	31
Verifiche nella direzione secondaria											
0	(8+9)-VIII-4	4238	90	383	15.10	18.39	14.11	132.00	192.00	192.00	3.5
0	(8+9)-VII-2	2189	-240	1450	7.80	-49.00	53.45	132.00	192.00	192.00	1.7
0	(8+9)-III-3	-4204	172	-1344	-14.97	35.00	-49.51	132.00	192.00	192.00	2.2
0	(8+9)-IV-2	5043	-39	1070	17.96	-7.85	39.44	132.00	192.00	192.00	2.6
0	(8+9)-III-4	-492	189	-841	-1.75	38.48	-30.98	132.00	192.00	192.00	2.8
0	(8+9)-VIII-2	5291	-53	1146	18.85	-10.84	42.24	132.00	192.00	192.00	2.4
0	(8+9)-IV-1	-7331	-95	-606	-26.12	-19.45	-22.32	132.00	192.00	192.00	4.2

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-VII-4	-1321	238	-1094	-4.70	48.43	-40.32	132.00	192.00	192.00	2.2
0	(8+9)-I-1	-2867	-214	649	-10.21	-43.65	23.93	132.00	192.00	192.00	2.8
0	(8+9)-IV-3	-7887	19	-1217	-28.09	3.81	-44.85	132.00	192.00	192.00	3.6
0	(8+9)-I-3	-4719	166	-1388	-16.81	33.89	-51.16	132.00	192.00	192.00	2.2
0	(8+9)-IV-4	4487	76	459	15.98	15.41	16.91	132.00	192.00	192.00	3.5
0	(8+9)-II-1	-9048	-114	-755	-32.23	-23.18	-27.82	132.00	192.00	192.00	3.4
0	(8+9)-V-1	-2038	-263	903	-7.26	-53.60	33.27	132.00	192.00	192.00	2.2
0	(8+9)-II-3	-9603	0	-1366	-34.21	0.08	-50.35	132.00	192.00	192.00	3.4
0	(8+9)-V-2	2704	-235	1495	9.63	-47.88	55.10	132.00	192.00	192.00	1.6
0	(8+9)-III-1	-2352	-209	694	-8.38	-42.53	25.58	132.00	192.00	192.00	2.8
0	(8+9)-V-3	-5548	215	-1642	-19.76	43.84	-60.50	132.00	192.00	192.00	1.8
0	(8+9)-VIII-3	-8135	33	-1293	-28.98	6.79	-47.65	132.00	192.00	192.00	3.3
0	(8+9)-V-4	-806	243	-1049	-2.87	49.55	-38.67	132.00	192.00	192.00	2.2
0	(8+9)-VII-3	-5033	221	-1597	-17.93	44.95	-58.85	132.00	192.00	192.00	1.8
0	(8+9)-VI-1	-8799	-128	-679	-31.34	-26.16	-25.02	132.00	192.00	192.00	3.4
0	(8+9)-I-4	23	194	-796	0.08	39.60	-29.33	132.00	192.00	192.00	2.8
0	(8+9)-VI-2	7008	-35	1296	24.96	-7.11	47.74	132.00	192.00	192.00	2.1
0	(8+9)-II-4	6204	94	608	22.10	19.13	22.41	132.00	192.00	192.00	2.6
0	(8+9)-VIII-1	-7082	-110	-530	-25.23	-22.44	-19.52	132.00	192.00	192.00	4.2
0	(8+9)-I-2	1875	-186	1242	6.68	-37.93	45.75	132.00	192.00	192.00	2.1
0	(8+9)-II-2	6759	-20	1220	24.08	-4.13	44.94	132.00	192.00	192.00	2.3
0	(8+9)-III-2	1360	-192	1197	4.84	-39.05	44.10	132.00	192.00	192.00	2.1
0	(8+9)-VI-3	-9852	15	-1442	-35.10	3.07	-53.15	132.00	192.00	192.00	3.1
0	(8+9)-VI-4	5955	109	532	21.21	22.12	19.61	132.00	192.00	192.00	2.6
0	(8+9)-VII-1	-1523	-257	948	-5.43	-52.48	34.92	132.00	192.00	192.00	2.2
3870	1	-4819	42	53	-17.17	8.59	1.94	79.20	115.20	115.20	8.8
3870	2	-9902	90	100	-35.27	18.30	3.69	118.80	172.80	172.80	5.9
3870	3	-9902	90	100	-35.27	18.30	3.69	118.80	172.80	172.80	5.9
3870	4	-4819	42	53	-17.17	8.59	1.94	105.60	153.60	153.60	12
3870	5	-4819	42	53	-17.17	8.59	1.94	105.60	153.60	153.60	12
3870	6	-4819	42	53	-17.17	8.59	1.94	105.60	153.60	153.60	12
3870	7	-4819	42	53	-17.17	8.59	1.94	105.60	153.60	153.60	12

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
0	(8+9)-III-3	204	0.05	6.40	Si	>100
0	(8+9)-VI-3	150	0.04	6.40	Si	>100
0	(8+9)-I-3	223	0.06	6.40	Si	>100
0	(8+9)-III-4	196	0.05	6.40	Si	>100
0	(8+9)-IV-3	147	0.04	6.40	Si	>100
0	(8+9)-II-3	211	0.05	6.40	Si	>100
0	(8+9)-IV-4	120	0.03	6.40	Si	>100
0	(8+9)-VIII-3	86	0.02	6.40	Si	>100
0	(8+9)-I-4	177	0.05	6.40	Si	>100
290	1	152	0.04	3.84	Si	98
290	2	316	0.08	5.76	Si	70
290	3	316	0.08	5.76	Si	70
290	4	152	0.04	5.12	Si	>100
290	5	152	0.04	5.12	Si	>100
290	6	152	0.04	5.12	Si	>100
290	7	152	0.04	5.12	Si	>100
290	(8+9)-V-3	-238	0.06	6.40	Si	>100
290	(8+9)-VII-3	-282	0.07	6.40	Si	88
290	(8+9)-II-1	242	0.06	6.40	Si	>100
290	(8+9)-III-2	230	0.06	6.40	Si	>100
290	(8+9)-V-4	-300	0.08	6.40	Si	82
290	(8+9)-I-1	248	0.06	6.40	Si	100
290	(8+9)-VI-1	320	0.08	6.40	Si	77
290	(8+9)-VIII-2	259	0.07	6.40	Si	95
290	(8+9)-VI-2	113	0.03	6.40	Si	>100
290	(8+9)-V-1	509	0.13	6.40	Si	49
290	(8+9)-I-2	186	0.05	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
290	(8+9)-II-2	35	0.01	6.40	Si	>100
290	(8+9)-V-2	447	0.12	6.40	Si	55
290	(8+9)-IV-2	181	0.05	6.40	Si	>100
290	(8+9)-VIII-1	174	0.05	6.40	Si	>100
290	(8+9)-VII-1	465	0.12	6.40	Si	53
290	(8+9)-VII-2	491	0.13	6.40	Si	50
290	(8+9)-III-1	205	0.05	6.40	Si	>100
580	(8+9)-VII-4	-257	0.07	6.40	Si	96
580	(8+9)-VI-4	-141	0.04	6.40	Si	>100
580	(8+9)-II-4	-98	0.03	6.40	Si	>100
580	(8+9)-IV-1	112	0.03	6.40	Si	>100
580	(8+9)-VIII-4	-99	0.03	6.40	Si	>100
Verifiche nella direzione secondaria						
0	(8+9)-III-3	-76	0.25	6.40	Si	26
0	(8+9)-VI-3	-70	0.23	6.40	Si	28
0	(8+9)-V-3	-82	0.27	6.40	Si	24
0	(8+9)-VIII-3	-82	0.27	6.40	Si	24
0	(8+9)-IV-3	-79	0.26	6.40	Si	25
0	(8+9)-V-4	-51	0.17	6.40	Si	38
0	(8+9)-VII-4	-48	0.16	6.40	Si	41
0	(8+9)-VII-3	-86	0.28	6.40	Si	23
0	(8+9)-IV-1	-44	0.15	6.40	Si	44
0	(8+9)-I-3	-72	0.24	6.40	Si	27
0	(8+9)-I-4	-42	0.14	6.40	Si	47
3870	1	164	0.54	3.84	Si	7.1
3870	2	346	1.14	5.76	Si	5.1
3870	3	346	1.14	5.76	Si	5.1
3870	4	164	0.54	5.12	Si	9.5
3870	5	164	0.54	5.12	Si	9.5
3870	6	164	0.54	5.12	Si	9.5
3870	7	164	0.54	5.12	Si	9.5
3870	(8+9)-VIII-4	173	0.57	6.40	Si	11
3870	(8+9)-II-2	142	0.47	6.40	Si	14
3870	(8+9)-III-2	227	0.75	6.40	Si	8.6
3870	(8+9)-I-2	196	0.65	6.40	Si	9.9
3870	(8+9)-VI-4	70	0.23	6.40	Si	28
3870	(8+9)-I-1	194	0.64	6.40	Si	10
3870	(8+9)-VII-1	239	0.79	6.40	Si	8.1
3870	(8+9)-V-1	270	0.89	6.40	Si	7.2
3870	(8+9)-VII-2	304	1.00	6.40	Si	6.4
3870	(8+9)-III-4	63	0.21	6.40	Si	31
3870	(8+9)-III-1	163	0.54	6.40	Si	12
3870	(8+9)-VI-1	156	0.51	6.40	Si	12
3870	(8+9)-II-4	93	0.31	6.40	Si	21
3870	(8+9)-V-2	273	0.90	6.40	Si	7.1
3870	(8+9)-II-1	133	0.44	6.40	Si	15
3870	(8+9)-VI-2	165	0.54	6.40	Si	12
3870	(8+9)-IV-4	196	0.64	6.40	Si	9.9
3870	(8+9)-VIII-1	53	0.18	6.40	Si	37
3870	(8+9)-VIII-2	268	0.88	6.40	Si	7.3
3870	(8+9)-II-3	84	0.28	6.40	Si	23
3870	(8+9)-IV-2	245	0.81	6.40	Si	7.9

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	1	-1038	-0.55	19.20	35	-0.13	12.00	89	V	35
0	2	-2026	-1.08	28.80	27	-0.26	18.00	69	V	27
0	3	-2026	-1.08	28.80	27	-0.26	18.00	69	V	27
0	4	-1038	-0.55	25.60	46	-0.13	16.00	>100	V	46
0	5	-1038	-0.55	25.60	46	-0.13	16.00	>100	V	46
0	6	-1038	-0.55	25.60	46	-0.13	16.00	>100	V	46
0	7	-1038	-0.55	25.60	46	-0.13	16.00	>100	V	46

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
0	(8+9)-VIII-4	-8412	-4.49	32.00	7.1	-1.09	20.00	18	V	7.1
0	(8+9)-IV-1	7003	3.74	32.00	8.6	0.90	20.00	22	V	8.6
0	(8+9)-VIII-1	6937	3.70	32.00	8.6	0.90	20.00	22	V	8.6
0	(8+9)-VI-4	-9485	-5.06	32.00	6.3	-1.23	20.00	16	V	6.3
0	(8+9)-II-1	8076	4.31	32.00	7.4	1.04	20.00	19	V	7.4
0	(8+9)-VI-1	8010	4.28	32.00	7.5	1.03	20.00	19	V	7.5
0	(8+9)-IV-4	-8478	-4.53	32.00	7.1	-1.10	20.00	18	V	7.1
0	(8+9)-II-4	-9551	-5.10	32.00	6.3	-1.23	20.00	16	V	6.3
290	(8+9)-V-1	-5681	-3.03	32.00	11	-0.73	20.00	27	V	11
290	(8+9)-I-2	-9129	-4.87	32.00	6.6	-1.18	20.00	17	V	6.6
290	(8+9)-II-2	-11422	-6.10	32.00	5.2	-1.48	20.00	14	V	5.2
290	(8+9)-III-2	-8843	-4.72	32.00	6.8	-1.14	20.00	18	V	6.8
290	(8+9)-VI-2	-12015	-6.41	32.00	5.0	-1.55	20.00	13	V	5.0
290	(8+9)-IV-2	-10469	-5.59	32.00	5.7	-1.35	20.00	15	V	5.7
290	(8+9)-VIII-2	-11062	-5.91	32.00	5.4	-1.43	20.00	14	V	5.4
290	(8+9)-III-1	-3990	-2.13	32.00	15	-0.52	20.00	39	V	15
290	(8+9)-VII-2	-10820	-5.78	32.00	5.5	-1.40	20.00	14	V	5.5
290	(8+9)-V-2	-11106	-5.93	32.00	5.4	-1.43	20.00	14	V	5.4
290	(8+9)-VII-1	-5967	-3.19	32.00	10	-0.77	20.00	26	V	10
290	(8+9)-I-1	-3704	-1.98	32.00	16	-0.48	20.00	42	V	16
580	(8+9)-III-4	4299	2.30	32.00	14	0.56	20.00	36	V	14
580	(8+9)-VI-3	11876	6.34	32.00	5.0	1.53	20.00	13	V	5.0
580	(8+9)-VII-3	11282	6.02	32.00	5.3	1.46	20.00	14	V	5.3
580	(8+9)-III-3	8999	4.80	32.00	6.7	1.16	20.00	17	V	6.7
580	(8+9)-VII-4	6582	3.51	32.00	9.1	0.85	20.00	24	V	9.1
580	(8+9)-II-3	11191	5.97	32.00	5.4	1.45	20.00	14	V	5.4
580	(8+9)-V-4	6303	3.36	32.00	9.5	0.81	20.00	25	V	9.5
580	(8+9)-V-3	11561	6.17	32.00	5.2	1.49	20.00	13	V	5.2
580	(8+9)-I-3	9278	4.95	32.00	6.5	1.20	20.00	17	V	6.5
580	(8+9)-IV-3	10262	5.48	32.00	5.8	1.33	20.00	15	V	5.8
580	(8+9)-VIII-3	10946	5.84	32.00	5.5	1.41	20.00	14	V	5.5
580	(8+9)-I-4	4020	2.15	32.00	15	0.52	20.00	39	V	15
Verifiche nella direzione secondaria										
1935	(8+9)-VIII-4	2826	10.07	32.00	3.2	2.44	20.00	8.2	V	3.2
1935	(8+9)-VII-2	4764	16.97	32.00	1.9	4.11	20.00	4.9	V	1.9
1935	(8+9)-III-3	-3565	-12.70	32.00	2.5	-3.07	20.00	6.5	V	2.5
1935	(8+9)-IV-2	4641	16.53	32.00	1.9	4.00	20.00	5.0	V	1.9
1935	(8+9)-III-4	-1286	-4.58	32.00	7.0	-1.11	20.00	18	V	7.0
1935	(8+9)-VIII-2	4947	17.62	32.00	1.8	4.26	20.00	4.7	V	1.8
1935	(8+9)-IV-1	-2954	-10.52	32.00	3.0	-2.55	20.00	7.9	V	3.0
1935	(8+9)-VII-4	-2307	-8.22	32.00	3.9	-1.99	20.00	10	V	3.9
1935	(8+9)-I-1	1240	4.42	32.00	7.2	1.07	20.00	19	V	7.2
1935	(8+9)-IV-3	-4463	-15.90	32.00	2.0	-3.85	20.00	5.2	V	2.0
1935	(8+9)-I-3	-3789	-13.50	32.00	2.4	-3.27	20.00	6.1	V	2.4
1935	(8+9)-IV-4	3132	11.16	32.00	2.9	2.70	20.00	7.4	V	2.9
1935	(8+9)-II-1	-3700	-13.18	32.00	2.4	-3.19	20.00	6.3	V	2.4
1935	(8+9)-V-1	2261	8.06	32.00	4.0	1.95	20.00	10	V	4.0
1935	(8+9)-II-3	-5209	-18.56	32.00	1.7	-4.49	20.00	4.5	V	1.7
1935	(8+9)-V-2	4987	17.77	32.00	1.8	4.30	20.00	4.7	V	1.8
1935	(8+9)-III-1	1464	5.22	32.00	6.1	1.26	20.00	16	V	6.1
1935	(8+9)-V-3	-4810	-17.13	32.00	1.9	-4.15	20.00	4.8	V	1.9
1935	(8+9)-VIII-3	-4769	-16.99	32.00	1.9	-4.11	20.00	4.9	V	1.9
1935	(8+9)-V-4	-2083	-7.42	32.00	4.3	-1.80	20.00	11	V	4.3
1935	(8+9)-VII-3	-4586	-16.34	32.00	2.0	-3.95	20.00	5.1	V	2.0
1935	(8+9)-VI-1	-3394	-12.09	32.00	2.6	-2.93	20.00	6.8	V	2.6
1935	(8+9)-I-4	-1062	-3.78	32.00	8.5	-0.92	20.00	22	V	8.5
1935	(8+9)-VI-2	5693	20.28	32.00	1.6	4.91	20.00	4.1	V	1.6
1935	(8+9)-II-4	3878	13.82	32.00	2.3	3.34	20.00	6.0	V	2.3
1935	(8+9)-VIII-1	-2648	-9.43	32.00	3.4	-2.28	20.00	8.8	V	3.4
1935	(8+9)-I-2	3966	14.13	32.00	2.3	3.42	20.00	5.8	V	2.3
1935	(8+9)-II-2	5387	19.19	32.00	1.7	4.64	20.00	4.3	V	1.7
1935	(8+9)-III-2	3743	13.33	32.00	2.4	3.23	20.00	6.2	V	2.4
1935	(8+9)-VI-3	-5515	-19.65	32.00	1.6	-4.75	20.00	4.2	V	1.6
1935	(8+9)-VI-4	3572	12.72	32.00	2.5	3.08	20.00	6.5	V	2.5

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
1935	(8+9)-VII-1	2485	8.85	32.00	3.6	2.14	20.00	9.3	V	3.6
3870	1	504	1.80	19.20	11	0.43	12.00	28	V	11
3870	2	1047	3.73	28.80	7.7	0.90	18.00	20	V	7.7
3870	3	1047	3.73	28.80	7.7	0.90	18.00	20	V	7.7
3870	4	504	1.80	25.60	14	0.43	16.00	37	V	14
3870	5	504	1.80	25.60	14	0.43	16.00	37	V	14
3870	6	504	1.80	25.60	14	0.43	16.00	37	V	14
3870	7	504	1.80	25.60	14	0.43	16.00	37	V	14

Setto 44: origine (1519.8,1768.0,303.5), direzione (-0.199392,0.97992,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	1	-488	-12	-116	-0.40	-0.36	-0.34	79.20	115.20	115.20	>100
0	2	-1005	-25	-235	-0.83	-0.76	-0.70	118.80	172.80	172.80	>100
0	3	-1005	-25	-235	-0.83	-0.76	-0.70	118.80	172.80	172.80	>100
0	4	-488	-12	-116	-0.40	-0.36	-0.34	105.60	153.60	153.60	>100
0	5	-488	-12	-116	-0.40	-0.36	-0.34	105.60	153.60	153.60	>100
0	6	-488	-12	-116	-0.40	-0.36	-0.34	105.60	153.60	153.60	>100
0	7	-488	-12	-116	-0.40	-0.36	-0.34	105.60	153.60	153.60	>100
2200	(8+9)-VIII-4	4935	-6	2733	4.07	-0.20	8.10	132.00	192.00	192.00	14
2200	(8+9)-IV-1	-5439	-6	-3098	-4.49	-0.18	-9.18	132.00	192.00	192.00	20
2200	(8+9)-V-1	3661	-7	2243	3.02	-0.21	6.65	132.00	192.00	192.00	17
2200	(8+9)-I-2	7007	-8	3682	5.78	-0.26	10.91	132.00	192.00	192.00	9.8
2200	(8+9)-V-2	8585	-6	4984	7.08	-0.20	14.77	132.00	192.00	192.00	7.6
2200	(8+9)-I-4	-2115	-3	-916	-1.74	-0.08	-2.71	132.00	192.00	192.00	68
2200	(8+9)-V-3	-8616	-5	-4959	-7.11	-0.16	-14.69	132.00	192.00	192.00	13
2200	(8+9)-II-2	9558	-6	5271	7.88	-0.19	15.62	132.00	192.00	192.00	7.0
2200	(8+9)-V-4	-3693	-5	-2218	-3.05	-0.15	-6.57	132.00	192.00	192.00	28
2200	(8+9)-II-4	6821	-4	3892	5.63	-0.13	11.53	132.00	192.00	192.00	9.7
2200	(8+9)-VI-1	-6379	-6	-3476	-5.26	-0.20	-10.30	132.00	192.00	192.00	18
2200	(8+9)-III-2	6583	-9	3452	5.43	-0.28	10.23	132.00	192.00	192.00	10
2200	(8+9)-VI-2	10031	-5	5662	8.27	-0.17	16.78	132.00	192.00	192.00	6.6
2200	(8+9)-III-4	-2539	-3	-1146	-2.09	-0.10	-3.40	132.00	192.00	192.00	55
2200	(8+9)-VI-3	-10062	-6	-5636	-8.30	-0.19	-16.70	132.00	192.00	192.00	11
2200	(8+9)-IV-2	8145	-7	4503	6.72	-0.23	13.34	132.00	192.00	192.00	8.2
2200	(8+9)-VI-4	6348	-5	3501	5.24	-0.15	10.37	132.00	192.00	192.00	11
2200	(8+9)-IV-4	5408	-6	3123	4.46	-0.18	9.26	132.00	192.00	192.00	12
2200	(8+9)-VII-1	4085	-6	2474	3.37	-0.19	7.33	132.00	192.00	192.00	15
2200	(8+9)-II-1	-6852	-7	-3866	-5.65	-0.22	-11.46	132.00	192.00	192.00	16
2200	(8+9)-VII-2	8161	-7	4754	6.73	-0.21	14.09	132.00	192.00	192.00	8.0
2200	(8+9)-III-1	2508	-8	1172	2.07	-0.26	3.47	132.00	192.00	192.00	28
2200	(8+9)-VII-3	-8192	-5	-4728	-6.76	-0.14	-14.01	132.00	192.00	192.00	13
2200	(8+9)-I-1	2084	-9	941	1.72	-0.27	2.79	132.00	192.00	192.00	35
2200	(8+9)-VII-4	-4117	-5	-2448	-3.40	-0.16	-7.25	132.00	192.00	192.00	26
2200	(8+9)-III-3	-6615	-3	-3426	-5.46	-0.08	-10.15	132.00	192.00	192.00	18
2200	(8+9)-IV-3	-8176	-4	-4477	-6.74	-0.12	-13.27	132.00	192.00	192.00	14
2200	(8+9)-II-3	-9589	-5	-5246	-7.91	-0.17	-15.54	132.00	192.00	192.00	12
2200	(8+9)-VIII-1	-4966	-5	-2707	-4.10	-0.16	-8.02	132.00	192.00	192.00	23
2200	(8+9)-VIII-2	8618	-7	4893	7.11	-0.21	14.50	132.00	192.00	192.00	7.7
2200	(8+9)-VIII-3	-8649	-5	-4868	-7.13	-0.14	-14.42	132.00	192.00	192.00	13
2200	(8+9)-I-3	-7039	-3	-3657	-5.81	-0.09	-10.84	132.00	192.00	192.00	17
Verifiche nella direzione secondaria											
0	(8+9)-VIII-4	696	0	4468	0.65	0.00	11.44	132.00	192.00	192.00	15
0	(8+9)-VI-4	871	2	5400	0.82	0.10	13.83	132.00	192.00	192.00	13
0	(8+9)-III-2	389	6	4956	0.37	0.34	12.69	132.00	192.00	192.00	14
0	(8+9)-IV-2	700	5	6154	0.66	0.29	15.76	132.00	192.00	192.00	11
0	(8+9)-III-3	-1874	-22	-5025	-1.76	-1.18	-12.87	132.00	192.00	192.00	14
0	(8+9)-VIII-2	243	4	5774	0.23	0.23	14.79	132.00	192.00	192.00	13
0	(8+9)-III-4	-1147	-16	-1932	-1.08	-0.86	-4.95	132.00	192.00	192.00	33
0	(8+9)-VII-4	376	-12	-664	0.35	-0.63	-1.70	132.00	192.00	192.00	67
0	(8+9)-IV-1	-1724	-14	-4157	-1.62	-0.77	-10.65	132.00	192.00	192.00	17
0	(8+9)-I-1	-391	-0	1583	-0.37	-0.01	4.05	132.00	192.00	192.00	47

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-I-3	-1927	-22	-5305	-1.81	-1.21	-13.59	132.00	192.00	192.00	13
0	(8+9)-IV-3	-2185	-21	-6224	-2.05	-1.13	-15.94	132.00	192.00	192.00	11
0	(8+9)-II-1	-1899	-16	-5090	-1.78	-0.87	-13.04	132.00	192.00	192.00	14
0	(8+9)-IV-4	239	-1	4088	0.22	-0.06	10.47	132.00	192.00	192.00	18
0	(8+9)-II-3	-2360	-23	-7156	-2.22	-1.23	-18.33	132.00	192.00	192.00	9.8
0	(8+9)-VII-2	-1134	2	3687	-1.06	0.12	9.44	132.00	192.00	192.00	20
0	(8+9)-III-1	-338	0	1862	-0.32	0.02	4.77	132.00	192.00	192.00	40
0	(8+9)-V-2	-1081	3	3967	-1.02	0.15	10.16	132.00	192.00	192.00	19
0	(8+9)-VIII-1	-2181	-16	-4538	-2.05	-0.84	-11.62	132.00	192.00	192.00	15
0	(8+9)-V-3	-404	-18	-4037	-0.38	-0.98	-10.34	132.00	192.00	192.00	17
0	(8+9)-I-2	442	7	5235	0.41	0.37	13.41	132.00	192.00	192.00	13
0	(8+9)-V-4	429	-11	-384	0.40	-0.60	-0.98	132.00	192.00	192.00	88
0	(8+9)-II-2	875	7	7086	0.82	0.39	18.15	132.00	192.00	192.00	9.7
0	(8+9)-VIII-3	-1728	-20	-5843	-1.62	-1.06	-14.97	132.00	192.00	192.00	12
0	(8+9)-VII-3	-351	-18	-3757	-0.33	-0.95	-9.62	132.00	192.00	192.00	18
0	(8+9)-I-4	-1094	-15	-1652	-1.03	-0.83	-4.23	132.00	192.00	192.00	38
0	(8+9)-II-4	414	1	5020	0.39	0.03	12.86	132.00	192.00	192.00	14
0	(8+9)-VI-1	-2356	-17	-5470	-2.21	-0.94	-14.01	132.00	192.00	192.00	13
0	(8+9)-VI-2	418	6	6706	0.39	0.33	17.18	132.00	192.00	192.00	11
0	(8+9)-VI-3	-1903	-22	-6775	-1.79	-1.16	-17.35	132.00	192.00	192.00	10
835	1	-708	-14	-18	-0.67	-0.75	-0.05	79.20	115.20	115.20	>100
835	2	-1374	-29	-128	-1.29	-1.57	-0.33	118.80	172.80	172.80	91
835	3	-1374	-29	-128	-1.29	-1.57	-0.33	118.80	172.80	172.80	91
835	4	-708	-14	-18	-0.67	-0.75	-0.05	105.60	153.60	153.60	>100
835	5	-708	-14	-18	-0.67	-0.75	-0.05	105.60	153.60	153.60	>100
835	6	-708	-14	-18	-0.67	-0.75	-0.05	105.60	153.60	153.60	>100
835	7	-708	-14	-18	-0.67	-0.75	-0.05	105.60	153.60	153.60	>100
1670	(8+9)-VII-1	-392	6	-696	-0.37	0.33	-1.78	132.00	192.00	192.00	91
1670	(8+9)-V-1	-400	6	-654	-0.38	0.32	-1.68	132.00	192.00	192.00	96

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
0	1	13	0.01	3.84	Si	>100
0	2	28	0.02	5.76	Si	>100
0	3	28	0.02	5.76	Si	>100
0	4	13	0.01	5.12	Si	>100
0	5	13	0.01	5.12	Si	>100
0	6	13	0.01	5.12	Si	>100
0	7	13	0.01	5.12	Si	>100
0	(8+9)-VI-1	8	0.00	6.40	Si	>100
0	(8+9)-VI-3	16	0.01	6.40	Si	>100
0	(8+9)-III-4	17	0.01	6.40	Si	>100
0	(8+9)-IV-1	9	0.01	6.40	Si	>100
0	(8+9)-I-4	17	0.01	6.40	Si	>100
0	(8+9)-VII-4	21	0.01	6.40	Si	>100
0	(8+9)-VIII-4	10	0.01	6.40	Si	>100
0	(8+9)-IV-3	15	0.01	6.40	Si	>100
0	(8+9)-II-4	8	0.00	6.40	Si	>100
0	(8+9)-IV-4	8	0.01	6.40	Si	>100
0	(8+9)-VIII-1	8	0.00	6.40	Si	>100
0	(8+9)-VII-3	23	0.01	6.40	Si	>100
0	(8+9)-I-3	19	0.01	6.40	Si	>100
0	(8+9)-II-3	15	0.01	6.40	Si	>100
0	(8+9)-VIII-3	16	0.01	6.40	Si	>100
0	(8+9)-III-3	19	0.01	6.40	Si	>100
0	(8+9)-II-1	9	0.01	6.40	Si	>100
0	(8+9)-VI-4	10	0.01	6.40	Si	>100
0	(8+9)-V-3	23	0.01	6.40	Si	>100
0	(8+9)-V-4	21	0.01	6.40	Si	>100
1100	(8+9)-VII-1	-5	0.00	6.40	Si	>100
1100	(8+9)-I-2	-4	0.00	6.40	Si	>100
1100	(8+9)-II-2	-3	0.00	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
1100	(8+9)-IV-2	-3	0.00	6.40	Si	>100
1100	(8+9)-V-2	-7	0.00	6.40	Si	>100
1100	(8+9)-VII-2	-7	0.00	6.40	Si	>100
1100	(8+9)-V-1	-5	0.00	6.40	Si	>100
1100	(8+9)-VI-2	-5	0.00	6.40	Si	>100
1100	(8+9)-III-2	-4	0.00	6.40	Si	>100
1100	(8+9)-VIII-2	-4	0.00	6.40	Si	>100
2200	(8+9)-I-1	-4	0.00	6.40	Si	>100
2200	(8+9)-III-1	-4	0.00	6.40	Si	>100
Verifiche nella direzione secondaria						
0	(8+9)-III-3	-22	0.02	6.40	Si	>100
0	(8+9)-VII-4	-18	0.02	6.40	Si	>100
0	(8+9)-IV-2	6	0.00	6.40	Si	>100
0	(8+9)-VIII-3	-27	0.02	6.40	Si	>100
0	(8+9)-I-3	-23	0.02	6.40	Si	>100
0	(8+9)-VII-3	-26	0.02	6.40	Si	>100
0	(8+9)-IV-1	-20	0.02	6.40	Si	>100
0	(8+9)-IV-3	-25	0.02	6.40	Si	>100
0	(8+9)-V-4	-18	0.02	6.40	Si	>100
0	(8+9)-VI-3	-28	0.02	6.40	Si	>100
0	(8+9)-V-3	-27	0.02	6.40	Si	>100
0	(8+9)-II-1	-22	0.02	6.40	Si	>100
0	(8+9)-II-2	7	0.01	6.40	Si	>100
0	(8+9)-II-3	-27	0.02	6.40	Si	>100
1670	1	20	0.02	3.84	Si	>100
1670	2	41	0.04	5.76	Si	>100
1670	3	41	0.04	5.76	Si	>100
1670	4	20	0.02	5.12	Si	>100
1670	5	20	0.02	5.12	Si	>100
1670	6	20	0.02	5.12	Si	>100
1670	7	20	0.02	5.12	Si	>100
1670	(8+9)-VIII-4	-2	0.00	6.40	Si	>100
1670	(8+9)-VI-1	30	0.03	6.40	Si	>100
1670	(8+9)-III-1	9	0.01	6.40	Si	>100
1670	(8+9)-VII-1	45	0.04	6.40	Si	>100
1670	(8+9)-V-1	45	0.04	6.40	Si	>100
1670	(8+9)-VII-2	40	0.04	6.40	Si	>100
1670	(8+9)-IV-4	9	0.01	6.40	Si	>100
1670	(8+9)-III-4	18	0.02	6.40	Si	>100
1670	(8+9)-I-2	5	0.00	6.40	Si	>100
1670	(8+9)-II-4	8	0.01	6.40	Si	>100
1670	(8+9)-V-2	40	0.03	6.40	Si	>100
1670	(8+9)-I-1	10	0.01	6.40	Si	>100
1670	(8+9)-VI-2	15	0.01	6.40	Si	>100
1670	(8+9)-VI-4	-3	0.00	6.40	Si	>100
1670	(8+9)-VIII-1	29	0.03	6.40	Si	>100
1670	(8+9)-VIII-2	15	0.01	6.40	Si	>100
1670	(8+9)-III-2	5	0.00	6.40	Si	>100
1670	(8+9)-I-4	18	0.02	6.40	Si	>100

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	1	-507	-0.63	19.20	31	-0.15	12.00	79	V	31
0	2	-929	-1.15	28.80	25	-0.28	18.00	65	V	25
0	3	-929	-1.15	28.80	25	-0.28	18.00	65	V	25
0	4	-507	-0.63	25.60	41	-0.15	16.00	>100	V	41
0	5	-507	-0.63	25.60	41	-0.15	16.00	>100	V	41
0	6	-507	-0.63	25.60	41	-0.15	16.00	>100	V	41
0	7	-507	-0.63	25.60	41	-0.15	16.00	>100	V	41
0	(8+9)-VIII-4	-2579	-3.19	32.00	10	-0.77	20.00	26	V	10
0	(8+9)-IV-2	-4127	-5.11	32.00	6.3	-1.24	20.00	16	V	6.3
0	(8+9)-II-2	-4727	-5.85	32.00	5.5	-1.42	20.00	14	V	5.5

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
0	(8+9)-VI-4	-3179	-3.93	32.00	8.1	-0.95	20.00	21	V	8.1
0	(8+9)-VI-2	-5012	-6.20	32.00	5.2	-1.50	20.00	13	V	5.2
0	(8+9)-VIII-2	-4412	-5.46	32.00	5.9	-1.32	20.00	15	V	5.9
0	(8+9)-IV-4	-2864	-3.54	32.00	9.0	-0.86	20.00	23	V	9.0
0	(8+9)-II-4	-3464	-4.29	32.00	7.5	-1.04	20.00	19	V	7.5
2200	(8+9)-V-1	-2761	-3.42	32.00	9.4	-0.83	20.00	24	V	9.4
2200	(8+9)-IV-1	2360	2.92	32.00	11	0.71	20.00	28	V	11
2200	(8+9)-I-2	-3930	-4.86	32.00	6.6	-1.18	20.00	17	V	6.6
2200	(8+9)-II-1	2949	3.65	32.00	8.8	0.88	20.00	23	V	8.8
2200	(8+9)-III-3	3925	4.86	32.00	6.6	1.18	20.00	17	V	6.6
2200	(8+9)-VI-3	5008	6.20	32.00	5.2	1.50	20.00	13	V	5.2
2200	(8+9)-I-1	-1691	-2.09	32.00	15	-0.51	20.00	39	V	15
2200	(8+9)-I-4	1863	2.30	32.00	14	0.56	20.00	36	V	14
2200	(8+9)-IV-3	4098	5.07	32.00	6.3	1.23	20.00	16	V	6.3
2200	(8+9)-VII-1	-2937	-3.63	32.00	8.8	-0.88	20.00	23	V	8.8
2200	(8+9)-II-3	4687	5.80	32.00	5.5	1.40	20.00	14	V	5.5
2200	(8+9)-VII-2	-4823	-5.97	32.00	5.4	-1.44	20.00	14	V	5.4
2200	(8+9)-V-3	5172	6.40	32.00	5.0	1.55	20.00	13	V	5.0
2200	(8+9)-VII-3	4995	6.18	32.00	5.2	1.50	20.00	13	V	5.2
2200	(8+9)-VI-1	2628	3.25	32.00	9.8	0.79	20.00	25	V	9.8
2200	(8+9)-VII-4	3109	3.85	32.00	8.3	0.93	20.00	21	V	8.3
2200	(8+9)-V-2	-5000	-6.19	32.00	5.2	-1.50	20.00	13	V	5.2
2200	(8+9)-V-4	2933	3.63	32.00	8.8	0.88	20.00	23	V	8.8
2200	(8+9)-III-4	2040	2.52	32.00	13	0.61	20.00	33	V	13
2200	(8+9)-III-1	-1868	-2.31	32.00	14	-0.56	20.00	36	V	14
2200	(8+9)-VIII-1	2039	2.52	32.00	13	0.61	20.00	33	V	13
2200	(8+9)-I-3	4102	5.08	32.00	6.3	1.23	20.00	16	V	6.3
2200	(8+9)-VIII-3	4419	5.47	32.00	5.9	1.32	20.00	15	V	5.9
2200	(8+9)-III-2	-3754	-4.64	32.00	6.9	-1.12	20.00	18	V	6.9
Verifiche nella direzione secondaria										
835	1	309	0.29	19.20	66	0.07	12.00	>100	V	66
835	2	637	0.60	28.80	48	0.14	18.00	>100	V	48
835	3	637	0.60	28.80	48	0.14	18.00	>100	V	48
835	4	309	0.29	25.60	88	0.07	16.00	>100	V	88
835	5	309	0.29	25.60	88	0.07	16.00	>100	V	88
835	6	309	0.29	25.60	88	0.07	16.00	>100	V	88
835	7	309	0.29	25.60	88	0.07	16.00	>100	V	88
1670	(8+9)-VIII-4	3954	3.71	32.00	8.6	0.90	20.00	22	V	8.6
1670	(8+9)-IV-2	6660	6.25	32.00	5.1	1.51	20.00	13	V	5.1
1670	(8+9)-V-1	3658	3.44	32.00	9.3	0.83	20.00	24	V	9.3
1670	(8+9)-I-2	5708	5.36	32.00	6.0	1.30	20.00	15	V	6.0
1670	(8+9)-V-2	7509	7.05	32.00	4.5	1.71	20.00	12	V	4.5
1670	(8+9)-I-4	-1510	-1.42	32.00	23	-0.34	20.00	58	V	23
1670	(8+9)-V-3	-7161	-6.73	32.00	4.8	-1.63	20.00	12	V	4.8
1670	(8+9)-II-2	7674	7.21	32.00	4.4	1.74	20.00	11	V	4.4
1670	(8+9)-V-4	-3311	-3.11	32.00	10	-0.75	20.00	27	V	10
1670	(8+9)-II-4	5509	5.17	32.00	6.2	1.25	20.00	16	V	6.2
1670	(8+9)-VI-1	-4621	-4.34	32.00	7.4	-1.05	20.00	19	V	7.4
1670	(8+9)-III-2	5403	5.07	32.00	6.3	1.23	20.00	16	V	6.3
1670	(8+9)-VI-2	8214	7.71	32.00	4.1	1.87	20.00	11	V	4.1
1670	(8+9)-III-4	-1814	-1.70	32.00	19	-0.41	20.00	49	V	19
1670	(8+9)-VI-3	-7867	-7.39	32.00	4.3	-1.79	20.00	11	V	4.3
1670	(8+9)-I-1	1857	1.74	32.00	18	0.42	20.00	47	V	18
1670	(8+9)-VI-4	4969	4.67	32.00	6.9	1.13	20.00	18	V	6.9
1670	(8+9)-IV-4	4494	4.22	32.00	7.6	1.02	20.00	20	V	7.6
1670	(8+9)-VII-1	3962	3.72	32.00	8.6	0.90	20.00	22	V	8.6
1670	(8+9)-II-1	-5162	-4.85	32.00	6.6	-1.17	20.00	17	V	6.6
1670	(8+9)-VII-2	7204	6.77	32.00	4.7	1.64	20.00	12	V	4.7
1670	(8+9)-III-1	2161	2.03	32.00	16	0.49	20.00	41	V	16
1670	(8+9)-VII-3	-6857	-6.44	32.00	5.0	-1.56	20.00	13	V	5.0
1670	(8+9)-IV-1	-4147	-3.89	32.00	8.2	-0.94	20.00	21	V	8.2
1670	(8+9)-VII-4	-3615	-3.40	32.00	9.4	-0.82	20.00	24	V	9.4
1670	(8+9)-III-3	-5056	-4.75	32.00	6.7	-1.15	20.00	17	V	6.7
1670	(8+9)-IV-3	-6312	-5.93	32.00	5.4	-1.43	20.00	14	V	5.4

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
1670	(8+9)-II-3	-7327	-6.88	32.00	4.7	-1.67	20.00	12	V	4.7
1670	(8+9)-VIII-1	-3607	-3.39	32.00	9.4	-0.82	20.00	24	V	9.4
1670	(8+9)-VIII-2	7200	6.76	32.00	4.7	1.64	20.00	12	V	4.7
1670	(8+9)-VIII-3	-6853	-6.44	32.00	5.0	-1.56	20.00	13	V	5.0
1670	(8+9)-I-3	-5361	-5.03	32.00	6.4	-1.22	20.00	16	V	6.4

Setto 45: origine (1573.6,1503.5,303.5), direzione (-0.199392,0.97992,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X mm	Comb.	N kg	Mx kg*m	My kg*m	σ_n kg/cm ²	σ_{mx} kg/cm ²	σ_{my} kg/cm ²	ftd kg/cm ²	fcd kg/cm ²	fmd kg/cm ²	Cs
0	(8+9)-V-1	-2268	-23	-901	-1.87	-0.71	-2.67	132.00	192.00	192.00	57
0	(8+9)-VI-1	3205	10	1004	2.64	0.31	2.98	132.00	192.00	192.00	27
0	(8+9)-V-2	-4807	-35	-1787	-3.96	-1.08	-5.30	132.00	192.00	192.00	30
0	(8+9)-II-3	5002	25	1638	4.13	0.77	4.85	132.00	192.00	192.00	17
0	(8+9)-VIII-1	2678	5	788	2.21	0.15	2.33	132.00	192.00	192.00	34
0	(8+9)-V-4	2369	20	705	1.95	0.62	2.09	132.00	192.00	192.00	35
0	(8+9)-VII-3	4750	30	1526	3.92	0.94	4.52	132.00	192.00	192.00	17
0	(8+9)-III-1	-1239	-19	-586	-1.02	-0.58	-1.74	132.00	192.00	192.00	83
0	(8+9)-VII-1	-2426	-24	-966	-2.00	-0.76	-2.86	132.00	192.00	192.00	53
0	(8+9)-III-2	-3461	-28	-1342	-2.85	-0.85	-3.98	132.00	192.00	192.00	39
0	(8+9)-VI-3	5358	27	1752	4.42	0.82	5.19	132.00	192.00	192.00	15
0	(8+9)-III-3	3563	25	1146	2.94	0.76	3.40	132.00	192.00	192.00	23
0	(8+9)-I-4	1182	14	325	0.97	0.45	0.96	132.00	192.00	192.00	68
0	(8+9)-III-4	1340	16	390	1.11	0.50	1.16	132.00	192.00	192.00	59
0	(8+9)-VIII-3	4831	21	1536	3.98	0.66	4.55	132.00	192.00	192.00	17
0	(8+9)-IV-1	3035	7	902	2.50	0.20	2.67	132.00	192.00	192.00	29
0	(8+9)-I-3	3721	26	1211	3.07	0.81	3.59	132.00	192.00	192.00	22
0	(8+9)-II-1	3562	12	1118	2.94	0.37	3.31	132.00	192.00	192.00	24
0	(8+9)-VII-4	2528	22	770	2.08	0.67	2.28	132.00	192.00	192.00	32
0	(8+9)-I-1	-1081	-17	-521	-0.89	-0.53	-1.55	132.00	192.00	192.00	92
0	(8+9)-V-3	4908	32	1591	4.05	0.99	4.71	132.00	192.00	192.00	17
0	(8+9)-IV-3	4475	20	1422	3.69	0.61	4.21	132.00	192.00	192.00	19
0	(8+9)-VII-2	-4649	-33	-1722	-3.83	-1.03	-5.10	132.00	192.00	192.00	31
1200	1	188	-12	-109	0.16	-0.37	-0.32	79.20	115.20	115.20	>100
1200	2	411	-25	-229	0.34	-0.79	-0.68	118.80	172.80	172.80	88
1200	3	411	-25	-229	0.34	-0.79	-0.68	118.80	172.80	172.80	88
1200	4	188	-12	-109	0.16	-0.37	-0.32	105.60	153.60	153.60	>100
1200	5	188	-12	-109	0.16	-0.37	-0.32	105.60	153.60	153.60	>100
1200	6	188	-12	-109	0.16	-0.37	-0.32	105.60	153.60	153.60	>100
1200	7	188	-12	-109	0.16	-0.37	-0.32	105.60	153.60	153.60	>100
2400	(8+9)-VIII-2	2369	-15	1060	1.95	-0.46	3.14	132.00	192.00	192.00	30
2400	(8+9)-IV-4	1333	-27	633	1.10	-0.85	1.87	132.00	192.00	192.00	44
2400	(8+9)-VI-4	1728	-23	775	1.43	-0.71	2.30	132.00	192.00	192.00	38
2400	(8+9)-I-2	1943	9	847	1.60	0.29	2.51	132.00	192.00	192.00	37
2400	(8+9)-VI-2	2918	-11	1269	2.41	-0.35	3.76	132.00	192.00	192.00	25
2400	(8+9)-II-2	2764	-10	1202	2.28	-0.32	3.56	132.00	192.00	192.00	27
2400	(8+9)-II-4	1882	-24	842	1.55	-0.74	2.49	132.00	192.00	192.00	35
2400	(8+9)-IV-2	2216	-14	993	1.83	-0.43	2.94	132.00	192.00	192.00	32
2400	(8+9)-VIII-4	1180	-26	566	0.97	-0.82	1.68	132.00	192.00	192.00	49
Verifiche nella direzione secondaria											
0	(8+9)-II-2	523	-7	2104	0.45	-0.33	4.53	132.00	192.00	192.00	35
0	(8+9)-VII-1	-536	-30	1390	-0.46	-1.49	2.99	132.00	192.00	192.00	43
0	(8+9)-III-2	-41	-23	1694	-0.04	-1.14	3.65	132.00	192.00	192.00	40
0	(8+9)-V-2	294	-21	2036	0.25	-1.04	4.38	132.00	192.00	192.00	33
0	(8+9)-V-1	-616	-29	1342	-0.53	-1.44	2.89	132.00	192.00	192.00	44
0	(8+9)-VI-2	600	-6	2192	0.52	-0.29	4.72	132.00	192.00	192.00	33
0	(8+9)-III-1	-791	-33	1097	-0.68	-1.64	2.36	132.00	192.00	192.00	48
0	(8+9)-I-1	-871	-32	1048	-0.75	-1.59	2.26	132.00	192.00	192.00	50
0	(8+9)-I-2	39	-24	1743	0.03	-1.19	3.75	132.00	192.00	192.00	38
835	(8+9)-VIII-4	-509	-9	1384	-0.44	-0.42	2.98	132.00	192.00	192.00	56
835	(8+9)-IV-2	-727	-7	2145	-0.63	-0.33	4.62	132.00	192.00	192.00	39
835	(8+9)-VI-4	-476	-8	1624	-0.41	-0.38	3.49	132.00	192.00	192.00	50
835	(8+9)-VII-2	-1155	-11	2349	-0.99	-0.52	5.06	132.00	192.00	192.00	34

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
835	(8+9)-IV-4	-537	-8	1509	-0.46	-0.42	3.25	132.00	192.00	192.00	52
835	(8+9)-II-4	-505	-8	1748	-0.43	-0.38	3.76	132.00	192.00	192.00	46
835	(8+9)-VIII-2	-755	-7	2270	-0.65	-0.33	4.89	132.00	192.00	192.00	37
1670	1	-791	-39	765	-0.68	-1.91	1.65	79.20	115.20	115.20	32
1670	2	-1627	-82	1703	-1.40	-4.05	3.66	118.80	172.80	172.80	22
1670	3	-1627	-82	1703	-1.40	-4.05	3.66	118.80	172.80	172.80	22
1670	4	-791	-39	765	-0.68	-1.91	1.65	105.60	153.60	153.60	43
1670	5	-791	-39	765	-0.68	-1.91	1.65	105.60	153.60	153.60	43
1670	6	-791	-39	765	-0.68	-1.91	1.65	105.60	153.60	153.60	43
1670	7	-791	-39	765	-0.68	-1.91	1.65	105.60	153.60	153.60	43
1670	(8+9)-I-4	-453	-52	1011	-0.39	-2.55	2.18	132.00	192.00	192.00	41
1670	(8+9)-VI-3	-498	-39	2491	-0.43	-1.94	5.36	132.00	192.00	192.00	26
1670	(8+9)-IV-1	-579	-31	1568	-0.50	-1.52	3.37	132.00	192.00	192.00	39
1670	(8+9)-I-3	-450	-53	1941	-0.39	-2.63	4.18	132.00	192.00	192.00	28
1670	(8+9)-V-3	-398	-62	2387	-0.34	-3.05	5.14	132.00	192.00	192.00	23
1670	(8+9)-VII-3	-401	-65	2322	-0.34	-3.18	5.00	132.00	192.00	192.00	23
1670	(8+9)-VI-1	-586	-19	1649	-0.50	-0.93	3.55	132.00	192.00	192.00	43
1670	(8+9)-VII-4	-398	-57	1522	-0.34	-2.83	3.27	132.00	192.00	192.00	31
1670	(8+9)-II-3	-514	-37	2357	-0.44	-1.82	5.07	132.00	192.00	192.00	28
1670	(8+9)-V-4	-400	-60	1457	-0.34	-2.97	3.14	132.00	192.00	192.00	31
1670	(8+9)-III-3	-453	-56	1876	-0.39	-2.77	4.04	132.00	192.00	192.00	28
1670	(8+9)-IV-3	-522	-46	2141	-0.45	-2.28	4.61	132.00	192.00	192.00	28
1670	(8+9)-VIII-1	-594	-28	1434	-0.51	-1.39	3.09	132.00	192.00	192.00	43
1670	(8+9)-II-1	-571	-21	1783	-0.49	-1.05	3.84	132.00	192.00	192.00	39
1670	(8+9)-VIII-3	-506	-49	2275	-0.44	-2.41	4.90	132.00	192.00	192.00	26
1670	(8+9)-III-4	-450	-49	1075	-0.39	-2.41	2.31	132.00	192.00	192.00	41

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Ty kg	τ_d kg/cmq	fvd kg/cmq	RS	Cs
0	(8+9)-V-1	16	0.01	6.40	Si	>100
0	(8+9)-II-4	-15	0.01	6.40	Si	>100
0	(8+9)-V-4	-24	0.01	6.40	Si	>100
0	(8+9)-I-1	12	0.01	6.40	Si	>100
0	(8+9)-III-1	11	0.01	6.40	Si	>100
0	(8+9)-I-2	7	0.00	6.40	Si	>100
0	(8+9)-III-2	9	0.01	6.40	Si	>100
0	(8+9)-VII-2	13	0.01	6.40	Si	>100
0	(8+9)-VI-4	-16	0.01	6.40	Si	>100
0	(8+9)-VII-1	15	0.01	6.40	Si	>100
0	(8+9)-I-4	-19	0.01	6.40	Si	>100
0	(8+9)-V-2	12	0.01	6.40	Si	>100
1200	(8+9)-IV-2	-8	0.00	6.40	Si	>100
1200	(8+9)-II-2	-11	0.01	6.40	Si	>100
1200	(8+9)-VI-2	-9	0.01	6.40	Si	>100
1200	(8+9)-VIII-2	-6	0.00	6.40	Si	>100
1200	(8+9)-VIII-4	-14	0.01	6.40	Si	>100
1200	(8+9)-IV-4	-12	0.01	6.40	Si	>100
2400	1	21	0.01	3.84	Si	>100
2400	2	44	0.03	5.76	Si	>100
2400	3	44	0.03	5.76	Si	>100
2400	4	21	0.01	5.12	Si	>100
2400	5	21	0.01	5.12	Si	>100
2400	6	21	0.01	5.12	Si	>100
2400	7	21	0.01	5.12	Si	>100
2400	(8+9)-IV-1	19	0.01	6.40	Si	>100
2400	(8+9)-III-4	18	0.01	6.40	Si	>100
2400	(8+9)-III-3	22	0.01	6.40	Si	>100
2400	(8+9)-I-3	23	0.01	6.40	Si	>100
2400	(8+9)-VII-3	28	0.02	6.40	Si	>100
2400	(8+9)-V-3	29	0.02	6.40	Si	>100
2400	(8+9)-VII-4	24	0.01	6.40	Si	>100
2400	(8+9)-VI-1	20	0.01	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
2400	(8+9)-VI-3	27	0.02	6.40	Si	>100
2400	(8+9)-II-3	25	0.02	6.40	Si	>100
2400	(8+9)-VIII-1	17	0.01	6.40	Si	>100
2400	(8+9)-IV-3	23	0.01	6.40	Si	>100
2400	(8+9)-VIII-3	24	0.01	6.40	Si	>100
2400	(8+9)-II-1	21	0.01	6.40	Si	>100
Verifiche nella direzione secondaria						
0	(8+9)-III-3	68	0.05	6.40	Si	>100
0	(8+9)-VI-2	12	0.01	6.40	Si	>100
0	(8+9)-I-3	67	0.05	6.40	Si	>100
0	(8+9)-VIII-2	9	0.01	6.40	Si	>100
0	(8+9)-I-4	74	0.06	6.40	Si	>100
0	(8+9)-VI-1	-14	0.01	6.40	Si	>100
0	(8+9)-II-1	-40	0.03	6.40	Si	>100
0	(8+9)-IV-2	-18	0.01	6.40	Si	>100
0	(8+9)-II-2	-15	0.01	6.40	Si	>100
0	(8+9)-I-1	-84	0.07	6.40	Si	96
0	(8+9)-III-4	73	0.06	6.40	Si	>100
0	(8+9)-IV-1	-37	0.03	6.40	Si	>100
0	(8+9)-I-2	-76	0.06	6.40	Si	>100
0	(8+9)-IV-4	27	0.02	6.40	Si	>100
0	(8+9)-II-4	31	0.02	6.40	Si	>100
0	(8+9)-III-1	-83	0.07	6.40	Si	97
0	(8+9)-III-2	-77	0.06	6.40	Si	>100
1670	1	-22	0.02	3.84	Si	>100
1670	2	-47	0.04	5.76	Si	>100
1670	3	-47	0.04	5.76	Si	>100
1670	4	-22	0.02	5.12	Si	>100
1670	5	-22	0.02	5.12	Si	>100
1670	6	-22	0.02	5.12	Si	>100
1670	7	-22	0.02	5.12	Si	>100
1670	(8+9)-VIII-4	-16	0.01	6.40	Si	>100
1670	(8+9)-II-3	-28	0.02	6.40	Si	>100
1670	(8+9)-VII-2	27	0.02	6.40	Si	>100
1670	(8+9)-V-3	-56	0.04	6.40	Si	>100
1670	(8+9)-VII-3	-57	0.05	6.40	Si	>100
1670	(8+9)-V-2	25	0.02	6.40	Si	>100
1670	(8+9)-VII-4	-51	0.04	6.40	Si	>100
1670	(8+9)-VII-1	20	0.02	6.40	Si	>100
1670	(8+9)-V-4	-52	0.04	6.40	Si	>100
1670	(8+9)-V-1	22	0.02	6.40	Si	>100
1670	(8+9)-VI-4	-21	0.02	6.40	Si	>100
1670	(8+9)-VIII-1	-15	0.01	6.40	Si	>100
1670	(8+9)-IV-3	-33	0.03	6.40	Si	>100
1670	(8+9)-VIII-3	-38	0.03	6.40	Si	>100
1670	(8+9)-VI-3	-32	0.03	6.40	Si	>100

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Tx kg	τ_{vd} kg/cm ²	fvd kg/cm ²	Csv	τ_M kg/cm ²	fTd kg/cm ²	Csm	Mecc.	Cs
0	1	-494	-0.61	19.20	31	-0.15	12.00	81	V	31
0	2	-889	-1.10	28.80	26	-0.27	18.00	68	V	26
0	3	-889	-1.10	28.80	26	-0.27	18.00	68	V	26
0	4	-494	-0.61	25.60	42	-0.15	16.00	>100	V	42
0	5	-494	-0.61	25.60	42	-0.15	16.00	>100	V	42
0	6	-494	-0.61	25.60	42	-0.15	16.00	>100	V	42
0	7	-494	-0.61	25.60	42	-0.15	16.00	>100	V	42
0	(8+9)-V-1	-1725	-2.13	32.00	15	-0.52	20.00	39	V	15
0	(8+9)-I-1	-1010	-1.25	32.00	26	-0.30	20.00	66	V	26
0	(8+9)-III-2	-2747	-3.40	32.00	9.4	-0.82	20.00	24	V	9.4
0	(8+9)-I-2	-2897	-3.58	32.00	8.9	-0.87	20.00	23	V	8.9
0	(8+9)-VI-4	-2800	-3.46	32.00	9.2	-0.84	20.00	24	V	9.2
0	(8+9)-VIII-2	-3691	-4.57	32.00	7.0	-1.11	20.00	18	V	7.0

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
0	(8+9)-VI-2	-4191	-5.19	32.00	6.2	-1.25	20.00	16	V	6.2
0	(8+9)-II-2	-3976	-4.92	32.00	6.5	-1.19	20.00	17	V	6.5
0	(8+9)-II-4	-3015	-3.73	32.00	8.6	-0.90	20.00	22	V	8.6
0	(8+9)-VIII-4	-2300	-2.85	32.00	11	-0.69	20.00	29	V	11
0	(8+9)-VII-2	-3463	-4.28	32.00	7.5	-1.04	20.00	19	V	7.5
0	(8+9)-VII-1	-1875	-2.32	32.00	14	-0.56	20.00	36	V	14
0	(8+9)-III-1	-1160	-1.43	32.00	22	-0.35	20.00	58	V	22
0	(8+9)-IV-2	-3477	-4.30	32.00	7.4	-1.04	20.00	19	V	7.4
0	(8+9)-V-2	-3613	-4.47	32.00	7.2	-1.08	20.00	18	V	7.2
0	(8+9)-IV-4	-2515	-3.11	32.00	10	-0.75	20.00	27	V	10
2400	(8+9)-VI-1	2683	3.32	32.00	9.6	0.80	20.00	25	V	9.6
2400	(8+9)-VIII-1	2185	2.70	32.00	12	0.65	20.00	31	V	12
2400	(8+9)-IV-3	3460	4.28	32.00	7.5	1.04	20.00	19	V	7.5
2400	(8+9)-I-4	1042	1.29	32.00	25	0.31	20.00	64	V	25
2400	(8+9)-V-4	1782	2.21	32.00	15	0.53	20.00	37	V	15
2400	(8+9)-VIII-3	3682	4.56	32.00	7.0	1.10	20.00	18	V	7.0
2400	(8+9)-III-4	1191	1.47	32.00	22	0.36	20.00	56	V	22
2400	(8+9)-I-3	2954	3.66	32.00	8.8	0.88	20.00	23	V	8.8
2400	(8+9)-III-3	2805	3.47	32.00	9.2	0.84	20.00	24	V	9.2
2400	(8+9)-II-1	2906	3.59	32.00	8.9	0.87	20.00	23	V	8.9
2400	(8+9)-VII-3	3546	4.39	32.00	7.3	1.06	20.00	19	V	7.3
2400	(8+9)-VII-4	1932	2.39	32.00	13	0.58	20.00	35	V	13
2400	(8+9)-V-3	3695	4.57	32.00	7.0	1.11	20.00	18	V	7.0
2400	(8+9)-IV-1	2407	2.98	32.00	11	0.72	20.00	28	V	11
2400	(8+9)-VI-3	4180	5.17	32.00	6.2	1.25	20.00	16	V	6.2
2400	(8+9)-II-3	3958	4.90	32.00	6.5	1.19	20.00	17	V	6.5
Verifiche nella direzione secondaria										
835	(8+9)-I-1	1490	1.28	32.00	25	0.31	20.00	64	V	25
835	(8+9)-VII-1	3490	3.00	32.00	11	0.73	20.00	28	V	11
835	(8+9)-V-1	3156	2.72	32.00	12	0.66	20.00	30	V	12
835	(8+9)-III-4	-2338	-2.01	32.00	16	-0.49	20.00	41	V	16
835	(8+9)-III-1	1824	1.57	32.00	20	0.38	20.00	53	V	20
835	(8+9)-I-4	-2004	-1.72	32.00	19	-0.42	20.00	48	V	19
1670	1	-538	-0.46	19.20	41	-0.11	12.00	>100	V	41
1670	2	-1220	-1.05	28.80	27	-0.25	18.00	71	V	27
1670	3	-1220	-1.05	28.80	27	-0.25	18.00	71	V	27
1670	4	-538	-0.46	25.60	55	-0.11	16.00	>100	V	55
1670	5	-538	-0.46	25.60	55	-0.11	16.00	>100	V	55
1670	6	-538	-0.46	25.60	55	-0.11	16.00	>100	V	55
1670	7	-538	-0.46	25.60	55	-0.11	16.00	>100	V	55
1670	(8+9)-VIII-4	4629	3.99	32.00	8.0	0.96	20.00	21	V	8.0
1670	(8+9)-V-4	-3848	-3.31	32.00	9.7	-0.80	20.00	25	V	9.7
1670	(8+9)-II-3	-9484	-8.16	32.00	3.9	-1.98	20.00	10	V	3.9
1670	(8+9)-VI-1	-6537	-5.63	32.00	5.7	-1.36	20.00	15	V	5.7
1670	(8+9)-II-2	8750	7.53	32.00	4.2	1.82	20.00	11	V	4.2
1670	(8+9)-VI-2	9320	8.02	32.00	4.0	1.94	20.00	10	V	4.0
1670	(8+9)-III-3	-6356	-5.47	32.00	5.8	-1.32	20.00	15	V	5.8
1670	(8+9)-VI-3	-10053	-8.65	32.00	3.7	-2.09	20.00	9.5	V	3.7
1670	(8+9)-IV-1	-5932	-5.11	32.00	6.3	-1.24	20.00	16	V	6.3
1670	(8+9)-VI-4	5804	5.00	32.00	6.4	1.21	20.00	17	V	6.4
1670	(8+9)-IV-3	-8309	-7.15	32.00	4.5	-1.73	20.00	12	V	4.5
1670	(8+9)-I-2	5975	5.14	32.00	6.2	1.24	20.00	16	V	6.2
1670	(8+9)-I-3	-6708	-5.78	32.00	5.5	-1.40	20.00	14	V	5.5
1670	(8+9)-VII-2	7519	6.47	32.00	4.9	1.57	20.00	13	V	4.9
1670	(8+9)-V-3	-8605	-7.41	32.00	4.3	-1.79	20.00	11	V	4.3
1670	(8+9)-VII-3	-8253	-7.10	32.00	4.5	-1.72	20.00	12	V	4.5
1670	(8+9)-III-2	5623	4.84	32.00	6.6	1.17	20.00	17	V	6.6
1670	(8+9)-VII-4	-4201	-3.62	32.00	8.8	-0.88	20.00	23	V	8.8
1670	(8+9)-V-2	7872	6.78	32.00	4.7	1.64	20.00	12	V	4.7
1670	(8+9)-II-4	6373	5.49	32.00	5.8	1.33	20.00	15	V	5.8
1670	(8+9)-II-1	-7106	-6.12	32.00	5.2	-1.48	20.00	14	V	5.2
1670	(8+9)-IV-4	5198	4.48	32.00	7.2	1.08	20.00	18	V	7.2
1670	(8+9)-VIII-1	-5362	-4.62	32.00	6.9	-1.12	20.00	18	V	6.9
1670	(8+9)-VIII-2	8145	7.01	32.00	4.6	1.70	20.00	12	V	4.6

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
1670	(8+9)-VIII-3	-8878	-7.64	32.00	4.2	-1.85	20.00	11	V	4.2
1670	(8+9)-IV-2	7576	6.52	32.00	4.9	1.58	20.00	13	V	4.9

Setto 46: origine (1627.4,1238.9,303.5), direzione (-0.199392,0.97992,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	1	1955	-26	-459	1.61	-0.80	-1.36	79.20	115.20	115.20	26
0	2	4198	-54	-900	3.46	-1.68	-2.67	118.80	172.80	172.80	18
0	3	4198	-54	-900	3.46	-1.68	-2.67	118.80	172.80	172.80	18
0	4	1955	-26	-459	1.61	-0.80	-1.36	105.60	153.60	153.60	34
0	5	1955	-26	-459	1.61	-0.80	-1.36	105.60	153.60	153.60	34
0	6	1955	-26	-459	1.61	-0.80	-1.36	105.60	153.60	153.60	34
0	7	1955	-26	-459	1.61	-0.80	-1.36	105.60	153.60	153.60	34
0	(8+9)-VIII-4	-5748	179	-3216	-4.74	5.56	-9.53	132.00	192.00	192.00	13
0	(8+9)-IV-1	9403	-223	2932	7.76	-6.91	8.69	132.00	192.00	192.00	7.1
0	(8+9)-V-1	-4496	-283	-2655	-3.71	-8.76	-7.87	132.00	192.00	192.00	11
0	(8+9)-I-2	-8260	-301	-4376	-6.81	-9.32	-12.97	132.00	192.00	192.00	8.5
0	(8+9)-V-2	-11436	-273	-5576	-9.43	-8.47	-16.52	132.00	192.00	192.00	7.5
0	(8+9)-I-4	4022	274	813	3.32	8.50	2.41	132.00	192.00	192.00	12
0	(8+9)-V-3	14139	238	4932	11.66	7.37	14.62	132.00	192.00	192.00	4.9
0	(8+9)-II-2	-12059	-88	-5968	-9.95	-2.74	-17.68	132.00	192.00	192.00	9.2
0	(8+9)-V-4	7198	247	2012	5.94	7.66	5.96	132.00	192.00	192.00	8.6
0	(8+9)-II-4	-8374	84	-4411	-6.91	2.61	-13.07	132.00	192.00	192.00	12
0	(8+9)-VI-1	10124	-111	3408	8.35	-3.45	10.10	132.00	192.00	192.00	7.5
0	(8+9)-III-2	-7758	-270	-4126	-6.40	-8.35	-12.23	132.00	192.00	192.00	9.2
0	(8+9)-VI-2	-13012	-80	-6327	-10.73	-2.49	-18.75	132.00	192.00	192.00	8.8
0	(8+9)-III-4	4524	306	1063	3.73	9.47	3.15	132.00	192.00	192.00	11
0	(8+9)-VI-3	15714	45	5684	12.96	1.38	16.84	132.00	192.00	192.00	5.2
0	(8+9)-IV-2	-10385	15	-5133	-8.57	0.46	-15.21	132.00	192.00	192.00	12
0	(8+9)-VI-4	-7421	76	-4051	-6.12	2.35	-12.00	132.00	192.00	192.00	13
0	(8+9)-IV-4	-6701	188	-3576	-5.53	5.81	-10.60	132.00	192.00	192.00	12
0	(8+9)-VII-1	-4998	-314	-2906	-4.12	-9.72	-8.61	132.00	192.00	192.00	10
0	(8+9)-II-1	11077	-120	3767	9.14	-3.71	11.16	132.00	192.00	192.00	6.8
0	(8+9)-VII-2	-10934	-242	-5325	-9.02	-7.51	-15.78	132.00	192.00	192.00	8.1
0	(8+9)-III-1	-1822	-341	-1707	-1.50	-10.57	-5.06	132.00	192.00	192.00	12
0	(8+9)-VII-3	13637	207	4682	11.25	6.41	13.87	132.00	192.00	192.00	5.2
0	(8+9)-I-1	-1320	-310	-1456	-1.09	-9.61	-4.31	132.00	192.00	192.00	14
0	(8+9)-VII-4	7700	278	2262	6.35	8.62	6.70	132.00	192.00	192.00	7.8
0	(8+9)-III-3	10461	234	3483	8.63	7.25	10.32	132.00	192.00	192.00	6.4
0	(8+9)-IV-3	13088	-51	4489	10.79	-1.57	13.30	132.00	192.00	192.00	6.3
0	(8+9)-II-3	14761	53	5324	12.18	1.64	15.78	132.00	192.00	192.00	5.5
0	(8+9)-VIII-1	8450	-215	2573	6.97	-6.66	7.62	132.00	192.00	192.00	7.9
0	(8+9)-VIII-2	-11338	23	-5492	-9.35	0.72	-16.28	132.00	192.00	192.00	11
0	(8+9)-VIII-3	14041	-59	4849	11.58	-1.82	14.37	132.00	192.00	192.00	5.8
0	(8+9)-I-3	10963	265	3733	9.04	8.21	11.06	132.00	192.00	192.00	5.9
Verifiche nella direzione secondaria											
0	1	-3330	-34	1357	-2.87	-1.66	2.92	79.20	115.20	115.20	25
0	(8+9)-VIII-4	-3677	-9	4560	-3.17	-0.44	9.81	132.00	192.00	192.00	19
0	(8+9)-IV-2	-5010	-31	7521	-4.31	-1.53	16.19	132.00	192.00	192.00	11
0	(8+9)-VII-3	854	18	-6286	0.73	0.88	-13.53	132.00	192.00	192.00	12
0	(8+9)-III-4	-1053	9	-1708	-0.91	0.44	-3.68	132.00	192.00	192.00	47
0	(8+9)-IV-3	366	-16	-5645	0.32	-0.77	-12.15	132.00	192.00	192.00	14
0	(8+9)-IV-1	-776	-35	-3102	-0.67	-1.71	-6.68	132.00	192.00	192.00	23
0	(8+9)-VIII-2	-5201	-34	7938	-4.48	-1.67	17.08	132.00	192.00	192.00	10
0	(8+9)-VII-4	-417	19	-3099	-0.36	0.93	-6.67	132.00	192.00	192.00	25
0	(8+9)-I-1	-3521	-56	3325	-3.03	-2.77	7.16	132.00	192.00	192.00	19
0	(8+9)-I-3	287	7	-5153	0.25	0.35	-11.09	132.00	192.00	192.00	16
0	(8+9)-IV-4	-3868	-12	4977	-3.33	-0.59	10.71	132.00	192.00	192.00	17
0	(8+9)-II-1	-543	-37	-3963	-0.47	-1.81	-8.53	132.00	192.00	192.00	19
0	(8+9)-V-1	-4158	-66	4716	-3.58	-3.26	10.15	132.00	192.00	192.00	14
0	(8+9)-II-3	599	-18	-6506	0.52	-0.87	-14.00	132.00	192.00	192.00	12
0	(8+9)-V-2	-5568	-64	8420	-4.79	-3.15	18.12	132.00	192.00	192.00	9.0

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-III-1	-3591	-56	3583	-3.09	-2.74	7.71	132.00	192.00	192.00	18
0	(8+9)-V-3	923	17	-6544	0.79	0.85	-14.08	132.00	192.00	192.00	12
0	(8+9)-III-3	217	8	-4895	0.19	0.38	-10.53	132.00	192.00	192.00	17
0	(8+9)-V-4	-486	20	-2841	-0.42	0.96	-6.11	132.00	192.00	192.00	27
0	(8+9)-VIII-1	-967	-38	-2684	-0.83	-1.86	-5.78	132.00	192.00	192.00	25
0	(8+9)-VI-1	-734	-40	-3545	-0.63	-1.96	-7.63	132.00	192.00	192.00	20
0	(8+9)-I-4	-1123	9	-1450	-0.97	0.47	-3.12	132.00	192.00	192.00	53
0	(8+9)-VI-2	-5434	-32	8799	-4.68	-1.58	18.94	132.00	192.00	192.00	9.3
0	(8+9)-II-4	-4101	-10	5838	-3.53	-0.49	12.56	132.00	192.00	192.00	15
0	(8+9)-VI-3	790	-15	-6923	0.68	-0.72	-14.90	132.00	192.00	192.00	12
0	(8+9)-VIII-3	557	-13	-6063	0.48	-0.62	-13.05	132.00	192.00	192.00	13
0	(8+9)-II-2	-5243	-29	8381	-4.51	-1.43	18.04	132.00	192.00	192.00	9.8
0	(8+9)-III-2	-4861	-54	6770	-4.18	-2.68	14.57	132.00	192.00	192.00	11
0	(8+9)-I-2	-4931	-54	7028	-4.24	-2.65	15.13	132.00	192.00	192.00	11
0	(8+9)-VI-4	-3910	-7	5421	-3.37	-0.34	11.67	132.00	192.00	192.00	16
0	(8+9)-VII-1	-4227	-66	4975	-3.64	-3.23	10.71	132.00	192.00	192.00	14
0	(8+9)-VII-2	-5498	-65	8161	-4.73	-3.18	17.57	132.00	192.00	192.00	9.2
1670	2	-4281	48	3353	-3.69	2.37	7.22	118.80	172.80	172.80	18
1670	3	-4281	48	3353	-3.69	2.37	7.22	118.80	172.80	172.80	18
1670	4	-2060	23	1626	-1.77	1.12	3.50	105.60	153.60	153.60	33
1670	5	-2060	23	1626	-1.77	1.12	3.50	105.60	153.60	153.60	33
1670	6	-2060	23	1626	-1.77	1.12	3.50	105.60	153.60	153.60	33
1670	7	-2060	23	1626	-1.77	1.12	3.50	105.60	153.60	153.60	33

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
0	1	34	0.02	3.84	Si	>100
0	2	72	0.04	5.76	Si	>100
0	3	72	0.04	5.76	Si	>100
0	4	34	0.02	5.12	Si	>100
0	5	34	0.02	5.12	Si	>100
0	6	34	0.02	5.12	Si	>100
0	7	34	0.02	5.12	Si	>100
0	(8+9)-VI-2	34	0.02	6.40	Si	>100
0	(8+9)-VII-2	217	0.13	6.40	Si	49
0	(8+9)-I-2	170	0.10	6.40	Si	63
0	(8+9)-VII-3	-170	0.10	6.40	Si	63
0	(8+9)-I-4	-151	0.09	6.40	Si	70
0	(8+9)-VII-4	-174	0.10	6.40	Si	61
0	(8+9)-II-2	23	0.01	6.40	Si	>100
0	(8+9)-VIII-1	88	0.05	6.40	Si	>100
0	(8+9)-II-4	-73	0.04	6.40	Si	>100
0	(8+9)-VIII-2	76	0.05	6.40	Si	>100
0	(8+9)-III-2	182	0.11	6.40	Si	59
0	(8+9)-VIII-3	-29	0.02	6.40	Si	>100
0	(8+9)-III-4	-139	0.08	6.40	Si	77
0	(8+9)-VIII-4	-41	0.02	6.40	Si	>100
0	(8+9)-IV-2	66	0.04	6.40	Si	>100
0	(8+9)-IV-3	-19	0.01	6.40	Si	>100
0	(8+9)-VI-4	-83	0.05	6.40	Si	>100
0	(8+9)-IV-4	-30	0.02	6.40	Si	>100
0	(8+9)-VII-1	221	0.13	6.40	Si	48
0	(8+9)-V-2	204	0.12	6.40	Si	52
0	(8+9)-I-3	-122	0.07	6.40	Si	87
0	(8+9)-V-4	-186	0.11	6.40	Si	57
0	(8+9)-II-1	120	0.07	6.40	Si	89
0	(8+9)-I-1	198	0.12	6.40	Si	54
0	(8+9)-V-1	233	0.14	6.40	Si	46
0	(8+9)-VI-1	130	0.08	6.40	Si	82
0	(8+9)-IV-1	78	0.05	6.40	Si	>100
0	(8+9)-V-3	-157	0.09	6.40	Si	68
0	(8+9)-III-1	186	0.11	6.40	Si	57

X	Comb.	Ty	τ_d	fvd	RS	Cs
0	(8+9)-III-3	-135	0.08	6.40	Si	79
1200	(8+9)-VI-3	18	0.01	6.40	Si	>100
1200	(8+9)-II-3	28	0.02	6.40	Si	>100
Verifiche nella direzione secondaria						
0	(8+9)-III-3	-159	0.13	6.40	Si	51
0	(8+9)-I-3	-159	0.13	6.40	Si	51
0	(8+9)-VIII-3	-92	0.07	6.40	Si	87
0	(8+9)-I-4	-138	0.11	6.40	Si	58
0	(8+9)-VII-3	-187	0.15	6.40	Si	43
0	(8+9)-IV-3	-84	0.07	6.40	Si	96
0	(8+9)-VI-2	78	0.06	6.40	Si	>100
0	(8+9)-II-2	69	0.06	6.40	Si	>100
0	(8+9)-IV-4	-17	0.01	6.40	Si	>100
0	(8+9)-II-3	-86	0.07	6.40	Si	94
0	(8+9)-VII-4	-166	0.13	6.40	Si	48
0	(8+9)-V-3	-187	0.15	6.40	Si	43
0	(8+9)-I-2	142	0.11	6.40	Si	57
0	(8+9)-VI-3	-94	0.08	6.40	Si	85
0	(8+9)-IV-2	67	0.05	6.40	Si	>100
0	(8+9)-III-4	-138	0.11	6.40	Si	58
0	(8+9)-III-2	142	0.11	6.40	Si	57
1670	1	54	0.04	3.84	Si	90
1670	2	113	0.09	5.76	Si	64
1670	3	113	0.09	5.76	Si	64
1670	4	54	0.04	5.12	Si	>100
1670	5	54	0.04	5.12	Si	>100
1670	6	54	0.04	5.12	Si	>100
1670	7	54	0.04	5.12	Si	>100
1670	(8+9)-VIII-4	-38	0.03	6.40	Si	>100
1670	(8+9)-III-1	140	0.11	6.40	Si	58
1670	(8+9)-VII-2	228	0.18	6.40	Si	35
1670	(8+9)-V-2	222	0.18	6.40	Si	36
1670	(8+9)-II-1	103	0.08	6.40	Si	78
1670	(8+9)-VI-1	132	0.11	6.40	Si	61
1670	(8+9)-II-4	-29	0.02	6.40	Si	>100
1670	(8+9)-VII-1	238	0.19	6.40	Si	34
1670	(8+9)-V-4	-170	0.14	6.40	Si	47
1670	(8+9)-V-1	244	0.19	6.40	Si	33
1670	(8+9)-VI-4	-59	0.05	6.40	Si	>100
1670	(8+9)-VIII-1	112	0.09	6.40	Si	72
1670	(8+9)-VIII-2	79	0.06	6.40	Si	>100
1670	(8+9)-IV-1	83	0.07	6.40	Si	98
1670	(8+9)-I-1	146	0.12	6.40	Si	55

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	(8+9)-III-2	-3404	-4.21	32.00	7.6	-1.02	20.00	20	V	7.6
0	(8+9)-I-2	-3600	-4.45	32.00	7.2	-1.08	20.00	19	V	7.2
0	(8+9)-VIII-4	-2665	-3.30	32.00	9.7	-0.80	20.00	25	V	9.7
0	(8+9)-V-1	-2132	-2.64	32.00	12	-0.64	20.00	31	V	12
0	(8+9)-VII-2	-4325	-5.35	32.00	6.0	-1.29	20.00	15	V	6.0
0	(8+9)-IV-4	-2942	-3.64	32.00	8.8	-0.88	20.00	23	V	8.8
0	(8+9)-VI-4	-3316	-4.10	32.00	7.8	-0.99	20.00	20	V	7.8
0	(8+9)-IV-2	-4231	-5.23	32.00	6.1	-1.27	20.00	16	V	6.1
0	(8+9)-V-2	-4520	-5.59	32.00	5.7	-1.35	20.00	15	V	5.7
0	(8+9)-II-2	-4882	-6.04	32.00	5.3	-1.46	20.00	14	V	5.3
0	(8+9)-VI-2	-5158	-6.38	32.00	5.0	-1.54	20.00	13	V	5.0
0	(8+9)-I-1	-1212	-1.50	32.00	21	-0.36	20.00	55	V	21
0	(8+9)-VII-1	-2327	-2.88	32.00	11	-0.70	20.00	29	V	11
0	(8+9)-VIII-2	-4507	-5.58	32.00	5.7	-1.35	20.00	15	V	5.7
0	(8+9)-II-4	-3592	-4.44	32.00	7.2	-1.08	20.00	19	V	7.2
0	(8+9)-III-1	-1407	-1.74	32.00	18	-0.42	20.00	47	V	18

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
2400	1	833	1.03	19.20	19	0.25	12.00	48	V	19
2400	2	1644	2.03	28.80	14	0.49	18.00	37	V	14
2400	3	1644	2.03	28.80	14	0.49	18.00	37	V	14
2400	4	833	1.03	25.60	25	0.25	16.00	64	V	25
2400	5	833	1.03	25.60	25	0.25	16.00	64	V	25
2400	6	833	1.03	25.60	25	0.25	16.00	64	V	25
2400	7	833	1.03	25.60	25	0.25	16.00	64	V	25
2400	(8+9)-IV-1	3144	3.89	32.00	8.2	0.94	20.00	21	V	8.2
2400	(8+9)-III-3	3774	4.67	32.00	6.9	1.13	20.00	18	V	6.9
2400	(8+9)-II-1	3795	4.70	32.00	6.8	1.14	20.00	18	V	6.8
2400	(8+9)-I-3	3970	4.91	32.00	6.5	1.19	20.00	17	V	6.5
2400	(8+9)-II-3	5130	6.35	32.00	5.0	1.54	20.00	13	V	5.0
2400	(8+9)-V-4	2522	3.12	32.00	10	0.76	20.00	26	V	10
2400	(8+9)-VII-3	4657	5.76	32.00	5.6	1.39	20.00	14	V	5.6
2400	(8+9)-I-4	1639	2.03	32.00	16	0.49	20.00	41	V	16
2400	(8+9)-VII-4	2717	3.36	32.00	9.5	0.81	20.00	25	V	9.5
2400	(8+9)-VI-1	3531	4.37	32.00	7.3	1.06	20.00	19	V	7.3
2400	(8+9)-VI-3	5395	6.67	32.00	4.8	1.62	20.00	12	V	4.8
2400	(8+9)-V-3	4852	6.00	32.00	5.3	1.45	20.00	14	V	5.3
2400	(8+9)-VIII-1	2879	3.56	32.00	9.0	0.86	20.00	23	V	9.0
2400	(8+9)-III-4	1835	2.27	32.00	14	0.55	20.00	36	V	14
2400	(8+9)-VIII-3	4744	5.87	32.00	5.5	1.42	20.00	14	V	5.5
2400	(8+9)-IV-3	4479	5.54	32.00	5.8	1.34	20.00	15	V	5.8
Verifiche nella direzione secondaria										
1670	1	-1149	-0.99	19.20	19	-0.24	12.00	50	V	19
1670	2	-2417	-2.08	28.80	14	-0.50	18.00	36	V	14
1670	3	-2417	-2.08	28.80	14	-0.50	18.00	36	V	14
1670	4	-1149	-0.99	25.60	26	-0.24	16.00	67	V	26
1670	5	-1149	-0.99	25.60	26	-0.24	16.00	67	V	26
1670	6	-1149	-0.99	25.60	26	-0.24	16.00	67	V	26
1670	7	-1149	-0.99	25.60	26	-0.24	16.00	67	V	26
1670	(8+9)-VIII-4	3885	3.34	32.00	9.6	0.81	20.00	25	V	9.6
1670	(8+9)-IV-2	6963	5.99	32.00	5.3	1.45	20.00	14	V	5.3
1670	(8+9)-V-1	2947	2.54	32.00	13	0.61	20.00	33	V	13
1670	(8+9)-I-2	5737	4.94	32.00	6.5	1.20	20.00	17	V	6.5
1670	(8+9)-V-2	7550	6.50	32.00	4.9	1.57	20.00	13	V	4.9
1670	(8+9)-I-4	-2711	-2.33	32.00	14	-0.56	20.00	35	V	14
1670	(8+9)-V-3	-9127	-7.86	32.00	4.1	-1.90	20.00	11	V	4.1
1670	(8+9)-II-2	8150	7.02	32.00	4.6	1.70	20.00	12	V	4.6
1670	(8+9)-V-4	-4524	-3.89	32.00	8.2	-0.94	20.00	21	V	8.2
1670	(8+9)-II-4	5615	4.83	32.00	6.6	1.17	20.00	17	V	6.6
1670	(8+9)-VI-1	-6648	-5.72	32.00	5.6	-1.39	20.00	14	V	5.6
1670	(8+9)-III-2	5380	4.63	32.00	6.9	1.12	20.00	18	V	6.9
1670	(8+9)-VI-2	8694	7.48	32.00	4.3	1.81	20.00	11	V	4.3
1670	(8+9)-III-4	-3067	-2.64	32.00	12	-0.64	20.00	31	V	12
1670	(8+9)-VI-3	-10271	-8.84	32.00	3.6	-2.14	20.00	9.3	V	3.6
1670	(8+9)-I-1	1134	0.98	32.00	33	0.24	20.00	85	V	33
1670	(8+9)-VI-4	5071	4.37	32.00	7.3	1.06	20.00	19	V	7.3
1670	(8+9)-IV-4	4429	3.81	32.00	8.4	0.92	20.00	22	V	8.4
1670	(8+9)-VII-1	3303	2.84	32.00	11	0.69	20.00	29	V	11
1670	(8+9)-II-1	-7192	-6.19	32.00	5.2	-1.50	20.00	13	V	5.2
1670	(8+9)-VII-2	7194	6.19	32.00	5.2	1.50	20.00	13	V	5.2
1670	(8+9)-III-1	1490	1.28	32.00	25	0.31	20.00	64	V	25
1670	(8+9)-VII-3	-8771	-7.55	32.00	4.2	-1.83	20.00	11	V	4.2
1670	(8+9)-IV-1	-6006	-5.17	32.00	6.2	-1.25	20.00	16	V	6.2
1670	(8+9)-VII-4	-4880	-4.20	32.00	7.6	-1.02	20.00	20	V	7.6
1670	(8+9)-III-3	-6957	-5.99	32.00	5.3	-1.45	20.00	14	V	5.3
1670	(8+9)-IV-3	-8540	-7.35	32.00	4.4	-1.78	20.00	11	V	4.4
1670	(8+9)-II-3	-9727	-8.37	32.00	3.8	-2.03	20.00	9.9	V	3.8
1670	(8+9)-VIII-1	-5462	-4.70	32.00	6.8	-1.14	20.00	18	V	6.8
1670	(8+9)-VIII-2	7507	6.46	32.00	5.0	1.56	20.00	13	V	5.0
1670	(8+9)-VIII-3	-9084	-7.82	32.00	4.1	-1.89	20.00	11	V	4.1
1670	(8+9)-I-3	-7313	-6.30	32.00	5.1	-1.52	20.00	13	V	5.1

Verifiche a instabilità

Setto(X)	Comb.	k _{critc}	k _{critm}	λ_{relc}	λ_{relm}	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
(cm)						kg/cm ^q	kg/cm ^q	kg/cm ^q	kg/cm ^q	kg/cm ^q	kg/cm ^q	
40(0.0)	(8+9)-VI-2	--	--	--	--	3.16	-0.06	-4.33	132.00	192.00	192.00	21
41(0.0)	(8+9)-VI-3	1.00	--	0.11	--	-1.12	-0.14	1.84	132.00	192.00	192.00	62
42(0.0)	(8+9)-VI-3	--	--	--	--	2.18	0.30	-2.54	132.00	192.00	192.00	32
43(0.0)	3	--	--	--	--	4.13	-1.22	-11.37	118.80	172.80	172.80	9.3
44(220.0)	(8+9)-VI-2	--	--	--	--	8.27	-0.17	16.78	132.00	192.00	192.00	6.6
45(0.0)	(8+9)-VI-3	--	--	--	--	4.42	0.82	5.19	132.00	192.00	192.00	15
46(0.0)	(8+9)-V-3	--	--	--	--	11.66	7.37	14.62	132.00	192.00	192.00	4.9

Parete Xlam 8 - Nodi: [11-32-2-3-33-34-112-111] - **Crit.Prog.** Criterio di verifica XLAM 0 - **Verificato:**
[Cs=1.692,Comb=(8+9)-VI-3]

Geometria setti

Setto	Crit.	X mm	L cm	S cm	X90 mm	L90 cm	S90 cm
47	Criterio di verifica XLAM 0	0	291.7	12.1	0	40.0	12.1
		200	295.4	12.1	1495	40.0	12.1
		400	299.0	12.1	--	--	--
48	Criterio di verifica XLAM 0	0	237.0	12.1	0	180.9	12.1
		905	253.5	12.1	1350	180.9	12.1
		1809	269.9	12.1	--	--	--
49	Criterio di verifica XLAM 0	0	49.9	12.1	0	120.0	12.1
		600	60.8	12.1	359	120.0	12.1
		1200	71.7	12.1	--	--	--

Setto 47: origine (1737.0,704.8,145.9), direzione (-0.199495,0.979899,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X mm	Comb.	N kg	M _x kg*m	M _y kg*m	σ_n kg/cm ^q	σ_{mx} kg/cm ^q	σ_{my} kg/cm ^q	ftd kg/cm ^q	fcd kg/cm ^q	fmd kg/cm ^q	Cs
200	2	-222	7	77	-0.10	0.11	0.07	118.80	172.80	172.80	>100
200	3	-222	7	77	-0.10	0.11	0.07	118.80	172.80	172.80	>100
400	1	-110	5	-18	-0.05	0.08	-0.02	79.20	115.20	115.20	>100
400	4	-110	5	-18	-0.05	0.08	-0.02	105.60	153.60	153.60	>100
400	5	-110	5	-18	-0.05	0.08	-0.02	105.60	153.60	153.60	>100
400	6	-110	5	-18	-0.05	0.08	-0.02	105.60	153.60	153.60	>100
400	7	-110	5	-18	-0.05	0.08	-0.02	105.60	153.60	153.60	>100
400	(8+9)-VIII-4	-2155	156	3420	-0.99	2.70	3.16	132.00	192.00	192.00	33
400	(8+9)-IV-1	2273	-156	-3869	1.05	-2.71	-3.58	132.00	192.00	192.00	25
400	(8+9)-V-1	-1702	-268	2769	-0.78	-4.63	2.56	132.00	192.00	192.00	27
400	(8+9)-I-2	-2857	-211	4781	-1.32	-3.66	4.42	132.00	192.00	192.00	24
400	(8+9)-V-2	-3705	-189	6130	-1.71	-3.27	5.67	132.00	192.00	192.00	21
400	(8+9)-I-4	718	296	-1464	0.33	5.12	-1.35	132.00	192.00	192.00	28
400	(8+9)-V-3	3569	195	-6173	1.64	3.38	-5.71	132.00	192.00	192.00	17
400	(8+9)-II-2	-3942	58	6516	-1.82	1.00	6.02	132.00	192.00	192.00	27
400	(8+9)-V-4	1566	274	-2813	0.72	4.74	-2.60	132.00	192.00	192.00	23
400	(8+9)-II-4	-2870	210	4642	-1.32	3.63	4.29	132.00	192.00	192.00	24
400	(8+9)-VI-1	2479	-197	-4281	1.14	-3.41	-3.96	132.00	192.00	192.00	21
400	(8+9)-III-2	-2719	-226	4536	-1.25	-3.90	4.19	132.00	192.00	192.00	24
400	(8+9)-VI-2	-4197	64	6920	-1.93	1.11	6.40	132.00	192.00	192.00	25
400	(8+9)-III-4	856	282	-1709	0.39	4.88	-1.58	132.00	192.00	192.00	27
400	(8+9)-VI-3	4060	-58	-6964	1.87	-1.01	-6.44	132.00	192.00	192.00	19
400	(8+9)-IV-2	-3482	10	5699	-1.60	0.18	5.27	132.00	192.00	192.00	35

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
400	(8+9)-VI-4	-2615	203	4238	-1.20	3.52	3.92	132.00	192.00	192.00	26
400	(8+9)-IV-4	-2410	163	3825	-1.11	2.81	3.54	132.00	192.00	192.00	30
400	(8+9)-VII-1	-1840	-253	3015	-0.85	-4.38	2.79	132.00	192.00	192.00	27
400	(8+9)-II-1	2734	-204	-4686	1.26	-3.53	-4.33	132.00	192.00	192.00	20
400	(8+9)-VII-2	-3567	-203	5885	-1.64	-3.52	5.44	132.00	192.00	192.00	21
400	(8+9)-III-1	-992	-276	1666	-0.46	-4.77	1.54	132.00	192.00	192.00	30
400	(8+9)-VII-3	3431	209	-5928	1.58	3.63	-5.48	132.00	192.00	192.00	17
400	(8+9)-I-1	-854	-290	1420	-0.39	-5.02	1.31	132.00	192.00	192.00	30
400	(8+9)-VII-4	1704	259	-3058	0.79	4.49	-2.83	132.00	192.00	192.00	23
400	(8+9)-III-3	2582	232	-4579	1.19	4.01	-4.23	132.00	192.00	192.00	19
400	(8+9)-IV-3	3346	-4	-5742	1.54	-0.07	-5.31	132.00	192.00	192.00	25
400	(8+9)-II-3	3806	-52	-6559	1.75	-0.89	-6.06	132.00	192.00	192.00	20
400	(8+9)-VIII-1	2019	-150	-3464	0.93	-2.59	-3.20	132.00	192.00	192.00	27
400	(8+9)-VIII-2	-3736	17	6103	-1.72	0.29	5.64	132.00	192.00	192.00	32
400	(8+9)-VIII-3	3600	-11	-6147	1.66	-0.19	-5.68	132.00	192.00	192.00	23
400	(8+9)-I-3	2720	217	-4825	1.25	3.76	-4.46	132.00	192.00	192.00	19
Verifiche nella direzione secondaria											
0	1	-590	-1	10	-3.05	-0.18	0.75	79.20	115.20	115.20	>100
0	2	-970	-1	16	-5.01	-0.42	1.25	118.80	172.80	172.80	95
0	3	-970	-1	16	-5.01	-0.42	1.25	118.80	172.80	172.80	95
0	4	-590	-1	10	-3.05	-0.18	0.75	105.60	153.60	153.60	>100
0	5	-590	-1	10	-3.05	-0.18	0.75	105.60	153.60	153.60	>100
0	6	-590	-1	10	-3.05	-0.18	0.75	105.60	153.60	153.60	>100
0	7	-590	-1	10	-3.05	-0.18	0.75	105.60	153.60	153.60	>100
0	(8+9)-VIII-4	-3665	2	415	-18.93	0.58	32.16	132.00	192.00	192.00	5.5
0	(8+9)-IV-2	-6218	-3	668	-32.12	-0.75	51.79	132.00	192.00	192.00	3.3
0	(8+9)-V-1	-3618	-8	313	-18.69	-2.23	24.25	132.00	192.00	192.00	6.8
0	(8+9)-I-2	-5705	-8	545	-29.47	-2.38	42.24	132.00	192.00	192.00	3.9
0	(8+9)-V-2	-6985	-8	712	-36.08	-2.24	55.17	132.00	192.00	192.00	3.0
0	(8+9)-I-4	1524	7	-133	7.87	2.18	-10.28	132.00	192.00	192.00	8.0
0	(8+9)-V-3	6170	7	-699	31.87	2.06	-54.13	132.00	192.00	192.00	1.9
0	(8+9)-II-2	-7103	-3	774	-36.69	-0.80	59.94	132.00	192.00	192.00	2.8
0	(8+9)-V-4	2804	7	-299	14.48	2.04	-23.20	132.00	192.00	192.00	4.1
0	(8+9)-II-4	-4934	2	570	-25.49	0.56	44.18	132.00	192.00	192.00	4.0
0	(8+9)-VI-1	3736	-2	-507	19.30	-0.70	-39.25	132.00	192.00	192.00	2.8
0	(8+9)-III-2	-5440	-8	514	-28.10	-2.36	39.80	132.00	192.00	192.00	4.1
0	(8+9)-VI-2	-7487	-3	824	-38.67	-0.76	63.81	132.00	192.00	192.00	2.7
0	(8+9)-III-4	1790	7	-164	9.24	2.19	-12.72	132.00	192.00	192.00	6.8
0	(8+9)-VI-3	6672	2	-810	34.47	0.58	-62.77	132.00	192.00	192.00	1.7
0	(8+9)-I-1	-2338	-8	146	-12.08	-2.36	11.32	132.00	192.00	192.00	13
0	(8+9)-VI-4	-4550	2	520	-23.50	0.52	40.30	132.00	192.00	192.00	4.4
0	(8+9)-IV-4	-4049	2	465	-20.91	0.62	36.04	132.00	192.00	192.00	4.9
0	(8+9)-VII-1	-3883	-8	345	-20.06	-2.24	26.69	132.00	192.00	192.00	6.2
0	(8+9)-II-1	4120	-3	-557	21.28	-0.74	-43.13	132.00	192.00	192.00	2.6
0	(8+9)-VII-2	-6719	-8	681	-34.71	-2.23	52.73	132.00	192.00	192.00	3.1
0	(8+9)-III-1	-2604	-8	178	-13.45	-2.37	13.77	132.00	192.00	192.00	11
0	(8+9)-VII-3	5905	7	-667	30.50	2.05	-51.68	132.00	192.00	192.00	2.0
0	(8+9)-IV-1	3235	-3	-452	16.71	-0.80	-34.99	132.00	192.00	192.00	3.2
0	(8+9)-VII-4	3069	7	-331	15.85	2.06	-25.65	132.00	192.00	192.00	3.8
0	(8+9)-III-3	4625	7	-500	23.89	2.18	-38.75	132.00	192.00	192.00	2.5
0	(8+9)-IV-3	5404	2	-655	27.91	0.57	-50.75	132.00	192.00	192.00	2.1
0	(8+9)-II-3	6289	2	-760	32.48	0.62	-58.89	132.00	192.00	192.00	1.8
0	(8+9)-VIII-1	2851	-3	-402	14.73	-0.76	-31.11	132.00	192.00	192.00	3.6
0	(8+9)-VIII-2	-6602	-2	719	-34.10	-0.71	55.67	132.00	192.00	192.00	3.1
0	(8+9)-VIII-3	5787	2	-705	29.89	0.53	-54.62	132.00	192.00	192.00	1.9
0	(8+9)-I-3	4891	7	-532	25.26	2.20	-41.20	132.00	192.00	192.00	2.4

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
0	1	7	0.00	3.84	Si	>100
0	2	13	0.00	5.76	Si	>100
0	3	13	0.00	5.76	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
0	4	7	0.00	5.12	Si	>100
0	5	7	0.00	5.12	Si	>100
0	6	7	0.00	5.12	Si	>100
0	7	7	0.00	5.12	Si	>100
0	(8+9)-IV-2	-36	0.01	6.40	Si	>100
0	(8+9)-VIII-1	33	0.01	6.40	Si	>100
0	(8+9)-VI-1	76	0.03	6.40	Si	>100
0	(8+9)-IV-3	46	0.02	6.40	Si	>100
0	(8+9)-II-1	57	0.02	6.40	Si	>100
0	(8+9)-II-2	-79	0.03	6.40	Si	>100
0	(8+9)-II-3	89	0.03	6.40	Si	>100
0	(8+9)-II-4	-48	0.02	6.40	Si	>100
0	(8+9)-VI-4	-66	0.02	6.40	Si	>100
200	(8+9)-VIII-4	30	0.01	6.40	Si	>100
200	(8+9)-I-3	91	0.03	6.40	Si	>100
200	(8+9)-IV-4	29	0.01	6.40	Si	>100
200	(8+9)-III-2	-70	0.02	6.40	Si	>100
200	(8+9)-III-1	-70	0.02	6.40	Si	>100
200	(8+9)-I-4	68	0.02	6.40	Si	>100
200	(8+9)-III-4	80	0.03	6.40	Si	>100
200	(8+9)-I-1	-58	0.02	6.40	Si	>100
200	(8+9)-I-2	-82	0.03	6.40	Si	>100
200	(8+9)-III-3	79	0.03	6.40	Si	>100
400	(8+9)-IV-1	21	0.01	6.40	Si	>100
400	(8+9)-VI-2	-76	0.03	6.40	Si	>100
400	(8+9)-VII-3	125	0.04	6.40	Si	>100
400	(8+9)-V-4	108	0.04	6.40	Si	>100
400	(8+9)-VII-4	119	0.04	6.40	Si	>100
400	(8+9)-VII-1	-109	0.04	6.40	Si	>100
400	(8+9)-VII-2	-116	0.04	6.40	Si	>100
400	(8+9)-V-3	136	0.05	6.40	Si	>100
400	(8+9)-V-2	-126	0.04	6.40	Si	>100
400	(8+9)-V-1	-99	0.03	6.40	Si	>100
400	(8+9)-VIII-2	-42	0.01	6.40	Si	>100
400	(8+9)-VIII-3	51	0.02	6.40	Si	>100
400	(8+9)-VI-3	86	0.03	6.40	Si	>100
Verifiche nella direzione secondaria						
0	1	1	0.01	3.84	Si	>100
0	2	3	0.02	5.76	Si	>100
0	3	3	0.02	5.76	Si	>100
0	4	1	0.01	5.12	Si	>100
0	5	1	0.01	5.12	Si	>100
0	6	1	0.01	5.12	Si	>100
0	7	1	0.01	5.12	Si	>100
0	(8+9)-VIII-4	-8	0.04	6.40	Si	>100
0	(8+9)-I-1	14	0.07	6.40	Si	93
0	(8+9)-II-4	-9	0.04	6.40	Si	>100
0	(8+9)-III-1	14	0.07	6.40	Si	94
0	(8+9)-I-4	-13	0.06	6.40	Si	>100
0	(8+9)-VI-4	-9	0.04	6.40	Si	>100
0	(8+9)-VI-1	10	0.05	6.40	Si	>100
0	(8+9)-VIII-1	10	0.05	6.40	Si	>100
0	(8+9)-II-1	11	0.05	6.40	Si	>100
0	(8+9)-IV-1	10	0.05	6.40	Si	>100
0	(8+9)-IV-4	-9	0.04	6.40	Si	>100
0	(8+9)-III-4	-13	0.06	6.40	Si	>100
1495	(8+9)-IV-2	9	0.04	6.40	Si	>100
1495	(8+9)-V-1	15	0.07	6.40	Si	91
1495	(8+9)-I-2	12	0.06	6.40	Si	>100
1495	(8+9)-II-2	8	0.04	6.40	Si	>100
1495	(8+9)-IV-3	-9	0.04	6.40	Si	>100
1495	(8+9)-VII-1	14	0.07	6.40	Si	93
1495	(8+9)-III-2	12	0.06	6.40	Si	>100
1495	(8+9)-VII-2	18	0.09	6.40	Si	75

X	Comb.	Ty	τ_d	fvd	RS	Cs
1495	(8+9)-V-3	-18	0.08	6.40	Si	76
1495	(8+9)-VII-3	-18	0.09	6.40	Si	75
1495	(8+9)-II-3	-8	0.04	6.40	Si	>100
1495	(8+9)-VII-4	-15	0.07	6.40	Si	92
1495	(8+9)-V-2	18	0.08	6.40	Si	77
1495	(8+9)-V-4	-15	0.07	6.40	Si	90
1495	(8+9)-VI-2	9	0.04	6.40	Si	>100
1495	(8+9)-III-3	-13	0.06	6.40	Si	>100
1495	(8+9)-I-3	-12	0.06	6.40	Si	>100
1495	(8+9)-VIII-2	11	0.05	6.40	Si	>100
1495	(8+9)-VIII-3	-11	0.05	6.40	Si	>100
1495	(8+9)-VI-3	-10	0.05	6.40	Si	>100

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	(8+9)-II-2	-7849	-5.56	32.00	5.8	-1.35	20.00	15	V	5.8
0	(8+9)-VIII-4	-4004	-2.84	32.00	11	-0.69	20.00	29	V	11
0	(8+9)-III-3	5490	3.89	32.00	8.2	0.94	20.00	21	V	8.2
0	(8+9)-I-4	1731	1.23	32.00	26	0.30	20.00	67	V	26
0	(8+9)-II-3	8000	5.67	32.00	5.6	1.37	20.00	15	V	5.6
0	(8+9)-III-4	2061	1.46	32.00	22	0.35	20.00	57	V	22
0	(8+9)-IV-2	-6750	-4.78	32.00	6.7	-1.16	20.00	17	V	6.7
0	(8+9)-VIII-2	-7276	-5.15	32.00	6.2	-1.25	20.00	16	V	6.2
0	(8+9)-VI-2	-8375	-5.93	32.00	5.4	-1.44	20.00	14	V	5.4
0	(8+9)-I-2	-5669	-4.01	32.00	8.0	-0.97	20.00	21	V	8.0
0	(8+9)-VII-2	-7093	-5.02	32.00	6.4	-1.22	20.00	16	V	6.4
0	(8+9)-VI-4	-5103	-3.61	32.00	8.9	-0.87	20.00	23	V	8.9
0	(8+9)-I-1	-1580	-1.12	32.00	29	-0.27	20.00	74	V	29
0	(8+9)-I-3	5820	4.12	32.00	7.8	1.00	20.00	20	V	7.8
0	(8+9)-II-4	-5629	-3.99	32.00	8.0	-0.96	20.00	21	V	8.0
0	(8+9)-III-1	-1910	-1.35	32.00	24	-0.33	20.00	61	V	24
0	(8+9)-III-2	-5339	-3.78	32.00	8.5	-0.92	20.00	22	V	8.5
200	(8+9)-V-1	-3443	-2.41	32.00	13	-0.58	20.00	34	V	13
200	(8+9)-V-4	3621	2.53	32.00	13	0.61	20.00	33	V	13
200	(8+9)-VII-4	3965	2.77	32.00	12	0.67	20.00	30	V	12
200	(8+9)-VII-1	-3787	-2.65	32.00	12	-0.64	20.00	31	V	12
200	(8+9)-V-3	7702	5.39	32.00	5.9	1.30	20.00	15	V	5.9
200	(8+9)-V-2	-7524	-5.26	32.00	6.1	-1.27	20.00	16	V	6.1
400	1	178	0.12	19.20	>100	0.03	12.00	>100	V	>100
400	2	248	0.17	28.80	>100	0.04	18.00	>100	V	>100
400	3	248	0.17	28.80	>100	0.04	18.00	>100	V	>100
400	4	178	0.12	25.60	>100	0.03	16.00	>100	V	>100
400	5	178	0.12	25.60	>100	0.03	16.00	>100	V	>100
400	6	178	0.12	25.60	>100	0.03	16.00	>100	V	>100
400	7	178	0.12	25.60	>100	0.03	16.00	>100	V	>100
400	(8+9)-IV-1	4907	3.39	32.00	9.4	0.82	20.00	24	V	9.4
400	(8+9)-VI-3	8745	6.04	32.00	5.3	1.46	20.00	14	V	5.3
400	(8+9)-VI-1	5402	3.73	32.00	8.6	0.90	20.00	22	V	8.6
400	(8+9)-VII-3	7467	5.16	32.00	6.2	1.25	20.00	16	V	6.2
400	(8+9)-II-1	5967	4.12	32.00	7.8	1.00	20.00	20	V	7.8
400	(8+9)-VIII-1	4343	3.00	32.00	11	0.73	20.00	28	V	11
400	(8+9)-IV-3	7121	4.92	32.00	6.5	1.19	20.00	17	V	6.5
400	(8+9)-VIII-3	7686	5.31	32.00	6.0	1.29	20.00	16	V	6.0
400	(8+9)-IV-4	-4648	-3.21	32.00	10.0	-0.78	20.00	26	V	10.0
Verifiche nella direzione secondaria										
0	1	17	0.09	19.20	>100	0.02	12.00	>100	V	>100
0	2	30	0.16	28.80	>100	0.04	18.00	>100	V	>100
0	3	30	0.16	28.80	>100	0.04	18.00	>100	V	>100
0	4	17	0.09	25.60	>100	0.02	16.00	>100	V	>100
0	5	17	0.09	25.60	>100	0.02	16.00	>100	V	>100
0	6	17	0.09	25.60	>100	0.02	16.00	>100	V	>100
0	7	17	0.09	25.60	>100	0.02	16.00	>100	V	>100

X	Comb.	Tx	τvd	fvd	Csv	τM	fTd	Csm	Mecc.	Cs
1495	(8+9)-VIII-4	820	4.24	32.00	7.6	1.03	20.00	20	V	7.6
1495	(8+9)-IV-2	1372	7.09	32.00	4.5	1.71	20.00	12	V	4.5
1495	(8+9)-V-1	669	3.46	32.00	9.3	0.84	20.00	24	V	9.3
1495	(8+9)-I-2	1178	6.08	32.00	5.3	1.47	20.00	14	V	5.3
1495	(8+9)-V-2	1479	7.64	32.00	4.2	1.85	20.00	11	V	4.2
1495	(8+9)-I-4	-359	-1.86	32.00	17	-0.45	20.00	45	V	17
1495	(8+9)-V-3	-1471	-7.60	32.00	4.2	-1.84	20.00	11	V	4.2
1495	(8+9)-II-2	1585	8.19	32.00	3.9	1.98	20.00	10	V	3.9
1495	(8+9)-V-4	-661	-3.41	32.00	9.4	-0.83	20.00	24	V	9.4
1495	(8+9)-II-4	1124	5.80	32.00	5.5	1.40	20.00	14	V	5.5
1495	(8+9)-VI-1	-1025	-5.30	32.00	6.0	-1.28	20.00	16	V	6.0
1495	(8+9)-III-2	1114	5.75	32.00	5.6	1.39	20.00	14	V	5.6
1495	(8+9)-VI-2	1675	8.65	32.00	3.7	2.09	20.00	9.5	V	3.7
1495	(8+9)-III-4	-423	-2.19	32.00	15	-0.53	20.00	38	V	15
1495	(8+9)-VI-3	-1667	-8.61	32.00	3.7	-2.08	20.00	9.6	V	3.7
1495	(8+9)-I-1	368	1.90	32.00	17	0.46	20.00	43	V	17
1495	(8+9)-VI-4	1033	5.34	32.00	6.0	1.29	20.00	15	V	6.0
1495	(8+9)-IV-4	911	4.70	32.00	6.8	1.14	20.00	18	V	6.8
1495	(8+9)-VII-1	733	3.79	32.00	8.5	0.92	20.00	22	V	8.5
1495	(8+9)-II-1	-1116	-5.76	32.00	5.6	-1.39	20.00	14	V	5.6
1495	(8+9)-VII-2	1415	7.31	32.00	4.4	1.77	20.00	11	V	4.4
1495	(8+9)-III-1	432	2.23	32.00	14	0.54	20.00	37	V	14
1495	(8+9)-VII-3	-1407	-7.27	32.00	4.4	-1.76	20.00	11	V	4.4
1495	(8+9)-IV-1	-902	-4.66	32.00	6.9	-1.13	20.00	18	V	6.9
1495	(8+9)-VII-4	-725	-3.74	32.00	8.5	-0.91	20.00	22	V	8.5
1495	(8+9)-III-3	-1106	-5.71	32.00	5.6	-1.38	20.00	14	V	5.6
1495	(8+9)-IV-3	-1363	-7.04	32.00	4.5	-1.70	20.00	12	V	4.5
1495	(8+9)-II-3	-1577	-8.14	32.00	3.9	-1.97	20.00	10	V	3.9
1495	(8+9)-VIII-1	-812	-4.19	32.00	7.6	-1.01	20.00	20	V	7.6
1495	(8+9)-VIII-2	1462	7.55	32.00	4.2	1.83	20.00	11	V	4.2
1495	(8+9)-VIII-3	-1454	-7.51	32.00	4.3	-1.82	20.00	11	V	4.3
1495	(8+9)-I-3	-1170	-6.04	32.00	5.3	-1.46	20.00	14	V	5.3

Setto 48: origine (1797.0,410.0,118.5), direzione (-0.199495,0.979899,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σn	σmx	σmy	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	1	24	-10	111	0.01	-0.22	0.16	79.20	115.20	115.20	>100
0	2	32	-20	94	0.02	-0.43	0.14	118.80	172.80	172.80	>100
0	3	32	-20	94	0.02	-0.43	0.14	118.80	172.80	172.80	>100
0	4	24	-10	111	0.01	-0.22	0.16	105.60	153.60	153.60	>100
0	5	24	-10	111	0.01	-0.22	0.16	105.60	153.60	153.60	>100
0	6	24	-10	111	0.01	-0.22	0.16	105.60	153.60	153.60	>100
0	7	24	-10	111	0.01	-0.22	0.16	105.60	153.60	153.60	>100
0	(8+9)-I-1	162	-217	-803	0.09	-4.74	-1.18	132.00	192.00	192.00	32
0	(8+9)-IV-2	220	-128	-2909	0.13	-2.79	-4.28	132.00	192.00	192.00	26
1809	(8+9)-VIII-4	-2252	135	3316	-1.15	2.59	3.76	132.00	192.00	192.00	30
1809	(8+9)-IV-1	2797	-143	-3983	1.43	-2.74	-4.52	132.00	192.00	192.00	21
1809	(8+9)-V-2	-4404	-215	6355	-2.25	-4.12	7.21	132.00	192.00	192.00	17
1809	(8+9)-I-4	1200	177	-1698	0.61	3.40	-1.93	132.00	192.00	192.00	31
1809	(8+9)-V-3	4641	212	-6594	2.37	4.06	-7.48	132.00	192.00	192.00	13
1809	(8+9)-II-2	-4586	-149	6663	-2.34	-2.85	7.56	132.00	192.00	192.00	18
1809	(8+9)-V-4	2230	160	-3121	1.14	3.08	-3.54	132.00	192.00	192.00	23
1809	(8+9)-II-4	-3214	-26	4674	-1.64	-0.50	5.30	132.00	192.00	192.00	33
1809	(8+9)-VI-1	3141	28	-4487	1.60	0.54	-5.09	132.00	192.00	192.00	24
1809	(8+9)-III-2	-3179	-182	4652	-1.62	-3.49	5.28	132.00	192.00	192.00	22
1809	(8+9)-VI-2	-4895	-144	7090	-2.50	-2.76	8.04	132.00	192.00	192.00	18
1809	(8+9)-III-4	1396	227	-1977	0.71	4.36	-2.24	132.00	192.00	192.00	25
1809	(8+9)-VI-3	5131	141	-7330	2.62	2.70	-8.32	132.00	192.00	192.00	13
1809	(8+9)-I-2	-3375	-232	4931	-1.72	-4.44	5.60	132.00	192.00	192.00	19
1809	(8+9)-VI-4	-2905	-31	4247	-1.48	-0.60	4.82	132.00	192.00	192.00	35
1809	(8+9)-IV-4	-2561	140	3743	-1.31	2.68	4.25	132.00	192.00	192.00	28
1809	(8+9)-VII-1	-2189	-213	3161	-1.12	-4.09	3.59	132.00	192.00	192.00	25

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
1809	(8+9)-II-1	3450	23	-4914	1.76	0.44	-5.58	132.00	192.00	192.00	22
1809	(8+9)-VII-2	-4208	-165	6075	-2.15	-3.16	6.89	132.00	192.00	192.00	19
1809	(8+9)-III-1	-1160	-230	1737	-0.59	-4.41	1.97	132.00	192.00	192.00	30
1809	(8+9)-VII-3	4445	162	-6315	2.27	3.11	-7.17	132.00	192.00	192.00	14
1809	(8+9)-I-3	3611	229	-5171	1.84	4.39	-5.87	132.00	192.00	192.00	15
1809	(8+9)-VII-4	2426	210	-3401	1.24	4.03	-3.86	132.00	192.00	192.00	20
1809	(8+9)-III-3	3415	179	-4892	1.74	3.43	-5.55	132.00	192.00	192.00	17
1809	(8+9)-IV-3	4170	-20	-5972	2.13	-0.39	-6.78	132.00	192.00	192.00	19
1809	(8+9)-II-3	4823	146	-6903	2.46	2.80	-7.83	132.00	192.00	192.00	14
1809	(8+9)-VIII-1	2488	-138	-3556	1.27	-2.64	-4.04	132.00	192.00	192.00	23
1809	(8+9)-VIII-2	-4242	22	6159	-2.17	0.43	6.99	132.00	192.00	192.00	26
1809	(8+9)-VIII-3	4479	-25	-6399	2.29	-0.48	-7.26	132.00	192.00	192.00	17
1809	(8+9)-V-1	-1993	-163	2882	-1.02	-3.13	3.27	132.00	192.00	192.00	30
Verifiche nella direzione secondaria											
0	1	-1367	5	-350	-1.56	0.31	-1.33	79.20	115.20	115.20	69
0	4	-1367	5	-350	-1.56	0.31	-1.33	105.60	153.60	153.60	93
0	5	-1367	5	-350	-1.56	0.31	-1.33	105.60	153.60	153.60	93
0	6	-1367	5	-350	-1.56	0.31	-1.33	105.60	153.60	153.60	93
0	7	-1367	5	-350	-1.56	0.31	-1.33	105.60	153.60	153.60	93
0	(8+9)-VIII-4	944	-9	5743	1.08	-0.56	21.76	132.00	192.00	192.00	8.0
0	(8+9)-IV-2	2181	-20	9779	2.49	-1.30	37.04	132.00	192.00	192.00	4.6
0	(8+9)-V-1	477	-8	4578	0.54	-0.52	17.34	132.00	192.00	192.00	10
0	(8+9)-I-1	-141	1	2324	-0.16	0.04	8.80	132.00	192.00	192.00	22
0	(8+9)-V-2	2323	-31	10586	2.65	-2.03	40.10	132.00	192.00	192.00	4.2
0	(8+9)-I-3	-3648	30	-8874	-4.17	1.95	-33.62	132.00	192.00	192.00	5.4
0	(8+9)-V-3	-4266	38	-11128	-4.87	2.51	-42.16	132.00	192.00	192.00	4.3
0	(8+9)-II-1	-3523	38	-8605	-4.02	2.47	-32.60	132.00	192.00	192.00	5.5
0	(8+9)-V-4	-2420	15	-5120	-2.76	1.00	-19.40	132.00	192.00	192.00	9.4
0	(8+9)-II-3	-4575	47	-11964	-5.23	3.04	-45.32	132.00	192.00	192.00	4.0
0	(8+9)-VI-1	-3337	35	-7929	-3.81	2.30	-30.04	132.00	192.00	192.00	5.9
0	(8+9)-III-1	-6	-5	2817	-0.01	-0.34	10.67	132.00	192.00	192.00	17
0	(8+9)-VI-2	2817	-42	12099	3.22	-2.74	45.83	132.00	192.00	192.00	3.6
0	(8+9)-III-3	-3513	24	-8381	-4.01	1.57	-31.75	132.00	192.00	192.00	5.7
0	(8+9)-VI-3	-4760	49	-12641	-5.44	3.21	-47.89	132.00	192.00	192.00	3.7
0	(8+9)-IV-1	-3073	18	-6962	-3.51	1.20	-26.37	132.00	192.00	192.00	6.9
0	(8+9)-VI-4	1394	-28	7387	1.59	-1.83	27.98	132.00	192.00	192.00	6.0
0	(8+9)-IV-3	-4125	27	-10321	-4.71	1.77	-39.10	132.00	192.00	192.00	4.7
0	(8+9)-VII-1	612	-14	5071	0.70	-0.90	19.21	132.00	192.00	192.00	9.1
0	(8+9)-I-2	1705	-23	8332	1.95	-1.47	31.56	132.00	192.00	192.00	5.4
0	(8+9)-VII-2	2188	-25	10093	2.50	-1.65	38.24	132.00	192.00	192.00	4.4
0	(8+9)-II-2	2631	-39	11422	3.01	-2.57	43.27	132.00	192.00	192.00	3.8
0	(8+9)-VII-3	-4131	33	-10635	-4.72	2.13	-40.29	132.00	192.00	192.00	4.5
0	(8+9)-III-2	1570	-17	7839	1.79	-1.09	29.70	132.00	192.00	192.00	5.7
0	(8+9)-VIII-3	-4310	30	-10997	-4.92	1.94	-41.66	132.00	192.00	192.00	4.4
0	(8+9)-III-4	-1937	12	-3359	-2.21	0.82	-12.72	132.00	192.00	192.00	14
0	(8+9)-I-4	-1802	7	-2866	-2.06	0.43	-10.86	132.00	192.00	192.00	17
0	(8+9)-II-4	1579	-31	8063	1.80	-2.00	30.54	132.00	192.00	192.00	5.5
0	(8+9)-IV-4	1129	-11	6420	1.29	-0.73	24.32	132.00	192.00	192.00	7.1
0	(8+9)-VII-4	-2555	21	-5613	-2.92	1.38	-21.26	132.00	192.00	192.00	8.5
0	(8+9)-VIII-1	-2887	16	-6285	-3.30	1.03	-23.81	132.00	192.00	192.00	7.7
0	(8+9)-VIII-2	2366	-22	10455	2.70	-1.47	39.61	132.00	192.00	192.00	4.3
1350	2	-1782	1	-496	-2.03	0.07	-1.88	118.80	172.80	172.80	88
1350	3	-1782	1	-496	-2.03	0.07	-1.88	118.80	172.80	172.80	88

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
0	(8+9)-VII-1	-59	0.02	6.40	Si	>100
0	(8+9)-III-2	-49	0.02	6.40	Si	>100
0	(8+9)-IV-1	43	0.02	6.40	Si	>100
0	(8+9)-III-3	52	0.02	6.40	Si	>100
0	(8+9)-VIII-2	-73	0.03	6.40	Si	>100
0	(8+9)-III-4	21	0.01	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
0	(8+9)-VII-4	63	0.03	6.40	Si	>100
0	(8+9)-VII-2	-90	0.04	6.40	Si	>100
0	(8+9)-IV-2	-61	0.03	6.40	Si	>100
0	(8+9)-I-2	-52	0.02	6.40	Si	>100
0	(8+9)-IV-3	64	0.03	6.40	Si	>100
0	(8+9)-I-4	18	0.01	6.40	Si	>100
0	(8+9)-IV-4	-40	0.02	6.40	Si	>100
0	(8+9)-II-2	-70	0.03	6.40	Si	>100
0	(8+9)-V-1	-56	0.02	6.40	Si	>100
0	(8+9)-II-4	-50	0.02	6.40	Si	>100
0	(8+9)-V-2	-93	0.04	6.40	Si	>100
0	(8+9)-VIII-3	77	0.03	6.40	Si	>100
0	(8+9)-V-3	97	0.04	6.40	Si	>100
0	(8+9)-VII-3	94	0.04	6.40	Si	>100
0	(8+9)-V-4	60	0.03	6.40	Si	>100
0	(8+9)-I-3	55	0.02	6.40	Si	>100
0	(8+9)-VI-1	41	0.02	6.40	Si	>100
0	(8+9)-II-3	74	0.03	6.40	Si	>100
0	(8+9)-VIII-1	31	0.01	6.40	Si	>100
0	(8+9)-I-1	-14	0.01	6.40	Si	>100
0	(8+9)-II-1	53	0.02	6.40	Si	>100
0	(8+9)-III-1	-17	0.01	6.40	Si	>100
0	(8+9)-VI-2	-83	0.04	6.40	Si	>100
0	(8+9)-VI-3	86	0.04	6.40	Si	>100
0	(8+9)-VI-4	-37	0.02	6.40	Si	>100
905	1	5	0.00	3.84	Si	>100
905	2	10	0.00	5.76	Si	>100
905	3	10	0.00	5.76	Si	>100
905	4	5	0.00	5.12	Si	>100
905	5	5	0.00	5.12	Si	>100
905	6	5	0.00	5.12	Si	>100
905	7	5	0.00	5.12	Si	>100
905	(8+9)-VIII-4	35	0.01	6.40	Si	>100
Verifiche nella direzione secondaria						
0	1	-5	0.01	3.84	Si	>100
0	2	-6	0.01	5.76	Si	>100
0	3	-6	0.01	5.76	Si	>100
0	4	-5	0.01	5.12	Si	>100
0	5	-5	0.01	5.12	Si	>100
0	6	-5	0.01	5.12	Si	>100
0	7	-5	0.01	5.12	Si	>100
0	(8+9)-V-1	27	0.03	6.40	Si	>100
0	(8+9)-VI-3	-65	0.07	6.40	Si	93
0	(8+9)-VI-2	57	0.06	6.40	Si	>100
0	(8+9)-VII-3	-59	0.06	6.40	Si	>100
0	(8+9)-VI-1	-38	0.04	6.40	Si	>100
0	(8+9)-VII-1	33	0.03	6.40	Si	>100
0	(8+9)-V-4	-36	0.04	6.40	Si	>100
0	(8+9)-VII-4	-41	0.04	6.40	Si	>100
0	(8+9)-III-4	-15	0.02	6.40	Si	>100
0	(8+9)-II-1	-46	0.05	6.40	Si	>100
0	(8+9)-II-3	-58	0.06	6.40	Si	>100
0	(8+9)-VII-2	50	0.05	6.40	Si	>100
0	(8+9)-V-3	-64	0.07	6.40	Si	95
0	(8+9)-II-4	37	0.04	6.40	Si	>100
0	(8+9)-V-2	56	0.06	6.40	Si	>100
1350	(8+9)-VIII-4	-35	0.04	6.40	Si	>100
1350	(8+9)-IV-2	-50	0.05	6.40	Si	>100
1350	(8+9)-I-4	14	0.01	6.40	Si	>100
1350	(8+9)-IV-4	-34	0.04	6.40	Si	>100
1350	(8+9)-I-3	39	0.04	6.40	Si	>100
1350	(8+9)-IV-1	35	0.04	6.40	Si	>100
1350	(8+9)-I-2	-38	0.04	6.40	Si	>100
1350	(8+9)-III-2	-38	0.04	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
1350	(8+9)-I-1	-13	0.01	6.40	Si	>100
1350	(8+9)-IV-3	50	0.05	6.40	Si	>100
1350	(8+9)-III-3	39	0.04	6.40	Si	>100
1350	(8+9)-III-1	-13	0.01	6.40	Si	>100
1350	(8+9)-VI-4	-35	0.04	6.40	Si	>100
1350	(8+9)-VIII-1	36	0.04	6.40	Si	>100
1350	(8+9)-VIII-2	-48	0.05	6.40	Si	>100
1350	(8+9)-VIII-3	49	0.05	6.40	Si	>100
1350	(8+9)-II-2	-49	0.05	6.40	Si	>100

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Tx kg	τ_{vd} kg/cm ²	fvd kg/cm ²	Csv	τ_M kg/cm ²	fTd kg/cm ²	Csm	Mecc.	Cs
905	1	390	0.32	19.20	60	0.08	12.00	>100	V	60
905	2	422	0.34	28.80	84	0.08	18.00	>100	V	84
905	3	422	0.34	28.80	84	0.08	18.00	>100	V	84
905	4	390	0.32	25.60	81	0.08	16.00	>100	V	81
905	5	390	0.32	25.60	81	0.08	16.00	>100	V	81
905	6	390	0.32	25.60	81	0.08	16.00	>100	V	81
905	7	390	0.32	25.60	81	0.08	16.00	>100	V	81
905	(8+9)-VIII-4	-6110	-4.98	32.00	6.4	-1.21	20.00	17	V	6.4
905	(8+9)-IV-1	7442	6.07	32.00	5.3	1.47	20.00	14	V	5.3
905	(8+9)-V-1	-4913	-4.01	32.00	8.0	-0.97	20.00	21	V	8.0
905	(8+9)-I-2	-8890	-7.25	32.00	4.4	-1.75	20.00	11	V	4.4
905	(8+9)-V-2	-11308	-9.22	32.00	3.5	-2.23	20.00	9.0	V	3.5
905	(8+9)-I-4	3101	2.53	32.00	13	0.61	20.00	33	V	13
905	(8+9)-V-3	11915	9.71	32.00	3.3	2.35	20.00	8.5	V	3.3
905	(8+9)-II-2	-12154	-9.91	32.00	3.2	-2.40	20.00	8.3	V	3.2
905	(8+9)-V-4	5520	4.50	32.00	7.1	1.09	20.00	18	V	7.1
905	(8+9)-II-4	-8557	-6.98	32.00	4.6	-1.69	20.00	12	V	4.6
905	(8+9)-VI-1	8438	6.88	32.00	4.7	1.66	20.00	12	V	4.7
905	(8+9)-III-2	-8373	-6.83	32.00	4.7	-1.65	20.00	12	V	4.7
905	(8+9)-VI-2	-12880	-10.50	32.00	3.0	-2.54	20.00	7.9	V	3.0
905	(8+9)-III-4	3618	2.95	32.00	11	0.71	20.00	28	V	11
905	(8+9)-VI-3	13487	10.99	32.00	2.9	2.66	20.00	7.5	V	2.9
905	(8+9)-IV-2	-10433	-8.50	32.00	3.8	-2.06	20.00	9.7	V	3.8
905	(8+9)-VI-4	-7832	-6.38	32.00	5.0	-1.54	20.00	13	V	5.0
905	(8+9)-IV-4	-6836	-5.57	32.00	5.7	-1.35	20.00	15	V	5.7
905	(8+9)-VII-1	-5430	-4.43	32.00	7.2	-1.07	20.00	19	V	7.2
905	(8+9)-II-1	9164	7.47	32.00	4.3	1.81	20.00	11	V	4.3
905	(8+9)-VII-2	-10792	-8.80	32.00	3.6	-2.13	20.00	9.4	V	3.6
905	(8+9)-III-1	-3011	-2.45	32.00	13	-0.59	20.00	34	V	13
905	(8+9)-VII-3	11399	9.29	32.00	3.4	2.25	20.00	8.9	V	3.4
905	(8+9)-I-1	-2494	-2.03	32.00	16	-0.49	20.00	41	V	16
905	(8+9)-VII-4	6036	4.92	32.00	6.5	1.19	20.00	17	V	6.5
905	(8+9)-III-3	8980	7.32	32.00	4.4	1.77	20.00	11	V	4.4
905	(8+9)-IV-3	11039	9.00	32.00	3.6	2.18	20.00	9.2	V	3.6
905	(8+9)-II-3	12761	10.40	32.00	3.1	2.52	20.00	7.9	V	3.1
905	(8+9)-VIII-1	6717	5.48	32.00	5.8	1.33	20.00	15	V	5.8
905	(8+9)-VIII-2	-11158	-9.10	32.00	3.5	-2.20	20.00	9.1	V	3.5
905	(8+9)-VIII-3	11765	9.59	32.00	3.3	2.32	20.00	8.6	V	3.3
905	(8+9)-I-3	9496	7.74	32.00	4.1	1.87	20.00	11	V	4.1
Verifiche nella direzione secondaria										
1350	1	-79	-0.09	19.20	>100	-0.02	12.00	>100	V	>100
1350	2	-7	-0.01	28.80	>100	-0.00	18.00	>100	V	>100
1350	3	-7	-0.01	28.80	>100	-0.00	18.00	>100	V	>100
1350	4	-79	-0.09	25.60	>100	-0.02	16.00	>100	V	>100
1350	5	-79	-0.09	25.60	>100	-0.02	16.00	>100	V	>100
1350	6	-79	-0.09	25.60	>100	-0.02	16.00	>100	V	>100
1350	7	-79	-0.09	25.60	>100	-0.02	16.00	>100	V	>100
1350	(8+9)-VIII-4	4684	5.35	32.00	6.0	1.29	20.00	15	V	6.0
1350	(8+9)-IV-2	7905	9.03	32.00	3.5	2.18	20.00	9.2	V	3.5
1350	(8+9)-V-1	3811	4.35	32.00	7.4	1.05	20.00	19	V	7.4

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
1350	(8+9)-I-2	6774	7.74	32.00	4.1	1.87	20.00	11	V	4.1
1350	(8+9)-V-2	8552	9.77	32.00	3.3	2.36	20.00	8.5	V	3.3
1350	(8+9)-I-4	-2184	-2.49	32.00	13	-0.60	20.00	33	V	13
1350	(8+9)-V-3	-8702	-9.94	32.00	3.2	-2.41	20.00	8.3	V	3.2
1350	(8+9)-II-2	9169	10.47	32.00	3.1	2.53	20.00	7.9	V	3.1
1350	(8+9)-V-4	-3961	-4.52	32.00	7.1	-1.09	20.00	18	V	7.1
1350	(8+9)-II-4	6482	7.40	32.00	4.3	1.79	20.00	11	V	4.3
1350	(8+9)-VI-1	-6099	-6.97	32.00	4.6	-1.69	20.00	12	V	4.6
1350	(8+9)-III-2	6395	7.30	32.00	4.4	1.77	20.00	11	V	4.4
1350	(8+9)-VI-2	9702	11.08	32.00	2.9	2.68	20.00	7.5	V	2.9
1350	(8+9)-III-4	-2563	-2.93	32.00	11	-0.71	20.00	28	V	11
1350	(8+9)-VI-3	-9853	-11.25	32.00	2.8	-2.72	20.00	7.3	V	2.8
1350	(8+9)-I-1	2034	2.32	32.00	14	0.56	20.00	36	V	14
1350	(8+9)-VI-4	5949	6.79	32.00	4.7	1.64	20.00	12	V	4.7
1350	(8+9)-IV-4	5217	5.96	32.00	5.4	1.44	20.00	14	V	5.4
1350	(8+9)-VII-1	4191	4.79	32.00	6.7	1.16	20.00	17	V	6.7
1350	(8+9)-II-1	-6632	-7.57	32.00	4.2	-1.83	20.00	11	V	4.2
1350	(8+9)-VII-2	8172	9.33	32.00	3.4	2.26	20.00	8.9	V	3.4
1350	(8+9)-III-1	2413	2.76	32.00	12	0.67	20.00	30	V	12
1350	(8+9)-VII-3	-8322	-9.51	32.00	3.4	-2.30	20.00	8.7	V	3.4
1350	(8+9)-IV-1	-5367	-6.13	32.00	5.2	-1.48	20.00	13	V	5.2
1350	(8+9)-VII-4	-4341	-4.96	32.00	6.5	-1.20	20.00	17	V	6.5
1350	(8+9)-III-3	-6545	-7.48	32.00	4.3	-1.81	20.00	11	V	4.3
1350	(8+9)-IV-3	-8055	-9.20	32.00	3.5	-2.23	20.00	9.0	V	3.5
1350	(8+9)-II-3	-9319	-10.64	32.00	3.0	-2.58	20.00	7.8	V	3.0
1350	(8+9)-VIII-1	-4834	-5.52	32.00	5.8	-1.34	20.00	15	V	5.8
1350	(8+9)-VIII-2	8438	9.64	32.00	3.3	2.33	20.00	8.6	V	3.3
1350	(8+9)-VIII-3	-8588	-9.81	32.00	3.3	-2.37	20.00	8.4	V	3.3
1350	(8+9)-I-3	-6924	-7.91	32.00	4.0	-1.91	20.00	10	V	4.0

Setto 49: origine (1760.9,587.2,245.0), direzione (-0.199495,0.979899,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	1	127	-2	-39	0.35	-0.22	-1.29	79.20	115.20	115.20	57
0	2	162	-5	-67	0.45	-0.51	-2.24	118.80	172.80	172.80	51
0	3	162	-5	-67	0.45	-0.51	-2.24	118.80	172.80	172.80	51
0	4	127	-2	-39	0.35	-0.22	-1.29	105.60	153.60	153.60	76
0	5	127	-2	-39	0.35	-0.22	-1.29	105.60	153.60	153.60	76
0	6	127	-2	-39	0.35	-0.22	-1.29	105.60	153.60	153.60	76
0	7	127	-2	-39	0.35	-0.22	-1.29	105.60	153.60	153.60	76
0	(8+9)-VIII-4	-2817	135	-627	-7.77	14.02	-20.79	132.00	192.00	192.00	5.5
0	(8+9)-IV-1	3376	-148	643	9.31	-15.34	21.33	132.00	192.00	192.00	3.8
0	(8+9)-V-1	-2466	-166	-533	-6.81	-17.25	-17.68	132.00	192.00	192.00	5.5
0	(8+9)-I-2	-4197	-250	-896	-11.58	-25.92	-29.73	132.00	192.00	192.00	3.4
0	(8+9)-V-2	-5418	-217	-1125	-14.95	-22.52	-37.33	132.00	192.00	192.00	3.1
0	(8+9)-I-4	1438	196	252	3.97	20.36	8.35	132.00	192.00	192.00	5.6
0	(8+9)-V-3	5610	214	1073	15.48	22.22	35.59	132.00	192.00	192.00	2.4
0	(8+9)-II-2	-5668	-153	-1186	-15.64	-15.86	-39.32	132.00	192.00	192.00	3.4
0	(8+9)-V-4	2659	164	481	7.34	16.95	15.95	132.00	192.00	192.00	4.4
0	(8+9)-II-4	-3978	-19	-841	-10.98	-1.98	-27.90	132.00	192.00	192.00	6.3
0	(8+9)-VI-1	3804	26	720	10.50	2.70	23.88	132.00	192.00	192.00	4.6
0	(8+9)-III-2	-3959	-201	-853	-10.92	-20.81	-28.28	132.00	192.00	192.00	3.9
0	(8+9)-VI-2	-6035	-143	-1254	-16.65	-14.84	-41.60	132.00	192.00	192.00	3.3
0	(8+9)-III-4	1676	246	295	4.62	25.46	9.80	132.00	192.00	192.00	4.6
0	(8+9)-VI-3	6227	140	1202	17.18	14.54	39.86	132.00	192.00	192.00	2.4
0	(8+9)-IV-2	-4874	11	-1040	-13.45	1.15	-34.49	132.00	192.00	192.00	5.2
0	(8+9)-VI-4	-3612	-29	-772	-9.97	-3.00	-25.62	132.00	192.00	192.00	6.6
0	(8+9)-IV-4	-3184	145	-695	-8.78	15.04	-23.06	132.00	192.00	192.00	5.0
0	(8+9)-VII-1	-2705	-216	-577	-7.46	-22.36	-19.13	132.00	192.00	192.00	4.6
0	(8+9)-II-1	4170	16	789	11.51	1.68	26.16	132.00	192.00	192.00	4.3
0	(8+9)-VII-2	-5180	-168	-1082	-14.29	-17.41	-35.88	132.00	192.00	192.00	3.5
0	(8+9)-III-1	-1484	-249	-348	-4.09	-25.76	-11.53	132.00	192.00	192.00	5.1

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-VII-3	5372	165	1029	14.82	17.11	34.14	132.00	192.00	192.00	2.6
0	(8+9)-I-1	-1246	-199	-304	-3.44	-20.66	-10.08	132.00	192.00	192.00	6.2
0	(8+9)-VII-4	2897	213	525	7.99	22.06	17.40	132.00	192.00	192.00	3.8
0	(8+9)-III-3	4151	198	800	11.45	20.51	26.54	132.00	192.00	192.00	3.0
0	(8+9)-IV-3	5066	-14	988	13.98	-1.45	32.75	132.00	192.00	192.00	3.5
0	(8+9)-II-3	5860	150	1133	16.17	15.56	37.58	132.00	192.00	192.00	2.5
0	(8+9)-VIII-1	3009	-138	574	8.30	-14.32	19.05	132.00	192.00	192.00	4.2
0	(8+9)-VIII-2	-5240	21	-1109	-14.46	2.18	-36.77	132.00	192.00	192.00	4.8
0	(8+9)-VIII-3	5432	-24	1056	14.99	-2.48	35.03	132.00	192.00	192.00	3.2
0	(8+9)-I-3	4389	247	844	12.11	25.62	27.99	132.00	192.00	192.00	2.7
Verifiche nella direzione secondaria											
0	1	-1025	-1	44	-1.76	-0.09	0.38	79.20	115.20	115.20	>100
0	2	-1701	-2	86	-2.93	-0.17	0.74	118.80	172.80	172.80	>100
0	3	-1701	-2	86	-2.93	-0.17	0.74	118.80	172.80	172.80	>100
0	4	-1025	-1	44	-1.76	-0.09	0.38	105.60	153.60	153.60	>100
0	5	-1025	-1	44	-1.76	-0.09	0.38	105.60	153.60	153.60	>100
0	6	-1025	-1	44	-1.76	-0.09	0.38	105.60	153.60	153.60	>100
0	7	-1025	-1	44	-1.76	-0.09	0.38	105.60	153.60	153.60	>100
0	(8+9)-VIII-4	-483	-11	2648	-0.83	-1.12	22.80	132.00	192.00	192.00	8.0
0	(8+9)-IV-2	-475	-6	4348	-0.82	-0.58	37.43	132.00	192.00	192.00	5.1
0	(8+9)-V-1	-828	18	2007	-1.43	1.78	17.28	132.00	192.00	192.00	10
0	(8+9)-I-2	-554	-1	3712	-0.95	-0.11	31.96	132.00	192.00	192.00	6.0
0	(8+9)-V-2	-672	12	4592	-1.16	1.21	39.53	132.00	192.00	192.00	4.7
0	(8+9)-I-4	-699	-6	-1074	-1.20	-0.59	-9.25	132.00	192.00	192.00	19
0	(8+9)-V-3	-736	-14	-4538	-1.27	-1.33	-39.07	132.00	192.00	192.00	4.8
0	(8+9)-II-2	-424	-10	5052	-0.73	-0.94	43.49	132.00	192.00	192.00	4.3
0	(8+9)-V-4	-581	-19	-1954	-1.00	-1.91	-16.82	132.00	192.00	192.00	10
0	(8+9)-II-4	-467	-11	3616	-0.80	-1.09	31.13	132.00	192.00	192.00	6.0
0	(8+9)-VI-1	-977	14	-3299	-1.68	1.36	-28.40	132.00	192.00	192.00	6.4
0	(8+9)-III-2	-570	0	3501	-0.98	0.00	30.14	132.00	192.00	192.00	6.4
0	(8+9)-VI-2	-459	-6	5316	-0.79	-0.55	45.76	132.00	192.00	192.00	4.1
0	(8+9)-III-4	-714	-5	-1285	-1.23	-0.48	-11.06	132.00	192.00	192.00	17
0	(8+9)-VI-3	-950	4	-5263	-1.64	0.42	-45.30	132.00	192.00	192.00	4.2
0	(8+9)-I-1	-710	5	1127	-1.22	0.47	9.71	132.00	192.00	192.00	19
0	(8+9)-VI-4	-431	-15	3352	-0.74	-1.49	28.86	132.00	192.00	192.00	6.3
0	(8+9)-IV-4	-518	-7	2912	-0.89	-0.73	25.07	132.00	192.00	192.00	7.4
0	(8+9)-VII-1	-813	17	2218	-1.40	1.67	19.10	132.00	192.00	192.00	9.2
0	(8+9)-II-1	-942	10	-3563	-1.62	0.96	-30.67	132.00	192.00	192.00	6.1
0	(8+9)-VII-2	-688	13	4380	-1.18	1.32	37.71	132.00	192.00	192.00	4.9
0	(8+9)-III-1	-695	4	1339	-1.20	0.36	11.52	132.00	192.00	192.00	16
0	(8+9)-VII-3	-721	-15	-4327	-1.24	-1.44	-37.25	132.00	192.00	192.00	5.0
0	(8+9)-IV-1	-891	6	-2859	-1.53	0.60	-24.61	132.00	192.00	192.00	7.6
0	(8+9)-VII-4	-596	-18	-2165	-1.03	-1.80	-18.64	132.00	192.00	192.00	9.4
0	(8+9)-III-3	-839	-1	-3447	-1.44	-0.13	-29.68	132.00	192.00	192.00	6.4
0	(8+9)-IV-3	-934	5	-4294	-1.61	0.46	-36.97	132.00	192.00	192.00	5.1
0	(8+9)-II-3	-985	8	-4999	-1.70	0.82	-43.03	132.00	192.00	192.00	4.4
0	(8+9)-VIII-1	-926	10	-2595	-1.59	1.00	-22.34	132.00	192.00	192.00	8.2
0	(8+9)-VIII-2	-510	-2	4612	-0.88	-0.19	39.70	132.00	192.00	192.00	4.8
0	(8+9)-VIII-3	-899	1	-4558	-1.55	0.06	-39.24	132.00	192.00	192.00	4.9
0	(8+9)-I-3	-854	-0	-3658	-1.47	-0.02	-31.50	132.00	192.00	192.00	6.1

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
0	(8+9)-VIII-1	-16	0.03	6.40	Si	>100
0	(8+9)-VIII-4	20	0.04	6.40	Si	>100
1200	1	6	0.01	3.84	Si	>100
1200	2	12	0.02	5.76	Si	>100
1200	3	12	0.02	5.76	Si	>100
1200	4	6	0.01	5.12	Si	>100
1200	5	6	0.01	5.12	Si	>100
1200	6	6	0.01	5.12	Si	>100
1200	7	6	0.01	5.12	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
1200	(8+9)-VI-3	41	0.06	6.40	Si	>100
1200	(8+9)-VII-4	193	0.27	6.40	Si	24
1200	(8+9)-I-4	246	0.34	6.40	Si	19
1200	(8+9)-I-2	-223	0.31	6.40	Si	21
1200	(8+9)-II-2	-42	0.06	6.40	Si	>100
1200	(8+9)-VIII-2	-102	0.14	6.40	Si	45
1200	(8+9)-II-4	99	0.14	6.40	Si	46
1200	(8+9)-VIII-3	110	0.15	6.40	Si	42
1200	(8+9)-III-2	-244	0.34	6.40	Si	19
1200	(8+9)-I-1	-238	0.33	6.40	Si	19
1200	(8+9)-III-4	226	0.32	6.40	Si	20
1200	(8+9)-IV-1	-21	0.03	6.40	Si	>100
1200	(8+9)-I-3	232	0.32	6.40	Si	20
1200	(8+9)-IV-2	-111	0.16	6.40	Si	41
1200	(8+9)-VI-4	89	0.12	6.40	Si	51
1200	(8+9)-IV-4	29	0.04	6.40	Si	>100
1200	(8+9)-VII-1	-184	0.26	6.40	Si	25
1200	(8+9)-V-2	-190	0.27	6.40	Si	24
1200	(8+9)-VII-2	-211	0.29	6.40	Si	22
1200	(8+9)-V-4	213	0.30	6.40	Si	21
1200	(8+9)-VII-3	220	0.31	6.40	Si	21
1200	(8+9)-VI-2	-32	0.04	6.40	Si	>100
1200	(8+9)-II-1	-90	0.13	6.40	Si	51
1200	(8+9)-VI-1	-80	0.11	6.40	Si	57
1200	(8+9)-IV-3	120	0.17	6.40	Si	38
1200	(8+9)-V-3	199	0.28	6.40	Si	23
1200	(8+9)-II-3	51	0.07	6.40	Si	90
1200	(8+9)-III-1	-217	0.30	6.40	Si	21
1200	(8+9)-III-3	253	0.35	6.40	Si	18
1200	(8+9)-V-1	-205	0.29	6.40	Si	22
Verifiche nella direzione secondaria						
0	(8+9)-III-4	-222	0.35	6.40	Si	18
0	(8+9)-I-4	-247	0.39	6.40	Si	16
0	(8+9)-VIII-3	-79	0.13	6.40	Si	51
0	(8+9)-II-1	95	0.15	6.40	Si	42
0	(8+9)-VI-4	-49	0.08	6.40	Si	82
0	(8+9)-II-2	43	0.07	6.40	Si	94
0	(8+9)-IV-3	-129	0.21	6.40	Si	31
0	(8+9)-II-3	-47	0.08	6.40	Si	85
0	(8+9)-I-1	242	0.39	6.40	Si	17
0	(8+9)-II-4	-99	0.16	6.40	Si	41
0	(8+9)-I-3	-231	0.37	6.40	Si	17
0	(8+9)-VI-1	45	0.07	6.40	Si	90
0	(8+9)-IV-2	125	0.20	6.40	Si	32
0	(8+9)-I-2	227	0.36	6.40	Si	18
0	(8+9)-VIII-2	75	0.12	6.40	Si	54
0	(8+9)-III-1	218	0.35	6.40	Si	18
0	(8+9)-III-2	251	0.40	6.40	Si	16
0	(8+9)-III-3	-256	0.41	6.40	Si	16
359	1	-8	0.01	3.84	Si	>100
359	2	-12	0.02	5.76	Si	>100
359	3	-12	0.02	5.76	Si	>100
359	4	-8	0.01	5.12	Si	>100
359	5	-8	0.01	5.12	Si	>100
359	6	-8	0.01	5.12	Si	>100
359	7	-8	0.01	5.12	Si	>100
359	(8+9)-VIII-4	54	0.09	6.40	Si	75
359	(8+9)-VI-3	55	0.09	6.40	Si	73
359	(8+9)-IV-1	-32	0.05	6.40	Si	>100
359	(8+9)-VII-3	94	0.15	6.40	Si	43
359	(8+9)-V-4	94	0.15	6.40	Si	43
359	(8+9)-VII-4	110	0.18	6.40	Si	37
359	(8+9)-VII-1	-121	0.19	6.40	Si	33
359	(8+9)-VII-2	-105	0.17	6.40	Si	38

X	Comb.	Ty	τ_d	fvd	RS	Cs
359	(8+9)-VI-2	-66	0.10	6.40	Si	61
359	(8+9)-V-2	-121	0.19	6.40	Si	33
359	(8+9)-VIII-1	-64	0.10	6.40	Si	62
359	(8+9)-V-1	-104	0.17	6.40	Si	39
359	(8+9)-IV-4	22	0.03	6.40	Si	>100
359	(8+9)-V-3	111	0.18	6.40	Si	36

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	(8+9)-VIII-4	-1512	-6.26	32.00	5.1	-1.51	20.00	13	V	5.1
0	(8+9)-IV-1	1462	6.05	32.00	5.3	1.46	20.00	14	V	5.3
0	(8+9)-VI-4	-1898	-7.86	32.00	4.1	-1.90	20.00	11	V	4.1
0	(8+9)-III-2	-2059	-8.52	32.00	3.8	-2.06	20.00	9.7	V	3.8
0	(8+9)-IV-2	-2494	-10.32	32.00	3.1	-2.50	20.00	8.0	V	3.1
0	(8+9)-III-3	1840	7.62	32.00	4.2	1.84	20.00	11	V	4.2
0	(8+9)-VIII-2	-2662	-11.02	32.00	2.9	-2.67	20.00	7.5	V	2.9
0	(8+9)-VII-2	-2619	-10.84	32.00	3.0	-2.62	20.00	7.6	V	3.0
0	(8+9)-VII-4	1214	5.02	32.00	6.4	1.22	20.00	16	V	6.4
0	(8+9)-VII-1	-1432	-5.93	32.00	5.4	-1.43	20.00	14	V	5.4
0	(8+9)-I-2	-2175	-9.00	32.00	3.6	-2.18	20.00	9.2	V	3.6
0	(8+9)-VII-3	2401	9.94	32.00	3.2	2.40	20.00	8.3	V	3.2
0	(8+9)-IV-3	2276	9.42	32.00	3.4	2.28	20.00	8.8	V	3.4
0	(8+9)-II-2	-2880	-11.92	32.00	2.7	-2.88	20.00	6.9	V	2.7
0	(8+9)-IV-4	-1680	-6.96	32.00	4.6	-1.68	20.00	12	V	4.6
0	(8+9)-II-4	-2066	-8.55	32.00	3.7	-2.07	20.00	9.7	V	3.7
0	(8+9)-V-1	-1317	-5.45	32.00	5.9	-1.32	20.00	15	V	5.9
0	(8+9)-VIII-3	2444	10.11	32.00	3.2	2.45	20.00	8.2	V	3.2
0	(8+9)-V-2	-2735	-11.32	32.00	2.8	-2.74	20.00	7.3	V	2.8
0	(8+9)-I-1	-756	-3.13	32.00	10	-0.76	20.00	26	V	10
0	(8+9)-V-3	2516	10.42	32.00	3.1	2.52	20.00	7.9	V	3.1
0	(8+9)-II-1	1848	7.65	32.00	4.2	1.85	20.00	11	V	4.2
0	(8+9)-V-4	1098	4.54	32.00	7.0	1.10	20.00	18	V	7.0
0	(8+9)-III-1	-872	-3.61	32.00	8.9	-0.87	20.00	23	V	8.9
0	(8+9)-I-3	1956	8.10	32.00	4.0	1.96	20.00	10	V	4.0
0	(8+9)-II-3	2662	11.02	32.00	2.9	2.67	20.00	7.5	V	2.9
0	(8+9)-VIII-1	1294	5.35	32.00	6.0	1.30	20.00	15	V	6.0
0	(8+9)-VI-1	1680	6.95	32.00	4.6	1.68	20.00	12	V	4.6
0	(8+9)-VI-2	-3048	-12.62	32.00	2.5	-3.05	20.00	6.6	V	2.5
0	(8+9)-VI-3	2830	11.71	32.00	2.7	2.83	20.00	7.1	V	2.7
1200	1	413	1.19	19.20	16	0.29	12.00	42	V	16
1200	2	674	1.94	28.80	15	0.47	18.00	38	V	15
1200	3	674	1.94	28.80	15	0.47	18.00	38	V	15
1200	4	413	1.19	25.60	22	0.29	16.00	56	V	22
1200	5	413	1.19	25.60	22	0.29	16.00	56	V	22
1200	6	413	1.19	25.60	22	0.29	16.00	56	V	22
1200	7	413	1.19	25.60	22	0.29	16.00	56	V	22
1200	(8+9)-III-4	995	2.87	32.00	11	0.69	20.00	29	V	11
1200	(8+9)-I-4	876	2.52	32.00	13	0.61	20.00	33	V	13
Verifiche nella direzione secondaria										
0	(8+9)-VIII-4	3218	5.54	32.00	5.8	1.34	20.00	15	V	5.8
0	(8+9)-VII-2	5929	10.21	32.00	3.1	2.47	20.00	8.1	V	3.1
0	(8+9)-III-3	-4684	-8.06	32.00	4.0	-1.95	20.00	10	V	4.0
0	(8+9)-IV-2	5575	9.60	32.00	3.3	2.32	20.00	8.6	V	3.3
0	(8+9)-III-4	-1928	-3.32	32.00	9.6	-0.80	20.00	25	V	9.6
0	(8+9)-VIII-2	5953	10.25	32.00	3.1	2.48	20.00	8.1	V	3.1
0	(8+9)-IV-1	-3611	-6.22	32.00	5.1	-1.50	20.00	13	V	5.1
0	(8+9)-VII-4	-3188	-5.49	32.00	5.8	-1.33	20.00	15	V	5.8
0	(8+9)-I-1	1653	2.85	32.00	11	0.69	20.00	29	V	11
0	(8+9)-IV-3	-5590	-9.63	32.00	3.3	-2.33	20.00	8.6	V	3.3
0	(8+9)-I-3	-4943	-8.51	32.00	3.8	-2.06	20.00	9.7	V	3.8
0	(8+9)-IV-4	3596	6.19	32.00	5.2	1.50	20.00	13	V	5.2
0	(8+9)-II-1	-4476	-7.71	32.00	4.2	-1.87	20.00	11	V	4.2

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
0	(8+9)-V-1	2913	5.02	32.00	6.4	1.21	20.00	16	V	6.4
0	(8+9)-II-3	-6455	-11.11	32.00	2.9	-2.69	20.00	7.4	V	2.9
0	(8+9)-V-2	6188	10.65	32.00	3.0	2.58	20.00	7.8	V	3.0
0	(8+9)-III-1	1913	3.29	32.00	9.7	0.80	20.00	25	V	9.7
0	(8+9)-V-3	-6203	-10.68	32.00	3.0	-2.58	20.00	7.7	V	3.0
0	(8+9)-VIII-3	-5968	-10.28	32.00	3.1	-2.49	20.00	8.0	V	3.1
0	(8+9)-V-4	-2928	-5.04	32.00	6.3	-1.22	20.00	16	V	6.3
0	(8+9)-VII-3	-5944	-10.23	32.00	3.1	-2.48	20.00	8.1	V	3.1
0	(8+9)-VI-1	-4098	-7.06	32.00	4.5	-1.71	20.00	12	V	4.5
0	(8+9)-I-4	-1668	-2.87	32.00	11	-0.70	20.00	29	V	11
0	(8+9)-VI-2	6818	11.74	32.00	2.7	2.84	20.00	7.0	V	2.7
0	(8+9)-II-4	4461	7.68	32.00	4.2	1.86	20.00	11	V	4.2
0	(8+9)-VIII-1	-3233	-5.57	32.00	5.7	-1.35	20.00	15	V	5.7
0	(8+9)-I-2	4928	8.49	32.00	3.8	2.05	20.00	9.7	V	3.8
0	(8+9)-II-2	6440	11.09	32.00	2.9	2.68	20.00	7.5	V	2.9
0	(8+9)-III-2	4669	8.04	32.00	4.0	1.95	20.00	10	V	4.0
0	(8+9)-VI-3	-6833	-11.77	32.00	2.7	-2.85	20.00	7.0	V	2.7
0	(8+9)-VI-4	4083	7.03	32.00	4.6	1.70	20.00	12	V	4.6
0	(8+9)-VII-1	3173	5.46	32.00	5.9	1.32	20.00	15	V	5.9
359	1	-50	-0.09	19.20	>100	-0.02	12.00	>100	V	>100
359	2	-40	-0.07	28.80	>100	-0.02	18.00	>100	V	>100
359	3	-40	-0.07	28.80	>100	-0.02	18.00	>100	V	>100
359	4	-50	-0.09	25.60	>100	-0.02	16.00	>100	V	>100
359	5	-50	-0.09	25.60	>100	-0.02	16.00	>100	V	>100
359	6	-50	-0.09	25.60	>100	-0.02	16.00	>100	V	>100
359	7	-50	-0.09	25.60	>100	-0.02	16.00	>100	V	>100

Verifiche a instabilità

Setto(X)	Comb.	k _{critc}	k _{critm}	λ_{relc}	λ_{relm}	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
(cm)						kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	
47(40.0)	(8+9)-V-3	--	--	--	--	1.64	3.38	-5.71	132.00	192.00	192.00	17
48(180.9)	(8+9)-V-3	--	--	--	--	2.37	4.06	-7.48	132.00	192.00	192.00	13
49(0.0)	(8+9)-V-3	--	--	--	--	15.48	22.22	35.59	132.00	192.00	192.00	2.4

Parete Xlam 8 - Nodi: [11-32-2-3-33-34-112-111] - **Crit.Prog.** Criterio di verifica XLAM 0 - **Verificato:** [Cs=1.692,Comb=(8+9)-VI-3]

Geometria setti

Setto	Crit.	X	L	S	X90	L90	S90
		mm	cm	cm	mm	cm	cm
47	Criterio di verifica XLAM 0	0	291.7	12.1	0	40.0	12.1
		200	295.4	12.1	1495	40.0	12.1
		400	299.0	12.1	--	--	--
48	Criterio di verifica XLAM 0	0	237.0	12.1	0	180.9	12.1
		905	253.5	12.1	1350	180.9	12.1
		1809	269.9	12.1	--	--	--
49	Criterio di verifica XLAM 0	0	49.9	12.1	0	120.0	12.1
		600	60.8	12.1	359	120.0	12.1
		1200	71.7	12.1	--	--	--

Setto 47: origine (1737.0,704.8,145.9), direzione (-0.199495,0.979899,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	
200	2	-222	7	77	-0.10	0.11	0.07	118.80	172.80	172.80	>100
200	3	-222	7	77	-0.10	0.11	0.07	118.80	172.80	172.80	>100
400	1	-110	5	-18	-0.05	0.08	-0.02	79.20	115.20	115.20	>100

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
400	4	-110	5	-18	-0.05	0.08	-0.02	105.60	153.60	153.60	>100
400	5	-110	5	-18	-0.05	0.08	-0.02	105.60	153.60	153.60	>100
400	6	-110	5	-18	-0.05	0.08	-0.02	105.60	153.60	153.60	>100
400	7	-110	5	-18	-0.05	0.08	-0.02	105.60	153.60	153.60	>100
400	(8+9)-VIII-4	-2155	156	3420	-0.99	2.70	3.16	132.00	192.00	192.00	33
400	(8+9)-IV-1	2273	-156	-3869	1.05	-2.71	-3.58	132.00	192.00	192.00	25
400	(8+9)-V-1	-1702	-268	2769	-0.78	-4.63	2.56	132.00	192.00	192.00	27
400	(8+9)-I-2	-2857	-211	4781	-1.32	-3.66	4.42	132.00	192.00	192.00	24
400	(8+9)-V-2	-3705	-189	6130	-1.71	-3.27	5.67	132.00	192.00	192.00	21
400	(8+9)-I-4	718	296	-1464	0.33	5.12	-1.35	132.00	192.00	192.00	28
400	(8+9)-V-3	3569	195	-6173	1.64	3.38	-5.71	132.00	192.00	192.00	17
400	(8+9)-II-2	-3942	58	6516	-1.82	1.00	6.02	132.00	192.00	192.00	27
400	(8+9)-V-4	1566	274	-2813	0.72	4.74	-2.60	132.00	192.00	192.00	23
400	(8+9)-II-4	-2870	210	4642	-1.32	3.63	4.29	132.00	192.00	192.00	24
400	(8+9)-VI-1	2479	-197	-4281	1.14	-3.41	-3.96	132.00	192.00	192.00	21
400	(8+9)-III-2	-2719	-226	4536	-1.25	-3.90	4.19	132.00	192.00	192.00	24
400	(8+9)-VI-2	-4197	64	6920	-1.93	1.11	6.40	132.00	192.00	192.00	25
400	(8+9)-III-4	856	282	-1709	0.39	4.88	-1.58	132.00	192.00	192.00	27
400	(8+9)-VI-3	4060	-58	-6964	1.87	-1.01	-6.44	132.00	192.00	192.00	19
400	(8+9)-IV-2	-3482	10	5699	-1.60	0.18	5.27	132.00	192.00	192.00	35
400	(8+9)-VI-4	-2615	203	4238	-1.20	3.52	3.92	132.00	192.00	192.00	26
400	(8+9)-IV-4	-2410	163	3825	-1.11	2.81	3.54	132.00	192.00	192.00	30
400	(8+9)-VII-1	-1840	-253	3015	-0.85	-4.38	2.79	132.00	192.00	192.00	27
400	(8+9)-II-1	2734	-204	-4686	1.26	-3.53	-4.33	132.00	192.00	192.00	20
400	(8+9)-VII-2	-3567	-203	5885	-1.64	-3.52	5.44	132.00	192.00	192.00	21
400	(8+9)-III-1	-992	-276	1666	-0.46	-4.77	1.54	132.00	192.00	192.00	30
400	(8+9)-VII-3	3431	209	-5928	1.58	3.63	-5.48	132.00	192.00	192.00	17
400	(8+9)-I-1	-854	-290	1420	-0.39	-5.02	1.31	132.00	192.00	192.00	30
400	(8+9)-VII-4	1704	259	-3058	0.79	4.49	-2.83	132.00	192.00	192.00	23
400	(8+9)-III-3	2582	232	-4579	1.19	4.01	-4.23	132.00	192.00	192.00	19
400	(8+9)-IV-3	3346	-4	-5742	1.54	-0.07	-5.31	132.00	192.00	192.00	25
400	(8+9)-II-3	3806	-52	-6559	1.75	-0.89	-6.06	132.00	192.00	192.00	20
400	(8+9)-VIII-1	2019	-150	-3464	0.93	-2.59	-3.20	132.00	192.00	192.00	27
400	(8+9)-VIII-2	-3736	17	6103	-1.72	0.29	5.64	132.00	192.00	192.00	32
400	(8+9)-VIII-3	3600	-11	-6147	1.66	-0.19	-5.68	132.00	192.00	192.00	23
400	(8+9)-I-3	2720	217	-4825	1.25	3.76	-4.46	132.00	192.00	192.00	19
Verifiche nella direzione secondaria											
0	1	-590	-1	10	-3.05	-0.18	0.75	79.20	115.20	115.20	>100
0	2	-970	-1	16	-5.01	-0.42	1.25	118.80	172.80	172.80	95
0	3	-970	-1	16	-5.01	-0.42	1.25	118.80	172.80	172.80	95
0	4	-590	-1	10	-3.05	-0.18	0.75	105.60	153.60	153.60	>100
0	5	-590	-1	10	-3.05	-0.18	0.75	105.60	153.60	153.60	>100
0	6	-590	-1	10	-3.05	-0.18	0.75	105.60	153.60	153.60	>100
0	7	-590	-1	10	-3.05	-0.18	0.75	105.60	153.60	153.60	>100
0	(8+9)-VIII-4	-3665	2	415	-18.93	0.58	32.16	132.00	192.00	192.00	5.5
0	(8+9)-IV-2	-6218	-3	668	-32.12	-0.75	51.79	132.00	192.00	192.00	3.3
0	(8+9)-V-1	-3618	-8	313	-18.69	-2.23	24.25	132.00	192.00	192.00	6.8
0	(8+9)-I-2	-5705	-8	545	-29.47	-2.38	42.24	132.00	192.00	192.00	3.9
0	(8+9)-V-2	-6985	-8	712	-36.08	-2.24	55.17	132.00	192.00	192.00	3.0
0	(8+9)-I-4	1524	7	-133	7.87	2.18	-10.28	132.00	192.00	192.00	8.0
0	(8+9)-V-3	6170	7	-699	31.87	2.06	-54.13	132.00	192.00	192.00	1.9
0	(8+9)-II-2	-7103	-3	774	-36.69	-0.80	59.94	132.00	192.00	192.00	2.8
0	(8+9)-V-4	2804	7	-299	14.48	2.04	-23.20	132.00	192.00	192.00	4.1
0	(8+9)-II-4	-4934	2	570	-25.49	0.56	44.18	132.00	192.00	192.00	4.0
0	(8+9)-VI-1	3736	-2	-507	19.30	-0.70	-39.25	132.00	192.00	192.00	2.8
0	(8+9)-III-2	-5440	-8	514	-28.10	-2.36	39.80	132.00	192.00	192.00	4.1
0	(8+9)-VI-2	-7487	-3	824	-38.67	-0.76	63.81	132.00	192.00	192.00	2.7
0	(8+9)-III-4	1790	7	-164	9.24	2.19	-12.72	132.00	192.00	192.00	6.8
0	(8+9)-VI-3	6672	2	-810	34.47	0.58	-62.77	132.00	192.00	192.00	1.7
0	(8+9)-I-1	-2338	-8	146	-12.08	-2.36	11.32	132.00	192.00	192.00	13
0	(8+9)-VI-4	-4550	2	520	-23.50	0.52	40.30	132.00	192.00	192.00	4.4
0	(8+9)-IV-4	-4049	2	465	-20.91	0.62	36.04	132.00	192.00	192.00	4.9
0	(8+9)-VII-1	-3883	-8	345	-20.06	-2.24	26.69	132.00	192.00	192.00	6.2
0	(8+9)-II-1	4120	-3	-557	21.28	-0.74	-43.13	132.00	192.00	192.00	2.6

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-VII-2	-6719	-8	681	-34.71	-2.23	52.73	132.00	192.00	192.00	3.1
0	(8+9)-III-1	-2604	-8	178	-13.45	-2.37	13.77	132.00	192.00	192.00	11
0	(8+9)-VII-3	5905	7	-667	30.50	2.05	-51.68	132.00	192.00	192.00	2.0
0	(8+9)-IV-1	3235	-3	-452	16.71	-0.80	-34.99	132.00	192.00	192.00	3.2
0	(8+9)-VII-4	3069	7	-331	15.85	2.06	-25.65	132.00	192.00	192.00	3.8
0	(8+9)-III-3	4625	7	-500	23.89	2.18	-38.75	132.00	192.00	192.00	2.5
0	(8+9)-IV-3	5404	2	-655	27.91	0.57	-50.75	132.00	192.00	192.00	2.1
0	(8+9)-II-3	6289	2	-760	32.48	0.62	-58.89	132.00	192.00	192.00	1.8
0	(8+9)-VIII-1	2851	-3	-402	14.73	-0.76	-31.11	132.00	192.00	192.00	3.6
0	(8+9)-VIII-2	-6602	-2	719	-34.10	-0.71	55.67	132.00	192.00	192.00	3.1
0	(8+9)-VIII-3	5787	2	-705	29.89	0.53	-54.62	132.00	192.00	192.00	1.9
0	(8+9)-I-3	4891	7	-532	25.26	2.20	-41.20	132.00	192.00	192.00	2.4

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Ty kg	τ_d kg/cmq	fvd kg/cmq	RS	Cs
0	1	7	0.00	3.84	Si	>100
0	2	13	0.00	5.76	Si	>100
0	3	13	0.00	5.76	Si	>100
0	4	7	0.00	5.12	Si	>100
0	5	7	0.00	5.12	Si	>100
0	6	7	0.00	5.12	Si	>100
0	7	7	0.00	5.12	Si	>100
0	(8+9)-IV-2	-36	0.01	6.40	Si	>100
0	(8+9)-VIII-1	33	0.01	6.40	Si	>100
0	(8+9)-VI-1	76	0.03	6.40	Si	>100
0	(8+9)-IV-3	46	0.02	6.40	Si	>100
0	(8+9)-II-1	57	0.02	6.40	Si	>100
0	(8+9)-II-2	-79	0.03	6.40	Si	>100
0	(8+9)-II-3	89	0.03	6.40	Si	>100
0	(8+9)-II-4	-48	0.02	6.40	Si	>100
0	(8+9)-VI-4	-66	0.02	6.40	Si	>100
200	(8+9)-VIII-4	30	0.01	6.40	Si	>100
200	(8+9)-I-3	91	0.03	6.40	Si	>100
200	(8+9)-IV-4	29	0.01	6.40	Si	>100
200	(8+9)-III-2	-70	0.02	6.40	Si	>100
200	(8+9)-III-1	-70	0.02	6.40	Si	>100
200	(8+9)-I-4	68	0.02	6.40	Si	>100
200	(8+9)-III-4	80	0.03	6.40	Si	>100
200	(8+9)-I-1	-58	0.02	6.40	Si	>100
200	(8+9)-I-2	-82	0.03	6.40	Si	>100
200	(8+9)-III-3	79	0.03	6.40	Si	>100
400	(8+9)-IV-1	21	0.01	6.40	Si	>100
400	(8+9)-VI-2	-76	0.03	6.40	Si	>100
400	(8+9)-VII-3	125	0.04	6.40	Si	>100
400	(8+9)-V-4	108	0.04	6.40	Si	>100
400	(8+9)-VII-4	119	0.04	6.40	Si	>100
400	(8+9)-VII-1	-109	0.04	6.40	Si	>100
400	(8+9)-VII-2	-116	0.04	6.40	Si	>100
400	(8+9)-V-3	136	0.05	6.40	Si	>100
400	(8+9)-V-2	-126	0.04	6.40	Si	>100
400	(8+9)-V-1	-99	0.03	6.40	Si	>100
400	(8+9)-VIII-2	-42	0.01	6.40	Si	>100
400	(8+9)-VIII-3	51	0.02	6.40	Si	>100
400	(8+9)-VI-3	86	0.03	6.40	Si	>100
Verifiche nella direzione secondaria						
0	1	1	0.01	3.84	Si	>100
0	2	3	0.02	5.76	Si	>100
0	3	3	0.02	5.76	Si	>100
0	4	1	0.01	5.12	Si	>100
0	5	1	0.01	5.12	Si	>100
0	6	1	0.01	5.12	Si	>100
0	7	1	0.01	5.12	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
0	(8+9)-VIII-4	-8	0.04	6.40	Si	>100
0	(8+9)-I-1	14	0.07	6.40	Si	93
0	(8+9)-II-4	-9	0.04	6.40	Si	>100
0	(8+9)-III-1	14	0.07	6.40	Si	94
0	(8+9)-I-4	-13	0.06	6.40	Si	>100
0	(8+9)-VI-4	-9	0.04	6.40	Si	>100
0	(8+9)-VI-1	10	0.05	6.40	Si	>100
0	(8+9)-VIII-1	10	0.05	6.40	Si	>100
0	(8+9)-II-1	11	0.05	6.40	Si	>100
0	(8+9)-IV-1	10	0.05	6.40	Si	>100
0	(8+9)-IV-4	-9	0.04	6.40	Si	>100
0	(8+9)-III-4	-13	0.06	6.40	Si	>100
1495	(8+9)-IV-2	9	0.04	6.40	Si	>100
1495	(8+9)-V-1	15	0.07	6.40	Si	91
1495	(8+9)-I-2	12	0.06	6.40	Si	>100
1495	(8+9)-II-2	8	0.04	6.40	Si	>100
1495	(8+9)-IV-3	-9	0.04	6.40	Si	>100
1495	(8+9)-VII-1	14	0.07	6.40	Si	93
1495	(8+9)-III-2	12	0.06	6.40	Si	>100
1495	(8+9)-VII-2	18	0.09	6.40	Si	75
1495	(8+9)-V-3	-18	0.08	6.40	Si	76
1495	(8+9)-VII-3	-18	0.09	6.40	Si	75
1495	(8+9)-II-3	-8	0.04	6.40	Si	>100
1495	(8+9)-VII-4	-15	0.07	6.40	Si	92
1495	(8+9)-V-2	18	0.08	6.40	Si	77
1495	(8+9)-V-4	-15	0.07	6.40	Si	90
1495	(8+9)-VI-2	9	0.04	6.40	Si	>100
1495	(8+9)-III-3	-13	0.06	6.40	Si	>100
1495	(8+9)-I-3	-12	0.06	6.40	Si	>100
1495	(8+9)-VIII-2	11	0.05	6.40	Si	>100
1495	(8+9)-VIII-3	-11	0.05	6.40	Si	>100
1495	(8+9)-VI-3	-10	0.05	6.40	Si	>100

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	(8+9)-II-2	-7849	-5.56	32.00	5.8	-1.35	20.00	15	V	5.8
0	(8+9)-VIII-4	-4004	-2.84	32.00	11	-0.69	20.00	29	V	11
0	(8+9)-III-3	5490	3.89	32.00	8.2	0.94	20.00	21	V	8.2
0	(8+9)-I-4	1731	1.23	32.00	26	0.30	20.00	67	V	26
0	(8+9)-II-3	8000	5.67	32.00	5.6	1.37	20.00	15	V	5.6
0	(8+9)-III-4	2061	1.46	32.00	22	0.35	20.00	57	V	22
0	(8+9)-IV-2	-6750	-4.78	32.00	6.7	-1.16	20.00	17	V	6.7
0	(8+9)-VIII-2	-7276	-5.15	32.00	6.2	-1.25	20.00	16	V	6.2
0	(8+9)-VI-2	-8375	-5.93	32.00	5.4	-1.44	20.00	14	V	5.4
0	(8+9)-I-2	-5669	-4.01	32.00	8.0	-0.97	20.00	21	V	8.0
0	(8+9)-VII-2	-7093	-5.02	32.00	6.4	-1.22	20.00	16	V	6.4
0	(8+9)-VI-4	-5103	-3.61	32.00	8.9	-0.87	20.00	23	V	8.9
0	(8+9)-I-1	-1580	-1.12	32.00	29	-0.27	20.00	74	V	29
0	(8+9)-I-3	5820	4.12	32.00	7.8	1.00	20.00	20	V	7.8
0	(8+9)-II-4	-5629	-3.99	32.00	8.0	-0.96	20.00	21	V	8.0
0	(8+9)-III-1	-1910	-1.35	32.00	24	-0.33	20.00	61	V	24
0	(8+9)-III-2	-5339	-3.78	32.00	8.5	-0.92	20.00	22	V	8.5
200	(8+9)-V-1	-3443	-2.41	32.00	13	-0.58	20.00	34	V	13
200	(8+9)-V-4	3621	2.53	32.00	13	0.61	20.00	33	V	13
200	(8+9)-VII-4	3965	2.77	32.00	12	0.67	20.00	30	V	12
200	(8+9)-VII-1	-3787	-2.65	32.00	12	-0.64	20.00	31	V	12
200	(8+9)-V-3	7702	5.39	32.00	5.9	1.30	20.00	15	V	5.9
200	(8+9)-V-2	-7524	-5.26	32.00	6.1	-1.27	20.00	16	V	6.1
400	1	178	0.12	19.20	>100	0.03	12.00	>100	V	>100
400	2	248	0.17	28.80	>100	0.04	18.00	>100	V	>100
400	3	248	0.17	28.80	>100	0.04	18.00	>100	V	>100
400	4	178	0.12	25.60	>100	0.03	16.00	>100	V	>100

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
400	5	178	0.12	25.60	>100	0.03	16.00	>100	V	>100
400	6	178	0.12	25.60	>100	0.03	16.00	>100	V	>100
400	7	178	0.12	25.60	>100	0.03	16.00	>100	V	>100
400	(8+9)-IV-1	4907	3.39	32.00	9.4	0.82	20.00	24	V	9.4
400	(8+9)-VI-3	8745	6.04	32.00	5.3	1.46	20.00	14	V	5.3
400	(8+9)-VI-1	5402	3.73	32.00	8.6	0.90	20.00	22	V	8.6
400	(8+9)-VII-3	7467	5.16	32.00	6.2	1.25	20.00	16	V	6.2
400	(8+9)-II-1	5967	4.12	32.00	7.8	1.00	20.00	20	V	7.8
400	(8+9)-VIII-1	4343	3.00	32.00	11	0.73	20.00	28	V	11
400	(8+9)-IV-3	7121	4.92	32.00	6.5	1.19	20.00	17	V	6.5
400	(8+9)-VIII-3	7686	5.31	32.00	6.0	1.29	20.00	16	V	6.0
400	(8+9)-IV-4	-4648	-3.21	32.00	10.0	-0.78	20.00	26	V	10.0
Verifiche nella direzione secondaria										
0	1	17	0.09	19.20	>100	0.02	12.00	>100	V	>100
0	2	30	0.16	28.80	>100	0.04	18.00	>100	V	>100
0	3	30	0.16	28.80	>100	0.04	18.00	>100	V	>100
0	4	17	0.09	25.60	>100	0.02	16.00	>100	V	>100
0	5	17	0.09	25.60	>100	0.02	16.00	>100	V	>100
0	6	17	0.09	25.60	>100	0.02	16.00	>100	V	>100
0	7	17	0.09	25.60	>100	0.02	16.00	>100	V	>100
1495	(8+9)-VIII-4	820	4.24	32.00	7.6	1.03	20.00	20	V	7.6
1495	(8+9)-IV-2	1372	7.09	32.00	4.5	1.71	20.00	12	V	4.5
1495	(8+9)-V-1	669	3.46	32.00	9.3	0.84	20.00	24	V	9.3
1495	(8+9)-I-2	1178	6.08	32.00	5.3	1.47	20.00	14	V	5.3
1495	(8+9)-V-2	1479	7.64	32.00	4.2	1.85	20.00	11	V	4.2
1495	(8+9)-I-4	-359	-1.86	32.00	17	-0.45	20.00	45	V	17
1495	(8+9)-V-3	-1471	-7.60	32.00	4.2	-1.84	20.00	11	V	4.2
1495	(8+9)-II-2	1585	8.19	32.00	3.9	1.98	20.00	10	V	3.9
1495	(8+9)-V-4	-661	-3.41	32.00	9.4	-0.83	20.00	24	V	9.4
1495	(8+9)-II-4	1124	5.80	32.00	5.5	1.40	20.00	14	V	5.5
1495	(8+9)-VI-1	-1025	-5.30	32.00	6.0	-1.28	20.00	16	V	6.0
1495	(8+9)-III-2	1114	5.75	32.00	5.6	1.39	20.00	14	V	5.6
1495	(8+9)-VI-2	1675	8.65	32.00	3.7	2.09	20.00	9.5	V	3.7
1495	(8+9)-III-4	-423	-2.19	32.00	15	-0.53	20.00	38	V	15
1495	(8+9)-VI-3	-1667	-8.61	32.00	3.7	-2.08	20.00	9.6	V	3.7
1495	(8+9)-I-1	368	1.90	32.00	17	0.46	20.00	43	V	17
1495	(8+9)-VI-4	1033	5.34	32.00	6.0	1.29	20.00	15	V	6.0
1495	(8+9)-IV-4	911	4.70	32.00	6.8	1.14	20.00	18	V	6.8
1495	(8+9)-VII-1	733	3.79	32.00	8.5	0.92	20.00	22	V	8.5
1495	(8+9)-II-1	-1116	-5.76	32.00	5.6	-1.39	20.00	14	V	5.6
1495	(8+9)-VII-2	1415	7.31	32.00	4.4	1.77	20.00	11	V	4.4
1495	(8+9)-III-1	432	2.23	32.00	14	0.54	20.00	37	V	14
1495	(8+9)-VII-3	-1407	-7.27	32.00	4.4	-1.76	20.00	11	V	4.4
1495	(8+9)-IV-1	-902	-4.66	32.00	6.9	-1.13	20.00	18	V	6.9
1495	(8+9)-VII-4	-725	-3.74	32.00	8.5	-0.91	20.00	22	V	8.5
1495	(8+9)-III-3	-1106	-5.71	32.00	5.6	-1.38	20.00	14	V	5.6
1495	(8+9)-IV-3	-1363	-7.04	32.00	4.5	-1.70	20.00	12	V	4.5
1495	(8+9)-II-3	-1577	-8.14	32.00	3.9	-1.97	20.00	10	V	3.9
1495	(8+9)-VIII-1	-812	-4.19	32.00	7.6	-1.01	20.00	20	V	7.6
1495	(8+9)-VIII-2	1462	7.55	32.00	4.2	1.83	20.00	11	V	4.2
1495	(8+9)-VIII-3	-1454	-7.51	32.00	4.3	-1.82	20.00	11	V	4.3
1495	(8+9)-I-3	-1170	-6.04	32.00	5.3	-1.46	20.00	14	V	5.3

Setto 48: origine (1797,0,410,0,118.5), direzione (-0.199495,0.979899,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	1	24	-10	111	0.01	-0.22	0.16	79.20	115.20	115.20	>100
0	2	32	-20	94	0.02	-0.43	0.14	118.80	172.80	172.80	>100
0	3	32	-20	94	0.02	-0.43	0.14	118.80	172.80	172.80	>100
0	4	24	-10	111	0.01	-0.22	0.16	105.60	153.60	153.60	>100
0	5	24	-10	111	0.01	-0.22	0.16	105.60	153.60	153.60	>100
0	6	24	-10	111	0.01	-0.22	0.16	105.60	153.60	153.60	>100

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	7	24	-10	111	0.01	-0.22	0.16	105.60	153.60	153.60	>100
0	(8+9)-I-1	162	-217	-803	0.09	-4.74	-1.18	132.00	192.00	192.00	32
0	(8+9)-IV-2	220	-128	-2909	0.13	-2.79	-4.28	132.00	192.00	192.00	26
1809	(8+9)-VIII-4	-2252	135	3316	-1.15	2.59	3.76	132.00	192.00	192.00	30
1809	(8+9)-IV-1	2797	-143	-3983	1.43	-2.74	-4.52	132.00	192.00	192.00	21
1809	(8+9)-V-2	-4404	-215	6355	-2.25	-4.12	7.21	132.00	192.00	192.00	17
1809	(8+9)-I-4	1200	177	-1698	0.61	3.40	-1.93	132.00	192.00	192.00	31
1809	(8+9)-V-3	4641	212	-6594	2.37	4.06	-7.48	132.00	192.00	192.00	13
1809	(8+9)-II-2	-4586	-149	6663	-2.34	-2.85	7.56	132.00	192.00	192.00	18
1809	(8+9)-V-4	2230	160	-3121	1.14	3.08	-3.54	132.00	192.00	192.00	23
1809	(8+9)-II-4	-3214	-26	4674	-1.64	-0.50	5.30	132.00	192.00	192.00	33
1809	(8+9)-VI-1	3141	28	-4487	1.60	0.54	-5.09	132.00	192.00	192.00	24
1809	(8+9)-III-2	-3179	-182	4652	-1.62	-3.49	5.28	132.00	192.00	192.00	22
1809	(8+9)-VI-2	-4895	-144	7090	-2.50	-2.76	8.04	132.00	192.00	192.00	18
1809	(8+9)-III-4	1396	227	-1977	0.71	4.36	-2.24	132.00	192.00	192.00	25
1809	(8+9)-VI-3	5131	141	-7330	2.62	2.70	-8.32	132.00	192.00	192.00	13
1809	(8+9)-I-2	-3375	-232	4931	-1.72	-4.44	5.60	132.00	192.00	192.00	19
1809	(8+9)-VI-4	-2905	-31	4247	-1.48	-0.60	4.82	132.00	192.00	192.00	35
1809	(8+9)-IV-4	-2561	140	3743	-1.31	2.68	4.25	132.00	192.00	192.00	28
1809	(8+9)-VII-1	-2189	-213	3161	-1.12	-4.09	3.59	132.00	192.00	192.00	25
1809	(8+9)-II-1	3450	23	-4914	1.76	0.44	-5.58	132.00	192.00	192.00	22
1809	(8+9)-VII-2	-4208	-165	6075	-2.15	-3.16	6.89	132.00	192.00	192.00	19
1809	(8+9)-III-1	-1160	-230	1737	-0.59	-4.41	1.97	132.00	192.00	192.00	30
1809	(8+9)-VII-3	4445	162	-6315	2.27	3.11	-7.17	132.00	192.00	192.00	14
1809	(8+9)-I-3	3611	229	-5171	1.84	4.39	-5.87	132.00	192.00	192.00	15
1809	(8+9)-VII-4	2426	210	-3401	1.24	4.03	-3.86	132.00	192.00	192.00	20
1809	(8+9)-III-3	3415	179	-4892	1.74	3.43	-5.55	132.00	192.00	192.00	17
1809	(8+9)-IV-3	4170	-20	-5972	2.13	-0.39	-6.78	132.00	192.00	192.00	19
1809	(8+9)-II-3	4823	146	-6903	2.46	2.80	-7.83	132.00	192.00	192.00	14
1809	(8+9)-VIII-1	2488	-138	-3556	1.27	-2.64	-4.04	132.00	192.00	192.00	23
1809	(8+9)-VIII-2	-4242	22	6159	-2.17	0.43	6.99	132.00	192.00	192.00	26
1809	(8+9)-VIII-3	4479	-25	-6399	2.29	-0.48	-7.26	132.00	192.00	192.00	17
1809	(8+9)-V-1	-1993	-163	2882	-1.02	-3.13	3.27	132.00	192.00	192.00	30
Verifiche nella direzione secondaria											
0	1	-1367	5	-350	-1.56	0.31	-1.33	79.20	115.20	115.20	69
0	4	-1367	5	-350	-1.56	0.31	-1.33	105.60	153.60	153.60	93
0	5	-1367	5	-350	-1.56	0.31	-1.33	105.60	153.60	153.60	93
0	6	-1367	5	-350	-1.56	0.31	-1.33	105.60	153.60	153.60	93
0	7	-1367	5	-350	-1.56	0.31	-1.33	105.60	153.60	153.60	93
0	(8+9)-VIII-4	944	-9	5743	1.08	-0.56	21.76	132.00	192.00	192.00	8.0
0	(8+9)-IV-2	2181	-20	9779	2.49	-1.30	37.04	132.00	192.00	192.00	4.6
0	(8+9)-V-1	477	-8	4578	0.54	-0.52	17.34	132.00	192.00	192.00	10
0	(8+9)-I-1	-141	1	2324	-0.16	0.04	8.80	132.00	192.00	192.00	22
0	(8+9)-V-2	2323	-31	10586	2.65	-2.03	40.10	132.00	192.00	192.00	4.2
0	(8+9)-I-3	-3648	30	-8874	-4.17	1.95	-33.62	132.00	192.00	192.00	5.4
0	(8+9)-V-3	-4266	38	-11128	-4.87	2.51	-42.16	132.00	192.00	192.00	4.3
0	(8+9)-II-1	-3523	38	-8605	-4.02	2.47	-32.60	132.00	192.00	192.00	5.5
0	(8+9)-V-4	-2420	15	-5120	-2.76	1.00	-19.40	132.00	192.00	192.00	9.4
0	(8+9)-II-3	-4575	47	-11964	-5.23	3.04	-45.32	132.00	192.00	192.00	4.0
0	(8+9)-VI-1	-3337	35	-7929	-3.81	2.30	-30.04	132.00	192.00	192.00	5.9
0	(8+9)-III-1	-6	-5	2817	-0.01	-0.34	10.67	132.00	192.00	192.00	17
0	(8+9)-VI-2	2817	-42	12099	3.22	-2.74	45.83	132.00	192.00	192.00	3.6
0	(8+9)-III-3	-3513	24	-8381	-4.01	1.57	-31.75	132.00	192.00	192.00	5.7
0	(8+9)-VI-3	-4760	49	-12641	-5.44	3.21	-47.89	132.00	192.00	192.00	3.7
0	(8+9)-IV-1	-3073	18	-6962	-3.51	1.20	-26.37	132.00	192.00	192.00	6.9
0	(8+9)-VI-4	1394	-28	7387	1.59	-1.83	27.98	132.00	192.00	192.00	6.0
0	(8+9)-IV-3	-4125	27	-10321	-4.71	1.77	-39.10	132.00	192.00	192.00	4.7
0	(8+9)-VII-1	612	-14	5071	0.70	-0.90	19.21	132.00	192.00	192.00	9.1
0	(8+9)-I-2	1705	-23	8332	1.95	-1.47	31.56	132.00	192.00	192.00	5.4
0	(8+9)-VII-2	2188	-25	10093	2.50	-1.65	38.24	132.00	192.00	192.00	4.4
0	(8+9)-II-2	2631	-39	11422	3.01	-2.57	43.27	132.00	192.00	192.00	3.8
0	(8+9)-VII-3	-4131	33	-10635	-4.72	2.13	-40.29	132.00	192.00	192.00	4.5
0	(8+9)-III-2	1570	-17	7839	1.79	-1.09	29.70	132.00	192.00	192.00	5.7
0	(8+9)-VIII-3	-4310	30	-10997	-4.92	1.94	-41.66	132.00	192.00	192.00	4.4

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-III-4	-1937	12	-3359	-2.21	0.82	-12.72	132.00	192.00	192.00	14
0	(8+9)-I-4	-1802	7	-2866	-2.06	0.43	-10.86	132.00	192.00	192.00	17
0	(8+9)-II-4	1579	-31	8063	1.80	-2.00	30.54	132.00	192.00	192.00	5.5
0	(8+9)-IV-4	1129	-11	6420	1.29	-0.73	24.32	132.00	192.00	192.00	7.1
0	(8+9)-VII-4	-2555	21	-5613	-2.92	1.38	-21.26	132.00	192.00	192.00	8.5
0	(8+9)-VIII-1	-2887	16	-6285	-3.30	1.03	-23.81	132.00	192.00	192.00	7.7
0	(8+9)-VIII-2	2366	-22	10455	2.70	-1.47	39.61	132.00	192.00	192.00	4.3
1350	2	-1782	1	-496	-2.03	0.07	-1.88	118.80	172.80	172.80	88
1350	3	-1782	1	-496	-2.03	0.07	-1.88	118.80	172.80	172.80	88

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Ty kg	τ_d kg/cmq	fvd kg/cmq	RS	Cs
0	(8+9)-VII-1	-59	0.02	6.40	Si	>100
0	(8+9)-III-2	-49	0.02	6.40	Si	>100
0	(8+9)-IV-1	43	0.02	6.40	Si	>100
0	(8+9)-III-3	52	0.02	6.40	Si	>100
0	(8+9)-VIII-2	-73	0.03	6.40	Si	>100
0	(8+9)-III-4	21	0.01	6.40	Si	>100
0	(8+9)-VII-4	63	0.03	6.40	Si	>100
0	(8+9)-VII-2	-90	0.04	6.40	Si	>100
0	(8+9)-IV-2	-61	0.03	6.40	Si	>100
0	(8+9)-I-2	-52	0.02	6.40	Si	>100
0	(8+9)-IV-3	64	0.03	6.40	Si	>100
0	(8+9)-I-4	18	0.01	6.40	Si	>100
0	(8+9)-IV-4	-40	0.02	6.40	Si	>100
0	(8+9)-II-2	-70	0.03	6.40	Si	>100
0	(8+9)-V-1	-56	0.02	6.40	Si	>100
0	(8+9)-II-4	-50	0.02	6.40	Si	>100
0	(8+9)-V-2	-93	0.04	6.40	Si	>100
0	(8+9)-VIII-3	77	0.03	6.40	Si	>100
0	(8+9)-V-3	97	0.04	6.40	Si	>100
0	(8+9)-VII-3	94	0.04	6.40	Si	>100
0	(8+9)-V-4	60	0.03	6.40	Si	>100
0	(8+9)-I-3	55	0.02	6.40	Si	>100
0	(8+9)-VI-1	41	0.02	6.40	Si	>100
0	(8+9)-II-3	74	0.03	6.40	Si	>100
0	(8+9)-VIII-1	31	0.01	6.40	Si	>100
0	(8+9)-I-1	-14	0.01	6.40	Si	>100
0	(8+9)-II-1	53	0.02	6.40	Si	>100
0	(8+9)-III-1	-17	0.01	6.40	Si	>100
0	(8+9)-VI-2	-83	0.04	6.40	Si	>100
0	(8+9)-VI-3	86	0.04	6.40	Si	>100
0	(8+9)-VI-4	-37	0.02	6.40	Si	>100
905	1	5	0.00	3.84	Si	>100
905	2	10	0.00	5.76	Si	>100
905	3	10	0.00	5.76	Si	>100
905	4	5	0.00	5.12	Si	>100
905	5	5	0.00	5.12	Si	>100
905	6	5	0.00	5.12	Si	>100
905	7	5	0.00	5.12	Si	>100
905	(8+9)-VIII-4	35	0.01	6.40	Si	>100
Verifiche nella direzione secondaria						
0	1	-5	0.01	3.84	Si	>100
0	2	-6	0.01	5.76	Si	>100
0	3	-6	0.01	5.76	Si	>100
0	4	-5	0.01	5.12	Si	>100
0	5	-5	0.01	5.12	Si	>100
0	6	-5	0.01	5.12	Si	>100
0	7	-5	0.01	5.12	Si	>100
0	(8+9)-V-1	27	0.03	6.40	Si	>100
0	(8+9)-VI-3	-65	0.07	6.40	Si	93
0	(8+9)-VI-2	57	0.06	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
0	(8+9)-VII-3	-59	0.06	6.40	Si	>100
0	(8+9)-VI-1	-38	0.04	6.40	Si	>100
0	(8+9)-VII-1	33	0.03	6.40	Si	>100
0	(8+9)-V-4	-36	0.04	6.40	Si	>100
0	(8+9)-VII-4	-41	0.04	6.40	Si	>100
0	(8+9)-III-4	-15	0.02	6.40	Si	>100
0	(8+9)-II-1	-46	0.05	6.40	Si	>100
0	(8+9)-II-3	-58	0.06	6.40	Si	>100
0	(8+9)-VII-2	50	0.05	6.40	Si	>100
0	(8+9)-V-3	-64	0.07	6.40	Si	95
0	(8+9)-II-4	37	0.04	6.40	Si	>100
0	(8+9)-V-2	56	0.06	6.40	Si	>100
1350	(8+9)-VIII-4	-35	0.04	6.40	Si	>100
1350	(8+9)-IV-2	-50	0.05	6.40	Si	>100
1350	(8+9)-I-4	14	0.01	6.40	Si	>100
1350	(8+9)-IV-4	-34	0.04	6.40	Si	>100
1350	(8+9)-I-3	39	0.04	6.40	Si	>100
1350	(8+9)-IV-1	35	0.04	6.40	Si	>100
1350	(8+9)-I-2	-38	0.04	6.40	Si	>100
1350	(8+9)-III-2	-38	0.04	6.40	Si	>100
1350	(8+9)-I-1	-13	0.01	6.40	Si	>100
1350	(8+9)-IV-3	50	0.05	6.40	Si	>100
1350	(8+9)-III-3	39	0.04	6.40	Si	>100
1350	(8+9)-III-1	-13	0.01	6.40	Si	>100
1350	(8+9)-VI-4	-35	0.04	6.40	Si	>100
1350	(8+9)-VIII-1	36	0.04	6.40	Si	>100
1350	(8+9)-VIII-2	-48	0.05	6.40	Si	>100
1350	(8+9)-VIII-3	49	0.05	6.40	Si	>100
1350	(8+9)-II-2	-49	0.05	6.40	Si	>100

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
905	1	390	0.32	19.20	60	0.08	12.00	>100	V	60
905	2	422	0.34	28.80	84	0.08	18.00	>100	V	84
905	3	422	0.34	28.80	84	0.08	18.00	>100	V	84
905	4	390	0.32	25.60	81	0.08	16.00	>100	V	81
905	5	390	0.32	25.60	81	0.08	16.00	>100	V	81
905	6	390	0.32	25.60	81	0.08	16.00	>100	V	81
905	7	390	0.32	25.60	81	0.08	16.00	>100	V	81
905	(8+9)-VIII-4	-6110	-4.98	32.00	6.4	-1.21	20.00	17	V	6.4
905	(8+9)-IV-1	7442	6.07	32.00	5.3	1.47	20.00	14	V	5.3
905	(8+9)-V-1	-4913	-4.01	32.00	8.0	-0.97	20.00	21	V	8.0
905	(8+9)-I-2	-8890	-7.25	32.00	4.4	-1.75	20.00	11	V	4.4
905	(8+9)-V-2	-11308	-9.22	32.00	3.5	-2.23	20.00	9.0	V	3.5
905	(8+9)-I-4	3101	2.53	32.00	13	0.61	20.00	33	V	13
905	(8+9)-V-3	11915	9.71	32.00	3.3	2.35	20.00	8.5	V	3.3
905	(8+9)-II-2	-12154	-9.91	32.00	3.2	-2.40	20.00	8.3	V	3.2
905	(8+9)-V-4	5520	4.50	32.00	7.1	1.09	20.00	18	V	7.1
905	(8+9)-II-4	-8557	-6.98	32.00	4.6	-1.69	20.00	12	V	4.6
905	(8+9)-VI-1	8438	6.88	32.00	4.7	1.66	20.00	12	V	4.7
905	(8+9)-III-2	-8373	-6.83	32.00	4.7	-1.65	20.00	12	V	4.7
905	(8+9)-VI-2	-12880	-10.50	32.00	3.0	-2.54	20.00	7.9	V	3.0
905	(8+9)-III-4	3618	2.95	32.00	11	0.71	20.00	28	V	11
905	(8+9)-VI-3	13487	10.99	32.00	2.9	2.66	20.00	7.5	V	2.9
905	(8+9)-IV-2	-10433	-8.50	32.00	3.8	-2.06	20.00	9.7	V	3.8
905	(8+9)-VI-4	-7832	-6.38	32.00	5.0	-1.54	20.00	13	V	5.0
905	(8+9)-IV-4	-6836	-5.57	32.00	5.7	-1.35	20.00	15	V	5.7
905	(8+9)-VII-1	-5430	-4.43	32.00	7.2	-1.07	20.00	19	V	7.2
905	(8+9)-II-1	9164	7.47	32.00	4.3	1.81	20.00	11	V	4.3
905	(8+9)-VII-2	-10792	-8.80	32.00	3.6	-2.13	20.00	9.4	V	3.6
905	(8+9)-III-1	-3011	-2.45	32.00	13	-0.59	20.00	34	V	13
905	(8+9)-VII-3	11399	9.29	32.00	3.4	2.25	20.00	8.9	V	3.4

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
905	(8+9)-I-1	-2494	-2.03	32.00	16	-0.49	20.00	41	V	16
905	(8+9)-VII-4	6036	4.92	32.00	6.5	1.19	20.00	17	V	6.5
905	(8+9)-III-3	8980	7.32	32.00	4.4	1.77	20.00	11	V	4.4
905	(8+9)-IV-3	11039	9.00	32.00	3.6	2.18	20.00	9.2	V	3.6
905	(8+9)-II-3	12761	10.40	32.00	3.1	2.52	20.00	7.9	V	3.1
905	(8+9)-VIII-1	6717	5.48	32.00	5.8	1.33	20.00	15	V	5.8
905	(8+9)-VIII-2	-11158	-9.10	32.00	3.5	-2.20	20.00	9.1	V	3.5
905	(8+9)-VIII-3	11765	9.59	32.00	3.3	2.32	20.00	8.6	V	3.3
905	(8+9)-I-3	9496	7.74	32.00	4.1	1.87	20.00	11	V	4.1
Verifiche nella direzione secondaria										
1350	1	-79	-0.09	19.20	>100	-0.02	12.00	>100	V	>100
1350	2	-7	-0.01	28.80	>100	-0.00	18.00	>100	V	>100
1350	3	-7	-0.01	28.80	>100	-0.00	18.00	>100	V	>100
1350	4	-79	-0.09	25.60	>100	-0.02	16.00	>100	V	>100
1350	5	-79	-0.09	25.60	>100	-0.02	16.00	>100	V	>100
1350	6	-79	-0.09	25.60	>100	-0.02	16.00	>100	V	>100
1350	7	-79	-0.09	25.60	>100	-0.02	16.00	>100	V	>100
1350	(8+9)-VIII-4	4684	5.35	32.00	6.0	1.29	20.00	15	V	6.0
1350	(8+9)-IV-2	7905	9.03	32.00	3.5	2.18	20.00	9.2	V	3.5
1350	(8+9)-V-1	3811	4.35	32.00	7.4	1.05	20.00	19	V	7.4
1350	(8+9)-I-2	6774	7.74	32.00	4.1	1.87	20.00	11	V	4.1
1350	(8+9)-V-2	8552	9.77	32.00	3.3	2.36	20.00	8.5	V	3.3
1350	(8+9)-I-4	-2184	-2.49	32.00	13	-0.60	20.00	33	V	13
1350	(8+9)-V-3	-8702	-9.94	32.00	3.2	-2.41	20.00	8.3	V	3.2
1350	(8+9)-II-2	9169	10.47	32.00	3.1	2.53	20.00	7.9	V	3.1
1350	(8+9)-V-4	-3961	-4.52	32.00	7.1	-1.09	20.00	18	V	7.1
1350	(8+9)-II-4	6482	7.40	32.00	4.3	1.79	20.00	11	V	4.3
1350	(8+9)-VI-1	-6099	-6.97	32.00	4.6	-1.69	20.00	12	V	4.6
1350	(8+9)-III-2	6395	7.30	32.00	4.4	1.77	20.00	11	V	4.4
1350	(8+9)-VI-2	9702	11.08	32.00	2.9	2.68	20.00	7.5	V	2.9
1350	(8+9)-III-4	-2563	-2.93	32.00	11	-0.71	20.00	28	V	11
1350	(8+9)-VI-3	-9853	-11.25	32.00	2.8	-2.72	20.00	7.3	V	2.8
1350	(8+9)-I-1	2034	2.32	32.00	14	0.56	20.00	36	V	14
1350	(8+9)-VI-4	5949	6.79	32.00	4.7	1.64	20.00	12	V	4.7
1350	(8+9)-IV-4	5217	5.96	32.00	5.4	1.44	20.00	14	V	5.4
1350	(8+9)-VII-1	4191	4.79	32.00	6.7	1.16	20.00	17	V	6.7
1350	(8+9)-II-1	-6632	-7.57	32.00	4.2	-1.83	20.00	11	V	4.2
1350	(8+9)-VII-2	8172	9.33	32.00	3.4	2.26	20.00	8.9	V	3.4
1350	(8+9)-III-1	2413	2.76	32.00	12	0.67	20.00	30	V	12
1350	(8+9)-VII-3	-8322	-9.51	32.00	3.4	-2.30	20.00	8.7	V	3.4
1350	(8+9)-IV-1	-5367	-6.13	32.00	5.2	-1.48	20.00	13	V	5.2
1350	(8+9)-VII-4	-4341	-4.96	32.00	6.5	-1.20	20.00	17	V	6.5
1350	(8+9)-III-3	-6545	-7.48	32.00	4.3	-1.81	20.00	11	V	4.3
1350	(8+9)-IV-3	-8055	-9.20	32.00	3.5	-2.23	20.00	9.0	V	3.5
1350	(8+9)-II-3	-9319	-10.64	32.00	3.0	-2.58	20.00	7.8	V	3.0
1350	(8+9)-VIII-1	-4834	-5.52	32.00	5.8	-1.34	20.00	15	V	5.8
1350	(8+9)-VIII-2	8438	9.64	32.00	3.3	2.33	20.00	8.6	V	3.3
1350	(8+9)-VIII-3	-8588	-9.81	32.00	3.3	-2.37	20.00	8.4	V	3.3
1350	(8+9)-I-3	-6924	-7.91	32.00	4.0	-1.91	20.00	10	V	4.0

Setto 49: origine (1760.9,587.2,245.0), direzione (-0.199495,0.979899,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	1	127	-2	-39	0.35	-0.22	-1.29	79.20	115.20	115.20	57
0	2	162	-5	-67	0.45	-0.51	-2.24	118.80	172.80	172.80	51
0	3	162	-5	-67	0.45	-0.51	-2.24	118.80	172.80	172.80	51
0	4	127	-2	-39	0.35	-0.22	-1.29	105.60	153.60	153.60	76
0	5	127	-2	-39	0.35	-0.22	-1.29	105.60	153.60	153.60	76
0	6	127	-2	-39	0.35	-0.22	-1.29	105.60	153.60	153.60	76
0	7	127	-2	-39	0.35	-0.22	-1.29	105.60	153.60	153.60	76
0	(8+9)-VIII-4	-2817	135	-627	-7.77	14.02	-20.79	132.00	192.00	192.00	5.5
0	(8+9)-IV-1	3376	-148	643	9.31	-15.34	21.33	132.00	192.00	192.00	3.8

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-V-1	-2466	-166	-533	-6.81	-17.25	-17.68	132.00	192.00	192.00	5.5
0	(8+9)-I-2	-4197	-250	-896	-11.58	-25.92	-29.73	132.00	192.00	192.00	3.4
0	(8+9)-V-2	-5418	-217	-1125	-14.95	-22.52	-37.33	132.00	192.00	192.00	3.1
0	(8+9)-I-4	1438	196	252	3.97	20.36	8.35	132.00	192.00	192.00	5.6
0	(8+9)-V-3	5610	214	1073	15.48	22.22	35.59	132.00	192.00	192.00	2.4
0	(8+9)-II-2	-5668	-153	-1186	-15.64	-15.86	-39.32	132.00	192.00	192.00	3.4
0	(8+9)-V-4	2659	164	481	7.34	16.95	15.95	132.00	192.00	192.00	4.4
0	(8+9)-II-4	-3978	-19	-841	-10.98	-1.98	-27.90	132.00	192.00	192.00	6.3
0	(8+9)-VI-1	3804	26	720	10.50	2.70	23.88	132.00	192.00	192.00	4.6
0	(8+9)-III-2	-3959	-201	-853	-10.92	-20.81	-28.28	132.00	192.00	192.00	3.9
0	(8+9)-VI-2	-6035	-143	-1254	-16.65	-14.84	-41.60	132.00	192.00	192.00	3.3
0	(8+9)-III-4	1676	246	295	4.62	25.46	9.80	132.00	192.00	192.00	4.6
0	(8+9)-VI-3	6227	140	1202	17.18	14.54	39.86	132.00	192.00	192.00	2.4
0	(8+9)-IV-2	-4874	11	-1040	-13.45	1.15	-34.49	132.00	192.00	192.00	5.2
0	(8+9)-VI-4	-3612	-29	-772	-9.97	-3.00	-25.62	132.00	192.00	192.00	6.6
0	(8+9)-IV-4	-3184	145	-695	-8.78	15.04	-23.06	132.00	192.00	192.00	5.0
0	(8+9)-VII-1	-2705	-216	-577	-7.46	-22.36	-19.13	132.00	192.00	192.00	4.6
0	(8+9)-II-1	4170	16	789	11.51	1.68	26.16	132.00	192.00	192.00	4.3
0	(8+9)-VII-2	-5180	-168	-1082	-14.29	-17.41	-35.88	132.00	192.00	192.00	3.5
0	(8+9)-III-1	-1484	-249	-348	-4.09	-25.76	-11.53	132.00	192.00	192.00	5.1
0	(8+9)-VII-3	5372	165	1029	14.82	17.11	34.14	132.00	192.00	192.00	2.6
0	(8+9)-I-1	-1246	-199	-304	-3.44	-20.66	-10.08	132.00	192.00	192.00	6.2
0	(8+9)-VII-4	2897	213	525	7.99	22.06	17.40	132.00	192.00	192.00	3.8
0	(8+9)-III-3	4151	198	800	11.45	20.51	26.54	132.00	192.00	192.00	3.0
0	(8+9)-IV-3	5066	-14	988	13.98	-1.45	32.75	132.00	192.00	192.00	3.5
0	(8+9)-II-3	5860	150	1133	16.17	15.56	37.58	132.00	192.00	192.00	2.5
0	(8+9)-VIII-1	3009	-138	574	8.30	-14.32	19.05	132.00	192.00	192.00	4.2
0	(8+9)-VIII-2	-5240	21	-1109	-14.46	2.18	-36.77	132.00	192.00	192.00	4.8
0	(8+9)-VIII-3	5432	-24	1056	14.99	-2.48	35.03	132.00	192.00	192.00	3.2
0	(8+9)-I-3	4389	247	844	12.11	25.62	27.99	132.00	192.00	192.00	2.7
Verifiche nella direzione secondaria											
0	1	-1025	-1	44	-1.76	-0.09	0.38	79.20	115.20	115.20	>100
0	2	-1701	-2	86	-2.93	-0.17	0.74	118.80	172.80	172.80	>100
0	3	-1701	-2	86	-2.93	-0.17	0.74	118.80	172.80	172.80	>100
0	4	-1025	-1	44	-1.76	-0.09	0.38	105.60	153.60	153.60	>100
0	5	-1025	-1	44	-1.76	-0.09	0.38	105.60	153.60	153.60	>100
0	6	-1025	-1	44	-1.76	-0.09	0.38	105.60	153.60	153.60	>100
0	7	-1025	-1	44	-1.76	-0.09	0.38	105.60	153.60	153.60	>100
0	(8+9)-VIII-4	-483	-11	2648	-0.83	-1.12	22.80	132.00	192.00	192.00	8.0
0	(8+9)-IV-2	-475	-6	4348	-0.82	-0.58	37.43	132.00	192.00	192.00	5.1
0	(8+9)-V-1	-828	18	2007	-1.43	1.78	17.28	132.00	192.00	192.00	10
0	(8+9)-I-2	-554	-1	3712	-0.95	-0.11	31.96	132.00	192.00	192.00	6.0
0	(8+9)-V-2	-672	12	4592	-1.16	1.21	39.53	132.00	192.00	192.00	4.7
0	(8+9)-I-4	-699	-6	-1074	-1.20	-0.59	-9.25	132.00	192.00	192.00	19
0	(8+9)-V-3	-736	-14	-4538	-1.27	-1.33	-39.07	132.00	192.00	192.00	4.8
0	(8+9)-II-2	-424	-10	5052	-0.73	-0.94	43.49	132.00	192.00	192.00	4.3
0	(8+9)-V-4	-581	-19	-1954	-1.00	-1.91	-16.82	132.00	192.00	192.00	10
0	(8+9)-II-4	-467	-11	3616	-0.80	-1.09	31.13	132.00	192.00	192.00	6.0
0	(8+9)-VI-1	-977	14	-3299	-1.68	1.36	-28.40	132.00	192.00	192.00	6.4
0	(8+9)-III-2	-570	0	3501	-0.98	0.00	30.14	132.00	192.00	192.00	6.4
0	(8+9)-VI-2	-459	-6	5316	-0.79	-0.55	45.76	132.00	192.00	192.00	4.1
0	(8+9)-III-4	-714	-5	-1285	-1.23	-0.48	-11.06	132.00	192.00	192.00	17
0	(8+9)-VI-3	-950	4	-5263	-1.64	0.42	-45.30	132.00	192.00	192.00	4.2
0	(8+9)-I-1	-710	5	1127	-1.22	0.47	9.71	132.00	192.00	192.00	19
0	(8+9)-VI-4	-431	-15	3352	-0.74	-1.49	28.86	132.00	192.00	192.00	6.3
0	(8+9)-IV-4	-518	-7	2912	-0.89	-0.73	25.07	132.00	192.00	192.00	7.4
0	(8+9)-VII-1	-813	17	2218	-1.40	1.67	19.10	132.00	192.00	192.00	9.2
0	(8+9)-II-1	-942	10	-3563	-1.62	0.96	-30.67	132.00	192.00	192.00	6.1
0	(8+9)-VII-2	-688	13	4380	-1.18	1.32	37.71	132.00	192.00	192.00	4.9
0	(8+9)-III-1	-695	4	1339	-1.20	0.36	11.52	132.00	192.00	192.00	16
0	(8+9)-VII-3	-721	-15	-4327	-1.24	-1.44	-37.25	132.00	192.00	192.00	5.0
0	(8+9)-IV-1	-891	6	-2859	-1.53	0.60	-24.61	132.00	192.00	192.00	7.6
0	(8+9)-VII-4	-596	-18	-2165	-1.03	-1.80	-18.64	132.00	192.00	192.00	9.4
0	(8+9)-III-3	-839	-1	-3447	-1.44	-0.13	-29.68	132.00	192.00	192.00	6.4

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-IV-3	-934	5	-4294	-1.61	0.46	-36.97	132.00	192.00	192.00	5.1
0	(8+9)-II-3	-985	8	-4999	-1.70	0.82	-43.03	132.00	192.00	192.00	4.4
0	(8+9)-VIII-1	-926	10	-2595	-1.59	1.00	-22.34	132.00	192.00	192.00	8.2
0	(8+9)-VIII-2	-510	-2	4612	-0.88	-0.19	39.70	132.00	192.00	192.00	4.8
0	(8+9)-VIII-3	-899	1	-4558	-1.55	0.06	-39.24	132.00	192.00	192.00	4.9
0	(8+9)-I-3	-854	-0	-3658	-1.47	-0.02	-31.50	132.00	192.00	192.00	6.1

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
0	(8+9)-VIII-1	-16	0.03	6.40	Si	>100
0	(8+9)-VIII-4	20	0.04	6.40	Si	>100
1200	1	6	0.01	3.84	Si	>100
1200	2	12	0.02	5.76	Si	>100
1200	3	12	0.02	5.76	Si	>100
1200	4	6	0.01	5.12	Si	>100
1200	5	6	0.01	5.12	Si	>100
1200	6	6	0.01	5.12	Si	>100
1200	7	6	0.01	5.12	Si	>100
1200	(8+9)-VI-3	41	0.06	6.40	Si	>100
1200	(8+9)-VII-4	193	0.27	6.40	Si	24
1200	(8+9)-I-4	246	0.34	6.40	Si	19
1200	(8+9)-I-2	-223	0.31	6.40	Si	21
1200	(8+9)-II-2	-42	0.06	6.40	Si	>100
1200	(8+9)-VIII-2	-102	0.14	6.40	Si	45
1200	(8+9)-II-4	99	0.14	6.40	Si	46
1200	(8+9)-VIII-3	110	0.15	6.40	Si	42
1200	(8+9)-III-2	-244	0.34	6.40	Si	19
1200	(8+9)-I-1	-238	0.33	6.40	Si	19
1200	(8+9)-III-4	226	0.32	6.40	Si	20
1200	(8+9)-IV-1	-21	0.03	6.40	Si	>100
1200	(8+9)-I-3	232	0.32	6.40	Si	20
1200	(8+9)-IV-2	-111	0.16	6.40	Si	41
1200	(8+9)-VI-4	89	0.12	6.40	Si	51
1200	(8+9)-IV-4	29	0.04	6.40	Si	>100
1200	(8+9)-VII-1	-184	0.26	6.40	Si	25
1200	(8+9)-V-2	-190	0.27	6.40	Si	24
1200	(8+9)-VII-2	-211	0.29	6.40	Si	22
1200	(8+9)-V-4	213	0.30	6.40	Si	21
1200	(8+9)-VII-3	220	0.31	6.40	Si	21
1200	(8+9)-VI-2	-32	0.04	6.40	Si	>100
1200	(8+9)-II-1	-90	0.13	6.40	Si	51
1200	(8+9)-VI-1	-80	0.11	6.40	Si	57
1200	(8+9)-IV-3	120	0.17	6.40	Si	38
1200	(8+9)-V-3	199	0.28	6.40	Si	23
1200	(8+9)-II-3	51	0.07	6.40	Si	90
1200	(8+9)-III-1	-217	0.30	6.40	Si	21
1200	(8+9)-III-3	253	0.35	6.40	Si	18
1200	(8+9)-V-1	-205	0.29	6.40	Si	22
Verifiche nella direzione secondaria						
0	(8+9)-III-4	-222	0.35	6.40	Si	18
0	(8+9)-I-4	-247	0.39	6.40	Si	16
0	(8+9)-VIII-3	-79	0.13	6.40	Si	51
0	(8+9)-II-1	95	0.15	6.40	Si	42
0	(8+9)-VI-4	-49	0.08	6.40	Si	82
0	(8+9)-II-2	43	0.07	6.40	Si	94
0	(8+9)-IV-3	-129	0.21	6.40	Si	31
0	(8+9)-II-3	-47	0.08	6.40	Si	85
0	(8+9)-I-1	242	0.39	6.40	Si	17
0	(8+9)-II-4	-99	0.16	6.40	Si	41
0	(8+9)-I-3	-231	0.37	6.40	Si	17
0	(8+9)-VI-1	45	0.07	6.40	Si	90
0	(8+9)-IV-2	125	0.20	6.40	Si	32

X	Comb.	Ty	τ_d	fvd	RS	Cs
0	(8+9)-I-2	227	0.36	6.40	Si	18
0	(8+9)-VIII-2	75	0.12	6.40	Si	54
0	(8+9)-III-1	218	0.35	6.40	Si	18
0	(8+9)-III-2	251	0.40	6.40	Si	16
0	(8+9)-III-3	-256	0.41	6.40	Si	16
359	1	-8	0.01	3.84	Si	>100
359	2	-12	0.02	5.76	Si	>100
359	3	-12	0.02	5.76	Si	>100
359	4	-8	0.01	5.12	Si	>100
359	5	-8	0.01	5.12	Si	>100
359	6	-8	0.01	5.12	Si	>100
359	7	-8	0.01	5.12	Si	>100
359	(8+9)-VIII-4	54	0.09	6.40	Si	75
359	(8+9)-VI-3	55	0.09	6.40	Si	73
359	(8+9)-IV-1	-32	0.05	6.40	Si	>100
359	(8+9)-VII-3	94	0.15	6.40	Si	43
359	(8+9)-V-4	94	0.15	6.40	Si	43
359	(8+9)-VII-4	110	0.18	6.40	Si	37
359	(8+9)-VII-1	-121	0.19	6.40	Si	33
359	(8+9)-VII-2	-105	0.17	6.40	Si	38
359	(8+9)-VI-2	-66	0.10	6.40	Si	61
359	(8+9)-V-2	-121	0.19	6.40	Si	33
359	(8+9)-VIII-1	-64	0.10	6.40	Si	62
359	(8+9)-V-1	-104	0.17	6.40	Si	39
359	(8+9)-IV-4	22	0.03	6.40	Si	>100
359	(8+9)-V-3	111	0.18	6.40	Si	36

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Tx kg	τ_{vd} kg/cmq	fvd kg/cmq	Csv	τ_M kg/cmq	fTd kg/cmq	Csm	Mecc.	Cs
0	(8+9)-VIII-4	-1512	-6.26	32.00	5.1	-1.51	20.00	13	V	5.1
0	(8+9)-IV-1	1462	6.05	32.00	5.3	1.46	20.00	14	V	5.3
0	(8+9)-VI-4	-1898	-7.86	32.00	4.1	-1.90	20.00	11	V	4.1
0	(8+9)-III-2	-2059	-8.52	32.00	3.8	-2.06	20.00	9.7	V	3.8
0	(8+9)-IV-2	-2494	-10.32	32.00	3.1	-2.50	20.00	8.0	V	3.1
0	(8+9)-III-3	1840	7.62	32.00	4.2	1.84	20.00	11	V	4.2
0	(8+9)-VIII-2	-2662	-11.02	32.00	2.9	-2.67	20.00	7.5	V	2.9
0	(8+9)-VII-2	-2619	-10.84	32.00	3.0	-2.62	20.00	7.6	V	3.0
0	(8+9)-VII-4	1214	5.02	32.00	6.4	1.22	20.00	16	V	6.4
0	(8+9)-VII-1	-1432	-5.93	32.00	5.4	-1.43	20.00	14	V	5.4
0	(8+9)-I-2	-2175	-9.00	32.00	3.6	-2.18	20.00	9.2	V	3.6
0	(8+9)-VII-3	2401	9.94	32.00	3.2	2.40	20.00	8.3	V	3.2
0	(8+9)-IV-3	2276	9.42	32.00	3.4	2.28	20.00	8.8	V	3.4
0	(8+9)-II-2	-2880	-11.92	32.00	2.7	-2.88	20.00	6.9	V	2.7
0	(8+9)-IV-4	-1680	-6.96	32.00	4.6	-1.68	20.00	12	V	4.6
0	(8+9)-II-4	-2066	-8.55	32.00	3.7	-2.07	20.00	9.7	V	3.7
0	(8+9)-V-1	-1317	-5.45	32.00	5.9	-1.32	20.00	15	V	5.9
0	(8+9)-VIII-3	2444	10.11	32.00	3.2	2.45	20.00	8.2	V	3.2
0	(8+9)-V-2	-2735	-11.32	32.00	2.8	-2.74	20.00	7.3	V	2.8
0	(8+9)-I-1	-756	-3.13	32.00	10	-0.76	20.00	26	V	10
0	(8+9)-V-3	2516	10.42	32.00	3.1	2.52	20.00	7.9	V	3.1
0	(8+9)-II-1	1848	7.65	32.00	4.2	1.85	20.00	11	V	4.2
0	(8+9)-V-4	1098	4.54	32.00	7.0	1.10	20.00	18	V	7.0
0	(8+9)-III-1	-872	-3.61	32.00	8.9	-0.87	20.00	23	V	8.9
0	(8+9)-I-3	1956	8.10	32.00	4.0	1.96	20.00	10	V	4.0
0	(8+9)-II-3	2662	11.02	32.00	2.9	2.67	20.00	7.5	V	2.9
0	(8+9)-VIII-1	1294	5.35	32.00	6.0	1.30	20.00	15	V	6.0
0	(8+9)-VI-1	1680	6.95	32.00	4.6	1.68	20.00	12	V	4.6
0	(8+9)-VI-2	-3048	-12.62	32.00	2.5	-3.05	20.00	6.6	V	2.5
0	(8+9)-VI-3	2830	11.71	32.00	2.7	2.83	20.00	7.1	V	2.7
1200	1	413	1.19	19.20	16	0.29	12.00	42	V	16
1200	2	674	1.94	28.80	15	0.47	18.00	38	V	15
1200	3	674	1.94	28.80	15	0.47	18.00	38	V	15

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
1200	4	413	1.19	25.60	22	0.29	16.00	56	V	22
1200	5	413	1.19	25.60	22	0.29	16.00	56	V	22
1200	6	413	1.19	25.60	22	0.29	16.00	56	V	22
1200	7	413	1.19	25.60	22	0.29	16.00	56	V	22
1200	(8+9)-III-4	995	2.87	32.00	11	0.69	20.00	29	V	11
1200	(8+9)-I-4	876	2.52	32.00	13	0.61	20.00	33	V	13
Verifiche nella direzione secondaria										
0	(8+9)-VIII-4	3218	5.54	32.00	5.8	1.34	20.00	15	V	5.8
0	(8+9)-VII-2	5929	10.21	32.00	3.1	2.47	20.00	8.1	V	3.1
0	(8+9)-III-3	-4684	-8.06	32.00	4.0	-1.95	20.00	10	V	4.0
0	(8+9)-IV-2	5575	9.60	32.00	3.3	2.32	20.00	8.6	V	3.3
0	(8+9)-III-4	-1928	-3.32	32.00	9.6	-0.80	20.00	25	V	9.6
0	(8+9)-VIII-2	5953	10.25	32.00	3.1	2.48	20.00	8.1	V	3.1
0	(8+9)-IV-1	-3611	-6.22	32.00	5.1	-1.50	20.00	13	V	5.1
0	(8+9)-VII-4	-3188	-5.49	32.00	5.8	-1.33	20.00	15	V	5.8
0	(8+9)-I-1	1653	2.85	32.00	11	0.69	20.00	29	V	11
0	(8+9)-IV-3	-5590	-9.63	32.00	3.3	-2.33	20.00	8.6	V	3.3
0	(8+9)-I-3	-4943	-8.51	32.00	3.8	-2.06	20.00	9.7	V	3.8
0	(8+9)-IV-4	3596	6.19	32.00	5.2	1.50	20.00	13	V	5.2
0	(8+9)-II-1	-4476	-7.71	32.00	4.2	-1.87	20.00	11	V	4.2
0	(8+9)-V-1	2913	5.02	32.00	6.4	1.21	20.00	16	V	6.4
0	(8+9)-II-3	-6455	-11.11	32.00	2.9	-2.69	20.00	7.4	V	2.9
0	(8+9)-V-2	6188	10.65	32.00	3.0	2.58	20.00	7.8	V	3.0
0	(8+9)-III-1	1913	3.29	32.00	9.7	0.80	20.00	25	V	9.7
0	(8+9)-V-3	-6203	-10.68	32.00	3.0	-2.58	20.00	7.7	V	3.0
0	(8+9)-VIII-3	-5968	-10.28	32.00	3.1	-2.49	20.00	8.0	V	3.1
0	(8+9)-V-4	-2928	-5.04	32.00	6.3	-1.22	20.00	16	V	6.3
0	(8+9)-VII-3	-5944	-10.23	32.00	3.1	-2.48	20.00	8.1	V	3.1
0	(8+9)-VI-1	-4098	-7.06	32.00	4.5	-1.71	20.00	12	V	4.5
0	(8+9)-I-4	-1668	-2.87	32.00	11	-0.70	20.00	29	V	11
0	(8+9)-VI-2	6818	11.74	32.00	2.7	2.84	20.00	7.0	V	2.7
0	(8+9)-II-4	4461	7.68	32.00	4.2	1.86	20.00	11	V	4.2
0	(8+9)-VIII-1	-3233	-5.57	32.00	5.7	-1.35	20.00	15	V	5.7
0	(8+9)-I-2	4928	8.49	32.00	3.8	2.05	20.00	9.7	V	3.8
0	(8+9)-II-2	6440	11.09	32.00	2.9	2.68	20.00	7.5	V	2.9
0	(8+9)-III-2	4669	8.04	32.00	4.0	1.95	20.00	10	V	4.0
0	(8+9)-VI-3	-6833	-11.77	32.00	2.7	-2.85	20.00	7.0	V	2.7
0	(8+9)-VI-4	4083	7.03	32.00	4.6	1.70	20.00	12	V	4.6
0	(8+9)-VII-1	3173	5.46	32.00	5.9	1.32	20.00	15	V	5.9
359	1	-50	-0.09	19.20	>100	-0.02	12.00	>100	V	>100
359	2	-40	-0.07	28.80	>100	-0.02	18.00	>100	V	>100
359	3	-40	-0.07	28.80	>100	-0.02	18.00	>100	V	>100
359	4	-50	-0.09	25.60	>100	-0.02	16.00	>100	V	>100
359	5	-50	-0.09	25.60	>100	-0.02	16.00	>100	V	>100
359	6	-50	-0.09	25.60	>100	-0.02	16.00	>100	V	>100
359	7	-50	-0.09	25.60	>100	-0.02	16.00	>100	V	>100

Verifiche a instabilità

Setto(X)	Comb.	k _{critc}	k _{critm}	λ_{relc}	λ_{relm}	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
(cm)						kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	
47(40.0)	(8+9)-V-3	--	--	--	--	1.64	3.38	-5.71	132.00	192.00	192.00	17
48(180.9)	(8+9)-V-3	--	--	--	--	2.37	4.06	-7.48	132.00	192.00	192.00	13
49(0.0)	(8+9)-V-3	--	--	--	--	15.48	22.22	35.59	132.00	192.00	192.00	2.4

Parete Xlam 2 - Nodi: [12-35-38-39-36-11-111-3-2-1-102] - **Crit.Prog.** Criterio di verifica XLAM 0 - **Verificato:** [Cs=3.309,Comb=3]

Geometria setti

Setto	Crit.	X	L	S	X90	L90	S90
		mm	cm	cm	mm	cm	cm
50	Criterio di verifica XLAM 0	0	299.0	12.1	0	150.0	12.1
		750	299.0	12.1	1495	150.0	12.1
		1500	299.0	12.1	2990	150.0	12.1
51	Criterio di verifica XLAM 0	0	299.0	12.1	0	529.1	12.1
		2646	299.0	12.1	1495	529.1	12.1
		5291	299.0	12.1	2990	529.1	12.1
52	Criterio di verifica XLAM 0	0	89.0	12.1	0	80.0	12.1
		400	89.0	12.1	445	80.0	12.1
		800	89.0	12.1	890	80.0	12.1

Setto 50: origine (1023.0,465.0,149.5), direzione (0.930013,0.367526,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	(8+9)-VIII-1	111	-134	534	0.05	-2.31	0.49	132.00	192.00	192.00	67
0	(8+9)-III-4	401	-320	-1381	0.18	-5.53	-1.28	132.00	192.00	192.00	27
0	(8+9)-VI-2	-171	-332	-497	-0.08	-5.75	-0.46	132.00	192.00	192.00	31
0	(8+9)-III-1	-519	316	1473	-0.24	5.47	1.36	132.00	192.00	192.00	28
0	(8+9)-IV-1	-1	-57	756	-0.00	-0.98	0.70	132.00	192.00	192.00	>100
0	(8+9)-III-2	-649	415	1287	-0.30	7.18	1.19	132.00	192.00	192.00	23
0	(8+9)-VII-3	158	-162	-458	0.07	-2.81	-0.42	132.00	192.00	192.00	58
0	(8+9)-III-3	530	-419	-1195	0.24	-7.24	-1.11	132.00	192.00	192.00	22
0	(8+9)-VIII-2	-321	196	-84	-0.15	3.40	-0.08	132.00	192.00	192.00	55
0	(8+9)-VI-4	-80	-399	-855	-0.04	-6.90	-0.79	132.00	192.00	192.00	25
0	(8+9)-I-2	-604	256	1163	-0.28	4.44	1.08	132.00	192.00	192.00	35
0	(8+9)-I-4	446	-478	-1505	0.21	-8.27	-1.39	132.00	192.00	192.00	19
0	(8+9)-IV-2	-433	273	137	-0.20	4.73	0.13	132.00	192.00	192.00	40
0	(8+9)-II-2	-283	-255	-276	-0.13	-4.42	-0.26	132.00	192.00	192.00	41
0	(8+9)-IV-3	314	-277	-45	0.14	-4.79	-0.04	132.00	192.00	192.00	38
0	(8+9)-II-4	32	-475	-1076	0.01	-8.23	-1.00	132.00	192.00	192.00	21
0	(8+9)-VI-3	53	328	589	0.02	5.68	0.54	132.00	192.00	192.00	31
0	(8+9)-VII-2	-277	158	550	-0.13	2.74	0.51	132.00	192.00	192.00	59
0	(8+9)-V-1	-193	218	860	-0.09	3.77	0.79	132.00	192.00	192.00	42
0	(8+9)-I-3	485	-260	-1072	0.22	-4.50	-0.99	132.00	192.00	192.00	33
0	(8+9)-VIII-4	-230	130	-443	-0.11	2.25	-0.41	132.00	192.00	192.00	72
0	(8+9)-II-3	164	251	368	0.08	4.35	0.34	132.00	192.00	192.00	40
0	(8+9)-I-1	-564	474	1597	-0.26	8.21	1.48	132.00	192.00	192.00	20
0	(8+9)-II-1	-151	472	1168	-0.07	8.16	1.08	132.00	192.00	192.00	21
0	(8+9)-VII-4	29	-63	-644	0.01	-1.09	-0.60	132.00	192.00	192.00	>100
0	(8+9)-VIII-3	203	-200	176	0.09	-3.46	0.16	132.00	192.00	192.00	51
0	(8+9)-V-4	74	-222	-768	0.03	-3.84	-0.71	132.00	192.00	192.00	42
0	(8+9)-VI-1	-39	395	947	-0.02	6.83	0.88	132.00	192.00	192.00	25
1500	1	727	-4	-599	0.34	-0.06	-0.55	79.20	115.20	115.20	>100
1500	2	1086	-7	-889	0.50	-0.12	-0.82	118.80	172.80	172.80	>100
1500	3	1086	-7	-889	0.50	-0.12	-0.82	118.80	172.80	172.80	>100
1500	4	727	-4	-599	0.34	-0.06	-0.55	105.60	153.60	153.60	>100
1500	5	727	-4	-599	0.34	-0.06	-0.55	105.60	153.60	153.60	>100
1500	6	727	-4	-599	0.34	-0.06	-0.55	105.60	153.60	153.60	>100
1500	7	727	-4	-599	0.34	-0.06	-0.55	105.60	153.60	153.60	>100
1500	(8+9)-IV-4	897	13	-880	0.41	0.23	-0.81	132.00	192.00	192.00	>100
1500	(8+9)-VII-1	785	35	-922	0.36	0.61	-0.85	132.00	192.00	192.00	97
1500	(8+9)-V-3	130	-59	225	0.06	-1.02	0.21	132.00	192.00	192.00	>100
1500	(8+9)-V-2	898	54	-1076	0.41	0.93	-0.99	132.00	192.00	192.00	76
Verifiche nella direzione secondaria											
0	(8+9)-I-1	-4865	-22	2789	-6.70	-1.72	15.37	132.00	192.00	192.00	11
0	(8+9)-VII-1	-4228	-19	2064	-5.82	-1.50	11.37	132.00	192.00	192.00	15
0	(8+9)-VI-1	-4132	-71	1886	-5.69	-5.57	10.39	132.00	192.00	192.00	12
0	(8+9)-III-1	-4869	-28	2779	-6.71	-2.18	15.31	132.00	192.00	192.00	11
0	(8+9)-II-1	-4324	-73	2101	-5.96	-5.78	11.57	132.00	192.00	192.00	11
2990	1	-4476	1	2500	-6.17	0.09	13.77	79.20	115.20	115.20	8.1
2990	2	-7133	4	3996	-9.83	0.32	22.02	118.80	172.80	172.80	7.5
2990	3	-7133	4	3996	-9.83	0.32	22.02	118.80	172.80	172.80	7.5

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
2990	4	-4476	1	2500	-6.17	0.09	13.77	105.60	153.60	153.60	11
2990	5	-4476	1	2500	-6.17	0.09	13.77	105.60	153.60	153.60	11
2990	6	-4476	1	2500	-6.17	0.09	13.77	105.60	153.60	153.60	11
2990	7	-4476	1	2500	-6.17	0.09	13.77	105.60	153.60	153.60	11
2990	(8+9)-VIII-4	-3523	-152	1588	-4.85	-11.97	8.75	132.00	192.00	192.00	9.2
2990	(8+9)-IV-4	-3506	-149	1706	-4.83	-11.71	9.40	132.00	192.00	192.00	9.0
2990	(8+9)-V-4	-3017	87	2194	-4.16	6.83	12.09	132.00	192.00	192.00	10
2990	(8+9)-II-3	-3490	147	1709	-4.81	11.62	9.41	132.00	192.00	192.00	9.1
2990	(8+9)-I-3	-3205	163	2437	-4.41	12.81	13.42	132.00	192.00	192.00	7.3
2990	(8+9)-II-2	-2687	-145	1735	-3.70	-11.47	9.56	132.00	192.00	192.00	9.1
2990	(8+9)-VI-2	-2671	-142	1853	-3.68	-11.20	10.21	132.00	192.00	192.00	8.9
2990	(8+9)-III-3	-2958	187	2588	-4.07	14.72	14.26	132.00	192.00	192.00	6.6
2990	(8+9)-VI-3	-3506	144	1591	-4.83	11.36	8.76	132.00	192.00	192.00	9.5
2990	(8+9)-IV-1	-2670	151	1738	-3.68	11.86	9.58	132.00	192.00	192.00	8.9
2990	(8+9)-VI-4	-2700	-71	2091	-3.72	-5.62	11.52	132.00	192.00	192.00	11
2990	(8+9)-IV-3	-2668	228	2212	-3.67	17.98	12.19	132.00	192.00	192.00	6.4
2990	(8+9)-I-2	-2972	-161	1007	-4.09	-12.65	5.55	132.00	192.00	192.00	10
2990	(8+9)-V-1	-3160	-85	1250	-4.35	-6.67	6.89	132.00	192.00	192.00	14
2990	(8+9)-VII-2	-3165	-173	1249	-4.36	-13.67	6.88	132.00	192.00	192.00	9.3
2990	(8+9)-V-3	-3259	151	2044	-4.49	11.92	11.26	132.00	192.00	192.00	8.2
2990	(8+9)-VII-3	-3012	175	2195	-4.15	13.83	12.09	132.00	192.00	192.00	7.4
2990	(8+9)-III-2	-3219	-185	856	-4.43	-14.56	4.72	132.00	192.00	192.00	9.9
2990	(8+9)-VII-4	-3264	62	2043	-4.50	4.92	11.26	132.00	192.00	192.00	12
2990	(8+9)-V-2	-2918	-149	1400	-4.02	-11.76	7.71	132.00	192.00	192.00	9.8
2990	(8+9)-II-4	-2684	-68	2209	-3.70	-5.35	12.17	132.00	192.00	192.00	11
2990	(8+9)-III-4	-3210	74	2436	-4.42	5.81	13.42	132.00	192.00	192.00	9.9
2990	(8+9)-I-4	-2963	98	2587	-4.08	7.72	14.25	132.00	192.00	192.00	8.7
2990	(8+9)-VIII-1	-2654	154	1856	-3.66	12.13	10.23	132.00	192.00	192.00	8.6
2990	(8+9)-VIII-2	-3493	-223	1350	-4.81	-17.55	7.44	132.00	192.00	192.00	7.6
2990	(8+9)-VIII-3	-2684	225	2094	-3.70	17.71	11.54	132.00	192.00	192.00	6.5
2990	(8+9)-IV-2	-3509	-226	1232	-4.83	-17.82	6.79	132.00	192.00	192.00	7.8

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
0	(8+9)-IV-2	269	0.09	6.40	Si	71
0	(8+9)-I-4	-537	0.18	6.40	Si	36
0	(8+9)-IV-3	-268	0.09	6.40	Si	71
0	(8+9)-V-2	382	0.13	6.40	Si	50
0	(8+9)-VII-3	-342	0.11	6.40	Si	56
0	(8+9)-II-2	402	0.13	6.40	Si	48
0	(8+9)-VII-1	290	0.10	6.40	Si	66
0	(8+9)-II-3	-401	0.13	6.40	Si	48
0	(8+9)-V-3	-381	0.13	6.40	Si	50
0	(8+9)-V-1	250	0.08	6.40	Si	76
0	(8+9)-I-2	670	0.22	6.40	Si	28
0	(8+9)-III-1	578	0.19	6.40	Si	33
0	(8+9)-VII-4	-289	0.10	6.40	Si	66
0	(8+9)-III-2	631	0.21	6.40	Si	30
0	(8+9)-I-3	-669	0.22	6.40	Si	29
0	(8+9)-VII-2	343	0.11	6.40	Si	56
0	(8+9)-I-1	538	0.18	6.40	Si	35
0	(8+9)-III-3	-630	0.21	6.40	Si	30
0	(8+9)-III-4	-577	0.19	6.40	Si	33
0	(8+9)-V-4	-249	0.08	6.40	Si	77
750	1	3	0.00	3.84	Si	>100
750	2	4	0.00	5.76	Si	>100
750	3	4	0.00	5.76	Si	>100
750	4	3	0.00	5.12	Si	>100
750	5	3	0.00	5.12	Si	>100
750	6	3	0.00	5.12	Si	>100
750	7	3	0.00	5.12	Si	>100
750	(8+9)-IV-1	-180	0.06	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
750	(8+9)-VIII-1	-105	0.04	6.40	Si	>100
750	(8+9)-VI-2	418	0.14	6.40	Si	46
750	(8+9)-VIII-2	254	0.09	6.40	Si	75
750	(8+9)-VI-4	273	0.09	6.40	Si	70
750	(8+9)-VIII-3	-250	0.08	6.40	Si	77
750	(8+9)-II-1	-344	0.12	6.40	Si	56
750	(8+9)-IV-4	184	0.06	6.40	Si	>100
750	(8+9)-VI-3	-413	0.14	6.40	Si	46
750	(8+9)-VI-1	-269	0.09	6.40	Si	71
750	(8+9)-II-4	348	0.12	6.40	Si	55
750	(8+9)-VIII-4	109	0.04	6.40	Si	>100
Verifiche nella direzione secondaria						
0	2	-6	0.01	5.76	Si	>100
0	3	-6	0.01	5.76	Si	>100
2990	1	-3	0.00	3.84	Si	>100
2990	4	-3	0.00	5.12	Si	>100
2990	5	-3	0.00	5.12	Si	>100
2990	6	-3	0.00	5.12	Si	>100
2990	7	-3	0.00	5.12	Si	>100
2990	(8+9)-VIII-4	-218	0.28	6.40	Si	23
2990	(8+9)-IV-3	301	0.38	6.40	Si	17
2990	(8+9)-V-1	66	0.08	6.40	Si	77
2990	(8+9)-I-2	-360	0.46	6.40	Si	14
2990	(8+9)-V-2	-109	0.14	6.40	Si	46
2990	(8+9)-I-4	181	0.23	6.40	Si	28
2990	(8+9)-V-3	105	0.13	6.40	Si	48
2990	(8+9)-II-2	-374	0.48	6.40	Si	13
2990	(8+9)-V-4	-69	0.09	6.40	Si	72
2990	(8+9)-II-4	-212	0.27	6.40	Si	24
2990	(8+9)-VI-1	283	0.36	6.40	Si	18
2990	(8+9)-III-2	-339	0.43	6.40	Si	15
2990	(8+9)-VI-2	-299	0.38	6.40	Si	17
2990	(8+9)-III-4	202	0.26	6.40	Si	25
2990	(8+9)-VI-3	295	0.38	6.40	Si	17
2990	(8+9)-IV-2	-305	0.39	6.40	Si	16
2990	(8+9)-VI-4	-287	0.37	6.40	Si	18
2990	(8+9)-IV-4	-143	0.18	6.40	Si	35
2990	(8+9)-VII-1	45	0.06	6.40	Si	>100
2990	(8+9)-II-1	208	0.26	6.40	Si	24
2990	(8+9)-VII-2	-88	0.11	6.40	Si	57
2990	(8+9)-III-1	-206	0.26	6.40	Si	24
2990	(8+9)-VII-3	84	0.11	6.40	Si	60
2990	(8+9)-IV-1	139	0.18	6.40	Si	36
2990	(8+9)-VII-4	-49	0.06	6.40	Si	>100
2990	(8+9)-III-3	335	0.43	6.40	Si	15
2990	(8+9)-I-1	-185	0.24	6.40	Si	27
2990	(8+9)-II-3	370	0.47	6.40	Si	14
2990	(8+9)-VIII-1	214	0.27	6.40	Si	24
2990	(8+9)-VIII-2	-230	0.29	6.40	Si	22
2990	(8+9)-VIII-3	226	0.29	6.40	Si	22
2990	(8+9)-I-3	356	0.45	6.40	Si	14

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
750	1	-1380	-0.95	19.20	20	-0.23	12.00	52	V	20
750	2	-2343	-1.62	28.80	18	-0.39	18.00	46	V	18
750	3	-2343	-1.62	28.80	18	-0.39	18.00	46	V	18
750	4	-1380	-0.95	25.60	27	-0.23	16.00	69	V	27
750	5	-1380	-0.95	25.60	27	-0.23	16.00	69	V	27
750	6	-1380	-0.95	25.60	27	-0.23	16.00	69	V	27
750	7	-1380	-0.95	25.60	27	-0.23	16.00	69	V	27
750	(8+9)-VIII-4	-2980	-2.06	32.00	16	-0.50	20.00	40	V	16

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
750	(8+9)-V-3	-2723	-1.88	32.00	17	-0.46	20.00	44	V	17
750	(8+9)-VI-4	-3204	-2.21	32.00	14	-0.54	20.00	37	V	14
750	(8+9)-III-3	-4256	-2.94	32.00	11	-0.71	20.00	28	V	11
750	(8+9)-I-4	-5145	-3.56	32.00	9.0	-0.86	20.00	23	V	9.0
750	(8+9)-III-4	-5078	-3.51	32.00	9.1	-0.85	20.00	24	V	9.1
750	(8+9)-II-2	-1400	-0.97	32.00	33	-0.23	20.00	85	V	33
750	(8+9)-VI-2	-1840	-1.27	32.00	25	-0.31	20.00	65	V	25
750	(8+9)-II-4	-3643	-2.52	32.00	13	-0.61	20.00	33	V	13
750	(8+9)-IV-2	-1177	-0.81	32.00	39	-0.20	20.00	>100	V	39
750	(8+9)-I-3	-4189	-2.89	32.00	11	-0.70	20.00	29	V	11
750	(8+9)-VII-4	-3612	-2.50	32.00	13	-0.60	20.00	33	V	13
750	(8+9)-VII-3	-2790	-1.93	32.00	17	-0.47	20.00	43	V	17
750	(8+9)-VIII-2	-1617	-1.12	32.00	29	-0.27	20.00	74	V	29
750	(8+9)-V-4	-3679	-2.54	32.00	13	-0.62	20.00	33	V	13
750	(8+9)-IV-4	-3420	-2.36	32.00	14	-0.57	20.00	35	V	14
1500	(8+9)-V-1	2932	2.03	32.00	16	0.49	20.00	41	V	16
1500	(8+9)-IV-1	3090	2.14	32.00	15	0.52	20.00	39	V	15
1500	(8+9)-I-2	3593	2.48	32.00	13	0.60	20.00	33	V	13
1500	(8+9)-VII-2	2197	1.52	32.00	21	0.37	20.00	54	V	21
1500	(8+9)-V-2	2227	1.54	32.00	21	0.37	20.00	54	V	21
1500	(8+9)-III-1	4328	2.99	32.00	11	0.72	20.00	28	V	11
1500	(8+9)-VI-1	2578	1.78	32.00	18	0.43	20.00	46	V	18
1500	(8+9)-II-3	1160	0.80	32.00	40	0.19	20.00	>100	V	40
1500	(8+9)-VII-1	2963	2.05	32.00	16	0.50	20.00	40	V	16
1500	(8+9)-IV-3	1263	0.87	32.00	37	0.21	20.00	95	V	37
1500	(8+9)-I-1	4297	2.97	32.00	11	0.72	20.00	28	V	11
1500	(8+9)-III-2	3562	2.46	32.00	13	0.60	20.00	34	V	13
1500	(8+9)-VIII-1	2681	1.85	32.00	17	0.45	20.00	45	V	17
1500	(8+9)-II-1	2987	2.06	32.00	16	0.50	20.00	40	V	16
1500	(8+9)-VIII-3	1673	1.16	32.00	28	0.28	20.00	71	V	28
1500	(8+9)-VI-3	1570	1.08	32.00	29	0.26	20.00	76	V	29
Verifiche nella direzione secondaria										
1495	(8+9)-VIII-4	-1387	-1.91	32.00	17	-0.46	20.00	43	V	17
1495	(8+9)-IV-4	-1597	-2.20	32.00	15	-0.53	20.00	38	V	15
1495	(8+9)-II-1	1240	1.71	32.00	19	0.41	20.00	48	V	19
1495	(8+9)-V-3	-1216	-1.67	32.00	19	-0.41	20.00	49	V	19
1495	(8+9)-VIII-1	999	1.38	32.00	23	0.33	20.00	60	V	23
1495	(8+9)-V-2	828	1.14	32.00	28	0.28	20.00	72	V	28
1495	(8+9)-VII-2	838	1.15	32.00	28	0.28	20.00	72	V	28
1495	(8+9)-V-1	1334	1.84	32.00	17	0.44	20.00	45	V	17
1495	(8+9)-I-1	2033	2.80	32.00	11	0.68	20.00	30	V	11
1495	(8+9)-III-1	2023	2.79	32.00	11	0.67	20.00	30	V	11
1495	(8+9)-I-3	-1915	-2.64	32.00	12	-0.64	20.00	31	V	12
1495	(8+9)-III-2	1537	2.12	32.00	15	0.51	20.00	39	V	15
1495	(8+9)-VIII-2	-622	-0.86	32.00	37	-0.21	20.00	96	V	37
1495	(8+9)-III-3	-1924	-2.65	32.00	12	-0.64	20.00	31	V	12
1495	(8+9)-VII-1	1324	1.82	32.00	18	0.44	20.00	45	V	18
1495	(8+9)-I-4	-2420	-3.33	32.00	9.6	-0.81	20.00	25	V	9.6
1495	(8+9)-VII-4	-1712	-2.36	32.00	14	-0.57	20.00	35	V	14
1495	(8+9)-I-2	1527	2.10	32.00	15	0.51	20.00	39	V	15
1495	(8+9)-III-4	-2411	-3.32	32.00	9.6	-0.80	20.00	25	V	9.6
1495	(8+9)-IV-1	1209	1.67	32.00	19	0.40	20.00	50	V	19
2990	1	-622	-0.86	19.20	22	-0.21	12.00	58	V	22
2990	2	-1047	-1.44	28.80	20	-0.35	18.00	52	V	20
2990	3	-1047	-1.44	28.80	20	-0.35	18.00	52	V	20
2990	4	-622	-0.86	25.60	30	-0.21	16.00	77	V	30
2990	5	-622	-0.86	25.60	30	-0.21	16.00	77	V	30
2990	6	-622	-0.86	25.60	30	-0.21	16.00	77	V	30
2990	7	-622	-0.86	25.60	30	-0.21	16.00	77	V	30
2990	(8+9)-IV-2	-420	-0.58	32.00	55	-0.14	20.00	>100	V	55
2990	(8+9)-VI-4	-1874	-2.58	32.00	12	-0.62	20.00	32	V	12
2990	(8+9)-IV-3	-421	-0.58	32.00	55	-0.14	20.00	>100	V	55
2990	(8+9)-II-2	-1190	-1.64	32.00	20	-0.40	20.00	50	V	20
2990	(8+9)-VI-1	1033	1.42	32.00	22	0.34	20.00	58	V	22

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
2990	(8+9)-V-4	-1873	-2.58	32.00	12	-0.62	20.00	32	V	12
2990	(8+9)-VII-3	-1433	-1.97	32.00	16	-0.48	20.00	42	V	16
2990	(8+9)-VI-2	-1204	-1.66	32.00	19	-0.40	20.00	50	V	19
2990	(8+9)-II-3	349	0.48	32.00	67	0.12	20.00	>100	V	67
2990	(8+9)-II-4	-1888	-2.60	32.00	12	-0.63	20.00	32	V	12
2990	(8+9)-VIII-3	-407	-0.56	32.00	57	-0.14	20.00	>100	V	57
2990	(8+9)-VI-3	363	0.50	32.00	64	0.12	20.00	>100	V	64

Setto 51: origine (1236.9,549.5,149.5), direzione (0.930013,0.367526,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
2646	1	-298	9	336	-0.14	0.16	0.31	79.20	115.20	115.20	>100
2646	2	-519	16	576	-0.24	0.27	0.53	118.80	172.80	172.80	>100
2646	3	-519	16	576	-0.24	0.27	0.53	118.80	172.80	172.80	>100
2646	4	-298	9	336	-0.14	0.16	0.31	105.60	153.60	153.60	>100
2646	5	-298	9	336	-0.14	0.16	0.31	105.60	153.60	153.60	>100
2646	6	-298	9	336	-0.14	0.16	0.31	105.60	153.60	153.60	>100
2646	7	-298	9	336	-0.14	0.16	0.31	105.60	153.60	153.60	>100
5291	(8+9)-VIII-4	-337	370	916	-0.16	6.40	0.85	132.00	192.00	192.00	26
5291	(8+9)-IV-1	257	-420	-887	0.12	-7.27	-0.82	132.00	192.00	192.00	23
5291	(8+9)-V-1	284	-413	-1033	0.13	-7.14	-0.96	132.00	192.00	192.00	23
5291	(8+9)-I-2	134	-502	-1007	0.06	-8.69	-0.93	132.00	192.00	192.00	20
5291	(8+9)-V-2	166	-419	-740	0.08	-7.24	-0.68	132.00	192.00	192.00	24
5291	(8+9)-I-4	-322	471	1409	-0.15	8.16	1.30	132.00	192.00	192.00	20
5291	(8+9)-V-3	-236	394	849	-0.11	6.82	0.79	132.00	192.00	192.00	25
5291	(8+9)-II-2	-164	-168	180	-0.08	-2.91	0.17	132.00	192.00	192.00	62
5291	(8+9)-V-4	-355	388	1142	-0.16	6.71	1.06	132.00	192.00	192.00	25
5291	(8+9)-II-4	-301	124	905	-0.14	2.14	0.84	132.00	192.00	192.00	64
5291	(8+9)-VI-1	240	-123	-716	0.11	-2.14	-0.66	132.00	192.00	192.00	65
5291	(8+9)-III-2	126	-421	-979	0.06	-7.28	-0.91	132.00	192.00	192.00	23
5291	(8+9)-VI-2	-154	-143	260	-0.07	-2.48	0.24	132.00	192.00	192.00	71
5291	(8+9)-III-4	-330	553	1436	-0.15	9.57	1.33	132.00	192.00	192.00	18
5291	(8+9)-VI-3	84	119	-151	0.04	2.05	-0.14	132.00	192.00	192.00	85
5291	(8+9)-IV-2	-191	103	272	-0.09	1.78	0.25	132.00	192.00	192.00	94
5291	(8+9)-VI-4	-310	99	825	-0.14	1.71	0.76	132.00	192.00	192.00	78
5291	(8+9)-IV-4	-328	395	996	-0.15	6.84	0.92	132.00	192.00	192.00	25
5291	(8+9)-VII-1	292	-494	-1061	0.13	-8.55	-0.98	132.00	192.00	192.00	20
5291	(8+9)-II-1	230	-149	-796	0.11	-2.57	-0.74	132.00	192.00	192.00	55
5291	(8+9)-VII-2	158	-337	-713	0.07	-5.83	-0.66	132.00	192.00	192.00	29
5291	(8+9)-III-1	260	-578	-1327	0.12	-10.00	-1.23	132.00	192.00	192.00	17
5291	(8+9)-VII-3	-228	312	822	-0.11	5.41	0.76	132.00	192.00	192.00	31
5291	(8+9)-I-1	252	-496	-1300	0.12	-8.59	-1.20	132.00	192.00	192.00	19
5291	(8+9)-VII-4	-363	469	1170	-0.17	8.12	1.08	132.00	192.00	192.00	21
5291	(8+9)-III-3	-196	396	1089	-0.09	6.85	1.01	132.00	192.00	192.00	24
5291	(8+9)-IV-3	120	-128	-162	0.06	-2.21	-0.15	132.00	192.00	192.00	79
5291	(8+9)-II-3	93	144	-71	0.04	2.48	-0.07	132.00	192.00	192.00	73
5291	(8+9)-VIII-1	267	-395	-807	0.12	-6.83	-0.75	132.00	192.00	192.00	25
5291	(8+9)-VIII-2	-181	128	352	-0.08	2.22	0.32	132.00	192.00	192.00	76
5291	(8+9)-VIII-3	111	-153	-242	0.05	-2.65	-0.22	132.00	192.00	192.00	65
5291	(8+9)-I-3	-204	477	1116	-0.09	8.26	1.03	132.00	192.00	192.00	21
Verifiche nella direzione secondaria											
0	(8+9)-VIII-4	-9880	260	-9180	-3.86	5.81	-4.07	132.00	192.00	192.00	19
0	(8+9)-VI-2	-9389	681	-6030	-3.67	15.21	-2.67	132.00	192.00	192.00	11
0	(8+9)-III-1	-8640	782	5946	-3.37	17.47	2.63	132.00	192.00	192.00	9.5
0	(8+9)-IV-2	-9376	722	-4575	-3.66	16.13	-2.03	132.00	192.00	192.00	11
0	(8+9)-III-2	-8578	1047	4099	-3.35	23.40	1.82	132.00	192.00	192.00	7.6
0	(8+9)-VIII-2	-9618	639	-5556	-3.76	14.27	-2.46	132.00	192.00	192.00	11
0	(8+9)-III-3	-11127	-1034	-12677	-4.35	-23.10	-5.61	132.00	192.00	192.00	6.7
0	(8+9)-VII-3	-10320	-757	-9405	-4.03	-16.91	-4.16	132.00	192.00	192.00	9.1
0	(8+9)-III-4	-11065	-768	-14524	-4.32	-17.17	-6.43	132.00	192.00	192.00	8.1
0	(8+9)-I-1	-8709	769	6088	-3.40	17.18	2.70	132.00	192.00	192.00	9.6
0	(8+9)-VI-4	-9650	302	-9654	-3.77	6.76	-4.27	132.00	192.00	192.00	17

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-I-3	-11196	-1047	-12535	-4.37	-23.38	-5.55	132.00	192.00	192.00	6.6
0	(8+9)-VII-1	-9448	505	2674	-3.69	11.27	1.18	132.00	192.00	192.00	15
0	(8+9)-IV-3	-10329	-708	-4004	-4.03	-15.83	-1.77	132.00	192.00	192.00	11
0	(8+9)-II-3	-10559	-751	-3530	-4.12	-16.77	-1.56	132.00	192.00	192.00	10
0	(8+9)-IV-4	-10122	177	-10161	-3.95	3.96	-4.50	132.00	192.00	192.00	22
0	(8+9)-VIII-3	-10087	-625	-3022	-3.94	-13.97	-1.34	132.00	192.00	192.00	12
0	(8+9)-V-1	-9516	492	2816	-3.72	10.99	1.25	132.00	192.00	192.00	16
0	(8+9)-VII-2	-9385	770	827	-3.66	17.21	0.37	132.00	192.00	192.00	11
0	(8+9)-V-2	-9316	783	684	-3.64	17.49	0.30	132.00	192.00	192.00	11
0	(8+9)-I-4	-10996	-756	-14667	-4.29	-16.88	-6.49	132.00	192.00	192.00	8.2
0	(8+9)-II-4	-9892	219	-10636	-3.86	4.90	-4.71	132.00	192.00	192.00	20
0	(8+9)-VII-4	-10257	-491	-11252	-4.01	-10.97	-4.98	132.00	192.00	192.00	12
0	(8+9)-I-2	-8509	1060	3957	-3.32	23.68	1.75	132.00	192.00	192.00	7.5
0	(8+9)-II-2	-9146	764	-5049	-3.57	17.07	-2.24	132.00	192.00	192.00	9.9
0	(8+9)-V-3	-10389	-769	-9263	-4.06	-17.19	-4.10	132.00	192.00	192.00	9.0
0	(8+9)-V-4	-10189	-478	-11395	-3.98	-10.69	-5.05	132.00	192.00	192.00	12
0	(8+9)-VI-3	-10316	-667	-2548	-4.03	-14.91	-1.13	132.00	192.00	192.00	12
1495	1	-13634	-6	-6859	-5.32	-0.13	-3.04	79.20	115.20	115.20	34
1495	2	-21367	-5	-10637	-8.34	-0.12	-4.71	118.80	172.80	172.80	33
1495	3	-21367	-5	-10637	-8.34	-0.12	-4.71	118.80	172.80	172.80	33
1495	4	-13634	-6	-6859	-5.32	-0.13	-3.04	105.60	153.60	153.60	46
1495	5	-13634	-6	-6859	-5.32	-0.13	-3.04	105.60	153.60	153.60	46
1495	6	-13634	-6	-6859	-5.32	-0.13	-3.04	105.60	153.60	153.60	46
1495	7	-13634	-6	-6859	-5.32	-0.13	-3.04	105.60	153.60	153.60	46
2990	(8+9)-VIII-1	-8707	255	-6253	-3.40	5.71	-2.77	132.00	192.00	192.00	22
2990	(8+9)-II-1	-8967	249	-5757	-3.50	5.56	-2.55	132.00	192.00	192.00	23
2990	(8+9)-IV-1	-8498	240	-6317	-3.32	5.35	-2.80	132.00	192.00	192.00	23
2990	(8+9)-VI-1	-9176	265	-5693	-3.58	5.92	-2.52	132.00	192.00	192.00	23

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Ty kg	τ_d kg/cmq	fvd kg/cmq	RS	Cs
0	(8+9)-VI-1	12	0.00	6.40	Si	>100
0	(8+9)-VI-4	-11	0.00	6.40	Si	>100
2646	1	12	0.00	3.84	Si	>100
2646	2	20	0.01	5.76	Si	>100
2646	3	20	0.01	5.76	Si	>100
2646	4	12	0.00	5.12	Si	>100
2646	5	12	0.00	5.12	Si	>100
2646	6	12	0.00	5.12	Si	>100
2646	7	12	0.00	5.12	Si	>100
5291	(8+9)-VIII-4	20	0.01	6.40	Si	>100
5291	(8+9)-IV-1	-87	0.03	6.40	Si	>100
5291	(8+9)-V-2	259	0.09	6.40	Si	74
5291	(8+9)-I-4	-54	0.02	6.40	Si	>100
5291	(8+9)-V-3	-274	0.09	6.40	Si	70
5291	(8+9)-II-2	88	0.03	6.40	Si	>100
5291	(8+9)-V-4	-229	0.08	6.40	Si	83
5291	(8+9)-II-4	46	0.02	6.40	Si	>100
5291	(8+9)-I-2	84	0.03	6.40	Si	>100
5291	(8+9)-III-2	93	0.03	6.40	Si	>100
5291	(8+9)-VI-2	140	0.05	6.40	Si	>100
5291	(8+9)-III-4	-46	0.02	6.40	Si	>100
5291	(8+9)-VI-3	-154	0.05	6.40	Si	>100
5291	(8+9)-IV-2	115	0.04	6.40	Si	>100
5291	(8+9)-I-1	40	0.01	6.40	Si	>100
5291	(8+9)-IV-4	73	0.02	6.40	Si	>100
5291	(8+9)-VII-1	207	0.07	6.40	Si	92
5291	(8+9)-II-1	-60	0.02	6.40	Si	>100
5291	(8+9)-VII-2	268	0.09	6.40	Si	71
5291	(8+9)-III-1	32	0.01	6.40	Si	>100
5291	(8+9)-VII-3	-282	0.09	6.40	Si	68
5291	(8+9)-I-3	-99	0.03	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
5291	(8+9)-VII-4	-221	0.07	6.40	Si	86
5291	(8+9)-III-3	-107	0.04	6.40	Si	>100
5291	(8+9)-IV-3	-129	0.04	6.40	Si	>100
5291	(8+9)-II-3	-102	0.03	6.40	Si	>100
5291	(8+9)-VIII-1	-35	0.01	6.40	Si	>100
5291	(8+9)-VIII-2	167	0.06	6.40	Si	>100
5291	(8+9)-VIII-3	-181	0.06	6.40	Si	>100
5291	(8+9)-V-1	215	0.07	6.40	Si	89
Verifiche nella direzione secondaria						
0	(8+9)-VIII-4	-306	0.11	6.40	Si	58
0	(8+9)-VI-2	-434	0.16	6.40	Si	41
0	(8+9)-III-1	-293	0.11	6.40	Si	61
0	(8+9)-IV-2	-458	0.17	6.40	Si	39
0	(8+9)-III-2	-493	0.18	6.40	Si	36
0	(8+9)-VIII-2	-380	0.14	6.40	Si	47
0	(8+9)-III-3	474	0.17	6.40	Si	37
0	(8+9)-III-4	273	0.10	6.40	Si	65
0	(8+9)-I-1	-277	0.10	6.40	Si	64
0	(8+9)-VI-4	-360	0.13	6.40	Si	49
0	(8+9)-VIII-1	287	0.10	6.40	Si	62
0	(8+9)-I-3	490	0.18	6.40	Si	36
0	(8+9)-VI-1	341	0.12	6.40	Si	52
0	(8+9)-II-1	263	0.09	6.40	Si	68
0	(8+9)-I-2	-509	0.18	6.40	Si	35
0	(8+9)-VIII-3	361	0.13	6.40	Si	49
0	(8+9)-I-4	257	0.09	6.40	Si	69
0	(8+9)-II-2	-512	0.18	6.40	Si	35
0	(8+9)-II-4	-282	0.10	6.40	Si	63
0	(8+9)-II-3	492	0.18	6.40	Si	36
0	(8+9)-VI-3	415	0.15	6.40	Si	43
0	(8+9)-IV-3	439	0.16	6.40	Si	40
1495	(8+9)-VII-4	113	0.04	6.40	Si	>100
1495	(8+9)-VII-1	-131	0.05	6.40	Si	>100
1495	(8+9)-V-2	-295	0.11	6.40	Si	60
1495	(8+9)-V-3	277	0.10	6.40	Si	64
1495	(8+9)-VII-2	-285	0.10	6.40	Si	62
1495	(8+9)-VII-3	267	0.10	6.40	Si	66
2990	1	-23	0.01	3.84	Si	>100
2990	2	-37	0.01	5.76	Si	>100
2990	3	-37	0.01	5.76	Si	>100
2990	4	-23	0.01	5.12	Si	>100
2990	5	-23	0.01	5.12	Si	>100
2990	6	-23	0.01	5.12	Si	>100
2990	7	-23	0.01	5.12	Si	>100
2990	(8+9)-IV-1	270	0.10	6.40	Si	66
2990	(8+9)-IV-4	-301	0.11	6.40	Si	59
2990	(8+9)-V-1	-170	0.06	6.40	Si	>100
2990	(8+9)-V-4	139	0.05	6.40	Si	>100

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	(8+9)-III-1	3354	2.32	32.00	14	0.56	20.00	36	V	14
0	(8+9)-V-1	2312	1.60	32.00	20	0.39	20.00	52	V	20
0	(8+9)-IV-1	2203	1.52	32.00	21	0.37	20.00	54	V	21
0	(8+9)-I-1	3391	2.34	32.00	14	0.57	20.00	35	V	14
0	(8+9)-VII-1	2276	1.57	32.00	20	0.38	20.00	53	V	20
0	(8+9)-V-2	1536	1.06	32.00	30	0.26	20.00	78	V	30
0	(8+9)-VIII-3	836	0.58	32.00	55	0.14	20.00	>100	V	55
0	(8+9)-VII-2	1572	1.09	32.00	29	0.26	20.00	76	V	29
0	(8+9)-I-2	2615	1.81	32.00	18	0.44	20.00	46	V	18
0	(8+9)-VIII-1	1879	1.30	32.00	25	0.31	20.00	64	V	25
0	(8+9)-III-2	2651	1.83	32.00	17	0.44	20.00	45	V	17

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
2646	1	-1661	-1.15	19.20	17	-0.28	12.00	43	V	17
2646	2	-2531	-1.75	28.80	16	-0.42	18.00	43	V	16
2646	3	-2531	-1.75	28.80	16	-0.42	18.00	43	V	16
2646	4	-1661	-1.15	25.60	22	-0.28	16.00	58	V	22
2646	5	-1661	-1.15	25.60	22	-0.28	16.00	58	V	22
2646	6	-1661	-1.15	25.60	22	-0.28	16.00	58	V	22
2646	7	-1661	-1.15	25.60	22	-0.28	16.00	58	V	22
2646	(8+9)-VIII-4	-3518	-2.43	32.00	13	-0.59	20.00	34	V	13
2646	(8+9)-V-3	-3062	-2.12	32.00	15	-0.51	20.00	39	V	15
2646	(8+9)-II-2	-1701	-1.18	32.00	27	-0.28	20.00	70	V	27
2646	(8+9)-IV-2	-1645	-1.14	32.00	28	-0.28	20.00	73	V	28
2646	(8+9)-VI-4	-3574	-2.47	32.00	13	-0.60	20.00	33	V	13
2646	(8+9)-IV-4	-3944	-2.73	32.00	12	-0.66	20.00	30	V	12
2646	(8+9)-I-4	-5497	-3.80	32.00	8.4	-0.92	20.00	22	V	8.4
2646	(8+9)-III-4	-5480	-3.79	32.00	8.5	-0.92	20.00	22	V	8.5
2646	(8+9)-II-4	-4000	-2.76	32.00	12	-0.67	20.00	30	V	12
2646	(8+9)-III-3	-4498	-3.11	32.00	10	-0.75	20.00	27	V	10
2646	(8+9)-VI-2	-2127	-1.47	32.00	22	-0.36	20.00	56	V	22
2646	(8+9)-IV-3	-671	-0.46	32.00	69	-0.11	20.00	>100	V	69
2646	(8+9)-I-3	-4482	-3.10	32.00	10	-0.75	20.00	27	V	10
2646	(8+9)-VIII-2	-2071	-1.43	32.00	22	-0.35	20.00	58	V	22
2646	(8+9)-V-4	-4078	-2.82	32.00	11	-0.68	20.00	29	V	11
2646	(8+9)-VII-3	-3079	-2.13	32.00	15	-0.51	20.00	39	V	15
2646	(8+9)-VII-4	-4061	-2.81	32.00	11	-0.68	20.00	29	V	11
5291	(8+9)-VI-3	1313	0.91	32.00	35	0.22	20.00	91	V	35
5291	(8+9)-VI-1	2048	1.42	32.00	23	0.34	20.00	58	V	23
5291	(8+9)-II-3	1015	0.70	32.00	46	0.17	20.00	>100	V	46
5291	(8+9)-II-1	2345	1.62	32.00	20	0.39	20.00	51	V	20
Verifiche nella direzione secondaria										
1495	1	311	0.12	19.20	>100	0.03	12.00	>100	V	>100
1495	2	582	0.23	28.80	>100	0.05	18.00	>100	V	>100
1495	3	582	0.23	28.80	>100	0.05	18.00	>100	V	>100
1495	4	311	0.12	25.60	>100	0.03	16.00	>100	V	>100
1495	5	311	0.12	25.60	>100	0.03	16.00	>100	V	>100
1495	6	311	0.12	25.60	>100	0.03	16.00	>100	V	>100
1495	7	311	0.12	25.60	>100	0.03	16.00	>100	V	>100
1495	(8+9)-VI-1	5128	2.00	32.00	16	0.48	20.00	41	V	16
1495	(8+9)-II-4	-5578	-2.18	32.00	15	-0.53	20.00	38	V	15
1495	(8+9)-III-4	-8195	-3.20	32.00	10	-0.77	20.00	26	V	10
1495	(8+9)-I-2	6504	2.54	32.00	13	0.61	20.00	33	V	13
1495	(8+9)-VII-2	3721	1.45	32.00	22	0.35	20.00	57	V	22
1495	(8+9)-I-4	-8244	-3.22	32.00	9.9	-0.78	20.00	26	V	9.9
1495	(8+9)-VII-4	-5362	-2.09	32.00	15	-0.51	20.00	39	V	15
1495	(8+9)-VII-1	5762	2.25	32.00	14	0.54	20.00	37	V	14
1495	(8+9)-I-1	8643	3.38	32.00	9.5	0.82	20.00	24	V	9.5
1495	(8+9)-VI-4	-4729	-1.85	32.00	17	-0.45	20.00	45	V	17
1495	(8+9)-III-2	6554	2.56	32.00	13	0.62	20.00	32	V	13
1495	(8+9)-V-1	5811	2.27	32.00	14	0.55	20.00	36	V	14
1495	(8+9)-I-3	-6105	-2.38	32.00	13	-0.58	20.00	35	V	13
1495	(8+9)-VII-3	-3322	-1.30	32.00	25	-0.31	20.00	64	V	25
1495	(8+9)-III-1	8594	3.36	32.00	9.5	0.81	20.00	25	V	9.5
1495	(8+9)-III-3	-6154	-2.40	32.00	13	-0.58	20.00	34	V	13
1495	(8+9)-II-1	5978	2.33	32.00	14	0.56	20.00	35	V	14
1495	(8+9)-V-2	3672	1.43	32.00	22	0.35	20.00	58	V	22
1495	(8+9)-V-3	-3273	-1.28	32.00	25	-0.31	20.00	65	V	25
1495	(8+9)-V-4	-5412	-2.11	32.00	15	-0.51	20.00	39	V	15
2990	(8+9)-VIII-4	-4868	-1.90	32.00	17	-0.46	20.00	43	V	17
2990	(8+9)-IV-2	-2106	-0.82	32.00	39	-0.20	20.00	>100	V	39
2990	(8+9)-II-3	1619	0.63	32.00	51	0.15	20.00	>100	V	51
2990	(8+9)-VI-2	-2125	-0.83	32.00	39	-0.20	20.00	100	V	39
2990	(8+9)-II-2	-1225	-0.48	32.00	67	-0.12	20.00	>100	V	67
2990	(8+9)-IV-1	6163	2.41	32.00	13	0.58	20.00	34	V	13
2990	(8+9)-VI-3	2520	0.98	32.00	33	0.24	20.00	84	V	33
2990	(8+9)-IV-3	2500	0.98	32.00	33	0.24	20.00	85	V	33

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
2990	(8+9)-VIII-1	5262	2.05	32.00	16	0.50	20.00	40	V	16
2990	(8+9)-VIII-2	-3006	-1.17	32.00	27	-0.28	20.00	70	V	27
2990	(8+9)-VIII-3	3401	1.33	32.00	24	0.32	20.00	62	V	24
2990	(8+9)-IV-4	-5768	-2.25	32.00	14	-0.55	20.00	37	V	14

Setto 52: origine (1162.5,520.1,254.5), direzione (0.930013,0.367526,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	1	690	-4	138	1.07	-0.21	1.44	79.20	115.20	115.20	36
0	2	1031	-7	213	1.60	-0.41	2.22	118.80	172.80	172.80	35
0	3	1031	-7	213	1.60	-0.41	2.22	118.80	172.80	172.80	35
0	4	690	-4	138	1.07	-0.21	1.44	105.60	153.60	153.60	48
0	5	690	-4	138	1.07	-0.21	1.44	105.60	153.60	153.60	48
0	6	690	-4	138	1.07	-0.21	1.44	105.60	153.60	153.60	48
0	7	690	-4	138	1.07	-0.21	1.44	105.60	153.60	153.60	48
0	(8+9)-IV-1	203	-19	518	0.31	-1.09	5.40	132.00	192.00	192.00	28
0	(8+9)-V-1	952	38	294	1.47	2.23	3.07	132.00	192.00	192.00	26
0	(8+9)-I-2	167	72	475	0.26	4.20	4.96	132.00	192.00	192.00	20
0	(8+9)-V-2	980	54	136	1.52	3.13	1.42	132.00	192.00	192.00	28
0	(8+9)-I-4	838	-62	-441	1.30	-3.58	-4.60	132.00	192.00	192.00	19
0	(8+9)-VII-2	1022	57	130	1.58	3.32	1.36	132.00	192.00	192.00	28
0	(8+9)-IV-4	774	14	-325	1.20	0.81	-3.39	132.00	192.00	192.00	32
0	(8+9)-II-2	435	44	-30	0.67	2.53	-0.31	132.00	192.00	192.00	50
0	(8+9)-I-3	810	-77	-283	1.25	-4.48	-2.95	132.00	192.00	192.00	21
0	(8+9)-VIII-3	160	-53	344	0.25	-3.11	3.59	132.00	192.00	192.00	27
0	(8+9)-II-1	340	-8	497	0.53	-0.49	5.19	132.00	192.00	192.00	30
0	(8+9)-III-2	208	75	469	0.32	4.38	4.90	132.00	192.00	192.00	20
0	(8+9)-III-4	879	-58	-447	1.36	-3.40	-4.66	132.00	192.00	192.00	19
0	(8+9)-VIII-2	816	48	-152	1.26	2.82	-1.59	132.00	192.00	192.00	31
0	(8+9)-IV-2	572	54	-50	0.89	3.14	-0.52	132.00	192.00	192.00	39
0	(8+9)-VI-1	584	-14	395	0.90	-0.81	4.13	132.00	192.00	192.00	31
0	(8+9)-II-3	541	-48	222	0.84	-2.82	2.32	132.00	192.00	192.00	30
0	(8+9)-VI-2	679	38	-132	1.05	2.21	-1.37	132.00	192.00	192.00	38
0	(8+9)-III-3	769	-80	-277	1.19	-4.67	-2.89	132.00	192.00	192.00	21
0	(8+9)-IV-3	404	-59	243	0.63	-3.43	2.53	132.00	192.00	192.00	28
0	(8+9)-III-1	97	53	640	0.15	3.11	6.67	132.00	192.00	192.00	19
0	(8+9)-I-1	138	57	633	0.21	3.29	6.61	132.00	192.00	192.00	19
0	(8+9)-VI-3	297	-43	324	0.46	-2.50	3.38	132.00	192.00	192.00	29
0	(8+9)-VIII-1	447	-24	416	0.69	-1.41	4.34	132.00	192.00	192.00	28
0	(8+9)-VII-1	911	35	300	1.41	2.05	3.13	132.00	192.00	192.00	27
800	(8+9)-VIII-4	560	27	198	0.87	1.60	2.07	132.00	192.00	192.00	39
800	(8+9)-VII-3	-398	-39	304	-0.62	-2.24	3.17	132.00	192.00	192.00	35
800	(8+9)-VII-4	67	-17	376	0.10	-0.96	3.92	132.00	192.00	192.00	38
800	(8+9)-VI-4	422	20	220	0.65	1.18	2.30	132.00	192.00	192.00	43
800	(8+9)-V-4	25	-19	383	0.04	-1.09	3.99	132.00	192.00	192.00	37
800	(8+9)-II-4	809	20	218	1.25	1.19	2.27	132.00	192.00	192.00	36
800	(8+9)-V-3	-356	-36	297	-0.55	-2.12	3.10	132.00	192.00	192.00	37
Verifiche nella direzione secondaria											
890	1	-3694	1	-1630	-9.54	0.21	-31.57	79.20	115.20	115.20	3.5
890	2	-5888	5	-2592	-15.21	0.69	-50.20	118.80	172.80	172.80	3.3
890	3	-5888	5	-2592	-15.21	0.69	-50.20	118.80	172.80	172.80	3.3
890	4	-3694	1	-1630	-9.54	0.21	-31.57	105.60	153.60	153.60	4.7
890	5	-3694	1	-1630	-9.54	0.21	-31.57	105.60	153.60	153.60	4.7
890	6	-3694	1	-1630	-9.54	0.21	-31.57	105.60	153.60	153.60	4.7
890	7	-3694	1	-1630	-9.54	0.21	-31.57	105.60	153.60	153.60	4.7
890	(8+9)-VIII-4	-2163	-87	-870	-5.59	-12.88	-16.85	132.00	192.00	192.00	6.4
890	(8+9)-IV-2	-2126	-155	-956	-5.49	-22.93	-18.52	132.00	192.00	192.00	4.6
890	(8+9)-V-1	-2617	-53	-1316	-6.76	-7.77	-25.50	132.00	192.00	192.00	5.7
890	(8+9)-I-2	-2359	-172	-1222	-6.09	-25.43	-23.67	132.00	192.00	192.00	3.9
890	(8+9)-V-2	-2450	-108	-1171	-6.33	-15.97	-22.69	132.00	192.00	192.00	4.9
890	(8+9)-I-4	-2571	119	-883	-6.64	17.56	-17.11	132.00	192.00	192.00	5.5
890	(8+9)-V-3	-2647	110	-1079	-6.84	16.29	-20.89	132.00	192.00	192.00	5.1

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
890	(8+9)-II-2	-2238	-135	-934	-5.78	-19.95	-18.10	132.00	192.00	192.00	5.0
890	(8+9)-V-4	-2480	55	-934	-6.41	8.09	-18.09	132.00	192.00	192.00	7.3
890	(8+9)-II-4	-2302	-48	-833	-5.94	-7.05	-16.13	132.00	192.00	192.00	8.2
890	(8+9)-VI-1	-2823	69	-1402	-7.29	10.22	-27.16	132.00	192.00	192.00	5.1
890	(8+9)-III-2	-2325	-178	-1228	-6.00	-26.33	-23.80	132.00	192.00	192.00	3.8
890	(8+9)-VI-2	-2265	-116	-919	-5.85	-17.11	-17.81	132.00	192.00	192.00	5.5
890	(8+9)-III-4	-2538	113	-890	-6.55	16.66	-17.23	132.00	192.00	192.00	5.6
890	(8+9)-VI-3	-2832	118	-1331	-7.31	17.44	-25.78	132.00	192.00	192.00	4.4
890	(8+9)-I-1	-2526	-117	-1367	-6.52	-17.23	-26.47	132.00	192.00	192.00	4.4
890	(8+9)-VI-4	-2274	-67	-848	-5.87	-9.89	-16.43	132.00	192.00	192.00	7.2
890	(8+9)-IV-4	-2190	-68	-855	-5.66	-10.04	-16.55	132.00	192.00	192.00	7.2
890	(8+9)-VII-1	-2651	-47	-1310	-6.85	-6.87	-25.37	132.00	192.00	192.00	5.9
890	(8+9)-II-1	-2795	50	-1417	-7.22	7.38	-27.45	132.00	192.00	192.00	5.5
890	(8+9)-VII-2	-2416	-114	-1178	-6.24	-16.86	-22.82	132.00	192.00	192.00	4.8
890	(8+9)-III-1	-2559	-111	-1360	-6.61	-16.34	-26.35	132.00	192.00	192.00	4.5
890	(8+9)-VII-3	-2681	116	-1072	-6.92	17.19	-20.77	132.00	192.00	192.00	5.0
890	(8+9)-IV-1	-2907	70	-1395	-7.51	10.36	-27.03	132.00	192.00	192.00	5.1
890	(8+9)-VII-4	-2447	49	-940	-6.32	7.20	-18.21	132.00	192.00	192.00	7.5
890	(8+9)-III-3	-2772	180	-1022	-7.16	26.65	-19.79	132.00	192.00	192.00	4.1
890	(8+9)-IV-3	-2971	157	-1294	-7.67	23.26	-25.06	132.00	192.00	192.00	3.9
890	(8+9)-II-3	-2859	137	-1316	-7.38	20.28	-25.48	132.00	192.00	192.00	4.2
890	(8+9)-VIII-1	-2935	89	-1380	-7.58	13.20	-26.74	132.00	192.00	192.00	4.8
890	(8+9)-VIII-2	-2154	-136	-941	-5.56	-20.09	-18.23	132.00	192.00	192.00	5.0
890	(8+9)-VIII-3	-2944	138	-1309	-7.60	20.42	-25.36	132.00	192.00	192.00	4.2
890	(8+9)-I-3	-2739	174	-1028	-7.07	25.76	-19.91	132.00	192.00	192.00	4.2

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
0	1	-2	0.00	3.84	Si	>100
0	2	-3	0.00	5.76	Si	>100
0	3	-3	0.00	5.76	Si	>100
0	4	-2	0.00	5.12	Si	>100
0	5	-2	0.00	5.12	Si	>100
0	6	-2	0.00	5.12	Si	>100
0	7	-2	0.00	5.12	Si	>100
0	(8+9)-IV-4	-90	0.10	6.40	Si	63
0	(8+9)-I-1	251	0.28	6.40	Si	23
0	(8+9)-III-1	253	0.28	6.40	Si	23
0	(8+9)-I-2	245	0.28	6.40	Si	23
0	(8+9)-III-2	244	0.27	6.40	Si	23
0	(8+9)-I-4	-253	0.29	6.40	Si	22
0	(8+9)-III-3	-246	0.28	6.40	Si	23
0	(8+9)-II-2	64	0.07	6.40	Si	89
0	(8+9)-III-4	-255	0.29	6.40	Si	22
0	(8+9)-II-1	84	0.09	6.40	Si	68
0	(8+9)-II-3	-66	0.07	6.40	Si	86
0	(8+9)-I-3	-247	0.28	6.40	Si	23
0	(8+9)-IV-1	88	0.10	6.40	Si	65
0	(8+9)-IV-2	60	0.07	6.40	Si	95
0	(8+9)-IV-3	-62	0.07	6.40	Si	92
0	(8+9)-II-4	-86	0.10	6.40	Si	66
400	(8+9)-V-4	87	0.10	6.40	Si	66
400	(8+9)-VII-4	81	0.09	6.40	Si	70
400	(8+9)-V-2	-93	0.10	6.40	Si	61
400	(8+9)-V-3	92	0.10	6.40	Si	62
400	(8+9)-VIII-2	-54	0.06	6.40	Si	>100
400	(8+9)-VI-2	-36	0.04	6.40	Si	>100
400	(8+9)-VI-3	35	0.04	6.40	Si	>100
400	(8+9)-VIII-3	54	0.06	6.40	Si	>100
400	(8+9)-VII-1	-82	0.09	6.40	Si	70
400	(8+9)-VII-2	-98	0.11	6.40	Si	58
400	(8+9)-VII-3	97	0.11	6.40	Si	58

X	Comb.	Ty	τ_d	fvd	RS	Cs
400	(8+9)-V-1	-87	0.10	6.40	Si	65
800	(8+9)-VIII-1	26	0.03	6.40	Si	>100
800	(8+9)-VI-4	-20	0.02	6.40	Si	>100
800	(8+9)-VI-1	21	0.02	6.40	Si	>100
800	(8+9)-VIII-4	-25	0.03	6.40	Si	>100
Verifiche nella direzione secondaria						
0	(8+9)-I-1	-239	0.57	6.40	Si	11
0	(8+9)-III-4	237	0.56	6.40	Si	11
0	(8+9)-III-1	-241	0.57	6.40	Si	11
0	(8+9)-I-4	235	0.56	6.40	Si	11
890	1	-5	0.01	3.84	Si	>100
890	2	-5	0.01	5.76	Si	>100
890	3	-5	0.01	5.76	Si	>100
890	4	-5	0.01	5.12	Si	>100
890	5	-5	0.01	5.12	Si	>100
890	6	-5	0.01	5.12	Si	>100
890	7	-5	0.01	5.12	Si	>100
890	(8+9)-VIII-4	-169	0.40	6.40	Si	16
890	(8+9)-IV-4	-86	0.20	6.40	Si	31
890	(8+9)-V-3	25	0.06	6.40	Si	>100
890	(8+9)-II-2	-209	0.50	6.40	Si	13
890	(8+9)-V-4	-50	0.12	6.40	Si	54
890	(8+9)-II-4	-48	0.11	6.40	Si	56
890	(8+9)-VI-1	125	0.30	6.40	Si	21
890	(8+9)-III-2	-320	0.76	6.40	Si	8.4
890	(8+9)-VI-2	-126	0.30	6.40	Si	21
890	(8+9)-I-3	303	0.72	6.40	Si	8.9
890	(8+9)-VI-3	120	0.29	6.40	Si	22
890	(8+9)-IV-2	-247	0.59	6.40	Si	11
890	(8+9)-VI-4	-131	0.31	6.40	Si	20
890	(8+9)-I-2	-309	0.74	6.40	Si	8.7
890	(8+9)-VII-1	55	0.13	6.40	Si	49
890	(8+9)-V-2	-32	0.08	6.40	Si	85
890	(8+9)-VII-2	-43	0.10	6.40	Si	63
890	(8+9)-II-1	42	0.10	6.40	Si	64
890	(8+9)-VII-3	37	0.09	6.40	Si	73
890	(8+9)-IV-1	79	0.19	6.40	Si	34
890	(8+9)-VII-4	-61	0.15	6.40	Si	44
890	(8+9)-III-3	314	0.75	6.40	Si	8.5
890	(8+9)-IV-3	240	0.57	6.40	Si	11
890	(8+9)-II-3	203	0.48	6.40	Si	13
890	(8+9)-VIII-1	163	0.39	6.40	Si	17
890	(8+9)-VIII-2	-163	0.39	6.40	Si	16
890	(8+9)-VIII-3	157	0.37	6.40	Si	17
890	(8+9)-V-1	44	0.10	6.40	Si	62

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Tx kg	τ_{vd} kg/cm ²	fvd kg/cm ²	Csv	τ_M kg/cm ²	fTd kg/cm ²	Csm	Mecc.	Cs
0	(8+9)-IV-4	-985	-2.29	32.00	14	-0.55	20.00	36	V	14
0	(8+9)-VII-4	-986	-2.29	32.00	14	-0.55	20.00	36	V	14
0	(8+9)-II-4	-977	-2.27	32.00	14	-0.55	20.00	36	V	14
0	(8+9)-VIII-2	-213	-0.49	32.00	65	-0.12	20.00	>100	V	65
0	(8+9)-VII-3	-564	-1.31	32.00	24	-0.32	20.00	63	V	24
0	(8+9)-I-3	-1195	-2.77	32.00	12	-0.67	20.00	30	V	12
0	(8+9)-III-4	-1614	-3.75	32.00	8.5	-0.91	20.00	22	V	8.5
0	(8+9)-I-4	-1611	-3.74	32.00	8.6	-0.91	20.00	22	V	8.6
0	(8+9)-V-3	-567	-1.32	32.00	24	-0.32	20.00	63	V	24
0	(8+9)-III-3	-1192	-2.77	32.00	12	-0.67	20.00	30	V	12
0	(8+9)-VIII-4	-797	-1.85	32.00	17	-0.45	20.00	45	V	17
0	(8+9)-VI-2	-205	-0.48	32.00	67	-0.11	20.00	>100	V	67
0	(8+9)-V-4	-983	-2.28	32.00	14	-0.55	20.00	36	V	14
0	(8+9)-VI-4	-788	-1.83	32.00	17	-0.44	20.00	45	V	17

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
800	1	917	2.13	19.20	9.0	0.52	12.00	23	V	9.0
800	2	1413	3.28	28.80	8.8	0.79	18.00	23	V	8.8
800	3	1413	3.28	28.80	8.8	0.79	18.00	23	V	8.8
800	4	917	2.13	25.60	12	0.52	16.00	31	V	12
800	5	917	2.13	25.60	12	0.52	16.00	31	V	12
800	6	917	2.13	25.60	12	0.52	16.00	31	V	12
800	7	917	2.13	25.60	12	0.52	16.00	31	V	12
800	(8+9)-IV-2	359	0.83	32.00	38	0.20	20.00	99	V	38
800	(8+9)-VII-1	1840	4.27	32.00	7.5	1.03	20.00	19	V	7.5
800	(8+9)-IV-3	922	2.14	32.00	15	0.52	20.00	39	V	15
800	(8+9)-VII-2	1382	3.21	32.00	10.0	0.78	20.00	26	V	10.0
800	(8+9)-V-2	1376	3.19	32.00	10	0.77	20.00	26	V	10
800	(8+9)-II-2	337	0.78	32.00	41	0.19	20.00	>100	V	41
800	(8+9)-III-2	2013	4.67	32.00	6.8	1.13	20.00	18	V	6.8
800	(8+9)-II-1	1905	4.42	32.00	7.2	1.07	20.00	19	V	7.2
800	(8+9)-III-1	2470	5.73	32.00	5.6	1.39	20.00	14	V	5.6
800	(8+9)-VIII-1	1694	3.93	32.00	8.1	0.95	20.00	21	V	8.1
800	(8+9)-II-3	945	2.19	32.00	15	0.53	20.00	38	V	15
800	(8+9)-I-2	2006	4.66	32.00	6.9	1.13	20.00	18	V	6.9
800	(8+9)-IV-1	1883	4.37	32.00	7.3	1.06	20.00	19	V	7.3
800	(8+9)-VI-3	1134	2.63	32.00	12	0.64	20.00	31	V	12
800	(8+9)-V-1	1846	4.29	32.00	7.5	1.04	20.00	19	V	7.5
800	(8+9)-VI-1	1716	3.98	32.00	8.0	0.96	20.00	21	V	8.0
800	(8+9)-VIII-3	1111	2.58	32.00	12	0.62	20.00	32	V	12
800	(8+9)-I-1	2477	5.75	32.00	5.6	1.39	20.00	14	V	5.6
Verifiche nella direzione secondaria										
0	(8+9)-IV-2	-90	-0.23	32.00	>100	-0.06	20.00	>100	V	>100
445	(8+9)-VIII-4	-1074	-2.77	32.00	12	-0.67	20.00	30	V	12
445	(8+9)-V-4	-1393	-3.60	32.00	8.9	-0.87	20.00	23	V	8.9
445	(8+9)-II-4	-1345	-3.47	32.00	9.2	-0.84	20.00	24	V	9.2
445	(8+9)-III-1	2436	6.29	32.00	5.1	1.52	20.00	13	V	5.1
445	(8+9)-VII-4	-1373	-3.55	32.00	9.0	-0.86	20.00	23	V	9.0
445	(8+9)-III-2	1912	4.94	32.00	6.5	1.19	20.00	17	V	6.5
445	(8+9)-VII-2	1231	3.18	32.00	10	0.77	20.00	26	V	10
445	(8+9)-III-3	-1529	-3.95	32.00	8.1	-0.96	20.00	21	V	8.1
445	(8+9)-I-2	1891	4.88	32.00	6.6	1.18	20.00	17	V	6.6
445	(8+9)-III-4	-2053	-5.30	32.00	6.0	-1.28	20.00	16	V	6.0
445	(8+9)-I-4	-2074	-5.36	32.00	6.0	-1.30	20.00	15	V	6.0
445	(8+9)-VI-4	-1141	-2.95	32.00	11	-0.71	20.00	28	V	11
445	(8+9)-II-2	-156	-0.40	32.00	80	-0.10	20.00	>100	V	80
445	(8+9)-V-3	-828	-2.14	32.00	15	-0.52	20.00	39	V	15
445	(8+9)-VIII-2	-292	-0.76	32.00	42	-0.18	20.00	>100	V	42
445	(8+9)-VI-2	-360	-0.93	32.00	34	-0.23	20.00	89	V	34
445	(8+9)-I-1	2457	6.34	32.00	5.0	1.54	20.00	13	V	5.0
445	(8+9)-II-1	1728	4.46	32.00	7.2	1.08	20.00	19	V	7.2
445	(8+9)-VII-1	1756	4.53	32.00	7.1	1.10	20.00	18	V	7.1
445	(8+9)-VII-3	-848	-2.19	32.00	15	-0.53	20.00	38	V	15
445	(8+9)-I-3	-1509	-3.90	32.00	8.2	-0.94	20.00	21	V	8.2
445	(8+9)-IV-4	-1278	-3.30	32.00	9.7	-0.80	20.00	25	V	9.7
445	(8+9)-V-1	1776	4.59	32.00	7.0	1.11	20.00	18	V	7.0
445	(8+9)-VI-1	1524	3.94	32.00	8.1	0.95	20.00	21	V	8.1
890	1	518	1.34	19.20	14	0.32	12.00	37	V	14
890	2	785	2.03	28.80	14	0.49	18.00	37	V	14
890	3	785	2.03	28.80	14	0.49	18.00	37	V	14
890	4	518	1.34	25.60	19	0.32	16.00	49	V	19
890	5	518	1.34	25.60	19	0.32	16.00	49	V	19
890	6	518	1.34	25.60	19	0.32	16.00	49	V	19
890	7	518	1.34	25.60	19	0.32	16.00	49	V	19
890	(8+9)-II-3	635	1.64	32.00	20	0.40	20.00	50	V	20
890	(8+9)-IV-1	1721	4.44	32.00	7.2	1.08	20.00	19	V	7.2
890	(8+9)-VI-3	803	2.07	32.00	15	0.50	20.00	40	V	15
890	(8+9)-VIII-1	1553	4.01	32.00	8.0	0.97	20.00	21	V	8.0
890	(8+9)-IV-3	735	1.90	32.00	17	0.46	20.00	44	V	17
890	(8+9)-VIII-3	902	2.33	32.00	14	0.56	20.00	35	V	14

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
890	(8+9)-V-2	1219	3.15	32.00	10	0.76	20.00	26	V	10

Verifiche a instabilità

Setto(X)	Comb.	kcrit _c	kcrit _m	$\lambda_{rel,c}$	$\lambda_{rel,m}$	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
(cm)						kg/cm ² q	kg/cm ² q	kg/cm ² q	kg/cm ² q	kg/cm ² q	kg/cm ² q	
50(0.0)	(8+9)-I-4	--	--	--	--	0.21	-8.27	-1.39	132.00	192.00	192.00	19
51(529.1)	(8+9)-III-4	0.26	--	1.92	--	-0.15	9.57	1.33	132.00	192.00	192.00	17
52(0.0)	(8+9)-I-1	--	--	--	--	0.21	3.29	6.61	132.00	192.00	192.00	19

Parete Xlam 2 - Nodi: [12-35-38-39-36-11-111-3-2-1-102] - **Crit.Prog.** Criterio di verifica XLAM 0 - **Verificato:** [Cs=3.309,Comb=3]

Geometria setti

Setto	Crit.	X	L	S	X90	L90	S90
		mm	cm	cm	mm	cm	cm
50	Criterio di verifica XLAM 0	0	299.0	12.1	0	150.0	12.1
		750	299.0	12.1	1495	150.0	12.1
		1500	299.0	12.1	2990	150.0	12.1
51	Criterio di verifica XLAM 0	0	299.0	12.1	0	529.1	12.1
		2646	299.0	12.1	1495	529.1	12.1
		5291	299.0	12.1	2990	529.1	12.1
52	Criterio di verifica XLAM 0	0	89.0	12.1	0	80.0	12.1
		400	89.0	12.1	445	80.0	12.1
		800	89.0	12.1	890	80.0	12.1

Setto 50: origine (1023.0,465.0,149.5), direzione (0.930013,0.367526,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	
0	(8+9)-VIII-1	111	-134	534	0.05	-2.31	0.49	132.00	192.00	192.00	67
0	(8+9)-III-4	401	-320	-1381	0.18	-5.53	-1.28	132.00	192.00	192.00	27
0	(8+9)-VI-2	-171	-332	-497	-0.08	-5.75	-0.46	132.00	192.00	192.00	31
0	(8+9)-III-1	-519	316	1473	-0.24	5.47	1.36	132.00	192.00	192.00	28
0	(8+9)-IV-1	-1	-57	756	-0.00	-0.98	0.70	132.00	192.00	192.00	>100
0	(8+9)-III-2	-649	415	1287	-0.30	7.18	1.19	132.00	192.00	192.00	23
0	(8+9)-VII-3	158	-162	-458	0.07	-2.81	-0.42	132.00	192.00	192.00	58
0	(8+9)-III-3	530	-419	-1195	0.24	-7.24	-1.11	132.00	192.00	192.00	22
0	(8+9)-VIII-2	-321	196	-84	-0.15	3.40	-0.08	132.00	192.00	192.00	55
0	(8+9)-VI-4	-80	-399	-855	-0.04	-6.90	-0.79	132.00	192.00	192.00	25
0	(8+9)-I-2	-604	256	1163	-0.28	4.44	1.08	132.00	192.00	192.00	35
0	(8+9)-I-4	446	-478	-1505	0.21	-8.27	-1.39	132.00	192.00	192.00	19
0	(8+9)-IV-2	-433	273	137	-0.20	4.73	0.13	132.00	192.00	192.00	40
0	(8+9)-II-2	-283	-255	-276	-0.13	-4.42	-0.26	132.00	192.00	192.00	41
0	(8+9)-IV-3	314	-277	-45	0.14	-4.79	-0.04	132.00	192.00	192.00	38
0	(8+9)-II-4	32	-475	-1076	0.01	-8.23	-1.00	132.00	192.00	192.00	21
0	(8+9)-VI-3	53	328	589	0.02	5.68	0.54	132.00	192.00	192.00	31
0	(8+9)-VII-2	-277	158	550	-0.13	2.74	0.51	132.00	192.00	192.00	59
0	(8+9)-V-1	-193	218	860	-0.09	3.77	0.79	132.00	192.00	192.00	42
0	(8+9)-I-3	485	-260	-1072	0.22	-4.50	-0.99	132.00	192.00	192.00	33
0	(8+9)-VIII-4	-230	130	-443	-0.11	2.25	-0.41	132.00	192.00	192.00	72
0	(8+9)-II-3	164	251	368	0.08	4.35	0.34	132.00	192.00	192.00	40
0	(8+9)-I-1	-564	474	1597	-0.26	8.21	1.48	132.00	192.00	192.00	20
0	(8+9)-II-1	-151	472	1168	-0.07	8.16	1.08	132.00	192.00	192.00	21
0	(8+9)-VII-4	29	-63	-644	0.01	-1.09	-0.60	132.00	192.00	192.00	>100
0	(8+9)-VIII-3	203	-200	176	0.09	-3.46	0.16	132.00	192.00	192.00	51
0	(8+9)-V-4	74	-222	-768	0.03	-3.84	-0.71	132.00	192.00	192.00	42
0	(8+9)-VI-1	-39	395	947	-0.02	6.83	0.88	132.00	192.00	192.00	25

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
1500	1	727	-4	-599	0.34	-0.06	-0.55	79.20	115.20	115.20	>100
1500	2	1086	-7	-889	0.50	-0.12	-0.82	118.80	172.80	172.80	>100
1500	3	1086	-7	-889	0.50	-0.12	-0.82	118.80	172.80	172.80	>100
1500	4	727	-4	-599	0.34	-0.06	-0.55	105.60	153.60	153.60	>100
1500	5	727	-4	-599	0.34	-0.06	-0.55	105.60	153.60	153.60	>100
1500	6	727	-4	-599	0.34	-0.06	-0.55	105.60	153.60	153.60	>100
1500	7	727	-4	-599	0.34	-0.06	-0.55	105.60	153.60	153.60	>100
1500	(8+9)-IV-4	897	13	-880	0.41	0.23	-0.81	132.00	192.00	192.00	>100
1500	(8+9)-VII-1	785	35	-922	0.36	0.61	-0.85	132.00	192.00	192.00	97
1500	(8+9)-V-3	130	-59	225	0.06	-1.02	0.21	132.00	192.00	192.00	>100
1500	(8+9)-V-2	898	54	-1076	0.41	0.93	-0.99	132.00	192.00	192.00	76
Verifiche nella direzione secondaria											
0	(8+9)-I-1	-4865	-22	2789	-6.70	-1.72	15.37	132.00	192.00	192.00	11
0	(8+9)-VII-1	-4228	-19	2064	-5.82	-1.50	11.37	132.00	192.00	192.00	15
0	(8+9)-VI-1	-4132	-71	1886	-5.69	-5.57	10.39	132.00	192.00	192.00	12
0	(8+9)-III-1	-4869	-28	2779	-6.71	-2.18	15.31	132.00	192.00	192.00	11
0	(8+9)-II-1	-4324	-73	2101	-5.96	-5.78	11.57	132.00	192.00	192.00	11
2990	1	-4476	1	2500	-6.17	0.09	13.77	79.20	115.20	115.20	8.1
2990	2	-7133	4	3996	-9.83	0.32	22.02	118.80	172.80	172.80	7.5
2990	3	-7133	4	3996	-9.83	0.32	22.02	118.80	172.80	172.80	7.5
2990	4	-4476	1	2500	-6.17	0.09	13.77	105.60	153.60	153.60	11
2990	5	-4476	1	2500	-6.17	0.09	13.77	105.60	153.60	153.60	11
2990	6	-4476	1	2500	-6.17	0.09	13.77	105.60	153.60	153.60	11
2990	7	-4476	1	2500	-6.17	0.09	13.77	105.60	153.60	153.60	11
2990	(8+9)-VIII-4	-3523	-152	1588	-4.85	-11.97	8.75	132.00	192.00	192.00	9.2
2990	(8+9)-IV-4	-3506	-149	1706	-4.83	-11.71	9.40	132.00	192.00	192.00	9.0
2990	(8+9)-V-4	-3017	87	2194	-4.16	6.83	12.09	132.00	192.00	192.00	10
2990	(8+9)-II-3	-3490	147	1709	-4.81	11.62	9.41	132.00	192.00	192.00	9.1
2990	(8+9)-I-3	-3205	163	2437	-4.41	12.81	13.42	132.00	192.00	192.00	7.3
2990	(8+9)-II-2	-2687	-145	1735	-3.70	-11.47	9.56	132.00	192.00	192.00	9.1
2990	(8+9)-VI-2	-2671	-142	1853	-3.68	-11.20	10.21	132.00	192.00	192.00	8.9
2990	(8+9)-III-3	-2958	187	2588	-4.07	14.72	14.26	132.00	192.00	192.00	6.6
2990	(8+9)-VI-3	-3506	144	1591	-4.83	11.36	8.76	132.00	192.00	192.00	9.5
2990	(8+9)-IV-1	-2670	151	1738	-3.68	11.86	9.58	132.00	192.00	192.00	8.9
2990	(8+9)-VI-4	-2700	-71	2091	-3.72	-5.62	11.52	132.00	192.00	192.00	11
2990	(8+9)-IV-3	-2668	228	2212	-3.67	17.98	12.19	132.00	192.00	192.00	6.4
2990	(8+9)-I-2	-2972	-161	1007	-4.09	-12.65	5.55	132.00	192.00	192.00	10
2990	(8+9)-V-1	-3160	-85	1250	-4.35	-6.67	6.89	132.00	192.00	192.00	14
2990	(8+9)-VII-2	-3165	-173	1249	-4.36	-13.67	6.88	132.00	192.00	192.00	9.3
2990	(8+9)-V-3	-3259	151	2044	-4.49	11.92	11.26	132.00	192.00	192.00	8.2
2990	(8+9)-VII-3	-3012	175	2195	-4.15	13.83	12.09	132.00	192.00	192.00	7.4
2990	(8+9)-III-2	-3219	-185	856	-4.43	-14.56	4.72	132.00	192.00	192.00	9.9
2990	(8+9)-VII-4	-3264	62	2043	-4.50	4.92	11.26	132.00	192.00	192.00	12
2990	(8+9)-V-2	-2918	-149	1400	-4.02	-11.76	7.71	132.00	192.00	192.00	9.8
2990	(8+9)-II-4	-2684	-68	2209	-3.70	-5.35	12.17	132.00	192.00	192.00	11
2990	(8+9)-III-4	-3210	74	2436	-4.42	5.81	13.42	132.00	192.00	192.00	9.9
2990	(8+9)-I-4	-2963	98	2587	-4.08	7.72	14.25	132.00	192.00	192.00	8.7
2990	(8+9)-VIII-1	-2654	154	1856	-3.66	12.13	10.23	132.00	192.00	192.00	8.6
2990	(8+9)-VIII-2	-3493	-223	1350	-4.81	-17.55	7.44	132.00	192.00	192.00	7.6
2990	(8+9)-VIII-3	-2684	225	2094	-3.70	17.71	11.54	132.00	192.00	192.00	6.5
2990	(8+9)-IV-2	-3509	-226	1232	-4.83	-17.82	6.79	132.00	192.00	192.00	7.8

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
0	(8+9)-IV-2	269	0.09	6.40	Si	71
0	(8+9)-I-4	-537	0.18	6.40	Si	36
0	(8+9)-IV-3	-268	0.09	6.40	Si	71
0	(8+9)-V-2	382	0.13	6.40	Si	50
0	(8+9)-VII-3	-342	0.11	6.40	Si	56
0	(8+9)-II-2	402	0.13	6.40	Si	48
0	(8+9)-VII-1	290	0.10	6.40	Si	66
0	(8+9)-II-3	-401	0.13	6.40	Si	48

X	Comb.	Ty	τ_d	fvd	RS	Cs
0	(8+9)-V-3	-381	0.13	6.40	Si	50
0	(8+9)-V-1	250	0.08	6.40	Si	76
0	(8+9)-I-2	670	0.22	6.40	Si	28
0	(8+9)-III-1	578	0.19	6.40	Si	33
0	(8+9)-VII-4	-289	0.10	6.40	Si	66
0	(8+9)-III-2	631	0.21	6.40	Si	30
0	(8+9)-I-3	-669	0.22	6.40	Si	29
0	(8+9)-VII-2	343	0.11	6.40	Si	56
0	(8+9)-I-1	538	0.18	6.40	Si	35
0	(8+9)-III-3	-630	0.21	6.40	Si	30
0	(8+9)-III-4	-577	0.19	6.40	Si	33
0	(8+9)-V-4	-249	0.08	6.40	Si	77
750	1	3	0.00	3.84	Si	>100
750	2	4	0.00	5.76	Si	>100
750	3	4	0.00	5.76	Si	>100
750	4	3	0.00	5.12	Si	>100
750	5	3	0.00	5.12	Si	>100
750	6	3	0.00	5.12	Si	>100
750	7	3	0.00	5.12	Si	>100
750	(8+9)-IV-1	-180	0.06	6.40	Si	>100
750	(8+9)-VIII-1	-105	0.04	6.40	Si	>100
750	(8+9)-VI-2	418	0.14	6.40	Si	46
750	(8+9)-VIII-2	254	0.09	6.40	Si	75
750	(8+9)-VI-4	273	0.09	6.40	Si	70
750	(8+9)-VIII-3	-250	0.08	6.40	Si	77
750	(8+9)-II-1	-344	0.12	6.40	Si	56
750	(8+9)-IV-4	184	0.06	6.40	Si	>100
750	(8+9)-VI-3	-413	0.14	6.40	Si	46
750	(8+9)-VI-1	-269	0.09	6.40	Si	71
750	(8+9)-II-4	348	0.12	6.40	Si	55
750	(8+9)-VIII-4	109	0.04	6.40	Si	>100
Verifiche nella direzione secondaria						
0	2	-6	0.01	5.76	Si	>100
0	3	-6	0.01	5.76	Si	>100
2990	1	-3	0.00	3.84	Si	>100
2990	4	-3	0.00	5.12	Si	>100
2990	5	-3	0.00	5.12	Si	>100
2990	6	-3	0.00	5.12	Si	>100
2990	7	-3	0.00	5.12	Si	>100
2990	(8+9)-VIII-4	-218	0.28	6.40	Si	23
2990	(8+9)-IV-3	301	0.38	6.40	Si	17
2990	(8+9)-V-1	66	0.08	6.40	Si	77
2990	(8+9)-I-2	-360	0.46	6.40	Si	14
2990	(8+9)-V-2	-109	0.14	6.40	Si	46
2990	(8+9)-I-4	181	0.23	6.40	Si	28
2990	(8+9)-V-3	105	0.13	6.40	Si	48
2990	(8+9)-II-2	-374	0.48	6.40	Si	13
2990	(8+9)-V-4	-69	0.09	6.40	Si	72
2990	(8+9)-II-4	-212	0.27	6.40	Si	24
2990	(8+9)-VI-1	283	0.36	6.40	Si	18
2990	(8+9)-III-2	-339	0.43	6.40	Si	15
2990	(8+9)-VI-2	-299	0.38	6.40	Si	17
2990	(8+9)-III-4	202	0.26	6.40	Si	25
2990	(8+9)-VI-3	295	0.38	6.40	Si	17
2990	(8+9)-IV-2	-305	0.39	6.40	Si	16
2990	(8+9)-VI-4	-287	0.37	6.40	Si	18
2990	(8+9)-IV-4	-143	0.18	6.40	Si	35
2990	(8+9)-VII-1	45	0.06	6.40	Si	>100
2990	(8+9)-II-1	208	0.26	6.40	Si	24
2990	(8+9)-VII-2	-88	0.11	6.40	Si	57
2990	(8+9)-III-1	-206	0.26	6.40	Si	24
2990	(8+9)-VII-3	84	0.11	6.40	Si	60
2990	(8+9)-IV-1	139	0.18	6.40	Si	36
2990	(8+9)-VII-4	-49	0.06	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
2990	(8+9)-III-3	335	0.43	6.40	Si	15
2990	(8+9)-I-1	-185	0.24	6.40	Si	27
2990	(8+9)-II-3	370	0.47	6.40	Si	14
2990	(8+9)-VIII-1	214	0.27	6.40	Si	24
2990	(8+9)-VIII-2	-230	0.29	6.40	Si	22
2990	(8+9)-VIII-3	226	0.29	6.40	Si	22
2990	(8+9)-I-3	356	0.45	6.40	Si	14

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
750	1	-1380	-0.95	19.20	20	-0.23	12.00	52	V	20
750	2	-2343	-1.62	28.80	18	-0.39	18.00	46	V	18
750	3	-2343	-1.62	28.80	18	-0.39	18.00	46	V	18
750	4	-1380	-0.95	25.60	27	-0.23	16.00	69	V	27
750	5	-1380	-0.95	25.60	27	-0.23	16.00	69	V	27
750	6	-1380	-0.95	25.60	27	-0.23	16.00	69	V	27
750	7	-1380	-0.95	25.60	27	-0.23	16.00	69	V	27
750	(8+9)-VIII-4	-2980	-2.06	32.00	16	-0.50	20.00	40	V	16
750	(8+9)-V-3	-2723	-1.88	32.00	17	-0.46	20.00	44	V	17
750	(8+9)-VI-4	-3204	-2.21	32.00	14	-0.54	20.00	37	V	14
750	(8+9)-III-3	-4256	-2.94	32.00	11	-0.71	20.00	28	V	11
750	(8+9)-I-4	-5145	-3.56	32.00	9.0	-0.86	20.00	23	V	9.0
750	(8+9)-III-4	-5078	-3.51	32.00	9.1	-0.85	20.00	24	V	9.1
750	(8+9)-II-2	-1400	-0.97	32.00	33	-0.23	20.00	85	V	33
750	(8+9)-VI-2	-1840	-1.27	32.00	25	-0.31	20.00	65	V	25
750	(8+9)-II-4	-3643	-2.52	32.00	13	-0.61	20.00	33	V	13
750	(8+9)-IV-2	-1177	-0.81	32.00	39	-0.20	20.00	>100	V	39
750	(8+9)-I-3	-4189	-2.89	32.00	11	-0.70	20.00	29	V	11
750	(8+9)-VII-4	-3612	-2.50	32.00	13	-0.60	20.00	33	V	13
750	(8+9)-VII-3	-2790	-1.93	32.00	17	-0.47	20.00	43	V	17
750	(8+9)-VIII-2	-1617	-1.12	32.00	29	-0.27	20.00	74	V	29
750	(8+9)-V-4	-3679	-2.54	32.00	13	-0.62	20.00	33	V	13
750	(8+9)-IV-4	-3420	-2.36	32.00	14	-0.57	20.00	35	V	14
1500	(8+9)-V-1	2932	2.03	32.00	16	0.49	20.00	41	V	16
1500	(8+9)-IV-1	3090	2.14	32.00	15	0.52	20.00	39	V	15
1500	(8+9)-I-2	3593	2.48	32.00	13	0.60	20.00	33	V	13
1500	(8+9)-VII-2	2197	1.52	32.00	21	0.37	20.00	54	V	21
1500	(8+9)-V-2	2227	1.54	32.00	21	0.37	20.00	54	V	21
1500	(8+9)-III-1	4328	2.99	32.00	11	0.72	20.00	28	V	11
1500	(8+9)-VI-1	2578	1.78	32.00	18	0.43	20.00	46	V	18
1500	(8+9)-II-3	1160	0.80	32.00	40	0.19	20.00	>100	V	40
1500	(8+9)-VII-1	2963	2.05	32.00	16	0.50	20.00	40	V	16
1500	(8+9)-IV-3	1263	0.87	32.00	37	0.21	20.00	95	V	37
1500	(8+9)-I-1	4297	2.97	32.00	11	0.72	20.00	28	V	11
1500	(8+9)-III-2	3562	2.46	32.00	13	0.60	20.00	34	V	13
1500	(8+9)-VIII-1	2681	1.85	32.00	17	0.45	20.00	45	V	17
1500	(8+9)-II-1	2987	2.06	32.00	16	0.50	20.00	40	V	16
1500	(8+9)-VIII-3	1673	1.16	32.00	28	0.28	20.00	71	V	28
1500	(8+9)-VI-3	1570	1.08	32.00	29	0.26	20.00	76	V	29
Verifiche nella direzione secondaria										
1495	(8+9)-VIII-4	-1387	-1.91	32.00	17	-0.46	20.00	43	V	17
1495	(8+9)-IV-4	-1597	-2.20	32.00	15	-0.53	20.00	38	V	15
1495	(8+9)-II-1	1240	1.71	32.00	19	0.41	20.00	48	V	19
1495	(8+9)-V-3	-1216	-1.67	32.00	19	-0.41	20.00	49	V	19
1495	(8+9)-VIII-1	999	1.38	32.00	23	0.33	20.00	60	V	23
1495	(8+9)-V-2	828	1.14	32.00	28	0.28	20.00	72	V	28
1495	(8+9)-VII-2	838	1.15	32.00	28	0.28	20.00	72	V	28
1495	(8+9)-V-1	1334	1.84	32.00	17	0.44	20.00	45	V	17
1495	(8+9)-I-1	2033	2.80	32.00	11	0.68	20.00	30	V	11
1495	(8+9)-III-1	2023	2.79	32.00	11	0.67	20.00	30	V	11
1495	(8+9)-I-3	-1915	-2.64	32.00	12	-0.64	20.00	31	V	12
1495	(8+9)-III-2	1537	2.12	32.00	15	0.51	20.00	39	V	15

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
1495	(8+9)-VIII-2	-622	-0.86	32.00	37	-0.21	20.00	96	V	37
1495	(8+9)-III-3	-1924	-2.65	32.00	12	-0.64	20.00	31	V	12
1495	(8+9)-VII-1	1324	1.82	32.00	18	0.44	20.00	45	V	18
1495	(8+9)-I-4	-2420	-3.33	32.00	9.6	-0.81	20.00	25	V	9.6
1495	(8+9)-VII-4	-1712	-2.36	32.00	14	-0.57	20.00	35	V	14
1495	(8+9)-I-2	1527	2.10	32.00	15	0.51	20.00	39	V	15
1495	(8+9)-III-4	-2411	-3.32	32.00	9.6	-0.80	20.00	25	V	9.6
1495	(8+9)-IV-1	1209	1.67	32.00	19	0.40	20.00	50	V	19
2990	1	-622	-0.86	19.20	22	-0.21	12.00	58	V	22
2990	2	-1047	-1.44	28.80	20	-0.35	18.00	52	V	20
2990	3	-1047	-1.44	28.80	20	-0.35	18.00	52	V	20
2990	4	-622	-0.86	25.60	30	-0.21	16.00	77	V	30
2990	5	-622	-0.86	25.60	30	-0.21	16.00	77	V	30
2990	6	-622	-0.86	25.60	30	-0.21	16.00	77	V	30
2990	7	-622	-0.86	25.60	30	-0.21	16.00	77	V	30
2990	(8+9)-IV-2	-420	-0.58	32.00	55	-0.14	20.00	>100	V	55
2990	(8+9)-VI-4	-1874	-2.58	32.00	12	-0.62	20.00	32	V	12
2990	(8+9)-IV-3	-421	-0.58	32.00	55	-0.14	20.00	>100	V	55
2990	(8+9)-II-2	-1190	-1.64	32.00	20	-0.40	20.00	50	V	20
2990	(8+9)-VI-1	1033	1.42	32.00	22	0.34	20.00	58	V	22
2990	(8+9)-V-4	-1873	-2.58	32.00	12	-0.62	20.00	32	V	12
2990	(8+9)-VII-3	-1433	-1.97	32.00	16	-0.48	20.00	42	V	16
2990	(8+9)-VI-2	-1204	-1.66	32.00	19	-0.40	20.00	50	V	19
2990	(8+9)-II-3	349	0.48	32.00	67	0.12	20.00	>100	V	67
2990	(8+9)-II-4	-1888	-2.60	32.00	12	-0.63	20.00	32	V	12
2990	(8+9)-VIII-3	-407	-0.56	32.00	57	-0.14	20.00	>100	V	57
2990	(8+9)-VI-3	363	0.50	32.00	64	0.12	20.00	>100	V	64

Setto 51: origine (1236.9,549.5,149.5), direzione (0.930013,0.367526,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
2646	1	-298	9	336	-0.14	0.16	0.31	79.20	115.20	115.20	>100
2646	2	-519	16	576	-0.24	0.27	0.53	118.80	172.80	172.80	>100
2646	3	-519	16	576	-0.24	0.27	0.53	118.80	172.80	172.80	>100
2646	4	-298	9	336	-0.14	0.16	0.31	105.60	153.60	153.60	>100
2646	5	-298	9	336	-0.14	0.16	0.31	105.60	153.60	153.60	>100
2646	6	-298	9	336	-0.14	0.16	0.31	105.60	153.60	153.60	>100
2646	7	-298	9	336	-0.14	0.16	0.31	105.60	153.60	153.60	>100
5291	(8+9)-VIII-4	-337	370	916	-0.16	6.40	0.85	132.00	192.00	192.00	26
5291	(8+9)-IV-1	257	-420	-887	0.12	-7.27	-0.82	132.00	192.00	192.00	23
5291	(8+9)-V-1	284	-413	-1033	0.13	-7.14	-0.96	132.00	192.00	192.00	23
5291	(8+9)-I-2	134	-502	-1007	0.06	-8.69	-0.93	132.00	192.00	192.00	20
5291	(8+9)-V-2	166	-419	-740	0.08	-7.24	-0.68	132.00	192.00	192.00	24
5291	(8+9)-I-4	-322	471	1409	-0.15	8.16	1.30	132.00	192.00	192.00	20
5291	(8+9)-V-3	-236	394	849	-0.11	6.82	0.79	132.00	192.00	192.00	25
5291	(8+9)-II-2	-164	-168	180	-0.08	-2.91	0.17	132.00	192.00	192.00	62
5291	(8+9)-V-4	-355	388	1142	-0.16	6.71	1.06	132.00	192.00	192.00	25
5291	(8+9)-II-4	-301	124	905	-0.14	2.14	0.84	132.00	192.00	192.00	64
5291	(8+9)-VI-1	240	-123	-716	0.11	-2.14	-0.66	132.00	192.00	192.00	65
5291	(8+9)-III-2	126	-421	-979	0.06	-7.28	-0.91	132.00	192.00	192.00	23
5291	(8+9)-VI-2	-154	-143	260	-0.07	-2.48	0.24	132.00	192.00	192.00	71
5291	(8+9)-III-4	-330	553	1436	-0.15	9.57	1.33	132.00	192.00	192.00	18
5291	(8+9)-VI-3	84	119	-151	0.04	2.05	-0.14	132.00	192.00	192.00	85
5291	(8+9)-IV-2	-191	103	272	-0.09	1.78	0.25	132.00	192.00	192.00	94
5291	(8+9)-VI-4	-310	99	825	-0.14	1.71	0.76	132.00	192.00	192.00	78
5291	(8+9)-IV-4	-328	395	996	-0.15	6.84	0.92	132.00	192.00	192.00	25
5291	(8+9)-VII-1	292	-494	-1061	0.13	-8.55	-0.98	132.00	192.00	192.00	20
5291	(8+9)-II-1	230	-149	-796	0.11	-2.57	-0.74	132.00	192.00	192.00	55
5291	(8+9)-VII-2	158	-337	-713	0.07	-5.83	-0.66	132.00	192.00	192.00	29
5291	(8+9)-III-1	260	-578	-1327	0.12	-10.00	-1.23	132.00	192.00	192.00	17
5291	(8+9)-VII-3	-228	312	822	-0.11	5.41	0.76	132.00	192.00	192.00	31
5291	(8+9)-I-1	252	-496	-1300	0.12	-8.59	-1.20	132.00	192.00	192.00	19

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
5291	(8+9)-VII-4	-363	469	1170	-0.17	8.12	1.08	132.00	192.00	192.00	21
5291	(8+9)-III-3	-196	396	1089	-0.09	6.85	1.01	132.00	192.00	192.00	24
5291	(8+9)-IV-3	120	-128	-162	0.06	-2.21	-0.15	132.00	192.00	192.00	79
5291	(8+9)-II-3	93	144	-71	0.04	2.48	-0.07	132.00	192.00	192.00	73
5291	(8+9)-VIII-1	267	-395	-807	0.12	-6.83	-0.75	132.00	192.00	192.00	25
5291	(8+9)-VIII-2	-181	128	352	-0.08	2.22	0.32	132.00	192.00	192.00	76
5291	(8+9)-VIII-3	111	-153	-242	0.05	-2.65	-0.22	132.00	192.00	192.00	65
5291	(8+9)-I-3	-204	477	1116	-0.09	8.26	1.03	132.00	192.00	192.00	21
Verifiche nella direzione secondaria											
0	(8+9)-VIII-4	-9880	260	-9180	-3.86	5.81	-4.07	132.00	192.00	192.00	19
0	(8+9)-VI-2	-9389	681	-6030	-3.67	15.21	-2.67	132.00	192.00	192.00	11
0	(8+9)-III-1	-8640	782	5946	-3.37	17.47	2.63	132.00	192.00	192.00	9.5
0	(8+9)-IV-2	-9376	722	-4575	-3.66	16.13	-2.03	132.00	192.00	192.00	11
0	(8+9)-III-2	-8578	1047	4099	-3.35	23.40	1.82	132.00	192.00	192.00	7.6
0	(8+9)-VIII-2	-9618	639	-5556	-3.76	14.27	-2.46	132.00	192.00	192.00	11
0	(8+9)-III-3	-11127	-1034	-12677	-4.35	-23.10	-5.61	132.00	192.00	192.00	6.7
0	(8+9)-VII-3	-10320	-757	-9405	-4.03	-16.91	-4.16	132.00	192.00	192.00	9.1
0	(8+9)-III-4	-11065	-768	-14524	-4.32	-17.17	-6.43	132.00	192.00	192.00	8.1
0	(8+9)-I-1	-8709	769	6088	-3.40	17.18	2.70	132.00	192.00	192.00	9.6
0	(8+9)-VI-4	-9650	302	-9654	-3.77	6.76	-4.27	132.00	192.00	192.00	17
0	(8+9)-I-3	-11196	-1047	-12535	-4.37	-23.38	-5.55	132.00	192.00	192.00	6.6
0	(8+9)-VII-1	-9448	505	2674	-3.69	11.27	1.18	132.00	192.00	192.00	15
0	(8+9)-IV-3	-10329	-708	-4004	-4.03	-15.83	-1.77	132.00	192.00	192.00	11
0	(8+9)-II-3	-10559	-751	-3530	-4.12	-16.77	-1.56	132.00	192.00	192.00	10
0	(8+9)-IV-4	-10122	177	-10161	-3.95	3.96	-4.50	132.00	192.00	192.00	22
0	(8+9)-VIII-3	-10087	-625	-3022	-3.94	-13.97	-1.34	132.00	192.00	192.00	12
0	(8+9)-V-1	-9516	492	2816	-3.72	10.99	1.25	132.00	192.00	192.00	16
0	(8+9)-VII-2	-9385	770	827	-3.66	17.21	0.37	132.00	192.00	192.00	11
0	(8+9)-V-2	-9316	783	684	-3.64	17.49	0.30	132.00	192.00	192.00	11
0	(8+9)-I-4	-10996	-756	-14667	-4.29	-16.88	-6.49	132.00	192.00	192.00	8.2
0	(8+9)-II-4	-9892	219	-10636	-3.86	4.90	-4.71	132.00	192.00	192.00	20
0	(8+9)-VII-4	-10257	-491	-11252	-4.01	-10.97	-4.98	132.00	192.00	192.00	12
0	(8+9)-I-2	-8509	1060	3957	-3.32	23.68	1.75	132.00	192.00	192.00	7.5
0	(8+9)-II-2	-9146	764	-5049	-3.57	17.07	-2.24	132.00	192.00	192.00	9.9
0	(8+9)-V-3	-10389	-769	-9263	-4.06	-17.19	-4.10	132.00	192.00	192.00	9.0
0	(8+9)-V-4	-10189	-478	-11395	-3.98	-10.69	-5.05	132.00	192.00	192.00	12
0	(8+9)-VI-3	-10316	-667	-2548	-4.03	-14.91	-1.13	132.00	192.00	192.00	12
1495	1	-13634	-6	-6859	-5.32	-0.13	-3.04	79.20	115.20	115.20	34
1495	2	-21367	-5	-10637	-8.34	-0.12	-4.71	118.80	172.80	172.80	33
1495	3	-21367	-5	-10637	-8.34	-0.12	-4.71	118.80	172.80	172.80	33
1495	4	-13634	-6	-6859	-5.32	-0.13	-3.04	105.60	153.60	153.60	46
1495	5	-13634	-6	-6859	-5.32	-0.13	-3.04	105.60	153.60	153.60	46
1495	6	-13634	-6	-6859	-5.32	-0.13	-3.04	105.60	153.60	153.60	46
1495	7	-13634	-6	-6859	-5.32	-0.13	-3.04	105.60	153.60	153.60	46
2990	(8+9)-VIII-1	-8707	255	-6253	-3.40	5.71	-2.77	132.00	192.00	192.00	22
2990	(8+9)-II-1	-8967	249	-5757	-3.50	5.56	-2.55	132.00	192.00	192.00	23
2990	(8+9)-IV-1	-8498	240	-6317	-3.32	5.35	-2.80	132.00	192.00	192.00	23
2990	(8+9)-VI-1	-9176	265	-5693	-3.58	5.92	-2.52	132.00	192.00	192.00	23

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X	Comb.	Ty	τ_d	fvd	RS	Cs
mm		kg	kg/cmq	kg/cmq		
0	(8+9)-VI-1	12	0.00	6.40	Si	>100
0	(8+9)-VI-4	-11	0.00	6.40	Si	>100
2646	1	12	0.00	3.84	Si	>100
2646	2	20	0.01	5.76	Si	>100
2646	3	20	0.01	5.76	Si	>100
2646	4	12	0.00	5.12	Si	>100
2646	5	12	0.00	5.12	Si	>100
2646	6	12	0.00	5.12	Si	>100
2646	7	12	0.00	5.12	Si	>100
5291	(8+9)-VIII-4	20	0.01	6.40	Si	>100
5291	(8+9)-IV-1	-87	0.03	6.40	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
5291	(8+9)-V-2	259	0.09	6.40	Si	74
5291	(8+9)-I-4	-54	0.02	6.40	Si	>100
5291	(8+9)-V-3	-274	0.09	6.40	Si	70
5291	(8+9)-II-2	88	0.03	6.40	Si	>100
5291	(8+9)-V-4	-229	0.08	6.40	Si	83
5291	(8+9)-II-4	46	0.02	6.40	Si	>100
5291	(8+9)-I-2	84	0.03	6.40	Si	>100
5291	(8+9)-III-2	93	0.03	6.40	Si	>100
5291	(8+9)-VI-2	140	0.05	6.40	Si	>100
5291	(8+9)-III-4	-46	0.02	6.40	Si	>100
5291	(8+9)-VI-3	-154	0.05	6.40	Si	>100
5291	(8+9)-IV-2	115	0.04	6.40	Si	>100
5291	(8+9)-I-1	40	0.01	6.40	Si	>100
5291	(8+9)-IV-4	73	0.02	6.40	Si	>100
5291	(8+9)-VII-1	207	0.07	6.40	Si	92
5291	(8+9)-II-1	-60	0.02	6.40	Si	>100
5291	(8+9)-VII-2	268	0.09	6.40	Si	71
5291	(8+9)-III-1	32	0.01	6.40	Si	>100
5291	(8+9)-VII-3	-282	0.09	6.40	Si	68
5291	(8+9)-I-3	-99	0.03	6.40	Si	>100
5291	(8+9)-VII-4	-221	0.07	6.40	Si	86
5291	(8+9)-III-3	-107	0.04	6.40	Si	>100
5291	(8+9)-IV-3	-129	0.04	6.40	Si	>100
5291	(8+9)-II-3	-102	0.03	6.40	Si	>100
5291	(8+9)-VIII-1	-35	0.01	6.40	Si	>100
5291	(8+9)-VIII-2	167	0.06	6.40	Si	>100
5291	(8+9)-VIII-3	-181	0.06	6.40	Si	>100
5291	(8+9)-V-1	215	0.07	6.40	Si	89
Verifiche nella direzione secondaria						
0	(8+9)-VIII-4	-306	0.11	6.40	Si	58
0	(8+9)-VI-2	-434	0.16	6.40	Si	41
0	(8+9)-III-1	-293	0.11	6.40	Si	61
0	(8+9)-IV-2	-458	0.17	6.40	Si	39
0	(8+9)-III-2	-493	0.18	6.40	Si	36
0	(8+9)-VIII-2	-380	0.14	6.40	Si	47
0	(8+9)-III-3	474	0.17	6.40	Si	37
0	(8+9)-III-4	273	0.10	6.40	Si	65
0	(8+9)-I-1	-277	0.10	6.40	Si	64
0	(8+9)-VI-4	-360	0.13	6.40	Si	49
0	(8+9)-VIII-1	287	0.10	6.40	Si	62
0	(8+9)-I-3	490	0.18	6.40	Si	36
0	(8+9)-VI-1	341	0.12	6.40	Si	52
0	(8+9)-II-1	263	0.09	6.40	Si	68
0	(8+9)-I-2	-509	0.18	6.40	Si	35
0	(8+9)-VIII-3	361	0.13	6.40	Si	49
0	(8+9)-I-4	257	0.09	6.40	Si	69
0	(8+9)-II-2	-512	0.18	6.40	Si	35
0	(8+9)-II-4	-282	0.10	6.40	Si	63
0	(8+9)-II-3	492	0.18	6.40	Si	36
0	(8+9)-VI-3	415	0.15	6.40	Si	43
0	(8+9)-IV-3	439	0.16	6.40	Si	40
1495	(8+9)-VII-4	113	0.04	6.40	Si	>100
1495	(8+9)-VII-1	-131	0.05	6.40	Si	>100
1495	(8+9)-V-2	-295	0.11	6.40	Si	60
1495	(8+9)-V-3	277	0.10	6.40	Si	64
1495	(8+9)-VII-2	-285	0.10	6.40	Si	62
1495	(8+9)-VII-3	267	0.10	6.40	Si	66
2990	1	-23	0.01	3.84	Si	>100
2990	2	-37	0.01	5.76	Si	>100
2990	3	-37	0.01	5.76	Si	>100
2990	4	-23	0.01	5.12	Si	>100
2990	5	-23	0.01	5.12	Si	>100
2990	6	-23	0.01	5.12	Si	>100
2990	7	-23	0.01	5.12	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
2990	(8+9)-IV-1	270	0.10	6.40	Si	66
2990	(8+9)-IV-4	-301	0.11	6.40	Si	59
2990	(8+9)-V-1	-170	0.06	6.40	Si	>100
2990	(8+9)-V-4	139	0.05	6.40	Si	>100

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	(8+9)-III-1	3354	2.32	32.00	14	0.56	20.00	36	V	14
0	(8+9)-V-1	2312	1.60	32.00	20	0.39	20.00	52	V	20
0	(8+9)-IV-1	2203	1.52	32.00	21	0.37	20.00	54	V	21
0	(8+9)-I-1	3391	2.34	32.00	14	0.57	20.00	35	V	14
0	(8+9)-VII-1	2276	1.57	32.00	20	0.38	20.00	53	V	20
0	(8+9)-V-2	1536	1.06	32.00	30	0.26	20.00	78	V	30
0	(8+9)-VIII-3	836	0.58	32.00	55	0.14	20.00	>100	V	55
0	(8+9)-VII-2	1572	1.09	32.00	29	0.26	20.00	76	V	29
0	(8+9)-I-2	2615	1.81	32.00	18	0.44	20.00	46	V	18
0	(8+9)-VIII-1	1879	1.30	32.00	25	0.31	20.00	64	V	25
0	(8+9)-III-2	2651	1.83	32.00	17	0.44	20.00	45	V	17
2646	1	-1661	-1.15	19.20	17	-0.28	12.00	43	V	17
2646	2	-2531	-1.75	28.80	16	-0.42	18.00	43	V	16
2646	3	-2531	-1.75	28.80	16	-0.42	18.00	43	V	16
2646	4	-1661	-1.15	25.60	22	-0.28	16.00	58	V	22
2646	5	-1661	-1.15	25.60	22	-0.28	16.00	58	V	22
2646	6	-1661	-1.15	25.60	22	-0.28	16.00	58	V	22
2646	7	-1661	-1.15	25.60	22	-0.28	16.00	58	V	22
2646	(8+9)-VIII-4	-3518	-2.43	32.00	13	-0.59	20.00	34	V	13
2646	(8+9)-V-3	-3062	-2.12	32.00	15	-0.51	20.00	39	V	15
2646	(8+9)-II-2	-1701	-1.18	32.00	27	-0.28	20.00	70	V	27
2646	(8+9)-IV-2	-1645	-1.14	32.00	28	-0.28	20.00	73	V	28
2646	(8+9)-VI-4	-3574	-2.47	32.00	13	-0.60	20.00	33	V	13
2646	(8+9)-IV-4	-3944	-2.73	32.00	12	-0.66	20.00	30	V	12
2646	(8+9)-I-4	-5497	-3.80	32.00	8.4	-0.92	20.00	22	V	8.4
2646	(8+9)-III-4	-5480	-3.79	32.00	8.5	-0.92	20.00	22	V	8.5
2646	(8+9)-II-4	-4000	-2.76	32.00	12	-0.67	20.00	30	V	12
2646	(8+9)-III-3	-4498	-3.11	32.00	10	-0.75	20.00	27	V	10
2646	(8+9)-VI-2	-2127	-1.47	32.00	22	-0.36	20.00	56	V	22
2646	(8+9)-IV-3	-671	-0.46	32.00	69	-0.11	20.00	>100	V	69
2646	(8+9)-I-3	-4482	-3.10	32.00	10	-0.75	20.00	27	V	10
2646	(8+9)-VIII-2	-2071	-1.43	32.00	22	-0.35	20.00	58	V	22
2646	(8+9)-V-4	-4078	-2.82	32.00	11	-0.68	20.00	29	V	11
2646	(8+9)-VII-3	-3079	-2.13	32.00	15	-0.51	20.00	39	V	15
2646	(8+9)-VII-4	-4061	-2.81	32.00	11	-0.68	20.00	29	V	11
5291	(8+9)-VI-3	1313	0.91	32.00	35	0.22	20.00	91	V	35
5291	(8+9)-VI-1	2048	1.42	32.00	23	0.34	20.00	58	V	23
5291	(8+9)-II-3	1015	0.70	32.00	46	0.17	20.00	>100	V	46
5291	(8+9)-II-1	2345	1.62	32.00	20	0.39	20.00	51	V	20
Verifiche nella direzione secondaria										
1495	1	311	0.12	19.20	>100	0.03	12.00	>100	V	>100
1495	2	582	0.23	28.80	>100	0.05	18.00	>100	V	>100
1495	3	582	0.23	28.80	>100	0.05	18.00	>100	V	>100
1495	4	311	0.12	25.60	>100	0.03	16.00	>100	V	>100
1495	5	311	0.12	25.60	>100	0.03	16.00	>100	V	>100
1495	6	311	0.12	25.60	>100	0.03	16.00	>100	V	>100
1495	7	311	0.12	25.60	>100	0.03	16.00	>100	V	>100
1495	(8+9)-VI-1	5128	2.00	32.00	16	0.48	20.00	41	V	16
1495	(8+9)-II-4	-5578	-2.18	32.00	15	-0.53	20.00	38	V	15
1495	(8+9)-III-4	-8195	-3.20	32.00	10	-0.77	20.00	26	V	10
1495	(8+9)-I-2	6504	2.54	32.00	13	0.61	20.00	33	V	13
1495	(8+9)-VII-2	3721	1.45	32.00	22	0.35	20.00	57	V	22
1495	(8+9)-I-4	-8244	-3.22	32.00	9.9	-0.78	20.00	26	V	9.9
1495	(8+9)-VII-4	-5362	-2.09	32.00	15	-0.51	20.00	39	V	15
1495	(8+9)-VII-1	5762	2.25	32.00	14	0.54	20.00	37	V	14

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
1495	(8+9)-I-1	8643	3.38	32.00	9.5	0.82	20.00	24	V	9.5
1495	(8+9)-VI-4	-4729	-1.85	32.00	17	-0.45	20.00	45	V	17
1495	(8+9)-III-2	6554	2.56	32.00	13	0.62	20.00	32	V	13
1495	(8+9)-V-1	5811	2.27	32.00	14	0.55	20.00	36	V	14
1495	(8+9)-I-3	-6105	-2.38	32.00	13	-0.58	20.00	35	V	13
1495	(8+9)-VII-3	-3322	-1.30	32.00	25	-0.31	20.00	64	V	25
1495	(8+9)-III-1	8594	3.36	32.00	9.5	0.81	20.00	25	V	9.5
1495	(8+9)-III-3	-6154	-2.40	32.00	13	-0.58	20.00	34	V	13
1495	(8+9)-II-1	5978	2.33	32.00	14	0.56	20.00	35	V	14
1495	(8+9)-V-2	3672	1.43	32.00	22	0.35	20.00	58	V	22
1495	(8+9)-V-3	-3273	-1.28	32.00	25	-0.31	20.00	65	V	25
1495	(8+9)-V-4	-5412	-2.11	32.00	15	-0.51	20.00	39	V	15
2990	(8+9)-VIII-4	-4868	-1.90	32.00	17	-0.46	20.00	43	V	17
2990	(8+9)-IV-2	-2106	-0.82	32.00	39	-0.20	20.00	>100	V	39
2990	(8+9)-II-3	1619	0.63	32.00	51	0.15	20.00	>100	V	51
2990	(8+9)-VI-2	-2125	-0.83	32.00	39	-0.20	20.00	100	V	39
2990	(8+9)-II-2	-1225	-0.48	32.00	67	-0.12	20.00	>100	V	67
2990	(8+9)-IV-1	6163	2.41	32.00	13	0.58	20.00	34	V	13
2990	(8+9)-VI-3	2520	0.98	32.00	33	0.24	20.00	84	V	33
2990	(8+9)-IV-3	2500	0.98	32.00	33	0.24	20.00	85	V	33
2990	(8+9)-VIII-1	5262	2.05	32.00	16	0.50	20.00	40	V	16
2990	(8+9)-VIII-2	-3006	-1.17	32.00	27	-0.28	20.00	70	V	27
2990	(8+9)-VIII-3	3401	1.33	32.00	24	0.32	20.00	62	V	24
2990	(8+9)-IV-4	-5768	-2.25	32.00	14	-0.55	20.00	37	V	14

Setto 52: origine (1162.5,520.1,254.5), direzione (0.930013,0.367526,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X mm	Comb.	N kg	Mx kg*m	My kg*m	σ_n kg/cmq	σ_{mx} kg/cmq	σ_{my} kg/cmq	ftd kg/cmq	fcd kg/cmq	fmd kg/cmq	Cs
0	1	690	-4	138	1.07	-0.21	1.44	79.20	115.20	115.20	36
0	2	1031	-7	213	1.60	-0.41	2.22	118.80	172.80	172.80	35
0	3	1031	-7	213	1.60	-0.41	2.22	118.80	172.80	172.80	35
0	4	690	-4	138	1.07	-0.21	1.44	105.60	153.60	153.60	48
0	5	690	-4	138	1.07	-0.21	1.44	105.60	153.60	153.60	48
0	6	690	-4	138	1.07	-0.21	1.44	105.60	153.60	153.60	48
0	7	690	-4	138	1.07	-0.21	1.44	105.60	153.60	153.60	48
0	(8+9)-IV-1	203	-19	518	0.31	-1.09	5.40	132.00	192.00	192.00	28
0	(8+9)-V-1	952	38	294	1.47	2.23	3.07	132.00	192.00	192.00	26
0	(8+9)-I-2	167	72	475	0.26	4.20	4.96	132.00	192.00	192.00	20
0	(8+9)-V-2	980	54	136	1.52	3.13	1.42	132.00	192.00	192.00	28
0	(8+9)-I-4	838	-62	-441	1.30	-3.58	-4.60	132.00	192.00	192.00	19
0	(8+9)-VII-2	1022	57	130	1.58	3.32	1.36	132.00	192.00	192.00	28
0	(8+9)-IV-4	774	14	-325	1.20	0.81	-3.39	132.00	192.00	192.00	32
0	(8+9)-II-2	435	44	-30	0.67	2.53	-0.31	132.00	192.00	192.00	50
0	(8+9)-I-3	810	-77	-283	1.25	-4.48	-2.95	132.00	192.00	192.00	21
0	(8+9)-VIII-3	160	-53	344	0.25	-3.11	3.59	132.00	192.00	192.00	27
0	(8+9)-II-1	340	-8	497	0.53	-0.49	5.19	132.00	192.00	192.00	30
0	(8+9)-III-2	208	75	469	0.32	4.38	4.90	132.00	192.00	192.00	20
0	(8+9)-III-4	879	-58	-447	1.36	-3.40	-4.66	132.00	192.00	192.00	19
0	(8+9)-VIII-2	816	48	-152	1.26	2.82	-1.59	132.00	192.00	192.00	31
0	(8+9)-IV-2	572	54	-50	0.89	3.14	-0.52	132.00	192.00	192.00	39
0	(8+9)-VI-1	584	-14	395	0.90	-0.81	4.13	132.00	192.00	192.00	31
0	(8+9)-II-3	541	-48	222	0.84	-2.82	2.32	132.00	192.00	192.00	30
0	(8+9)-VI-2	679	38	-132	1.05	2.21	-1.37	132.00	192.00	192.00	38
0	(8+9)-III-3	769	-80	-277	1.19	-4.67	-2.89	132.00	192.00	192.00	21
0	(8+9)-IV-3	404	-59	243	0.63	-3.43	2.53	132.00	192.00	192.00	28
0	(8+9)-III-1	97	53	640	0.15	3.11	6.67	132.00	192.00	192.00	19
0	(8+9)-I-1	138	57	633	0.21	3.29	6.61	132.00	192.00	192.00	19
0	(8+9)-VI-3	297	-43	324	0.46	-2.50	3.38	132.00	192.00	192.00	29
0	(8+9)-VIII-1	447	-24	416	0.69	-1.41	4.34	132.00	192.00	192.00	28
0	(8+9)-VII-1	911	35	300	1.41	2.05	3.13	132.00	192.00	192.00	27
800	(8+9)-VIII-4	560	27	198	0.87	1.60	2.07	132.00	192.00	192.00	39
800	(8+9)-VII-3	-398	-39	304	-0.62	-2.24	3.17	132.00	192.00	192.00	35

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
800	(8+9)-VII-4	67	-17	376	0.10	-0.96	3.92	132.00	192.00	192.00	38
800	(8+9)-VI-4	422	20	220	0.65	1.18	2.30	132.00	192.00	192.00	43
800	(8+9)-V-4	25	-19	383	0.04	-1.09	3.99	132.00	192.00	192.00	37
800	(8+9)-II-4	809	20	218	1.25	1.19	2.27	132.00	192.00	192.00	36
800	(8+9)-V-3	-356	-36	297	-0.55	-2.12	3.10	132.00	192.00	192.00	37
Verifiche nella direzione secondaria											
890	1	-3694	1	-1630	-9.54	0.21	-31.57	79.20	115.20	115.20	3.5
890	2	-5888	5	-2592	-15.21	0.69	-50.20	118.80	172.80	172.80	3.3
890	3	-5888	5	-2592	-15.21	0.69	-50.20	118.80	172.80	172.80	3.3
890	4	-3694	1	-1630	-9.54	0.21	-31.57	105.60	153.60	153.60	4.7
890	5	-3694	1	-1630	-9.54	0.21	-31.57	105.60	153.60	153.60	4.7
890	6	-3694	1	-1630	-9.54	0.21	-31.57	105.60	153.60	153.60	4.7
890	7	-3694	1	-1630	-9.54	0.21	-31.57	105.60	153.60	153.60	4.7
890	(8+9)-VIII-4	-2163	-87	-870	-5.59	-12.88	-16.85	132.00	192.00	192.00	6.4
890	(8+9)-IV-2	-2126	-155	-956	-5.49	-22.93	-18.52	132.00	192.00	192.00	4.6
890	(8+9)-V-1	-2617	-53	-1316	-6.76	-7.77	-25.50	132.00	192.00	192.00	5.7
890	(8+9)-I-2	-2359	-172	-1222	-6.09	-25.43	-23.67	132.00	192.00	192.00	3.9
890	(8+9)-V-2	-2450	-108	-1171	-6.33	-15.97	-22.69	132.00	192.00	192.00	4.9
890	(8+9)-I-4	-2571	119	-883	-6.64	17.56	-17.11	132.00	192.00	192.00	5.5
890	(8+9)-V-3	-2647	110	-1079	-6.84	16.29	-20.89	132.00	192.00	192.00	5.1
890	(8+9)-II-2	-2238	-135	-934	-5.78	-19.95	-18.10	132.00	192.00	192.00	5.0
890	(8+9)-V-4	-2480	55	-934	-6.41	8.09	-18.09	132.00	192.00	192.00	7.3
890	(8+9)-II-4	-2302	-48	-833	-5.94	-7.05	-16.13	132.00	192.00	192.00	8.2
890	(8+9)-VI-1	-2823	69	-1402	-7.29	10.22	-27.16	132.00	192.00	192.00	5.1
890	(8+9)-III-2	-2325	-178	-1228	-6.00	-26.33	-23.80	132.00	192.00	192.00	3.8
890	(8+9)-VI-2	-2265	-116	-919	-5.85	-17.11	-17.81	132.00	192.00	192.00	5.5
890	(8+9)-III-4	-2538	113	-890	-6.55	16.66	-17.23	132.00	192.00	192.00	5.6
890	(8+9)-VI-3	-2832	118	-1331	-7.31	17.44	-25.78	132.00	192.00	192.00	4.4
890	(8+9)-I-1	-2526	-117	-1367	-6.52	-17.23	-26.47	132.00	192.00	192.00	4.4
890	(8+9)-VI-4	-2274	-67	-848	-5.87	-9.89	-16.43	132.00	192.00	192.00	7.2
890	(8+9)-IV-4	-2190	-68	-855	-5.66	-10.04	-16.55	132.00	192.00	192.00	7.2
890	(8+9)-VII-1	-2651	-47	-1310	-6.85	-6.87	-25.37	132.00	192.00	192.00	5.9
890	(8+9)-II-1	-2795	50	-1417	-7.22	7.38	-27.45	132.00	192.00	192.00	5.5
890	(8+9)-VII-2	-2416	-114	-1178	-6.24	-16.86	-22.82	132.00	192.00	192.00	4.8
890	(8+9)-III-1	-2559	-111	-1360	-6.61	-16.34	-26.35	132.00	192.00	192.00	4.5
890	(8+9)-VII-3	-2681	116	-1072	-6.92	17.19	-20.77	132.00	192.00	192.00	5.0
890	(8+9)-IV-1	-2907	70	-1395	-7.51	10.36	-27.03	132.00	192.00	192.00	5.1
890	(8+9)-VII-4	-2447	49	-940	-6.32	7.20	-18.21	132.00	192.00	192.00	7.5
890	(8+9)-III-3	-2772	180	-1022	-7.16	26.65	-19.79	132.00	192.00	192.00	4.1
890	(8+9)-IV-3	-2971	157	-1294	-7.67	23.26	-25.06	132.00	192.00	192.00	3.9
890	(8+9)-II-3	-2859	137	-1316	-7.38	20.28	-25.48	132.00	192.00	192.00	4.2
890	(8+9)-VIII-1	-2935	89	-1380	-7.58	13.20	-26.74	132.00	192.00	192.00	4.8
890	(8+9)-VIII-2	-2154	-136	-941	-5.56	-20.09	-18.23	132.00	192.00	192.00	5.0
890	(8+9)-VIII-3	-2944	138	-1309	-7.60	20.42	-25.36	132.00	192.00	192.00	4.2
890	(8+9)-I-3	-2739	174	-1028	-7.07	25.76	-19.91	132.00	192.00	192.00	4.2

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Ty kg	τ_d kg/cm ²	fvd kg/cm ²	RS	Cs
0	1	-2	0.00	3.84	Si	>100
0	2	-3	0.00	5.76	Si	>100
0	3	-3	0.00	5.76	Si	>100
0	4	-2	0.00	5.12	Si	>100
0	5	-2	0.00	5.12	Si	>100
0	6	-2	0.00	5.12	Si	>100
0	7	-2	0.00	5.12	Si	>100
0	(8+9)-IV-4	-90	0.10	6.40	Si	63
0	(8+9)-I-1	251	0.28	6.40	Si	23
0	(8+9)-III-1	253	0.28	6.40	Si	23
0	(8+9)-I-2	245	0.28	6.40	Si	23
0	(8+9)-III-2	244	0.27	6.40	Si	23
0	(8+9)-I-4	-253	0.29	6.40	Si	22
0	(8+9)-III-3	-246	0.28	6.40	Si	23

X	Comb.	Ty	τ_d	fvd	RS	Cs
0	(8+9)-II-2	64	0.07	6.40	Si	89
0	(8+9)-III-4	-255	0.29	6.40	Si	22
0	(8+9)-II-1	84	0.09	6.40	Si	68
0	(8+9)-II-3	-66	0.07	6.40	Si	86
0	(8+9)-I-3	-247	0.28	6.40	Si	23
0	(8+9)-IV-1	88	0.10	6.40	Si	65
0	(8+9)-IV-2	60	0.07	6.40	Si	95
0	(8+9)-IV-3	-62	0.07	6.40	Si	92
0	(8+9)-II-4	-86	0.10	6.40	Si	66
400	(8+9)-V-4	87	0.10	6.40	Si	66
400	(8+9)-VII-4	81	0.09	6.40	Si	70
400	(8+9)-V-2	-93	0.10	6.40	Si	61
400	(8+9)-V-3	92	0.10	6.40	Si	62
400	(8+9)-VIII-2	-54	0.06	6.40	Si	>100
400	(8+9)-VI-2	-36	0.04	6.40	Si	>100
400	(8+9)-VI-3	35	0.04	6.40	Si	>100
400	(8+9)-VIII-3	54	0.06	6.40	Si	>100
400	(8+9)-VII-1	-82	0.09	6.40	Si	70
400	(8+9)-VII-2	-98	0.11	6.40	Si	58
400	(8+9)-VII-3	97	0.11	6.40	Si	58
400	(8+9)-V-1	-87	0.10	6.40	Si	65
800	(8+9)-VIII-1	26	0.03	6.40	Si	>100
800	(8+9)-VI-4	-20	0.02	6.40	Si	>100
800	(8+9)-VI-1	21	0.02	6.40	Si	>100
800	(8+9)-VIII-4	-25	0.03	6.40	Si	>100
Verifiche nella direzione secondaria						
0	(8+9)-I-1	-239	0.57	6.40	Si	11
0	(8+9)-III-4	237	0.56	6.40	Si	11
0	(8+9)-III-1	-241	0.57	6.40	Si	11
0	(8+9)-I-4	235	0.56	6.40	Si	11
890	1	-5	0.01	3.84	Si	>100
890	2	-5	0.01	5.76	Si	>100
890	3	-5	0.01	5.76	Si	>100
890	4	-5	0.01	5.12	Si	>100
890	5	-5	0.01	5.12	Si	>100
890	6	-5	0.01	5.12	Si	>100
890	7	-5	0.01	5.12	Si	>100
890	(8+9)-VIII-4	-169	0.40	6.40	Si	16
890	(8+9)-IV-4	-86	0.20	6.40	Si	31
890	(8+9)-V-3	25	0.06	6.40	Si	>100
890	(8+9)-II-2	-209	0.50	6.40	Si	13
890	(8+9)-V-4	-50	0.12	6.40	Si	54
890	(8+9)-II-4	-48	0.11	6.40	Si	56
890	(8+9)-VI-1	125	0.30	6.40	Si	21
890	(8+9)-III-2	-320	0.76	6.40	Si	8.4
890	(8+9)-VI-2	-126	0.30	6.40	Si	21
890	(8+9)-I-3	303	0.72	6.40	Si	8.9
890	(8+9)-VI-3	120	0.29	6.40	Si	22
890	(8+9)-IV-2	-247	0.59	6.40	Si	11
890	(8+9)-VI-4	-131	0.31	6.40	Si	20
890	(8+9)-I-2	-309	0.74	6.40	Si	8.7
890	(8+9)-VII-1	55	0.13	6.40	Si	49
890	(8+9)-V-2	-32	0.08	6.40	Si	85
890	(8+9)-VII-2	-43	0.10	6.40	Si	63
890	(8+9)-II-1	42	0.10	6.40	Si	64
890	(8+9)-VII-3	37	0.09	6.40	Si	73
890	(8+9)-IV-1	79	0.19	6.40	Si	34
890	(8+9)-VII-4	-61	0.15	6.40	Si	44
890	(8+9)-III-3	314	0.75	6.40	Si	8.5
890	(8+9)-IV-3	240	0.57	6.40	Si	11
890	(8+9)-II-3	203	0.48	6.40	Si	13
890	(8+9)-VIII-1	163	0.39	6.40	Si	17
890	(8+9)-VIII-2	-163	0.39	6.40	Si	16
890	(8+9)-VIII-3	157	0.37	6.40	Si	17

X	Comb.	Ty	τ_d	fvd	RS	Cs
890	(8+9)-V-1	44	0.10	6.40	Si	62

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	(8+9)-IV-4	-985	-2.29	32.00	14	-0.55	20.00	36	V	14
0	(8+9)-VII-4	-986	-2.29	32.00	14	-0.55	20.00	36	V	14
0	(8+9)-II-4	-977	-2.27	32.00	14	-0.55	20.00	36	V	14
0	(8+9)-VIII-2	-213	-0.49	32.00	65	-0.12	20.00	>100	V	65
0	(8+9)-VII-3	-564	-1.31	32.00	24	-0.32	20.00	63	V	24
0	(8+9)-I-3	-1195	-2.77	32.00	12	-0.67	20.00	30	V	12
0	(8+9)-III-4	-1614	-3.75	32.00	8.5	-0.91	20.00	22	V	8.5
0	(8+9)-I-4	-1611	-3.74	32.00	8.6	-0.91	20.00	22	V	8.6
0	(8+9)-V-3	-567	-1.32	32.00	24	-0.32	20.00	63	V	24
0	(8+9)-III-3	-1192	-2.77	32.00	12	-0.67	20.00	30	V	12
0	(8+9)-VIII-4	-797	-1.85	32.00	17	-0.45	20.00	45	V	17
0	(8+9)-VI-2	-205	-0.48	32.00	67	-0.11	20.00	>100	V	67
0	(8+9)-V-4	-983	-2.28	32.00	14	-0.55	20.00	36	V	14
0	(8+9)-VI-4	-788	-1.83	32.00	17	-0.44	20.00	45	V	17
800	1	917	2.13	19.20	9.0	0.52	12.00	23	V	9.0
800	2	1413	3.28	28.80	8.8	0.79	18.00	23	V	8.8
800	3	1413	3.28	28.80	8.8	0.79	18.00	23	V	8.8
800	4	917	2.13	25.60	12	0.52	16.00	31	V	12
800	5	917	2.13	25.60	12	0.52	16.00	31	V	12
800	6	917	2.13	25.60	12	0.52	16.00	31	V	12
800	7	917	2.13	25.60	12	0.52	16.00	31	V	12
800	(8+9)-IV-2	359	0.83	32.00	38	0.20	20.00	99	V	38
800	(8+9)-VII-1	1840	4.27	32.00	7.5	1.03	20.00	19	V	7.5
800	(8+9)-IV-3	922	2.14	32.00	15	0.52	20.00	39	V	15
800	(8+9)-VII-2	1382	3.21	32.00	10.0	0.78	20.00	26	V	10.0
800	(8+9)-V-2	1376	3.19	32.00	10	0.77	20.00	26	V	10
800	(8+9)-II-2	337	0.78	32.00	41	0.19	20.00	>100	V	41
800	(8+9)-III-2	2013	4.67	32.00	6.8	1.13	20.00	18	V	6.8
800	(8+9)-II-1	1905	4.42	32.00	7.2	1.07	20.00	19	V	7.2
800	(8+9)-III-1	2470	5.73	32.00	5.6	1.39	20.00	14	V	5.6
800	(8+9)-VIII-1	1694	3.93	32.00	8.1	0.95	20.00	21	V	8.1
800	(8+9)-II-3	945	2.19	32.00	15	0.53	20.00	38	V	15
800	(8+9)-I-2	2006	4.66	32.00	6.9	1.13	20.00	18	V	6.9
800	(8+9)-IV-1	1883	4.37	32.00	7.3	1.06	20.00	19	V	7.3
800	(8+9)-VI-3	1134	2.63	32.00	12	0.64	20.00	31	V	12
800	(8+9)-V-1	1846	4.29	32.00	7.5	1.04	20.00	19	V	7.5
800	(8+9)-VI-1	1716	3.98	32.00	8.0	0.96	20.00	21	V	8.0
800	(8+9)-VIII-3	1111	2.58	32.00	12	0.62	20.00	32	V	12
800	(8+9)-I-1	2477	5.75	32.00	5.6	1.39	20.00	14	V	5.6
Verifiche nella direzione secondaria										
0	(8+9)-IV-2	-90	-0.23	32.00	>100	-0.06	20.00	>100	V	>100
445	(8+9)-VIII-4	-1074	-2.77	32.00	12	-0.67	20.00	30	V	12
445	(8+9)-V-4	-1393	-3.60	32.00	8.9	-0.87	20.00	23	V	8.9
445	(8+9)-II-4	-1345	-3.47	32.00	9.2	-0.84	20.00	24	V	9.2
445	(8+9)-III-1	2436	6.29	32.00	5.1	1.52	20.00	13	V	5.1
445	(8+9)-VII-4	-1373	-3.55	32.00	9.0	-0.86	20.00	23	V	9.0
445	(8+9)-III-2	1912	4.94	32.00	6.5	1.19	20.00	17	V	6.5
445	(8+9)-VII-2	1231	3.18	32.00	10	0.77	20.00	26	V	10
445	(8+9)-III-3	-1529	-3.95	32.00	8.1	-0.96	20.00	21	V	8.1
445	(8+9)-I-2	1891	4.88	32.00	6.6	1.18	20.00	17	V	6.6
445	(8+9)-III-4	-2053	-5.30	32.00	6.0	-1.28	20.00	16	V	6.0
445	(8+9)-I-4	-2074	-5.36	32.00	6.0	-1.30	20.00	15	V	6.0
445	(8+9)-VI-4	-1141	-2.95	32.00	11	-0.71	20.00	28	V	11
445	(8+9)-II-2	-156	-0.40	32.00	80	-0.10	20.00	>100	V	80
445	(8+9)-V-3	-828	-2.14	32.00	15	-0.52	20.00	39	V	15
445	(8+9)-VIII-2	-292	-0.76	32.00	42	-0.18	20.00	>100	V	42
445	(8+9)-VI-2	-360	-0.93	32.00	34	-0.23	20.00	89	V	34
445	(8+9)-I-1	2457	6.34	32.00	5.0	1.54	20.00	13	V	5.0

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
445	(8+9)-II-1	1728	4.46	32.00	7.2	1.08	20.00	19	V	7.2
445	(8+9)-VII-1	1756	4.53	32.00	7.1	1.10	20.00	18	V	7.1
445	(8+9)-VII-3	-848	-2.19	32.00	15	-0.53	20.00	38	V	15
445	(8+9)-I-3	-1509	-3.90	32.00	8.2	-0.94	20.00	21	V	8.2
445	(8+9)-IV-4	-1278	-3.30	32.00	9.7	-0.80	20.00	25	V	9.7
445	(8+9)-V-1	1776	4.59	32.00	7.0	1.11	20.00	18	V	7.0
445	(8+9)-VI-1	1524	3.94	32.00	8.1	0.95	20.00	21	V	8.1
890	1	518	1.34	19.20	14	0.32	12.00	37	V	14
890	2	785	2.03	28.80	14	0.49	18.00	37	V	14
890	3	785	2.03	28.80	14	0.49	18.00	37	V	14
890	4	518	1.34	25.60	19	0.32	16.00	49	V	19
890	5	518	1.34	25.60	19	0.32	16.00	49	V	19
890	6	518	1.34	25.60	19	0.32	16.00	49	V	19
890	7	518	1.34	25.60	19	0.32	16.00	49	V	19
890	(8+9)-II-3	635	1.64	32.00	20	0.40	20.00	50	V	20
890	(8+9)-IV-1	1721	4.44	32.00	7.2	1.08	20.00	19	V	7.2
890	(8+9)-VI-3	803	2.07	32.00	15	0.50	20.00	40	V	15
890	(8+9)-VIII-1	1553	4.01	32.00	8.0	0.97	20.00	21	V	8.0
890	(8+9)-IV-3	735	1.90	32.00	17	0.46	20.00	44	V	17
890	(8+9)-VIII-3	902	2.33	32.00	14	0.56	20.00	35	V	14
890	(8+9)-V-2	1219	3.15	32.00	10	0.76	20.00	26	V	10

Verifiche a instabilità

Setto(X)	Comb.	kcrit _c	kcrit _m	λ_{relc}	λ_{relm}	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
(cm)						kg/cm ^q	kg/cm ^q	kg/cm ^q	kg/cm ^q	kg/cm ^q	kg/cm ^q	
50(0.0)	(8+9)-I-4	--	--	--	--	0.21	-8.27	-1.39	132.00	192.00	192.00	19
51(529.1)	(8+9)-III-4	0.26	--	1.92	--	-0.15	9.57	1.33	132.00	192.00	192.00	17
52(0.0)	(8+9)-I-1	--	--	--	--	0.21	3.29	6.61	132.00	192.00	192.00	19

Parete Xlam 1 - Nodi: [13-34-112-6-5-4-101] - **Crit.Prog.** Criterio di verifica XLAM 0 - **Verificato:**
[Cs=8.825,Comb=(8+9)-VI-3]

Geometria setti

Setto	Crit.	X mm	L cm	S cm	X90 mm	L90 cm	S90 cm
53	Criterio di verifica XLAM 0	0	237.0	12.1	0	603.0	12.1
		3015	237.0	12.1	1185	603.0	12.1
		6030	237.0	12.1	2370	603.0	12.1

Setto 53: origine (1236.0,189.0,118.5), direzione (0.930457,0.366402,0)

Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X mm	Comb.	N kg	Mx kg*m	My kg*m	σ_n kg/cm ^q	σ_{mx} kg/cm ^q	σ_{my} kg/cm ^q	ftd kg/cm ^q	fcd kg/cm ^q	fmd kg/cm ^q	Cs
0	(8+9)-VIII-4	-112	-147	18	-0.06	-3.20	0.03	132.00	192.00	192.00	59
0	(8+9)-IV-1	143	204	86	0.08	4.45	0.13	132.00	192.00	192.00	41
0	(8+9)-VI-1	107	144	49	0.06	3.14	0.07	132.00	192.00	192.00	58
0	(8+9)-III-1	-48	280	166	-0.03	6.11	0.24	132.00	192.00	192.00	30
0	(8+9)-III-2	-145	200	158	-0.08	4.36	0.23	132.00	192.00	192.00	42
0	(8+9)-VIII-2	-186	-123	26	-0.11	-2.68	0.04	132.00	192.00	192.00	71
0	(8+9)-III-3	173	-203	-88	0.10	-4.43	-0.13	132.00	192.00	192.00	41
0	(8+9)-VII-4	88	-82	18	0.05	-1.79	0.03	132.00	192.00	192.00	>100
0	(8+9)-III-4	75	-283	-96	0.04	-6.18	-0.14	132.00	192.00	192.00	30
0	(8+9)-I-2	-135	200	159	-0.08	4.36	0.23	132.00	192.00	192.00	42
0	(8+9)-VI-2	-153	-123	28	-0.09	-2.68	0.04	132.00	192.00	192.00	71
0	(8+9)-I-3	163	-203	-89	0.09	-4.43	-0.13	132.00	192.00	192.00	41
0	(8+9)-I-4	85	-283	-95	0.05	-6.18	-0.14	132.00	192.00	192.00	30
0	(8+9)-VII-1	-61	79	52	-0.04	1.72	0.08	132.00	192.00	192.00	>100

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-V-4	98	-82	19	0.06	-1.79	0.03	132.00	192.00	192.00	>100
0	(8+9)-II-4	-83	-207	-14	-0.05	-4.53	-0.02	132.00	192.00	192.00	42
0	(8+9)-VI-4	-79	-147	21	-0.05	-3.21	0.03	132.00	192.00	192.00	59
0	(8+9)-VIII-1	139	144	52	0.08	3.13	0.08	132.00	192.00	192.00	58
0	(8+9)-II-1	111	204	84	0.06	4.46	0.12	132.00	192.00	192.00	41
0	(8+9)-II-3	177	59	7	0.10	1.29	0.01	132.00	192.00	192.00	>100
0	(8+9)-VIII-3	213	119	44	0.12	2.61	0.07	132.00	192.00	192.00	67
0	(8+9)-I-1	-57	280	165	-0.03	6.11	0.24	132.00	192.00	192.00	30
0	(8+9)-IV-4	-116	-207	-16	-0.07	-4.52	-0.02	132.00	192.00	192.00	42
0	(8+9)-V-1	-71	79	51	-0.04	1.72	0.08	132.00	192.00	192.00	>100
0	(8+9)-VI-3	181	120	42	0.11	2.61	0.06	132.00	192.00	192.00	68
3015	1	208	-2	-66	0.12	-0.04	-0.10	79.20	115.20	115.20	>100
3015	2	302	-4	-104	0.18	-0.10	-0.15	118.80	172.80	172.80	>100
3015	3	302	-4	-104	0.18	-0.10	-0.15	118.80	172.80	172.80	>100
3015	4	208	-2	-66	0.12	-0.04	-0.10	105.60	153.60	153.60	>100
3015	5	208	-2	-66	0.12	-0.04	-0.10	105.60	153.60	153.60	>100
3015	6	208	-2	-66	0.12	-0.04	-0.10	105.60	153.60	153.60	>100
3015	7	208	-2	-66	0.12	-0.04	-0.10	105.60	153.60	153.60	>100
3015	(8+9)-IV-2	424	-18	-786	0.25	-0.40	-1.16	132.00	192.00	192.00	>100
3015	(8+9)-II-2	343	-21	-775	0.20	-0.45	-1.14	132.00	192.00	192.00	>100
6030	(8+9)-VII-3	343	65	-190	0.20	1.43	-0.28	132.00	192.00	192.00	96
6030	(8+9)-VII-2	-313	-76	185	-0.18	-1.65	0.27	132.00	192.00	192.00	100
6030	(8+9)-IV-3	291	63	-162	0.17	1.37	-0.24	132.00	192.00	192.00	>100
6030	(8+9)-V-2	-337	-68	195	-0.20	-1.49	0.29	132.00	192.00	192.00	>100
6030	(8+9)-V-3	366	58	-201	0.21	1.27	-0.30	132.00	192.00	192.00	>100
Verifiche nella direzione secondaria											
0	1	-5356	-19	-114	-1.84	-0.37	-0.04	79.20	115.20	115.20	>100
0	4	-5356	-19	-114	-1.84	-0.37	-0.04	105.60	153.60	153.60	>100
0	5	-5356	-19	-114	-1.84	-0.37	-0.04	105.60	153.60	153.60	>100
0	6	-5356	-19	-114	-1.84	-0.37	-0.04	105.60	153.60	153.60	>100
0	7	-5356	-19	-114	-1.84	-0.37	-0.04	105.60	153.60	153.60	>100
0	(8+9)-VIII-4	-10170	382	2612	-3.48	7.48	0.89	132.00	192.00	192.00	23
0	(8+9)-IV-2	-14430	684	5367	-4.94	13.40	1.83	132.00	192.00	192.00	13
0	(8+9)-V-1	-8743	309	4009	-3.00	6.06	1.37	132.00	192.00	192.00	26
0	(8+9)-I-1	-7269	332	-143	-2.49	6.50	-0.05	132.00	192.00	192.00	29
0	(8+9)-V-2	-14399	644	9095	-4.93	12.62	3.10	132.00	192.00	192.00	12
0	(8+9)-I-3	5454	-697	-5177	1.87	-13.67	-1.77	132.00	192.00	192.00	11
0	(8+9)-V-3	6928	-675	-9329	2.37	-13.23	-3.18	132.00	192.00	192.00	9.7
0	(8+9)-II-1	3783	-419	-7839	1.30	-8.22	-2.67	132.00	192.00	192.00	15
0	(8+9)-V-4	1273	-340	-4242	0.44	-6.67	-1.45	132.00	192.00	192.00	22
0	(8+9)-II-3	7599	-728	-9349	2.60	-14.27	-3.19	132.00	192.00	192.00	9.0
0	(8+9)-VI-1	3340	-426	-6594	1.14	-8.35	-2.25	132.00	192.00	192.00	16
0	(8+9)-III-1	-7461	335	981	-2.56	6.58	0.33	132.00	192.00	192.00	28
0	(8+9)-VI-2	-15512	690	10361	-5.32	13.52	3.53	132.00	192.00	192.00	11
0	(8+9)-III-3	5262	-694	-4053	1.80	-13.60	-1.38	132.00	192.00	192.00	11
0	(8+9)-VI-3	8042	-721	-10595	2.76	-14.14	-3.61	132.00	192.00	192.00	8.8
0	(8+9)-IV-1	3142	-406	-4091	1.08	-7.96	-1.39	132.00	192.00	192.00	18
0	(8+9)-VI-4	-10811	395	6360	-3.70	7.74	2.17	132.00	192.00	192.00	19
0	(8+9)-IV-3	6959	-715	-5601	2.38	-14.01	-1.91	132.00	192.00	192.00	9.9
0	(8+9)-VII-1	-8935	313	5133	-3.06	6.14	1.75	132.00	192.00	192.00	24
0	(8+9)-I-2	-12924	666	4943	-4.43	13.06	1.69	132.00	192.00	192.00	13
0	(8+9)-VII-2	-14207	640	7971	-4.87	12.54	2.72	132.00	192.00	192.00	12
0	(8+9)-II-2	-15070	697	9116	-5.16	13.66	3.11	132.00	192.00	192.00	11
0	(8+9)-VII-3	6736	-671	-8204	2.31	-13.16	-2.80	132.00	192.00	192.00	9.9
0	(8+9)-III-2	-12732	662	3819	-4.36	12.98	1.30	132.00	192.00	192.00	13
0	(8+9)-VIII-3	7401	-708	-6847	2.54	-13.88	-2.33	132.00	192.00	192.00	9.6
0	(8+9)-III-4	-10	-367	-1215	-0.00	-7.19	-0.41	132.00	192.00	192.00	25
0	(8+9)-I-4	-202	-363	-91	-0.07	-7.11	-0.03	132.00	192.00	192.00	27
0	(8+9)-II-4	-11253	388	7605	-3.86	7.60	2.59	132.00	192.00	192.00	19
0	(8+9)-IV-4	-10613	375	3857	-3.64	7.35	1.32	132.00	192.00	192.00	22
0	(8+9)-VII-4	1465	-344	-5367	0.50	-6.75	-1.83	132.00	192.00	192.00	21
0	(8+9)-VIII-1	2700	-413	-2845	0.93	-8.09	-0.97	132.00	192.00	192.00	18
0	(8+9)-VIII-2	-14872	677	6613	-5.10	13.27	2.25	132.00	192.00	192.00	12
2370	2	-8091	-17	877	-2.77	-0.32	0.30	118.80	172.80	172.80	>100

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
2370	3	-8091	-17	877	-2.77	-0.32	0.30	118.80	172.80	172.80	>100

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Ty kg	τ_d kg/cmq	fvd kg/cmq	RS	Cs
0	(8+9)-VIII-4	46	0.02	6.40	Si	>100
0	(8+9)-IV-1	-43	0.02	6.40	Si	>100
0	(8+9)-IV-4	46	0.02	6.40	Si	>100
0	(8+9)-II-2	90	0.04	6.40	Si	>100
0	(8+9)-IV-2	88	0.04	6.40	Si	>100
0	(8+9)-VI-2	90	0.04	6.40	Si	>100
0	(8+9)-VIII-2	88	0.04	6.40	Si	>100
0	(8+9)-V-2	91	0.04	6.40	Si	>100
0	(8+9)-VII-2	90	0.04	6.40	Si	>100
0	(8+9)-III-1	52	0.02	6.40	Si	>100
0	(8+9)-I-2	92	0.04	6.40	Si	>100
0	(8+9)-III-2	91	0.04	6.40	Si	>100
0	(8+9)-I-4	-48	0.02	6.40	Si	>100
0	(8+9)-III-3	-88	0.04	6.40	Si	>100
0	(8+9)-VIII-3	-84	0.04	6.40	Si	>100
0	(8+9)-III-4	-48	0.02	6.40	Si	>100
0	(8+9)-VI-4	48	0.02	6.40	Si	>100
0	(8+9)-VIII-1	-43	0.02	6.40	Si	>100
0	(8+9)-I-3	-88	0.04	6.40	Si	>100
0	(8+9)-V-1	50	0.02	6.40	Si	>100
0	(8+9)-I-1	51	0.02	6.40	Si	>100
0	(8+9)-IV-3	-84	0.04	6.40	Si	>100
6030	1	-19	0.01	3.84	Si	>100
6030	2	-33	0.01	5.76	Si	>100
6030	3	-33	0.01	5.76	Si	>100
6030	4	-19	0.01	5.12	Si	>100
6030	5	-19	0.01	5.12	Si	>100
6030	6	-19	0.01	5.12	Si	>100
6030	7	-19	0.01	5.12	Si	>100
6030	(8+9)-VII-1	56	0.02	6.40	Si	>100
6030	(8+9)-V-3	-110	0.05	6.40	Si	>100
6030	(8+9)-VII-4	-82	0.03	6.40	Si	>100
6030	(8+9)-VI-3	-109	0.05	6.40	Si	>100
6030	(8+9)-VII-3	-93	0.04	6.40	Si	>100
6030	(8+9)-II-4	53	0.02	6.40	Si	>100
6030	(8+9)-II-3	-93	0.04	6.40	Si	>100
6030	(8+9)-VI-1	-64	0.03	6.40	Si	>100
6030	(8+9)-V-4	-66	0.03	6.40	Si	>100
6030	(8+9)-II-1	-80	0.03	6.40	Si	>100
Verifiche nella direzione secondaria						
0	1	21	0.01	3.84	Si	>100
0	2	15	0.00	5.76	Si	>100
0	3	15	0.00	5.76	Si	>100
0	4	21	0.01	5.12	Si	>100
0	5	21	0.01	5.12	Si	>100
0	6	21	0.01	5.12	Si	>100
0	7	21	0.01	5.12	Si	>100
0	(8+9)-VIII-4	-369	0.12	6.40	Si	55
0	(8+9)-IV-2	-632	0.20	6.40	Si	32
0	(8+9)-I-2	-602	0.19	6.40	Si	34
0	(8+9)-VI-3	718	0.23	6.40	Si	28
0	(8+9)-VII-3	600	0.19	6.40	Si	34
0	(8+9)-IV-3	665	0.21	6.40	Si	30
0	(8+9)-II-2	-690	0.22	6.40	Si	29
0	(8+9)-IV-4	-363	0.11	6.40	Si	56
0	(8+9)-II-4	-422	0.13	6.40	Si	48
0	(8+9)-I-3	636	0.20	6.40	Si	32
0	(8+9)-VIII-2	-626	0.20	6.40	Si	32

X	Comb.	Ty	τ_d	fvd	RS	Cs
0	(8+9)-VI-2	-684	0.22	6.40	Si	30
0	(8+9)-III-3	619	0.20	6.40	Si	33
0	(8+9)-VIII-1	403	0.13	6.40	Si	50
0	(8+9)-II-1	455	0.14	6.40	Si	44
0	(8+9)-VIII-3	660	0.21	6.40	Si	31
0	(8+9)-IV-1	397	0.13	6.40	Si	51
0	(8+9)-II-3	724	0.23	6.40	Si	28
0	(8+9)-V-3	618	0.20	6.40	Si	33
0	(8+9)-VI-4	-427	0.14	6.40	Si	47
0	(8+9)-VI-1	461	0.15	6.40	Si	44
2370	(8+9)-V-1	-342	0.11	6.40	Si	59
2370	(8+9)-V-2	-590	0.19	6.40	Si	34
2370	(8+9)-I-4	332	0.10	6.40	Si	61
2370	(8+9)-VII-4	337	0.11	6.40	Si	60
2370	(8+9)-VII-2	-598	0.19	6.40	Si	34
2370	(8+9)-I-1	-329	0.10	6.40	Si	61
2370	(8+9)-VII-1	-334	0.11	6.40	Si	61
2370	(8+9)-III-4	324	0.10	6.40	Si	62
2370	(8+9)-III-2	-585	0.19	6.40	Si	35
2370	(8+9)-III-1	-322	0.10	6.40	Si	63
2370	(8+9)-V-4	344	0.11	6.40	Si	59

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
mm		kg	kg/cmq	kg/cmq		kg/cmq	kg/cmq			
0	(8+9)-III-1	769	0.67	32.00	48	0.16	20.00	>100	V	48
0	(8+9)-I-1	815	0.71	32.00	45	0.17	20.00	>100	V	45
3015	1	-620	-0.54	19.20	36	-0.13	12.00	92	V	36
3015	2	-1014	-0.88	28.80	33	-0.21	18.00	84	V	33
3015	3	-1014	-0.88	28.80	33	-0.21	18.00	84	V	33
3015	4	-620	-0.54	25.60	47	-0.13	16.00	>100	V	47
3015	5	-620	-0.54	25.60	47	-0.13	16.00	>100	V	47
3015	6	-620	-0.54	25.60	47	-0.13	16.00	>100	V	47
3015	7	-620	-0.54	25.60	47	-0.13	16.00	>100	V	47
3015	(8+9)-III-4	-1564	-1.36	32.00	23	-0.33	20.00	61	V	23
3015	(8+9)-I-4	-1585	-1.38	32.00	23	-0.33	20.00	60	V	23
6030	(8+9)-IV-3	3219	2.81	32.00	11	0.68	20.00	29	V	11
6030	(8+9)-VI-1	2458	2.14	32.00	15	0.52	20.00	39	V	15
6030	(8+9)-II-2	-3390	-2.96	32.00	11	-0.72	20.00	28	V	11
6030	(8+9)-VI-2	-3615	-3.15	32.00	10	-0.76	20.00	26	V	10
6030	(8+9)-II-4	-2406	-2.10	32.00	15	-0.51	20.00	39	V	15
6030	(8+9)-VI-3	3892	3.39	32.00	9.4	0.82	20.00	24	V	9.4
6030	(8+9)-III-2	-2279	-1.99	32.00	16	-0.48	20.00	42	V	16
6030	(8+9)-VI-4	-2181	-1.90	32.00	17	-0.46	20.00	43	V	17
6030	(8+9)-I-3	2690	2.34	32.00	14	0.57	20.00	35	V	14
6030	(8+9)-VII-1	-1475	-1.29	32.00	25	-0.31	20.00	64	V	25
6030	(8+9)-IV-2	-2942	-2.57	32.00	12	-0.62	20.00	32	V	12
6030	(8+9)-VII-2	-3028	-2.64	32.00	12	-0.64	20.00	31	V	12
6030	(8+9)-IV-4	-1958	-1.71	32.00	19	-0.41	20.00	48	V	19
6030	(8+9)-VII-3	3305	2.88	32.00	11	0.70	20.00	29	V	11
6030	(8+9)-V-2	-3163	-2.76	32.00	12	-0.67	20.00	30	V	12
6030	(8+9)-VII-4	1752	1.53	32.00	21	0.37	20.00	54	V	21
6030	(8+9)-V-4	1617	1.41	32.00	23	0.34	20.00	59	V	23
6030	(8+9)-VIII-1	2010	1.75	32.00	18	0.42	20.00	47	V	18
6030	(8+9)-II-1	2682	2.34	32.00	14	0.57	20.00	35	V	14
6030	(8+9)-VIII-2	-3167	-2.76	32.00	12	-0.67	20.00	30	V	12
6030	(8+9)-IV-1	2234	1.95	32.00	16	0.47	20.00	42	V	16
6030	(8+9)-VIII-3	3444	3.00	32.00	11	0.73	20.00	28	V	11
6030	(8+9)-V-1	-1341	-1.17	32.00	27	-0.28	20.00	71	V	27
6030	(8+9)-II-3	3667	3.20	32.00	10	0.77	20.00	26	V	10
6030	(8+9)-III-3	2555	2.23	32.00	14	0.54	20.00	37	V	14
6030	(8+9)-I-2	-2413	-2.10	32.00	15	-0.51	20.00	39	V	15
6030	(8+9)-V-3	3439	3.00	32.00	11	0.73	20.00	28	V	11

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
6030	(8+9)-VIII-4	-1733	-1.51	32.00	21	-0.37	20.00	55	V	21
Verifiche nella direzione secondaria										
0	2	59	0.02	28.80	>100	0.00	18.00	>100	V	>100
0	3	59	0.02	28.80	>100	0.00	18.00	>100	V	>100
0	(8+9)-VIII-4	-807	-0.28	32.00	>100	-0.07	20.00	>100	V	>100
0	(8+9)-VI-4	-973	-0.33	32.00	96	-0.08	20.00	>100	V	96
0	(8+9)-III-2	2429	0.83	32.00	38	0.20	20.00	99	V	38
0	(8+9)-III-3	-2402	-0.82	32.00	39	-0.20	20.00	>100	V	39
0	(8+9)-VII-4	-700	-0.24	32.00	>100	-0.06	20.00	>100	V	>100
0	(8+9)-III-4	-2802	-0.96	32.00	33	-0.23	20.00	86	V	33
0	(8+9)-I-1	2878	0.99	32.00	32	0.24	20.00	84	V	32
0	(8+9)-IV-1	1464	0.50	32.00	64	0.12	20.00	>100	V	64
0	(8+9)-I-3	-2353	-0.81	32.00	40	-0.20	20.00	>100	V	40
0	(8+9)-IV-2	132	0.05	32.00	>100	0.01	20.00	>100	V	>100
0	(8+9)-II-1	1630	0.56	32.00	57	0.14	20.00	>100	V	57
0	(8+9)-VI-1	999	0.34	32.00	93	0.08	20.00	>100	V	93
0	(8+9)-VII-2	327	0.11	32.00	>100	0.03	20.00	>100	V	>100
0	(8+9)-VII-1	726	0.25	32.00	>100	0.06	20.00	>100	V	>100
0	(8+9)-III-1	2829	0.97	32.00	33	0.23	20.00	85	V	33
0	(8+9)-IV-4	-1438	-0.49	32.00	65	-0.12	20.00	>100	V	65
0	(8+9)-VII-3	-300	-0.10	32.00	>100	-0.02	20.00	>100	V	>100
0	(8+9)-V-1	776	0.27	32.00	>100	0.06	20.00	>100	V	>100
0	(8+9)-I-4	-2852	-0.98	32.00	33	-0.24	20.00	85	V	33
0	(8+9)-VIII-1	833	0.29	32.00	>100	0.07	20.00	>100	V	>100
0	(8+9)-I-2	2379	0.82	32.00	39	0.20	20.00	>100	V	39
0	(8+9)-II-4	-1604	-0.55	32.00	58	-0.13	20.00	>100	V	58
0	(8+9)-V-2	277	0.09	32.00	>100	0.02	20.00	>100	V	>100
0	(8+9)-V-3	-251	-0.09	32.00	>100	-0.02	20.00	>100	V	>100
0	(8+9)-V-4	-750	-0.26	32.00	>100	-0.06	20.00	>100	V	>100
1185	1	22	0.01	19.20	>100	0.00	12.00	>100	V	>100
1185	4	22	0.01	25.60	>100	0.00	16.00	>100	V	>100
1185	5	22	0.01	25.60	>100	0.00	16.00	>100	V	>100
1185	6	22	0.01	25.60	>100	0.00	16.00	>100	V	>100
1185	7	22	0.01	25.60	>100	0.00	16.00	>100	V	>100
1185	(8+9)-IV-3	157	0.05	32.00	>100	0.01	20.00	>100	V	>100
1185	(8+9)-II-2	-317	-0.11	32.00	>100	-0.03	20.00	>100	V	>100
1185	(8+9)-II-3	344	0.12	32.00	>100	0.03	20.00	>100	V	>100
1185	(8+9)-VI-2	-712	-0.24	32.00	>100	-0.06	20.00	>100	V	>100
1185	(8+9)-VIII-2	-525	-0.18	32.00	>100	-0.04	20.00	>100	V	>100
1185	(8+9)-VIII-3	553	0.19	32.00	>100	0.05	20.00	>100	V	>100
1185	(8+9)-VI-3	740	0.25	32.00	>100	0.06	20.00	>100	V	>100

Verifiche a instabilità

Setto(X)	Comb.	krit _c	krit _m	λ_{relc}	λ_{relm}	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
(cm)						kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	
53(0.0)	(8+9)-I-1	0.20	--	2.19	--	-0.03	6.11	0.24	132.00	192.00	192.00	29

Parete Xlam 1 - Nodi: [13-34-112-6-5-4-101] - **Crit.Prog.** Criterio di verifica XLAM 0 - **Verificato:**
 [Cs=8.825,Comb=(8+9)-VI-3]

Geometria setti

Setto	Crit.	X	L	S	X90	L90	S90
		mm	cm	cm	mm	cm	cm
53	Criterio di verifica XLAM 0	0	237.0	12.1	0	603.0	12.1
		3015	237.0	12.1	1185	603.0	12.1
		6030	237.0	12.1	2370	603.0	12.1

Setto 53: origine (1236.0,189.0,118.5), direzione (0.930457,0.366402,0)
 Verifiche a flessione (Sezione più gravosa per ogni combinazione)

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
mm		kg	kg*m	kg*m	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	kg/cmq	
0	(8+9)-VIII-4	-112	-147	18	-0.06	-3.20	0.03	132.00	192.00	192.00	59
0	(8+9)-IV-1	143	204	86	0.08	4.45	0.13	132.00	192.00	192.00	41
0	(8+9)-VI-1	107	144	49	0.06	3.14	0.07	132.00	192.00	192.00	58
0	(8+9)-III-1	-48	280	166	-0.03	6.11	0.24	132.00	192.00	192.00	30
0	(8+9)-III-2	-145	200	158	-0.08	4.36	0.23	132.00	192.00	192.00	42
0	(8+9)-VIII-2	-186	-123	26	-0.11	-2.68	0.04	132.00	192.00	192.00	71
0	(8+9)-III-3	173	-203	-88	0.10	-4.43	-0.13	132.00	192.00	192.00	41
0	(8+9)-VII-4	88	-82	18	0.05	-1.79	0.03	132.00	192.00	192.00	>100
0	(8+9)-III-4	75	-283	-96	0.04	-6.18	-0.14	132.00	192.00	192.00	30
0	(8+9)-I-2	-135	200	159	-0.08	4.36	0.23	132.00	192.00	192.00	42
0	(8+9)-VI-2	-153	-123	28	-0.09	-2.68	0.04	132.00	192.00	192.00	71
0	(8+9)-I-3	163	-203	-89	0.09	-4.43	-0.13	132.00	192.00	192.00	41
0	(8+9)-I-4	85	-283	-95	0.05	-6.18	-0.14	132.00	192.00	192.00	30
0	(8+9)-VII-1	-61	79	52	-0.04	1.72	0.08	132.00	192.00	192.00	>100
0	(8+9)-V-4	98	-82	19	0.06	-1.79	0.03	132.00	192.00	192.00	>100
0	(8+9)-II-4	-83	-207	-14	-0.05	-4.53	-0.02	132.00	192.00	192.00	42
0	(8+9)-VI-4	-79	-147	21	-0.05	-3.21	0.03	132.00	192.00	192.00	59
0	(8+9)-VIII-1	139	144	52	0.08	3.13	0.08	132.00	192.00	192.00	58
0	(8+9)-II-1	111	204	84	0.06	4.46	0.12	132.00	192.00	192.00	41
0	(8+9)-II-3	177	59	7	0.10	1.29	0.01	132.00	192.00	192.00	>100
0	(8+9)-VIII-3	213	119	44	0.12	2.61	0.07	132.00	192.00	192.00	67
0	(8+9)-I-1	-57	280	165	-0.03	6.11	0.24	132.00	192.00	192.00	30
0	(8+9)-IV-4	-116	-207	-16	-0.07	-4.52	-0.02	132.00	192.00	192.00	42
0	(8+9)-V-1	-71	79	51	-0.04	1.72	0.08	132.00	192.00	192.00	>100
0	(8+9)-VI-3	181	120	42	0.11	2.61	0.06	132.00	192.00	192.00	68
3015	1	208	-2	-66	0.12	-0.04	-0.10	79.20	115.20	115.20	>100
3015	2	302	-4	-104	0.18	-0.10	-0.15	118.80	172.80	172.80	>100
3015	3	302	-4	-104	0.18	-0.10	-0.15	118.80	172.80	172.80	>100
3015	4	208	-2	-66	0.12	-0.04	-0.10	105.60	153.60	153.60	>100
3015	5	208	-2	-66	0.12	-0.04	-0.10	105.60	153.60	153.60	>100
3015	6	208	-2	-66	0.12	-0.04	-0.10	105.60	153.60	153.60	>100
3015	7	208	-2	-66	0.12	-0.04	-0.10	105.60	153.60	153.60	>100
3015	(8+9)-IV-2	424	-18	-786	0.25	-0.40	-1.16	132.00	192.00	192.00	>100
3015	(8+9)-II-2	343	-21	-775	0.20	-0.45	-1.14	132.00	192.00	192.00	>100
6030	(8+9)-VII-3	343	65	-190	0.20	1.43	-0.28	132.00	192.00	192.00	96
6030	(8+9)-VII-2	-313	-76	185	-0.18	-1.65	0.27	132.00	192.00	192.00	100
6030	(8+9)-IV-3	291	63	-162	0.17	1.37	-0.24	132.00	192.00	192.00	>100
6030	(8+9)-V-2	-337	-68	195	-0.20	-1.49	0.29	132.00	192.00	192.00	>100
6030	(8+9)-V-3	366	58	-201	0.21	1.27	-0.30	132.00	192.00	192.00	>100
Verifiche nella direzione secondaria											
0	1	-5356	-19	-114	-1.84	-0.37	-0.04	79.20	115.20	115.20	>100
0	4	-5356	-19	-114	-1.84	-0.37	-0.04	105.60	153.60	153.60	>100
0	5	-5356	-19	-114	-1.84	-0.37	-0.04	105.60	153.60	153.60	>100
0	6	-5356	-19	-114	-1.84	-0.37	-0.04	105.60	153.60	153.60	>100
0	7	-5356	-19	-114	-1.84	-0.37	-0.04	105.60	153.60	153.60	>100
0	(8+9)-VIII-4	-10170	382	2612	-3.48	7.48	0.89	132.00	192.00	192.00	23
0	(8+9)-IV-2	-14430	684	5367	-4.94	13.40	1.83	132.00	192.00	192.00	13
0	(8+9)-V-1	-8743	309	4009	-3.00	6.06	1.37	132.00	192.00	192.00	26
0	(8+9)-I-1	-7269	332	-143	-2.49	6.50	-0.05	132.00	192.00	192.00	29
0	(8+9)-V-2	-14399	644	9095	-4.93	12.62	3.10	132.00	192.00	192.00	12
0	(8+9)-I-3	5454	-697	-5177	1.87	-13.67	-1.77	132.00	192.00	192.00	11
0	(8+9)-V-3	6928	-675	-9329	2.37	-13.23	-3.18	132.00	192.00	192.00	9.7
0	(8+9)-II-1	3783	-419	-7839	1.30	-8.22	-2.67	132.00	192.00	192.00	15
0	(8+9)-V-4	1273	-340	-4242	0.44	-6.67	-1.45	132.00	192.00	192.00	22
0	(8+9)-II-3	7599	-728	-9349	2.60	-14.27	-3.19	132.00	192.00	192.00	9.0
0	(8+9)-VI-1	3340	-426	-6594	1.14	-8.35	-2.25	132.00	192.00	192.00	16
0	(8+9)-III-1	-7461	335	981	-2.56	6.58	0.33	132.00	192.00	192.00	28
0	(8+9)-VI-2	-15512	690	10361	-5.32	13.52	3.53	132.00	192.00	192.00	11
0	(8+9)-III-3	5262	-694	-4053	1.80	-13.60	-1.38	132.00	192.00	192.00	11
0	(8+9)-VI-3	8042	-721	-10595	2.76	-14.14	-3.61	132.00	192.00	192.00	8.8
0	(8+9)-IV-1	3142	-406	-4091	1.08	-7.96	-1.39	132.00	192.00	192.00	18
0	(8+9)-VI-4	-10811	395	6360	-3.70	7.74	2.17	132.00	192.00	192.00	19
0	(8+9)-IV-3	6959	-715	-5601	2.38	-14.01	-1.91	132.00	192.00	192.00	9.9

X	Comb.	N	Mx	My	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
0	(8+9)-VII-1	-8935	313	5133	-3.06	6.14	1.75	132.00	192.00	192.00	24
0	(8+9)-I-2	-12924	666	4943	-4.43	13.06	1.69	132.00	192.00	192.00	13
0	(8+9)-VII-2	-14207	640	7971	-4.87	12.54	2.72	132.00	192.00	192.00	12
0	(8+9)-II-2	-15070	697	9116	-5.16	13.66	3.11	132.00	192.00	192.00	11
0	(8+9)-VII-3	6736	-671	-8204	2.31	-13.16	-2.80	132.00	192.00	192.00	9.9
0	(8+9)-III-2	-12732	662	3819	-4.36	12.98	1.30	132.00	192.00	192.00	13
0	(8+9)-VIII-3	7401	-708	-6847	2.54	-13.88	-2.33	132.00	192.00	192.00	9.6
0	(8+9)-III-4	-10	-367	-1215	-0.00	-7.19	-0.41	132.00	192.00	192.00	25
0	(8+9)-I-4	-202	-363	-91	-0.07	-7.11	-0.03	132.00	192.00	192.00	27
0	(8+9)-II-4	-11253	388	7605	-3.86	7.60	2.59	132.00	192.00	192.00	19
0	(8+9)-IV-4	-10613	375	3857	-3.64	7.35	1.32	132.00	192.00	192.00	22
0	(8+9)-VII-4	1465	-344	-5367	0.50	-6.75	-1.83	132.00	192.00	192.00	21
0	(8+9)-VIII-1	2700	-413	-2845	0.93	-8.09	-0.97	132.00	192.00	192.00	18
0	(8+9)-VIII-2	-14872	677	6613	-5.10	13.27	2.25	132.00	192.00	192.00	12
2370	2	-8091	-17	877	-2.77	-0.32	0.30	118.80	172.80	172.80	>100
2370	3	-8091	-17	877	-2.77	-0.32	0.30	118.80	172.80	172.80	>100

Verifiche a taglio Ortogonale (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Ty kg	τ_d kg/cmq	fvd kg/cmq	RS	Cs
0	(8+9)-VIII-4	46	0.02	6.40	Si	>100
0	(8+9)-IV-1	-43	0.02	6.40	Si	>100
0	(8+9)-IV-4	46	0.02	6.40	Si	>100
0	(8+9)-II-2	90	0.04	6.40	Si	>100
0	(8+9)-IV-2	88	0.04	6.40	Si	>100
0	(8+9)-VI-2	90	0.04	6.40	Si	>100
0	(8+9)-VIII-2	88	0.04	6.40	Si	>100
0	(8+9)-V-2	91	0.04	6.40	Si	>100
0	(8+9)-VII-2	90	0.04	6.40	Si	>100
0	(8+9)-III-1	52	0.02	6.40	Si	>100
0	(8+9)-I-2	92	0.04	6.40	Si	>100
0	(8+9)-III-2	91	0.04	6.40	Si	>100
0	(8+9)-I-4	-48	0.02	6.40	Si	>100
0	(8+9)-III-3	-88	0.04	6.40	Si	>100
0	(8+9)-VIII-3	-84	0.04	6.40	Si	>100
0	(8+9)-III-4	-48	0.02	6.40	Si	>100
0	(8+9)-VI-4	48	0.02	6.40	Si	>100
0	(8+9)-VIII-1	-43	0.02	6.40	Si	>100
0	(8+9)-I-3	-88	0.04	6.40	Si	>100
0	(8+9)-V-1	50	0.02	6.40	Si	>100
0	(8+9)-I-1	51	0.02	6.40	Si	>100
0	(8+9)-IV-3	-84	0.04	6.40	Si	>100
6030	1	-19	0.01	3.84	Si	>100
6030	2	-33	0.01	5.76	Si	>100
6030	3	-33	0.01	5.76	Si	>100
6030	4	-19	0.01	5.12	Si	>100
6030	5	-19	0.01	5.12	Si	>100
6030	6	-19	0.01	5.12	Si	>100
6030	7	-19	0.01	5.12	Si	>100
6030	(8+9)-VII-1	56	0.02	6.40	Si	>100
6030	(8+9)-V-3	-110	0.05	6.40	Si	>100
6030	(8+9)-VII-4	-82	0.03	6.40	Si	>100
6030	(8+9)-VI-3	-109	0.05	6.40	Si	>100
6030	(8+9)-VII-3	-93	0.04	6.40	Si	>100
6030	(8+9)-II-4	53	0.02	6.40	Si	>100
6030	(8+9)-II-3	-93	0.04	6.40	Si	>100
6030	(8+9)-VI-1	-64	0.03	6.40	Si	>100
6030	(8+9)-V-4	-66	0.03	6.40	Si	>100
6030	(8+9)-II-1	-80	0.03	6.40	Si	>100
Verifiche nella direzione secondaria						
0	1	21	0.01	3.84	Si	>100
0	2	15	0.00	5.76	Si	>100
0	3	15	0.00	5.76	Si	>100

X	Comb.	Ty	τ_d	fvd	RS	Cs
0	4	21	0.01	5.12	Si	>100
0	5	21	0.01	5.12	Si	>100
0	6	21	0.01	5.12	Si	>100
0	7	21	0.01	5.12	Si	>100
0	(8+9)-VIII-4	-369	0.12	6.40	Si	55
0	(8+9)-IV-2	-632	0.20	6.40	Si	32
0	(8+9)-I-2	-602	0.19	6.40	Si	34
0	(8+9)-VI-3	718	0.23	6.40	Si	28
0	(8+9)-VII-3	600	0.19	6.40	Si	34
0	(8+9)-IV-3	665	0.21	6.40	Si	30
0	(8+9)-II-2	-690	0.22	6.40	Si	29
0	(8+9)-IV-4	-363	0.11	6.40	Si	56
0	(8+9)-II-4	-422	0.13	6.40	Si	48
0	(8+9)-I-3	636	0.20	6.40	Si	32
0	(8+9)-VIII-2	-626	0.20	6.40	Si	32
0	(8+9)-VI-2	-684	0.22	6.40	Si	30
0	(8+9)-III-3	619	0.20	6.40	Si	33
0	(8+9)-VIII-1	403	0.13	6.40	Si	50
0	(8+9)-II-1	455	0.14	6.40	Si	44
0	(8+9)-VIII-3	660	0.21	6.40	Si	31
0	(8+9)-IV-1	397	0.13	6.40	Si	51
0	(8+9)-II-3	724	0.23	6.40	Si	28
0	(8+9)-V-3	618	0.20	6.40	Si	33
0	(8+9)-VI-4	-427	0.14	6.40	Si	47
0	(8+9)-VI-1	461	0.15	6.40	Si	44
2370	(8+9)-V-1	-342	0.11	6.40	Si	59
2370	(8+9)-V-2	-590	0.19	6.40	Si	34
2370	(8+9)-I-4	332	0.10	6.40	Si	61
2370	(8+9)-VII-4	337	0.11	6.40	Si	60
2370	(8+9)-VII-2	-598	0.19	6.40	Si	34
2370	(8+9)-I-1	-329	0.10	6.40	Si	61
2370	(8+9)-VII-1	-334	0.11	6.40	Si	61
2370	(8+9)-III-4	324	0.10	6.40	Si	62
2370	(8+9)-III-2	-585	0.19	6.40	Si	35
2370	(8+9)-III-1	-322	0.10	6.40	Si	63
2370	(8+9)-V-4	344	0.11	6.40	Si	59

Verifiche a taglio Parallelo (Sezione più gravosa per ogni combinazione)

X mm	Comb.	Tx kg	τ_{vd} kg/cmq	fvd kg/cmq	Csv	τ_M kg/cmq	fTd kg/cmq	Csm	Mecc.	Cs
0	(8+9)-III-1	769	0.67	32.00	48	0.16	20.00	>100	V	48
0	(8+9)-I-1	815	0.71	32.00	45	0.17	20.00	>100	V	45
3015	1	-620	-0.54	19.20	36	-0.13	12.00	92	V	36
3015	2	-1014	-0.88	28.80	33	-0.21	18.00	84	V	33
3015	3	-1014	-0.88	28.80	33	-0.21	18.00	84	V	33
3015	4	-620	-0.54	25.60	47	-0.13	16.00	>100	V	47
3015	5	-620	-0.54	25.60	47	-0.13	16.00	>100	V	47
3015	6	-620	-0.54	25.60	47	-0.13	16.00	>100	V	47
3015	7	-620	-0.54	25.60	47	-0.13	16.00	>100	V	47
3015	(8+9)-III-4	-1564	-1.36	32.00	23	-0.33	20.00	61	V	23
3015	(8+9)-I-4	-1585	-1.38	32.00	23	-0.33	20.00	60	V	23
6030	(8+9)-IV-3	3219	2.81	32.00	11	0.68	20.00	29	V	11
6030	(8+9)-VI-1	2458	2.14	32.00	15	0.52	20.00	39	V	15
6030	(8+9)-II-2	-3390	-2.96	32.00	11	-0.72	20.00	28	V	11
6030	(8+9)-VI-2	-3615	-3.15	32.00	10	-0.76	20.00	26	V	10
6030	(8+9)-II-4	-2406	-2.10	32.00	15	-0.51	20.00	39	V	15
6030	(8+9)-VI-3	3892	3.39	32.00	9.4	0.82	20.00	24	V	9.4
6030	(8+9)-III-2	-2279	-1.99	32.00	16	-0.48	20.00	42	V	16
6030	(8+9)-VI-4	-2181	-1.90	32.00	17	-0.46	20.00	43	V	17
6030	(8+9)-I-3	2690	2.34	32.00	14	0.57	20.00	35	V	14
6030	(8+9)-VII-1	-1475	-1.29	32.00	25	-0.31	20.00	64	V	25
6030	(8+9)-IV-2	-2942	-2.57	32.00	12	-0.62	20.00	32	V	12
6030	(8+9)-VII-2	-3028	-2.64	32.00	12	-0.64	20.00	31	V	12

X	Comb.	Tx	τ_{vd}	fvd	Csv	τ_M	fTd	Csm	Mecc.	Cs
6030	(8+9)-IV-4	-1958	-1.71	32.00	19	-0.41	20.00	48	V	19
6030	(8+9)-VII-3	3305	2.88	32.00	11	0.70	20.00	29	V	11
6030	(8+9)-V-2	-3163	-2.76	32.00	12	-0.67	20.00	30	V	12
6030	(8+9)-VII-4	1752	1.53	32.00	21	0.37	20.00	54	V	21
6030	(8+9)-V-4	1617	1.41	32.00	23	0.34	20.00	59	V	23
6030	(8+9)-VIII-1	2010	1.75	32.00	18	0.42	20.00	47	V	18
6030	(8+9)-II-1	2682	2.34	32.00	14	0.57	20.00	35	V	14
6030	(8+9)-VIII-2	-3167	-2.76	32.00	12	-0.67	20.00	30	V	12
6030	(8+9)-IV-1	2234	1.95	32.00	16	0.47	20.00	42	V	16
6030	(8+9)-VIII-3	3444	3.00	32.00	11	0.73	20.00	28	V	11
6030	(8+9)-V-1	-1341	-1.17	32.00	27	-0.28	20.00	71	V	27
6030	(8+9)-II-3	3667	3.20	32.00	10	0.77	20.00	26	V	10
6030	(8+9)-III-3	2555	2.23	32.00	14	0.54	20.00	37	V	14
6030	(8+9)-I-2	-2413	-2.10	32.00	15	-0.51	20.00	39	V	15
6030	(8+9)-V-3	3439	3.00	32.00	11	0.73	20.00	28	V	11
6030	(8+9)-VIII-4	-1733	-1.51	32.00	21	-0.37	20.00	55	V	21
Verifiche nella direzione secondaria										
0	2	59	0.02	28.80	>100	0.00	18.00	>100	V	>100
0	3	59	0.02	28.80	>100	0.00	18.00	>100	V	>100
0	(8+9)-VIII-4	-807	-0.28	32.00	>100	-0.07	20.00	>100	V	>100
0	(8+9)-VI-4	-973	-0.33	32.00	96	-0.08	20.00	>100	V	96
0	(8+9)-III-2	2429	0.83	32.00	38	0.20	20.00	99	V	38
0	(8+9)-III-3	-2402	-0.82	32.00	39	-0.20	20.00	>100	V	39
0	(8+9)-VII-4	-700	-0.24	32.00	>100	-0.06	20.00	>100	V	>100
0	(8+9)-III-4	-2802	-0.96	32.00	33	-0.23	20.00	86	V	33
0	(8+9)-I-1	2878	0.99	32.00	32	0.24	20.00	84	V	32
0	(8+9)-IV-1	1464	0.50	32.00	64	0.12	20.00	>100	V	64
0	(8+9)-I-3	-2353	-0.81	32.00	40	-0.20	20.00	>100	V	40
0	(8+9)-IV-2	132	0.05	32.00	>100	0.01	20.00	>100	V	>100
0	(8+9)-II-1	1630	0.56	32.00	57	0.14	20.00	>100	V	57
0	(8+9)-VI-1	999	0.34	32.00	93	0.08	20.00	>100	V	93
0	(8+9)-VII-2	327	0.11	32.00	>100	0.03	20.00	>100	V	>100
0	(8+9)-VII-1	726	0.25	32.00	>100	0.06	20.00	>100	V	>100
0	(8+9)-III-1	2829	0.97	32.00	33	0.23	20.00	85	V	33
0	(8+9)-IV-4	-1438	-0.49	32.00	65	-0.12	20.00	>100	V	65
0	(8+9)-VII-3	-300	-0.10	32.00	>100	-0.02	20.00	>100	V	>100
0	(8+9)-V-1	776	0.27	32.00	>100	0.06	20.00	>100	V	>100
0	(8+9)-I-4	-2852	-0.98	32.00	33	-0.24	20.00	85	V	33
0	(8+9)-VIII-1	833	0.29	32.00	>100	0.07	20.00	>100	V	>100
0	(8+9)-I-2	2379	0.82	32.00	39	0.20	20.00	>100	V	39
0	(8+9)-II-4	-1604	-0.55	32.00	58	-0.13	20.00	>100	V	58
0	(8+9)-V-2	277	0.09	32.00	>100	0.02	20.00	>100	V	>100
0	(8+9)-V-3	-251	-0.09	32.00	>100	-0.02	20.00	>100	V	>100
0	(8+9)-V-4	-750	-0.26	32.00	>100	-0.06	20.00	>100	V	>100
1185	1	22	0.01	19.20	>100	0.00	12.00	>100	V	>100
1185	4	22	0.01	25.60	>100	0.00	16.00	>100	V	>100
1185	5	22	0.01	25.60	>100	0.00	16.00	>100	V	>100
1185	6	22	0.01	25.60	>100	0.00	16.00	>100	V	>100
1185	7	22	0.01	25.60	>100	0.00	16.00	>100	V	>100
1185	(8+9)-IV-3	157	0.05	32.00	>100	0.01	20.00	>100	V	>100
1185	(8+9)-II-2	-317	-0.11	32.00	>100	-0.03	20.00	>100	V	>100
1185	(8+9)-II-3	344	0.12	32.00	>100	0.03	20.00	>100	V	>100
1185	(8+9)-VI-2	-712	-0.24	32.00	>100	-0.06	20.00	>100	V	>100
1185	(8+9)-VIII-2	-525	-0.18	32.00	>100	-0.04	20.00	>100	V	>100
1185	(8+9)-VIII-3	553	0.19	32.00	>100	0.05	20.00	>100	V	>100
1185	(8+9)-VI-3	740	0.25	32.00	>100	0.06	20.00	>100	V	>100

Verifiche a instabilità

Setto(X)	Comb.	kcrit _c	kcrit _m	$\lambda_{rel,c}$	$\lambda_{rel,m}$	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
(cm)						kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	kg/cm ²	
53(0.0)	(8+9)-I-1	0.20	--	2.19	--	-0.03	6.11	0.24	132.00	192.00	192.00	29

Setto(X)	Comb.	k _{critc}	k _{critm}	λ_{relc}	λ_{relm}	σ_n	σ_{mx}	σ_{my}	ftd	fcd	fmd	Cs
)												

Verifica Stabilità aste Metalliche

Scenario di calcolo: **Set_NT_SLV_SLD_A2_STR/GEO_2018**

Simbologia

- L [cm] Lunghezza teorica elemento (da nodo a nodo)
 Ln1 [cm] Luce libera nella direzione principale 1 dell'elemento
 Ln2 [cm] Luce libera nella direzione principale 2 dell'elemento
 Sez. G Sezione Generica (Sigla)
 f_{yd} [kg/cm²] Tensione di progetto snervamento acciaio
 f_t [kg/cm²] Tensione di rottura acciaio
 γ_M Coefficiente di sicurezza acciaio
 N [kg] Sforzo Normale massimo
 M_y [kg*m] M_y massimo
 M_z [kg*m] M_z massimo
 N_{Rk} [kg] :A*f_y, Resistenza caratteristica instabilità a compressione ⁽¹⁾
 M_{yRk} [kg*m] :W_y*f_y, Momento resistente caratteristico all'instabilità in direzione Y ⁽¹⁾
 M_{zRk} [kg*m] :W_z*f_y, Momento resistente caratteristico all'instabilità in direzione Z ⁽¹⁾
 λ_y Snellezza in direzione y
 λ_z Snellezza in direzione z
 χ_y Coefficiente di riduzione per la presso flessione dir y
 χ_z Coefficiente di riduzione per la presso flessione dir z
 χ_{LT} Coefficiente di riduzione per la instabilità flesso-torsionale, il coefficiente è applicato al termine relativo all'asse forte
 k_{yy}, k_{yz} Coefficienti di interazione per l'instabilità (cfr. EC3 Annex B, tab B1 e B2, e cfr. Circ.NTC tab. C4.2.IV e C4.2.V)
 M_{yeq} [kg*m] M_y equivalente uguale a k_{yy}*M_y oppure k_{zy}*M_y
 M_{zeq} [kg*m] M_z equivalente uguale a k_{yz}*M_z oppure k_{zz}*M_z
 N_{Rd} [kg] :Resistenza instabilità a compressione ⁽²⁾
 M_{yRd} [kg*m] :Momento resistente all'instabilità in direzione Y ⁽²⁾
 M_{zRd} [kg*m] :Momento resistente all'instabilità in direzione Z ⁽²⁾
 SF Coefficiente di sicurezza (asta verificata se >=1)
 Comb Combinazione di carico: quando Comb non è sismica è individuata dal codice [C], quando è sismica è individuata dal codice [(Cx+Cy) Cm Sc].
 - C Individua la Combinazione di Carico non sismica (1, 2, ecc. come da scenario);
 - Cx Individua la Combinazione di Carico sismica in direzione x (SismaX, come da scenario);
 - Cy Individua la Combinazione di Carico sismica in direzione y (SismaY, come da scenario);
 - Cm Individua la Combinazione spostamento masse (I, II, III, IV, V, ecc. come da Combinazioni Sisma in Spostamento masse impalcato);
 - Sc Individua la sottocombinazione ottenuta mediante la permutazione dei segni (1, 2, 3, 4, 5, 6, 7, 8):
 1) Sc = + SismaZ*f_z + SismaX*f_x + SismaY*f_y
 2) Sc = + SismaZ*f_z + SismaX*f_x - SismaY*f_y
 3) Sc = + SismaZ*f_z - SismaX*f_x + SismaY*f_y
 4) Sc = + SismaZ*f_z - SismaX*f_x - SismaY*f_y
 5) Sc = - SismaZ*f_z + SismaX*f_x + SismaY*f_y
 6) Sc = - SismaZ*f_z + SismaX*f_x - SismaY*f_y
 7) Sc = - SismaZ*f_z - SismaX*f_x + SismaY*f_y
 8) Sc = - SismaZ*f_z - SismaX*f_x - SismaY*f_y.

Le ultime quattro sono assenti quando non è richiesto il contributo del sisma in direzione verticale. Le combinazioni delle azioni sismiche così ottenute vengono combinate con i carichi verticali (come da scenario).

Note:

- (¹) Y è l'asse forte della sezione, e Z l'asse debole della sezione; i valori da utilizzare per le resistenze sono $N_{Rk}=f_y \cdot A, M_{yRk}=f_y \cdot W_y, M_{zRk}=f_y \cdot W_z$ dove:

Classe	1	2	3	4
A	A	A	A	A _{eff}
W _y	W _{pl,y}	W _{pl,y}	W _{el,y}	W _{el,y,eff}
W _z	W _{pl,z}	W _{pl,z}	W _{el,z}	W _{el,z,eff}

- (²) le equazioni di verifica, le azioni e le resistenze di progetto sono date dalle seguenti equazioni:

$$\frac{N_{ed}}{\frac{\chi_y N_{Rk}}{\gamma_{M1}}} + k_{yy} \frac{M_{y,Ed}}{\chi_{LT} \frac{M_{yRk}}{\gamma_{M1}}} + k_{yz} \frac{M_{z,Ed}}{\frac{M_{zRk}}{\gamma_{M1}}} \leq 1$$

$$\frac{N_{ed}}{\frac{\chi_z N_{Rk}}{\gamma_{M1}}} + k_{zy} \frac{M_{y,Ed}}{\chi_{LT} \frac{M_{yRk}}{\gamma_{M1}}} + k_{zz} \frac{M_{z,Ed}}{\frac{M_{zRk}}{\gamma_{M1}}} \leq 1$$

$$N_{Rdy} = \frac{\chi_y N_{Rk}}{\gamma_{M1}} \quad M_{yRd} = \frac{\chi_{LT} M_{yRk}}{\gamma_{M1}} \quad M_{zRd} = \frac{M_{yRk}}{\gamma_{M1}}$$

$$M_{yyEq} = k_{yy} M_{yEd} \quad M_{yzEq} = k_{yz} M_{z,Ed}$$

$$M_{zyEq} = k_{zy} M_{yEd} \quad M_{zzEq} = k_{zz} M_{z,Ed}$$

$$\frac{N_{ed}}{N_{Rdy}} + \frac{M_{yyEq}}{M_{yRd}} + \frac{M_{yzEq}}{M_{zRd}} \leq 1$$

$$\frac{N_{ed}}{N_{Rdz}} + \frac{M_{zyEq}}{M_{yRd}} + \frac{M_{zzEq}}{M_{zRd}} \leq 1$$

Asta: 101 [6,13] Sez. G: HE 260 B L=756.1 cm Ln1=756.1 cm Ln2=756.1 cm Crit.: Acciaio_Pressflessione
 $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² :**Verificato**
 SF_λ=1.742

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-0	14514	-0	325722	35301	16565	67	115	0.73 9	0.37 9	--	0.95 0	0.60 0	0.57 0	1.00 0

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	0	13789	0	229286	33620	15776	2	2.4
1	Z	0	8273	0	117671	33620	15776	2	4.1

Asta: 101 [13,26] Sez. G: HE 260 B L=342.5 cm Ln1=342.5 cm Ln2=342.5 cm Crit.: Acciaio_Pressflessione
 $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² :**Verificato**
 SF_λ=3.844

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-0	4565	0	325722	35301	16565	31	52	0.94 5	0.78 6	--	0.60 3	0.24 0	0.36 2	0.40 0

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	0	2755	0	293110	33620	15776	(8+9)-I-1	12
1	Z	0	1653	0	243767	33620	15776	(8+9)-I-1	20

Asta: 102 [5,12] Sez. G: HE 260 B L=756.4 cm Ln1=756.4 cm Ln2=756.4 cm Crit.: Acciaio_Pressflessione
 $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² :**Verificato**
 SF_λ=1.741

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-0	19001	0	325722	35301	16565	67	115	0.73 9	0.37 9	--	0.58 5	0.36 0	0.35 1	0.60 0

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	0	11123	0	229235	33620	15776	2	3.0
1	Z	0	6674	0	117612	33620	15776	2	5.0

Asta: 102 [12,110] Sez. G: HE 260 B L=827.6 cm Ln1=827.6 cm Ln2=827.6 cm Crit.:
 Acciaio_Pressflessione $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² :**Verificato**
 SF_λ=1.591

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-0	18974	-0	325722	35301	16565	74	126	0.69 4	0.33 2	--	0.45 8	0.55 3	0.27 5	0.92 1

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	0	8685	0	215138	33620	15776	2	3.9
1	Z	0	5211	0	102997	33620	15776	2	6.5

Asta: 103 [4,11] Sez. G: HE 260 B L=755.5 cm Ln1=755.5 cm Ln2=755.5 cm Crit.: Acciaio_Pressflessione
 $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² :**Verificato**
 SF_λ=1.743

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kyz	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-0	6607	-0	325722	35301	16565	67	115	0.73 9	0.38 0	--	0.53 7	0.36 0	0.32 2	0.60 0

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	0	3545	0	229395	33620	15776	(8+9)-VI-4	9.5
1	Z	0	2127	0	117796	33620	15776	(8+9)-VI-4	16

Asta: 103 [11,18] Sez. G: HE 260 B L=785.8 cm Ln1=785.8 cm Ln2=785.8 cm Crit.: Acciaio_Pressflessione
 $\gamma M=1.05$ $f_y/k/\gamma M=2619$ kg/cm² $f_t=4300$ kg/cm² :**Verificato**
 SF_λ=1.676

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-0	20323	-0	325722	35301	16565	70	119	0.72 0	0.35 9	--	0.56 6	0.57 7	0.33 9	0.96 2

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	0	11499	0	223493	33620	15776	2	2.9
1	Z	0	6899	0	111287	33620	15776	2	4.9

Asta: 104 [3,10] Sez. G: HE 260 B L=755.5 cm Ln1=755.5 cm Ln2=755.5 cm Crit.: Acciaio_Pressflessione
 $\gamma M=1.05$ $f_y/k/\gamma M=2619$ kg/cm² $f_t=4300$ kg/cm² :**Verificato**
 SF_λ=1.743

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-0	17576	-0	325722	35301	16565	67	115	0.73 9	0.38 0	--	0.65 0	0.36 0	0.39 0	0.60 0

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	0	11428	0	229395	33620	15776	2	2.9
1	Z	0	6857	0	117796	33620	15776	2	4.9

Asta: 104 [10,17] Sez. G: HE 260 B L=740.3 cm Ln1=740.3 cm Ln2=740.3 cm Crit.: Acciaio_Pressflessione
 $\gamma M=1.05$ $f_y/k/\gamma M=2619$ kg/cm² $f_t=4300$ kg/cm² :**Verificato**
 SF_λ=1.779

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-0	9650	-0	325722	35301	16565	66	112	0.74 9	0.39 1	--	0.40 0	0.36 0	0.24 0	0.60 0

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	0	3860	0	232319	33620	15776	2	8.7
1	Z	0	2316	0	121252	33620	15776	2	15

Asta: 104 [17,3] Sez. G: HE 260 B L=460.3 cm Ln1=460.3 cm Ln2=460.3 cm Crit.: Acciaio_Pressflessione
 $\gamma M=1.05$ $f_y/k/\gamma M=2619$ kg/cm² $f_t=4300$ kg/cm² :**Verificato**
 SF_λ=2.861

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-1092	8449	-38	325722	35301	16565	41	70	0.89 6	0.65 9	--	0.40 0	0.24 1	0.24 0	0.40 2

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	1092	3383	9	278018	33620	15776	2	9.5
1	Z	1092	2030	15	204368	33620	15776	2	15

Asta: 104 [3,6] Sez. G: HE 260 B L=350.0 cm Ln1=350.0 cm Ln2=350.0 cm Crit.: Acciaio_Pressflessione
 $\gamma M=1.05$ $f_y/k/\gamma M=2619$ kg/cm² $f_t=4300$ kg/cm² :**Verificato**
 SF_λ=3.762

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-510	3160	5	325722	35301	16565	31	53	0.94 2	0.77 8	--	0.49 1	0.36 0	0.29 4	0.60 1

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	510	1550	2	292200	33620	15776	2	21
1	Z	510	930	3	241350	33620	15776	2	33

Asta: 105 [2,9] Sez. G: HE 260 B L=756.1 cm Ln1=756.1 cm Ln2=756.1 cm Crit.: Acciaio_Pressflessione
 $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² :**Verificato**
 SF _{λ} =1.742

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-0	16892	0	325722	35301	16565	67	115	0.73 9	0.37 9	--	0.68 8	0.36 0	0.41 3	0.60 0

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	0	11619	0	229286	33620	15776	2	2.9
1	Z	0	6972	0	117671	33620	15776	2	4.8

Asta: 105 [9,16] Sez. G: HE 260 B L=694.5 cm Ln1=694.5 cm Ln2=694.5 cm Crit.: Acciaio_Pressflessione
 $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² :**Verificato**
 SF _{λ} =1.896

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-0	16755	0	325722	35301	16565	62	105	0.77 6	0.42 7	--	0.40 0	0.24 0	0.24 0	0.40 0

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	0	6702	0	240857	33620	15776	2	5.0
1	Z	0	4021	0	132350	33620	15776	2	8.4

Asta: 105 [16,2] Sez. G: HE 260 B L=461.7 cm Ln1=461.7 cm Ln2=461.7 cm Crit.: Acciaio_Pressflessione
 $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² :**Verificato**
 SF _{λ} =2.852

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-737	6813	102	325722	35301	16565	41	70	0.89 6	0.65 7	--	0.40 0	0.26 8	0.24 0	0.44 7

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	737	2727	27	277832	33620	15776	2	12
1	Z	737	1636	46	203903	33620	15776	2	18

Asta: 105 [2,5] Sez. G: HE 260 B L=350.0 cm Ln1=350.0 cm Ln2=350.0 cm Crit.: Acciaio_Pressflessione
 $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² :**Verificato**
 SF _{λ} =3.762

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-481	2879	-18	325722	35301	16565	31	53	0.94 2	0.77 8	--	0.66 5	0.36 0	0.39 9	0.60 1

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	481	1914	7	292201	33620	15776	2	17
1	Z	481	1148	11	241350	33620	15776	2	27

Asta: 106 [1,8] Sez. G: HE 260 B L=756.1 cm Ln1=756.1 cm Ln2=756.1 cm Crit.: Acciaio_Pressflessione
 $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² :**Verificato**
 SF_λ=1.742

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-0	5365	-0	325722	35301	16565	67	115	0.73 9	0.37 9	--	0.75 5	0.36 0	0.45 3	0.60 0

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	0	4051	0	229286	33620	15776	(8+9)-VII-2	8.3
1	Z	0	2430	0	117671	33620	15776	(8+9)-VII-2	14

Asta: 106 [8,15] Sez. G: HE 260 B L=651.8 cm Ln1=651.8 cm Ln2=651.8 cm Crit.: Acciaio_Pressflessione
 $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² :**Verificato**
 SF_λ=2.020

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-0	9965	-0	325722	35301	16565	58	99	0.80 1	0.46 3	--	0.40 0	0.36 0	0.24 0	0.60 0

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	0	3986	0	248459	33620	15776	2	8.4
1	Z	0	2392	0	143695	33620	15776	2	14

Asta: 106 [15,1] Sez. G: HE 260 B L=459.8 cm Ln1=459.8 cm Ln2=459.8 cm Crit.: Acciaio_Pressflessione
 $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² :**Verificato**
 SF_λ=2.864

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-707	5248	45	325722	35301	16565	41	70	0.89 6	0.65 9	--	0.40 0	0.24 1	0.24 0	0.40 1

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	707	2101	11	278094	33620	15776	2	15
1	Z	707	1260	18	204557	33620	15776	2	24

Asta: 106 [1,4] Sez. G: HE 260 B L=350.0 cm Ln1=350.0 cm Ln2=350.0 cm Crit.: Acciaio_Pressflessione
 $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² :**Verificato**
 SF_λ=3.762

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-420	2536	-16	325722	35301	16565	31	53	0.94 2	0.77 8	--	0.61 5	0.36 0	0.36 9	0.60 1

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	420	1560	6	292201	33620	15776	2	21
1	Z	420	936	10	241350	33620	15776	2	33

Asta: 107 [7,25] Sez. G: HE 260 B L=632.4 cm Ln1=632.4 cm Ln2=632.4 cm Crit.: Acciaio_Pressflessione
 $\gamma M=1.05$ fyk/ $\gamma M=2619$ kg/cm² ft=4300 kg/cm² :**Verificato**
 SF_λ=2.082

N	My	Mz	NRk	MyRk	MzRk	λY	λZ	χY	χZ	χLT	kyy	kzy	kzy	kzz
kg	kg*m	kg*m	kg	kg*m	kg*m									
-0	-3378	0	325722	35301	16565	56	96	0.81 2	0.48 1	--	0.93 9	0.36 0	0.56 3	0.60 0

Cls	Dir	N	Myeq	Mzeq	NRd	MyRd	MzRd	Comb.	SF
		kg	kg*m	kg*m	kg	kg*m	kg*m		
1	Y	0	3171	0	251792	33620	15776	(8+9)-VII-4	11
1	Z	0	1902	0	149168	33620	15776	(8+9)-VII-4	18

Verifica Resistenza aste Metalliche

Scenario di calcolo: **Set_NT_SLV_SLD_A2_STR/GEO_2018**

Simbologia

L [cm]	Lunghezza teorica elemento (da nodo a nodo)
Sez. G	Sezione Generica (Sigla)
fyd [kg/cm ²]	Tensione di progetto snervamento acciaio
ft [kg/cm ²]	Tensione di rottura acciaio
γ_M	Coefficiente di sicurezza acciaio
X [cm]	Punto di verifica
N [kg]	Sforzo Normale
TY [kg]	Taglio dir Y
TZ [kg]	Taglio dir Z
MT [kg*m]	Momento torcente
MY [kg*m]	Momento flettente dir Y
MZ [kg*m]	Momento flettente dir Z
MY4 [kg*m]	Momento flettente dir Y + N* Δe_z , per sezioni di classe 4
MZ4 [kg*m]	Momento flettente dir Z + N* Δe_y , per sezioni di classe 4
cls	Classe della sezione per la sollecitazione della combinazione corrente
Comb.	Combinazione della sollecitazione
Nr [kg]	Sforzo Normale resistente
Vyr [kg]	Taglio resistente in dir Y
Vzr [kg]	Taglio resistente dir Z
Mry [kg*m]	Momento flettente resistente dir Y
Mrz [kg*m]	Momento flettente resistente dir Z
SF_V	Coefficiente di sicurezza taglio
SF_M	Coefficiente di sicurezza pressoflessione
SF	Coefficiente di sicurezza complessivo (asta verificata se ≥ 1)(¹)

Gerarchia travi/pilastri (quando richiesto):

NEd [kg]	Sforzo Normale di verifica
Npl,Rd [kg]	Sforzo Normale resistente (NTC 4.2.4.1.2)
VEdY(*) [kg]	Taglio trave dir Y dovuto ai momenti ultimi Mpl,RdZ di estremità (cfr. NTC f.(7.5.5))
Vpl,RdY [kg]	Taglio resistente dir Y (NTC 4.2.4.1.2)
VEdZ(*) [kg]	Taglio trave dir Z dovuto ai momenti ultimi Mpl,RdY di estremità (cfr. NTC f.(7.5.5))
Vpl,RdZ [kg]	Taglio resistente dir Z (NTC 4.2.4.1.2)
MEdY [kg*m]	Momento flettente dir Y
Mpl,RdY [kg*m]	Momento resistente dir Y (NTC 4.2.4.1.2)
MEdZ [kg*m]	Momento flettente dir Z
Mpl,RdZ [kg*m]	Momento resistente dir Z (NTC 4.2.4.1.2)

Verifiche Incendio:

Ky	fy(T)/fy(20°) fattore riduzione resistenza alla temperatura T
KE	E(T)/E(20) fattore riduzione modulo elastico alla temperatura T

SF	Coefficiente di sicurezza (asta verificata se ≥ 1)(²)
Ω^*	Smplicazione sollecitazioni sismiche (solo per $q > 1$)(³)
Fatt.Ampl.Sisma	Fattore moltiplicativo di gruppo per le azioni sismiche (solo se diverso da 1.0)

Note:

(¹): SF rappresenta il minimo tra SF_V ed SF_M dove:

- SF_V = VR/Vd con VR e Vd azione tagliante resistente ed agente
- SF_M = $1/[N/Nr + MY/Mry + MZ/Mrz]$, i valori di Mry ed Mrz sono ridotti opportunamente quando $Vd > 0.5 V_r$

(²): SF rappresenta il minimo tra i seguenti rapporti:

- MEdY/Mpl,RdY (travi)
- MEdZ/Mpl,RdZ (travi)
- NEd/(0.15*Npl,Rd) (travi)
- VEdY(*)/(0.5*Vpl,RdY) (travi)
- VEdZ(*)/(0.5*Vpl,RdZ) (travi)
- VEdY/(0.5*Vpl,RdY) (pilastri)
- VEdZ/(0.5*Vpl,RdZ) (pilastri)

(³): $\Omega^* = \min(q, 1.1 * \gamma_{ov} * \Omega)$, con Ω secondo NTC 7.5.4.2

Asta: 101 [6,13] Sez. G: HE 260 B L=756.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05 f_y k / \gamma M=2619$ kg/cmq
ft=4300 kg/cmq :**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
756	1	0	0	12213	-1	14514	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
756	1	310212	137565	56832	33620	15776	986	4.7	2.3	>100	2.3

Asta: 101 [13,26] Sez. G: HE 260 B L=342.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05 f_y k / \gamma M=2619$ kg/cmq ft=4300 kg/cmq :**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	0	0	-7693	-6	14059	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	310212	137283	56715	33620	15776	986	7.4	2.4	>100	2.4

Asta: 102 [5,12] Sez. G: HE 260 B L=756.4 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05 f_y k / \gamma M=2619$ kg/cmq ft=4300 kg/cmq :**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
756	1	0	0	13007	2	19001	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
756	1	310212	137510	56809	33620	15776	986	4.4	1.8	>100	1.8

Asta: 102 [12,110] Sez. G: HE 260 B L=827.6 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05 f_y k / \gamma M=2619$ kg/cmq ft=4300 kg/cmq :**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	0	0	-12345	1	18974	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	310212	137546	56824	33620	15776	986	4.6	1.8	>100	1.8

Asta: 103 [4,11] Sez. G: HE 260 B L=755.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05 f_y k / \gamma M=2619$ kg/cmq ft=4300 kg/cmq :**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
756	1	0	0	13170	-0	20174	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
756	1	310212	137597	56845	33620	15776	986	4.3	1.7	>100	1.7

Asta: 103 [11,18] Sez. G: HE 260 B L=785.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05 f_y k / \gamma M=2619$ kg/cmq ft=4300 kg/cmq :**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	0	0	-13317	-2	20323	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	310212	137476	56795	33620	15776	986	4.3	1.7	>100	1.7

Asta: 104 [3,10] Sez. G: HE 260 B L=755.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05 f_y k / \gamma M=2619$ kg/cm² $f_t=4300$ kg/cm² :**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
756	1	0	0	12801	-1	17576	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
756	1	310212	137545	56824	33620	15776	986	4.4	1.9	>100	1.9

Asta: 104 [10,17] Sez. G: HE 260 B L=740.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05 f_y k / \gamma M=2619$ kg/cm² $f_t=4300$ kg/cm² :**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	0	0	-11493	0	17460	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	310212	137599	56846	33620	15776	986	4.9	1.9	>100	1.9

Asta: 104 [17,3] Sez. G: HE 260 B L=460.3 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05 f_y k / \gamma M=2619$ kg/cm² $f_t=4300$ kg/cm² :**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	1301	-13	-7712	-0	8449	-38	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	310212	137596	56845	33620	15776	986	7.4	3.9	>100	3.9

Asta: 104 [3,6] Sez. G: HE 260 B L=350.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05 f_y k / \gamma M=2619$ kg/cm² $f_t=4300$ kg/cm² :**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	659	1	-4350	-0	3160	5	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	310212	137599	56846	33620	15776	986	13	10	>100	10

Asta: 105 [2,9] Sez. G: HE 260 B L=756.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05 f_y k / \gamma M=2619$ kg/cm² $f_t=4300$ kg/cm² :**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
756	1	0	0	12719	1	16892	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
756	1	310212	137523	56814	33620	15776	986	4.5	2.0	>100	2.0

Asta: 105 [9,16] Sez. G: HE 260 B L=694.5 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05 f_y k / \gamma M=2619$ kg/cm² $f_t=4300$ kg/cm² :**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	0	0	-11054	-1	16755	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	310212	137545	56823	33620	15776	986	5.1	2.0	>100	2.0

Asta: 105 [16,2] Sez. G: HE 260 B L=461.7 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ $f_y k / \gamma M=2619$ kg/cm² $f_t=4300$ kg/cm² :**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	1151	31	-5716	2	6813	102	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	310212	137513	56810	33620	15776	986	9.9	4.7	>100	4.7

Asta: 105 [2,5] Sez. G: HE 260 B L=350.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ $f_y k / \gamma M=2619$ kg/cm² $f_t=4300$ kg/cm² :**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	837	-5	-4486	-0	2879	-18	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	310212	137599	56845	33620	15776	986	13	11	>100	11

Asta: 106 [1,8] Sez. G: HE 260 B L=756.1 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ $f_y k / \gamma M=2619$ kg/cm² $f_t=4300$ kg/cm² :**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
756	1	0	0	13109	0	16616	0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
756	1	310212	137595	56844	33620	15776	986	4.3	2.0	>100	2.0

Asta: 106 [8,15] Sez. G: HE 260 B L=651.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ $f_y k / \gamma M=2619$ kg/cm² $f_t=4300$ kg/cm² :**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	0	0	-10561	-0	16309	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	310212	137589	56842	33620	15776	986	5.4	2.1	>100	2.1

Asta: 106 [15,1] Sez. G: HE 260 B L=459.8 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ $f_y k / \gamma M=2619$ kg/cm² $f_t=4300$ kg/cm² :**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	983	16	-4945	0	5248	45	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	310212	137598	56845	33620	15776	986	11	6.2	>100	6.2

Asta: 106 [1,4] Sez. G: HE 260 B L=350.0 cm Crit.: Acciaio_Pressflessione $\gamma M=1.05$ $f_y k / \gamma M=2619$ kg/cm² $f_t=4300$ kg/cm² :**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
0	1	686	-5	-3782	1	2536	-16	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
0	1	310212	137566	56832	33620	15776	986	15	13	>100	13

Asta: 107 [7,25] Sez. G: HE 260 B L=632.4 cm Crit.: Acciaio_Pressflessione $\gamma_M=1.05$ $f_yk/\gamma_M=2619$ kg/cm² $f_t=4300$ kg/cm² :**Verificato**

X	cls	N	TY	TZ	MT	MY	MZ	My4	Mz4	Comb.
cm		kg	kg	kg	kg*m	kg*m	kg*m			
253	1	0	0	-762	15	-9947	-0	--	--	2

X	cls	Nr	Vyr	Vzr	Mry	Mrz	MTrd	SF_V.	SF_M	SF_Mt	SF
cm		kg	kg	kg	kg*m	kg*m	kg*m				
253	1	310212	136753	56496	33620	15776	986	74	3.4	65	3.4

Verifiche stato limite di esercizio

Verifica dei Muri (Stati limite esercizio)

Scenario di calcolo: **Set_NT_SLV_SLD_A2_STR/GEO_2018**

Simbologia

P.	Numero pannello
Nx [kg/mq]	Sforzo normale in direzione x
Ny [kg/mq]	Sforzo normale in direzione y
Nxy [kg/mq]	Sforzo tagliante in direzione xy
Mx [kg]	Momento flettente in direzione x
My [kg]	Momento flettente in direzione y
Mxy [kg]	Momento torcente
Afx [cmq/m]	Area acciaio in direzione x per metro lineare
Afy [cmq/m]	Area acciaio in direzione y per metro lineare
σ_{max} [kg/cm ²]	Tensione massima nel calcestruzzo
σ_{sfmax} [kg/cm ²]	Tensione massima nell'acciaio
σ_{sc} [kg/cm ²]	Tensione nel calcestruzzo compresso
σ_{sct} [kg/cm ²]	Tensione nel calcestruzzo teso (quando richiesto dalla verifica)
σ_{sca} [kg/cm ²]	Tensione ammissibile nel calcestruzzo
σ_{sfa} [kg/cm ²]	Tensione ammissibile nell'acciaio
σ_{scta} [kg/cm ²]	Tensione ammissibile nel calcestruzzo teso
Cbc	Combinazione generatore tensione massima cls
Cbf	Combinazione generatore tensione massima acciaio
Cb	Combinazione
σ_{sfmed} [kg/cm ²]	Tensione media dell'acciaio
Wd [mm]	Apertura delle fessure
Wk [mm]	Apertura caratteristica delle fessure
Wamm_Freq [mm]	Apertura ammissibile delle fessure per combinazione Frequente
Wamm_Qp [mm]	Apertura ammissibile delle fessure per combinazione Quasi Permanente
Wamm_Rara [mm]	Apertura ammissibile delle fessure per combinazione Rara
Cs	Coefficiente di sicurezza definito come minimo di σ_{Amm}/σ tra acciaio e calcestruzzo oppure Wamm/Wk

Muro [Platea]: 1 - Nodi: [15-7-5-6-21-25-24-23-22-18-17-16]Pann=439Spess.=25 cm, Terreno=Terreno1,
,Criterio=CLS_Platee, Materiale=C30/37

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=149 σ_{fa} [kg/cm²]=3600

P.	Nx	Ny	Nxy	Mx	My	Mxy	Afx	Afy	σ_{cmax}	σ_{fmax}	Cbc	Cbf	Ver	Cs
	kg/mq	kg/mq	kg/mq	kg	kg	kg	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
35	2359	-7999	891	-205	-1321	-0	13.40	16.08	-21	726	14	15	Si	5.0

Combinazione QP: σ_{ca} [kg/cm²]=112 σ_{fa} [kg/cm²]=3600

P.	Nx	Ny	Nxy	Mx	My	Mxy	Afx	Afy	σ_{cmax}	σ_{fmax}	Cbc	Cbf	Ver	Cs
	kg/mq	kg/mq	kg/mq	kg	kg	kg	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
35	2359	-7999	891	-205	-1321	-0	13.40	16.08	-21	726	24	24	Si	5.0

Verifica aperture fessure:Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	kg/mq	kg/mq	kg/mq	kg	kg	kg	kg/cm ²	mm	mm			
35	2359	-7999	891	-205	-1321	-0	726	0.060	0.060	24(Qp)	Si	5.0
35	2359	-7999	891	-205	-1321	-0	726	0.060	0.060	16(Fr)	Si	6.7

Muro [Platea]: 2 - Nodi: [21-6-14-19-20-8-31-30-29-28-27-26]Pann=449Spess.=25 cm, Terreno=Terreno1,
,Criterio=CLS_Platee, Materiale=C30/37

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=149 σ_{fa} [kg/cm²]=3600

P.	Nx	Ny	Nxy	Mx	My	Mxy	Afx	Afy	σ_{cmax}	σ_{fmax}	Cbc	Cbf	Ver	Cs
	kg/mq	kg/mq	kg/mq	kg	kg	kg	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
76	3867	-3607	67	-198	-1190	-1	13.40	16.08	-19	708	14	15	Si	5.1
22	3405	-1489	-2932	-188	-659	-114	13.40	16.08	-10	743	14	13	Si	4.8

Combinazione QP: σ_{ca} [kg/cm²]=112 σ_{fa} [kg/cm²]=3600

P.	Nx	Ny	Nxy	Mx	My	Mxy	Afx	Afy	σ_{cmax}	σ_{fmax}	Cbc	Cbf	Ver	Cs
	kg/mq	kg/mq	kg/mq	kg	kg	kg	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
76	3867	-3607	67	-198	-1190	-1	13.40	16.08	-19	708	24	24	Si	5.1

Verifica aperture fessure:Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	kg/mq	kg/mq	kg/mq	kg	kg	kg	kg/cm ²	mm	mm			
62	-4409	20927	5102	64	-266	-81	509	0.061	0.061	24(Qp)	Si	4.9
62	-4409	20927	5102	64	-266	-81	509	0.061	0.061	16(Fr)	Si	6.6

Muro [Platea]: 3 - Nodi: [8-20-19-14-12-35-36-11-10-9]Pann=206Spess.=25 cm, Terreno=Terreno1,
,Criterio=CLS_Platee, Materiale=C30/37

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=149 σ_{fa} [kg/cm²]=3600

P.	Nx	Ny	Nxy	Mx	My	Mxy	Afx	Afy	σ_{cmax}	σ_{fmax}	Cbc	Cbf	Ver	Cs
	kg/mq	kg/mq	kg/mq	kg	kg	kg	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
7	4645	-1789	-1349	-150	-666	10	13.40	16.08	-10	727	14	13	Si	5.0

Combinazione QP: σ_{ca} [kg/cm²]=112 σ_{fa} [kg/cm²]=3600

P.	Nx	Ny	Nxy	Mx	My	Mxy	Afx	Afy	σ_{cmax}	σ_{fmax}	Cbc	Cbf	Ver	Cs
	kg/mq	kg/mq	kg/mq	kg	kg	kg	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
7	4645	-1789	-1349	-150	-666	10	13.40	16.08	-10	400	24	24	Si	9.0
62	3351	-132	-81	-127	-628	-12	13.40	16.08	-10	401	24	24	Si	9.0

Verifica aperture fessure: Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	kg/mq	kg/mq	kg/mq	kg	kg	kg	kg/cm ²	mm	mm			
55	-2379	13929	768	11	-203	-39	356	0.041	0.041	24(Qp)	Si	7.4
55	-2379	13929	768	11	-203	-39	356	0.041	0.041	16(Fr)	Si	9.9

Muro [Platea]: 4 - Nodi: [11-36-35-12-13-34-33-32] Pann=130 Spess.=25 cm, Terreno=Terreno1,
, Criterio=CLS_Platee, Materiale=C30/37

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=149 σ_{fa} [kg/cm²]=3600

P.	Nx	Ny	Nxy	Mx	My	Mxy	Afx	Afy	σ_{cmax}	σ_{fmax}	Cbc	Cbf	Ver	Cs
	kg/mq	kg/mq	kg/mq	kg	kg	kg	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
10	34	-4298	-1626	-67	-416	5	13.40	16.08	-7	202	14	15	Si	18

Combinazione QP: σ_{ca} [kg/cm²]=112 σ_{fa} [kg/cm²]=3600

P.	Nx	Ny	Nxy	Mx	My	Mxy	Afx	Afy	σ_{cmax}	σ_{fmax}	Cbc	Cbf	Ver	Cs
	kg/mq	kg/mq	kg/mq	kg	kg	kg	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
10	34	-4298	-1626	-67	-416	5	13.40	16.08	-7	202	24	24	Si	17

Verifica aperture fessure: Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	kg/mq	kg/mq	kg/mq	kg	kg	kg	kg/cm ²	mm	mm			
10	34	-4298	-1626	-67	-416	5	202	0.016	0.016	24(Qp)	Si	18
10	34	-4298	-1626	-67	-416	5	202	0.016	0.016	16(Fr)	Si	25

Muro [Platea]: 5 - Nodi: [6-106-114-112-213-13-12-14] Pann=104 Spess.=25 cm, Terreno=Terreno1,
, Criterio=CLS_Platee, Materiale=C30/37

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=149 σ_{fa} [kg/cm²]=3600

P.	Nx	Ny	Nxy	Mx	My	Mxy	Afx	Afy	σ_{cmax}	σ_{fmax}	Cbc	Cbf	Ver	Cs
	kg/mq	kg/mq	kg/mq	kg	kg	kg	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
5	1535	-551	-2206	-338	-37	12	13.40	16.08	-6	397	10	15	Si	9.1

Combinazione QP: σ_{ca} [kg/cm²]=112 σ_{fa} [kg/cm²]=3600

P.	Nx	Ny	Nxy	Mx	My	Mxy	Afx	Afy	σ_{cmax}	σ_{fmax}	Cbc	Cbf	Ver	Cs
	kg/mq	kg/mq	kg/mq	kg	kg	kg	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
5	4095	220	-730	-417	-51	-4	13.40	16.08	-7	397	24	24	Si	9.1

Verifica aperture fessure: Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	kg/mq	kg/mq	kg/mq	kg	kg	kg	kg/cm ²	mm	mm			
5	4095	220	-730	-417	-51	-4	397	0.041	0.041	24(Qp)	Si	7.3
5	4095	220	-730	-417	-51	-4	397	0.041	0.041	16(Fr)	Si	9.7

Muro [Platea]: 6 - Nodi: [13-213-113-134-34] Pann=59 Spess.=25 cm, Terreno=Terreno1,
, Criterio=CLS_Platee, Materiale=C30/37

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=149 σ_{fa} [kg/cm²]=3600

P.	Nx	Ny	Nxy	Mx	My	Mxy	Afx	Afy	σ_{cmax}	σ_{fmax}	Cbc	Cbf	Ver	Cs
	kg/mq	kg/mq	kg/mq	kg	kg	kg	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
4	4754	4072	3505	-286	-247	-205	13.40	16.08	-4	347	10	15	Si	10

Combinazione QP: $\sigma_{ca}[\text{kg/cm}^2]=112$ $\sigma_{fa}[\text{kg/cm}^2]=3600$

P.	Nx	Ny	Nxy	Mx	My	Mxy	Afx	Afy	σ_{cmax}	σ_{fmax}	Cbc	Cbf	Ver	Cs
	kg/mq	kg/mq	kg/mq	kg	kg	kg	cmq/m	cmq/m	kg/cmq	kg/cmq				
4	5482	4344	3893	-316	-274	-227	13.40	16.08	-5	347	24	24	Si	10

Verifica aperture fessure: Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	kg/mq	kg/mq	kg/mq	kg	kg	kg	kg/cmq	mm	mm			
29	9573	-3692	6033	-113	55	-77	272	0.039	0.039	24(Qp)	Si	7.7
29	9573	-3692	6033	-113	55	-77	272	0.039	0.039	16(Fr)	Si	10

Muro : 7 - Nodi: [106-114-214-206], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri, Materiale=C30/37

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: $\sigma_{ca}[\text{kg/cm}^2]=149$ $\sigma_{fa}[\text{kg/cm}^2]=3600$

P.	Nx	Ny	Nxy	Mx	My	Mxy	Afx	Afy	σ_{cmax}	σ_{fmax}	Cbc	Cbf	Ver	Cs
	kg/mq	kg/mq	kg/mq	kg	kg	kg	cmq/m	cmq/m	kg/cmq	kg/cmq				
1	-478	-4507	-8171	43	349	-9	13.40	16.08	-4	102	14	15	Si	35
9	-641	-6924	-8249	36	287	5	13.40	16.08	-3	140	10	15	Si	26

Combinazione QP: $\sigma_{ca}[\text{kg/cm}^2]=112$ $\sigma_{fa}[\text{kg/cm}^2]=3600$

P.	Nx	Ny	Nxy	Mx	My	Mxy	Afx	Afy	σ_{cmax}	σ_{fmax}	Cbc	Cbf	Ver	Cs
	kg/mq	kg/mq	kg/mq	kg	kg	kg	cmq/m	cmq/m	kg/cmq	kg/cmq				
9	-500	-5753	-9787	59	466	-1	13.40	16.08	-5	140	24	24	Si	22

Verifica aperture fessure: Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	kg/mq	kg/mq	kg/mq	kg	kg	kg	kg/cmq	mm	mm			
9	-500	-5753	-9787	59	466	-1	140	0.013	0.013	24(Qp)	Si	24
9	-500	-5753	-9787	59	466	-1	140	0.013	0.013	16(Fr)	Si	32

Muro : 8 - Nodi: [114-112-212-214], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri, Materiale=C30/37

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: $\sigma_{ca}[\text{kg/cm}^2]=149$ $\sigma_{fa}[\text{kg/cm}^2]=3600$

P.	Nx	Ny	Nxy	Mx	My	Mxy	Afx	Afy	σ_{cmax}	σ_{fmax}	Cbc	Cbf	Ver	Cs
	kg/mq	kg/mq	kg/mq	kg	kg	kg	cmq/m	cmq/m	kg/cmq	kg/cmq				
9	-587	-5163	-4960	11	248	-37	13.40	16.08	-3	104	10	15	Si	35
5	-647	-4520	-5623	12	216	30	13.40	16.08	-2	110	10	15	Si	33

Combinazione QP: $\sigma_{ca}[\text{kg/cm}^2]=112$ $\sigma_{fa}[\text{kg/cm}^2]=3600$

P.	Nx	Ny	Nxy	Mx	My	Mxy	Afx	Afy	σ_{cmax}	σ_{fmax}	Cbc	Cbf	Ver	Cs
	kg/mq	kg/mq	kg/mq	kg	kg	kg	cmq/m	cmq/m	kg/cmq	kg/cmq				
5	-656	-4771	-6708	38	373	23	13.40	16.08	-4	110	24	24	Si	27

Verifica aperture fessure: Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	kg/mq	kg/mq	kg/mq	kg	kg	kg	kg/cmq	mm	mm			
5	-656	-4771	-6708	38	373	23	110	0.010	0.010	24(Qp)	Si	31
5	-656	-4771	-6708	38	373	23	110	0.010	0.010	16(Fr)	Si	41

Muro : 9 - Nodi: [112-213-313-212], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri,

Materiale=C30/37

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=149 σ_{fa} [kg/cm²]=3600

P.	Nx	Ny	Nxy	Mx	My	Mxy	Afx	Afy	σ_{cmax}	σ_{fmax}	Cbc	Cbf	Ver	Cs
	kg/mq	kg/mq	kg/mq	kg	kg	kg	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
5	-659	-5339	-2718	11	308	48	13.40	16.08	-3	98	10	15	Si	37

Combinazione QP: σ_{ca} [kg/cm²]=112 σ_{fa} [kg/cm²]=3600

P.	Nx	Ny	Nxy	Mx	My	Mxy	Afx	Afy	σ_{cmax}	σ_{fmax}	Cbc	Cbf	Ver	Cs
	kg/mq	kg/mq	kg/mq	kg	kg	kg	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
5	-648	-5173	-3387	22	363	47	13.40	16.08	-4	98	24	24	Si	28

Verifica aperture fessure:Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	kg/mq	kg/mq	kg/mq	kg	kg	kg	kg/cm ²	mm	mm			
5	-648	-5173	-3387	22	363	47	98	0.009	0.009	24(Qp)	Si	35
5	-648	-5173	-3387	22	363	47	98	0.009	0.009	16(Fr)	Si	47

Muro : 10 - Nodi: [213-113-213-313], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri, Materiale=C30/37

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=149 σ_{fa} [kg/cm²]=3600

P.	Nx	Ny	Nxy	Mx	My	Mxy	Afx	Afy	σ_{cmax}	σ_{fmax}	Cbc	Cbf	Ver	Cs
	kg/mq	kg/mq	kg/mq	kg	kg	kg	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
13	-283	-6406	-934	33	212	-16	13.40	16.08	-2	30	10	15	Si	69
1	1851	-917	1674	24	156	4	13.40	16.08	-2	90	10	15	Si	40

Combinazione QP: σ_{ca} [kg/cm²]=112 σ_{fa} [kg/cm²]=3600

P.	Nx	Ny	Nxy	Mx	My	Mxy	Afx	Afy	σ_{cmax}	σ_{fmax}	Cbc	Cbf	Ver	Cs
	kg/mq	kg/mq	kg/mq	kg	kg	kg	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
13	-213	-6318	-958	35	245	-16	13.40	16.08	-3	30	24	24	Si	44
1	2185	44	1844	23	174	2	13.40	16.08	-2	90	24	24	Si	40

Verifica aperture fessure:Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	kg/mq	kg/mq	kg/mq	kg	kg	kg	kg/cm ²	mm	mm			
1	2185	44	1844	23	174	2	64	0.011	0.011	24(Qp)	Si	27
1	2185	44	1844	23	174	2	64	0.011	0.011	16(Fr)	Si	36

Muro : 11 - Nodi: [113-134-234-213], Pann.X=4, Pann.Y=4Spess.=30 cm, Terreno=--,Criterio=CLS_Muri, Materiale=C30/37

Armatura a maglia doppia, Stampa elementi piu' gravosi

Combinazione Rara: σ_{ca} [kg/cm²]=149 σ_{fa} [kg/cm²]=3600

P.	Nx	Ny	Nxy	Mx	My	Mxy	Afx	Afy	σ_{cmax}	σ_{fmax}	Cbc	Cbf	Ver	Cs
	kg/mq	kg/mq	kg/mq	kg	kg	kg	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
13	-1108	-6497	1864	74	438	-57	13.40	16.08	-5	161	10	15	Si	22

Combinazione QP: σ_{ca} [kg/cm²]=112 σ_{fa} [kg/cm²]=3600

P.	Nx	Ny	Nxy	Mx	My	Mxy	Afx	Afy	σ_{cmax}	σ_{fmax}	Cbc	Cbf	Ver	Cs
	kg/mq	kg/mq	kg/mq	kg	kg	kg	cmq/m	cmq/m	kg/cm ²	kg/cm ²				
13	-1130	-6451	1948	83	530	-53	13.40	16.08	-6	161	24	24	Si	19

Verifica aperture fessure: Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

P.	Nx	Ny	Nxy	Mx	My	Mxy	σ_{fmed}	Wd	Wk	Cb	Ver	Cs
	kg/mq	kg/mq	kg/mq	kg	kg	kg	kg/cm ²	mm	mm			
13	-1130	-6451	1948	83	530	-53	161	0.014	0.014	24(Qp)	Si	21
13	-1130	-6451	1948	83	530	-53	161	0.014	0.014	16(Fr)	Si	28

Verifica spostamenti verticali delle aste in Acciaio secondo NTC 2008

Scenario di calcolo: **Set_NT_SLV_SLD_A2_STR/GEO_2018**

Simbologia:

- L Luce della trave a cui appartiene l'asta
- δ_c Monta iniziale della trave
- x Ascissa, nel sistema locale dell'asta, corrispondente allo spostamento massimo
- Comb. Combinazione/i di carico Rara/e
- δ_{max} Spostamento nello stato finale depurato della monta iniziale (positivo se diretto verso il basso)
- δ_2 Spostamento elastico dovuto ai soli carichi variabili (positivo se diretto verso il basso)
- L/k: Valore limite
- N.b. La verifica è soddisfatta se il valore assoluto degli spostamenti è inferiore al limite

Travata: 101 [6,13]: L=756.1 cm, Modello =Appoggiata, Crit.Prog: Acciaio_Pressflessione, $\delta c = 0.0$ cm:
Verificato

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
378.1	13	14.59	30.24	2.1

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
378.1	13	7.55	25.20	3.3

Travata: 102 [5,12]: L=756.4 cm, Modello =Appoggiata, Crit.Prog: Acciaio_Pressflessione, $\delta c = 0.0$ cm:
Verificato

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
302.5	13	11.53	30.25	2.6

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
302.5	13	5.98	25.21	4.2

Travata: 102 [12,110]: L=827.6 cm, Modello =Appoggiata, Crit.Prog: Acciaio_Pressflessione, $\delta c = 0.0$ cm:
Verificato

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
413.8	13	9.25	33.10	3.6

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
413.8	13	4.73	27.59	5.8

Travata: 103 [4,11]: L=755.5 cm, Modello =Appoggiata, Crit.Prog: Acciaio_Pressflessione, $\delta c = 0.0$ cm:
Verificato

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
302.2	13	10.68	30.22	2.8

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
302.2	13	5.53	25.18	4.6

Travata: 103 [11,18]: L=785.8 cm, Modello =Appoggiata, Crit.Prog: Acciaio_Pressflessione, $\delta c = 0.0$ cm:
Verificato

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
471.5	13	12.58	31.43	2.5

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
471.5	13	6.50	26.19	4.0

Travata: 104 [3,10]: L=755.5 cm, Modello =Appoggiata, Crit.Prog: Acciaio_Pressflessione, $\delta_c = 0.0$ cm:
Verificato

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
302.2	13	12.44	30.22	2.4

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
302.2	13	6.40	25.18	3.9

Travata: 104 [10,17]: L=740.3 cm, Modello =Appoggiata, Crit.Prog: Acciaio_Pressflessione, $\delta_c = 0.0$ cm:
Verificato

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
444.2	13	4.75	29.61	6.2

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
444.2	13	2.59	24.68	9.5

Travata: 105 [2,9]: L=756.1 cm, Modello =Appoggiata, Crit.Prog: Acciaio_Pressflessione, $\delta_c = 0.0$ cm:
Verificato

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
302.4	13	12.96	30.24	2.3

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
302.4	13	6.68	25.20	3.8

Travata: 105 [9,16]: L=694.5 cm, Modello =Appoggiata, Crit.Prog: Acciaio_Pressflessione, $\delta_c = 0.0$ cm:
Verificato

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
416.7	13	3.26	27.78	8.5

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
416.7	13	1.79	23.15	13

Travata: 106 [1,8]: L=756.1 cm, Modello =Appoggiata, Crit.Prog: Acciaio_Pressflessione, $\delta_c = 0.0$ cm:

Verificato

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
302.4	13	14.22	30.24	2.1

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
302.4	13	7.35	25.20	3.4

Travata: 106 [8,15]: L=651.8 cm, Modello =Appoggiata, Crit.Prog: Acciaio_Pressflessione, $\delta_c = 0.0$ cm:
Verificato

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
391.1	13	1.68	26.07	16

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
391.1	13	0.95	21.73	23

Travata: 107 [7,25]: L=632.4 cm, Modello =Appoggiata, Crit.Prog: Acciaio_Pressflessione, $\delta_c = 0.0$ cm:
Verificato

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
316.2	13	8.73	25.30	2.9

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
316.2	13	4.45	21.08	4.7

Travata: 101 [13,26]: L=342.5 cm, Modello =Appoggiata, Crit.Prog: Acciaio_Pressflessione, $\delta_c = 0.0$ cm:
Verificato

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
137.0	13	-1.50	13.70	9.1

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
137.0	13	-0.78	11.42	15

Travata: 104 [17,3]: L=460.3 cm, Modello =Appoggiata, Crit.Prog: Acciaio_Pressflessione, $\delta_c = 0.0$ cm:
Verificato

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
276.2	15	0.25	18.41	72

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
92.1	13	-0.23	15.34	66

Travata: 104 [3,6]: L=350.0 cm, Modello =Appoggiata, Crit.Prog: Acciaio_Pressflessione, $\delta_c = 0.0$ cm:
Verificato

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
210.0	13	0.32	14.00	43

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
210.0	13	0.15	11.67	77

Travata: 105 [16,2]: L=461.7 cm, Modello =Appoggiata, Crit.Prog: Acciaio_Pressflessione, $\delta_c = 0.0$ cm:
Verificato

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
92.3	13	-0.25	18.47	75

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
92.3	13	-0.22	15.39	72

Travata: 105 [2,5]: L=350.0 cm, Modello =Appoggiata, Crit.Prog: Acciaio_Pressflessione, $\delta_c = 0.0$ cm:
Verificato

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
210.0	13	0.46	14.00	30

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
175.0	13	0.20	11.67	57

Travata: 106 [15,1]: L=459.8 cm, Modello =Appoggiata, Crit.Prog: Acciaio_Pressflessione, $\delta_c = 0.0$ cm:
Verificato

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
275.9	13	0.26	18.39	71

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
92.0	13	-0.10	15.33	>100

Travata: 106 [1,4]: L=350.0 cm, Modello =Appoggiata, Crit.Prog: Acciaio_Pressflessione, $\delta_c = 0.0$ cm:
Verificato

Verifica spostamento nello stato finale (§4.2.4.2.1 - NTC)

x	Comb.	δ_{max}	L/250.00	Cs
cm		mm	mm	
210.0	13	0.37	14.00	38

Verifica spostamento elastico dovuto ai soli carichi variabili (§4.2.4.2.1 - NTC)

x	Comb.	δ_2	L/300.00	Cs
cm		mm	mm	
210.0	13	0.16	11.67	74